WIND-TUNNEL STUDY OF HARRAH'S BOARDWALK HOTEL CASINO, ATLANTIC CITY

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LIST OF SYMBOLS

Symbol	Definition
U	Local mean velocity
D	Characteristic dimension (building height, width, etc.)
ν, ρ	Kinematic viscosity and density of approach flow
$\frac{UD}{\nu}$	Reynolds number
E	Mean voltage
A, B, n	Constants
U_{rms}	Root-mean-square of fluctuating velocity
E_{rms}	Root-mean-square of fluctuating voltage
U_∞	Reference mean velocity outside the boundary layer
X, Y	Horizontal coordinates
Z	Height above surface
δ	Height of boundary layer
T_u	Turbulence intensity $\frac{U_{rms}}{U_\infty}$ or $\frac{U_{rms}}{U}$
$C_{p_{mean}}$	Mean pressure coefficient, $\frac{(p-p_\infty)_{mean}}{0.5\ \rho\ U_\infty^2}$
$C_{p_{rms}}$	Root-mean-square pressure coefficient, $\frac{\left((p-p_\infty)-(p-p_\infty)_{mean}\right)_{rms}}{0.5\ \rho\ U_\infty^2}$
$C_{p_{max}}$	Peak maximum pressure coefficient, $\frac{(p-p_\infty)_{max}}{0.5\ \rho\ U_\infty^2}$
$C_{p_{min}}$	Peak minimum pressure coefficient, $\frac{(p-p_\infty)_{min}}{0.5\ \rho\ U_\infty^2}$
$(\ )_{min}$	Minimum value during data record
$(\ )_{max}$	Maximum value during data record

Symbol	Definition
p	Fluctuating pressure at a pressure tap on the structure
p_∞	Static pressure in the wind tunnel above the model
F_x, F_y	Forces in X, Y direction
A_R	Reference Area
CF_X	Force coefficient, X direction, $\frac{F_x}{A_R \; 0.5\rho \; U_\infty^2}$
CF_Y	Force coefficient, Y direction, $\frac{F_y}{A_R \; 0.5\rho \; U_\infty^2}$

1. INTRODUCTION

1.1 General

A significant characteristic of modern building design is lighter cladding and more flexible frames. These features produce an increased vulnerability of glass and cladding to wind damage and result in larger deflections of the building frame. In addition, increased use of pedestrian plazas at the base of the buildings has brought about a need to consider the effects of wind and gustiness in the design of these areas.

The building geometry itself may increase or decrease wind loading on the structure. Wind forces may be modified by nearby structures which can produce beneficial shielding or adverse increases in loading. Overestimating loads results in uneconomical design; underestimating may result in cladding or window failures. Tall structures have historically produced unpleasant wind and turbulence conditions at their bases. The intensity and frequency of objectionable winds in pedestrian areas is influenced both by the structure shape and by the shape and position of adjacent structures.

Techniques have been developed for wind tunnel modeling of proposed structures which allow the prediction of wind pressures on cladding and windows, overall structural loading, and also wind velocities and gusts in pedestrian areas adjacent to the building. Information on sidewalk-level gustiness allows plaza areas to be protected by design changes before the structure is constructed. Accurate knowledge of the intensity and distribution of the pressures on the structure permits adequate but economical selection of cladding strength to meet selected maximum design winds and overall wind loads for the design of the frame for flexural control.

Modeling of the aerodynamic loading on a structure requires special consideration of flow conditions in order to guarantee similitude between model and prototype. A detailed discussion of the similarity requirements and their wind-tunnel implementation can be found in references (1), (2), and (3). In general, the requirements are that the model and prototype be geometrically similar, that the approach mean velocity at the building site have a vertical profile shape similar to the full-scale flow, that the turbulence characteristics of the flows be similar, and that the Reynolds number for the model and prototype be equal.

These criteria are satisfied by constructing a scale model of the structure and its surroundings and performing the wind tests in a wind tunnel specifically designed to model atmospheric boundary-layer flows. Reynolds number similarity requires that the quantity UD/ν be similar for model and prototype. Since ν, the kinematic viscosity of air, is identical for both, Reynolds numbers cannot be made precisely equal with reasonable wind velocities. To accomplish this the air velocity in the wind tunnel would have to be as large as the model scale factor times the prototype wind velocity, a velocity which would introduce unacceptable compressibility effects. However, for sufficiently high Reynolds numbers ($>2\times10^4$) the pressure coefficient at any location on the structure will be essentially constant for a large range of Reynolds numbers. Typical values encountered are 10^7-10^8 for the full-scale and 10^5-10^6 for the wind-tunnel model. In this range acceptable flow similarity is achieved without precise Reynolds number equality.

1.2 The Wind-Tunnel Test

The wind-engineering study is performed on a building or building group modeled at scales ranging from 1:150 to 1:400. The building model

is constructed of clear plastic fastened together with screws. The structure is modeled in detail to provide accurate flow patterns in the wind passing over the building surfaces. The building under test is often located in a surrounding where nearby buildings or terrain may provide beneficial shielding or adverse wind loading. To achieve similarity in wind effects the area surrounding the test building is also modeled. A flow visualization study is first made (smoke is used to make the air currents visible) to define overall flow patterns and identify regions where local flow features might cause difficulties in building curtain-wall design or produce pedestrian discomfort.

The test model, equipped with pressure taps (200 to 600 or more), is exposed to an appropriately modeled atmospheric wind in the wind tunnel and the fluctuating pressure at each tap measured electronically. The model, and the modeled area, are rotated 10 or 15 degrees and another set of data recorded for each pressure tap. Normally, 24 or 36 sets of data (360 degrees of turning) are taken; however, when flow visualization or recorded data indicate high pressure regions of small azimuthal extent, data is obtained in smaller azimuthal steps.

Data are recorded, analyzed and processed by an on-line computerized data-acquisition system. Pressure coefficients of several types are calculated by the computer for each reading on each piezometer tap and are printed in tabular form as computer readout. Using wind data applicable to the building site, representative wind velocities are selected for combination with measured pressures on the building model. Integration of test data with wind data results in prediction of peak local wind pressures for design of glass or cladding and may include overall forces and moments on the structure (by floor if desired) for design of

the structural frame. Pressure contours are drawn on the developed building surfaces showing the intensity and distribution of peak wind loads on the building. These results may be used to divide the building into zones where lighter or heavier cladding or glass may be desirable.

Based on the visualization (smoke) tests and on a knowledge of heavy pedestrian use areas, a dozen or more locations may be chosen at the base of the building where wind velocities can be measured to determine the relative comfort or discomfort of pedestrians in plaza areas, near building entrances, near building corners, or on sidewalks. Usually a reference pedestrian position is also tested to determine whether the wind environment in the building area is better or worse than the environment a block or so away in an undisturbed area.

The following pages discuss in greater detail the procedures followed and the equipment and data collecting and processing methods used. In addition, the data presentation format is explained and the implications of the data are discussed.

2. EXPERIMENTAL CONFIGURATION

2.1 Wind Tunnel

Wind-engineering studies are performed in the Fluid Dynamics and Diffusion Laboratory at Colorado State University (Figure 1). Three large wind tunnels are available for wind loading studies depending on the detailed requirements of the study. The wind tunnel used for this investigation is shown in Figure 2. All tunnels have a flexible roof adjustable in height to maintain a zero pressure gradient along the test section. The mean velocity can be adjusted continuously in each tunnel to the maximum velocity available.

2.2 Model

In order to obtain an accurate assessment of local pressures using piezometer taps, models are constructed to the largest scale that does not produce significant blockage in the wind-tunnel test section. The models are constructed of 1/2 in. thick Lucite plastic and fastened together with metal screws. Significant variations in the building surface, such as mullions, are machined into the plastic surface. Piezometer taps (1/16 in. diameter) are drilled normal to the exterior vertical surfaces in rows at several or more elevations between the bottom and top of the building. Similarly, taps are placed in the roof and on any sloping, protruding, or otherwise distinctive features of the building that might need investigation.

Pressure tap locations are chosen so that the entire surface of the building can be investigated for pressure loading and at the same time permit critical examination of areas where experience has shown that maximum wind effects may be expected to occur. Locations of the pressure taps for this study are shown in Figure 3. Dimensions are

given both for full-scale building (in ft) and for model (in in.). The pressure tap numbers are shown adjacent to the taps.

The pressure tests are sometimes made in two stages. In the first stage measurements are made on the initial distribution of pressure taps. If it becomes apparent from the data that the loading on the building is being influenced by some unsuspected geometry of the building or adjacent structures, additional pressure taps are installed in the critical areas. The locations of the taps are selected so that the maximum loading can be detected and the area over which this loading is acting can be defined. Any added taps are also shown in Figure 3.

A circular area 750 to 2000 ft in radius depending on model scale and characteristics of the surrounding buildings and terrain is modeled in detail. Structures within the modeled region are made from styrofoam and cut to the individual building geometries. They are mounted on the turntable in their proper locations. Significant terrain features are included as needed. The model is mounted on a turntable (Figure 2) near the downwind end of the test section. Any buildings or terrain features which do not fit on the turntable are placed on removable pieces which are placed upwind of the turntable for appropriate wind directions. A plan view of the building and its surroundings is shown in Figure 4. The turntable is calibrated to indicate azimuthal orientation to 0.1 degree.

The region upstream from the modeled area is covered with a randomized roughness constructed using various sized cubes placed on the floor of the wind tunnel. Different roughness sizes may be used for different wind directions. Spires are installed at the test-section entrance to provide a thicker boundary layer than would otherwise be

available. The thicker boundary layer permits a somewhat larger scale model than would otherwise be possible. The spires are approximately triangularly shaped pieces of 1/2 in. thick plywood 6 in. wide at the base and 1 in. wide at the top, extending from the floor to the top of the test section. They are placed so that the broad side intercepts the flow. A barrier approximately 8 in. high is placed on the test-section floor downstream of the spires to aid in development of the boundary-layer flow.

The distribution of the roughness cubes and the spires in the roughened area was designed to provide a boundary-layer thickness of approximately 4 ft, a velocity profile power-law exponent similar to that expected to occur in the region approaching the modeled area for each wind direction (a number of wind directions may have the same approach roughness). A photograph of the completed model in the wind tunnel is shown in Figure 5. The wind-tunnel ceiling is adjusted after placement of the model to obtain a zero pressure gradient along the test section.

3. INSTRUMENTATION AND DATA ACQUISITION

3.1 Flow Visualization

Making the air flow visible in the vicinity of the model is helpful (a) in understanding and interpreting mean and fluctuating pressures, (b) in defining zones of separated flow and reattachment and zones of vortex formation where pressure coefficients may be expected to be high and (c) in indicating areas where pedestrian discomfort may be a problem. Titanium tetrachloride smoke is released from sources on and near the model to make the flow lines visible to the eye and to make it possible to obtain motion picture records of the tests. Conclusions obtained from these smoke studies are discussed in Sections 4.1 and 5.1.

3.2 Pressures

Mean and fluctuating pressures are measured at each of the pressure taps on the model structure. Data are obtained for 24 or 36 wind directions, rotating the entire model assembly in a complete circle. Seventy-six pieces of 1/16 in. I.D. plastic tubing are used to connect 76 pressure ports at a time to an 80 tap pressure switch mounted inside the model. The switch was designed and fabricated in the Fluid Dynamics and Diffusion Laboratory to minimize the attenuation of pressure fluctuations across the switch. Each of the 76 measurement ports is directed in turn by the switch to one of four pressure transducers mounted close to the switch. The four pressure input taps not used for transmitting building surface pressures are connected to a common tube leading outside the wind tunnel. This arrangement provides both a means of performing in-place calibration of the transducers and, by connecting this tube to a pitot tube mounted inside the wind tunnel, a means of automatically monitoring the tunnel speed. The switch is operated by means of a shaft projecting through

the floor of the wind tunnel. A computer-controlled stepping motor steps the switch into each of the 20 required positions. The computer keeps track of switch position but a digital readout of position is provided at the wind tunnel.

The pressure transducers used are setra differential transducers (Model 237) with a 0.10 psid range. Reference pressures are obtained by connecting the reference sides of the four transducers, using plastic tubing, to the static side of a pitot-static tube mounted in the wind tunnel free stream above the model building. In this way the transducer measures the instantaneous difference between the local pressures on the surface of the building and the static pressure in the free stream above the model.

Output from the pressure transducers is fed to an on-line data acquisition system consisting of a Hewlett-Packard 21 MX computer, disk unit, card reader, printer, Digi-Data digital tape drive and a Preston Scientific analog-to-digital converter. The data are processed immediately into pressure coefficient form as described in Section 4.3 and stored for printout or further analysis.

All four transducers are recorded simultaneously for 16 seconds at a 250 sample per second rate. The results of an experiment to determine the length of record required to obtain stable mean and rms (root-mean-square) pressures and to determine the overall accuracy of the pressure data acquisition system is shown in Figure 6. A typical pressure port record was integrated for a number of different time periods to obtain the data shown. Examination of a large number of pressure taps showed that the overall accuracy for a 16 second period is, in pressure coefficient form, 0.03 for mean pressures, 0.1 for peak pressures, and 0.01 for rms pressures. Pressure coefficients are defined in Section 4.3.

3.3 Velocity

Mean velocity and turbulence intensity profiles are measured upstream of the model to determine that an approach boundary-layer flow appropriate to the site has been established. Tests are made at one wind velocity in the tunnel. This velocity is well above that required to produce Reynolds number similarity between the model and the prototype as discussed in Section 1.1.

In addition, mean velocity and turbulence intensity measurements are made 5 to 7 ft (prototype) above the surface at a dozen or more locations on and near the building for 16 wind directions. The measurement locations are shown on Figure 4. The surface measurements are indicative of the wind environment to which a pedestrian at the measurement location would be subjected. The locations are chosen to determine the degree of pedestrian comfort or discomfort at the building corners where relatively severe conditions frequently are found, near building entrances and on adjacent sidewalks where pedestrian traffic is heavy, and in open plaza areas. In most studies a reference pedestrian position, located about a block away, is also tested. These data are helpful in evaluating the degree of pedestrian comfort or discomfort in the proposed plaza area in terms of the undisturbed environment in the immediate vicinity.

Measurements are made with a single hot-wire anemometer mounted with its axis vertical. The instrumentation used is a Thermo Systems constant temperature anemometer (Model 1050) with a 0.001 in. diameter platinum film sensing element 0.020 in. long. Output is directed to the on-line data acquisition system for analysis.

Calibration of the hot-wire anemometer is performed by comparing output with the pitot-static tube in the wind tunnel. The calibration

data are fit to a variable exponent King's Law relationship of the form

$$E^2 = A + BU^n$$

where E is the hot-wire output voltage, U the velocity and A, B, and n are coefficients selected to fit the data. The above relationship was used to determine the mean velocity at measurement points using the measured mean voltage. The fluctuating velocity in the form U_{rms} (root-mean-square velocity) was obtained from

$$U_{rms} = \frac{2\ E\ E_{rms}}{B\ n\ U^{n-1}}$$

where E_{rms} is the root-mean-square voltage output from the anemometer. For interpretation all turbulence measurements for pedestrian winds were divided by the mean velocity outside the boundary-layer U_∞. Turbulence intensity in velocity profile measurements used the local mean velocity.

4. RESULTS

4.1 Flow Visualization

A film is included as part of this report showing the characteristics of flow about the structure using smoke to make the flow visible. A listing of the contents of the film is shown in Table 1. Several features can be noted from the visualization. As with all large structures, wind approaching the building is deflected down to the plaza level, up over the structure and around the sides. A description of the smoke test results emphasizing flow patterns of concern relative to possible high-wind load areas and pedestrian comfort is given in Section 5.1.

4.2 Velocity

Velocity and turbulence profiles are shown in Figure 7. Profiles were taken upstream from the model which are characteristic of the boundary layer approaching the model and sometimes at the building site with building removed. The boundary-layer thickness, δ, is shown in Figure 7. The corresponding prototype value of δ for this study is also shown in the figure. This value was established as a reasonable height for this study. The mean velocity profile approaching the modeled area has the form

$$\frac{U}{U_\infty} = \left(\frac{z}{\delta}\right)^n .$$

The exponent n for the approach flow established for this study is shown in Figure 7.

Profiles of longitudinal turbulence intensity in the flow approaching the modeled area are shown in Figure 7. The turbulence intensities are appropriate for the approach mean velocity profile selected. For the velocity profiles, turbulence intensity is defined

as the root-mean-square about the mean of the longitudinal velocity fluctuations divided by the local mean velocity U,

$$Tu = \frac{U_{rms}}{U} .$$

Velocity data obtained at each of the pedestrian measurement locations shown in Figure 4 are listed in Table 2 as mean velocity U/U_∞, turbulence intensity U_{rms}/U_∞, and largest effective gust

$$U_{pk} = \frac{U + 3U_{rms}}{U_\infty} .$$

These data are plotted in polar form in Figure 8. Measurements were taken 5 to 7 ft above the ground surface. A site map is superimposed on the polar plots to aid in visualization of the effects of the nearby structures on the velocity and turbulence magnitudes. An analysis of these wind data is given in Section 5.2.

To enable a quantitative assessment of the wind environment, the wind-tunnel data were combined with wind frequency and direction information obtained at the local airport. Table 3 shows wind frequency by direction and magnitude obtained from summaries published by the National Weather Service. These data, usually obtained at an elevation of about 30-40 ft, were converted to velocities at the reference velocity height for the wind-tunnel measurements and combined with the wind-tunnel data to obtain cumulative probability distributions (percent time a given velocity is exceeded) for wind velocity at each measuring location. The percentage times were summed by wind direction to obtain a percent time exceeded at each measuring position independent of wind direction (but accounting for the fact that the wind blows from different directions with varying frequency). These results are plotted in Figure 9.

Interpretation of Figure 9 is aided by a description of the effects of wind of various magnitudes on people. The earliest quantitative description of wind effects was established by Sir Francis Beaufort in 1806 for use at sea and is still in use today. Several recent investigators have added to the knowledge of wind effects on pedestrians. These investigations along with suggested criteria for acceptance have been summarized by Penwarden and Wise (4) and Melbourne (5). The Beaufort scale (from ref. 4), based on mean velocity only, is reproduced as Table 4 including qualitative descriptions of wind effects. Table 4 suggests that mean wind speeds below 12 mph are of minor concern and that mean speeds above 24 mph are definitely inconvenient. Quantitative criteria for acceptance from reference 5 are superimposed as dashed lines on Figure 9. The peak gust curves shown in Figure 9 are the percent of time during which a short gust of the stated magnitude could occur (say about one of these gusts per hour). Implications of the data plotted in Figure 9 are presented in Section 5.2

Because some pedestrian wind measuring positions are purposely chosen at sites where the smoke tests showed large velocities of small spacial extent, the general wind environment about the structure may be less severe than one might infer from a strict analysis of Table 2 and Figure 9.

4.3 Pressures

For each of the pressure taps examined at each wind direction, the data record is analyzed to obtain four separate pressure coefficients. The first is the mean pressure coefficient

$$C_{p_{mean}} = \frac{(p-p_\infty)_{mean}}{0.5\ \rho\ U_\infty^2}$$

where the symbols are as defined in the List of Symbols. It represents the mean of the instantaneous pressure difference between the building pressure tap and the static pressure in the wind tunnel above the building model, nondimensionalized by the dynamic pressure

$$0.5\ \rho\ U_\infty^2$$

at the reference velocity position. This relationship produces a dimensionless coefficient which indicates that the mean pressure difference between building and ambient wind at a given point on the structure is some fraction less or some fraction greater than the undisturbed wind dynamic pressure near the upper edge of the boundary layer. Using the measured coefficient, prototype mean pressure values for any wind velocity may be calculated.

The magnitude of the fluctuating pressure is obtained by the rms pressure coefficient

$$C_{p_{rms}} = \frac{\left((p-p_\infty) - (p-p_\infty)_{mean}\right)_{rms}}{0.5\ \rho\ U_\infty^2}$$

in which the numerator is the root-mean-square of the instantaneous pressure difference about the mean .

If the pressure fluctuations followed a Gaussian probability distribution, no additional data would be required to predict the

frequency with which any given pressure level would be observed. However, the pressure fluctuations do not, in general, follow a Gaussian probability distribution so that additional information is required to show the extreme values of pressure expected. The peak maximum and peak minimum pressure coefficients are used to determine these values:

$$C_{p_{max}} = \frac{(p-p_\infty)_{max}}{0.5\ \rho\ U_\infty^2}$$

$$C_{p_{min}} = \frac{(p-p_\infty)_{min}}{0.5\ \rho\ U_\infty^2}$$

The values of $p-p_\infty$ which were digitized at 250 samples per second for 16 seconds, representing about one hour of time in the full-scale, are examined individually by the computer to obtain the most positive and most negative values during the 16-second period. These are converted to $C_{p_{max}}$ and $C_{p_{min}}$ by nondimensionalizing with the free stream dynamic pressure.

The four pressure coefficients are calculated by the on-line data acquisition system computer and tabulated along with the approach wind azimuth in degrees from true north. The list of coefficients is included as Appendix A. The pressure tap code numbers used in the appendix are explained in Figure 3.

To determine the largest peak loads acting at any point on the structure for cladding design purposes, the pressure coefficients for all wind directions were searched to obtain, at each pressure tap, the largest absolute value of peak pressure coefficient. Table 6 provides these pressure coefficients and associated wind directions. Included in Section 5.3 is an analysis of the coefficients of Table 6 including the maximum values obtained and where they occurred on the building.

The pressure coefficients of Table 6 can be converted to full-scale loads by multiplication by a suitable reference pressure selected for the field site. This reference pressure is represented in the equations for pressure coefficients by the $0.5\ \rho\ U_\infty^2$ denominator. This value is the dynamic pressure associated with an hourly mean wind at the reference velocity measurement position at the edge of the boundary layer. In general, the method of arriving at a design reference pressure for a particular site involves selection of a design wind velocity, translation of the velocity to an hourly mean wind at the reference velocity location and conversion to a reference pressure. Selection of the design velocity can be made from statistical analysis of extreme wind data or selected from wind maps contained in the proposed wind loading code ANSI A58.1 of the American National Standards Institute (6). The calculation of reference pressure for this study is shown in Table 5. The factor used in Table 5 to reduce gust winds to hourly mean winds is given in reference (7).

The reference pressure associated with the design hourly mean velocity at the reference velocity location can be used directly with the peak-pressure coefficients to obtain peak local design wind loads for cladding design. Local, instantaneous peak loads on the full-scale building suitable for cladding design were computed by multiplying the reference pressure of Table 5 by the peak coefficients of Table 6 and are listed as peak pressures in that table. The maximum psf load given at each tap location is the absolute value of the maximum value found in the tests, irrespective of its algebraic sign. For ease in visualizing the loads on the structure, contours of equal peak pressures for cladding load shown in Table 6 have been plotted on developed elevation

views of the structure, Figure 10. For control of water infiltration from outside to inside, the largest positive (inward-acting) pressure at each tap location is tabulated in Table 6.

For glass design pressures, a glass load factor is used to account for the different duration between measured peak pressures and the one minute loading commonly used in glass design charts. The design pressure used for glass is normally less than the peak pressures used for cladding design because of the static fatigue property of glass which can withstand higher pressures for short duration loads than for long duration loads. Recent research (8) indicates that the period of application of the peak pressures reported herein is about 5-10 seconds or less. If a glass design is based on these peak-pressure values, then a glass strength associated with this duration load should be used. Because glass design charts are normally based on some alternate load duration--usually one minute--then some reduction in peak loads should be made. An estimate of a load reduction factor can be obtained from an empirical relation of glass strength as a function of load duration. Current glass selection charts showing glass strength as a function of load duration (9) and older references (10) indicate the following load reduction factors:

	ref 9	ref 10
annealed float	0.80	0.81
heat strengthened	0.94	
tempered	0.97	0.98

Loadings appropriate for glass design can be computed by multiplying the peak-pressure loads of Table 6 by these load factors.

4.4 Forces and Moments

Force coefficients in the horizontal X and Y directions and moment coefficients about the X, Y, and Z axes with the origin at ground level at the base of the building with Z axis vertical may be computed for all wind directions tested by integration of mean pressures on the building. Overall forces and moments acting on the full-scale building due to wind loading which are useful in designing the structural framing of the proposed building may be obtained from use of these coefficients.

Force coefficients were computed for each floor for each wind direction using the equations shown below.

$$CF_X = \frac{F_X}{A_R \; 0.5 \; \rho \; U_\infty^2} \qquad CF_Y = \frac{F_Y}{A_R \; 0.5 \; \rho \; U_\infty^2}$$

Terms and symbols used in the equations are defined in the List of Symbols and the axes are defined for the building in Figure 3. Force coefficients CF_X and CF_Y were computed for the horizontal forces acting along the X and Y axes using the mean pressure coefficient at each pressure tap. A_R represents a constant reference area for nondimensionalization of the forces and moments.

The total forces acting on the full-scale building for each floor and wind direction were computed by multiplying the above coefficients by the appropriate full-scale reference area, by the reference pressure of Table 5, and by a gust load factor selected for an appropriate wind gust duration. The gust load factor, shown in Table 5, was selected to increase the loads from an hourly mean load to that of a gust whose duration would be sufficient for its effect to be fully felt by the structure. A table of gust load factors for various gust durations is

incorporated in Table 5 so that force and moment data of Table 7 may be adjusted to a different load duration if desired.

The forces obtained at each floor were used to obtain load, shear, and moment diagrams for the building for each wind direction. The shear diagram, in kips, was obtained by algebraic sum of all forces in each coordinate direction acting above the floor of interest. The load diagram, in psf, was obtained by dividing the shear values by their contributing areas (listed in Table 7). The moment diagram, in 1000 ft-kips, was obtained by integration of the shear values so that the moment due to forces acting above the floor level of interest was calculated. The sign of the moment was established by the right-hand rule about an X', Y' axis through the floor of interest. Moments about the Z axis were calculated by considering the displacement of forces in the X and Y directions from the Z axis shown in Figure 3. Load, shear, and moment diagrams are shown in Figure 11 for several wind directions.

5. DISCUSSION

5.1 Flow Visualization

Flow patterns identified with smoke did not show characteristics which would indicate exceptionally high pressures on the building. The slots on the corners of the tower did not appear to adversely affect flow patterns. Wind velocities in the slots were low except near the top where a significant upward velocity was evident for some wind velocities. Wind flows over the sloping terrace areas appeared to be moderate; partitions between terraces were apparently active in reducing wind speeds on the terraces. The wall on the diagonal between terraces near the south corner of the tower was important in keeping terrace velocities low--particularly where the wall joins the building. Velocities on the flat terrace area between the tower and boardwalk and on the boardwalk area appeared to be low to moderate. The roof area between the tower and theater stage loft appeared to have high winds for most approach wind directions. Velocities in the entrance area beneath the overhang on the northwest side were generally low to moderate although moderate to high winds were in evidence for some wind directions in the area near pedestrian locations 13 and 15 (see Figure 4).

5.2 Pedestrian Winds

Figure 4 shows the 22 pedestrian locations selected for investigation of pedestrian wind comfort. Location 1 was selected as a reference location which should be reasonably undisturbed by presence of the Harrah's Boardwalk Hotel Casino building. Locations

10, 11, 12, and 15 were located at ground level underneath the building overhang. Locations 17, 18 and 19 were located on terraces while locations 20, 21 and 22 were located on the open roof areas. Table 2 and Figure 8 show that the largest values of mean velocity were measured at locations 13 and 14 with values of 50 to 60 percent of the velocity U_∞ at the boundary layer height measured for 4 wind directions at each location. These are not large, comparing with a largest value of 50 percent at reference location 1 and about 45 percent expected in an open-country environment.

The largest values of fluctuating velocity, U_{rms}, were between 17 and 28 percent of U_∞ measured for several wind directions each at locations 2, 5 and 14. For comparison, reference location 1 had a maximum value of 11 percent which is typical of an open-country environment. The largest values of peak gust, represented by the mean plus three rms as discussed in section 4.2, were obtained at locations 5 and 14 with values of 113 and 107 percent of U_∞. These values are only moderately above the 77 percent measured at reference location 1 and the 80-90 percent expected in an open-country environment.

Velocity data of Table 2 integrated with local wind data of Table 3 are shown in Figure 9. Based on the data of this Figure, the windiest locations will be at locations 13 and 14 where comfort criteria will be exceeded for long exposure activities 10 to 20 percent of the time for mean winds. Comfort criteria for short exposure at these locations will be exceeded about 1 percent of the time. Most locations did not exceed the comfort criteria for long exposure for a significant percentage of time.

The results of the pedestrian wind analysis showed that all measured areas had acceptable wind environments and would not likely be considered as uncomfortable due to winds.

5.3 Pressures

Table 6 shows the largest pressure coefficients and corresponding loads measured on the building for each pressure tap location. Data listed as Configuration A in Table 6 and Appendix A represent data obtained at all tap locations for 36 wind directions including the presence of the proposed large structure to the northeast shown in the photograph of Figure 5. The Configuration A data includes pressures measured on portions of two adjacent buildings shown in Figures 3 and 4. Data listed as Configuration B represent data obtained at selected taps on the Harrah's building at selected wind directions without the presence of the large proposed building to the northeast to determine the influence of that building on the pressures on the Harrah's building. Comparisons between data for Configurations A and B are shown in Table 6. Data listed as Configuration C in Table 6 and Appendix A represent data obtained on the two adjacent buildings for which data was obtained in Configuration A but with the Harrah's building removed. The purpose of this data was to determine the impact of Harrah's on local pressure loads on these buildings. Comparison of Configuration A and C data are presented in Table 6.

The largest pressure coefficients measured on the Harrah's building for Configuration A were -2.68 and -2.65 at taps 1136 and 2510 for wind azimuths of 150 and 220 degrees respectively. These pressure coefficients correspond to pressures of 129 and 127 psf for

the 100-yr recurrence wind selected in Table 5. As shown in Figure 10, most areas of the building had 100-yr recurrence pressures ranging from 45 to 75 psf. Figure 11 shows the load, shear and moment diagrams for the two wind directions where base shear as calculated in Table 7 was near a maximum for the X and Y coordinate directions (see Figure 3 for coordinate system).

Data for Configuration B showed that the peak pressure coefficient at tap 1136 increased to -3.2 corresponding to a 154 psf load for a 100-yr recurrence wind without the presence of the proposed building to the northeast. More than one half of the taps measured with and without the proposed building in place showed higher pressures with the building in place.

Comparison of data for the two adjacent buildings for which data was obtained with Harrah's in place (Configuration A) and without Harrah's in place (Configuration C) showed that the predominant influence of Harrah's was to increase local pressures on the adjacent buildings (see Table 6). Some tap locations did show a decrease in pressure due to the presence of the Harrah's building.

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FIGURES

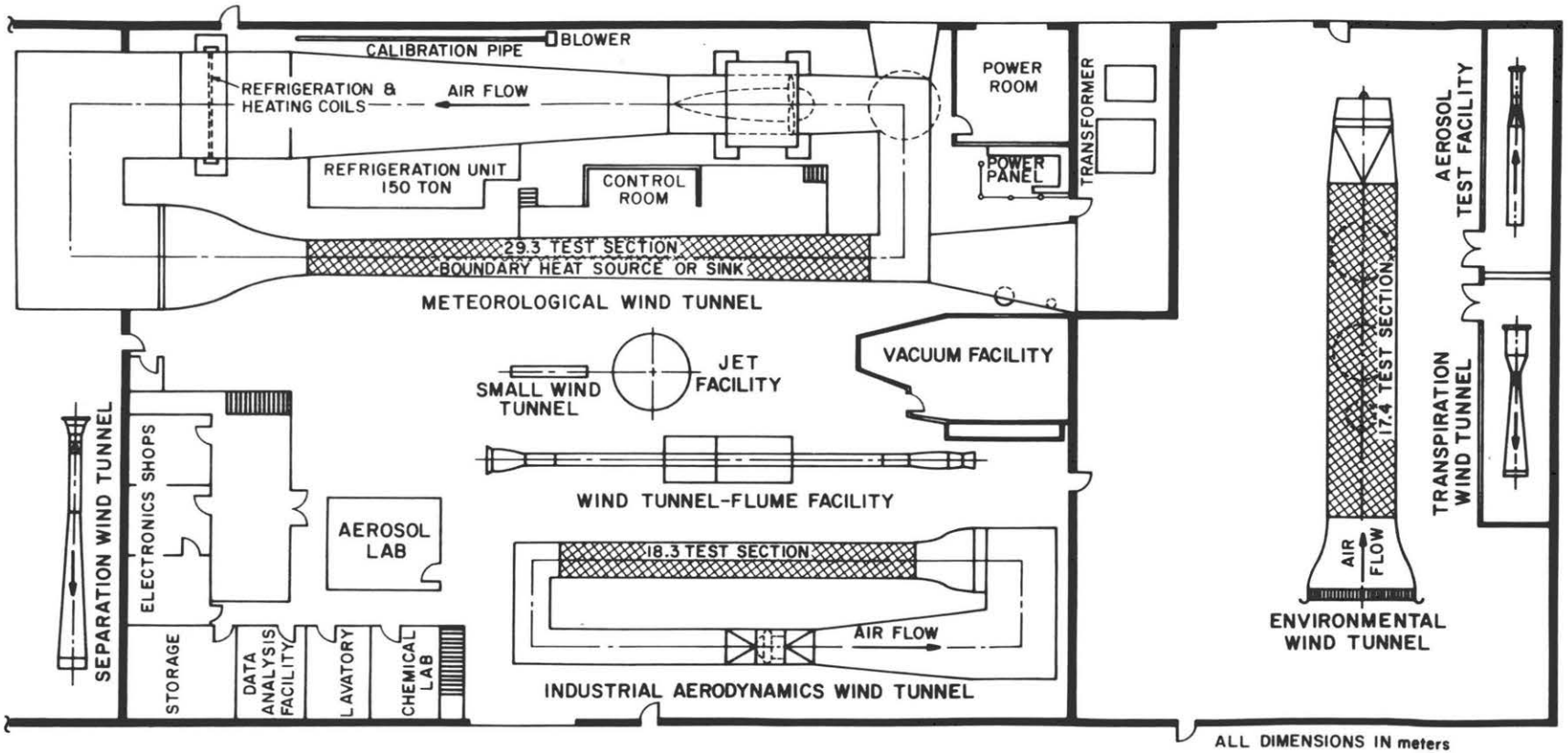
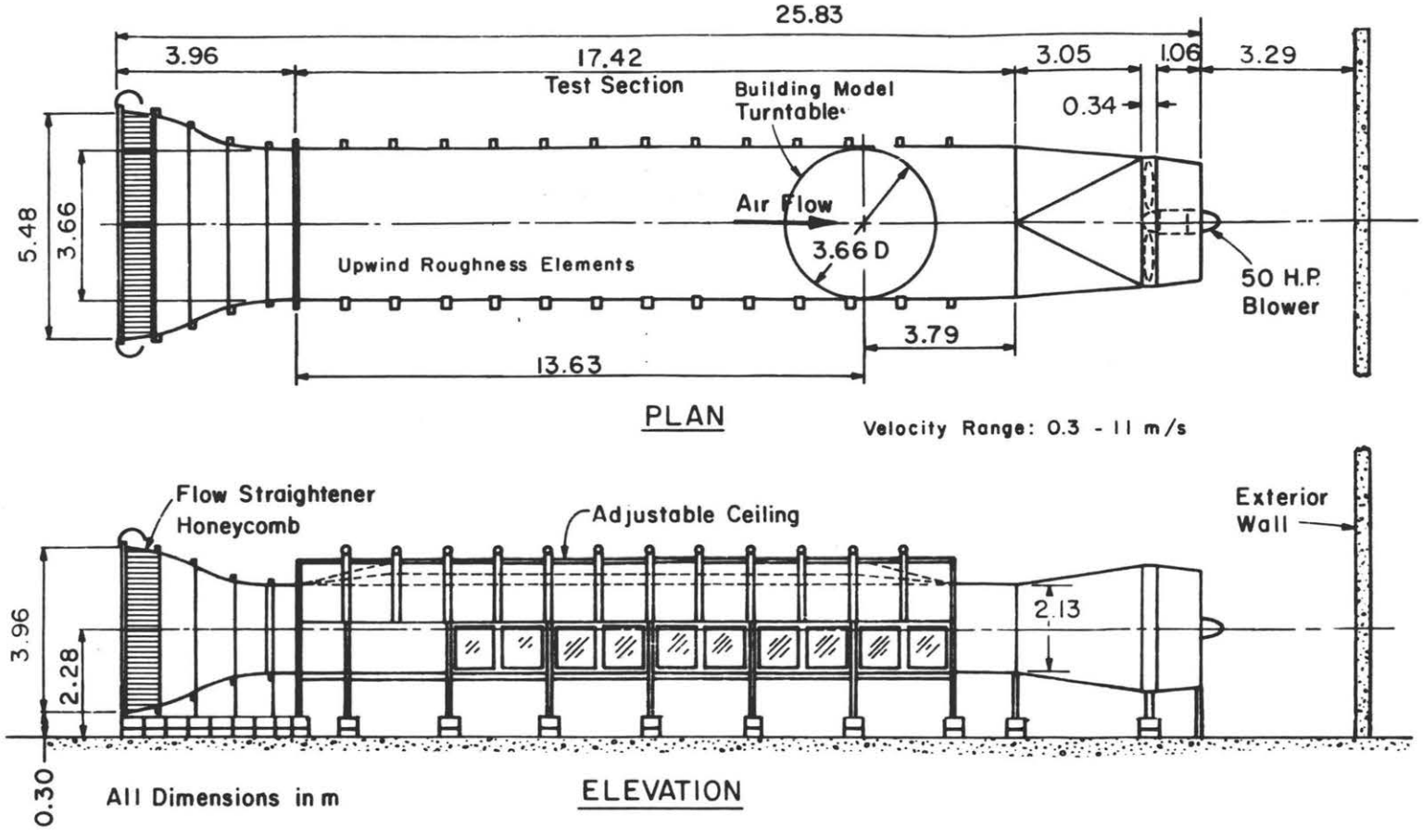
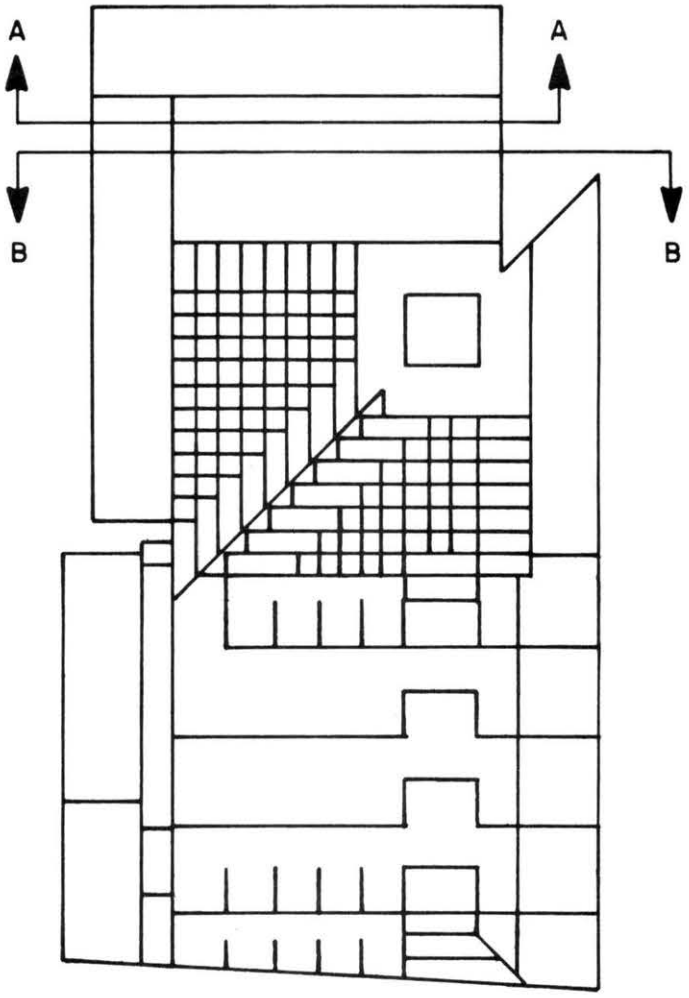


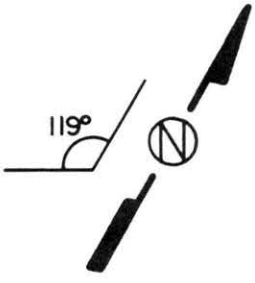
FIGURE 1 - FLUID DYNAMICS AND DIFFUSION LABORATORY
COLORADO STATE UNIVERSITY



ENVIRONMENTAL WIND TUNNEL

Figure 2 - Wind Tunnel Configuration





MODEL SCALE = 1/300
TOTAL TAPS = 474
DIMENSIONS IN FULL SCALE FEET
AND MODEL INCHES.

Figure 3a. Pressure Tap Locations

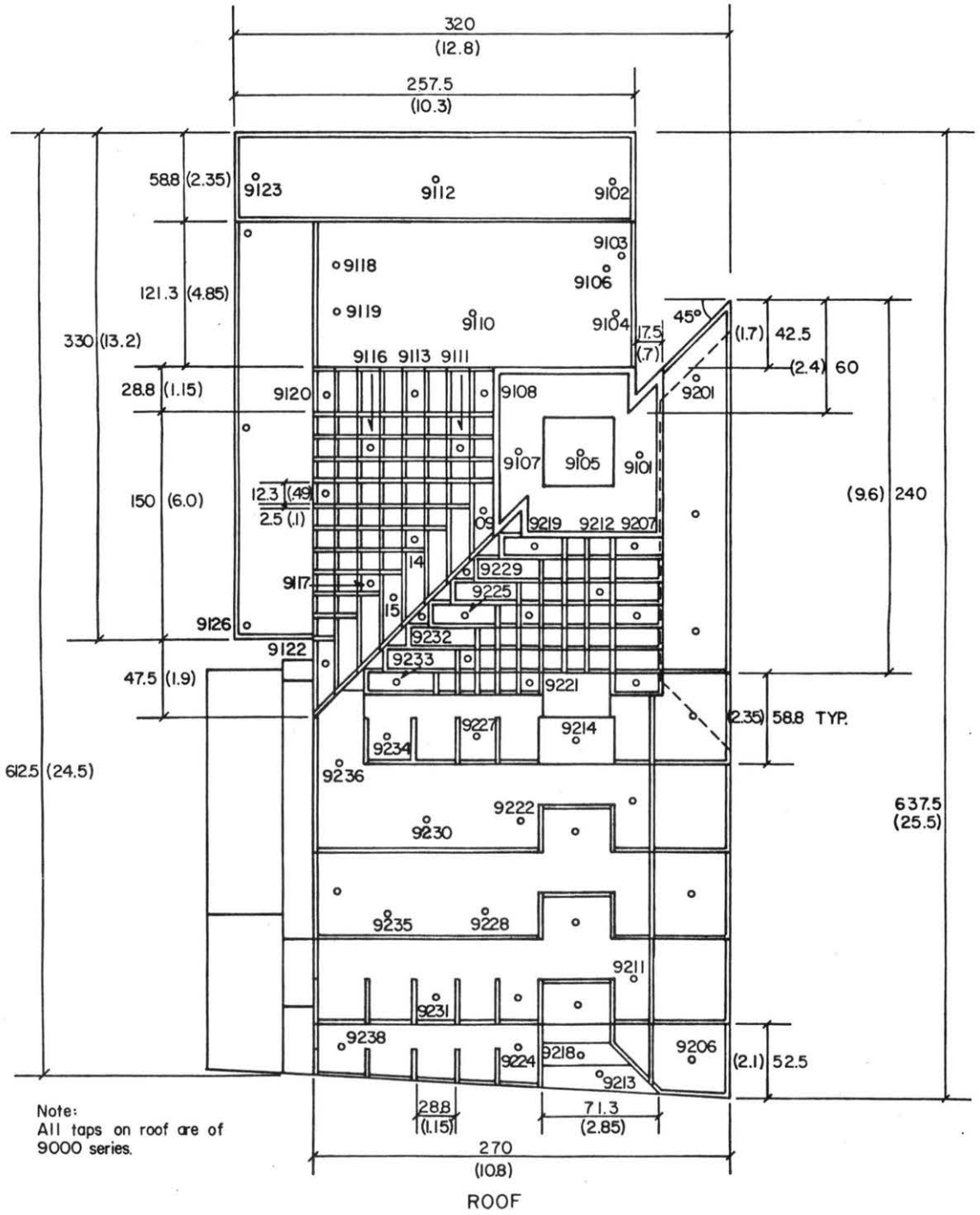


Figure 3b. Pressure Tap Locations

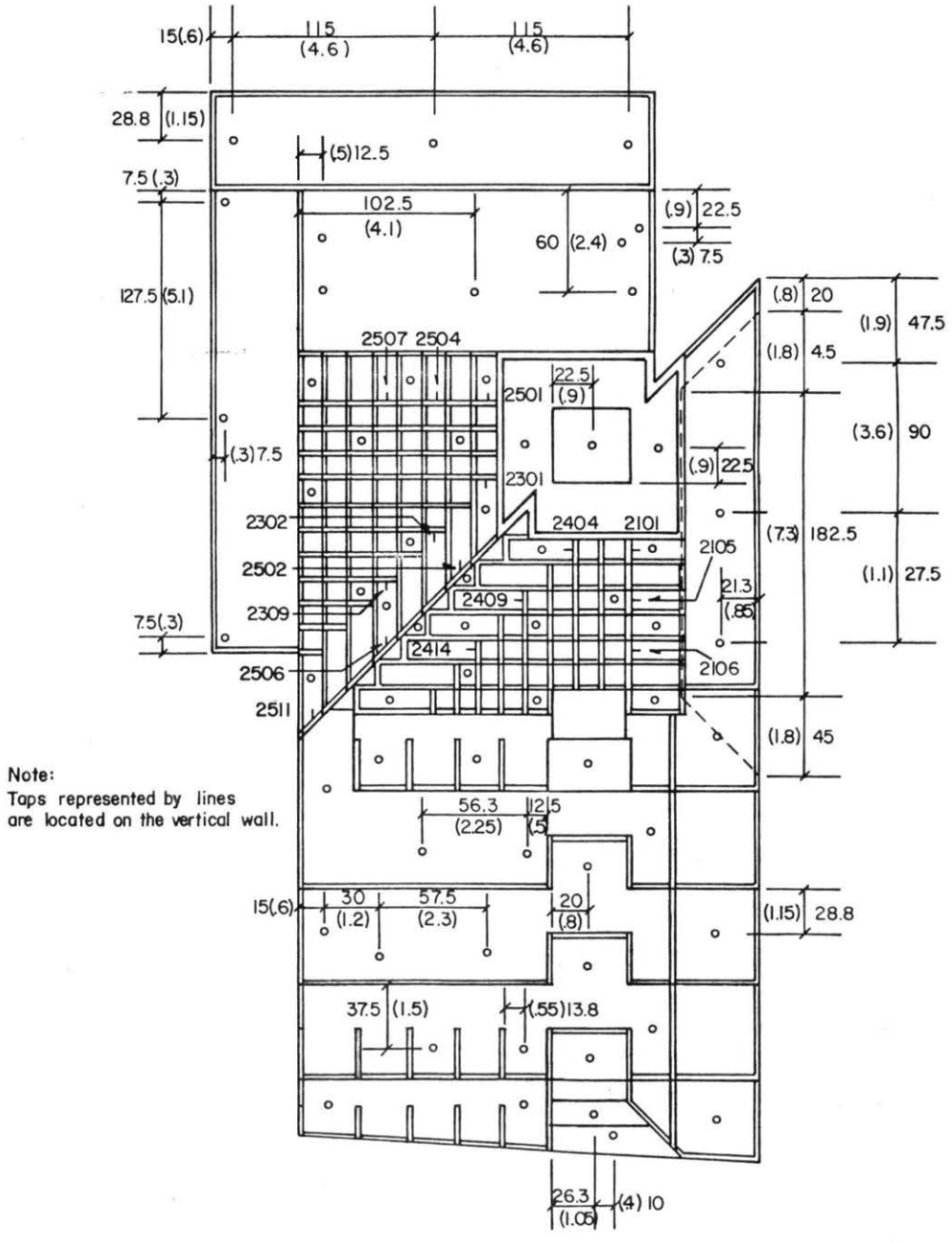


Figure 3c. Pressure Tap Locations

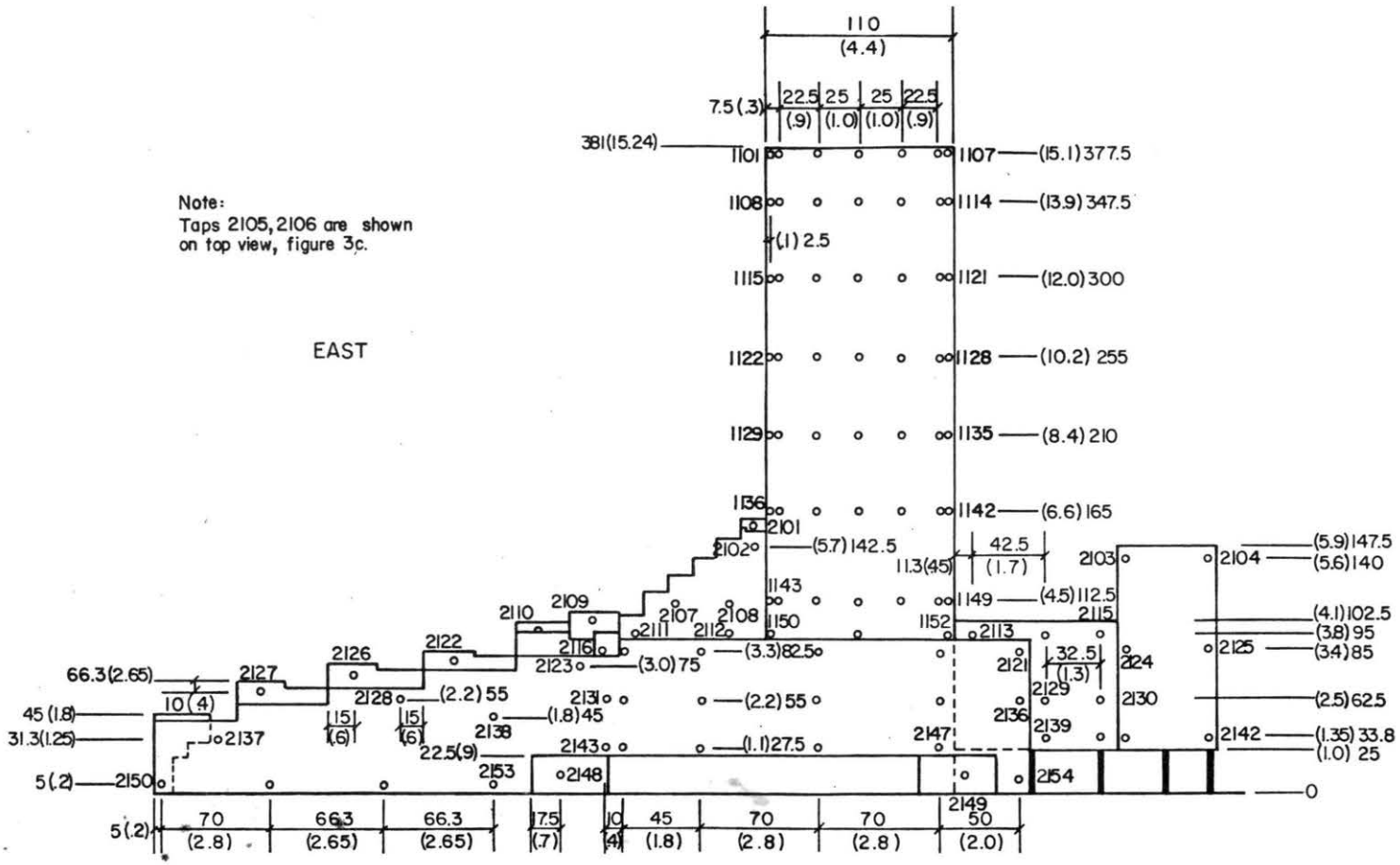


Figure 3d. Pressure Tap Locations

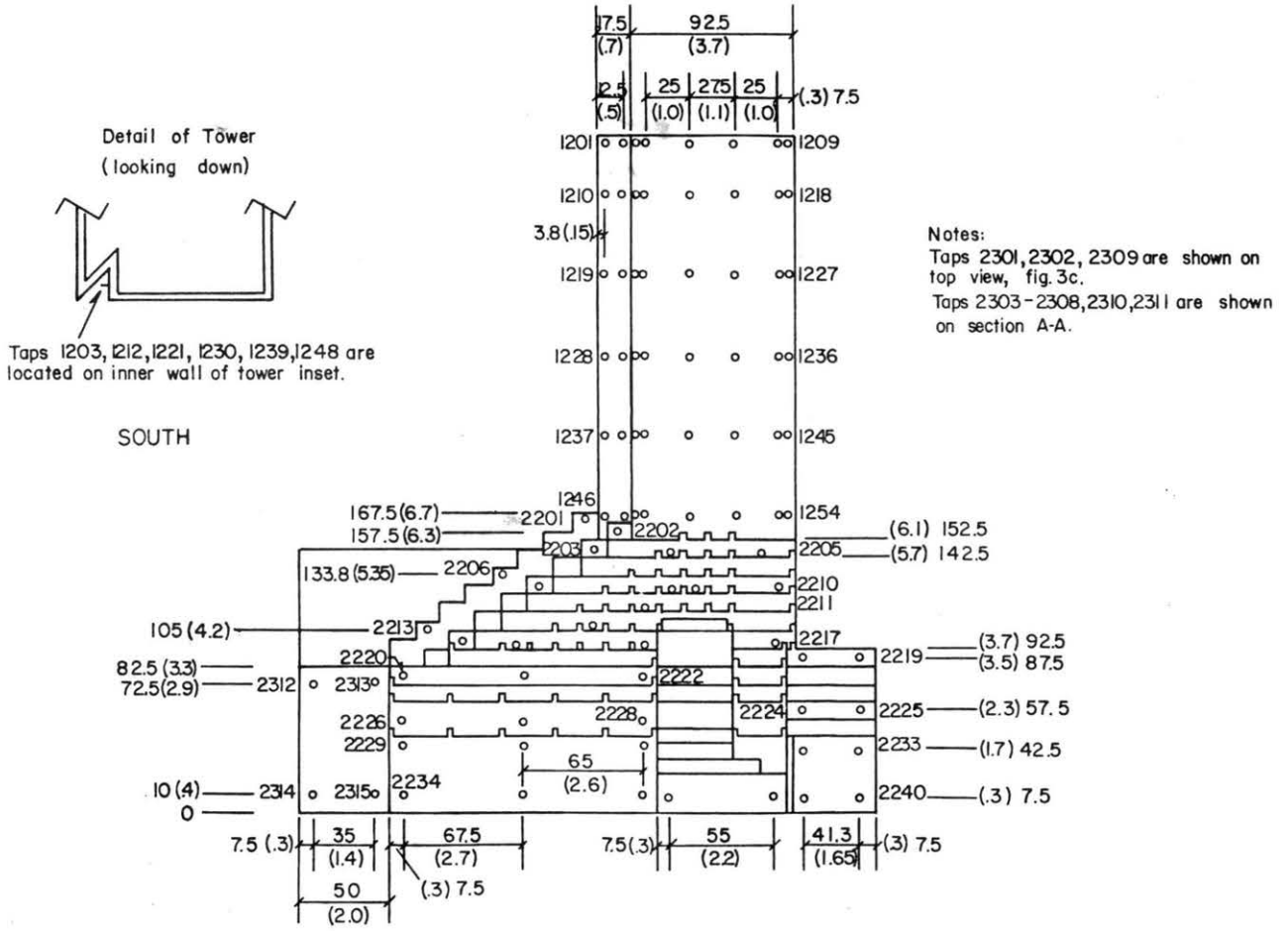
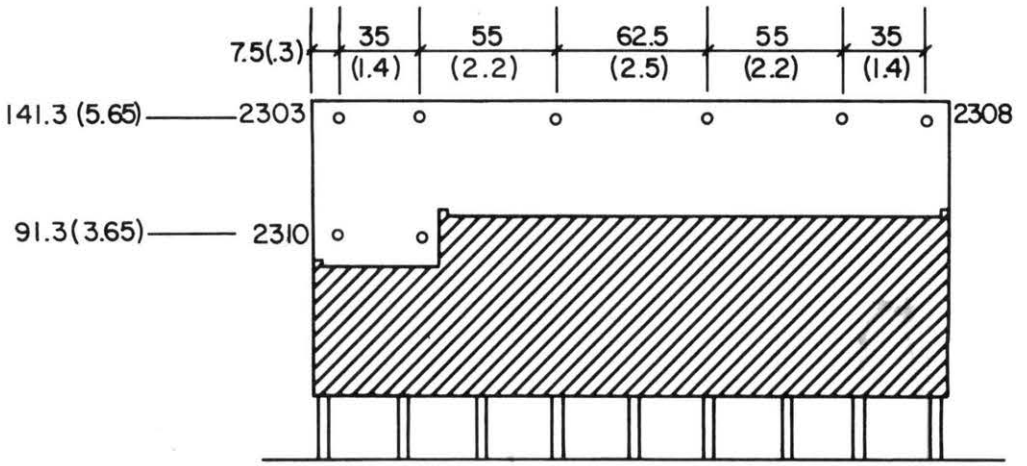


Figure 3e. Pressure Tap Locations



SECTION A-A

Figure 3f. Pressure Tap Locations

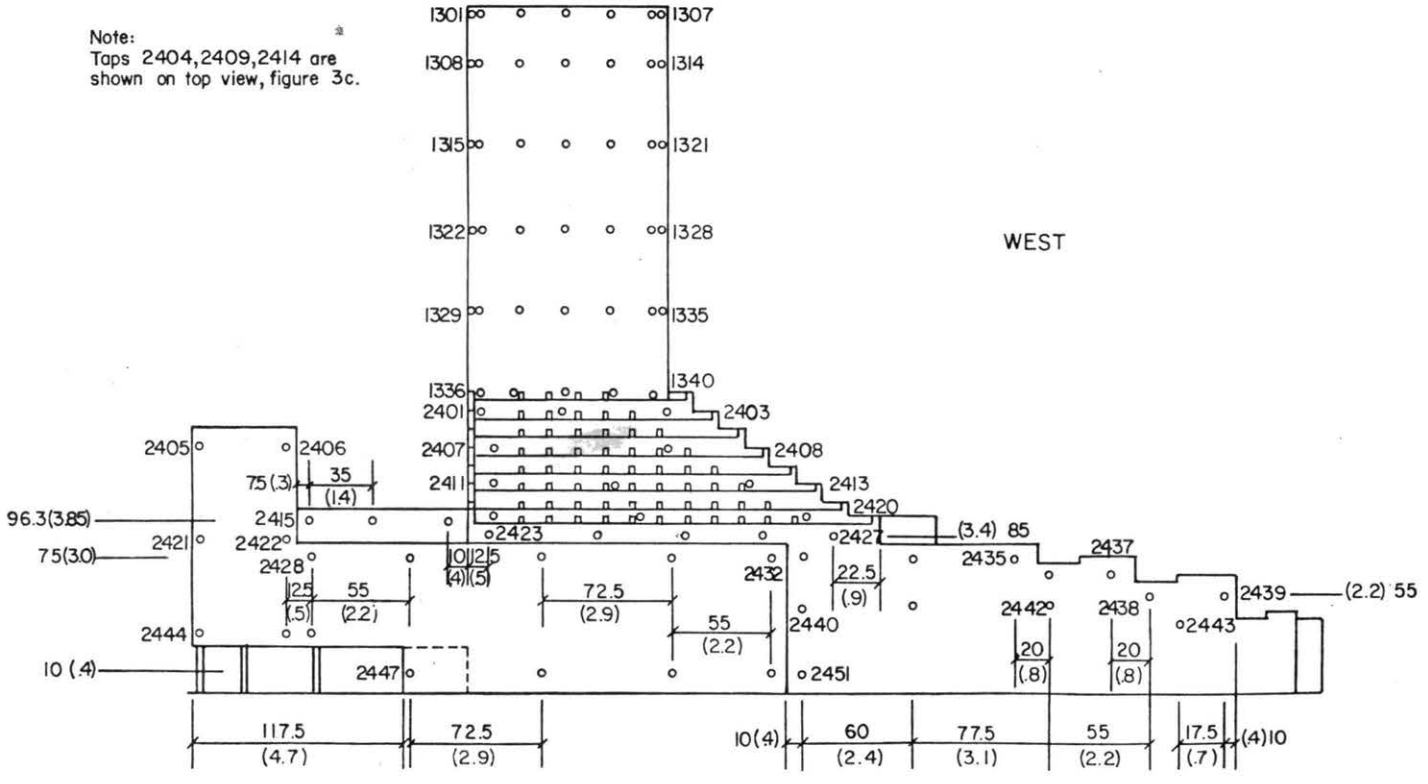
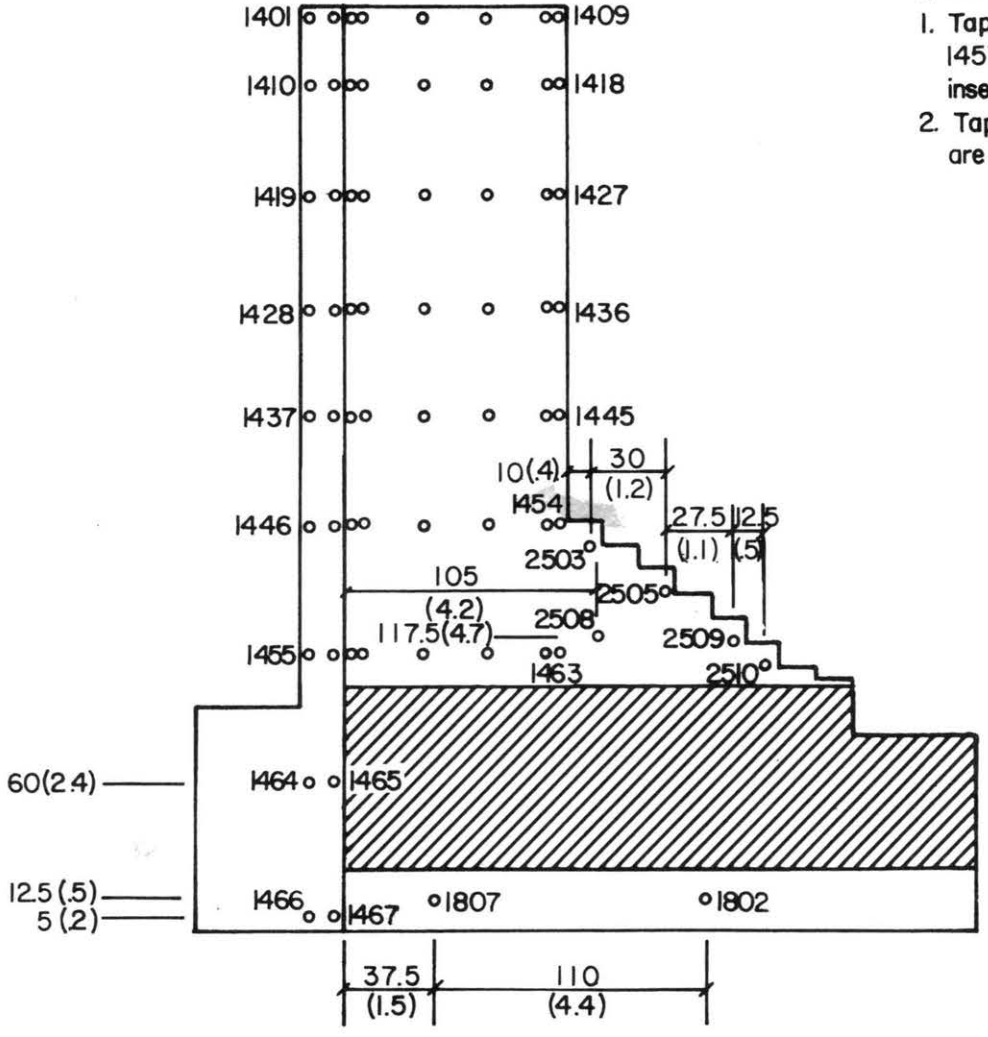


Figure 3g. Pressure Tap Locations



Notes

1. Taps 1403, 1412, 1421, 1430, 1439, 1448, 1457 are located on inner wall of tower inset. (See detail - fig.3e.)
2. Taps 2501, 2502, 2504, 2506, 2507, 2511 are shown on top view, figure 3c.

SECTION B-B

Figure 3h. Pressure Tap Locations

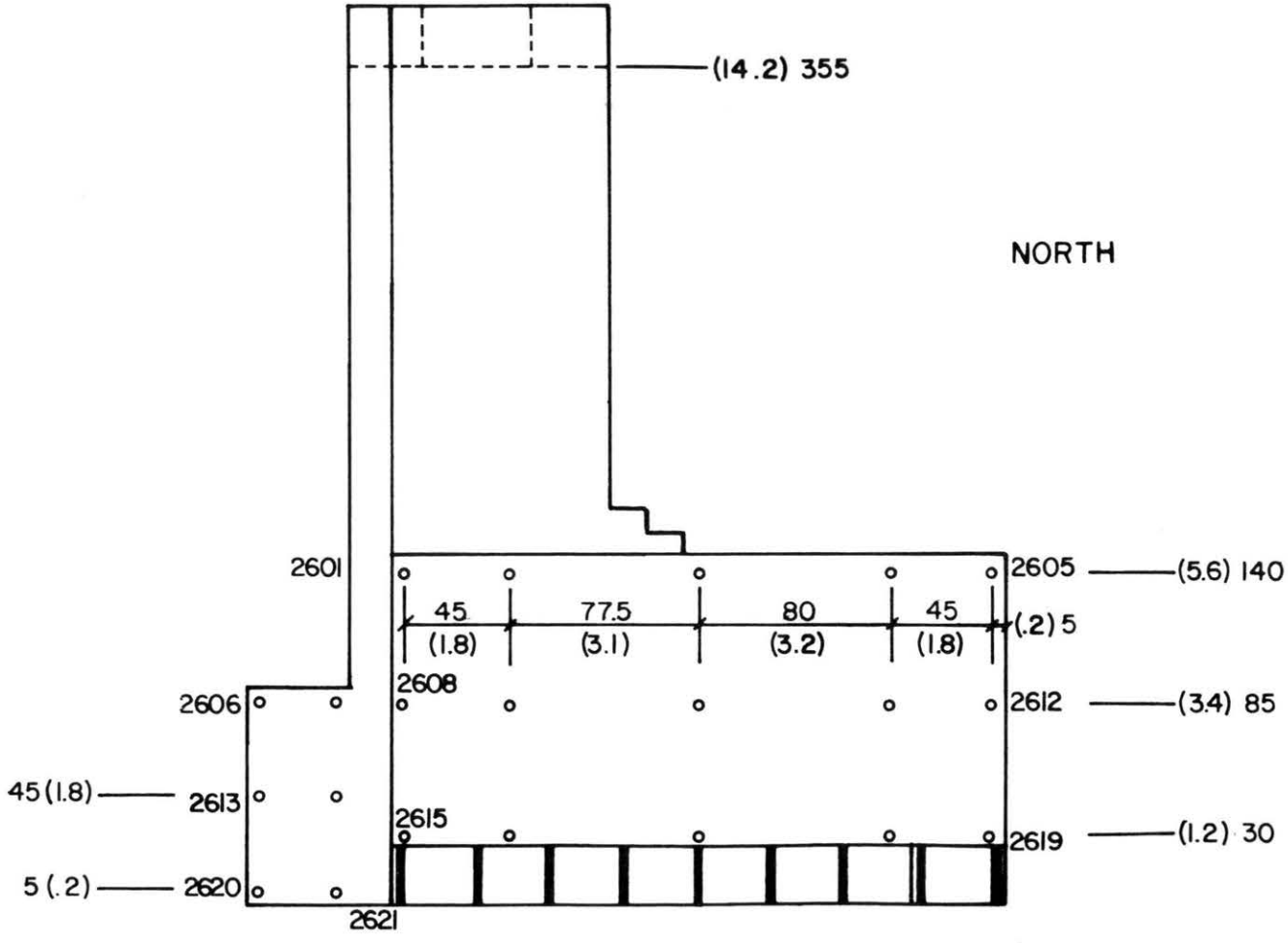


Figure 3i. Pressure Tap Locations

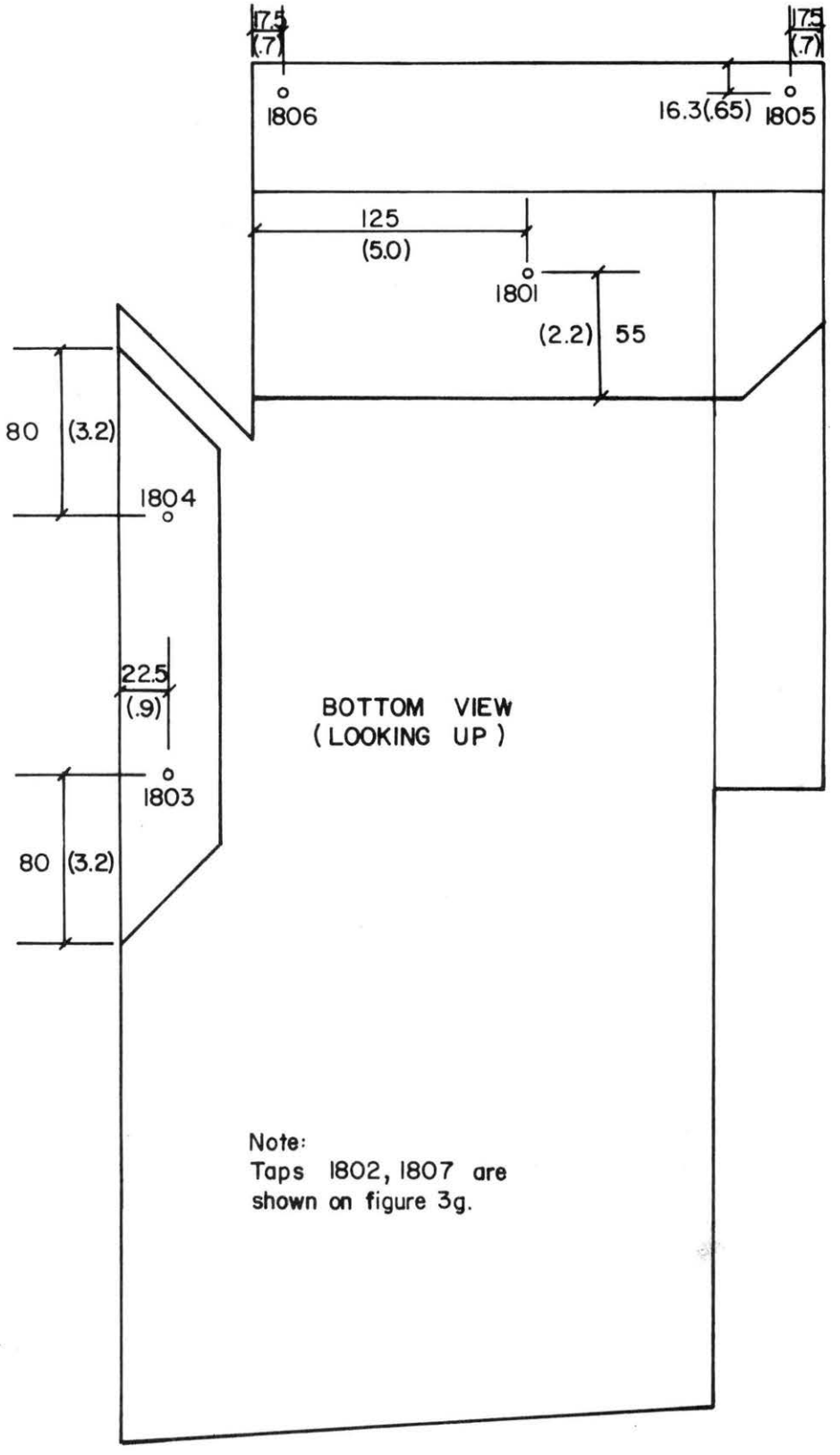


Figure 3j. Pressure Tap Locations

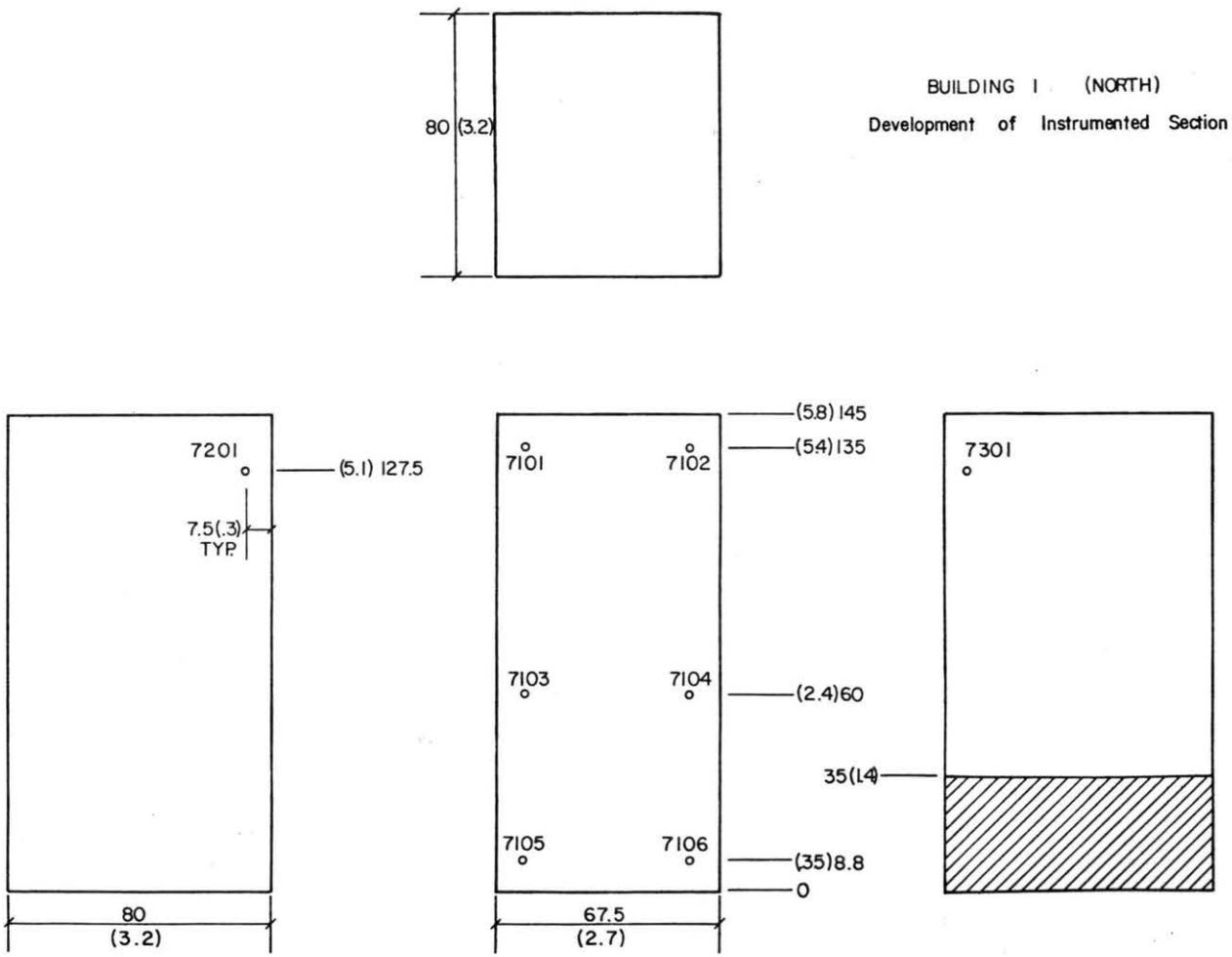


Figure 3k. Pressure Tap Locations

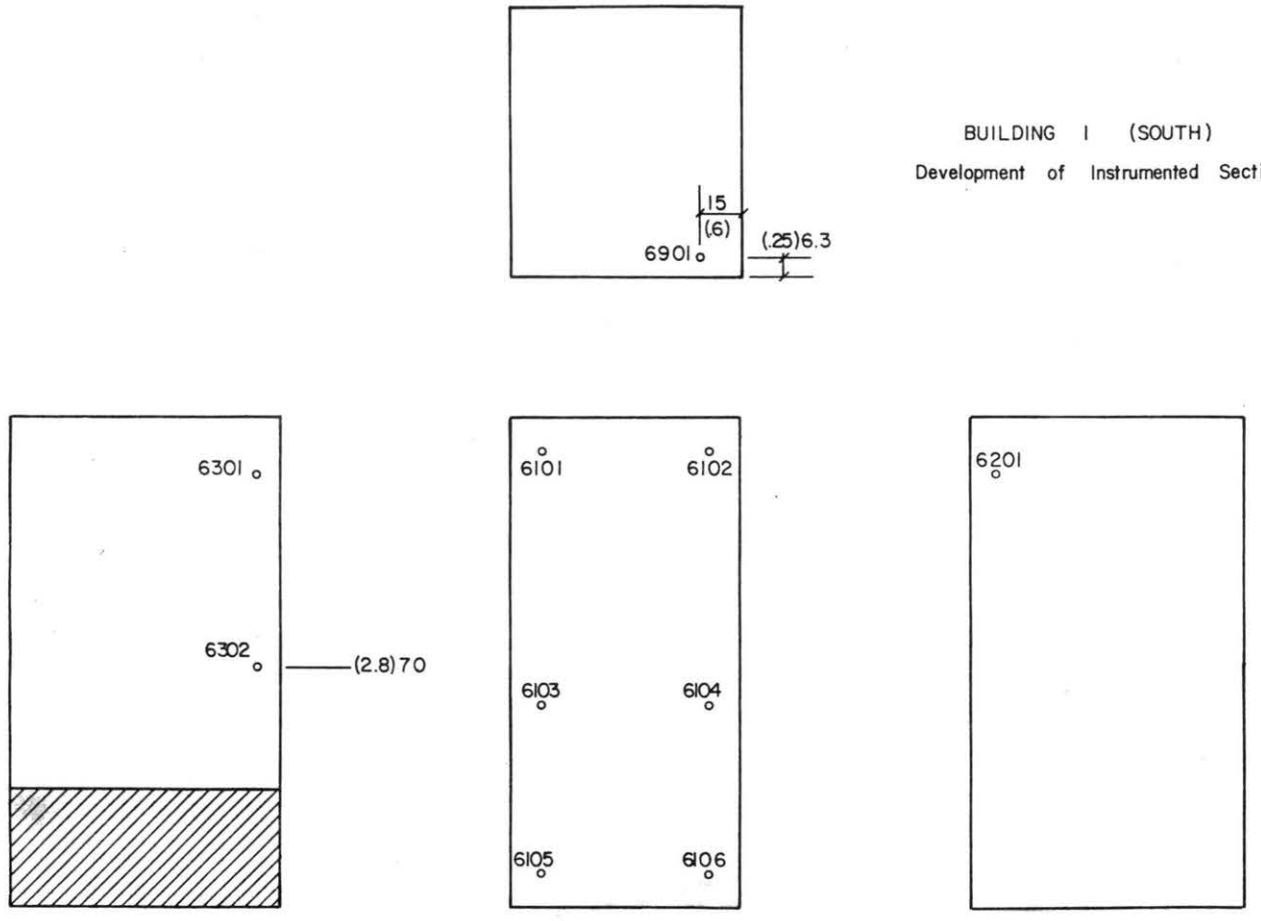


Figure 31. Pressure Tap Locations

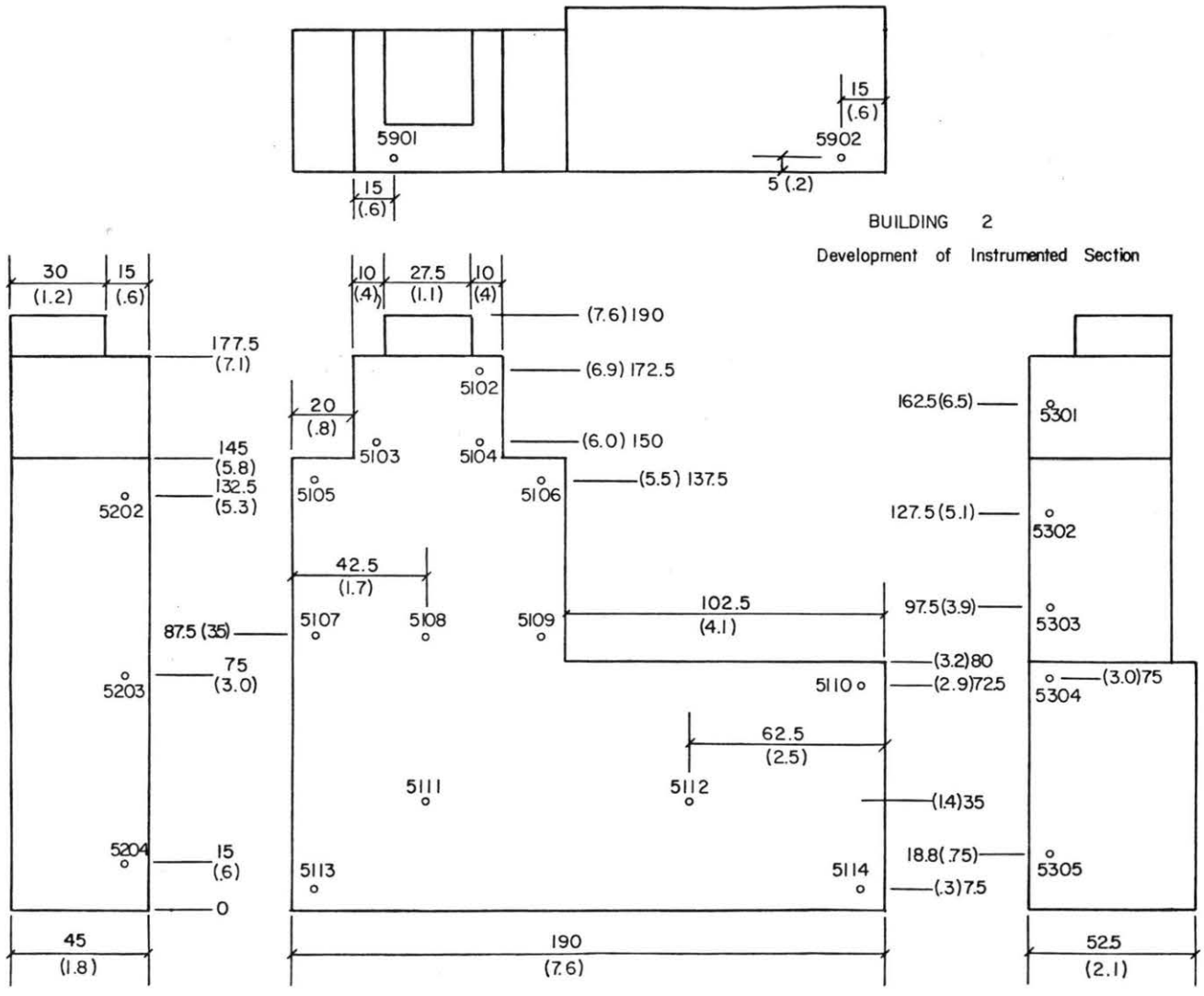


Figure 3m. Pressure Tap Locations

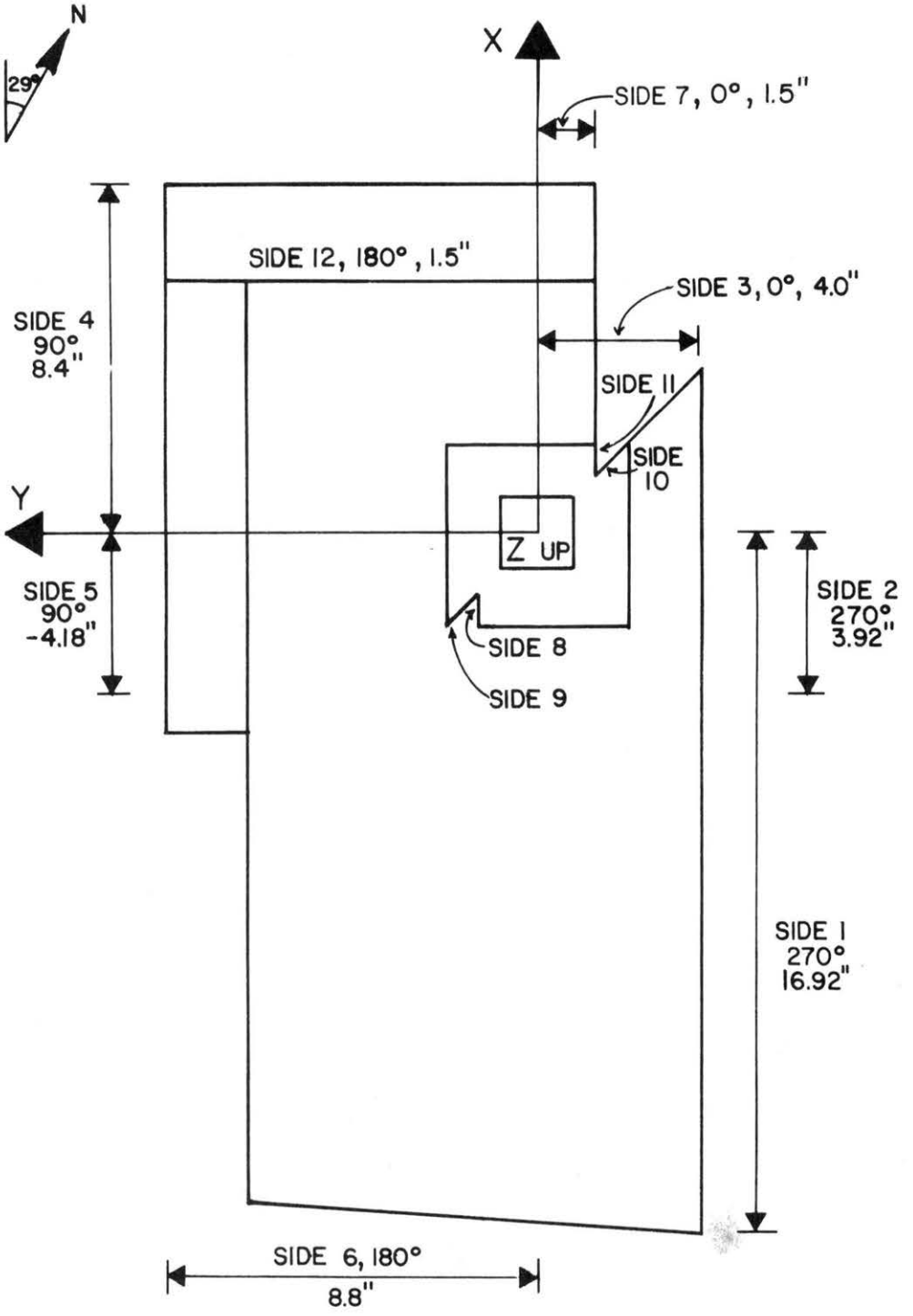


Figure 3n. Force and Moment Coordinate System

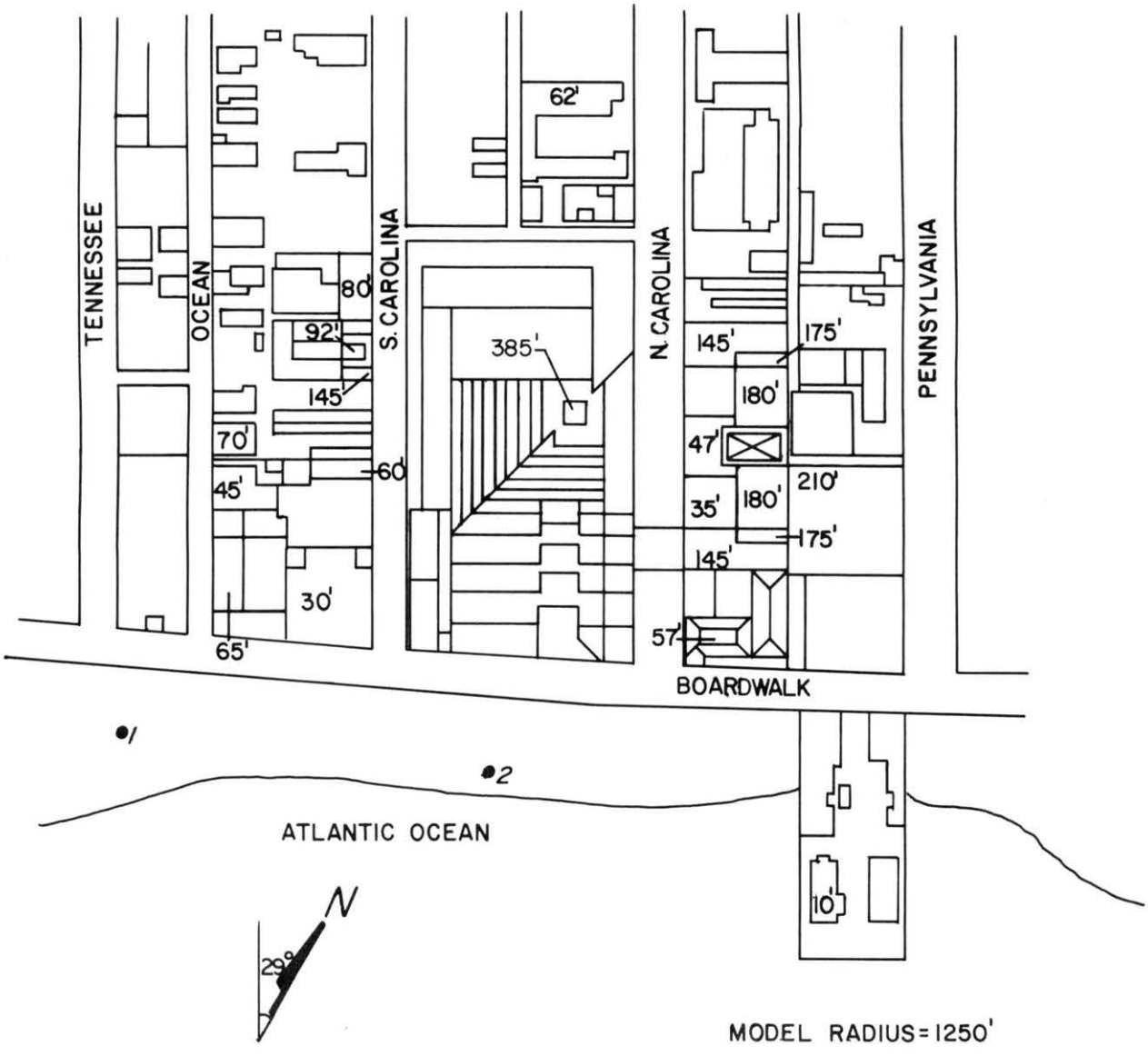


Figure 4a. Building Location and Pedestrian Wind Velocity Measuring Positions

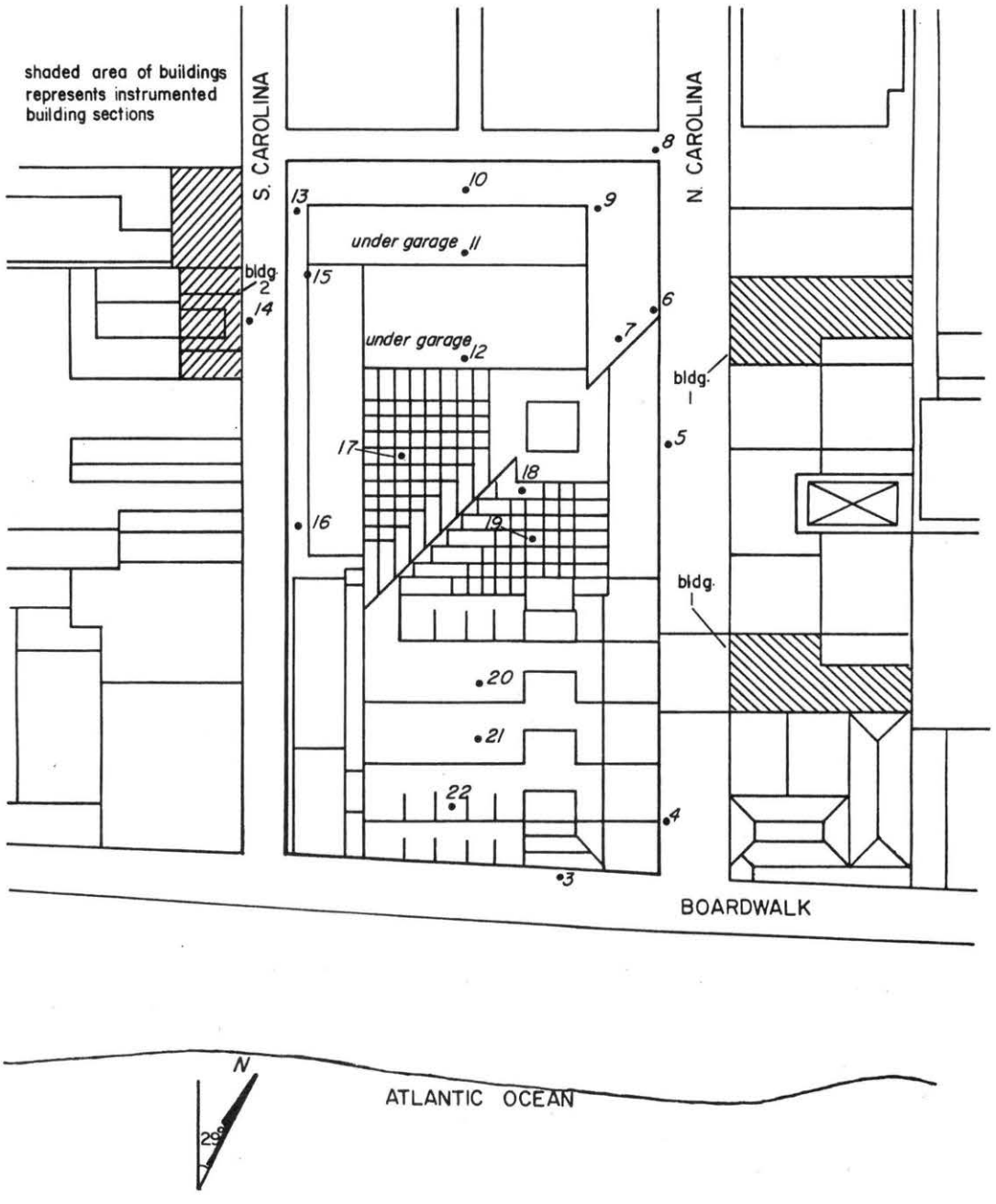


Figure 4b. Building Location and Pedestrian Wind Velocity Measuring Positions

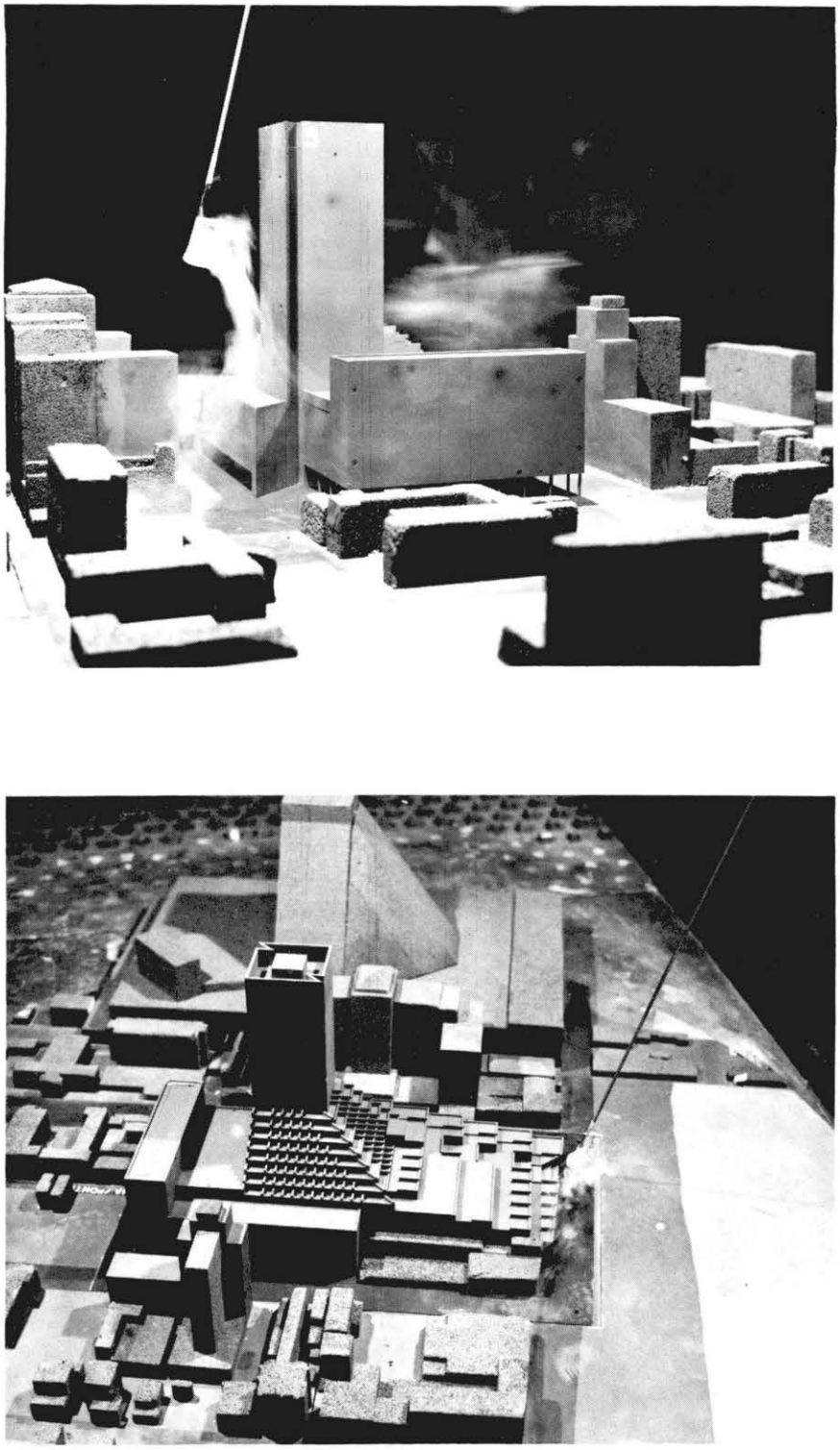


Figure 5. Completed Model in Wind Tunnel

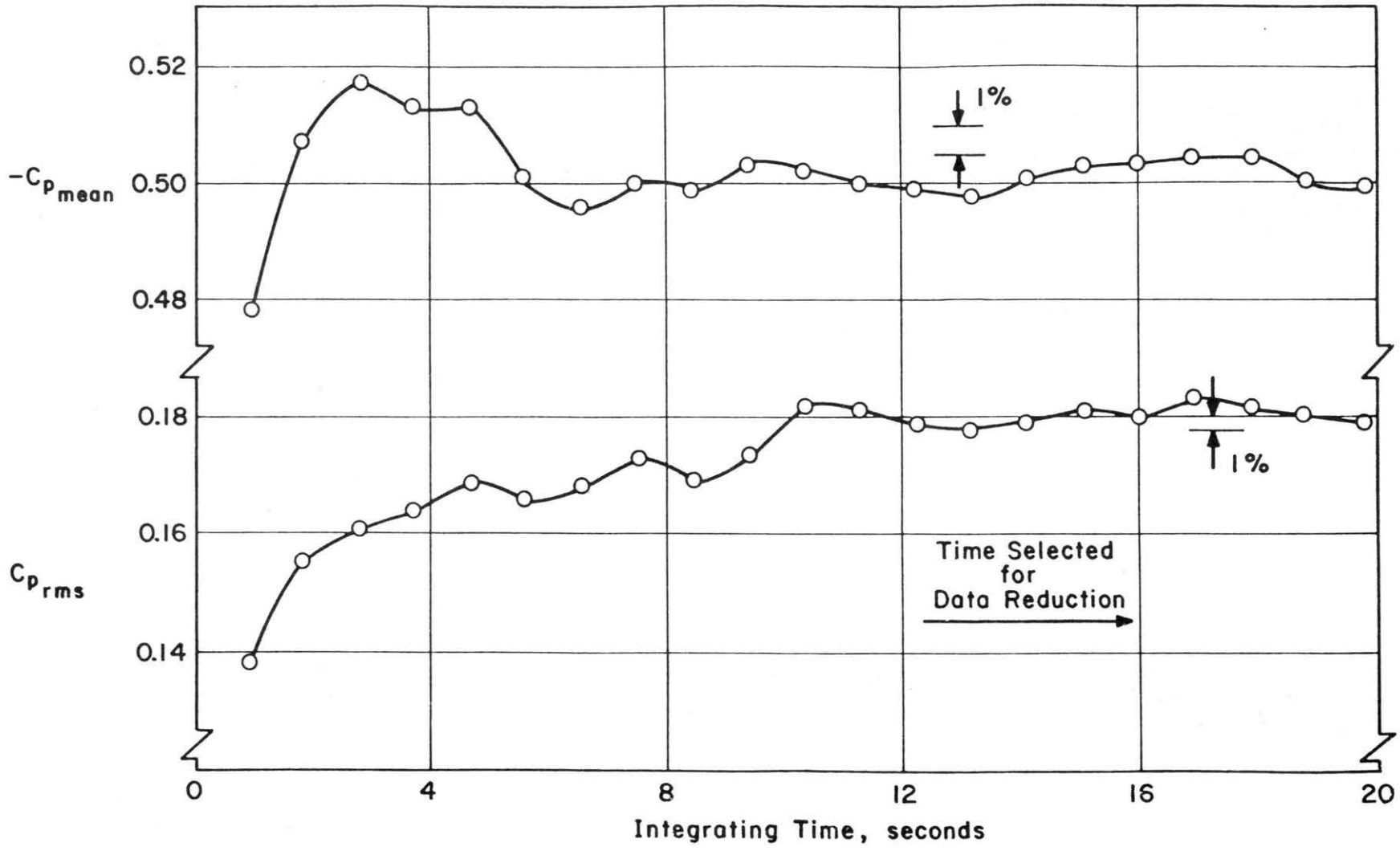


Figure 6 - Data Sampling Time Verification

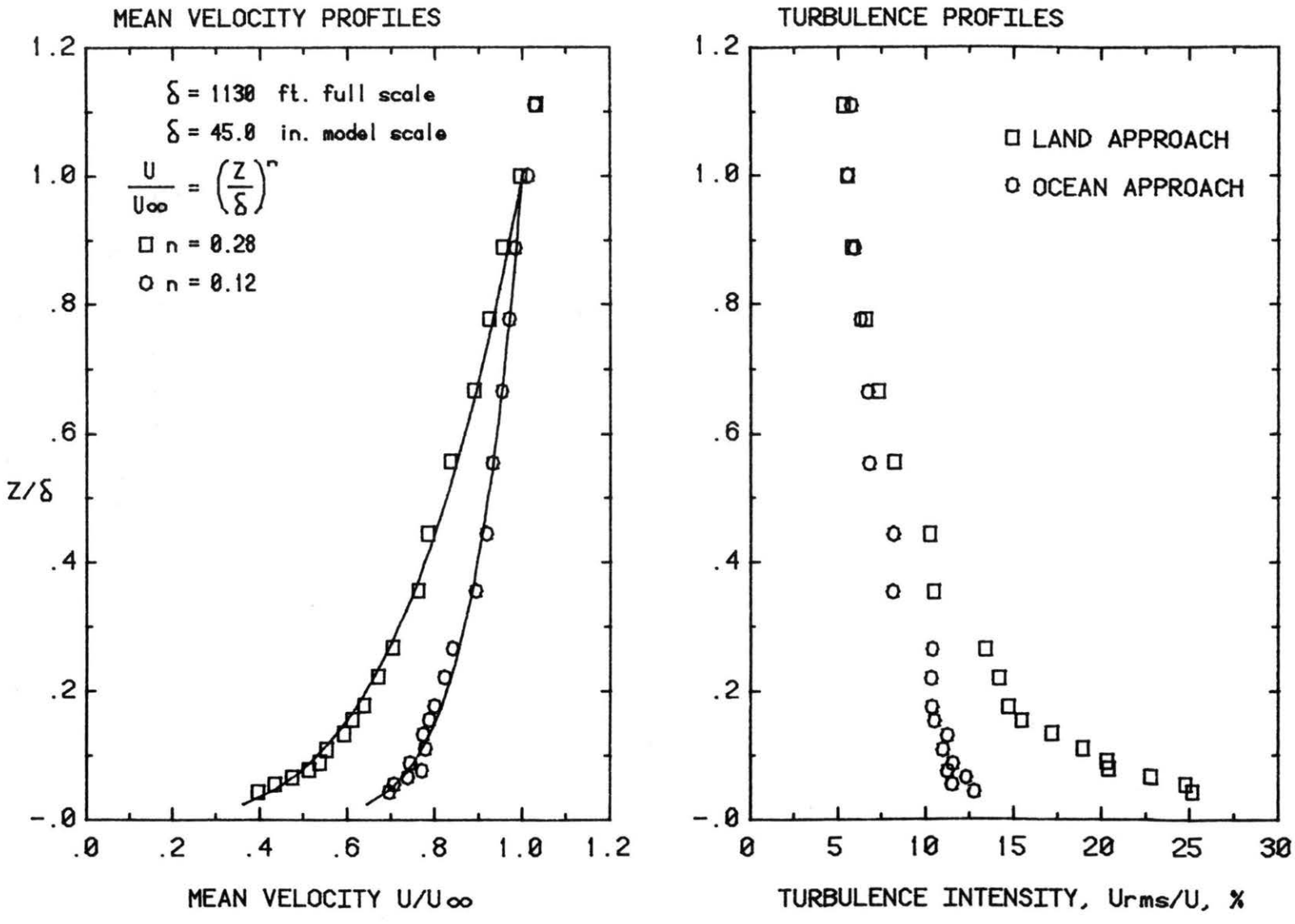


Figure 7. Mean Velocity and Turbulence Profiles Approaching the Model.

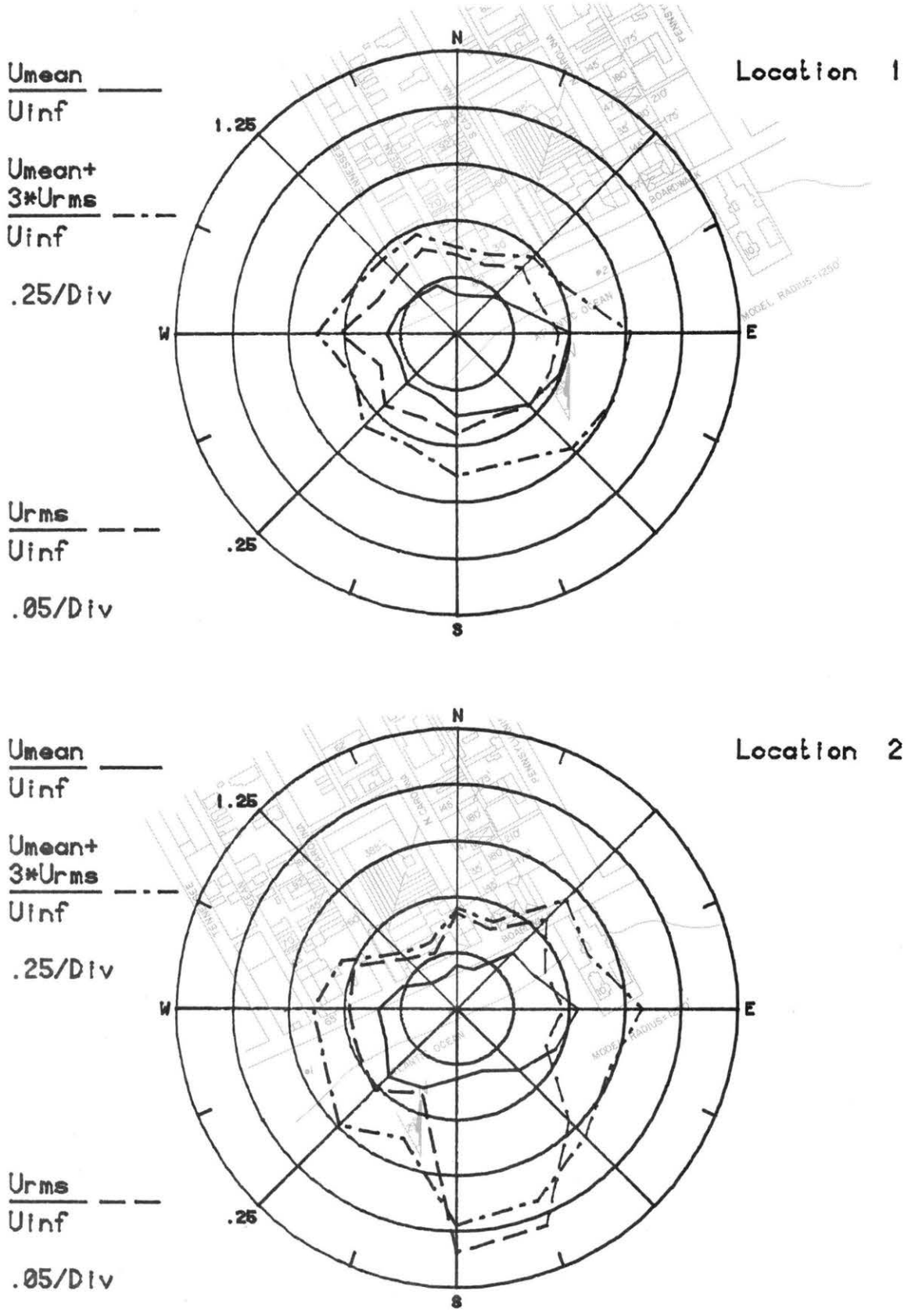
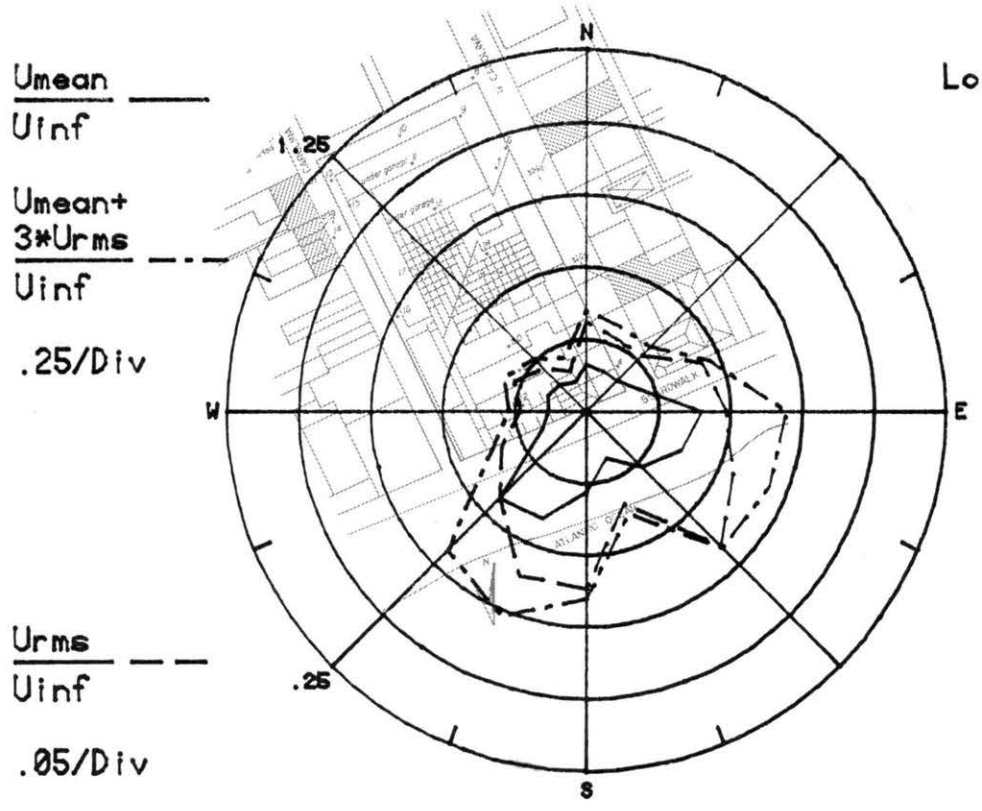


Figure 8a. Mean Velocities and Turbulence Intensities at Pedestrian Locations 1 and 2



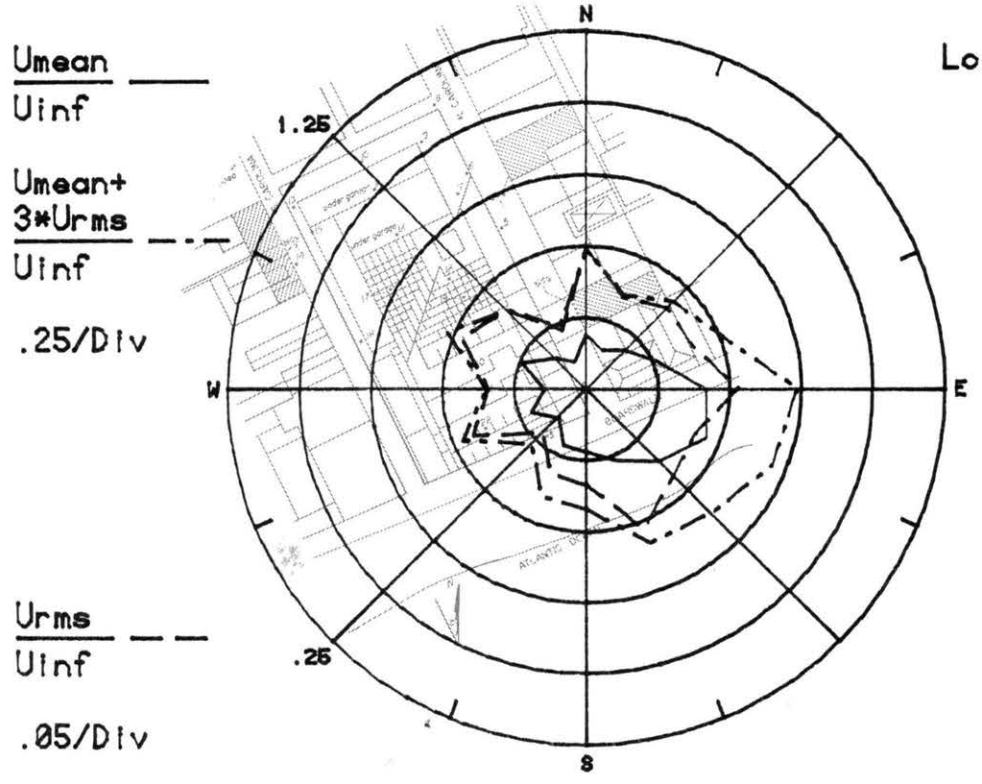


Figure 8b. Mean Velocities and Turbulence Intensities at Pedestrian Locations 3 and 4

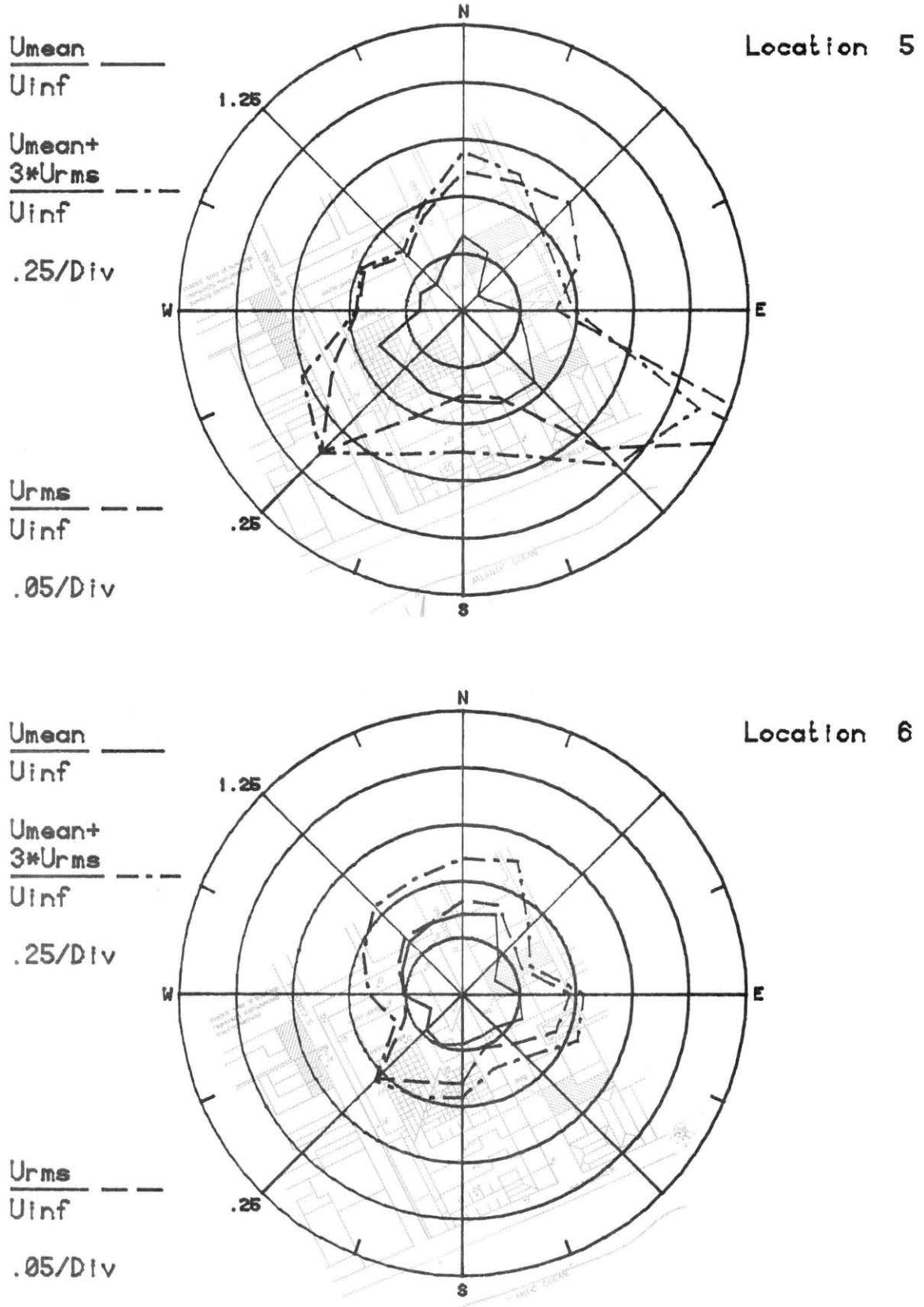
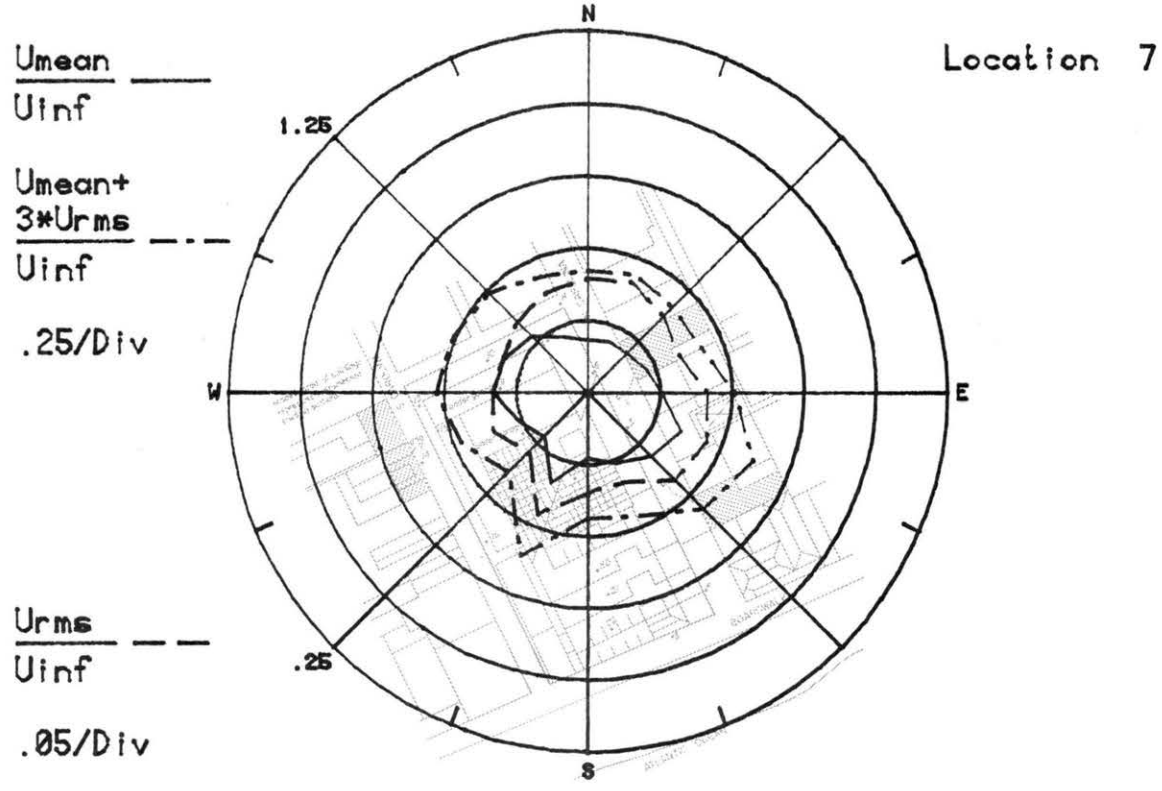


Figure 8c. Mean Velocities and Turbulence Intensities at Pedestrian Locations 5 and 6



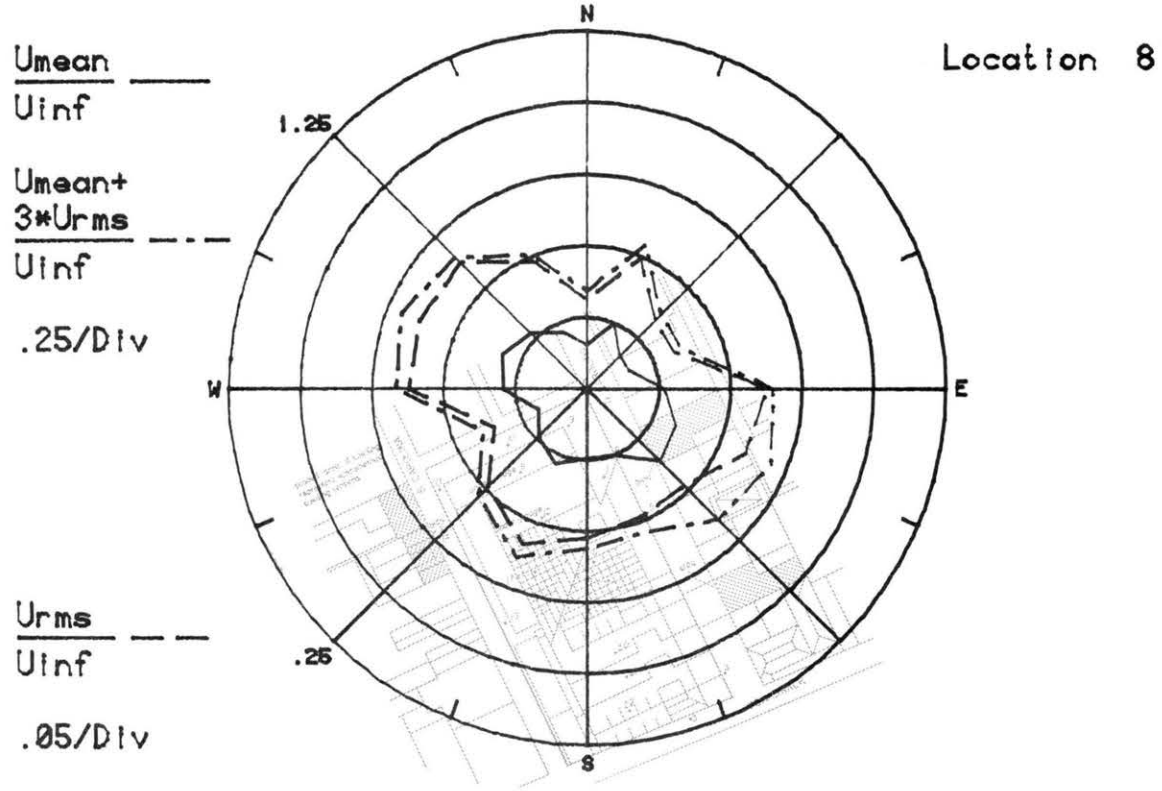


Figure 8d. Mean Velocities and Turbulence Intensities at Pedestrian Locations 7 and 8

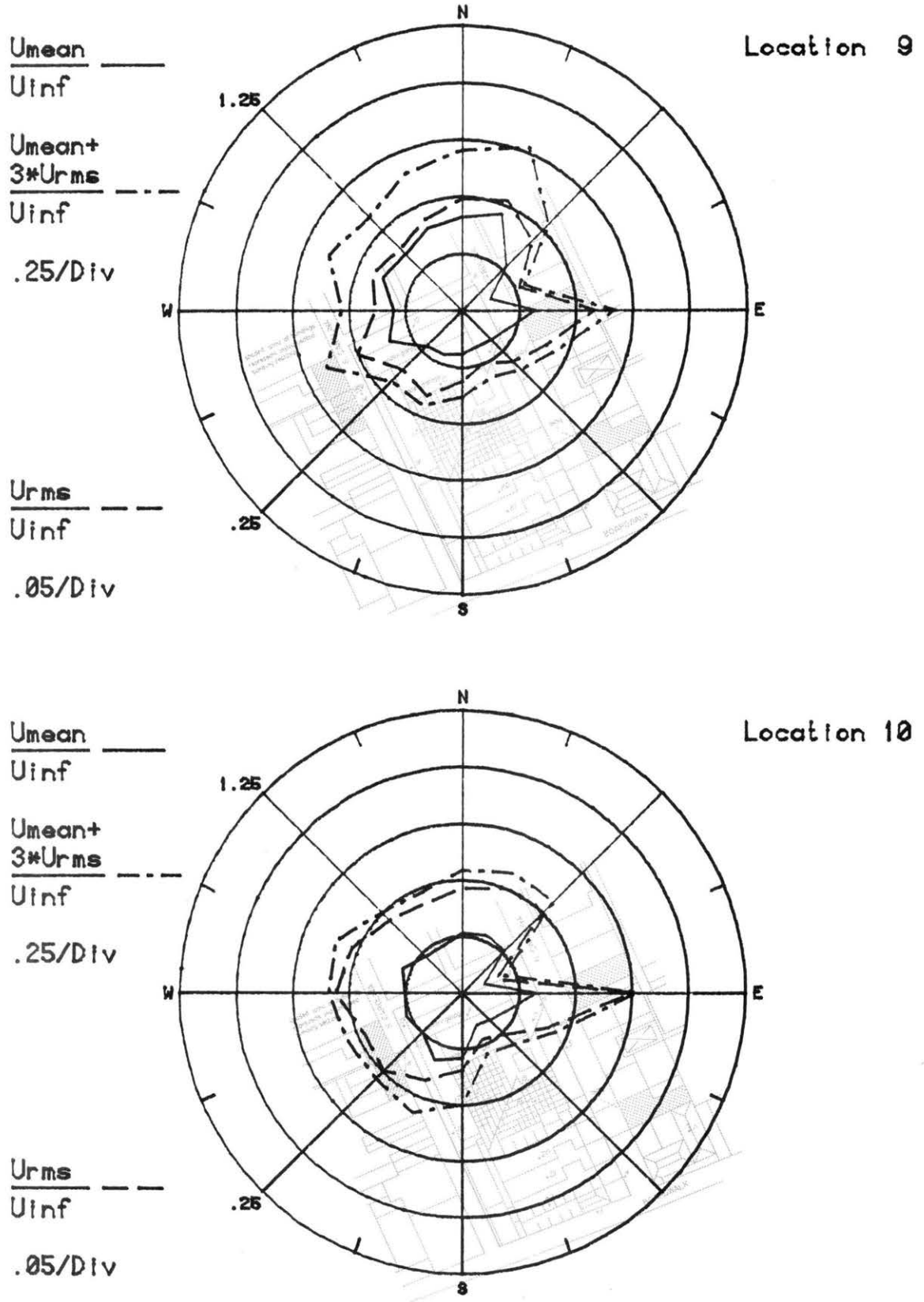


Figure 8e. Mean Velocities and Turbulence Intensities at Pedestrian Locations 9 and 10

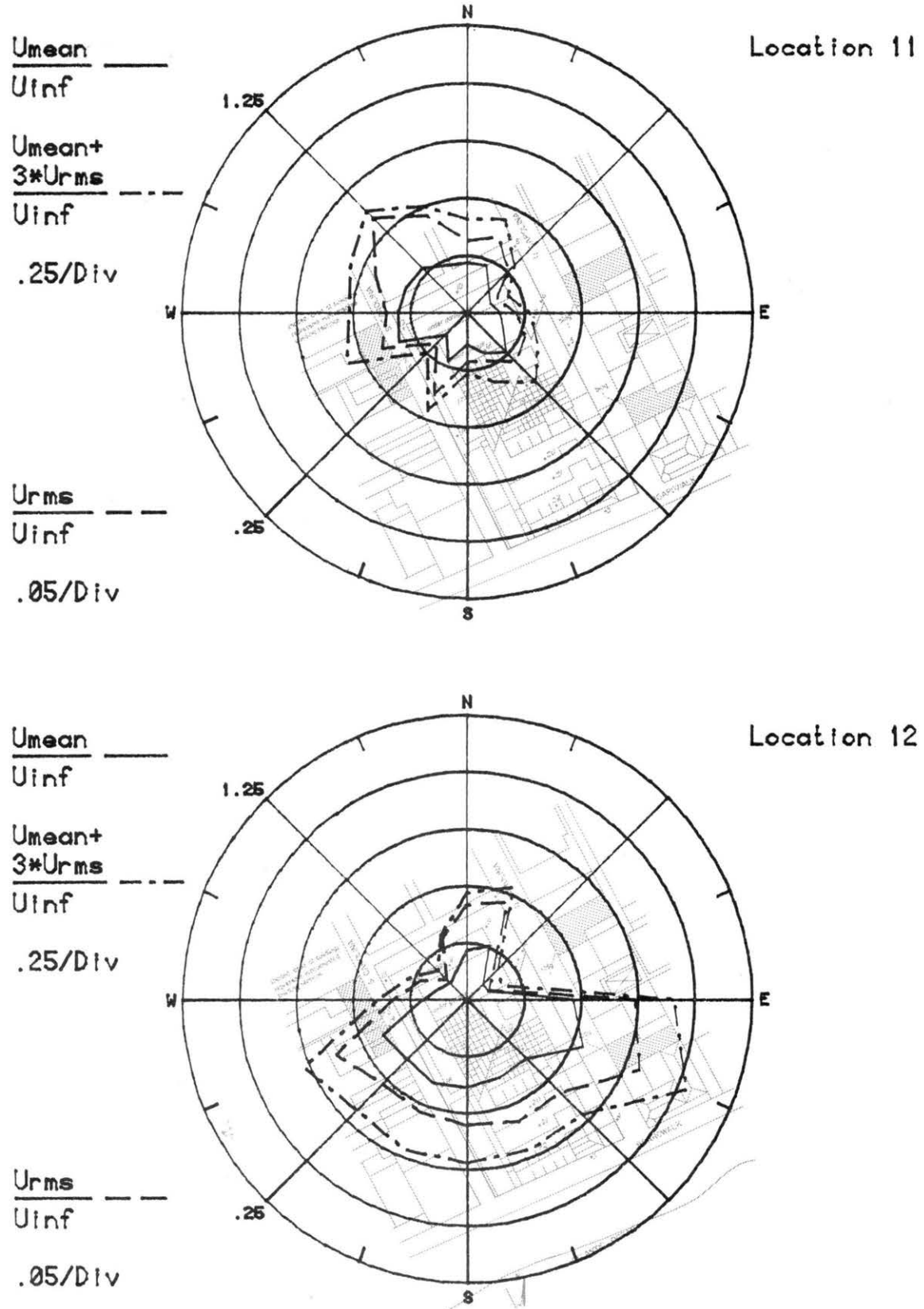


Figure 8f. Mean Velocities and Turbulence Intensities at Pedestrian Locations 11 and 12

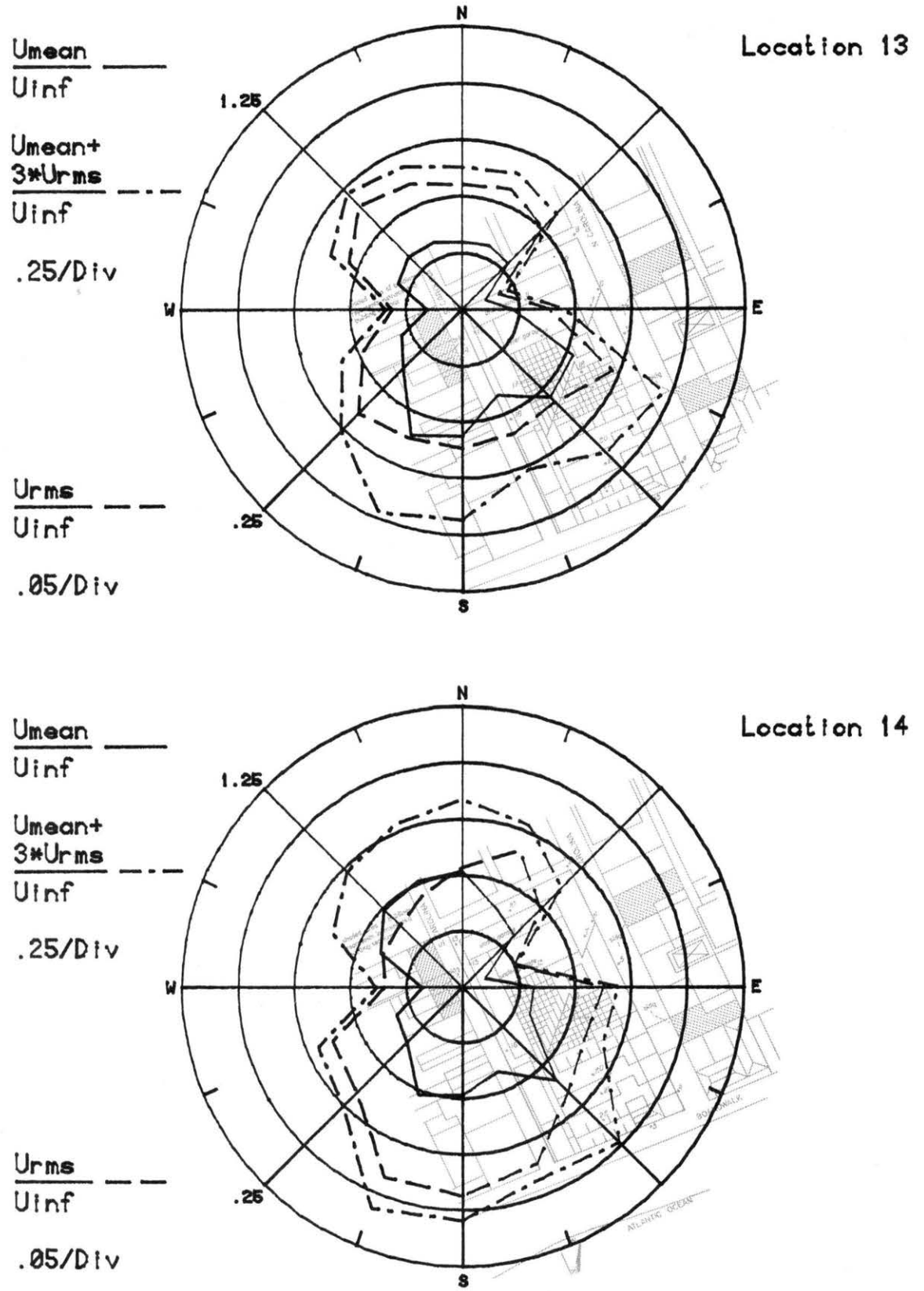
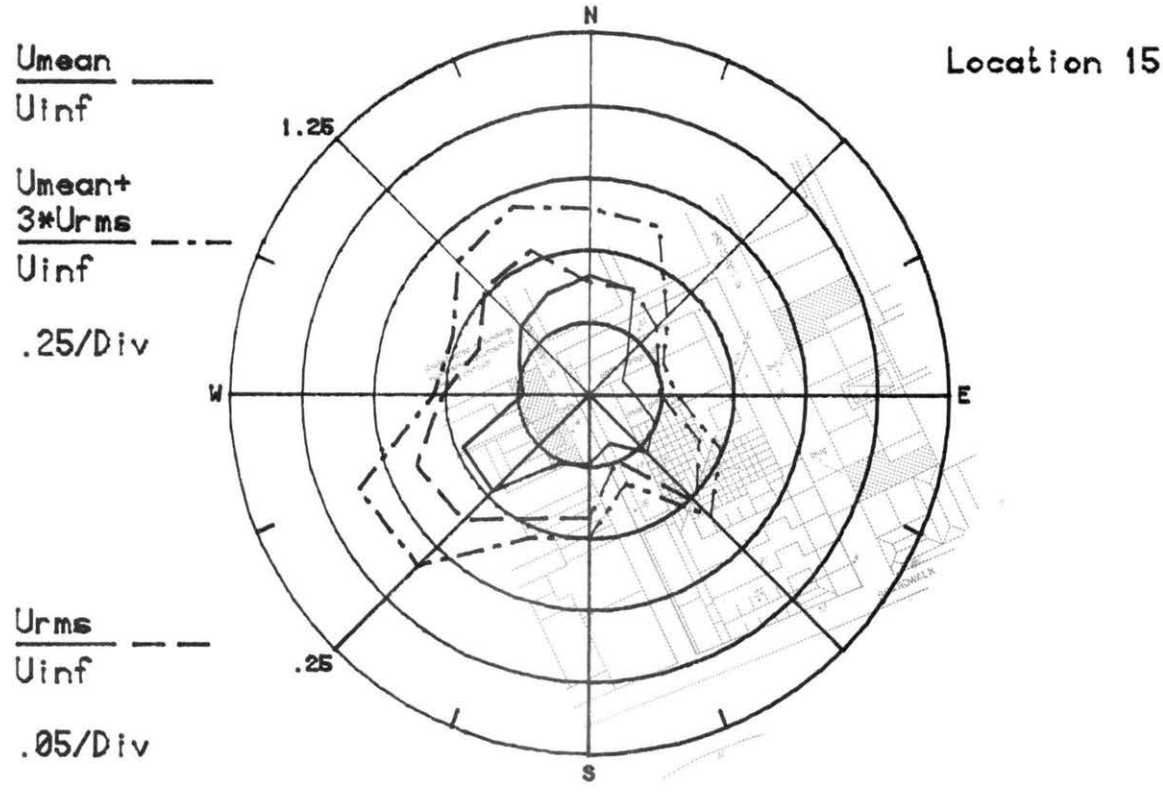


Figure 8g. Mean Velocities and Turbulence Intensities at Pedestrian Locations 13 and 14



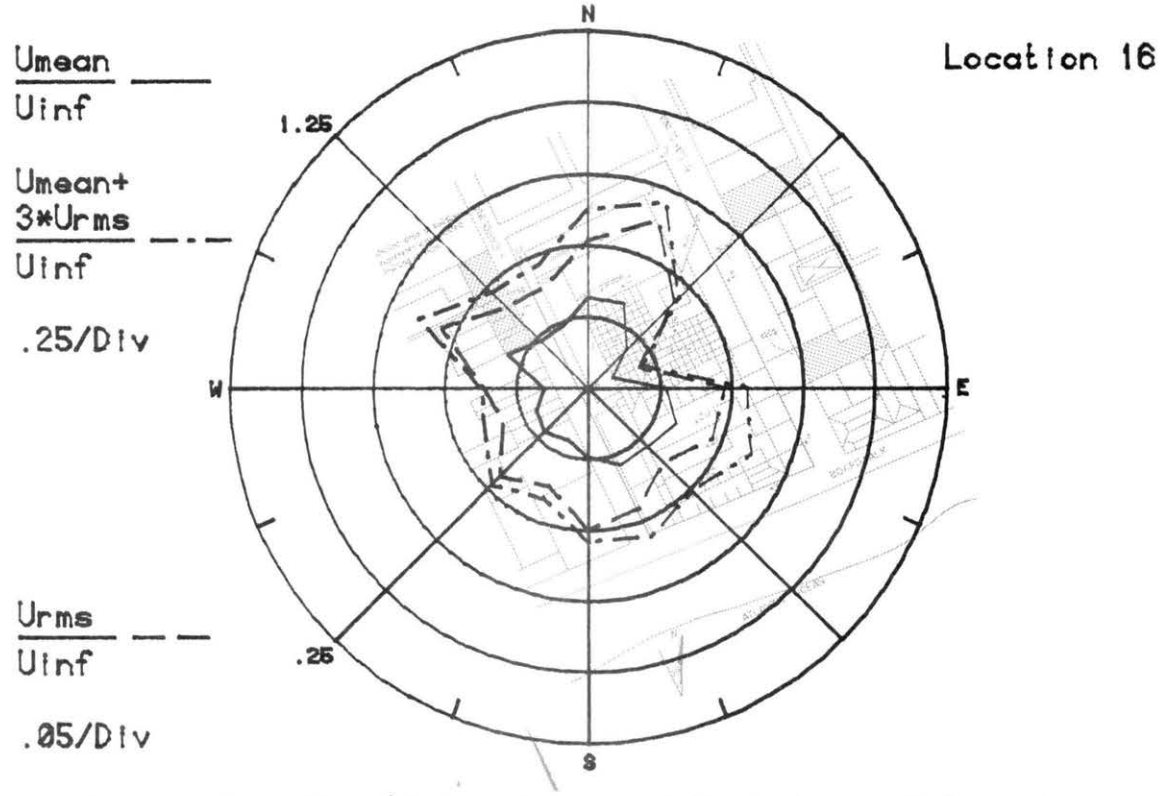


Figure 8h. Mean Velocities and Turbulence Intensities at Pedestrian Locations 15 and 16

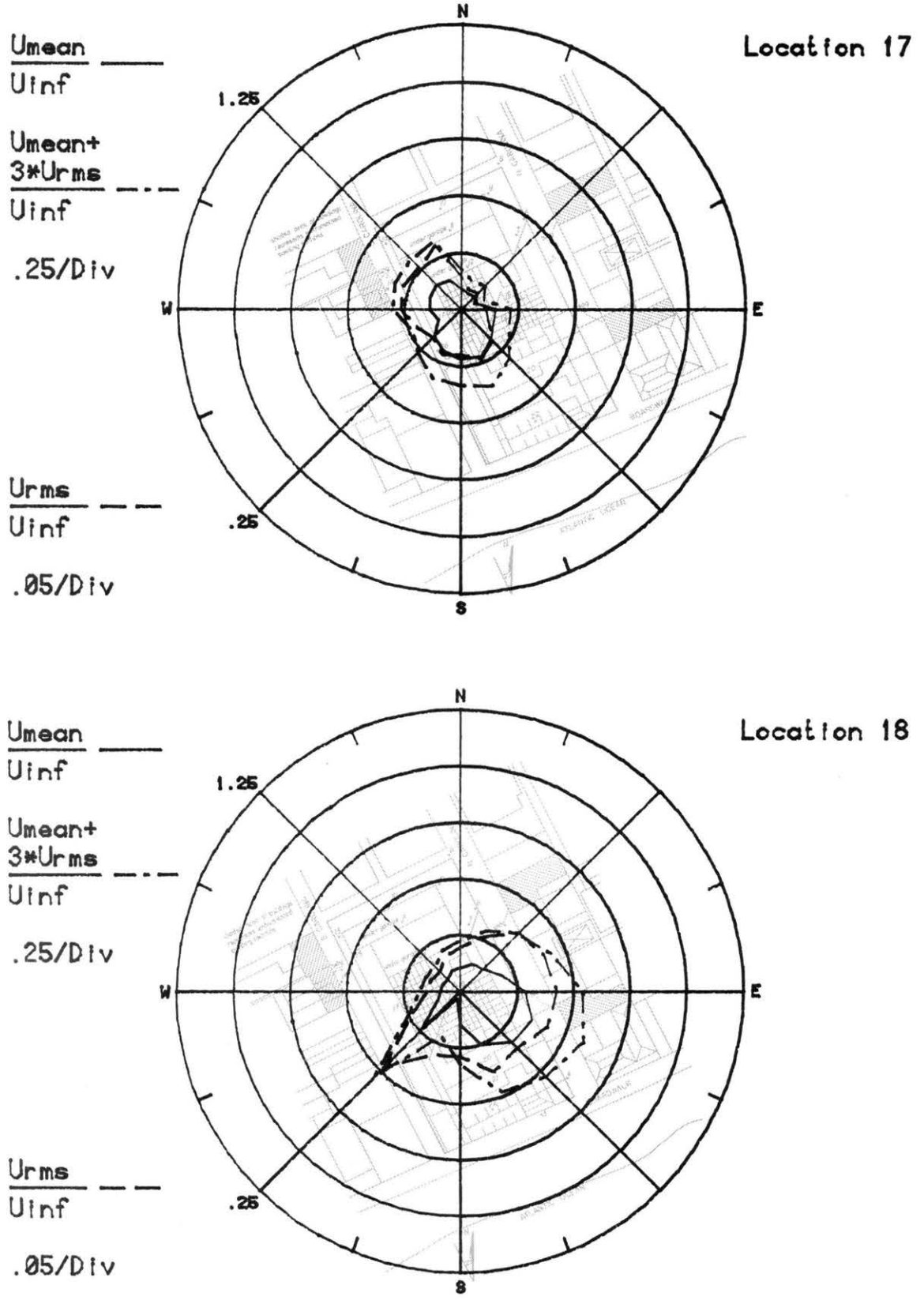
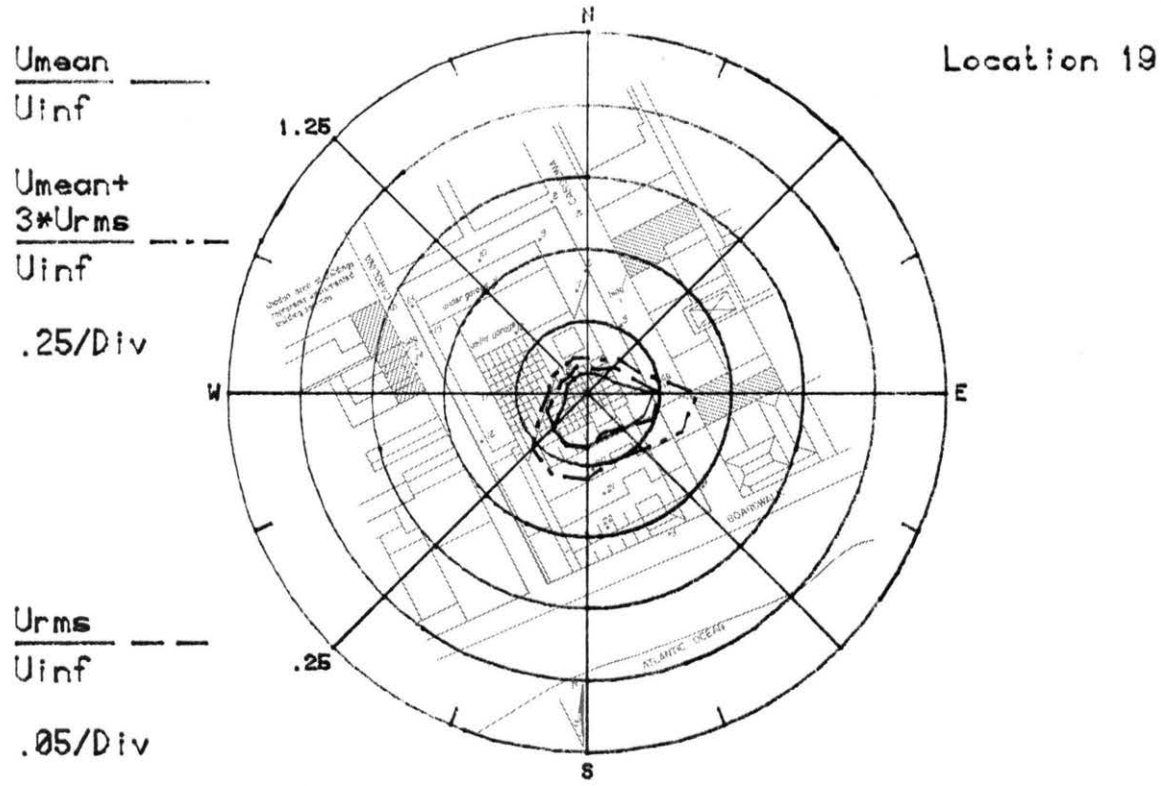


Figure 81. Mean Velocities and Turbulence Intensities at Pedestrian Locations 17 and 18



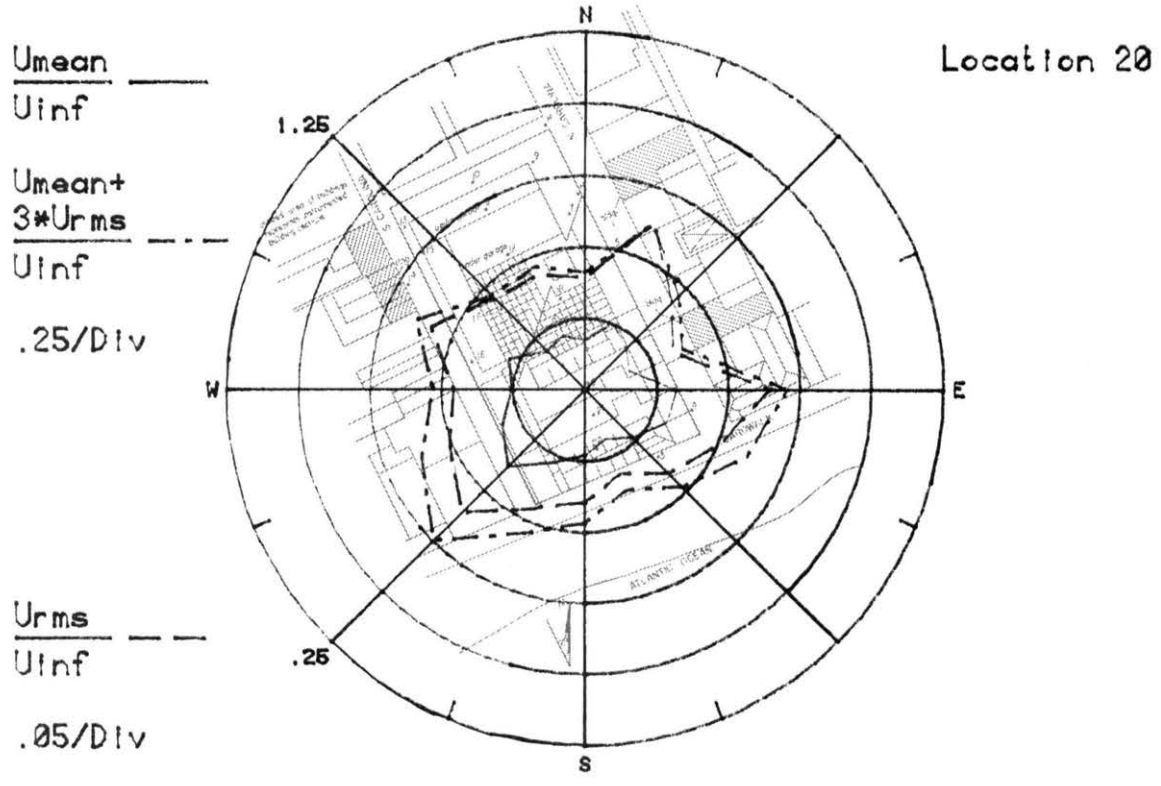


Figure 8J. Mean Velocities and Turbulence Intensities at Pedestrian Locations 19 and 20

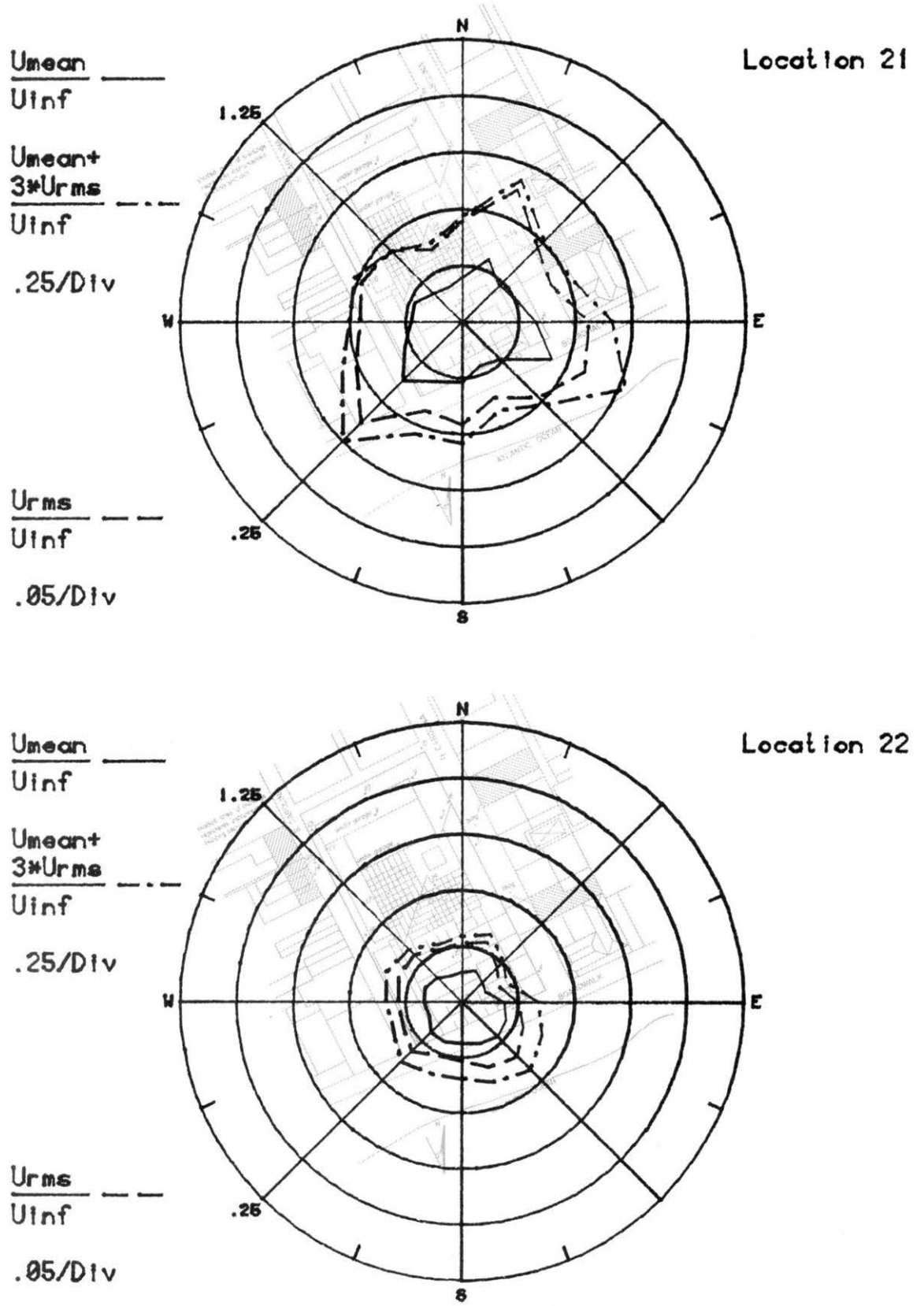


Figure 8k. Mean Velocities and Turbulence Intensities at Pedestrian Locations 21 and 22

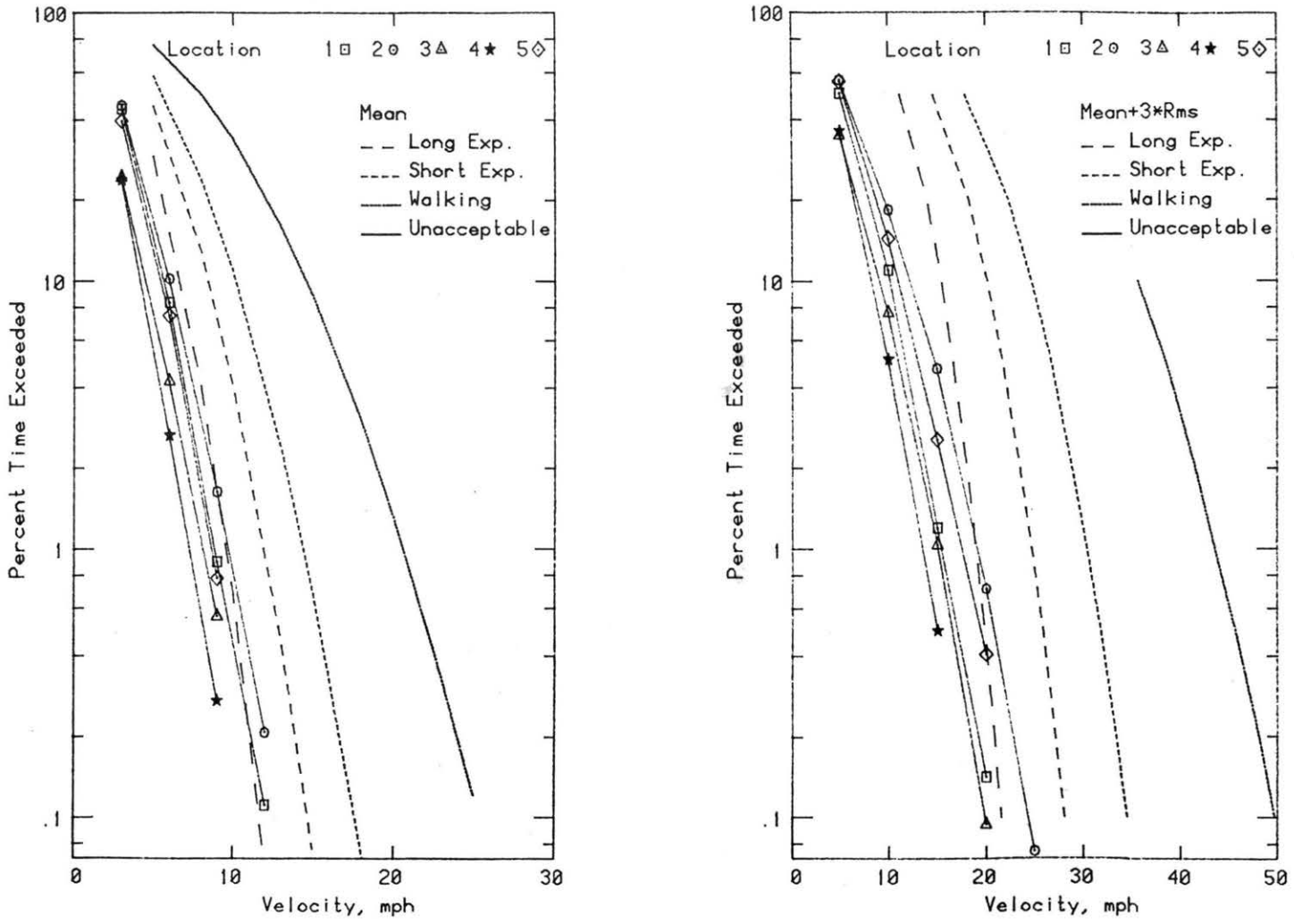


Figure 9a. Wind Velocity Probabilities for Pedestrian Locations

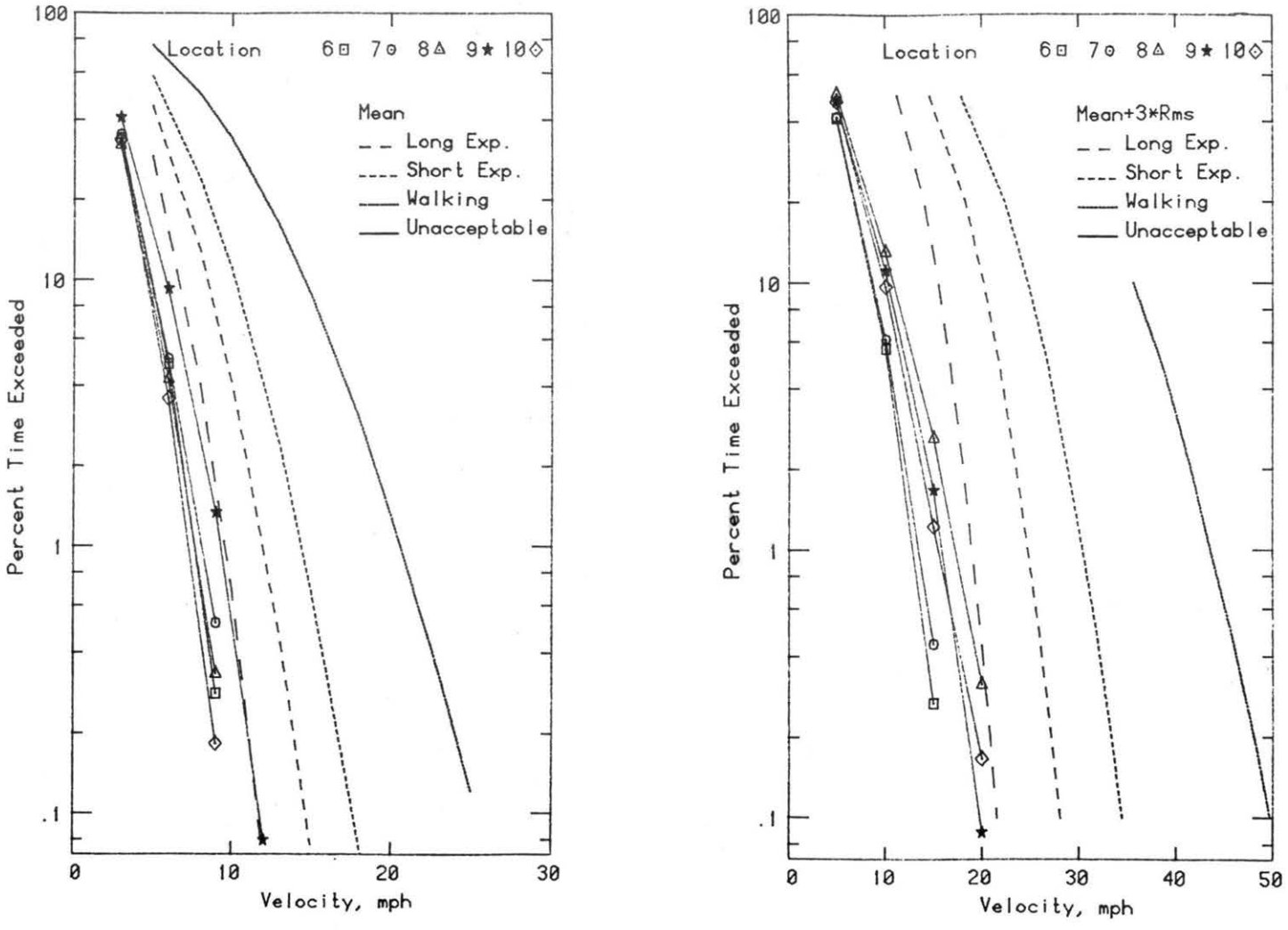


Figure 9b. Wind Velocity Probabilities for Pedestrian Locations

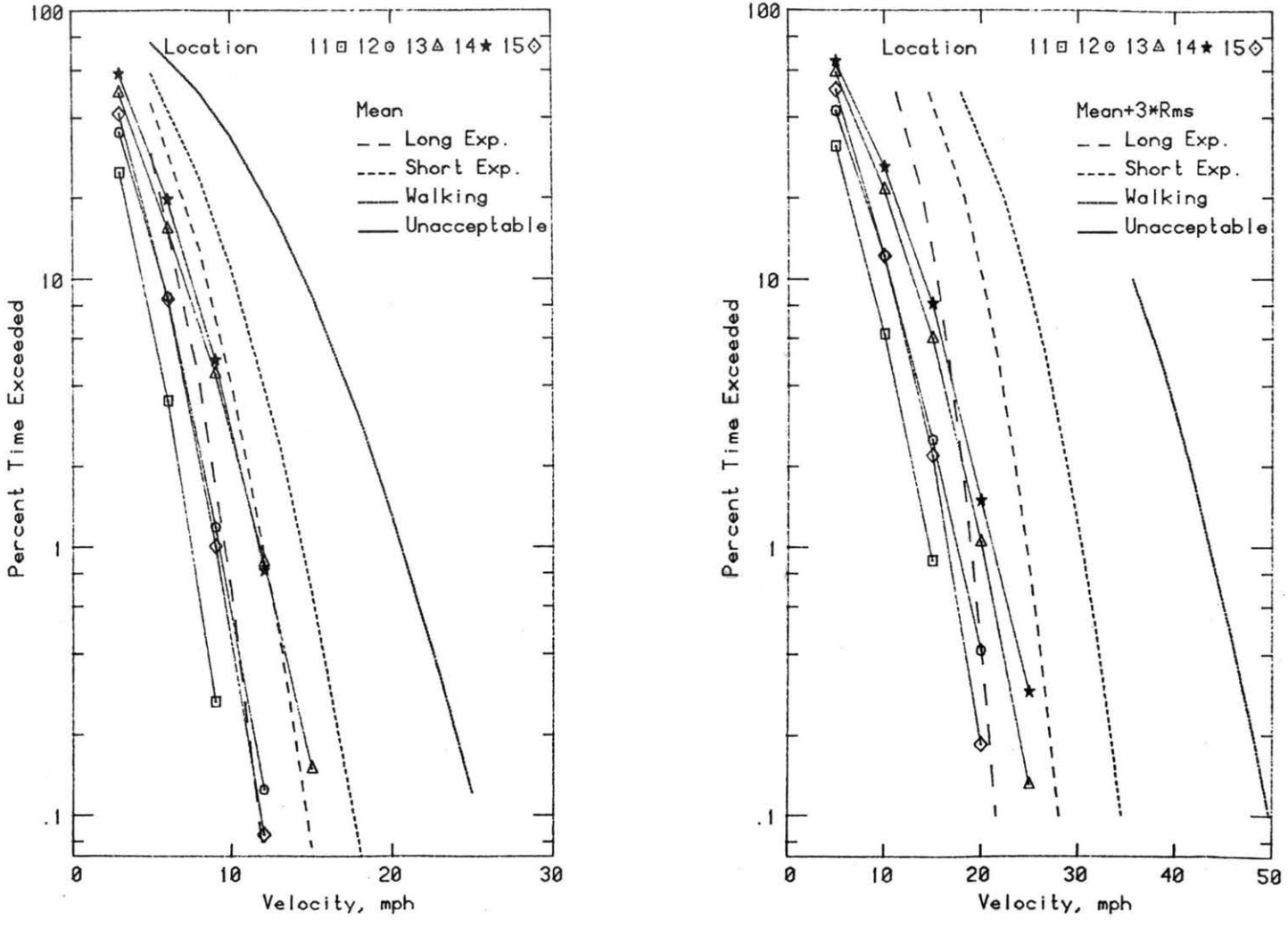


Figure 9c. Wind Velocity Probabilities for Pedestrian Locations

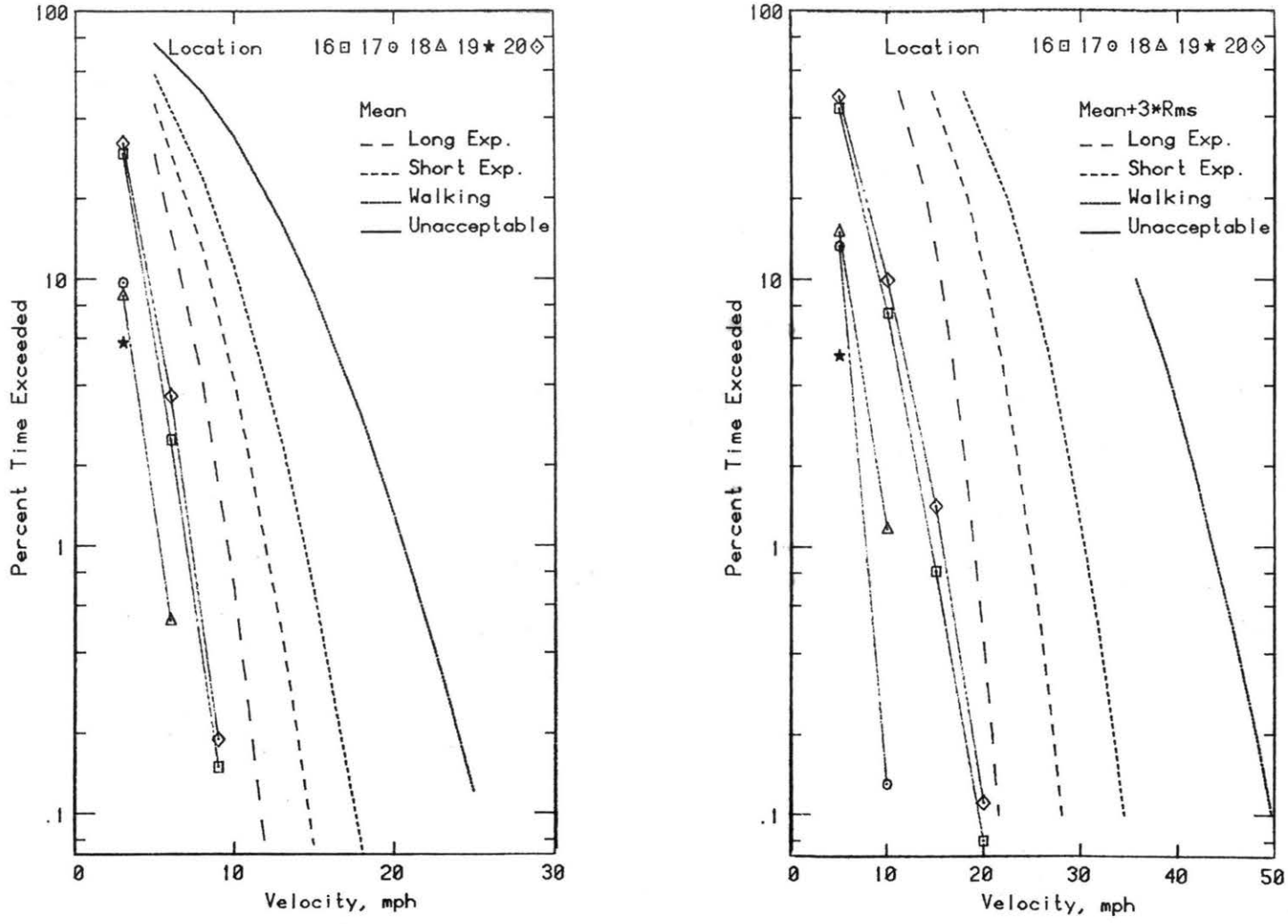


Figure 9d. Wind Velocity Probabilities for Pedestrian Locations

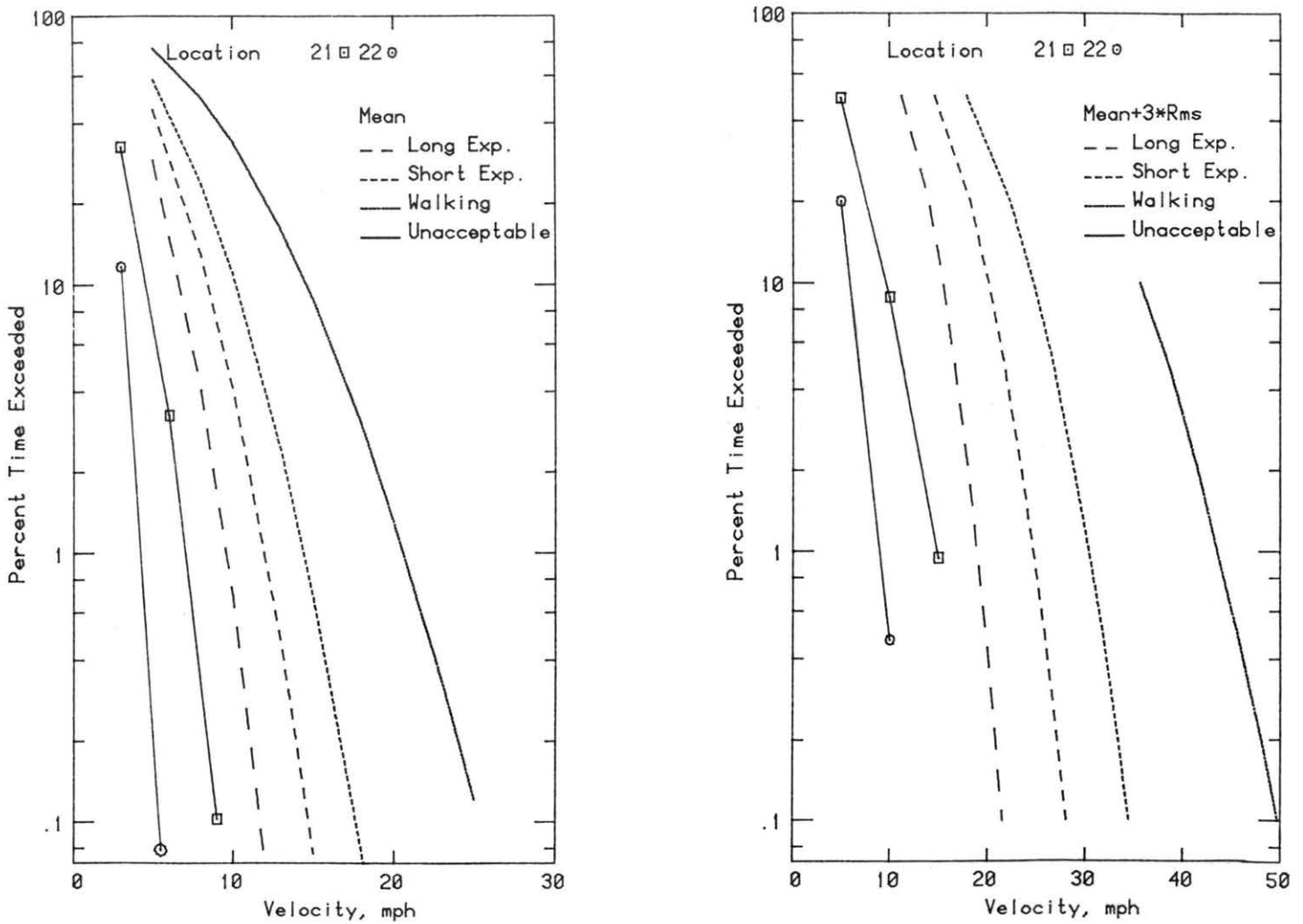


Figure 9e. Wind Velocity Probabilities for Pedestrian Locations

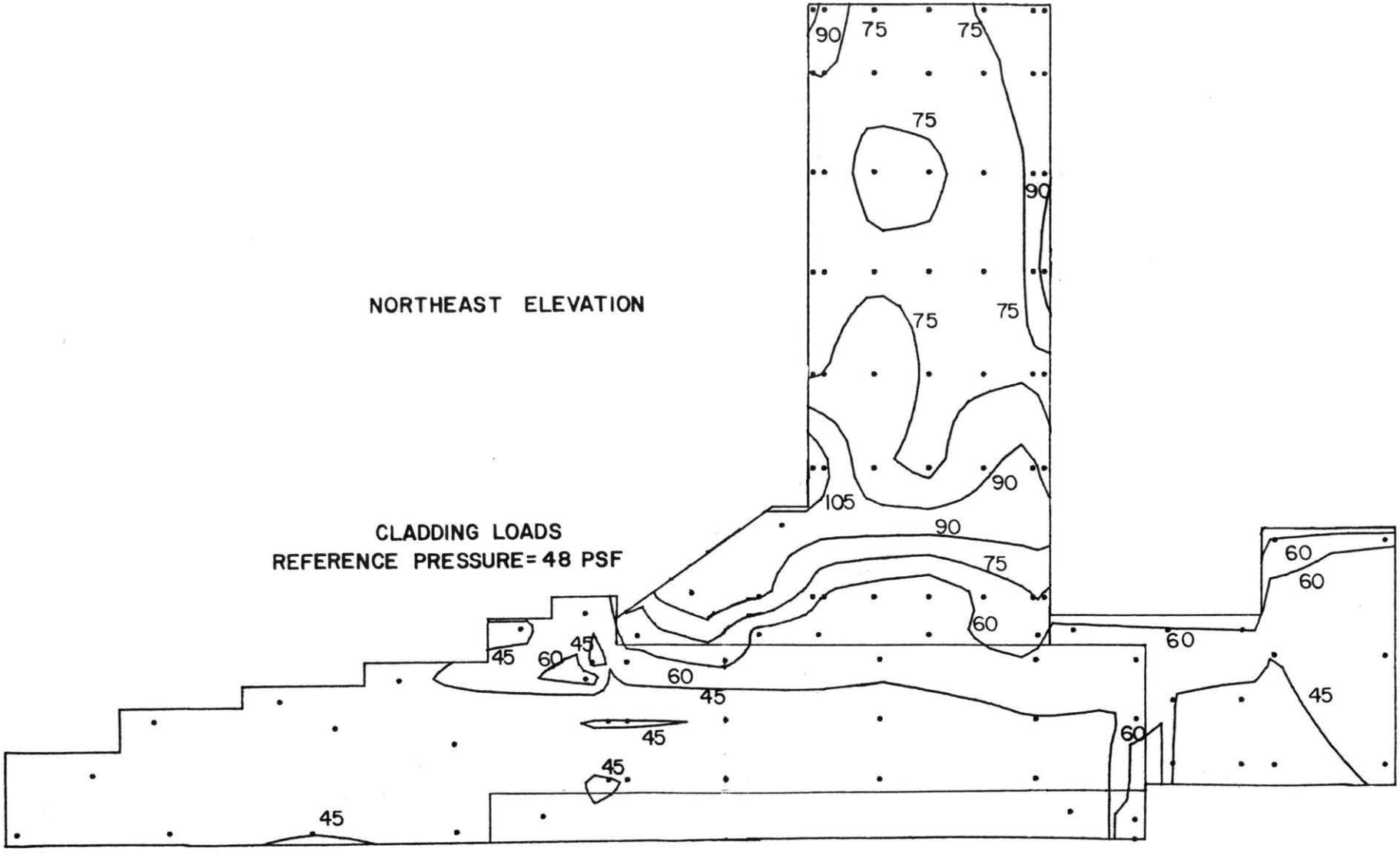


FIGURE 10a PEAK PRESSURE LOADS ON THE BUILDING.

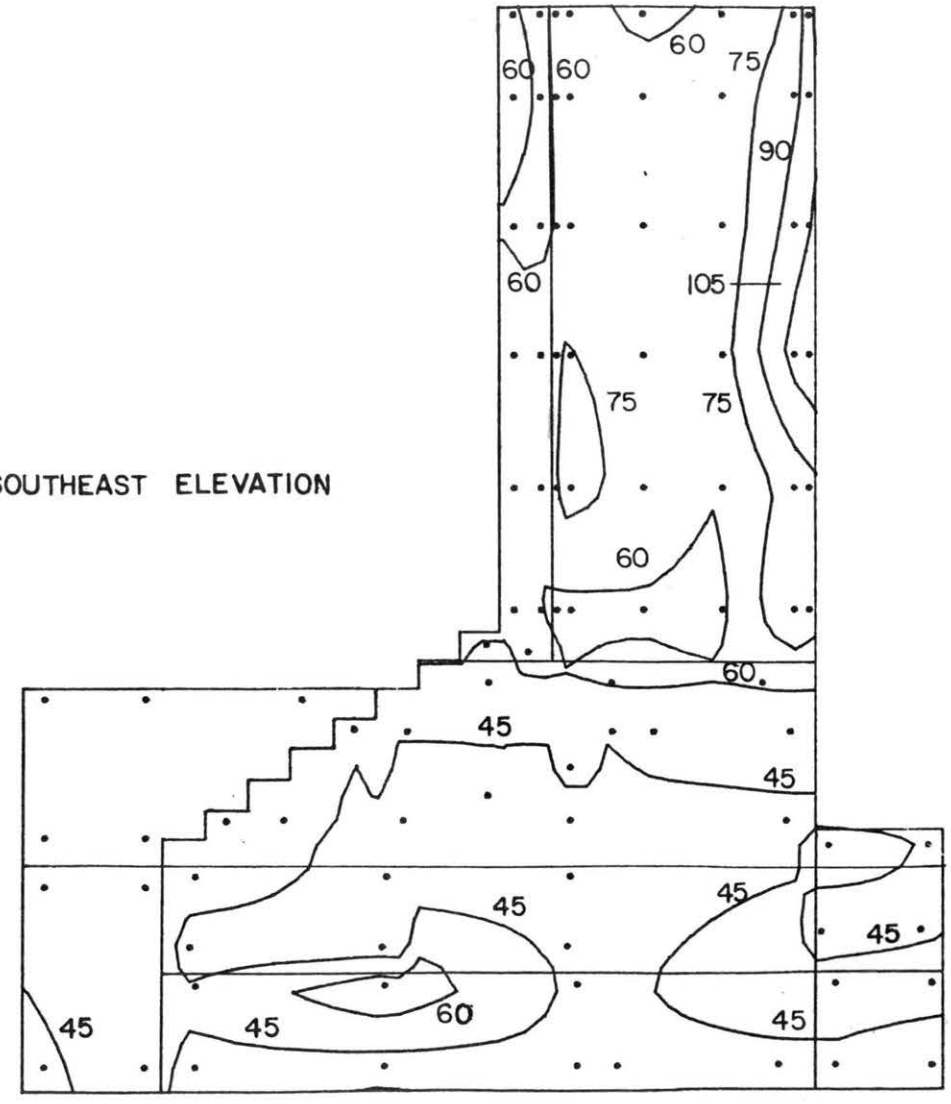


FIGURE 10b PEAK PRESSURE LOADS ON THE BUILDING.

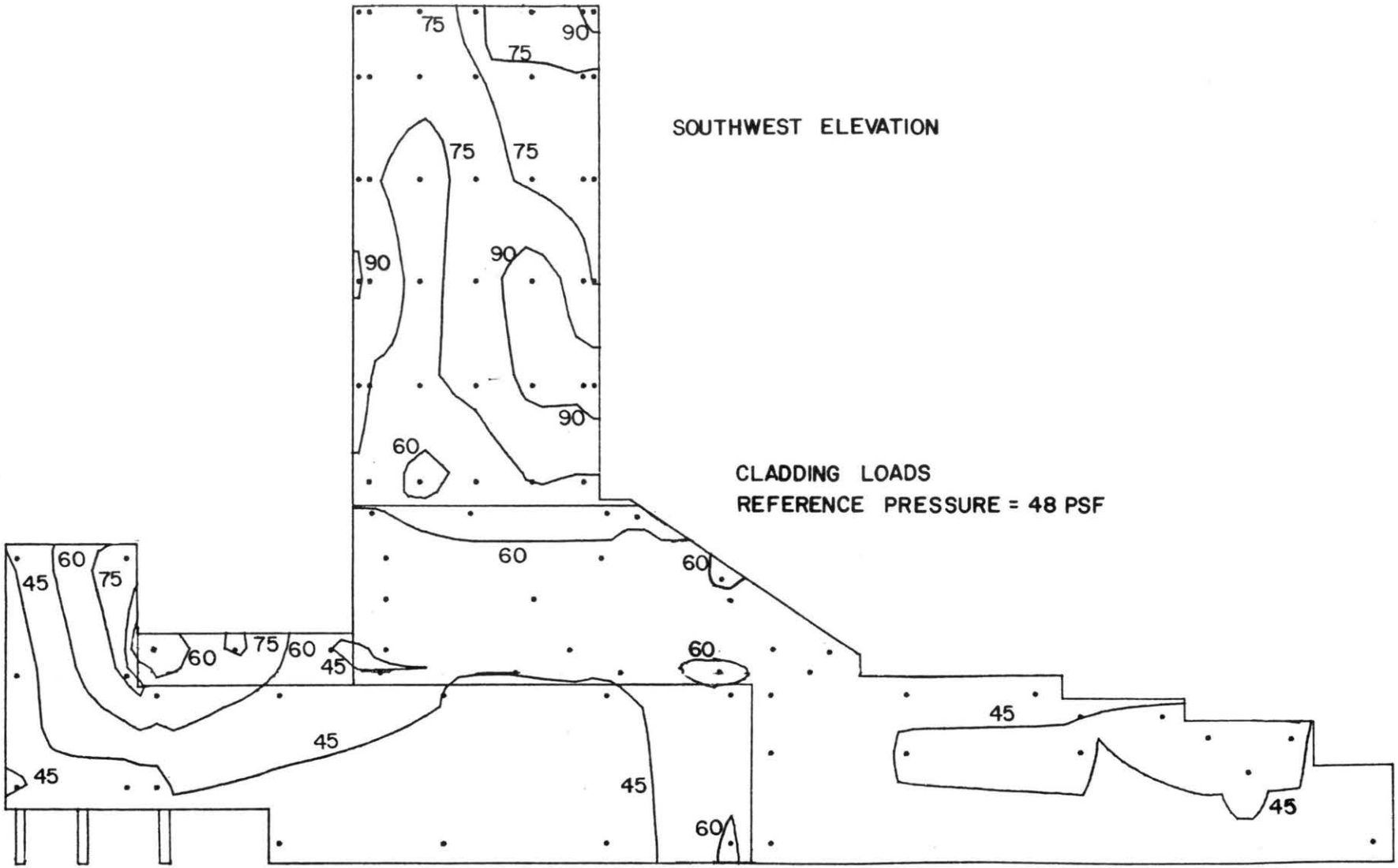
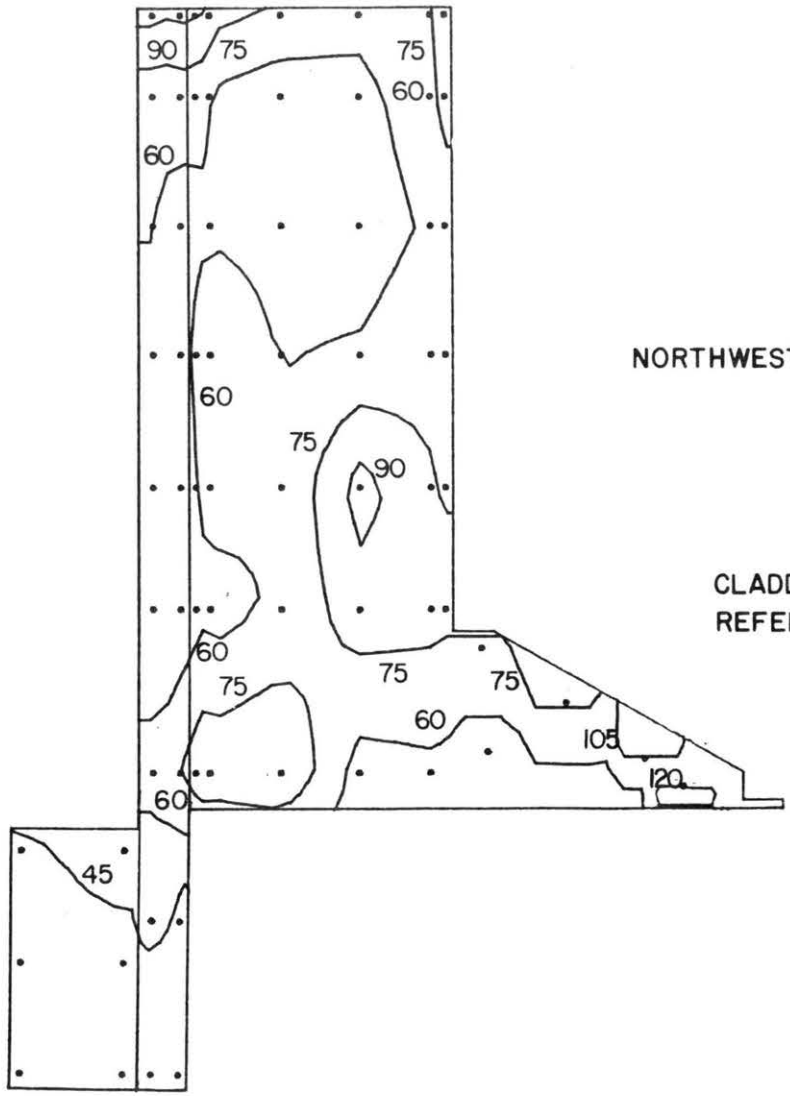


FIGURE 10c PEAK PRESSURE LOADS ON THE BUILDING.



NORTHWEST ELEVATION

CLADDING LOADS
REFERENCE PRESSURE = 48 PSF

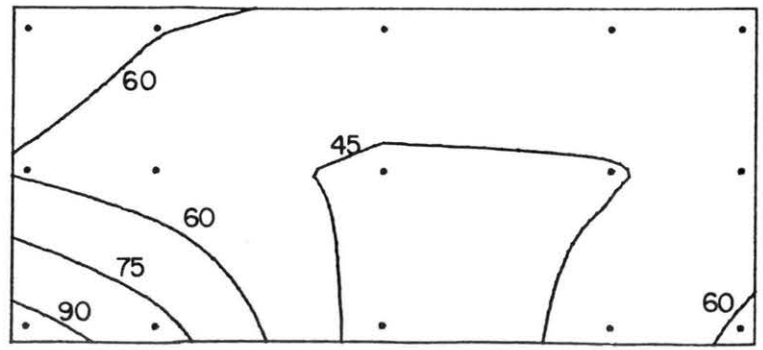


FIGURE 10d PEAK PRESSURE LOADS ON THE BUILDING.

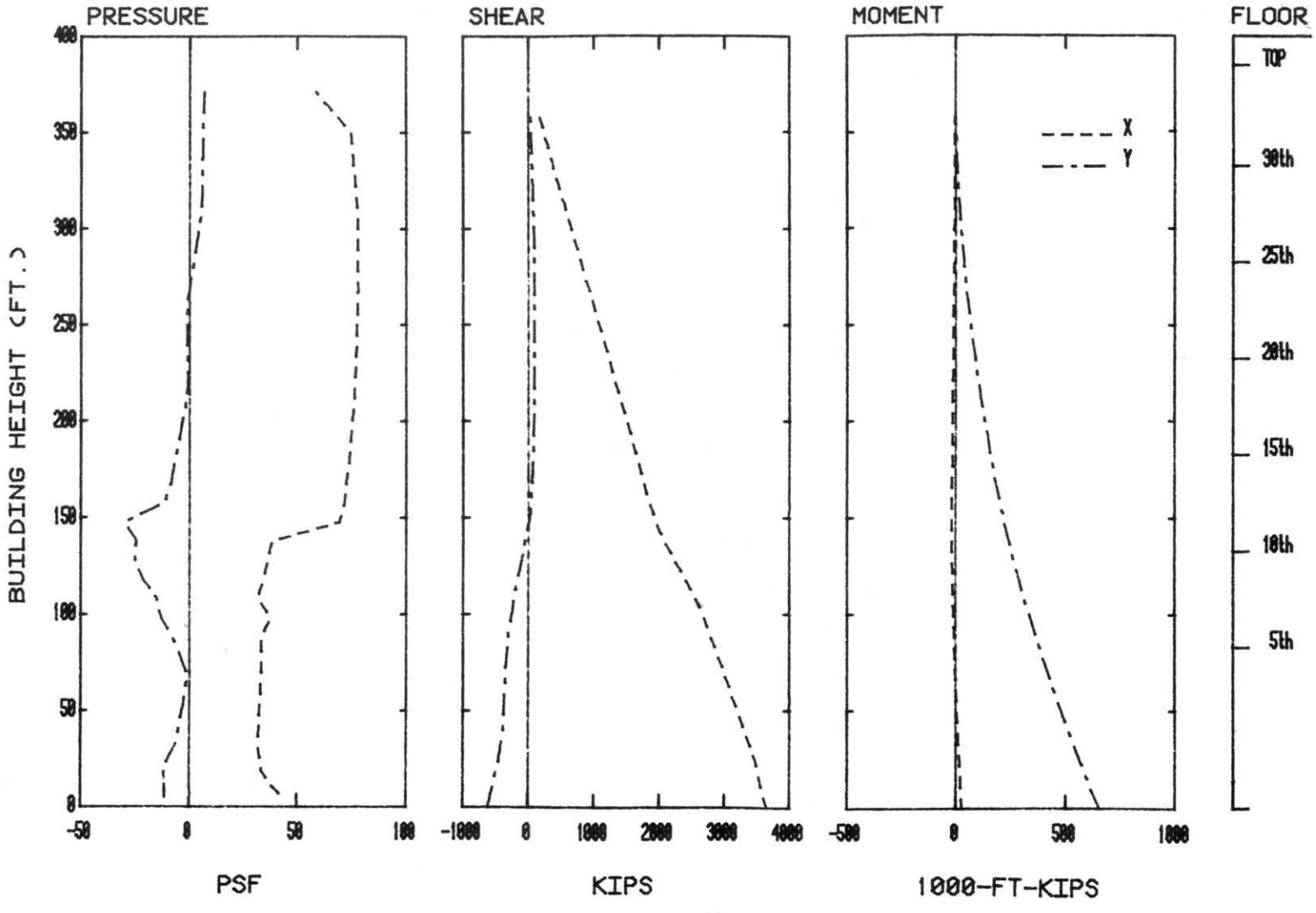


Figure 11. Load, Shear, and Moment Diagrams for Selected Wind Directions

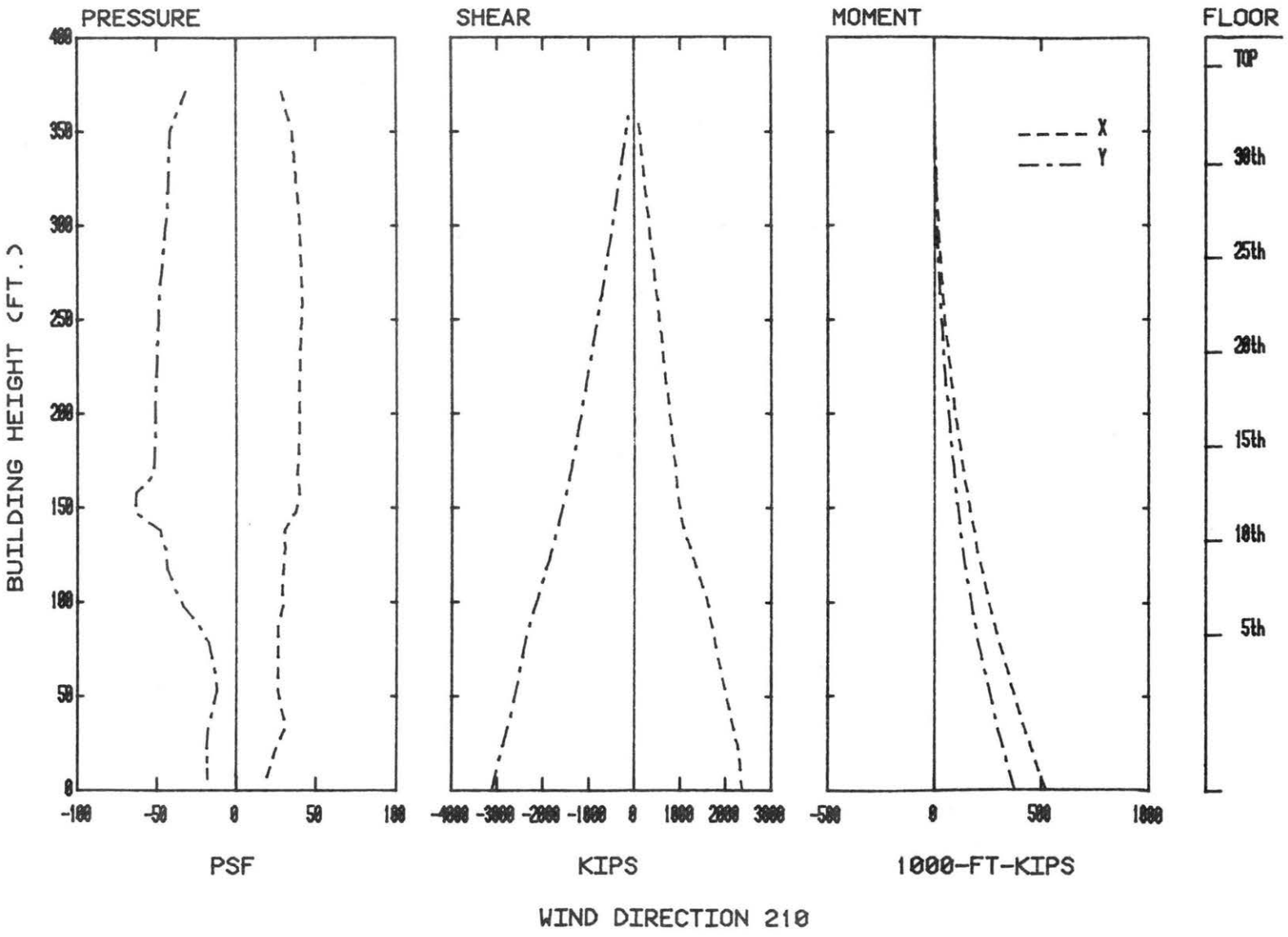


Figure 11. Load, Shear, and Moment Diagrams for Selected Wind Directions

TABLES

TABLE 1

MOTION PICTURE SCENE GUIDE

Run #	Approach Wind Azimuth, degrees
1	0
2	45
3	90
4	135
5	180
6	225
7	270
8	315

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

HARRAH'S HOLIDAY INN, ATLANTIC CITY

LOCATION 1

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	17.2	7.0	38.2
22.50	18.0	6.6	37.7
45.00	23.0	8.2	47.5
67.50	29.2	7.7	52.4
90.00	50.2	9.1	77.4
112.50	48.9	9.0	75.8
135.00	45.1	9.1	72.6
157.50	37.7	8.1	62.0
180.00	36.6	8.9	63.4
202.50	29.9	8.0	54.0
225.00	31.3	9.0	58.3
247.50	27.7	7.3	49.6
270.00	31.2	10.5	62.6
292.50	27.4	7.7	50.5
315.00	24.1	7.4	46.3
337.50	23.2	8.0	47.3

LOCATION 2

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	19.2	8.5	44.8
22.50	19.0	7.7	41.9
45.00	35.1	11.2	68.8
67.50	37.7	8.5	63.3
90.00	54.0	9.5	82.6
112.50	47.6	8.6	73.3
135.00	38.9	14.2	81.4
157.50	30.2	21.1	93.4
180.00	31.5	21.9	97.1
202.50	38.3	8.2	63.0
225.00	43.2	10.3	74.2
247.50	34.8	9.7	63.8
270.00	35.4	9.6	64.2
292.50	26.0	9.9	55.6
315.00	16.0	6.3	34.9
337.50	15.5	5.4	31.7

LOCATION 3

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	16.4	6.2	35.0
22.50	15.3	5.4	31.6
45.00	15.2	5.4	31.5
67.50	19.9	8.7	46.0
90.00	40.2	9.7	69.4
112.50	35.6	11.0	68.7
135.00	27.2	13.2	66.9
157.50	17.6	6.9	38.3
180.00	28.1	12.3	65.1
202.50	40.3	12.3	77.2
225.00	42.6	8.5	68.2
247.50	16.9	6.4	36.1
270.00	13.3	4.7	27.3
292.50	14.8	5.5	31.2
315.00	13.3	4.2	25.9
337.50	11.0	3.0	20.1

LOCATION 4

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	19.0	9.9	48.6
22.50	14.7	6.9	35.5
45.00	19.2	8.0	43.2
67.50	25.9	8.0	49.9
90.00	41.8	10.6	73.5
112.50	45.5	8.2	70.1
135.00	35.7	8.6	61.4
157.50	26.7	10.6	58.4
180.00	21.9	6.7	41.9
202.50	21.3	6.4	40.6
225.00	14.0	4.3	27.0
247.50	21.1	8.5	46.8
270.00	14.3	6.8	34.7
292.50	24.5	9.4	52.6
315.00	15.5	7.8	38.9
337.50	10.5	4.4	23.8

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

HARRAH'S HOLIDAY INN, ATLANTIC CITY

LOCATION 5

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	33.0	12.2	69.4
22.50	27.7	12.2	64.2
45.00	9.3	13.2	49.0
67.50	12.0	11.0	45.0
90.00	24.4	8.2	48.9
112.50	30.0	27.6	112.7
135.00	44.7	17.2	96.2
157.50	44.2	8.3	69.1
180.00	40.0	7.5	62.4
202.50	38.7	10.0	68.7
225.00	35.5	17.7	88.6
247.50	39.8	12.4	76.8
270.00	19.2	9.3	47.1
292.50	20.4	9.4	48.5
315.00	16.3	6.9	37.0
337.50	21.6	9.0	48.6

LOCATION 6

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	35.3	8.2	60.0
22.50	38.1	8.5	63.5
45.00	22.4	6.3	41.3
67.50	15.2	5.7	32.3
90.00	25.0	9.5	53.6
112.50	28.4	8.9	55.0
135.00	20.8	6.3	39.8
157.50	20.5	5.2	35.9
180.00	22.1	8.0	46.1
202.50	24.5	8.5	49.8
225.00	22.7	10.6	54.6
247.50	15.2	5.5	31.6
270.00	26.3	5.0	41.4
292.50	28.8	6.2	47.4
315.00	33.2	7.2	54.8
337.50	34.3	6.9	55.0

LOCATION 7

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	18.3	7.9	42.1
22.50	19.3	8.2	43.9
45.00	19.3	7.5	41.6
67.50	21.8	6.8	42.2
90.00	25.9	8.3	50.9
112.50	35.3	8.9	62.1
135.00	31.1	8.6	57.0
157.50	26.4	6.7	46.5
180.00	22.8	7.0	43.7
202.50	33.9	9.2	61.3
225.00	21.6	5.8	39.0
247.50	25.9	7.1	47.2
270.00	33.1	6.6	53.0
292.50	31.5	6.4	50.7
315.00	27.7	7.0	48.7
337.50	20.8	7.6	43.4

LOCATION 8

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	15.5	6.2	34.2
22.50	24.7	9.9	54.4
45.00	16.3	6.7	36.5
67.50	16.1	6.6	36.0
90.00	27.0	12.6	64.7
112.50	33.6	12.0	69.6
135.00	35.7	9.7	64.7
157.50	25.2	9.7	54.4
180.00	24.5	10.5	56.0
202.50	28.6	11.8	64.0
225.00	24.1	9.8	53.4
247.50	18.3	7.0	39.3
270.00	29.3	12.5	66.7
292.50	32.1	12.6	70.0
315.00	27.5	12.5	64.9
337.50	21.7	9.6	50.5

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES
HARRAH'S HOLIDAY INN, ATLANTIC CITY

LOCATION 9

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	41.1	9.8	70.6
22.50	45.9	10.5	77.3
45.00	27.4	8.7	53.5
67.50	13.1	5.4	29.3
90.00	32.2	11.7	67.3
112.50	21.4	8.0	45.3
135.00	17.9	6.3	36.9
157.50	17.0	5.0	32.1
180.00	19.2	6.2	37.9
202.50	20.8	8.1	45.1
225.00	21.8	7.3	43.8
247.50	34.9	10.0	64.9
270.00	30.3	7.7	53.4
292.50	38.2	8.6	64.0
315.00	35.1	7.7	58.2
337.50	39.3	8.6	65.2

LOCATION 10

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	26.4	9.3	54.3
22.50	27.5	10.0	57.5
45.00	26.6	10.1	57.0
67.50	10.3	3.2	20.0
90.00	32.6	15.0	77.7
112.50	20.9	8.2	45.3
135.00	16.9	5.3	32.7
157.50	15.6	4.5	29.1
180.00	29.2	6.9	50.0
202.50	32.5	8.4	57.6
225.00	24.8	9.8	54.2
247.50	26.9	9.4	55.2
270.00	25.6	11.2	59.2
292.50	28.9	10.6	60.7
315.00	23.0	9.1	50.3
337.50	22.4	8.6	48.1

LOCATION 11

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	21.9	6.3	40.8
22.50	22.4	7.1	43.8
45.00	13.6	5.2	29.1
67.50	10.9	2.8	19.2
90.00	14.5	4.3	27.4
112.50	17.0	5.5	33.6
135.00	24.4	6.0	42.3
157.50	19.1	4.5	32.6
180.00	13.7	4.3	26.6
202.50	23.0	7.8	46.2
225.00	13.3	3.8	24.7
247.50	32.8	8.1	57.3
270.00	30.5	7.1	51.9
292.50	29.1	8.8	55.4
315.00	27.7	11.7	62.8
337.50	22.9	9.2	50.4

LOCATION 12

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	21.9	8.3	46.9
22.50	25.7	9.3	53.5
45.00	9.6	3.1	18.9
67.50	10.1	2.1	16.3
90.00	46.7	14.7	90.9
112.50	55.0	16.4	104.2
135.00	36.8	11.6	71.6
157.50	36.8	11.6	71.7
180.00	38.6	11.1	71.8
202.50	39.5	10.7	71.7
225.00	36.9	10.5	68.4
247.50	40.3	12.5	77.8
270.00	19.7	6.5	39.2
292.50	13.3	4.4	26.5
315.00	10.5	2.5	18.1
337.50	13.2	5.8	30.7

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES
HARRAH'S HOLIDAY INN, ATLANTIC CITY

LOCATION 13

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	29.8	11.0	62.7
22.50	30.4	11.4	64.7
45.00	28.8	10.1	59.1
67.50	11.1	3.5	21.6
90.00	22.0	7.7	45.1
112.50	53.2	14.4	96.5
135.00	55.1	11.7	90.2
157.50	41.3	11.9	77.0
180.00	56.3	12.3	93.3
202.50	60.2	12.4	97.2
225.00	37.2	13.0	76.3
247.50	29.1	9.6	57.8
270.00	15.5	6.2	34.0
292.50	30.7	10.9	63.5
315.00	33.4	12.9	72.2
337.50	32.4	12.0	68.4

LOCATION 14

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	51.5	10.7	83.5
22.50	38.4	13.2	77.9
45.00	32.6	9.9	62.2
67.50	10.5	5.0	25.6
90.00	31.7	12.6	69.4
112.50	32.2	11.8	67.6
135.00	58.9	13.3	98.8
157.50	41.1	17.1	92.5
180.00	48.3	18.7	104.4
202.50	52.1	18.3	107.2
225.00	35.4	13.3	75.4
247.50	32.2	12.5	69.8
270.00	17.7	6.9	38.4
292.50	39.6	7.7	62.7
315.00	49.3	7.9	72.9
337.50	51.3	9.0	78.3

LOCATION 15

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	41.0	7.8	64.3
22.50	39.1	7.9	62.8
45.00	18.5	6.6	38.3
67.50	12.4	5.2	28.0
90.00	15.6	4.9	30.4
112.50	24.3	8.3	49.2
135.00	28.1	10.5	59.6
157.50	18.3	5.0	33.2
180.00	24.1	8.5	49.6
202.50	26.0	9.3	53.9
225.00	47.3	12.3	84.1
247.50	47.7	13.0	86.8
270.00	23.5	10.3	54.3
292.50	26.7	8.4	51.7
315.00	33.9	10.4	65.0
337.50	38.0	10.8	70.4

LOCATION 16

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	31.8	10.3	62.7
22.50	32.2	12.7	70.4
45.00	19.1	8.6	44.8
67.50	8.9	3.8	20.2
90.00	26.8	9.5	55.4
112.50	33.2	9.4	61.3
135.00	28.9	7.4	51.0
157.50	29.1	9.1	56.5
180.00	24.3	9.9	54.1
202.50	19.3	7.4	41.5
225.00	21.6	8.8	47.9
247.50	20.0	6.4	39.2
270.00	15.4	7.3	37.3
292.50	30.6	11.1	63.8
315.00	23.5	8.0	47.6
337.50	23.5	7.7	46.7

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

HARRAH'S HOLIDAY INN, ATLANTIC CITY

LOCATION 17

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	9.3	2.9	18.1
22.50	7.8	1.8	13.2
45.00	8.3	2.1	14.5
67.50	7.0	1.2	10.5
90.00	14.9	2.3	21.7
112.50	15.2	2.6	22.9
135.00	18.5	3.9	30.3
157.50	22.3	4.7	36.6
180.00	21.6	3.9	33.5
202.50	19.8	4.3	32.7
225.00	16.8	3.5	27.2
247.50	10.9	4.2	23.5
270.00	14.2	5.3	30.1
292.50	15.1	5.5	31.7
315.00	15.6	5.3	31.5
337.50	14.1	6.1	32.3

LOCATION 18

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	10.5	3.9	22.2
22.50	13.3	5.3	29.1
45.00	14.2	7.3	36.0
67.50	19.2	8.1	43.4
90.00	28.6	8.5	54.1
112.50	34.0	8.3	59.0
135.00	31.9	7.1	53.2
157.50	25.3	7.7	48.3
180.00	15.0	5.8	32.3
202.50	3.5	6.0	21.6
225.00	25.2	9.5	53.7
247.50	11.0	4.4	24.2
270.00	9.0	2.9	17.8
292.50	8.5	2.8	16.9
315.00	8.0	2.6	15.6
337.50	10.1	3.4	20.2

LOCATION 19

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	7.0	1.7	12.2
22.50	7.1	1.8	12.5
45.00	8.4	2.6	16.1
67.50	10.2	3.1	19.3
90.00	23.0	5.1	38.2
112.50	21.1	4.8	35.6
135.00	17.5	3.4	27.7
157.50	16.6	2.9	25.3
180.00	18.3	3.8	29.6
202.50	19.0	4.0	30.9
225.00	17.4	3.3	27.2
247.50	8.7	3.1	18.0
270.00	7.6	2.0	13.6
292.50	7.7	2.0	13.9
315.00	7.1	1.8	12.4
337.50	7.2	2.0	13.2

LOCATION 20

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	17.6	7.8	41.0
22.50	25.3	12.6	63.0
45.00	20.5	8.6	46.4
67.50	16.7	6.7	36.8
90.00	31.8	12.9	70.6
112.50	30.8	10.1	61.2
135.00	23.3	8.2	48.0
157.50	18.8	6.4	38.0
180.00	23.0	7.9	46.8
202.50	27.4	9.0	54.2
225.00	38.3	12.1	74.7
247.50	31.1	10.2	61.8
270.00	25.5	9.1	52.9
292.50	29.0	11.6	63.9
315.00	19.3	9.0	46.3
337.50	20.4	8.7	46.4

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

HARRAH'S HOLIDAY INN, ATLANTIC CITY

LOCATION 21

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	19.8	8.9	46.6
22.50	29.9	12.7	67.9
45.00	22.9	9.4	51.0
67.50	25.9	8.5	51.4
90.00	32.6	11.2	66.3
112.50	43.2	11.7	78.2
135.00	23.3	9.6	52.0
157.50	20.7	7.3	42.6
180.00	26.8	9.1	54.1
202.50	28.5	8.5	53.9
225.00	36.8	12.7	74.9
247.50	27.2	10.1	57.6
270.00	22.6	9.1	50.0
292.50	22.7	9.6	51.6
315.00	17.9	8.9	44.4
337.50	16.6	6.9	37.5

LOCATION 22

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	13.6	5.3	29.4
22.50	15.3	5.8	32.9
45.00	12.6	4.4	25.8
67.50	11.4	3.5	22.1
90.00	19.0	5.1	34.2
112.50	21.0	5.9	38.6
135.00	22.1	7.0	43.0
157.50	19.9	6.3	38.9
180.00	18.6	5.3	34.5
202.50	19.3	5.2	35.1
225.00	19.4	6.3	38.4
247.50	15.9	5.6	32.8
270.00	16.8	5.6	33.7
292.50	17.5	6.1	35.9
315.00	15.3	6.0	33.3
337.50	12.6	5.1	28.0

TABLE 3

PERCENTAGE FREQUENCY OF WIND DIRECTION AND SPEED

ATLANTIC CITY, NEW JERSEY NAT. AV. FAC. EXP. CTR.

SEASON : ANNUAL NO. OF OBS.= 29216 HT. OF MEAS.= 64. FT.

VELOCITY LEVELS IN MPH

DIRECTION	0- 3	4- 6	7-11	12-18	19-24	25-30	31-36	37 +	TOTAL
N	.30	2.40	3.30	1.50	.20	0.00	0.00	0.00	7.70
NNE	.20	1.00	1.10	.60	.10	0.00	0.00	0.00	2.90
NE	.10	1.00	1.10	.80	.20	0.00	0.00	0.00	3.30
ENE	.20	.90	1.20	1.30	.30	.10	0.00	0.00	4.00
E	.20	1.20	1.90	1.20	.20	.10	0.00	0.00	4.80
ESE	.20	.90	1.40	.70	.10	0.00	0.00	0.00	3.30
SE	.10	.80	1.20	.50	.10	0.00	0.00	0.00	2.80
SSE	.10	.80	1.40	.60	.10	0.00	0.00	0.00	3.10
S	.30	2.30	4.10	3.80	.60	.10	0.00	0.00	11.10
SSW	.20	1.60	2.70	1.90	.40	.10	0.00	0.00	6.90
SW	.20	1.70	2.30	1.30	.30	0.00	0.00	0.00	5.80
WSW	.20	2.20	3.00	1.60	.30	.10	0.00	0.00	7.40
W	.20	1.80	3.40	2.40	.80	.30	.10	0.00	9.00
WNW	.20	1.70	3.00	3.00	1.20	.40	.10	0.00	9.70
NW	.20	2.20	2.60	2.40	.90	.30	0.00	0.00	8.60
NNW	.20	1.50	1.80	1.40	.30	0.00	0.00	0.00	5.30
CALM	4.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	4.30
TOT	7.50	24.10	35.50	25.20	6.00	1.50	.30	0.00	100.00

TABLE 4

SUMMARY OF WIND EFFECTS ON PEOPLE

	Beaufort number	Speed (mph)	Effects
Calm, light air	0, 1	0- 3	Calm, no noticeable wind
Light breeze	2	4- 7	Wind felt on face
Gentle breeze	3	8-12	Wind extends light flag Hair is disturbed Clothing flaps
Moderate breeze	4	13-18	Raises dust, dry soil and loose paper Hair disarranged
Fresh breeze	5	19-24	Force of wind felt on body Drifting snow becomes airborne Limit of agreeable wind on land
Strong breeze	6	25-31	Umbrellas used with difficulty Hair blown straight Difficult to walk steadily Wind noise on ears unpleasant Windborne snow above head height (blizzard)
Near gale	7	32-38	Inconvenience felt when walking
Gale	8	39-46	Generally impedes progress Great difficulty with balance in gusts
Strong gale	9	47-54	People blown over by gusts

Note: Table from Reference 4, p. 40.

TABLE 5

CALCULATION OF REFERENCE PRESSURE

1. Basic wind speed from ANSI A58.1 (ref 6):

   100-yr fastest mile at 30 ft = 105 mph

   Mean hourly wind speed, 30 ft = 105/1.30 = 80.8 mph

   Mean hourly gradient wind speed = $80.8 \left(\frac{1000}{30}\right)^{0.15} = 136.7$ mph

   Reference wind speed U_∞ = gradient wind speed

   Reference pressure = $0.5 \rho U_\infty^2 = (0.00256)(136.7)^2 = 47.9$ psf

   Use 48 psf

2. Loads for 50-yr recurrence wind:

   50-yr fastest mile at 30 ft = 90 mph.

   Multiply 100-yr loads by $\left(\frac{90}{105}\right)^2 = 0.73$

3. Gust load factors to convert hourly mean integrated loads to various gust durations (see Sect. 4.4):

Gust Duration, sec	Gust Load Factor
10-15	$(1.4)^2 = 1.96$
30	$(1.32)^2 = 1.74$
45	$(1.26)^2 = 1.59$

TABLE 6 : PEAK LOADS FOR CONFIGURATION A : HARRAH'S HOLIDAY INN -- ATLANTIC CITY
LARGEST VALUE OF MAXIMUM OR MINIMUM PRESSURE AND LARGEST POSITIVE VALUE
REFERENCE PRESSURE USED = 48 PSF

TAP	AZIMUTH	PRESS COEFF	ABS PEAK LOAD (PSF)	POS PEAK LOAD (PSF)
1101	140	2.14	102.8	58.0
1102	130	1.68	80.5	63.2
1103	140	1.44	69.2	59.7
1104	150	1.33	63.8	55.8
1105	150	1.61	77.2	49.7
1106	340	1.51	72.6	44.6
1107	160	1.88	90.4	51.3
1108	140	1.51	72.3	62.4
1109	70	1.59	76.3	76.3
1110	140	1.43	68.7	62.9
1111	160	1.44	69.2	61.8
1112	160	1.51	72.7	66.7
1113	160	1.65	79.3	48.2
1114	160	1.84	88.5	45.2
1115	90	1.40	67.3	67.3
1116	130	1.41	67.5	66.9
1117	140	1.68	80.7	60.4
1118	140	1.62	77.9	53.3
1119	140	1.44	69.1	53.4
1120	140	1.57	75.4	47.5
1121	160	1.87	89.9	52.3
1122	120	1.43	68.4	64.2
1123	140	1.40	67.4	60.4
1124	140	1.48	71.2	52.9
1125	150	1.50	72.1	55.2
1126	150	1.47	70.5	42.8
1127	160	1.53	73.6	48.9
1128	160	2.28	109.6	44.7
1129	140	1.47	70.7	59.9
1130	140	1.54	74.1	58.4
1131	140	1.87	89.7	54.0
1132	140	1.51	72.3	47.7
1133	150	1.49	71.5	39.1
1134	350	1.53	73.2	38.5
1135	340	1.39	66.8	40.2
1136	150	2.68	128.5	42.3
1137	130	2.25	108.2	40.7
1138	160	1.60	76.7	37.6
1139	160	1.45	69.7	39.8
1140	330	1.82	87.6	33.2
1141	330	2.04	98.1	35.9
1142	330	1.66	79.5	37.1
1143	150	1.41	67.6	30.9
1144	210	1.18	56.9	37.0
1145	180	1.02	49.2	41.2
1146	80	.91	43.5	43.5
1147	320	1.29	61.9	45.3
1148	320	1.53	73.5	35.3
1149	240	1.64	78.8	33.2
1150	210	.95	45.8	44.0
1151	70	1.05	50.4	50.4
1152	330	1.63	78.2	44.0
1201	100	1.28	61.3	61.3
1202	230	1.19	57.3	28.2
1203	230	1.50	72.0	37.6
1204	230	1.28	61.6	40.7
1205	230	1.37	65.9	38.5
1206	320	1.18	56.6	36.9
1207	320	1.30	62.3	41.7
1208	80	1.58	75.9	46.9
1209	70	2.26	108.6	49.9
1210	120	1.32	63.5	63.5
1211	180	1.22	58.3	58.3
1212	190	1.25	60.0	60.0
1213	190	1.21	57.9	57.9
1214	170	1.39	66.5	66.5
1215	160	1.37	65.8	65.8
1216	80	1.36	65.3	62.3
1217	70	1.77	84.9	60.3
1218	80	2.11	101.2	57.2
1219	140	1.24	59.3	59.3
1220	190	1.17	56.1	56.1
1221	180	1.26	60.3	60.3
1222	170	1.32	63.1	63.1
1223	160	1.28	61.6	61.6
1224	170	1.42	68.2	68.2
1225	240	1.34	64.3	64.0
1226	70	1.99	95.6	62.0
1227	70	2.25	107.9	64.2
1228	230	1.37	65.6	62.4
1229	190	1.27	60.7	60.7
1230	220	1.46	70.3	66.3
1231	230	1.64	78.7	70.7
1232	230	1.56	75.0	68.3
1233	240	1.48	71.2	62.7
1234	230	1.45	69.4	59.3
1235	70	2.30	110.5	63.2
1236	70	2.48	119.2	60.6
1237	190	1.26	60.7	60.7
1238	190	1.27	61.0	61.0
1239	200	1.30	62.5	62.5
1240	230	1.68	80.5	58.1
1241	230	1.70	81.8	59.6
1242	230	1.42	68.0	58.0
1243	230	1.25	60.0	59.3
1244	60	1.67	80.2	59.7
1245	70	1.81	86.7	62.3
1246	110	1.44	69.3	69.3
1247	190	1.24	59.5	59.5
1248	230	1.31	62.7	60.1
1249	230	1.17	56.2	55.4
1250	230	1.17	56.2	53.6
1251	170	1.22	58.4	58.4
1252	120	1.16	55.5	55.5
1253	70	1.94	93.1	55.5
1254	240	1.73	83.1	53.5
1301	310	1.72	82.6	44.7
1302	90	1.53	73.3	39.5
1303	160	1.70	81.7	42.3
1304	80	1.49	71.7	42.3
1305	160	1.90	91.4	42.8
1306	160	1.81	87.0	50.3
1307	170	2.07	99.4	53.6
1308	150	1.68	80.8	43.2
1309	150	1.72	82.8	45.4
1310	160	1.64	78.9	55.7
1311	160	1.58	75.8	58.9
1312	170	1.46	70.1	64.1
1313	170	1.55	74.3	59.1
1314	170	1.48	71.0	63.5
1315	150	1.79	85.7	38.5
1316	150	1.60	76.6	46.9
1317	160	1.43	68.7	57.7
1318	160	1.68	80.5	69.5
1319	170	1.50	72.0	65.9
1320	170	1.37	65.7	59.1
1321	170	1.45	69.4	59.1
1322	160	1.91	91.8	39.0
1323	160	1.79	86.1	41.9
1324	160	1.46	70.2	52.4
1325	160	1.70	81.7	65.9
1326	160	2.09	100.5	66.9
1327	160	1.73	82.9	54.9
1328	160	1.53	73.3	55.3
1329	150	1.68	80.7	37.7
1330	310	1.50	72.0	41.7
1331	160	1.52	72.9	51.8
1332	160	1.65	79.1	53.6
1333	160	1.97	94.5	65.3
1334	170	1.96	94.1	57.8
1335	160	2.07	99.4	60.0
1336	320	1.51	72.6	53.6
1337	140	1.09	52.4	47.7
1338	330	1.32	63.5	60.1
1339	160	1.57	75.3	54.1
1340	170	1.52	72.9	56.1
1401	70	1.95	93.8	43.1
1402	70	1.85	88.9	29.9
1403	70	2.05	98.5	28.6
1404	70	2.07	99.1	38.4

TABLE 6 : PEAK LOADS FOR CONFIGURATION A : HARRAH'S HOLIDAY INN -- ATLANTIC CITY
LARGEST VALUE OF MAXIMUM OR MINIMUM PRESSURE AND LARGEST POSITIVE VALUE
REFERENCE PRESSURE USED = 48 PSF

TAP	AZI-MUTH	PRESS COEFF	ABS PEAK LOAD (PSF)	POS PEAK LOAD (PSF)
1405	70	1.66	79.8	34.9
1406	70	1.49	71.3	29.4
1407	80	1.33	64.1	31.0
1408	80	1.51	72.7	39.0
1409	80	1.77	84.9	40.7
1410	70	1.35	65.0	51.9
1411	70	1.34	64.2	44.5
1412	70	1.63	78.1	46.7
1413	70	1.45	69.6	45.6
1414	70	1.20	57.4	42.6
1415	80	1.05	50.5	43.1
1416	80	1.16	55.6	48.4
1417	80	1.42	68.0	49.1
1418	80	1.76	84.3	46.6
1419	70	1.26	60.5	50.0
1420	70	1.12	53.8	47.9
1421	70	1.81	87.0	47.1
1423	240	1.21	58.2	47.8
1424	70	1.17	56.0	44.6
1425	250	1.10	52.9	45.2
1426	80	1.29	61.8	40.5
1427	80	1.26	60.6	43.6
1428	70	1.18	56.4	48.4
1429	70	1.09	52.3	47.7
1430	70	1.26	60.4	41.6
1431	70	1.35	64.9	40.4
1432	70	1.45	69.7	41.3
1433	240	1.24	59.4	44.8
1434	240	1.28	61.5	43.2
1435	240	1.43	68.5	43.9
1436	160	1.43	68.9	45.5
1437	60	1.07	51.1	45.7
1438	70	1.07	51.4	44.3
1439	70	2.13	102.0	43.8
1440	70	1.21	58.3	41.0
1441	70	1.39	66.9	41.3
1442	210	1.25	60.1	38.2
1443	240	2.01	96.6	36.2
1444	240	1.61	77.2	43.1
1445	240	1.48	71.2	38.7
1446	80	1.03	49.4	37.5
1447	70	.95	45.8	41.2
1448	70	1.15	55.1	35.4
1449	70	1.23	59.0	36.8
1450	240	1.10	53.0	36.4
1451	80	1.31	62.9	32.1
1452	80	1.73	83.0	33.2
1453	240	1.68	80.6	35.9
1454	240	1.85	88.9	45.1
1455	80	1.36	65.1	43.3
1456	80	1.52	72.8	36.7
1457	80	1.50	71.8	36.3
1458	70	1.83	87.7	37.8
1459	70	1.78	85.3	36.6
1460	80	1.90	91.4	42.2
1461	90	1.12	53.6	41.0
1462	90	1.18	56.5	39.2
1463	80	1.24	59.5	40.1
1464	80	1.25	60.1	60.1
1465	130	.80	38.5	34.4
1466	150	.88	42.1	29.9
1467	150	.84	40.4	29.9
1801	130	.75	36.0	24.1
1802	180	.78	37.5	21.0
1803	90	.69	32.9	27.4
1804	90	.62	30.0	28.5
1805	190	.89	42.6	17.8
1806	90	.87	41.8	19.3
1807	150	.77	37.0	21.2
2101	90	1.44	69.1	69.1
2102	150	2.03	97.6	34.1
2103	80	1.40	67.3	37.5
2104	150	1.16	55.7	36.8
2105	90	1.18	56.6	56.6
2106	100	1.15	55.4	55.4
2107	160	2.15	103.3	40.0
2108	150	2.00	96.1	37.9
2109	100	1.04	50.0	50.0
2110	230	.82	39.5	35.5
2111	190	1.36	65.2	46.4
2112	210	1.09	52.1	41.3
2113	70	1.20	57.7	30.1
2114	170	1.23	59.2	34.0
2115	140	1.25	60.0	32.1
2116	90	.79	37.7	37.7
2117	90	1.14	54.7	23.4
2118	90	1.35	64.8	24.9
2119	100	1.06	50.9	25.3
2120	70	1.18	56.6	25.6
2121	300	1.17	56.1	27.3
2122	90	.84	40.2	40.2
2123	90	1.40	67.1	22.5
2124	170	.93	44.8	27.3
2125	190	1.09	52.1	30.1
2126	80	.82	39.2	39.2
2127	80	.80	38.5	38.5
2128	90	.96	46.2	46.2
2129	140	.90	43.4	28.8
2130	130	.84	40.2	24.4
2131	230	1.07	51.6	26.7
2132	230	1.03	49.5	27.1
2133	230	.85	40.7	24.9
2134	210	.73	34.9	34.9
2135	100	.93	44.4	30.4
2136	350	.88	42.3	20.2
2137	100	.69	33.1	33.1
2138	140	.74	35.7	28.1
2139	80	.82	39.2	26.5
2140	140	.85	40.6	21.0
2141	110	.87	41.6	24.8
2142	210	.97	46.7	25.2
2143	240	1.09	52.4	39.6
2144	240	.86	41.4	34.4
2145	230	.91	43.9	28.3
2146	220	.66	31.8	31.8
2147	100	.82	39.6	36.9
2148	240	.76	36.3	36.3
2149	130	.69	33.0	32.4
2150	140	.77	37.1	36.8
2151	90	.73	35.2	35.2
2152	90	.93	44.6	44.6
2153	130	.78	37.2	31.2
2154	310	1.27	60.9	22.6
2201	150	1.22	58.4	58.4
2202	240	1.35	64.6	64.4
2203	230	1.18	56.8	56.4
2204	230	1.32	63.3	60.5
2205	240	1.27	61.0	58.4
2206	130	.96	46.1	46.1
2207	150	.94	45.0	45.0
2208	240	.96	45.8	44.4
2209	230	1.04	49.7	49.3
2210	120	1.10	52.9	52.9
2211	230	.99	47.7	42.3
2212	230	.91	43.7	39.2
2213	160	.94	45.0	45.0
2214	230	1.00	47.9	43.5
2215	230	.86	41.4	37.3
2216	230	.84	40.3	40.3
2217	100	.87	41.6	41.6
2218	110	1.10	53.0	53.0
2219	100	.91	43.8	43.8
2220	240	1.22	58.7	39.5
2221	150	.73	35.1	35.1
2222	0	.80	38.5	38.1
2224	140	.75	36.1	36.1
2225	70	.89	42.5	42.3
2226	110	.70	33.4	27.5
2227	180	.68	32.6	32.6
2228	160	.65	31.0	31.0

TABLE 6 : PEAK LOADS FOR CONFIGURATION A : HARRAH'S HOLIDAY INN -- ATLANTIC CITY
LARGEST VALUE OF MAXIMUM OR MINIMUM PRESSURE AND LARGEST POSITIVE VALUE
REFERENCE PRESSURE USED = 48 PSF

TAP	AZI-MUTH	PRESS COEFF	ABS PEAK LOAD (PSF)	POS PEAK LOAD (PSF)
2229	150	1.02	49.1	49.1
2230	130	1.54	73.9	73.9
2231	160	.88	42.0	42.0
2232	160	1.10	52.6	52.6
2233	160	1.08	51.9	51.9
2234	170	.86	41.4	41.4
2235	160	.81	39.0	39.0
2236	180	.87	41.7	41.7
2237	180	.89	42.8	42.8
2238	180	.89	42.6	42.6
2239	180	.87	41.9	41.9
2240	130	.74	35.7	35.7
2301	160	1.77	84.7	63.2
2302	160	1.54	74.2	45.6
2303	200	1.16	55.6	55.6
2304	150	1.16	55.6	55.6
2305	80	1.24	59.6	45.5
2306	90	1.00	48.0	36.0
2307	170	1.30	62.4	34.0
2308	170	1.25	59.8	51.5
2309	140	1.29	61.9	35.8
2310	260	.96	45.9	40.8
2311	190	.94	45.3	45.3
2312	180	1.01	48.6	48.6
2313	210	1.05	50.2	50.2
2314	350	.91	43.7	37.2
2315	210	1.04	49.8	49.8
2401	330	1.19	57.3	49.3
2402	170	1.55	74.6	56.0
2403	160	1.45	69.7	50.4
2404	230	1.29	62.1	59.7
2405	140	.97	46.5	44.3
2406	190	1.87	89.7	57.5
2407	150	1.03	49.7	43.7
2408	150	1.12	53.7	41.7
2409	230	1.33	63.7	45.2
2411	140	1.05	50.2	36.2
2412	140	.97	46.4	45.9
2413	140	1.16	55.8	43.1
2414	230	1.13	54.4	39.0
2415	170	.91	43.5	43.5
2416	160	1.66	79.6	38.4
2417	120	.90	43.1	33.6
2418	230	.95	45.7	45.7
2419	110	1.16	55.8	46.2
2420	110	1.07	51.1	46.9
2421	160	.77	36.9	32.0
2422	140	1.63	78.3	39.7
2423	220	.93	44.5	44.5
2424	230	.90	43.4	43.4
2425	230	.99	47.5	47.5
2426	160	1.44	69.0	40.4
2427	210	.91	43.6	43.6
2428	160	1.46	70.0	44.2
2429	350	1.16	55.8	32.5
2430	220	.95	45.7	45.7
2431	240	.87	41.7	41.7
2432	150	1.13	54.1	45.4
2433	210	1.19	57.1	57.1
2434	220	1.03	49.4	49.4
2435	220	1.06	50.9	50.9
2436	240	.94	45.3	45.3
2437	240	.80	38.2	38.2
2438	220	.78	37.7	37.7
2439	110	.82	39.3	37.2
2440	210	.95	45.6	45.6
2441	210	.88	42.0	42.0
2442	240	.82	39.5	39.5
2443	220	.81	38.7	38.7
2444	330	.96	46.3	26.6
2445	120	.69	33.3	22.5
2446	120	.77	37.1	23.0
2447	130	.70	33.6	23.9
2448	230	.71	34.0	34.0
2449	210	.70	33.6	33.6
2450	160	1.29	61.7	31.2
2451	220	1.07	51.2	51.2
2501	240	1.22	58.7	58.7
2502	240	1.45	69.5	69.5
2503	240	1.44	68.9	33.7
2504	160	1.09	52.6	43.9
2505	230	1.60	76.9	30.3
2506	80	1.44	68.9	39.0
2507	150	1.13	54.0	37.4
2508	180	1.16	55.5	34.8
2509	160	2.29	110.1	24.8
2510	220	2.65	127.2	23.2
2511	140	1.01	48.6	36.6
2601	90	1.45	69.4	39.0
2602	100	1.26	60.6	38.1
2603	100	1.15	55.4	34.4
2604	180	1.10	52.9	40.7
2605	190	1.04	49.8	38.4
2606	130	.83	39.7	32.3
2607	80	1.14	54.8	32.6
2608	90	1.20	57.8	34.5
2609	90	1.06	50.7	33.0
2610	190	.88	42.3	31.9
2611	220	.92	44.2	31.4
2612	230	1.01	48.6	33.1
2613	180	.79	37.8	33.7
2614	180	.75	36.1	35.0
2615	90	1.97	94.6	21.7
2616	90	1.66	79.6	23.1
2617	110	.78	37.5	22.1
2618	190	1.00	47.9	22.4
2619	230	1.28	61.7	19.6
2620	170	.78	37.3	25.5
2621	160	.84	40.3	39.1
5102	170	1.34	64.3	39.7
5103	90	1.60	76.6	31.9
5104	170	1.20	57.7	37.4
5105	180	1.86	89.1	41.2
5106	310	1.02	49.1	38.3
5107	120	1.96	94.0	22.9
5108	160	1.31	63.1	24.1
5109	330	1.30	62.3	26.9
5110	120	.93	44.5	40.2
5111	180	1.10	53.0	23.8
5112	120	.72	34.6	23.4
5114	340	.81	38.8	38.8
5202	140	1.17	56.2	56.2
5203	150	.96	46.1	46.1
5204	210	.72	34.7	34.7
5301	150	1.00	48.1	43.5
5302	150	.90	43.4	41.0
5303	90	1.28	61.6	39.4
5304	120	1.22	58.5	34.1
5305	130	.85	41.0	23.8
5901	180	1.23	59.2	37.8
5902	190	1.18	56.5	23.1
6101	240	1.11	53.3	53.3
6102	140	1.27	60.7	53.2
6103	90	.97	46.5	30.1
6104	160	1.49	71.4	29.9
6105	100	.79	37.9	25.7
6106	100	.59	28.2	25.9
6201	150	1.11	53.4	53.4
6301	120	.82	39.5	34.8
6302	240	.86	41.2	41.2
6901	260	1.60	76.8	20.1
7101	200	1.10	52.8	50.1
7102	210	2.35	112.6	26.1
7103	10	1.03	49.3	22.6
7104	180	1.94	93.0	28.5
7105	190	.85	40.8	23.9
7106	190	.78	37.3	22.1
7201	240	1.04	49.8	37.1
7301	210	1.17	56.1	56.1
9101	70	1.21	58.2	12.0

TABLE 6 : PEAK LOADS FOR CONFIGURATION A : HARRAH'S HOLIDAY INN -- ATLANTIC CITY
LARGEST VALUE OF MAXIMUM OR MINIMUM PRESSURE AND LARGEST POSITIVE VALUE
REFERENCE PRESSURE USED = 48 PSF

TAP	AZI-MUTH	PRESS COEFF	ABS PEAK LOAD (PSF)	POS PEAK LOAD (PSF)
9102	140	1.40	67.2	33.5
9103	80	1.13	54.1	54.1
9104	80	1.36	65.4	33.5
9105	150	1.33	63.6	15.8
9106	120	.88	42.4	39.1
9107	150	1.31	62.9	13.8
9108	330	1.40	67.3	59.3
9109	160	2.01	96.6	63.0
9110	80	1.79	86.0	30.8
9111	150	1.51	72.4	58.6
9112	160	1.71	82.0	21.3
9113	150	1.25	59.8	42.6
9114	150	1.36	65.3	46.9
9115	140	1.23	59.2	38.0
9116	130	1.08	51.7	41.6
9117	140	1.46	69.9	38.6
9118	140	.91	43.8	35.7
9119	80	1.26	60.4	27.3
9120	80	.90	43.0	38.8
9121	110	1.02	49.1	46.5
9122	130	1.16	55.5	44.1
9123	180	1.72	82.3	26.8
9124	240	.98	47.0	44.8
9125	120	.92	44.2	27.9
9126	110	1.18	56.7	34.1
9201	240	1.99	95.7	49.6
9202	80	1.32	63.4	63.4
9203	220	1.13	54.2	39.7
9204	90	.93	44.6	44.6
9205	90	.82	39.5	26.2
9206	240	.69	32.9	31.4
9207	130	1.35	64.6	64.6
9208	100	1.02	49.0	49.0
9209	90	.86	41.1	41.1
9210	350	.83	39.8	28.0
9211	70	.71	34.1	27.5
9212	230	1.13	54.3	53.1
9213	160	.79	37.7	37.7
9214	0	.84	40.3	32.6
9215	10	.98	47.0	28.8
9216	0	.70	33.4	28.6
9217	140	.76	36.4	36.4
9218	170	.75	36.0	36.0
9219	160	1.33	64.1	64.1
9220	230	1.18	56.5	48.3
9221	160	.84	40.3	40.3
9222	350	.90	43.4	30.6
9223	10	.91	43.8	29.1
9224	210	.55	26.3	26.3
9225	230	1.03	49.5	48.3
9226	230	.90	43.3	42.3
9227	170	.68	32.4	32.4
9228	350	.61	29.4	29.3
9229	230	1.17	56.1	47.8
9230	10	.99	47.7	30.3
9231	10	.64	30.9	25.5
9232	240	1.09	52.5	45.0
9233	230	.90	43.2	38.6
9234	230	.88	42.0	31.7
9235	100	.62	29.8	28.2
9236	240	1.10	52.7	33.8
9237	240	.85	40.7	28.7
9238	160	.62	30.0	30.0

TABLE 6 : PEAK LOADS FOR CONFIGURATION B : HARRAH'S HOLIDAY INN -- ATLANTIC CITY
LARGEST VALUE OF MAXIMUM OR MINIMUM PRESSURE AND LARGEST POSITIVE VALUE
REFERENCE PRESSURE USED = 48 PSF

TAP	AZI-MUTH	PRESS COEFF	ABS PEAK LOAD (PSF)	POS PEAK LOAD)
1101	130	2.05	98.3	50.0
1104	160	1.65	79.1	39.0
1107	150	1.55	74.6	42.2
1122	90	1.58	75.8	75.8
1125	140	1.54	73.9	57.6
1128	140	1.46	70.0	44.7
1136	150	3.21	154.0	37.1
1139	150	1.37	65.7	37.2
1142	330	1.83	88.0	45.9
1149	330	1.64	78.6	38.1
1201	110	1.25	59.8	59.8
1204	60	1.16	55.4	42.1
1209	70	1.91	91.8	49.8
1219	140	1.46	70.0	70.0
1223	170	1.24	59.7	59.7
1227	80	1.36	65.4	57.0
1246	80	1.44	69.2	69.2
1249	160	1.20	57.6	57.6
1254	70	2.46	117.9	57.1
1301	150	1.68	80.8	13.4
1304	150	1.49	71.7	14.6
1307	170	1.79	86.0	16.7
1322	150	1.89	90.8	8.9
1325	160	1.30	62.6	18.6
1328	170	1.94	93.0	12.7
1336	150	1.09	52.5	14.3
1339	160	1.22	58.3	12.7
1401	150	1.02	48.8	38.8
1404	150	1.10	52.6	34.9
1409	70	1.66	79.7	29.9
1419	350	.95	45.6	45.6
1423	50	.99	47.4	44.4
1427	70	1.89	90.8	25.2
1446	60	1.66	79.7	39.9
1449	70	1.44	69.1	43.8
1454	70	1.25	60.2	30.4
2104	150	1.08	52.0	40.5
2106	130	1.00	47.9	47.9
2137	110	.83	39.8	39.8
2206	110	1.06	51.0	51.0
2210	110	1.10	52.7	52.7
2225	150	.83	39.8	39.8
2226	130	.59	28.2	28.2
2407	150	.93	44.8	14.8
2409	150	.96	46.1	46.1
2601	70	1.33	63.9	39.0
2606	70	1.18	56.7	37.1
9101	170	1.04	49.7	8.1
9107	140	1.17	56.2	5.5

TABLE 6 : PEAK LOADS FOR CONFIGURATION C : HARRAH'S HOLIDAY INN -- ATLANTIC CITY
LARGEST VALUE OF MAXIMUM OR MINIMUM PRESSURE AND LARGEST POSITIVE VALUE
REFERENCE PRESSURE USED = 48 PSF

TAP	AZI-MUTH	PRESS COEFF	ABS PEAK LOAD (PSF)	POS PEAK LOAD (PSF)	TAP	AZI-MUTH	PRESS COEFF	ABS PEAK LOAD (PSF)	POS PEAK LOAD (PSF)	TAP	AZI-MUTH	PRESS COEFF	ABS PEAK LOAD (PSF)	POS PEAK LOAD (PSF)
5102	150	1.36	65.4	48.9	5204	30	.76	36.4	29.0	6106	140	1.13	54.4	34.5
5103	140	1.50	71.9	51.4	5301	350	.89	42.8	42.8	6201	170	1.08	52.0	52.0
5104	170	1.15	55.4	37.6	5302	90	.88	42.0	40.6	6301	110	.83	39.8	35.4
5105	140	1.77	84.9	50.1	5303	90	1.27	61.0	35.9	6302	170	.85	40.7	34.6
5106	170	.91	43.8	34.9	5304	160	.83	39.9	32.4	6901	210	1.24	59.5	22.4
5107	150	1.44	69.0	32.6	5305	90	1.00	48.0	26.7	7101	230	.76	36.6	36.6
5108	160	1.10	52.8	34.9	5901	170	1.14	54.7	40.1	7102	190	1.42	68.2	48.3
5109	330	1.07	51.4	26.7	5902	160	1.47	70.3	24.9	7103	320	.78	37.4	28.9
5110	110	.78	37.5	27.4	6101	150	1.01	48.3	47.8	7104	200	1.11	53.1	30.6
5111	160	1.26	60.6	27.6	6102	160	1.20	57.6	54.0	7105	170	.91	43.5	28.3
5112	190	.83	40.0	21.2	6103	270	1.26	60.4	28.9	7106	120	.88	42.1	40.4
5114	130	.71	34.2	24.6	6104	150	1.57	75.6	43.4	7201	260	.76	36.6	32.6
5202	90	1.27	60.9	58.3	6105	150	1.19	57.3	28.7	7301	190	1.13	54.0	54.0
5203	150	1.01	48.5	48.5										

TABLE 6 --PEAK ABSOLUTE LOADS- CONFIGURATIONS A & B- HARRAH'S HOLIDAY INN -- ATLANTIC CITY
TAPS WHERE PEAK LOADS FOR CONFIGURATION A EXCEED THOSE FOR B BY 5.0 PSF OR MORE - REF. PRESS. = 48 PSF

CONFIGURATION A				CONFIGURATION B				DIFFERENCE		
TAP	AZI-MUTH	PRESS COEFF	PSF LOAD	TAP	AZI-MUTH	PRESS COEFF	PSF LOAD	TAP	PRESS COEFF	PSF LOAD
1107	160	1.88	90.4	1107	150	1.55	74.6	1107	.33	15.8
1128	160	2.28	109.6	1128	140	1.46	70.0	1128	.82	39.6
1204	230	1.28	61.6	1204	60	1.16	55.4	1204	.13	6.1
1209	70	2.26	108.6	1209	70	1.91	91.8	1209	.35	16.8
1227	70	2.25	107.9	1227	80	1.36	65.4	1227	.89	42.5
1307	170	2.07	99.4	1307	170	1.79	86.0	1307	.28	13.4
1325	160	1.70	81.7	1325	160	1.30	62.6	1325	.40	19.0
1336	320	1.51	72.6	1336	150	1.09	52.5	1336	.42	20.1
1339	160	1.57	75.3	1339	160	1.22	58.3	1339	.35	17.0
1401	70	1.95	93.8	1401	150	1.02	48.8	1401	.94	45.0
1404	70	2.07	99.1	1404	150	1.10	52.6	1404	.97	46.5
1409	80	1.77	84.9	1409	70	1.66	79.7	1409	.11	5.3
1419	70	1.26	60.5	1419	350	.95	45.6	1419	.31	14.9
1423	240	1.21	58.2	1423	50	.99	47.4	1423	.23	10.9
1454	240	1.85	88.9	1454	70	1.25	60.2	1454	.60	28.7
2106	100	1.15	55.4	2106	130	1.00	47.9	2106	.16	7.5
2226	110	.70	33.4	2226	130	.59	28.2	2226	.11	5.2
2409	230	1.33	63.7	2409	150	.96	46.1	2409	.37	17.6
2601	90	1.45	69.4	2601	70	1.33	63.9	2601	.12	5.6
9101	70	1.21	58.2	9101	170	1.04	49.7	9101	.18	8.5
9107	150	1.31	62.9	9107	140	1.17	56.2	9107	.14	6.7

TABLE 6 --PEAK POSITIVE LOADS- CONFIGURATIONS A & B- HARRAH'S HOLIDAY INN -- ATLANTIC CITY
TAPS WHERE PEAK LOADS FOR CONFIGURATION A EXCEED THOSE FOR B BY 5.0 PSF OR MORE - REF. PRESS. = 48 PSF

CONFIGURATION A				CONFIGURATION B				DIFFERENCE		
TAP	AZIMUTH	PRESS COEFF	PSF LOAD	TAP	AZIMUTH	PRESS COEFF	PSF LOAD	TAP	PRESS COEFF	PSF LOAD
1101	70	1.21	58.0	1101	90	1.04	50.0	1101	.17	8.0
1104	70	1.16	55.8	1104	80	.81	39.0	1104	.35	16.8
1107	60	1.07	51.3	1107	30	.88	42.2	1107	.19	9.1
1136	70	.88	42.3	1136	90	.77	37.1	1136	.11	5.1
1227	110	1.34	64.2	1227	110	1.19	57.0	1227	.15	7.1
1301	280	.93	44.7	1301	60	.28	13.4	1301	.65	31.2
1304	240	.88	42.3	1304	60	.30	14.6	1304	.58	27.7
1307	210	1.12	53.6	1307	70	.35	16.7	1307	.77	36.9
1322	290	.82	39.3	1322	160	.19	8.9	1322	.63	30.4
1325	240	1.37	65.9	1325	170	.39	18.6	1325	.99	47.3
1328	210	1.15	55.3	1328	60	.26	12.7	1328	.89	42.6
1336	240	1.12	53.6	1336	330	.30	14.3	1336	.82	39.3
1339	220	1.13	54.1	1339	170	.26	12.7	1339	.86	41.4
1409	300	.85	40.7	1409	330	.62	29.9	1409	.22	10.8
1427	290	.91	43.6	1427	330	.53	25.2	1427	.38	18.4
1454	300	.94	45.1	1454	330	.63	30.4	1454	.31	14.7
2106	100	1.15	55.4	2106	130	1.00	47.9	2106	.16	7.5
2407	230	.91	43.7	2407	170	.31	14.8	2407	.60	28.9
9107	70	.29	13.8	9107	140	.12	5.5	9107	.17	8.3

TABLE 6 --PEAK ABSOLUTE LOADS- CONFIGURATIONS A & B- HARRAH'S HOLIDAY INN -- ATLANTIC CITY
TAPS WHERE PEAK LOADS FOR CONFIGURATION B EXCEED THOSE FOR A BY 5.0 PSF OR MORE - REF. PRESS. = 48 PSF

CONFIGURATION A				CONFIGURATION B				DIFFERENCE		
TAP	AZI-MUTH	PRESS COEFF	PSF LOAD	TAP	AZI-MUTH	PRESS COEFF	PSF LOAD	TAP	PRESS COEFF	PSF LOAD
1104	150	1.33	63.8	1104	160	1.65	79.1	1104	.32	15.3
1122	120	1.43	68.4	1122	90	1.58	75.8	1122	.15	7.4
1136	150	2.68	128.5	1136	150	3.21	154.0	1136	.53	25.5
1142	330	1.66	79.5	1142	330	1.83	88.0	1142	.18	8.4
1219	140	1.24	59.3	1219	140	1.46	70.0	1219	.22	10.7
1254	240	1.73	83.1	1254	70	2.46	117.9	1254	.72	34.8
1328	160	1.53	73.3	1328	170	1.94	93.0	1328	.41	19.6
1427	80	1.26	60.6	1427	70	1.89	90.8	1427	.63	30.2
1446	80	1.03	49.4	1446	60	1.66	79.7	1446	.63	30.3
1449	70	1.23	59.0	1449	70	1.44	69.1	1449	.21	10.2
2137	100	.69	33.1	2137	110	.83	39.8	2137	.14	6.7
2606	130	.83	39.7	2606	70	1.18	56.7	2606	.35	17.0

TABLE 6 -- PEAK POSITIVE LOADS- CONFIGURATIONS A & B- HARRAH'S HOLIDAY INN -- ATLANTIC CITY
TAPS WHERE PEAK LOADS FOR CONFIGURATION B EXCEED THOSE FOR A BY 5.0 PSF OR MORE - REF. PRESS. = 48 PSF

CONFIGURATION A				CONFIGURATION B				DIFFERENCE		
TAP	AZI-MUTH	PRESS COEFF	PSF LOAD	TAP	AZI-MUTH	PRESS COEFF	PSF LOAD	TAP	PRESS COEFF	PSF LOAD
1122	90	1.34	64.2	1122	90	1.58	75.8	1122	.24	11.6
1142	40	.77	37.1	1142	30	.96	45.9	1142	.18	8.7
1219	140	1.24	59.3	1219	140	1.46	70.0	1219	.22	10.7
1449	350	.77	36.8	1449	10	.91	43.8	1449	.15	7.0
2137	100	.69	33.1	2137	110	.83	39.8	2137	.14	6.7

TABLE 6 --PEAK ABSOLUTE LOADS- CONFIGURATIONS A & C- HARRAH'S HOLIDAY INN -- ATLANTIC CITY
TAPS WHERE PEAK LOADS FOR CONFIGURATION A EXCEED THOSE FOR C BY 5.0 PSF OR MORE - REF. PRESS. = 48 PSF

CONFIGURATION A				CONFIGURATION C				DIFFERENCE		
TAP	AZI-MUTH	PRESS COEFF	PSF LOAD	TAP	AZI-MUTH	PRESS COEFF	PSF LOAD	TAP	PRESS COEFF	PSF LOAD
5106	310	1.02	49.1	5106	170	.91	43.8	5106	.11	5.3
5107	120	1.96	94.0	5107	150	1.44	69.0	5107	.52	25.0
5108	160	1.31	63.1	5108	160	1.10	52.8	5108	.21	10.3
5109	330	1.30	62.3	5109	330	1.07	51.4	5109	.23	10.9
5110	120	.93	44.5	5110	110	.78	37.5	5110	.15	7.0
5301	150	1.00	48.1	5301	350	.89	42.8	5301	.11	5.3
5304	120	1.22	58.5	5304	160	.83	39.9	5304	.39	18.6
6101	240	1.11	53.3	6101	150	1.01	48.3	6101	.10	5.0
6901	260	1.60	76.8	6901	210	1.24	59.5	6901	.36	17.2
7101	200	1.10	52.8	7101	230	.76	36.6	7101	.34	16.2
7102	210	2.35	112.6	7102	190	1.42	68.2	7102	.93	44.4
7103	10	1.03	49.3	7103	320	.78	37.4	7103	.25	11.9
7104	180	1.94	93.0	7104	200	1.11	53.1	7104	.83	39.9
7201	240	1.04	49.8	7201	260	.76	36.6	7201	.28	13.2

TABLE 6 --PEAK POSITIVE LOADS- CONFIGURATIONS A & C- HARRAH'S HOLIDAY INN -- ATLANTIC CITY
TAPS WHERE PEAK LOADS FOR CONFIGURATION A EXCEED THOSE FOR C BY 5.0 PSF OR MORE - REF. PRESS. = 48 PSF

CONFIGURATION A				CONFIGURATION C				DIFFERENCE		
TAP	AZI-MUTH	PRESS COEFF	PSF LOAD	TAP	AZI-MUTH	PRESS COEFF	PSF LOAD	TAP	PRESS COEFF	PSF LOAD
5110	0	.84	40.2	5110	10	.57	27.4	5110	.27	12.8
5114	340	.81	38.8	5114	240	.51	24.6	5114	.30	14.2
5204	210	.72	34.7	5204	140	.60	29.0	5204	.12	5.7
6101	240	1.11	53.3	6101	240	1.00	47.8	6101	.12	5.5
6302	240	.86	41.2	6302	240	.72	34.6	6302	.14	6.6
7101	240	1.04	50.1	7101	230	.76	36.6	7101	.28	13.5

TABLE 6 --PEAK ABSOLUTE LOADS- CONFIGURATIONS A & C- HARRAH'S HOLIDAY INN -- ATLANTIC CITY
TAPS WHERE PEAK LOADS FOR CONFIGURATION C EXCEED THOSE FOR A BY 5.0 PSF OR MORE - REF. PRESS. = 48 PSF

CONFIGURATION A				CONFIGURATION C				DIFFERENCE		
TAP	AZI-MUTH	PRESS COEFF	PSF LOAD	TAP	AZI-MUTH	PRESS COEFF	PSF LOAD	TAP	PRESS COEFF	PSF LOAD
5111	180	1.10	53.0	5111	160	1.26	60.6	5111	.16	7.6
5112	120	.72	34.6	5112	190	.83	40.0	5112	.11	5.4
5305	130	.85	41.0	5305	90	1.00	48.0	5305	.15	7.1
5902	190	1.18	56.5	5902	160	1.47	70.3	5902	.29	13.9
6103	90	.97	46.5	6103	270	1.26	60.4	6103	.29	13.9
6105	100	.79	37.9	6105	150	1.19	57.3	6105	.40	19.4
6106	100	.59	28.2	6106	140	1.13	54.4	6106	.55	26.2

TABLE 6 -- PEAK POSITIVE LOADS- CONFIGURATIONS A & C- HARRAH'S HOLIDAY INN -- ATLANTIC CITY
TAPS WHERE PEAK LOADS FOR CONFIGURATION C EXCEED THOSE FOR A BY 5.0 PSF OR MORE - REF. PRESS. = 48 PSF

CONFIGURATION A				CONFIGURATION C				DIFFERENCE		
TAP	AZI-MUTH	PRESS COEFF	PSF LOAD	TAP	AZI-MUTH	PRESS COEFF	PSF LOAD	TAP	PRESS COEFF	PSF LOAD
5102	30	.83	39.7	5102	70	1.02	48.9	5102	.19	9.2
5103	110	.66	31.9	5103	90	1.07	51.4	5103	.41	19.5
5105	90	.86	41.2	5105	70	1.04	50.1	5105	.18	8.8
5107	10	.48	22.9	5107	90	.68	32.6	5107	.20	9.7
5108	30	.50	24.1	5108	90	.73	34.9	5108	.22	10.7
6104	220	.62	29.9	6104	220	.90	43.4	6104	.28	13.5
6106	190	.54	25.9	6106	210	.72	34.5	6106	.18	8.6
7102	240	.54	26.1	7102	230	1.01	48.3	7102	.46	22.3
7103	70	.47	22.6	7103	210	.60	28.9	7103	.13	6.3
7106	70	.46	22.1	7106	120	.84	40.4	7106	.38	18.3

TABLE 7. BASE SHEAR AND MOMENT SUMMARY : HARRAH'S HOLIDAY INN, ATLANTIC CITY
CONFIGURATION A REFERENCE PRESSURE 48.0 GUST FACTOR 1.32

AZIMUTH DEGREES	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
0	-1877.5	695.3	-117.7	-312.9	61.6
10	-1716.2	910.8	-176.6	-282.9	61.1
20	-1453.6	994.0	-204.9	-243.0	56.2
30	-1132.3	953.4	-215.9	-187.9	50.8
40	-761.3	796.0	-202.3	-120.0	41.0
50	-346.3	453.8	-138.6	-71.4	16.0
60	55.8	301.1	-95.3	-7.7	-7.3
70	645.6	824.7	-210.0	117.4	-27.2
80	1275.8	1432.5	-358.9	245.8	-64.8
90	2159.3	1725.2	-387.1	379.0	-90.7
100	2300.4	1672.3	-350.2	424.5	-106.9
110	2467.2	1348.1	-272.7	486.1	-97.9
120	2914.6	673.1	-133.2	532.3	-92.1
130	3284.3	-119.5	22.8	566.3	-89.4
140	3437.9	-632.3	103.5	610.2	-77.3
150	3455.6	-690.2	80.6	638.0	-49.4
160	3657.4	-622.5	30.4	656.3	-46.1
170	3784.3	-1033.1	98.7	642.9	-51.4
180	3750.4	-1746.8	246.8	624.6	-43.9
190	3494.9	-2277.1	366.9	573.6	-25.3
200	2797.8	-2578.9	437.1	466.2	1.0
210	2372.9	-3112.0	523.1	377.6	22.9
220	1446.9	-2522.2	453.7	225.1	15.2
230	516.2	-2851.2	485.3	59.3	16.3
240	201.3	-2982.4	506.1	38.1	59.9
250	-65.3	-1848.9	312.4	1.5	37.4
260	-511.9	-1910.6	311.2	-88.0	50.4
270	-1133.3	-2033.9	333.5	-191.7	80.8
280	-1546.7	-1892.5	325.8	-264.4	89.4
290	-1814.0	-1585.7	280.3	-326.5	98.6
300	-1911.4	-998.4	179.5	-348.8	99.9
310	-1970.2	-483.2	74.3	-357.1	101.9
320	-2028.9	-169.9	21.9	-362.2	111.7
330	-2018.1	-80.2	13.3	-370.7	98.8
340	-2063.5	52.1	1.2	-371.1	87.2
350	-1933.1	317.6	-42.3	-343.8	65.4

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 0 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	-43.3	10.5	2676	7795	-16.2	1.3	-1877.5	695.3	-117.7	-312.9	61.6
PARK	14.00	-42.9	11.5	1911	5568	-22.4	2.1	-1834.2	684.8	-108.0	-287.0	65.3
2	24.00	-138.5	48.1	6078	12768	-22.8	3.8	-1791.3	673.4	-101.3	-268.8	67.3
3	43.00	-136.1	43.1	6398	12568	-21.3	3.4	-1652.8	625.3	-88.9	-236.1	54.0
4	63.00	-74.6	25.9	3199	5718	-23.3	4.5	-1516.7	582.2	-76.8	-204.4	41.8
4A	73.00	-78.7	26.6	3199	5169	-24.6	5.1	-1442.2	556.3	-71.1	-189.6	37.2
5	83.00	-84.1	32.7	3199	4443	-26.3	7.4	-1363.5	529.7	-65.7	-175.6	33.0
6	93.00	-71.7	51.9	2754	4176	-26.0	12.4	-1279.4	497.0	-60.6	-162.4	26.6
7	103.00	-90.6	27.5	4715	2962	-19.2	9.3	-1207.7	445.1	-55.9	-149.9	17.8
8	113.00	-83.1	30.7	4581	2670	-18.1	11.5	-1117.1	417.6	-51.6	-138.3	11.2
9	123.00	-76.9	26.8	4403	2513	-17.5	10.7	-1034.0	386.9	-47.5	-127.6	5.8
10	133.00	-73.5	25.8	4225	2379	-17.4	10.8	-957.1	360.0	-43.8	-117.6	.6
11	143.00	-38.0	16.6	1443	1621	-26.3	10.2	-883.6	334.2	-40.3	-108.4	-4.1
12	153.00	-34.2	16.3	1285	1489	-26.6	11.0	-845.6	317.6	-37.1	-99.8	-4.3
13	163.00	-32.0	13.4	1100	1448	-29.1	9.3	-811.4	301.3	-34.0	-91.5	-4.2
14	173.00	-32.5	13.3	1100	1448	-29.6	9.2	-779.4	287.9	-31.0	-83.5	-4.1
15	183.00	-33.4	13.4	1100	1448	-30.4	9.2	-746.9	274.6	-28.2	-75.9	-4.0
16	193.00	-34.3	13.4	1100	1448	-31.2	9.3	-713.5	261.2	-25.5	-68.6	-3.9
17	203.00	-35.2	13.5	1100	1448	-32.0	9.3	-679.2	247.8	-23.0	-61.6	-3.7
18	213.00	-35.8	13.4	1100	1448	-32.6	9.3	-644.1	234.3	-20.6	-55.0	-3.5
19	223.00	-36.1	13.0	1100	1448	-32.8	9.0	-608.2	220.9	-18.3	-48.7	-3.3
20	233.00	-36.4	12.7	1100	1448	-33.1	8.8	-572.1	207.9	-16.2	-42.8	-3.1
21	243.00	-36.7	12.3	1100	1448	-33.4	8.5	-535.7	195.2	-14.2	-37.3	-2.9
22	253.00	-37.0	12.0	1100	1448	-33.7	8.3	-498.9	182.9	-12.3	-32.1	-2.6
23	263.00	-37.6	12.3	1100	1448	-34.2	8.5	-461.9	170.9	-10.5	-27.3	-2.4
24	273.00	-38.2	13.0	1100	1448	-34.8	9.0	-424.3	158.6	-8.8	-22.9	-2.2
25	283.00	-38.9	13.6	1100	1448	-35.4	9.4	-386.1	145.6	-7.3	-18.8	-2.0
26	293.00	-39.6	14.3	1100	1448	-36.0	9.9	-347.2	132.0	-5.9	-15.2	-1.7
27	303.00	-40.2	14.9	1100	1448	-36.5	10.3	-307.6	117.7	-4.7	-11.9	-1.5
28	313.00	-40.5	14.9	1100	1448	-36.8	10.3	-267.4	102.8	-3.6	-9.0	-1.2
29	323.00	-40.7	15.0	1100	1448	-37.0	10.4	-226.9	87.9	-2.6	-6.6	-1.0
30	333.00	-41.0	15.0	1100	1448	-37.2	10.4	-186.2	72.9	-1.8	-4.5	-.8
31	343.00	-61.9	22.7	1650	2171	-37.5	10.4	-145.2	57.8	-1.2	-2.8	-.6
MECH	358.00	-83.3	35.2	2970	3908	-28.0	9.0	-83.3	35.2	-.5	-1.1	-.4

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 10 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT 1000-FT-KIPS	Y-MOMENT 1000-FT-KIPS	Z-MOMENT 1000-FT-KIPS
PARK	0.00	-44.8	4.2	2676	7795	-16.8	.5	-1716.2	910.8	-176.6	-282.9	61.1
PARK	14.00	-38.6	7.7	1911	5568	-20.2	1.4	-1671.4	906.7	-163.9	-259.2	63.1
2	24.00	-114.4	37.9	6078	12768	-18.8	3.0	-1632.8	899.0	-154.9	-242.7	64.7
3	43.00	-123.4	38.7	6398	12568	-19.3	3.1	-1518.3	861.1	-138.2	-212.7	54.4
4	63.00	-69.7	26.3	3199	5718	-21.8	4.6	-1394.9	822.4	-121.3	-183.6	43.2
4A	73.00	-74.8	28.5	3199	5169	-23.4	5.5	-1325.2	796.1	-113.2	-170.0	38.7
5	83.00	-79.7	38.8	3199	4443	-24.9	8.7	-1250.4	767.6	-105.4	-157.1	34.5
6	93.00	-67.7	59.7	2754	4176	-24.6	14.3	-1170.7	728.8	-97.9	-145.0	28.6
7	103.00	-85.7	35.5	4715	2962	-18.2	12.0	-1103.0	669.1	-91.0	-133.6	20.6
8	113.00	-79.4	37.4	4581	2670	-17.3	14.0	-1017.3	633.6	-84.4	-123.0	14.9
9	123.00	-74.4	32.3	4403	2513	-16.9	12.9	-937.9	596.2	-78.3	-113.3	10.0
10	133.00	-71.2	30.3	4225	2379	-16.8	12.8	-863.4	563.8	-72.5	-104.3	5.1
11	143.00	-35.8	19.5	1443	1621	-24.8	12.0	-792.3	533.5	-67.0	-96.0	.5
12	153.00	-32.3	19.1	1285	1489	-25.1	12.8	-756.4	514.0	-61.8	-88.2	.5
13	163.00	-30.7	16.6	11000	1448	-27.9	11.5	-724.1	494.9	-56.7	-80.8	.6
14	173.00	-30.8	17.7	11000	1448	-28.0	12.2	-693.5	478.3	-51.9	-73.7	.6
15	183.00	-31.0	19.1	11000	1448	-28.2	13.2	-662.7	460.6	-47.2	-67.0	.6
16	193.00	-31.3	20.5	11000	1448	-28.5	14.2	-631.7	441.5	-42.7	-60.5	.5
17	203.00	-31.6	22.0	11000	1448	-28.7	15.2	-600.4	421.0	-38.3	-54.3	.6
18	213.00	-31.9	22.8	11000	1448	-29.0	15.8	-568.8	399.0	-34.2	-48.5	.6
19	223.00	-32.2	22.9	11000	1448	-29.3	15.8	-536.9	376.2	-30.4	-43.0	.6
20	233.00	-32.5	22.9	11000	1448	-29.6	15.8	-504.7	353.3	-26.7	-37.8	.6
21	243.00	-32.9	22.9	11000	1448	-29.9	15.8	-472.2	330.4	-23.3	-32.9	.6
22	253.00	-33.2	23.0	11000	1448	-30.2	15.9	-439.3	307.5	-20.1	-28.3	.5
23	263.00	-33.5	23.1	11000	1448	-30.5	16.0	-406.1	284.5	-17.1	-24.1	.5
24	273.00	-33.8	23.3	11000	1448	-30.7	16.1	-372.6	261.4	-14.4	-20.2	.4
25	283.00	-34.1	23.4	11000	1448	-31.0	16.2	-338.8	238.2	-11.9	-16.6	.4
26	293.00	-34.5	23.6	11000	1448	-31.3	16.3	-304.7	214.8	-9.7	-13.4	.3
27	303.00	-34.8	23.8	11000	1448	-31.6	16.4	-270.2	191.2	-7.6	-10.5	.3
28	313.00	-35.1	24.1	11000	1448	-31.9	16.6	-235.4	167.4	-5.8	-8.0	.3
29	323.00	-35.4	24.4	11000	1448	-32.2	16.8	-200.3	143.3	-4.3	-5.8	.3
30	333.00	-35.8	24.6	11000	1448	-32.5	17.0	-164.9	119.0	-3.0	-4.0	.3
31	343.00	-54.3	37.5	1650	2171	-32.9	17.3	-129.1	94.4	-1.9	-2.5	.2
MECH	358.00	-74.9	56.8	2970	3908	-25.2	14.5	-74.9	56.8	-.8	-1.0	.1

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 20 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT 1000-FT-KIPS	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	-37.3	-7.2	2676	7795	-13.9	-.9	-1453.6	994.0	-204.9	-243.0	56.2
PARK	14.00	-28.8	-.4	1911	5568	-15.1	-.1	-1416.3	1001.1	-191.0	-222.9	56.2
2	24.00	-80.0	34.3	6078	12768	-13.2	2.7	-1387.5	1001.5	-180.9	-208.9	56.7
3	43.00	-96.1	36.7	6398	12568	-15.0	2.9	-1307.5	967.2	-162.2	-183.3	51.5
4	63.00	-55.3	26.5	3199	5718	-17.3	4.6	-1211.5	930.5	-143.3	-158.1	42.7
4A	73.00	-60.8	29.6	3199	5169	-19.0	5.7	-1156.1	904.0	-134.1	-146.2	38.7
5	83.00	-68.0	43.1	3199	4443	-21.3	9.7	-1095.3	874.5	-125.2	-135.0	34.6
6	93.00	-59.0	66.3	2754	4176	-21.4	15.9	-1027.3	831.3	-116.7	-124.4	28.7
7	103.00	-77.3	39.0	4715	2962	-16.4	13.2	-968.3	765.1	-108.7	-114.4	20.9
8	113.00	-70.8	39.5	4581	2670	-15.4	14.8	-891.0	726.1	-101.2	-105.1	15.7
9	123.00	-66.1	33.0	4403	2513	-15.0	13.1	-820.2	686.6	-94.2	-96.5	11.3
10	133.00	-62.1	29.8	4225	2379	-14.7	12.5	-754.2	653.6	-87.5	-88.7	6.9
11	143.00	-33.5	18.5	1443	1621	-23.2	11.4	-692.1	623.8	-81.1	-81.4	2.7
12	153.00	-30.3	18.0	1285	1489	-23.6	12.1	-658.6	605.3	-74.9	-74.7	2.8
13	163.00	-29.0	17.4	1100	1448	-26.3	12.0	-628.3	587.3	-69.0	-68.2	2.9
14	173.00	-29.0	19.0	1100	1448	-26.4	13.1	-599.4	569.9	-63.2	-62.1	2.8
15	183.00	-29.1	20.7	1100	1448	-26.4	14.3	-570.4	550.9	-57.6	-56.2	2.8
16	193.00	-29.2	22.5	1100	1448	-26.5	15.5	-541.3	530.1	-52.2	-50.7	2.7
17	203.00	-29.3	24.2	1100	1448	-26.6	16.7	-512.1	507.7	-47.0	-45.4	2.6
18	213.00	-29.3	25.4	1100	1448	-26.6	17.5	-482.8	483.5	-42.0	-40.4	2.5
19	223.00	-29.1	25.8	1100	1448	-26.5	17.9	-453.5	458.1	-37.3	-35.8	2.5
20	233.00	-29.0	26.3	1100	1448	-26.3	18.2	-424.4	432.3	-32.9	-31.4	2.3
21	243.00	-28.8	26.8	1100	1448	-26.2	18.5	-395.4	406.0	-28.7	-27.3	2.2
22	253.00	-28.7	27.2	1100	1448	-26.1	18.8	-366.6	379.2	-24.7	-23.5	2.0
23	263.00	-28.6	27.9	1100	1448	-26.0	19.2	-337.9	352.0	-21.1	-19.9	1.9
24	273.00	-28.7	28.6	1100	1448	-26.1	19.7	-309.3	324.1	-17.7	-16.7	1.7
25	283.00	-28.7	29.3	1100	1448	-26.1	20.2	-280.6	295.6	-14.6	-13.8	1.5
26	293.00	-28.8	30.0	1100	1448	-26.2	20.7	-251.8	266.3	-11.8	-11.1	1.4
27	303.00	-28.8	30.6	1100	1448	-26.2	21.1	-223.1	236.3	-9.3	-8.7	1.2
28	313.00	-29.0	30.6	1100	1448	-26.3	21.1	-194.2	205.7	-7.1	-6.6	1.0
29	323.00	-29.1	30.6	1100	1448	-26.5	21.1	-165.3	175.1	-5.2	-4.8	.9
30	333.00	-29.3	30.6	1100	1448	-26.6	21.1	-136.2	144.5	-3.6	-3.3	.7
31	343.00	-44.2	45.8	1650	2171	-26.8	21.1	-106.9	114.0	-2.3	-2.1	.6
MECH	358.00	-62.7	68.2	2970	3908	-21.1	17.4	-62.7	68.2	-.9	-.8	.3

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 30 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT 1000-FT-KIPS	Y-MOMENT 1000-FT-KIPS	Z-MOMENT 1000-FT-KIPS
PARK	0.00	-28.6	-21.9	2676	7795	-10.7	-2.8	-1132.3	953.4	-215.9	-187.9	50.8
PARK	14.00	-19.5	-13.8	1911	5568	-10.2	-2.5	-1103.7	975.2	-202.4	-172.2	49.2
2	24.00	-46.5	10.4	6078	12768	-7.6	.8	-1084.2	989.1	-192.6	-161.3	48.3
3	43.00	-65.8	18.7	6398	12568	-10.3	1.5	-1037.8	978.6	-173.9	-141.1	45.1
4	63.00	-38.3	15.8	3199	5718	-12.0	2.8	-971.9	959.9	-154.5	-121.0	38.5
4A	73.00	-43.1	22.5	3199	5169	-13.5	4.4	-933.6	944.1	-145.0	-111.5	35.0
5	83.00	-53.0	42.8	3199	4443	-16.6	9.6	-890.4	921.6	-135.7	-102.4	31.5
6	93.00	-49.3	65.7	2754	4176	-17.9	15.7	-837.4	878.8	-126.7	-93.7	26.7
7	103.00	-74.9	40.7	4715	2962	-15.9	13.8	-788.1	813.1	-118.2	-85.6	20.4
8	113.00	-68.4	39.2	4581	2670	-14.9	14.7	-713.2	772.4	-110.3	-78.1	15.8
9	123.00	-63.6	32.9	4403	2513	-14.4	13.1	-644.8	733.2	-102.8	-71.3	11.8
10	133.00	-59.4	29.4	4225	2379	-14.1	12.4	-581.2	700.3	-95.6	-65.2	7.9
11	143.00	-28.8	19.8	1443	1621	-20.0	12.2	-521.8	670.9	-88.7	-59.7	4.1
12	153.00	-25.4	20.3	1285	1489	-19.7	13.6	-493.0	651.1	-82.1	-54.6	4.2
13	163.00	-24.2	17.9	1100	1448	-22.0	12.4	-467.6	630.8	-75.7	-49.8	4.3
14	173.00	-23.6	19.1	1100	1448	-21.5	13.2	-443.4	612.9	-69.5	-45.2	4.1
15	183.00	-23.1	20.8	1100	1448	-21.0	14.4	-419.8	593.7	-63.5	-40.9	4.0
16	193.00	-22.5	22.5	1100	1448	-20.4	15.5	-396.8	572.9	-57.6	-36.8	3.8
17	203.00	-21.9	24.1	1100	1448	-19.9	16.7	-374.3	550.5	-52.0	-33.0	3.7
18	213.00	-21.6	25.5	1100	1448	-19.6	17.6	-352.3	526.3	-46.6	-29.3	3.6
19	223.00	-21.5	26.2	1100	1448	-19.6	18.1	-330.8	500.9	-41.5	-25.9	3.4
20	233.00	-21.5	27.0	1100	1448	-19.5	18.7	-309.2	474.6	-36.6	-22.7	3.3
21	243.00	-21.5	27.8	1100	1448	-19.5	19.2	-287.7	447.6	-32.0	-19.7	3.1
22	253.00	-21.4	28.6	1100	1448	-19.5	19.8	-266.3	419.8	-27.7	-17.0	2.9
23	263.00	-21.3	29.7	1100	1448	-19.3	20.5	-244.8	391.1	-23.6	-14.4	2.6
24	273.00	-21.1	31.0	1100	1448	-19.2	21.4	-223.6	361.4	-19.9	-12.1	2.4
25	283.00	-20.9	32.2	1100	1448	-19.0	22.2	-202.5	330.5	-16.4	-9.9	2.2
26	293.00	-20.7	33.4	1100	1448	-18.8	23.1	-181.6	298.3	-13.3	-8.0	2.0
27	303.00	-20.6	34.5	1100	1448	-18.7	23.9	-160.8	264.9	-10.4	-6.3	1.7
28	313.00	-20.8	34.3	1100	1448	-18.9	23.7	-140.3	230.3	-8.0	-4.8	1.6
29	323.00	-20.9	34.1	1100	1448	-19.0	23.6	-119.5	196.0	-5.8	-3.5	1.3
30	333.00	-21.1	33.9	1100	1448	-19.2	23.4	-98.6	161.9	-4.0	-2.4	1.1
31	343.00	-32.0	50.5	1650	2171	-19.4	23.2	-77.4	128.0	-2.6	-1.5	.9
MECH	358.00	-45.4	77.6	2970	3908	-15.3	19.8	-45.4	77.6	-1.0	-.6	.5

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 40 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT 1000-FT-KIPS	Y-MOMENT 1000-FT-KIPS	Z-MOMENT 1000-FT-KIPS
PARK	0.00	-17.3	-32.9	2676	7795	-6.5	-4.2	-761.3	796.0	-202.3	-120.0	41.0
PARK	14.00	-15.1	-22.6	1911	5568	-7.9	-4.1	-744.0	828.9	-191.0	-109.4	36.1
2	24.00	-44.6	-2.7	6078	12768	-7.3	-.2	-728.9	851.5	-182.6	-102.1	32.5
3	43.00	-48.0	-3.3	6398	12568	-7.5	-.3	-684.3	854.1	-166.4	-88.6	29.5
4	63.00	-26.1	6.4	3199	5718	-8.2	1.1	-636.3	857.4	-149.2	-75.4	24.2
4A	73.00	-28.3	11.6	3199	5169	-8.9	2.2	-610.2	851.0	-140.7	-69.2	22.3
5	83.00	-35.2	32.3	3199	4443	-11.0	7.3	-581.8	839.4	-132.2	-63.2	20.2
6	93.00	-35.0	48.2	2754	4176	-12.7	11.5	-546.7	807.1	-124.0	-57.6	17.6
7	103.00	-50.6	33.4	4715	2962	-10.7	11.3	-511.7	758.9	-116.2	-52.3	14.1
8	113.00	-47.9	30.9	4581	2670	-10.4	11.6	-461.1	725.5	-108.8	-47.4	11.6
9	123.00	-46.4	24.3	4403	2513	-10.5	9.7	-413.3	694.6	-101.7	-43.1	9.5
10	133.00	-44.6	20.3	4225	2379	-10.6	8.5	-366.9	670.3	-94.8	-39.2	7.1
11	143.00	-20.9	15.0	1443	1621	-14.5	9.3	-322.2	650.1	-88.2	-35.7	4.6
12	153.00	-17.9	16.1	1285	1489	-13.9	10.8	-301.3	635.1	-81.8	-32.6	4.8
13	163.00	-16.7	16.1	1100	1448	-15.2	11.1	-283.4	619.0	-75.5	-29.7	4.8
14	173.00	-16.0	17.7	1100	1448	-14.5	12.2	-266.7	602.9	-69.4	-26.9	4.7
15	183.00	-15.3	19.2	1100	1448	-13.9	13.3	-250.7	585.2	-63.5	-24.3	4.6
16	193.00	-14.6	20.8	1100	1448	-13.2	14.4	-235.4	565.9	-57.7	-21.9	4.4
17	203.00	-13.8	22.4	1100	1448	-12.6	15.4	-220.9	545.1	-52.2	-19.6	4.3
18	213.00	-13.3	23.8	1100	1448	-12.1	16.4	-207.0	522.8	-46.8	-17.5	4.1
19	223.00	-13.0	25.0	1100	1448	-11.8	17.3	-193.8	499.0	-41.7	-15.5	3.9
20	233.00	-12.6	26.2	1100	1448	-11.5	18.1	-180.8	474.0	-36.9	-13.6	3.7
21	243.00	-12.3	27.4	1100	1448	-11.2	18.9	-168.2	447.8	-32.2	-11.9	3.5
22	253.00	-12.0	28.6	1100	1448	-10.9	19.8	-155.8	420.5	-27.9	-10.2	3.2
23	263.00	-11.8	29.7	1100	1448	-10.7	20.5	-143.8	391.9	-23.8	-8.7	2.9
24	273.00	-11.7	30.7	1100	1448	-10.6	21.2	-132.0	362.2	-20.1	-7.4	2.6
25	283.00	-11.6	31.7	1100	1448	-10.5	21.9	-120.3	331.5	-16.6	-6.1	2.3
26	293.00	-11.5	32.7	1100	1448	-10.4	22.6	-108.7	299.8	-13.4	-5.0	2.1
27	303.00	-11.4	33.6	1100	1448	-10.4	23.2	-97.3	267.1	-10.6	-3.9	1.8
28	313.00	-11.8	33.9	1100	1448	-10.8	23.4	-85.9	233.5	-8.1	-3.0	1.6
29	323.00	-12.3	34.2	1100	1448	-11.2	23.6	-74.0	199.6	-5.9	-2.2	1.3
30	333.00	-12.7	34.4	1100	1448	-11.5	23.8	-61.8	165.4	-4.1	-1.5	1.1
31	343.00	-19.9	52.1	1650	2171	-12.0	24.0	-49.1	131.0	-2.6	-1.0	.9
MECH	358.00	-29.2	78.9	2970	3908	-9.8	20.2	-29.2	78.9	-1.1	-.4	.5

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 50 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT 1000-FT-KIPS	Y-MOMENT 1000-FT-KIPS	Z-MOMENT 1000-FT-KIPS
PARK	0.00	-4.7	-32.5	2676	7795	-1.8	-4.2	-346.3	453.8	-138.6	-71.4	16.0
PARK	14.00	-.9	-24.3	1911	5568	-.5	-4.4	-341.6	486.4	-132.0	-66.6	10.0
2	24.00	2.7	-14.0	6078	12768	.4	-1.1	-340.7	510.7	-127.0	-63.1	5.9
3	43.00	-8.1	-13.8	6398	12568	-1.3	-1.1	-343.4	524.7	-117.2	-56.6	7.7
4	63.00	-5.8	-.9	3199	5718	-1.8	-.2	-335.3	538.6	-106.5	-49.9	8.0
4A	73.00	-7.9	-3.2	3199	5169	-2.5	-.6	-329.4	539.4	-101.1	-46.5	8.6
5	83.00	-10.7	10.5	3199	4443	-3.3	2.4	-321.5	542.7	-95.7	-43.3	7.8
6	93.00	-10.9	20.0	2754	4176	-4.0	4.8	-310.8	532.2	-90.4	-40.1	6.8
7	103.00	-14.2	15.0	4715	2962	-3.0	5.0	-299.9	512.2	-85.1	-37.1	5.8
8	113.00	-14.6	14.7	4581	2670	-3.2	5.5	-285.7	497.2	-80.1	-34.1	5.4
9	123.00	-15.1	11.0	4403	2513	-3.4	4.4	-271.1	482.5	-75.2	-31.3	5.1
10	133.00	-16.9	9.8	4225	2379	-4.0	4.1	-256.0	471.5	-70.4	-28.7	4.6
11	143.00	-13.2	9.6	1443	1621	-9.2	5.9	-239.1	461.6	-65.8	-26.2	3.9
12	153.00	-12.2	9.1	1285	1489	-9.5	6.1	-225.9	452.0	-61.2	-23.9	4.1
13	163.00	-12.1	8.3	1100	1448	-11.0	5.7	-213.7	442.9	-56.7	-21.7	4.2
14	173.00	-12.0	9.6	1100	1448	-10.9	6.6	-201.6	434.7	-52.3	-19.6	4.1
15	183.00	-11.9	11.3	1100	1448	-10.8	7.8	-189.6	425.1	-48.0	-17.7	4.0
16	193.00	-11.7	13.0	1100	1448	-10.7	9.0	-177.7	413.8	-43.8	-15.8	3.9
17	203.00	-11.6	14.6	1100	1448	-10.6	10.1	-165.9	400.8	-39.8	-14.1	3.8
18	213.00	-11.4	16.0	1100	1448	-10.3	11.0	-154.3	386.2	-35.8	-12.5	3.7
19	223.00	-11.0	16.8	1100	1448	-10.0	11.6	-142.9	370.2	-32.0	-11.0	3.5
20	233.00	-10.5	17.5	1100	1448	-9.6	12.1	-132.0	353.5	-28.4	-9.7	3.3
21	243.00	-10.1	18.3	1100	1448	-9.2	12.7	-121.4	335.9	-25.0	-8.4	3.1
22	253.00	-9.7	19.1	1100	1448	-8.8	13.2	-111.3	317.6	-21.7	-7.2	2.9
23	263.00	-9.3	20.3	1100	1448	-8.4	14.0	-101.6	298.5	-18.6	-6.2	2.7
24	273.00	-8.8	21.7	1100	1448	-8.0	15.0	-92.3	278.2	-15.7	-5.2	2.4
25	283.00	-8.3	23.1	1100	1448	-7.5	16.0	-83.6	256.5	-13.1	-4.3	2.2
26	293.00	-7.8	24.5	1100	1448	-7.1	16.9	-75.3	233.4	-10.6	-3.5	1.9
27	303.00	-7.4	25.8	1100	1448	-6.7	17.8	-67.5	208.9	-8.4	-2.8	1.7
28	313.00	-7.8	26.0	1100	1448	-7.1	18.0	-60.1	183.1	-6.5	-2.2	1.5
29	323.00	-8.2	26.2	1100	1448	-7.4	18.1	-52.3	157.1	-4.8	-1.6	1.3
30	333.00	-8.5	26.5	1100	1448	-7.8	18.3	-44.2	130.9	-3.3	-1.1	1.0
31	343.00	-13.5	40.1	1650	2171	-8.2	18.5	-35.7	104.5	-2.1	-.7	.8
MECH	358.00	-22.1	64.3	2970	3908	-7.4	16.5	-22.1	64.3	-.9	-.3	.4

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 60 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	-.9	-30.6	2676	7795	-.3	-3.9	55.8	301.1	-95.3	-7.7	-7.3
PARK	14.00	-1.7	-22.3	1911	5568	-.9	-4.0	56.7	331.7	-90.9	-8.5	-13.5
2	24.00	9.5	-18.0	6078	12768	1.6	-1.4	58.4	354.0	-87.5	-9.1	-17.8
3	43.00	13.0	-9.1	6398	12568	2.0	-.7	48.9	372.0	-80.6	-10.1	-15.9
4	63.00	7.4	1.7	3199	5718	2.3	.3	35.9	381.1	-73.1	-10.9	-11.4
4A	73.00	7.8	-4.9	3199	5169	2.4	-.9	28.5	379.4	-69.2	-11.2	-8.7
5	83.00	7.6	5.2	3199	4443	2.4	1.2	20.7	384.3	-65.4	-11.5	-8.0
6	93.00	7.0	13.6	2754	4176	2.5	3.3	13.1	379.2	-61.6	-11.7	-7.6
7	103.00	10.6	11.7	4715	2962	2.2	3.9	6.1	365.5	-57.9	-11.8	-6.9
8	113.00	12.0	11.8	4581	2670	2.6	4.4	-4.5	353.8	-54.3	-11.8	-6.0
9	123.00	14.0	10.8	4403	2513	3.2	4.3	-16.4	342.0	-50.8	-11.7	-5.1
10	133.00	15.8	12.3	4225	2379	3.7	5.2	-30.4	331.2	-47.4	-11.4	-4.4
11	143.00	9.2	12.7	1443	1621	6.4	7.8	-46.2	318.9	-44.2	-11.0	-3.9
12	153.00	7.4	11.0	1285	1489	5.8	7.4	-55.4	306.2	-41.1	-10.5	-3.5
13	163.00	4.0	7.0	1100	1448	3.7	4.8	-62.8	295.2	-38.1	-9.9	-3.2
14	173.00	2.7	6.8	1100	1448	2.4	4.7	-66.9	288.2	-35.1	-9.3	-3.1
15	183.00	1.4	7.6	1100	1448	1.3	5.2	-69.6	281.4	-32.3	-8.6	-3.0
16	193.00	.1	8.3	1100	1448	.1	5.7	-70.9	273.9	-29.5	-7.9	-2.8
17	203.00	-1.2	9.1	1100	1448	-1.1	6.3	-71.0	265.6	-26.8	-7.2	-2.7
18	213.00	-2.2	9.8	1100	1448	-2.0	6.8	-69.8	256.5	-24.2	-6.5	-2.4
19	223.00	-2.6	10.4	1100	1448	-2.4	7.2	-67.7	246.7	-21.7	-5.8	-2.2
20	233.00	-3.1	11.1	1100	1448	-2.8	7.7	-65.0	236.2	-19.3	-5.1	-2.0
21	243.00	-3.6	11.8	1100	1448	-3.2	8.1	-61.9	225.1	-17.0	-4.5	-1.9
22	253.00	-4.0	12.4	1100	1448	-3.7	8.6	-58.4	213.4	-14.8	-3.9	-1.7
23	263.00	-4.2	13.3	1100	1448	-3.8	9.2	-54.3	200.9	-12.7	-3.3	-1.6
24	273.00	-4.2	14.2	1100	1448	-3.8	9.8	-50.1	187.7	-10.8	-2.8	-1.5
25	283.00	-4.2	15.2	1100	1448	-3.9	10.5	-45.9	173.4	-9.0	-2.3	-1.4
26	293.00	-4.3	16.1	1100	1448	-3.9	11.1	-41.7	158.3	-7.3	-1.9	-1.3
27	303.00	-4.3	17.0	1100	1448	-3.9	11.7	-37.4	142.2	-5.8	-1.5	-1.2
28	313.00	-4.5	17.3	1100	1448	-4.1	11.9	-33.1	125.2	-4.5	-1.2	-1.0
29	323.00	-4.7	17.6	1100	1448	-4.3	12.1	-28.6	108.0	-3.3	-.8	-.9
30	333.00	-4.9	17.9	1100	1448	-4.5	12.3	-23.8	90.4	-2.3	-.6	-.7
31	343.00	-7.8	27.4	1650	2171	-4.7	12.6	-18.9	72.6	-1.5	-.4	-.6
MECH	358.00	-11.1	45.2	2970	3908	-3.7	11.6	-11.1	45.2	-.6	-.1	-.4

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 70 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	-11.4	-40.3	2676	7795	-4.3	-5.2	645.6	824.7	-210.0	117.4	-27.2
PARK	14.00	-18.3	-29.7	1911	5568	-9.6	-5.3	657.0	865.0	-198.2	108.3	-36.4
2	24.00	-5.1	-21.0	6078	12768	-.8	-1.6	675.3	894.7	-189.4	101.7	-44.4
3	43.00	27.8	26.4	6398	12568	4.3	2.1	680.4	915.7	-172.2	88.8	-46.6
4	63.00	19.0	20.2	3199	5718	5.9	3.5	652.6	889.3	-154.1	75.4	-33.5
4A	73.00	22.5	-1.0	3199	5169	7.0	-.2	633.6	869.1	-145.3	69.0	-26.7
5	83.00	23.5	20.2	3199	4443	7.4	4.6	611.1	870.1	-136.6	62.8	-25.2
6	93.00	21.6	40.2	2754	4176	7.8	9.6	587.6	849.8	-128.0	56.8	-24.7
7	103.00	43.9	33.0	4715	2962	9.3	11.1	566.0	809.7	-119.7	51.0	-23.2
8	113.00	45.5	31.5	4581	2670	9.9	11.8	522.1	776.7	-111.8	45.6	-21.2
9	123.00	47.9	23.2	4403	2513	10.9	9.2	476.6	745.1	-104.2	40.6	-19.1
10	133.00	55.0	22.5	4225	2379	13.0	9.5	428.7	721.9	-96.9	36.1	-17.8
11	143.00	40.3	22.4	1443	1621	27.9	13.8	373.7	699.5	-89.7	32.1	-16.3
12	153.00	36.0	23.4	1285	1489	28.0	15.7	333.4	677.0	-82.9	28.5	-15.1
13	163.00	27.2	22.1	1100	1448	24.7	15.2	297.4	653.6	-76.2	25.4	-14.3
14	173.00	25.1	23.3	1100	1448	22.9	16.1	270.2	631.5	-69.8	22.5	-14.0
15	183.00	22.9	24.5	1100	1448	20.8	17.0	245.0	608.3	-63.6	20.0	-13.7
16	193.00	20.7	25.8	1100	1448	18.8	17.8	222.1	583.7	-57.6	17.6	-13.2
17	203.00	18.4	27.1	1100	1448	16.7	18.7	201.5	557.9	-51.9	15.5	-12.7
18	213.00	16.6	28.0	1100	1448	15.0	19.3	183.0	530.8	-46.5	13.6	-12.0
19	223.00	15.2	28.5	1100	1448	13.8	19.7	166.5	502.8	-41.3	11.8	-11.3
20	233.00	13.9	28.9	1100	1448	12.6	20.0	151.3	474.4	-36.4	10.2	-10.6
21	243.00	12.6	29.3	1100	1448	11.4	20.3	137.4	445.5	-31.8	8.8	-9.8
22	253.00	11.3	29.8	1100	1448	10.2	20.6	124.8	416.1	-27.5	7.5	-9.1
23	263.00	10.9	30.3	1100	1448	9.9	20.9	113.5	386.4	-23.5	6.3	-8.4
24	273.00	10.9	30.8	1100	1448	9.9	21.3	102.6	356.1	-19.8	5.2	-7.7
25	283.00	10.9	31.3	1100	1448	9.9	21.6	91.7	325.3	-16.4	4.2	-7.0
26	293.00	10.9	31.9	1100	1448	9.9	22.0	80.8	293.9	-13.3	3.4	-6.3
27	303.00	10.9	32.4	1100	1448	9.9	22.4	69.9	262.1	-10.5	2.6	-5.5
28	313.00	10.1	32.8	1100	1448	9.2	22.6	59.0	229.7	-8.0	2.0	-4.8
29	323.00	9.3	33.2	1100	1448	8.5	22.9	48.9	197.0	-5.9	1.4	-4.1
30	333.00	8.5	33.6	1100	1448	7.8	23.2	39.6	163.8	-4.1	1.0	-3.4
31	343.00	11.4	51.1	1650	2171	6.9	23.5	31.0	130.3	-2.6	.6	-2.7
MECH	358.00	19.7	79.2	2970	3908	6.6	20.3	19.7	79.2	-1.1	.3	-1.7

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 80 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT 1000-FT-KIPS	Y-MOMENT 1000-FT-KIPS	Z-MOMENT 1000-FT-KIPS
PARK	0.00	-11.9	-39.9	2676	7795	-4.4	-5.1	1275.8	1432.5	-358.9	245.8	-64.8
PARK	14.00	-16.7	-33.8	1911	5568	-8.7	-6.1	1287.7	1472.3	-338.6	227.9	-72.6
2	24.00	6.9	-4.1	6078	12768	1.1	-.3	1304.5	1506.1	-323.7	214.9	-81.3
3	43.00	39.8	124.4	6398	12568	6.2	9.9	1297.5	1510.3	-295.0	190.2	-78.5
4	63.00	28.4	30.2	3199	5718	8.9	5.3	1257.7	1385.8	-266.1	164.6	-42.8
4A	73.00	35.2	11.7	3199	5169	11.0	2.3	1229.3	1355.6	-252.4	152.2	-34.4
5	83.00	42.1	26.8	3199	4443	13.2	6.0	1194.1	1343.9	-238.9	140.1	-31.2
6	93.00	37.4	47.3	2754	4176	13.6	11.3	1151.9	1317.2	-225.5	128.3	-30.7
7	103.00	66.0	38.5	4715	2962	14.0	13.0	1114.6	1269.9	-212.6	117.0	-27.9
8	113.00	70.4	31.3	4581	2670	15.4	11.7	1048.6	1231.4	-200.1	106.2	-25.6
9	123.00	76.3	17.0	4403	2513	17.3	6.8	978.2	1200.1	-188.0	96.1	-23.7
10	133.00	85.1	13.9	4225	2379	20.1	5.8	901.9	1183.1	-176.0	86.7	-22.6
11	143.00	69.9	13.8	1443	1621	48.5	8.5	816.9	1169.2	-164.3	78.1	-21.4
12	153.00	63.6	20.6	1285	1489	49.5	13.8	746.9	1155.4	-152.6	70.2	-20.1
13	163.00	51.6	22.9	1100	1448	46.9	15.9	683.4	1134.9	-141.2	63.1	-19.0
14	173.00	49.1	26.7	1100	1448	44.6	18.4	631.8	1111.9	-130.0	56.5	-18.7
15	183.00	46.1	30.8	1100	1448	42.0	21.3	582.7	1085.2	-119.0	50.4	-18.3
16	193.00	43.2	34.9	1100	1448	39.3	24.1	536.6	1054.5	-108.3	44.8	-17.8
17	203.00	40.3	39.0	1100	1448	36.7	26.9	493.4	1019.6	-97.9	39.7	-17.2
18	213.00	37.6	42.6	1100	1448	34.2	29.4	453.0	980.7	-87.9	35.0	-16.4
19	223.00	35.1	45.7	1100	1448	31.9	31.5	415.5	938.0	-78.3	30.6	-15.7
20	233.00	32.6	48.7	1100	1448	29.6	33.6	380.4	892.4	-69.2	26.6	-14.9
21	243.00	30.1	51.7	1100	1448	27.3	35.7	347.8	843.7	-60.5	23.0	-14.0
22	253.00	27.6	54.7	1100	1448	25.1	37.8	317.8	792.0	-52.3	19.7	-13.2
23	263.00	26.7	56.9	1100	1448	24.3	39.3	290.2	737.2	-44.7	16.6	-12.4
24	273.00	26.5	58.6	1100	1448	24.1	40.5	263.5	680.4	-37.6	13.9	-11.5
25	283.00	26.3	60.4	1100	1448	24.0	41.7	237.0	621.7	-31.1	11.4	-10.6
26	293.00	26.2	62.2	1100	1448	23.8	43.0	210.6	561.3	-25.1	9.1	-9.6
27	303.00	25.9	63.8	1100	1448	23.6	44.0	184.5	499.1	-19.8	7.1	-8.6
28	313.00	25.0	63.7	1100	1448	22.7	44.0	158.5	435.4	-15.2	5.4	-7.5
29	323.00	24.0	63.6	1100	1448	21.8	43.9	133.6	371.7	-11.1	4.0	-6.5
30	333.00	23.1	63.5	1100	1448	21.0	43.9	109.5	308.1	-7.7	2.8	-5.4
31	343.00	32.8	95.1	1650	2171	19.9	43.8	86.5	244.6	-5.0	1.8	-4.4
MECH	358.00	53.6	149.4	2970	3908	18.1	38.2	53.6	149.4	-2.0	.7	-2.9

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 90 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT 1000-FT-KIPS	Y-MOMENT 1000-FT-KIPS	Z-MOMENT 1000-FT-KIPS
PARK	0.00	-1.4	-21.1	2676	7795	-.5	-2.7	2159.3	1725.2	-387.1	379.0	-90.7
PARK	14.00	4.9	-18.5	1911	5568	2.6	-3.3	2160.7	1746.3	-362.8	348.8	-97.0
2	24.00	129.9	34.9	6078	12768	21.4	2.7	2155.8	1764.8	-345.3	327.2	-102.9
3	43.00	124.4	148.3	6398	12568	19.5	11.8	2025.9	1729.9	-312.1	287.5	-86.2
4	63.00	66.7	11.5	3199	5718	20.8	2.0	1901.5	1581.6	-278.9	248.2	-43.1
4A	73.00	71.5	3.0	3199	5169	22.3	.6	1834.8	1570.2	-263.2	229.5	-37.8
5	83.00	79.1	37.1	3199	4443	24.7	8.3	1763.3	1567.2	-247.5	211.5	-36.4
6	93.00	69.7	82.5	2754	4176	25.3	19.8	1684.2	1530.1	-232.0	194.3	-35.7
7	103.00	90.8	75.2	4715	2962	19.3	25.4	1614.6	1447.6	-217.1	177.8	-30.3
8	113.00	100.9	67.7	4581	2670	22.0	25.4	1523.8	1372.4	-203.0	162.1	-24.0
9	123.00	107.6	47.5	4403	2513	24.4	18.9	1422.9	1304.7	-189.6	147.4	-19.1
10	133.00	113.6	48.5	4225	2379	26.9	20.4	1315.3	1257.2	-176.8	133.7	-17.2
11	143.00	86.1	39.4	1443	1621	59.7	24.3	1201.8	1208.7	-164.5	121.1	-15.9
12	153.00	78.5	33.8	1285	1489	61.1	22.7	1115.6	1169.4	-152.6	109.5	-14.1
13	163.00	66.5	29.9	1100	1448	60.4	20.7	1037.2	1135.6	-141.1	98.7	-13.0
14	173.00	64.8	30.3	1100	1448	59.0	20.9	970.7	1105.6	-129.9	88.7	-12.6
15	183.00	62.8	32.7	1100	1448	57.1	22.6	905.8	1075.4	-119.0	79.3	-12.2
16	193.00	60.7	35.2	1100	1448	55.2	24.3	843.0	1042.6	-108.4	70.6	-11.8
17	203.00	58.7	37.6	1100	1448	53.4	26.0	782.3	1007.5	-98.1	62.4	-11.4
18	213.00	56.6	40.4	1100	1448	51.5	27.9	723.6	969.8	-88.2	54.9	-11.0
19	223.00	54.6	43.5	1100	1448	49.6	30.1	667.0	929.4	-78.7	48.0	-10.5
20	233.00	52.5	46.7	1100	1448	47.7	32.3	612.4	885.9	-69.7	41.6	-10.1
21	243.00	50.4	49.9	1100	1448	45.8	34.5	559.9	839.2	-61.0	35.7	-9.6
22	253.00	48.4	53.0	1100	1448	44.0	36.6	509.5	789.3	-52.9	30.4	-9.1
23	263.00	46.7	55.2	1100	1448	42.5	38.1	461.1	736.3	-45.3	25.5	-8.6
24	273.00	45.3	56.9	1100	1448	41.2	39.3	414.4	681.1	-38.2	21.1	-8.1
25	283.00	43.8	58.6	1100	1448	39.8	40.5	369.1	624.3	-31.7	17.2	-7.5
26	293.00	42.4	60.3	1100	1448	38.5	41.6	325.3	565.7	-25.7	13.7	-6.8
27	303.00	40.9	61.9	1100	1448	37.2	42.8	282.9	505.4	-20.4	10.7	-6.2
28	313.00	39.5	62.7	1100	1448	35.9	43.3	242.0	443.5	-15.6	8.1	-5.5
29	323.00	38.0	63.5	1100	1448	34.5	43.9	202.5	380.8	-11.5	5.9	-4.8
30	333.00	36.5	64.4	1100	1448	33.2	44.5	164.5	317.3	-8.0	4.0	-4.1
31	343.00	52.0	98.1	1650	2171	31.5	45.2	128.0	252.9	-5.1	2.6	-3.4
MECH	358.00	75.9	154.8	2970	3908	25.6	39.6	75.9	154.8	-2.1	1.0	-2.4

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 100 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	15.8	-13.0	2676	7795	5.9	-1.7	2300.4	1672.3	-350.2	424.5	-106.9
PARK	14.00	14.0	-5.3	1911	5568	7.3	-.9	2284.6	1685.3	-326.7	392.4	-111.1
2	24.00	139.5	68.3	6078	12768	23.0	5.3	2270.6	1690.6	-309.8	369.6	-114.3
3	43.00	130.7	123.8	6398	12568	20.4	9.8	2131.1	1622.3	-278.4	327.8	-86.3
4	63.00	66.0	19.2	3199	5718	20.6	3.4	2000.3	1498.5	-247.2	286.5	-47.5
4A	73.00	66.6	13.7	3199	5169	20.8	2.7	1934.3	1479.2	-232.3	266.8	-40.1
5	83.00	68.6	39.4	3199	4443	21.4	8.9	1867.7	1465.5	-217.6	247.8	-35.9
6	93.00	58.7	83.3	2754	4176	21.3	19.9	1799.1	1426.1	-203.1	229.5	-33.8
7	103.00	75.1	78.7	4715	2962	15.9	26.6	1740.4	1342.9	-189.3	211.8	-27.5
8	113.00	86.2	73.4	4581	2670	18.8	27.5	1665.3	1264.1	-176.8	194.8	-20.9
9	123.00	94.2	56.7	4403	2513	21.4	22.6	1579.1	1190.7	-163.9	178.5	-15.6
10	133.00	101.2	57.8	4225	2379	23.9	24.3	1484.9	1134.0	-152.3	163.2	-13.2
11	143.00	87.5	44.5	1443	1621	60.6	27.4	1383.7	1076.2	-141.3	148.9	-11.5
12	153.00	80.2	38.5	1285	1489	62.4	25.9	1296.2	1031.7	-130.7	135.5	-9.6
13	163.00	68.0	31.4	1100	1448	61.8	21.7	1216.0	993.1	-120.6	122.9	-8.4
14	173.00	67.1	30.5	1100	1448	61.0	21.1	1148.0	961.7	-110.8	111.1	-8.1
15	183.00	65.8	32.0	1100	1448	59.8	22.1	1081.0	931.2	-101.4	100.0	-7.8
16	193.00	64.6	33.5	1100	1448	58.7	23.2	1015.1	899.1	-92.2	89.5	-7.5
17	203.00	63.4	35.0	1100	1448	57.6	24.2	950.5	865.6	-83.4	79.6	-7.2
18	213.00	62.1	36.8	1100	1448	56.4	25.4	887.2	830.6	-74.9	70.5	-7.0
19	223.00	60.7	39.0	1100	1448	55.2	27.0	825.1	793.8	-66.8	61.9	-6.7
20	233.00	59.3	41.2	1100	1448	53.9	28.5	764.4	754.7	-59.1	54.0	-6.4
21	243.00	57.8	43.4	1100	1448	52.6	30.0	705.2	713.5	-51.7	46.6	-6.1
22	253.00	56.4	45.6	1100	1448	51.3	31.5	647.3	670.2	-44.8	39.8	-5.8
23	263.00	55.4	47.2	1100	1448	50.3	32.6	590.9	624.6	-38.3	33.6	-5.4
24	273.00	54.4	48.6	1100	1448	49.5	33.6	535.5	577.4	-32.3	28.0	-5.1
25	283.00	53.5	50.0	1100	1448	48.6	34.6	481.1	528.7	-26.8	22.9	-4.8
26	293.00	52.6	51.4	1100	1448	47.8	35.5	427.6	478.2	-21.7	18.4	-4.4
27	303.00	51.7	52.8	1100	1448	47.0	36.4	375.0	427.2	-17.2	14.4	-4.1
28	313.00	50.7	53.2	1100	1448	46.1	36.7	323.3	374.5	-13.2	10.9	-3.7
29	323.00	49.8	53.6	1100	1448	45.3	37.0	272.6	321.3	-9.7	7.9	-3.3
30	333.00	48.9	54.0	1100	1448	44.5	37.3	222.7	267.7	-6.8	5.4	-2.9
31	343.00	71.7	81.8	1650	2171	43.5	37.7	173.8	213.7	-4.4	3.4	-2.5
MECH	358.00	102.1	131.8	2970	3908	34.4	33.7	102.1	131.8	-1.8	1.4	-1.8

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 110 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	40.9	-27.4	2676	7795	15.3	-3.5	2467.2	1348.1	-272.7	486.1	-97.9
PARK	14.00	5.7	-1.5	1911	5568	3.0	-.3	2426.3	1375.5	-253.6	451.8	-103.5
2	24.00	62.3	93.7	6078	12768	10.2	7.3	2420.6	1377.0	-239.8	427.6	-107.9
3	43.00	123.0	93.7	6398	12568	19.2	7.5	2358.3	1283.4	-214.6	382.2	-115.7
4	63.00	67.7	43.5	3199	5718	21.2	7.6	2235.4	1189.7	-189.8	336.2	-150.7
4A	73.00	70.5	31.0	3199	5169	22.0	6.0	2167.6	1146.2	-178.8	314.2	-339.7
5	83.00	69.8	38.3	3199	4443	21.8	8.6	2097.1	1115.1	-166.8	292.2	-330.8
6	93.00	57.9	71.0	2754	4176	21.0	17.0	2027.3	1076.8	-155.0	272.3	-321.8
7	103.00	76.6	66.1	4715	2962	16.2	22.3	1969.4	1005.0	-145.2	252.3	-311.8
8	113.00	87.6	57.9	4581	2670	19.1	21.3	1892.8	939.7	-135.5	232.4	-301.8
9	123.00	95.0	37.3	4403	2513	21.6	14.8	1805.2	881.8	-126.6	214.2	-291.8
10	133.00	100.8	33.1	4223	2379	23.8	13.9	1710.3	844.5	-118.8	196.0	-281.8
11	143.00	94.1	18.0	1443	1621	65.2	11.1	1609.5	811.4	-109.7	180.4	-271.8
12	153.00	85.7	23.2	1285	1489	66.7	15.6	1515.4	793.4	-101.9	164.7	-261.8
13	163.00	87.5	25.2	1100	1448	66.8	17.4	1429.6	770.2	-93.9	150.0	-251.8
14	173.00	72.6	25.4	1100	1448	66.0	17.6	1356.1	745.0	-86.0	136.8	-241.8
15	183.00	71.5	26.0	1100	1448	65.0	18.0	1283.5	719.6	-79.0	122.8	-231.8
16	193.00	70.3	26.7	1100	1448	63.9	18.4	1212.0	693.6	-71.9	110.4	-221.8
17	203.00	69.2	27.3	1100	1448	62.9	18.9	1141.7	666.9	-65.1	98.7	-211.8
18	213.00	68.3	28.2	1100	1448	62.1	19.5	1072.5	639.6	-58.3	87.7	-201.8
19	223.00	67.5	29.5	1100	1448	61.7	20.4	1004.2	611.4	-52.3	77.4	-191.8
20	233.00	67.1	30.9	1100	1448	61.4	21.3	936.8	581.9	-46.3	67.8	-181.8
21	243.00	67.1	32.2	1100	1448	61.0	22.2	868.7	551.0	-40.4	58.4	-171.8
22	253.00	66.7	33.5	1100	1448	60.6	23.2	801.7	518.8	-35.4	50.1	-161.8
23	263.00	66.2	34.8	1100	1448	60.1	24.2	735.0	485.3	-30.3	42.4	-151.8
24	273.00	65.6	36.0	1100	1448	59.6	24.9	668.8	450.5	-25.3	35.4	-141.8
25	283.00	65.0	37.3	1100	1448	59.1	25.8	603.2	414.4	-21.3	29.3	-131.8
26	293.00	64.4	38.5	1100	1448	58.6	26.6	538.2	377.2	-17.3	23.8	-121.8
27	303.00	63.8	39.8	1100	1448	58.0	27.5	473.8	338.8	-13.8	18.8	-111.8
28	313.00	63.4	40.9	1100	1448	57.6	28.3	410.0	299.3	-10.8	14.0	-101.8
29	323.00	62.9	42.1	1100	1448	57.2	29.1	346.6	258.4	-7.8	10.0	-91.8
30	333.00	62.5	43.3	1100	1448	56.8	29.9	283.7	215.9	-5.5	6.9	-82.1
31	343.00	92.9	67.1	1650	2171	56.3	30.9	221.2	172.6	-3.3	4.4	-71.8
MECH	358.00	128.3	105.5	2970	3908	43.2	27.0	128.3	105.5	-1.4	1.7	-1.3

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 120 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT	Z-MOMENT
										1000-FT-KIPS		
PARK	0.00	57.9	-53.5	2676	7795	21.6	-6.9	2914.6	673.1	-133.2	532.3	-92.1
PARK	14.00	34.0	-15.9	1911	5568	17.8	-2.9	2856.6	726.6	-123.4	491.9	-100.9
2	24.00	73.7	83.5	6078	12768	28.6	6.5	2822.6	742.6	-116.1	463.5	-105.4
3	43.00	179.8	79.5	6398	12568	28.1	6.3	2648.9	659.0	-102.7	411.5	-71.4
4	63.00	90.8	53.7	3199	5718	28.4	9.4	2469.0	579.5	-90.4	360.4	-45.2
4A	73.00	91.1	36.5	3199	5169	28.5	7.1	2378.3	525.9	-84.8	336.1	-33.2
5	83.00	91.3	26.8	3199	4443	28.5	6.0	2287.1	489.4	-79.7	312.8	-26.5
6	93.00	77.6	42.9	2754	4176	28.2	10.3	2195.8	462.6	-75.0	290.4	-23.5
7	103.00	95.6	38.3	4715	2962	20.3	12.9	2118.2	419.7	-70.6	268.8	-16.3
8	113.00	104.3	26.7	4581	2670	22.8	10.0	2022.6	381.4	-66.6	248.1	-9.9
9	123.00	110.4	4.1	4403	2513	25.1	1.6	1918.3	354.7	-62.9	228.4	-4.8
10	133.00	114.0	-3.0	4225	2379	27.0	-1.3	1807.9	350.6	-59.4	209.8	-2.0
11	143.00	96.0	-12.6	1443	1621	66.6	-7.7	1693.9	353.6	-55.8	192.3	.7
12	153.00	87.2	1.2	1285	1489	67.9	.8	1597.9	366.1	-52.2	175.8	1.7
13	163.00	74.7	8.8	1100	1448	67.9	6.1	1510.6	365.0	-48.6	160.3	2.4
14	173.00	74.1	9.4	1100	1448	67.4	6.5	1435.9	356.2	-45.0	145.5	2.5
15	183.00	73.4	9.5	1100	1448	66.7	6.6	1361.9	346.8	-41.5	131.5	2.5
16	193.00	72.7	9.6	1100	1448	66.1	6.6	1288.5	337.3	-38.0	118.3	2.5
17	203.00	72.0	9.7	1100	1448	65.4	6.7	1215.8	327.7	-34.7	105.8	2.4
18	213.00	71.4	10.1	1100	1448	64.9	7.0	1143.8	318.1	-31.5	94.0	2.2
19	223.00	71.0	11.2	1100	1448	64.5	7.7	1072.4	307.9	-28.4	82.9	2.0
20	233.00	70.6	12.2	1100	1448	64.1	8.4	1001.4	296.7	-25.3	72.5	1.8
21	243.00	70.1	13.3	1100	1448	63.8	9.2	930.8	284.5	-22.4	62.9	1.6
22	253.00	69.7	14.3	1100	1448	63.4	9.9	860.7	271.3	-19.7	53.9	1.4
23	263.00	69.7	15.3	1100	1448	63.4	10.6	791.0	257.0	-17.0	45.6	1.1
24	273.00	69.9	16.4	1100	1448	63.5	11.3	721.3	241.6	-14.5	38.1	.9
25	283.00	70.1	17.4	1100	1448	63.7	12.0	651.4	225.2	-12.2	31.2	.7
26	293.00	70.2	18.4	1100	1448	63.8	12.7	581.3	207.8	-10.0	25.0	.5
27	303.00	70.3	19.5	1100	1448	63.9	13.5	511.1	189.4	-8.0	19.6	.3
28	313.00	69.1	20.9	1100	1448	62.9	14.5	440.8	169.9	-6.2	14.8	.1
29	323.00	68.0	22.4	1100	1448	61.8	15.5	371.7	148.9	-4.6	10.8	-.1
30	333.00	66.9	23.8	1100	1448	60.8	16.4	303.7	126.5	-3.3	7.4	-.2
31	343.00	98.3	38.4	1650	2171	59.5	17.7	236.8	102.7	-2.1	4.7	-.3
MECH	358.00	138.5	64.3	2970	3908	46.6	16.5	138.5	64.3	-.9	1.9	-.3

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 130 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	72.9	-71.3	2676	7795	27.3	-9.1	3284.3	-119.5	22.8	566.3	-89.4
PARK	14.00	74.6	-31.6	1911	5568	39.1	-5.7	3211.4	-48.3	21.6	520.8	-102.1
2	24.00	320.0	62.4	6078	12768	52.7	4.9	3136.8	-16.7	21.3	489.1	-106.7
3	43.00	230.6	30.0	6398	12568	36.0	2.4	2816.7	-79.1	20.4	432.5	-62.6
4	63.00	103.2	33.7	3199	5718	32.3	5.9	2586.2	-109.0	18.5	378.5	-42.3
4A	73.00	97.0	18.7	3199	5169	30.3	3.6	2482.9	-142.8	17.2	353.1	-32.3
5	83.00	98.2	8.5	3199	4443	30.7	1.9	2385.9	-161.5	15.7	328.8	-27.0
6	93.00	86.4	20.1	2754	4176	31.4	4.8	2287.7	-170.0	14.1	305.4	-23.6
7	103.00	99.0	23.5	4715	2962	21.0	7.9	2201.3	-190.1	12.3	283.0	-15.8
8	113.00	109.2	8.3	4581	2670	23.8	3.1	2102.3	-213.6	10.2	261.5	-9.1
9	123.00	116.4	-23.4	4403	2513	26.4	-9.3	1993.1	-222.0	8.1	241.0	-3.3
10	133.00	121.7	-41.2	4225	2379	28.8	-17.3	1876.7	-198.6	6.0	221.6	.6
11	143.00	96.0	-52.4	1443	1621	66.5	-32.3	1755.0	-157.4	4.2	203.5	4.9
12	153.00	85.2	-30.3	1285	1489	66.3	-20.3	1659.0	-105.0	2.9	186.4	5.3
13	163.00	70.6	-11.1	1100	1448	64.2	-7.7	1573.8	-74.7	2.0	170.2	5.5
14	173.00	70.7	-8.5	1100	1448	64.3	-5.8	1503.2	-63.6	1.3	154.9	5.4
15	183.00	71.4	-7.4	1100	1448	64.9	-5.1	1432.5	-55.2	.7	140.2	5.2
16	193.00	72.0	-6.4	1100	1448	65.5	-4.4	1361.1	-47.7	.2	126.2	5.1
17	203.00	72.7	-5.4	1100	1448	66.1	-3.7	1289.0	-41.3	-.3	113.0	4.9
18	213.00	73.2	-5.0	1100	1448	66.6	-3.5	1216.3	-36.0	-.7	100.4	4.8
19	223.00	73.5	-5.6	1100	1448	66.8	-3.9	1143.1	-31.0	-1.0	88.6	4.6
20	233.00	73.8	-6.3	1100	1448	67.1	-4.3	1069.6	-25.3	-1.3	77.6	4.4
21	243.00	74.1	-6.9	1100	1448	67.3	-4.8	995.9	-19.1	-1.5	67.2	4.2
22	253.00	74.3	-7.6	1100	1448	67.6	-5.2	921.8	-12.1	-1.6	57.7	4.0
23	263.00	74.6	-7.1	1100	1448	67.8	-4.9	847.5	-4.6	-1.7	48.8	3.8
24	273.00	74.9	-6.2	1100	1448	68.0	-4.3	772.9	2.6	-1.7	40.7	3.5
25	283.00	75.1	-5.4	1100	1448	68.3	-3.7	698.0	8.8	-1.7	33.4	3.2
26	293.00	75.4	-4.5	1100	1448	68.5	-3.1	622.9	14.2	-1.6	26.7	2.8
27	303.00	75.5	-3.5	1100	1448	68.6	-2.4	547.5	18.6	-1.4	20.9	2.5
28	313.00	74.4	-1.7	1100	1448	67.6	-1.2	472.1	22.1	-1.2	15.8	2.1
29	323.00	73.3	.0	1100	1448	66.6	.0	397.7	23.9	-1.0	11.4	1.7
30	333.00	72.2	1.8	1100	1448	65.7	1.2	324.4	23.9	-.7	7.8	1.4
31	343.00	106.3	5.9	1650	2171	64.4	2.7	252.2	22.1	-.5	5.0	1.0
MECH	358.00	145.9	16.1	2970	3908	49.1	4.1	145.9	16.1	-.2	2.0	.6

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 140 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	92.6	-81.4	2676	7795	34.6	-10.4	3437.9	-632.3	103.5	610.2	-77.3
PARK	14.00	68.8	-45.8	1911	5568	36.0	-8.2	3345.2	-550.9	95.3	562.7	-91.3
2	24.00	250.6	26.3	6078	12768	41.2	2.1	3276.4	-505.0	90.1	529.6	-99.9
3	43.00	215.0	-25.5	6398	12568	33.6	-2.0	3025.8	-531.3	80.1	469.7	-69.5
4	63.00	102.0	9.7	3199	5718	31.9	1.7	2810.8	-505.8	69.8	411.3	-59.1
4A	73.00	100.5	-6.2	3199	5169	31.4	-1.2	2708.8	-515.4	64.7	383.7	-51.2
5	83.00	103.5	-15.4	3199	4443	32.4	-3.5	2608.3	-509.2	59.5	357.1	-46.6
6	93.00	94.0	-15.0	2754	4176	34.1	-3.6	2504.7	-493.8	54.5	331.6	-42.4
7	103.00	122.8	-6.0	4715	2962	26.1	-2.0	2410.8	-478.8	49.7	307.0	-33.7
8	113.00	129.3	-19.6	4581	2670	28.2	-7.3	2288.0	-472.8	44.9	283.5	-24.9
9	123.00	134.1	-42.0	4403	2513	30.5	-16.7	2158.7	-453.2	40.3	261.3	-16.9
10	133.00	139.4	-53.8	4225	2379	33.0	-22.6	2024.6	-411.3	35.9	240.4	-9.9
11	143.00	98.4	-60.1	1443	1621	68.2	-37.1	1885.2	-357.4	32.1	220.8	-1.9
12	153.00	89.3	-35.6	1285	1489	69.5	-23.9	1786.8	-297.3	28.8	202.4	-1.6
13	163.00	76.1	-16.6	1100	1448	69.2	-11.5	1697.5	-261.7	26.0	185.0	-1.1
14	173.00	76.5	-14.3	1100	1448	69.6	-9.9	1621.4	-245.0	23.5	168.4	-1.1
15	183.00	76.9	-13.8	1100	1448	69.9	-9.5	1544.9	-230.7	21.1	152.6	-1.1
16	193.00	77.2	-13.3	1100	1448	70.2	-9.2	1468.0	-216.9	18.8	137.5	-1.2
17	203.00	77.5	-12.7	1100	1448	70.5	-8.8	1390.8	-203.9	16.8	123.2	-1.1
18	213.00	77.8	-12.4	1100	1448	70.8	-8.6	1313.3	-190.9	14.8	109.7	-1.0
19	223.00	78.1	-12.5	1100	1448	71.0	-8.6	1235.4	-178.5	13.0	97.0	-1.0
20	233.00	78.5	-12.5	1100	1448	71.3	-8.6	1157.3	-166.5	11.2	85.0	-.9
21	243.00	78.8	-12.6	1100	1448	71.6	-8.7	1078.8	-153.5	9.6	73.8	-.7
22	253.00	79.1	-12.6	1100	1448	71.9	-8.7	1000.1	-141.0	8.2	63.4	-.6
23	263.00	79.3	-12.6	1100	1448	72.1	-8.7	921.0	-128.4	6.8	53.8	-.5
24	273.00	79.4	-12.7	1100	1448	72.2	-8.8	841.8	-115.8	5.6	45.0	-.4
25	283.00	79.6	-12.7	1100	1448	72.4	-8.8	762.3	-103.1	4.5	37.0	-.3
26	293.00	79.8	-12.7	1100	1448	72.5	-8.8	682.7	-90.3	3.5	29.8	-.2
27	303.00	79.9	-12.7	1100	1448	72.7	-8.8	602.9	-77.7	2.7	23.3	-.1
28	313.00	79.7	-12.1	1100	1448	72.5	-8.3	523.0	-65.0	2.0	17.7	.0
29	323.00	79.6	-11.4	1100	1448	72.3	-7.9	443.2	-52.9	1.4	12.9	.1
30	333.00	79.4	-10.8	1100	1448	72.2	-7.4	363.7	-41.5	.9	8.8	.1
31	343.00	118.7	-15.0	1650	2171	71.9	-6.9	284.3	-30.7	.6	5.6	.1
MECH	358.00	165.6	-15.7	2970	3908	55.8	-4.0	165.6	-15.7	.2	2.2	.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY GUST FACTOR 1.32
WIND DIRECTION 150 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	105.1	-93.6	2676	7795	39.3	-12.0	3455.6	-690.2	80.6	638.0	-49.4
PARK	14.00	54.1	-54.3	1911	5568	28.3	-9.8	3350.5	-596.7	71.6	590.4	-67.8
2	24.00	153.8	-21.1	6078	12768	25.3	-1.6	3296.4	-542.3	65.9	557.2	-80.6
3	43.00	184.0	-33.2	6398	12568	28.8	-2.6	3142.6	-521.3	55.8	496.0	-74.5
4	63.00	94.7	5.1	3199	5718	29.6	.9	2958.6	-488.1	45.7	435.0	-70.3
4A	73.00	97.5	-12.2	3199	5169	30.5	-2.4	2863.9	-493.2	40.8	405.9	-64.5
5	83.00	100.9	-23.2	3199	4443	31.5	-5.2	2766.4	-481.0	35.9	377.7	-61.2
6	93.00	96.2	-33.7	2754	4176	34.9	-8.1	2665.5	-457.9	31.2	350.5	-56.6
7	103.00	135.3	-27.1	4715	2962	28.7	-9.1	2569.4	-424.1	26.8	324.4	-48.0
8	113.00	143.5	-41.7	4581	2670	31.3	-15.6	2434.1	-397.1	22.7	299.4	-38.4
9	123.00	147.5	-54.0	4403	2513	33.5	-21.5	2290.6	-355.3	19.0	275.7	-29.1
10	133.00	152.7	-55.7	4225	2379	36.1	-23.4	2143.1	-301.4	15.7	253.6	-20.2
11	143.00	103.8	-56.5	1443	1621	72.0	-34.8	1990.4	-245.7	12.9	232.9	-9.9
12	153.00	95.0	-31.0	1285	1489	73.9	-20.8	1886.6	-189.2	10.8	213.5	-9.1
13	163.00	79.9	-19.5	1100	1448	72.7	-13.4	1791.6	-158.2	9.0	195.1	-8.3
14	173.00	80.5	-17.6	1100	1448	73.2	-12.2	1711.7	-138.7	7.5	177.6	-8.1
15	183.00	80.9	-15.7	1100	1448	73.6	-10.9	1631.2	-121.1	6.2	160.9	-8.0
16	193.00	81.3	-13.8	1100	1448	73.9	-9.6	1550.3	-105.4	5.1	145.0	-7.8
17	203.00	81.7	-12.0	1100	1448	74.3	-8.3	1468.9	-91.5	4.1	129.9	-7.5
18	213.00	82.2	-10.7	1100	1448	74.7	-7.4	1387.2	-79.6	3.3	115.6	-7.1
19	223.00	82.8	-10.3	1100	1448	75.3	-7.1	1305.0	-68.9	2.5	102.1	-6.7
20	233.00	83.4	-9.9	1100	1448	75.8	-6.9	1222.2	-58.6	1.9	89.5	-6.3
21	243.00	83.9	-9.6	1100	1448	76.3	-6.6	1138.9	-48.6	1.4	77.7	-5.9
22	253.00	84.5	-9.2	1100	1448	76.8	-6.4	1054.9	-39.0	.9	66.7	-5.5
23	263.00	84.6	-8.2	1100	1448	76.9	-5.6	970.4	-29.8	.6	56.6	-5.1
24	273.00	84.4	-6.9	1100	1448	76.8	-4.7	885.8	-21.7	.3	47.3	-4.7
25	283.00	84.3	-5.5	1100	1448	76.6	-3.8	801.4	-14.8	.1	38.9	-4.3
26	293.00	84.2	-4.2	1100	1448	76.5	-2.9	717.1	-9.3	.0	31.3	-3.8
27	303.00	84.0	-3.0	1100	1448	76.4	-2.0	632.9	-5.1	-.1	24.6	-3.4
28	313.00	83.6	-2.3	1100	1448	76.0	-1.6	548.9	-2.1	-.1	18.6	-2.9
29	323.00	83.2	-1.6	1100	1448	75.7	-1.1	465.3	-.1	-.1	13.6	-2.5
30	333.00	82.9	-.9	1100	1448	75.3	-.6	382.0	1.7	-.1	9.3	-2.1
31	343.00	123.6	-.0	1650	2171	74.9	-.0	299.2	2.6	-.1	5.9	-1.7
MECH	358.00	175.5	2.6	2970	3908	59.1	.7	175.5	2.6	-.0	2.4	-1.1

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 160 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	111.2	-98.7	2676	7795	41.6	-12.7	3657.4	-622.5	30.4	656.3	-46.1
PARK	14.00	64.6	-67.1	1911	5568	33.8	-12.0	3546.2	-523.8	22.4	605.9	-68.2
2	24.00	195.8	-76.0	6078	12768	32.2	-6.0	3481.6	-456.7	17.5	570.7	-84.8
3	43.00	210.7	-33.2	6398	12568	32.9	-2.6	3285.8	-380.8	9.6	506.4	-91.0
4	63.00	107.8	-5.3	3199	5718	33.7	-.9	3075.1	-347.5	2.3	442.8	-85.3
4A	73.00	108.3	-19.7	3199	5169	33.9	-3.8	2967.2	-342.2	-1.2	412.6	-79.9
5	83.00	108.1	-32.9	3199	4443	33.8	-7.4	2858.9	-322.5	-4.5	383.5	-75.7
6	93.00	104.7	-53.9	2754	4176	38.0	-12.9	2750.7	-289.6	-7.5	355.4	-69.7
7	103.00	151.3	-44.3	4715	2962	32.1	-15.0	2646.0	-235.7	-10.2	328.5	-60.6
8	113.00	159.8	-56.7	4581	2670	34.9	-21.2	2494.7	-191.4	-12.3	302.8	-50.6
9	123.00	163.0	-62.7	4403	2513	37.0	-24.9	2334.9	-134.7	-13.9	278.6	-40.5
10	133.00	164.2	-57.8	4225	2379	38.9	-24.3	2171.9	-72.1	-15.0	256.1	-30.5
11	143.00	100.4	-47.8	1443	1621	69.6	-29.5	2007.8	-14.3	-15.4	235.2	-19.5
12	153.00	92.5	-16.6	1285	1489	72.0	-11.2	1907.4	33.5	-15.3	215.6	-17.0
13	163.00	80.0	-12.0	1100	1448	72.7	-8.3	1814.9	50.2	-14.9	197.0	-16.8
14	173.00	81.3	-9.8	1100	1448	73.9	-6.7	1734.9	62.2	-14.3	179.2	-15.7
15	183.00	82.1	-7.2	1100	1448	74.7	-5.0	1653.6	71.9	-13.7	162.3	-15.0
16	193.00	83.0	-4.7	1100	1448	75.4	-3.2	1571.5	79.2	-12.9	146.2	-14.4
17	203.00	83.8	-2.1	1100	1448	76.2	-1.5	1488.5	83.8	-12.1	130.9	-13.7
18	213.00	84.5	-.7	1100	1448	76.8	-.5	1404.7	86.0	-11.2	116.4	-13.0
19	223.00	84.8	-.8	1100	1448	77.1	-.6	1320.2	86.7	-10.4	102.8	-12.3
20	233.00	85.2	-1.0	1100	1448	77.4	-.7	1235.4	87.5	-9.5	90.0	-11.7
21	243.00	85.5	-1.2	1100	1448	77.7	-.8	1150.2	88.5	-8.6	78.1	-11.0
22	253.00	85.9	-1.3	1100	1448	78.1	-.9	1064.7	89.7	-7.7	67.0	-10.4
23	263.00	85.9	.1	1100	1448	78.1	.1	978.8	91.0	-6.8	56.8	-9.8
24	273.00	85.9	2.2	1100	1448	78.1	1.5	892.9	90.9	-5.9	47.4	-9.1
25	283.00	85.9	4.3	1100	1448	78.1	3.0	807.0	88.7	-5.0	38.9	-8.5
26	293.00	85.8	6.4	1100	1448	78.0	4.5	721.1	84.3	-4.2	31.3	-7.8
27	303.00	85.7	8.4	1100	1448	77.9	5.8	635.3	77.9	-3.4	24.5	-7.0
28	313.00	84.9	8.6	1100	1448	77.2	6.0	549.6	69.5	-2.6	18.6	-6.3
29	323.00	84.1	8.9	1100	1448	76.4	6.1	464.7	60.9	-2.0	13.5	-5.5
30	333.00	83.2	9.1	1100	1448	75.7	6.3	380.6	52.0	-1.4	9.3	-4.6
31	343.00	123.3	14.2	1650	2171	74.7	6.5	297.4	42.8	-.9	5.9	-3.7
MECH	358.00	174.2	28.6	2970	3908	58.6	7.3	174.2	28.6	-.4	2.4	-2.3

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 170 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT	Z-MOMENT
										1000-FT-KIPS		
PARK	0.00	109.3	-113.3	2676	7795	40.8	-14.5	3784.3	-1033.1	98.7	642.9	-51.4
PARK	14.00	85.3	-80.8	1911	5568	44.6	-14.5	3675.0	-919.9	85.1	590.7	-79.0
2	24.00	291.6	-124.3	6078	12768	48.0	-9.7	3589.7	-839.1	76.3	554.3	-97.6
3	43.00	245.1	-52.6	6398	12568	38.3	-4.1	3298.1	-714.8	61.5	488.9	-105.3
4	63.00	120.7	-20.3	3199	5718	37.7	-3.5	3053.0	-662.7	47.7	425.4	-98.3
4A	73.00	117.1	-28.8	3199	5169	36.6	-5.6	2932.3	-642.5	41.2	395.5	-93.3
5	83.00	113.5	-40.3	3199	4443	35.5	-9.1	2815.2	-613.7	34.9	366.7	-88.4
6	93.00	109.0	-73.0	2754	4176	39.6	-17.5	2701.7	-573.4	29.0	339.1	-80.9
7	103.00	162.8	-61.3	4715	2962	34.5	-20.7	2592.6	-500.4	23.6	312.7	-71.1
8	113.00	169.3	-72.0	4581	2670	37.0	-27.0	2429.8	-439.1	18.9	287.6	-60.1
9	123.00	171.0	-74.5	4403	2513	38.8	-29.6	2260.6	-367.1	14.9	264.1	-49.1
10	133.00	171.9	-69.4	4225	2379	40.7	-29.2	2089.6	-292.6	11.6	242.4	-37.7
11	143.00	96.5	-57.7	1443	1621	66.9	-35.6	1917.7	-223.1	9.0	222.3	-24.8
12	153.00	89.6	-28.8	1285	1489	69.8	-19.4	1821.2	-165.4	7.1	203.6	-23.7
13	163.00	77.7	-24.7	1100	1448	70.6	-17.1	1731.6	-136.6	5.6	185.9	-22.1
14	173.00	79.1	-21.8	1100	1448	71.9	-15.0	1653.9	-111.9	4.3	168.9	-21.3
15	183.00	79.8	-18.2	1100	1448	72.5	-12.6	1574.8	-90.2	3.3	152.8	-20.5
16	193.00	80.4	-14.7	1100	1448	73.1	-10.1	1495.0	-72.0	2.5	137.4	-19.6
17	203.00	81.1	-11.1	1100	1448	73.7	-7.7	1414.6	-57.3	1.9	122.9	-18.7
18	213.00	81.6	-8.8	1100	1448	74.2	-6.1	1333.5	-46.2	1.3	109.2	-17.7
19	223.00	82.0	-8.4	1100	1448	74.6	-5.8	1251.9	-37.4	.9	96.2	-16.8
20	233.00	82.4	-7.9	1100	1448	74.9	-5.5	1169.9	-29.0	.6	84.1	-15.8
21	243.00	82.8	-7.5	1100	1448	75.3	-5.2	1087.5	-21.1	.3	72.8	-14.8
22	253.00	83.2	-7.0	1100	1448	75.6	-4.9	1004.7	-13.6	.2	62.4	-13.8
23	263.00	83.1	-5.5	1100	1448	75.5	-3.8	921.5	-6.6	.1	52.7	-12.8
24	273.00	82.7	-3.4	1100	1448	75.2	-2.3	838.4	-1.1	.0	43.9	-11.9
25	283.00	82.4	-1.3	1100	1448	74.9	-.9	755.6	2.2	.0	36.0	-10.9
26	293.00	82.1	.8	1100	1448	74.6	.5	673.2	3.5	.1	28.8	-9.9
27	303.00	81.6	2.6	1100	1448	74.2	1.8	591.2	2.7	.1	22.5	-8.8
28	313.00	80.5	1.7	1100	1448	73.2	1.2	509.6	.2	.1	17.0	-7.8
29	323.00	79.4	.9	1100	1448	72.2	.6	429.0	-1.6	.1	12.3	-6.8
30	333.00	78.3	.1	1100	1448	71.2	.1	349.6	-2.5	.1	8.4	-5.7
31	343.00	115.4	-1.4	1650	2171	70.0	-.6	271.3	-2.6	.0	5.3	-4.6
MECH	358.00	155.9	-1.2	2970	3908	52.5	-.3	155.9	-1.2	.0	2.1	-2.7

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 180 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	109.3	-117.8	2676	7795	40.8	-15.1	3750.4	-1746.8	246.8	624.6	-43.9
PARK	14.00	75.6	-89.7	1911	5568	39.6	-16.1	3641.2	-1629.1	223.2	572.9	-70.8
2	24.00	272.5	-162.2	6078	12768	44.8	-12.7	3565.6	-1539.4	207.4	536.8	-90.8
3	43.00	254.6	-89.5	6398	12568	39.8	-7.1	3293.1	-1377.2	179.7	471.7	-102.6
4	63.00	129.2	-40.2	3199	5718	40.4	-7.0	3038.5	-1287.7	153.0	408.3	-97.2
4A	73.00	127.2	-43.1	3199	5169	39.8	-8.3	2909.3	-1247.5	140.3	378.6	-93.1
5	83.00	122.2	-53.2	3199	4443	38.2	-12.0	2782.1	-1204.4	128.1	350.1	-88.2
6	93.00	117.4	-91.7	2754	4176	42.6	-22.0	2659.9	-1151.2	116.3	322.9	-80.1
7	103.00	177.6	-76.9	4715	2962	37.7	-26.0	2542.5	-1059.5	105.2	296.9	-70.5
8	113.00	182.4	-86.1	4581	2670	39.8	-32.3	2364.9	-982.6	95.0	272.4	-58.9
9	123.00	184.2	-85.3	4403	2513	41.8	-33.9	2182.6	-896.4	85.6	249.6	-47.6
10	133.00	183.3	-81.8	4225	2379	43.4	-34.4	1998.4	-811.2	77.1	228.7	-35.9
11	143.00	91.4	-73.6	1443	1621	63.4	-45.4	1815.1	-729.3	69.4	209.7	-21.9
12	153.00	84.9	-51.8	1285	1489	66.1	-34.8	1723.7	-655.8	62.5	192.0	-21.1
13	163.00	74.4	-42.1	1100	1448	67.7	-29.1	1638.8	-604.0	56.2	175.2	-19.9
14	173.00	76.0	-40.0	1100	1448	69.1	-27.6	1564.4	-561.9	50.3	159.2	-19.2
15	183.00	76.3	-37.8	1100	1448	69.4	-26.1	1488.4	-521.8	44.9	143.9	-18.4
16	193.00	76.7	-35.6	1100	1448	69.7	-24.6	1412.0	-484.0	39.9	129.4	-17.6
17	203.00	77.0	-33.5	1100	1448	70.0	-23.1	1335.3	-448.4	35.2	115.7	-16.8
18	213.00	77.4	-32.1	1100	1448	70.4	-22.2	1258.3	-414.9	30.9	102.7	-16.0
19	223.00	77.8	-31.9	1100	1448	70.8	-22.0	1180.9	-382.8	26.9	90.5	-15.1
20	233.00	78.2	-31.7	1100	1448	71.1	-21.9	1103.1	-350.9	23.3	79.1	-14.2
21	243.00	78.7	-31.5	1100	1448	71.5	-21.7	1024.8	-319.3	19.9	68.4	-13.3
22	253.00	79.1	-31.3	1100	1448	71.9	-21.6	946.2	-287.8	16.9	58.6	-12.4
23	263.00	78.9	-29.4	1100	1448	71.7	-20.3	867.1	-256.6	14.1	49.5	-11.4
24	273.00	78.4	-26.8	1100	1448	71.3	-18.5	788.2	-227.2	11.7	41.2	-10.4
25	283.00	77.9	-24.3	1100	1448	70.8	-16.8	709.9	-200.3	9.6	33.7	-9.4
26	293.00	77.4	-21.7	1100	1448	70.4	-15.0	632.0	-176.1	7.7	27.0	-8.4
27	303.00	76.8	-19.4	1100	1448	69.9	-13.4	554.6	-154.4	6.1	21.1	-7.4
28	313.00	75.7	-19.8	1100	1448	68.8	-13.7	477.7	-134.9	4.6	15.9	-6.4
29	323.00	74.5	-20.1	1100	1448	67.7	-13.9	402.0	-115.2	3.4	11.5	-5.3
30	333.00	73.3	-20.5	1100	1448	66.7	-14.2	327.5	-95.0	2.3	7.9	-4.4
31	343.00	107.8	-31.4	1650	2171	65.3	-14.5	254.2	-74.5	1.5	5.0	-3.4
MECH	358.00	146.4	-43.1	2970	3908	49.3	-11.0	146.4	-43.1	.6	2.0	-1.9

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 190 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	89.7	-118.9	2676	7795	33.5	-15.3	3494.9	-2277.1	366.9	573.6	-25.3
PARK	14.00	68.1	-91.5	1911	5568	35.7	-16.4	3405.2	-2158.2	335.9	525.3	-52.5
2	24.00	267.1	-181.5	6078	12768	44.0	-14.2	3337.1	-2066.8	314.8	491.6	-71.9
3	43.00	244.2	-102.0	6398	12568	38.2	-8.1	3069.9	-1885.3	277.2	430.7	-85.6
4	63.00	124.4	-50.1	3199	5718	38.9	-8.8	2825.8	-1783.3	240.5	371.8	-81.9
4A	73.00	122.7	-52.3	3199	5169	38.4	-10.1	2701.4	-1733.2	223.0	344.1	-79.5
5	83.00	119.7	-62.8	3199	4443	37.4	-14.1	2578.7	-1680.9	205.9	317.7	-75.6
6	93.00	114.9	-100.6	2754	4176	41.7	-24.1	2459.0	-1618.1	189.4	292.5	-68.4
7	103.00	176.4	-87.4	4715	2962	37.4	-29.5	2344.0	-1517.5	173.7	268.5	-59.4
8	113.00	178.2	-95.8	4581	2670	38.9	-35.9	2167.6	-1430.1	159.0	246.0	-48.1
9	123.00	178.8	-92.3	4403	2513	40.6	-36.7	1989.5	-1334.3	145.1	225.2	-37.3
10	133.00	175.8	-90.2	4225	2379	41.6	-37.9	1810.7	-1242.0	132.3	206.0	-25.6
11	143.00	82.2	-86.7	1443	1621	56.9	-53.5	1634.9	-1151.8	120.3	189.0	-12.9
12	153.00	77.1	-70.6	1285	1489	60.0	-47.4	1552.7	-1065.1	109.2	173.9	-12.3
13	163.00	67.3	-56.5	1100	1448	61.2	-39.0	1475.7	-994.5	98.9	157.9	-11.6
14	173.00	69.0	-55.2	1100	1448	62.7	-38.1	1408.4	-938.0	89.3	143.5	-11.1
15	183.00	69.2	-53.9	1100	1448	62.9	-37.3	1339.4	-882.8	80.1	129.7	-10.6
16	193.00	69.4	-52.7	1100	1448	63.1	-36.4	1270.2	-828.9	71.6	116.7	-10.1
17	203.00	69.6	-51.4	1100	1448	63.2	-35.5	1200.8	-776.2	63.6	104.3	-9.6
18	213.00	69.7	-50.6	1100	1448	63.4	-34.9	1131.2	-724.8	56.1	92.6	-9.1
19	223.00	69.9	-50.4	1100	1448	63.5	-34.8	1061.5	-674.3	49.1	81.7	-8.6
20	233.00	70.0	-50.2	1100	1448	63.7	-34.7	991.6	-623.9	42.6	71.4	-8.1
21	243.00	70.2	-50.1	1100	1448	63.8	-34.6	921.6	-573.6	36.6	61.9	-7.5
22	253.00	70.3	-49.9	1100	1448	63.9	-34.5	851.4	-523.6	31.1	53.0	-7.0
23	263.00	70.2	-48.6	1100	1448	63.8	-33.5	781.1	-473.7	26.1	44.8	-6.4
24	273.00	69.9	-46.7	1100	1448	63.5	-32.3	710.9	-425.1	21.6	37.4	-5.9
25	283.00	69.6	-44.9	1100	1448	63.3	-31.0	641.1	-378.4	17.6	30.6	-5.3
26	293.00	69.3	-43.0	1100	1448	63.0	-29.7	571.5	-333.5	14.0	24.5	-4.7
27	303.00	69.0	-41.2	1100	1448	62.7	-28.5	502.2	-290.6	10.9	19.2	-4.1
28	313.00	68.1	-40.4	1100	1448	61.9	-27.9	433.2	-249.3	8.2	14.5	-3.5
29	323.00	67.2	-39.5	1100	1448	61.1	-27.3	365.1	-208.9	5.9	10.5	-2.9
30	333.00	66.3	-38.7	1100	1448	60.3	-26.7	297.9	-169.4	4.0	7.2	-2.4
31	343.00	97.9	-56.5	1650	2171	59.3	-26.0	231.6	-130.7	2.5	4.5	-1.8
MECH	358.00	133.7	-74.2	2970	3908	45.0	-19.0	133.7	-74.2	1.0	1.8	-1.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 200 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	73.8	-112.2	2676	7795	27.6	-14.4	2797.8	-2578.9	437.1	466.2	1.0
PARK	14.00	45.3	-88.2	1911	5568	23.7	-15.8	2724.0	-2466.7	401.8	427.6	-22.0
2	24.00	173.4	-189.4	6078	12768	28.5	-14.8	2678.7	-2378.6	377.5	400.6	-39.6
3	43.00	184.7	-121.3	6398	12568	28.9	-9.6	2505.3	-2189.1	334.2	351.3	-58.4
4	63.00	97.7	-65.5	3199	5718	30.5	-11.5	2320.6	-2067.9	291.6	303.0	-58.3
4A	73.00	99.1	-65.6	3199	5169	31.0	-12.7	2222.9	-2002.3	271.2	280.3	-58.3
5	83.00	99.0	-72.1	3199	4443	31.0	-16.2	2123.8	-1936.7	251.5	258.6	-56.4
6	93.00	95.6	-108.0	2754	4176	34.7	-25.9	2024.8	-1864.6	232.5	237.9	-50.4
7	103.00	151.6	-90.7	4715	2962	32.2	-30.6	1929.1	-1756.6	214.4	218.1	-43.9
8	113.00	152.5	-95.4	4581	2670	33.3	-35.7	1777.5	-1665.9	197.3	199.5	-34.4
9	123.00	153.4	-91.3	4403	2513	34.8	-36.3	1625.0	-1570.6	181.1	182.5	-25.1
10	133.00	150.3	-91.8	4225	2379	35.6	-38.6	1471.6	-1479.3	165.9	167.1	-14.9
11	143.00	66.3	-89.8	1443	1621	45.9	-55.4	1321.3	-1387.6	151.5	153.1	-3.9
12	153.00	62.9	-79.0	1285	1489	48.9	-53.1	1255.0	-1297.7	138.1	140.2	3.6
13	163.00	54.0	-62.2	1100	1448	49.1	-43.0	1192.2	-1218.7	125.5	128.0	8.3
14	173.00	55.7	-61.5	1100	1448	50.6	-42.5	1138.2	-1156.5	113.7	116.3	13.1
15	183.00	55.9	-61.1	1100	1448	50.8	-42.2	1082.5	-1095.0	102.4	105.2	17.8
16	193.00	56.1	-60.8	1100	1448	51.0	-42.0	1026.6	-1033.8	91.8	94.7	22.7
17	203.00	56.3	-60.4	1100	1448	51.2	-41.7	970.6	-973.1	81.7	84.7	27.5
18	213.00	56.4	-60.2	1100	1448	51.3	-41.6	914.3	-912.6	72.3	75.3	32.3
19	223.00	56.5	-60.1	1100	1448	51.3	-41.5	857.8	-852.5	63.5	66.4	37.1
20	233.00	56.5	-60.1	1100	1448	51.4	-41.5	801.4	-792.3	55.2	58.1	42.0
21	243.00	56.6	-60.1	1100	1448	51.4	-41.5	744.8	-732.2	47.6	50.4	46.8
22	253.00	56.6	-60.0	1100	1448	51.5	-41.5	688.3	-672.2	40.6	43.2	51.7
23	263.00	56.3	-59.2	1100	1448	51.2	-40.9	631.7	-612.2	34.2	36.6	56.5
24	273.00	55.9	-58.0	1100	1448	50.9	-40.1	575.3	-553.0	28.4	30.6	61.5
25	283.00	55.5	-56.9	1100	1448	50.5	-39.3	519.4	-494.9	23.1	25.1	66.4
26	293.00	55.1	-55.7	1100	1448	50.1	-38.5	463.9	-438.0	18.5	20.2	71.2
27	303.00	54.7	-54.6	1100	1448	49.8	-37.7	408.7	-382.3	14.4	15.8	76.0
28	313.00	54.3	-53.3	1100	1448	49.4	-36.8	354.0	-327.7	10.8	12.0	80.8
29	323.00	53.9	-52.1	1100	1448	49.0	-36.0	299.7	-274.4	7.8	8.7	85.6
30	333.00	53.4	-50.8	1100	1448	48.6	-35.1	245.8	-222.3	5.3	6.0	90.4
31	343.00	79.3	-73.8	1650	2171	48.1	-34.0	192.4	-171.5	3.3	3.8	95.3
MECH	358.00	113.1	-97.7	2970	3908	38.1	-25.0	113.1	-97.7	1.3	1.5	100.1

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 210 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT 1000-FT-KIPS	Y-MOMENT 1000-FT-KIPS	Z-MOMENT 1000-FT-KIPS
PARK	0.00	54.0	-141.4	2676	7795	20.2	-18.1	2372.9	-3112.0	523.1	377.6	22.9
PARK	14.00	45.4	-100.2	1911	5568	23.8	-18.0	2318.9	-2970.6	480.5	344.8	-6.2
2	24.00	190.4	-218.2	6078	12768	31.3	-17.1	2273.4	-2870.5	451.3	321.8	-24.6
3	43.00	168.7	-146.6	6398	12568	26.4	-11.7	2083.0	-2652.2	398.8	280.4	-41.7
4	63.00	85.7	-79.6	3199	5718	26.8	-13.9	1914.3	-2505.6	347.2	240.4	-41.8
4A	73.00	84.8	-87.9	3199	5169	26.5	-17.0	1828.6	-2426.0	322.6	221.7	-42.3
5	83.00	85.4	-103.4	3199	4443	26.7	-23.3	1743.8	-2338.1	298.8	203.9	-41.9
6	93.00	82.0	-138.6	2754	4176	29.8	-33.2	1658.4	-2234.7	275.9	186.9	-37.5
7	103.00	138.0	-114.2	4715	2962	29.3	-38.5	1576.4	-2096.1	254.2	170.7	-32.6
8	113.00	137.5	-115.6	4581	2670	30.0	-43.3	1438.4	-1982.0	233.8	155.6	-24.6
9	123.00	136.6	-111.6	4403	2513	31.0	-44.4	1300.9	-1866.3	214.6	141.9	-16.6
10	133.00	129.9	-113.1	4225	2379	30.8	-47.5	1164.4	-1754.7	196.5	129.6	-7.7
11	143.00	54.1	-103.2	1443	1621	37.5	-63.7	1034.4	-1641.6	179.5	118.6	1.4
12	153.00	51.3	-93.6	1285	1489	40.0	-62.9	980.3	-1538.4	163.6	108.5	1.4
13	163.00	42.3	-74.8	1100	1448	38.4	-51.7	929.0	-1444.8	148.7	99.0	1.4
14	173.00	43.5	-74.0	1100	1448	39.5	-51.1	886.7	-1370.0	134.6	89.9	1.4
15	183.00	43.5	-73.6	1100	1448	39.6	-50.9	843.2	-1296.0	121.3	81.2	1.4
16	193.00	43.6	-73.3	1100	1448	39.6	-50.6	799.7	-1222.3	108.7	73.0	1.4
17	203.00	43.6	-72.9	1100	1448	39.7	-50.4	756.1	-1149.0	96.8	65.3	1.3
18	213.00	43.9	-72.5	1100	1448	39.9	-50.1	712.5	-1076.1	85.7	57.9	1.3
19	223.00	44.3	-71.8	1100	1448	40.3	-49.6	668.6	-1003.7	75.3	51.0	1.3
20	233.00	44.8	-71.2	1100	1448	40.7	-49.2	624.3	-931.9	65.6	44.5	1.2
21	243.00	45.2	-70.5	1100	1448	41.1	-48.7	579.6	-860.7	56.7	38.5	1.1
22	253.00	45.7	-69.8	1100	1448	41.5	-48.3	534.4	-790.2	48.4	32.9	1.0
23	263.00	45.4	-68.5	1100	1448	41.3	-47.4	488.7	-720.4	40.9	27.8	.9
24	273.00	44.9	-67.0	1100	1448	40.8	-46.3	443.3	-651.8	34.0	23.2	.8
25	283.00	44.3	-65.4	1100	1448	40.3	-45.2	398.4	-584.9	27.8	19.0	.8
26	293.00	43.8	-63.8	1100	1448	39.8	-44.1	354.1	-519.5	22.3	15.2	.7
27	303.00	43.2	-62.3	1100	1448	39.3	-43.0	310.3	-455.7	17.4	11.9	.7
28	313.00	42.2	-61.6	1100	1448	38.4	-42.5	267.1	-393.4	13.2	9.0	.6
29	323.00	41.3	-60.9	1100	1448	37.5	-42.1	224.9	-331.8	9.6	6.5	.6
30	333.00	40.3	-60.2	1100	1448	36.6	-41.6	183.6	-271.0	6.5	4.5	.5
31	343.00	58.6	-88.9	1650	2171	35.5	-41.0	143.3	-210.8	4.1	2.9	.4
MECH	358.00	84.7	-121.8	2970	3908	28.5	-31.2	84.7	-121.8	1.6	1.1	.2

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 220 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT 1000-FT-KIPS	Y-MOMENT 1000-FT-KIPS	Z-MOMENT 1000-FT-KIPS
PARK	0.00	33.7	-85.7	2676	7795	12.6	-11.0	1446.9	-2522.2	453.7	225.1	15.2
PARK	14.00	21.9	-52.7	1911	5568	11.5	-9.5	1413.1	-2436.5	419.0	205.1	-4.9
2	24.00	98.9	-162.2	6078	12768	16.3	-12.7	1391.2	-2383.7	394.9	191.1	-15.8
3	43.00	99.3	-119.2	6398	12568	15.5	-9.5	1292.3	-2221.6	351.1	165.6	-34.5
4	63.00	52.5	-75.5	3199	5718	16.4	-13.2	1193.0	-2102.4	307.9	140.7	-36.2
4A	73.00	52.7	-75.4	3199	5169	16.5	-14.6	1140.5	-2026.9	287.2	129.0	-37.3
5	83.00	53.0	-74.5	3199	4443	16.6	-16.8	1087.7	-1951.5	267.3	117.9	-36.2
6	93.00	50.8	-103.8	2754	4176	18.5	-24.9	1034.8	-1877.0	248.2	107.3	-31.2
7	103.00	85.1	-90.9	4715	2962	18.0	-30.7	983.9	-1773.2	229.9	97.2	-26.6
8	113.00	86.6	-94.0	4581	2670	18.9	-35.2	898.8	-1682.3	212.7	87.8	-20.2
9	123.00	87.6	-89.6	4403	2513	19.9	-35.7	812.3	-1588.3	196.3	79.2	-13.4
10	133.00	82.9	-90.5	4225	2379	19.6	-38.1	724.7	-1498.7	180.9	71.5	-5.7
11	143.00	39.6	-73.5	1443	1621	27.4	-45.3	641.8	-1408.1	166.3	64.7	2.5
12	153.00	39.0	-68.9	1285	1489	30.3	-46.3	602.2	-1334.7	152.6	58.5	2.2
13	163.00	32.7	-56.4	1100	1448	29.7	-39.0	563.2	-1265.8	139.6	52.7	2.2
14	173.00	33.7	-56.0	1100	1448	30.6	-38.7	530.6	-1209.4	127.2	47.2	2.2
15	183.00	33.4	-55.8	1100	1448	30.4	-38.6	496.9	-1153.4	115.4	42.1	3.3
16	193.00	33.2	-55.6	1100	1448	30.2	-38.4	463.4	-1097.5	104.2	37.3	3.3
17	203.00	32.9	-55.4	1100	1448	29.9	-38.3	430.3	-1041.9	93.5	32.8	3.3
18	213.00	32.5	-55.5	1100	1448	29.5	-38.4	397.3	-986.6	83.3	28.7	3.3
19	223.00	31.8	-56.3	1100	1448	28.9	-38.9	364.9	-931.0	73.7	24.8	3.3
20	233.00	31.1	-57.1	1100	1448	28.3	-39.4	333.1	-874.7	64.7	21.4	3.3
21	243.00	30.4	-57.8	1100	1448	27.6	-39.9	302.0	-817.7	56.3	18.2	3.3
22	253.00	29.7	-58.6	1100	1448	27.0	-40.5	271.6	-759.8	48.4	15.3	3.3
23	263.00	28.2	-59.2	1100	1448	25.7	-40.9	241.8	-701.3	41.1	12.7	2.2
24	273.00	26.4	-59.8	1100	1448	24.0	-41.3	213.6	-642.1	34.3	10.5	2.2
25	283.00	24.5	-60.3	1100	1448	22.3	-41.7	187.3	-582.3	28.2	8.5	2.2
26	293.00	22.7	-60.9	1100	1448	20.6	-42.1	162.7	-522.0	22.7	6.7	2.2
27	303.00	20.9	-61.4	1100	1448	19.0	-42.4	140.1	-461.1	17.8	5.2	2.1
28	313.00	20.1	-61.3	1100	1448	18.2	-42.3	119.2	-399.7	13.5	3.9	1.9
29	323.00	19.2	-61.1	1100	1448	17.5	-42.2	99.1	-338.4	9.8	2.8	1.6
30	333.00	18.4	-61.0	1100	1448	16.7	-42.1	79.9	-277.3	6.7	1.9	1.3
31	343.00	26.0	-91.2	1650	2171	15.8	-42.0	61.5	-216.3	4.3	1.2	1.1
MECH	358.00	35.4	-125.2	2970	3908	11.9	-32.0	35.4	-125.2	1.7	.5	.6

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 230 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT 1000-FT-KIPS	Y-MOMENT 1000-FT-KIPS	Z-MOMENT 1000-FT-KIPS
PARK	0.00	10.0	-97.0	2676	7795	3.7	-12.4	516.2	-2851.2	485.3	59.3	16.3
PARK	14.00	3.7	-67.0	1911	5568	2.0	-12.0	506.3	-2754.2	446.0	52.1	1.5
2	24.00	48.8	-196.5	6078	12768	8.0	-15.4	502.5	-2687.2	418.8	47.1	-17.2
3	43.00	43.7	-162.3	6398	12568	6.8	-12.9	453.7	-2490.7	369.6	38.0	-25.0
4	63.00	21.4	-102.5	3199	5718	6.7	-17.9	410.0	-2328.4	321.4	29.4	-25.9
4A	73.00	21.9	-114.1	3199	5169	6.8	-22.1	388.5	-2226.0	298.7	25.4	-28.2
5	83.00	21.7	-108.1	3199	4443	6.8	-24.3	366.6	-2111.9	277.0	21.6	-29.9
6	93.00	20.5	-134.3	2754	4176	7.5	-32.1	344.9	-2003.7	256.4	18.0	-27.0
7	103.00	48.5	-111.5	4715	2962	10.3	-37.6	324.4	-1869.5	237.0	14.7	-24.9
8	113.00	48.9	-107.1	4581	2670	10.7	-40.1	275.9	-1758.0	218.9	11.7	-20.3
9	123.00	50.3	-104.3	4403	2513	11.4	-41.5	226.9	-1650.9	201.9	9.2	-14.4
10	133.00	39.6	-104.2	4225	2379	9.4	-43.8	176.7	-1546.6	185.9	7.1	-7.8
11	143.00	6.5	-71.4	1443	1621	4.5	-44.0	137.1	-1442.4	170.9	5.6	-1.6
12	153.00	12.8	-70.8	1285	1489	10.0	-47.5	130.6	-1371.0	156.9	4.2	-1.2
13	163.00	13.5	-57.9	1100	1448	12.3	-40.0	117.8	-1300.3	143.5	3.0	-1.1
14	173.00	15.5	-57.1	1100	1448	14.1	-39.4	104.2	-1242.3	130.8	1.9	-1.9
15	183.00	15.1	-56.8	1100	1448	13.7	-39.2	88.7	-1185.3	118.6	.9	-1.6
16	193.00	14.7	-56.5	1100	1448	13.3	-39.1	73.6	-1128.5	107.1	.1	-1.5
17	203.00	14.2	-56.3	1100	1448	12.9	-38.9	58.9	-1071.9	96.1	-.5	-1.2
18	213.00	13.3	-56.6	1100	1448	12.1	-39.1	44.7	-1015.6	85.6	-1.1	-1.0
19	223.00	11.8	-58.0	1100	1448	10.7	-40.0	31.4	-959.0	75.8	-1.4	-.7
20	233.00	10.3	-59.3	1100	1448	9.4	-41.0	19.6	-901.0	66.5	-1.7	-.4
21	243.00	8.8	-60.6	1100	1448	8.0	-41.9	9.3	-841.8	57.8	-1.8	-.2
22	253.00	7.2	-61.9	1100	1448	6.6	-42.8	.5	-781.2	49.6	-1.9	-.1
23	263.00	5.8	-62.2	1100	1448	5.3	-43.0	-6.7	-719.2	42.1	-1.9	-.2
24	273.00	4.5	-62.1	1100	1448	4.1	-42.9	-12.6	-657.0	35.3	-1.8	-.3
25	283.00	3.1	-62.0	1100	1448	2.8	-42.8	-17.0	-594.9	29.0	-1.6	-.3
26	293.00	1.8	-61.8	1100	1448	1.6	-42.7	-20.2	-532.9	23.4	-1.4	-.3
27	303.00	.5	-61.7	1100	1448	.4	-42.6	-22.0	-471.1	18.3	-1.2	1.0
28	313.00	-.6	-61.8	1100	1448	-.5	-42.7	-22.4	-409.4	13.9	-1.0	.9
29	323.00	-1.6	-61.8	1100	1448	-1.4	-42.7	-21.9	-347.6	10.2	-.8	.8
30	333.00	-2.6	-61.8	1100	1448	-2.4	-42.7	-20.3	-285.8	7.0	-.6	.6
31	343.00	-5.8	-92.8	1650	2171	-3.5	-42.7	-17.7	-224.0	4.4	-.4	.4
MECH	358.00	-11.8	-131.2	2970	3908	-4.0	-33.6	-11.8	-131.2	1.8	-.2	.2

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 240 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	* HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	-4.7	-120.2	2676	7795	-1.8	-15.4	201.3	-2982.4	506.1	38.1	59.9
PARK	14.00	-6.6	-78.5	1911	5568	-3.4	-14.1	206.0	-2862.2	465.2	35.3	40.1
2	24.00	6.3	-233.6	6078	12768	1.0	-18.3	212.6	-2783.7	436.9	33.2	28.8
3	43.00	-.9	-192.5	6398	12568	-.1	-15.3	206.2	-2550.1	386.3	29.2	-.7
4	63.00	-2.8	-118.9	3199	5718	-.9	-20.8	207.2	-2357.7	337.2	25.1	-11.6
4A	73.00	-3.9	-119.0	3199	5169	-1.2	-23.0	210.0	-2238.7	314.2	23.0	-19.8
5	83.00	-3.8	-101.0	3199	4443	-1.2	-22.7	213.9	-2119.7	292.4	20.9	-25.2
6	93.00	-1.1	-120.7	2754	4176	-.4	-28.9	217.7	-2018.7	271.7	18.7	-24.5
7	103.00	13.9	-97.2	4715	2962	3.0	-32.8	218.8	-1898.0	252.1	16.5	-24.5
8	113.00	15.6	-91.7	4581	2670	3.4	-34.3	204.9	-1800.8	233.6	14.4	-22.5
9	123.00	21.1	-91.3	4403	2513	4.8	-36.3	189.3	-1709.1	216.1	12.4	-18.9
10	133.00	21.0	-92.5	4225	2379	5.0	-38.9	168.2	-1617.8	199.5	10.6	-14.5
11	143.00	6.0	-67.6	1443	1621	4.2	-41.7	147.2	-1525.3	183.7	9.1	-9.8
12	153.00	12.1	-71.3	1285	1489	9.4	-47.9	141.2	-1457.7	168.8	7.6	-9.4
13	163.00	11.3	-61.1	1100	1448	10.3	-42.2	129.1	-1386.4	154.6	6.3	-9.0
14	173.00	13.4	-60.6	1100	1448	12.2	-41.9	117.7	-1325.3	141.0	5.0	-8.4
15	183.00	13.6	-59.7	1100	1448	12.4	-41.2	104.3	-1264.7	128.1	3.9	-7.8
16	193.00	13.8	-58.8	1100	1448	12.6	-40.6	90.7	-1205.0	115.7	3.0	-7.2
17	203.00	14.0	-58.0	1100	1448	12.7	-40.0	76.9	-1146.2	104.0	2.1	-6.6
18	213.00	13.5	-58.1	1100	1448	12.3	-40.2	62.9	-1088.2	92.8	1.4	-6.0
19	223.00	11.8	-59.9	1100	1448	10.8	-41.4	49.4	-1030.1	82.2	.9	-5.4
20	233.00	10.2	-61.6	1100	1448	9.3	-42.6	37.5	-970.2	72.2	.4	-4.9
21	243.00	8.6	-63.4	1100	1448	7.8	-43.8	27.3	-908.5	62.8	.1	-4.5
22	253.00	6.9	-65.2	1100	1448	6.3	-45.0	18.7	-845.1	54.1	-.1	-4.1
23	263.00	5.7	-66.0	1100	1448	5.2	-45.6	11.8	-780.0	45.9	-.3	-3.7
24	273.00	4.6	-66.4	1100	1448	4.2	-45.9	6.1	-714.0	38.5	-.4	-3.4
25	283.00	3.6	-66.8	1100	1448	3.2	-46.1	1.5	-647.6	31.7	-.4	-3.0
26	293.00	2.5	-67.2	1100	1448	2.3	-46.4	-2.1	-580.9	25.5	-.4	-2.6
27	303.00	1.4	-67.5	1100	1448	1.3	-46.6	-4.6	-513.7	20.0	-.4	-2.2
28	313.00	.7	-67.3	1100	1448	.7	-46.5	-6.0	-446.2	15.2	-.3	-1.8
29	323.00	.0	-67.1	1100	1448	.0	-46.3	-6.8	-378.9	11.1	-.3	-1.5
30	333.00	-.7	-66.9	1100	1448	-.6	-46.2	-6.8	-311.8	7.7	-.2	-1.2
31	343.00	-2.4	-99.9	1650	2171	-1.4	-46.0	-6.1	-244.9	4.9	-.1	-.9
MECH	358.00	-3.7	-145.0	2970	3908	-1.3	-37.1	-3.7	-145.0	2.0	-.1	-.6

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 250 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	-.4	-90.8	2676	7795	-.1	-11.6	-65.3	-1848.2	312.4	1.5	37.4
PARK	14.00	-1.4	-63.3	1911	5568	-.8	-11.4	-65.0	-1758.1	287.2	2.4	20.6
2	24.00	-3.4	-126.4	6078	12768	-.6	-9.9	-63.5	-1694.8	269.9	3.1	9.5
3	43.00	-11.5	-131.4	6398	12568	-1.8	-10.5	-60.1	-1568.4	238.9	4.2	-1.8
4	63.00	-8.9	-77.3	3199	5718	-2.8	-13.5	-48.6	-1437.0	208.9	5.3	-9.3
4A	73.00	-11.3	-73.7	3199	5169	-3.5	-14.2	-39.7	-1359.6	194.9	5.8	-14.1
5	83.00	-14.2	-64.5	3199	4443	-4.4	-14.5	-28.4	-1286.0	181.7	6.1	-17.0
6	93.00	-15.7	-76.4	2754	4176	-5.7	-18.3	-14.2	-1221.5	169.1	6.3	-16.5
7	103.00	-7.1	-58.2	4715	2962	-1.5	-19.7	1.5	-1145.1	157.3	6.4	-16.7
8	113.00	-5.5	-53.8	4581	2670	-1.2	-20.1	8.6	-1086.8	146.1	6.3	-16.1
9	123.00	-3.3	-50.5	4403	2513	-.7	-20.1	14.1	-1033.1	135.5	6.2	-14.5
10	133.00	-3.7	-48.7	4225	2379	-.9	-20.5	17.4	-982.5	125.5	6.1	-12.5
11	143.00	-5.0	-31.7	1443	1621	-3.5	-19.5	21.1	-933.8	115.9	5.9	-10.0
12	153.00	-1.9	-36.4	1285	1489	-1.5	-24.5	26.1	-902.2	106.7	5.6	-10.0
13	163.00	-2.6	-35.4	1100	1448	-2.3	-24.5	28.0	-865.7	97.9	5.4	-9.9
14	173.00	-1.6	-36.4	1100	1448	-1.5	-25.2	30.6	-830.3	89.4	5.1	-9.6
15	183.00	-1.2	-36.2	1100	1448	-1.1	-25.0	32.2	-793.9	81.3	4.8	-9.2
16	193.00	-.7	-35.9	1100	1448	-.6	-24.8	33.4	-757.7	73.5	4.4	-8.8
17	203.00	-.2	-35.6	1100	1448	-.2	-24.6	34.1	-721.8	66.1	4.1	-8.4
18	213.00	.1	-35.9	1100	1448	.1	-24.8	34.3	-686.2	59.1	3.7	-8.0
19	223.00	.3	-36.9	1100	1448	.3	-25.5	34.2	-650.3	52.4	3.4	-7.5
20	233.00	.5	-37.9	1100	1448	.5	-26.2	33.8	-613.4	46.1	3.1	-7.0
21	243.00	.7	-39.0	1100	1448	.6	-26.9	33.3	-575.5	40.1	2.7	-6.6
22	253.00	.9	-40.0	1100	1448	.8	-27.6	32.6	-536.5	34.6	2.4	-6.1
23	263.00	1.3	-40.8	1100	1448	1.1	-28.2	31.7	-496.5	29.4	2.1	-5.6
24	273.00	1.7	-41.5	1100	1448	1.6	-28.6	30.5	-455.7	24.6	1.8	-5.1
25	283.00	2.2	-42.1	1100	1448	2.0	-29.1	28.7	-414.2	20.3	1.5	-4.6
26	293.00	2.7	-42.8	1100	1448	2.4	-29.6	26.5	-372.1	16.3	1.2	-4.2
27	303.00	3.1	-43.4	1100	1448	2.8	-30.0	23.9	-329.3	12.8	.9	-3.7
28	313.00	3.1	-43.2	1100	1448	2.8	-29.8	20.8	-285.9	9.8	.7	-3.2
29	323.00	3.1	-43.0	1100	1448	2.8	-29.7	17.7	-242.7	7.1	.5	-2.8
30	333.00	3.1	-42.9	1100	1448	2.8	-29.6	14.6	-199.7	4.9	.4	-2.3
31	343.00	4.7	-64.0	1650	2171	2.8	-29.5	11.5	-156.8	3.1	.2	-1.8
MECH	358.00	6.9	-92.8	2970	3908	2.3	-23.8	6.9	-92.8	1.3	.1	-1.2

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 260 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT 1000-FT-KIPS	Y-MOMENT 1000-FT-KIPS	Z-MOMENT 1000-FT-KIPS
PARK	0.00	-11.3	-110.0	2676	7795	-4.2	-14.1	-511.9	-1910.6	311.2	-88.0	50.4
PARK	14.00	-5.4	-74.4	1911	5568	-2.8	-13.4	-500.6	-1800.6	285.3	-80.9	32.4
2	24.00	-7.3	-165.7	6078	12768	-1.2	-13.0	-495.2	-1726.2	267.6	-76.0	20.9
3	43.00	-27.6	-150.9	6398	12568	-4.3	-12.0	-487.9	-1560.5	236.4	-66.6	5.2
4	63.00	-17.5	-78.0	3199	5718	-5.5	-13.6	-460.3	-1409.6	206.7	-57.1	-3.5
4A	73.00	-20.6	-70.7	3199	5169	-6.5	-13.7	-442.8	-1331.6	193.0	-52.6	-7.7
5	83.00	-23.6	-59.0	3199	4443	-7.4	-13.3	-422.2	-1260.9	180.0	-48.3	-9.8
6	93.00	-24.8	-72.5	2754	4176	-9.0	-17.4	-398.6	-1201.9	167.7	-44.2	-9.2
7	103.00	-23.6	-56.1	4715	2962	-5.0	-18.9	-373.8	-1129.4	156.1	-40.3	-9.4
8	113.00	-26.5	-51.9	4581	2670	-5.8	-19.4	-350.2	-1073.3	145.1	-36.7	-10.3
9	123.00	-26.6	-47.5	4403	2513	-6.1	-18.9	-323.7	-1021.4	134.6	-33.3	-10.3
10	133.00	-26.4	-47.4	4225	2379	-6.2	-19.9	-297.1	-973.9	124.6	-30.2	-9.5
11	143.00	-21.0	-32.1	1443	1621	-14.6	-19.8	-270.7	-926.6	115.1	-27.4	-8.4
12	153.00	-16.7	-37.2	1285	1489	-13.0	-25.0	-249.7	-894.5	106.0	-24.8	-8.9
13	163.00	-15.2	-36.0	1100	1448	-13.9	-24.9	-233.0	-857.2	97.2	-22.4	-9.1
14	173.00	-14.7	-36.9	1100	1448	-13.4	-25.5	-217.7	-821.3	88.8	-20.1	-9.0
15	183.00	-14.3	-36.4	1100	1448	-13.0	-25.2	-203.0	-784.4	80.8	-18.0	-8.8
16	193.00	-13.9	-36.0	1100	1448	-12.7	-24.9	-188.7	-748.0	73.2	-16.1	-8.5
17	203.00	-13.5	-35.6	1100	1448	-12.3	-24.6	-174.7	-711.9	65.9	-14.3	-8.2
18	213.00	-13.0	-35.6	1100	1448	-11.8	-24.6	-161.2	-676.3	58.9	-12.6	-7.9
19	223.00	-12.3	-36.2	1100	1448	-11.2	-25.0	-148.2	-640.7	52.3	-11.0	-7.5
20	233.00	-11.6	-36.9	1100	1448	-10.5	-25.5	-135.9	-604.4	46.1	-9.6	-7.2
21	243.00	-10.8	-37.5	1100	1448	-9.8	-25.9	-124.3	-567.6	40.2	-8.3	-6.8
22	253.00	-10.1	-38.1	1100	1448	-9.2	-26.3	-113.5	-530.1	34.8	-7.1	-6.4
23	263.00	-9.7	-38.9	1100	1448	-8.8	-26.9	-103.4	-492.0	29.9	-6.0	-6.0
24	273.00	-9.4	-39.8	1100	1448	-8.5	-27.5	-93.7	-453.1	24.9	-5.0	-5.6
25	283.00	-9.0	-40.8	1100	1448	-8.2	-28.2	-84.3	-413.2	20.6	-4.2	-5.1
26	293.00	-8.7	-41.7	1100	1448	-7.9	-28.8	-75.3	-372.5	16.7	-3.4	-4.7
27	303.00	-8.5	-42.5	1100	1448	-7.7	-29.4	-66.6	-330.8	13.1	-2.7	-4.2
28	313.00	-8.5	-42.3	1100	1448	-7.7	-29.2	-58.1	-288.3	10.0	-2.0	-3.7
29	323.00	-8.5	-42.1	1100	1448	-7.7	-29.1	-49.6	-246.0	7.4	-1.5	-3.2
30	333.00	-8.5	-42.0	1100	1448	-7.7	-29.0	-41.2	-203.8	5.1	-1.0	-2.7
31	343.00	-12.7	-62.6	1650	2171	-7.7	-28.8	-32.7	-161.8	3.3	-.7	-2.2
MECH	358.00	-20.0	-99.2	2970	3908	-6.7	-25.4	-20.0	-99.2	1.3	-.3	-1.4

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 270 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	-20.1	-102.2	2676	7795	-7.5	-13.1	-1133.3	-2033.9	333.5	-191.7	80.8
PARK	14.00	-20.2	-71.1	1911	5568	-10.6	-12.8	-1113.2	-1931.7	305.7	-176.0	65.3
2	24.00	-74.9	-164.6	6078	12768	-12.3	-12.9	-1093.0	-1860.6	286.8	-165.0	54.5
3	43.00	-74.2	-161.1	6398	12568	-11.6	-12.8	-1018.1	-1695.9	253.0	-144.9	33.8
4	63.00	-40.0	-82.8	3199	5718	-12.5	-14.5	-943.9	-1534.9	220.7	-125.3	19.3
4A	73.00	-43.0	-77.3	3199	5169	-13.4	-15.0	-903.9	-1452.1	205.7	-116.1	12.7
5	83.00	-50.0	-66.8	3199	4443	-15.6	-15.0	-860.9	-1374.8	191.6	-107.2	8.5
6	93.00	-50.5	-75.2	2754	4176	-18.3	-18.0	-810.9	-1308.0	178.2	-98.9	6.6
7	103.00	-53.3	-62.9	4715	2962	-11.3	-21.2	-760.4	-1232.8	165.5	-91.0	2.9
8	113.00	-54.8	-59.9	4581	2670	-12.0	-22.4	-707.1	-1169.9	153.5	-83.7	-1.2
9	123.00	-52.0	-57.2	4403	2513	-11.8	-22.8	-652.3	-1110.0	142.1	-76.9	-4.2
10	133.00	-48.3	-58.5	4225	2379	-11.4	-24.6	-600.3	-1052.8	131.3	-70.6	-6.1
11	143.00	-31.0	-44.0	1443	1621	-21.5	-27.1	-552.0	-994.3	121.0	-64.9	-7.2
12	153.00	-25.5	-45.9	1285	1489	-19.9	-30.9	-521.0	-950.4	111.3	-59.5	-8.0
13	163.00	-22.1	-35.9	1100	1448	-20.0	-24.8	-495.5	-904.4	102.0	-54.4	-8.3
14	173.00	-21.9	-35.9	1100	1448	-19.9	-24.8	-473.4	-868.5	93.2	-49.6	-8.1
15	183.00	-22.1	-37.2	1100	1448	-20.1	-25.7	-451.5	-832.6	84.7	-45.0	-7.8
16	193.00	-22.3	-38.4	1100	1448	-20.2	-26.5	-429.4	-795.5	76.5	-40.6	-7.5
17	203.00	-22.4	-39.7	1100	1448	-20.4	-27.4	-407.2	-757.0	68.8	-36.4	-7.2
18	213.00	-22.5	-40.6	1100	1448	-20.5	-28.0	-384.7	-717.4	61.4	-32.4	-6.8
19	223.00	-22.6	-41.0	1100	1448	-20.5	-28.3	-362.2	-676.8	54.4	-28.7	-6.4
20	233.00	-22.6	-41.4	1100	1448	-20.5	-28.6	-339.6	-635.9	47.8	-25.2	-6.1
21	243.00	-22.6	-41.8	1100	1448	-20.5	-28.8	-317.1	-594.5	41.7	-21.9	-5.7
22	253.00	-22.6	-42.2	1100	1448	-20.5	-29.1	-294.5	-552.8	36.0	-18.8	-5.3
23	263.00	-22.8	-42.4	1100	1448	-20.7	-29.3	-271.9	-510.6	30.6	-16.0	-5.0
24	273.00	-23.1	-42.5	1100	1448	-21.0	-29.4	-249.1	-468.3	25.7	-13.4	-4.6
25	283.00	-23.4	-42.6	1100	1448	-21.2	-29.4	-226.0	-425.8	21.3	-11.0	-4.3
26	293.00	-23.6	-42.8	1100	1448	-21.5	-29.5	-202.7	-383.1	17.2	-8.9	-3.9
27	303.00	-23.9	-42.9	1100	1448	-21.7	-29.6	-179.0	-340.4	13.6	-7.0	-3.5
28	313.00	-23.7	-43.0	1100	1448	-21.5	-29.7	-155.2	-297.5	10.4	-5.3	-3.1
29	323.00	-23.5	-43.1	1100	1448	-21.3	-29.8	-131.5	-254.5	7.7	-3.9	-2.7
30	333.00	-23.2	-43.2	1100	1448	-21.1	-29.8	-108.1	-211.5	5.3	-2.7	-2.3
31	343.00	-34.5	-64.9	1650	2171	-20.9	-29.9	-84.8	-168.3	3.4	-1.7	-1.9
MECH	358.00	-50.4	-103.4	2970	3908	-17.0	-26.5	-50.4	-103.4	1.4	-.7	-1.3

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 280 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	-29.8	-80.2	2676	7795	-11.1	-10.3	-1546.7	-1892.5	325.8	-264.4	89.4
PARK	14.00	-28.5	-51.5	1911	5568	-14.9	-9.2	-1516.9	-1812.3	299.9	-242.9	77.5
2	24.00	-100.5	-128.8	6078	12768	-16.5	-10.1	-1488.4	-1760.8	282.0	-227.9	69.7
3	43.00	-101.1	-128.8	6398	12568	-15.8	-10.2	-1388.0	-1631.9	249.8	-200.6	51.2
4	63.00	-55.3	-68.9	3199	5718	-17.3	-12.0	-1286.9	-1503.2	218.4	-173.8	36.5
4A	73.00	-59.3	-68.4	3199	5169	-18.5	-13.2	-1231.5	-1434.3	203.7	-161.2	29.5
5	83.00	-66.7	-63.8	3199	4443	-20.9	-14.4	-1172.3	-1365.9	189.7	-149.2	24.2
6	93.00	-64.7	-69.3	2754	4176	-23.5	-16.6	-1105.6	-1302.1	176.4	-137.8	20.1
7	103.00	-71.2	-63.3	4715	2962	-15.1	-21.4	-1040.9	-1232.8	163.7	-127.1	14.1
8	113.00	-73.1	-60.6	4581	2670	-16.0	-22.7	-969.7	-1169.5	151.7	-117.1	8.1
9	123.00	-70.3	-59.5	4403	2513	-16.0	-23.7	-896.6	-1108.9	140.3	-107.7	3.3
10	133.00	-66.5	-61.8	4225	2379	-15.7	-26.0	-826.3	-1049.4	129.5	-99.1	-1.3
11	143.00	-39.7	-45.4	1443	1621	-27.5	-28.0	-759.8	-987.6	119.3	-91.2	-2.9
12	153.00	-33.3	-46.1	1285	1489	-25.9	-31.0	-720.1	-942.2	109.7	-83.8	-4.1
13	163.00	-28.4	-39.6	1100	1448	-25.8	-27.4	-686.8	-896.0	100.5	-76.7	-4.7
14	173.00	-28.7	-39.5	1100	1448	-26.1	-27.3	-658.3	-856.4	91.7	-70.0	-4.6
15	183.00	-29.3	-39.3	1100	1448	-26.6	-27.1	-629.6	-816.9	83.4	-63.6	-4.4
16	193.00	-29.8	-39.1	1100	1448	-27.1	-27.0	-600.3	-777.6	75.4	-57.4	-4.2
17	203.00	-30.3	-38.8	1100	1448	-27.6	-26.8	-570.5	-738.5	67.8	-51.6	-4.0
18	213.00	-30.7	-38.8	1100	1448	-27.9	-26.8	-540.2	-699.7	60.6	-46.0	-3.9
19	223.00	-31.0	-39.0	1100	1448	-28.2	-27.0	-509.5	-661.0	53.8	-40.8	-3.7
20	233.00	-31.3	-39.3	1100	1448	-28.4	-27.1	-478.5	-621.9	47.4	-35.8	-3.5
21	243.00	-31.5	-39.6	1100	1448	-28.7	-27.3	-447.2	-582.6	41.4	-31.2	-3.3
22	253.00	-31.8	-39.8	1100	1448	-28.9	-27.5	-415.7	-543.1	35.7	-26.9	-3.1
23	263.00	-31.9	-40.2	1100	1448	-29.0	-27.8	-383.9	-503.2	30.5	-22.9	-2.9
24	273.00	-32.0	-40.6	1100	1448	-29.1	-28.1	-351.9	-463.0	25.7	-19.2	-2.8
25	283.00	-32.1	-41.0	1100	1448	-29.2	-28.3	-319.9	-422.4	21.3	-15.9	-2.6
26	293.00	-32.2	-41.4	1100	1448	-29.2	-28.6	-287.8	-381.4	17.2	-12.8	-2.4
27	303.00	-32.3	-41.9	1100	1448	-29.3	-28.9	-255.7	-340.0	13.6	-10.1	-2.2
28	313.00	-32.6	-42.5	1100	1448	-29.7	-29.3	-223.4	-298.1	10.4	-7.7	-1.9
29	323.00	-33.0	-43.0	1100	1448	-30.0	-29.7	-190.8	-255.6	7.7	-5.6	-1.7
30	333.00	-33.4	-43.6	1100	1448	-30.4	-30.1	-157.7	-212.6	5.3	-3.9	-1.5
31	343.00	-50.8	-66.5	1650	2171	-30.8	-30.6	-124.4	-168.9	3.4	-2.5	-1.2
MECH	358.00	-73.6	-102.4	2970	3908	-24.8	-26.2	-73.6	-102.4	1.4	-1.0	-0.8

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 290 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	-36.7	-59.7	2676	7795	-13.7	-7.7	-1814.0	-1585.7	280.3	-326.5	98.6
PARK	14.00	-24.9	-37.1	1911	5568	-13.0	-6.7	-1777.3	-1526.0	258.5	-301.3	89.1
2	24.00	-80.8	-101.5	6078	12768	-13.3	-8.0	-1752.4	-1489.0	243.4	-283.7	83.9
3	43.00	-109.8	-96.1	6398	12568	-17.2	-7.7	-1671.5	-1387.5	216.1	-251.2	66.9
4	63.00	-64.3	-52.3	3199	5718	-20.1	-9.2	-1561.7	-1291.3	189.3	-218.8	51.5
4A	73.00	-70.7	-52.5	3199	5169	-22.1	-10.2	-1497.4	-1239.0	176.7	-203.5	43.7
5	83.00	-78.2	-50.8	3199	4443	-24.4	-11.4	-1426.8	-1186.5	164.5	-188.9	37.2
6	93.00	-74.2	-54.4	2754	4176	-27.0	-13.0	-1348.6	-1135.7	152.9	-175.0	31.4
7	103.00	-79.7	-53.6	4715	2962	-16.9	-18.1	-1274.4	-1081.3	141.9	-161.9	23.4
8	113.00	-81.3	-50.6	4581	2670	-17.8	-18.9	-1194.7	-1027.7	131.3	-149.6	16.0
9	123.00	-79.6	-51.6	4403	2513	-18.1	-20.5	-1113.4	-977.1	121.3	-138.0	9.7
10	133.00	-76.6	-55.7	4225	2379	-18.1	-23.4	-1033.8	-925.4	111.8	-127.3	4.5
11	143.00	-43.7	-44.5	1443	1621	-30.3	-27.4	-957.2	-869.8	102.8	-117.3	.3
12	153.00	-38.4	-44.9	1285	1489	-29.9	-30.1	-913.5	-825.3	94.3	-108.0	-1.3
13	163.00	-32.5	-35.7	1100	1448	-29.6	-24.7	-875.1	-780.4	86.3	-99.1	-1.7
14	173.00	-33.6	-35.3	1100	1448	-30.6	-24.4	-842.6	-744.7	78.7	-90.5	-1.5
15	183.00	-34.8	-35.6	1100	1448	-31.6	-24.6	-809.0	-709.4	71.4	-82.2	-1.5
16	193.00	-36.0	-35.9	1100	1448	-32.7	-24.8	-774.2	-673.9	64.5	-74.3	-1.4
17	203.00	-37.2	-36.2	1100	1448	-33.8	-25.0	-738.2	-638.0	57.9	-66.7	-1.3
18	213.00	-38.2	-36.1	1100	1448	-34.8	-25.0	-701.0	-601.8	51.7	-59.5	-1.2
19	223.00	-39.1	-35.6	1100	1448	-35.5	-24.6	-662.7	-565.7	45.9	-52.7	-1.1
20	233.00	-39.9	-35.0	1100	1448	-36.2	-24.2	-623.7	-530.1	40.4	-46.3	-1.0
21	243.00	-40.7	-34.4	1100	1448	-37.0	-23.8	-583.8	-495.1	35.3	-40.2	-.
22	253.00	-41.5	-33.8	1100	1448	-37.7	-23.4	-543.1	-460.7	30.5	-34.6	-.
23	263.00	-42.1	-33.8	1100	1448	-38.3	-23.4	-501.6	-426.8	26.1	-29.4	-.
24	273.00	-42.7	-34.1	1100	1448	-38.8	-23.5	-459.5	-393.0	22.0	-24.6	-.
25	283.00	-43.3	-34.3	1100	1448	-39.3	-23.7	-416.8	-358.9	18.2	-20.2	-.
26	293.00	-43.8	-34.5	1100	1448	-39.8	-23.9	-373.5	-324.6	14.8	-16.2	-.
27	303.00	-44.3	-34.8	1100	1448	-40.3	-24.1	-329.7	-290.1	11.7	-12.7	-.
28	313.00	-43.9	-35.7	1100	1448	-39.9	-24.6	-285.4	-255.3	9.0	-9.7	-.
29	323.00	-43.6	-36.5	1100	1448	-39.6	-25.2	-241.5	-219.6	6.6	-7.0	-.
30	333.00	-43.2	-37.3	1100	1448	-39.3	-25.8	-197.9	-183.1	4.6	-4.8	-.
31	343.00	-64.1	-57.5	1650	2171	-38.8	-26.5	-154.7	-145.8	2.9	-3.1	-.
MECH	358.00	-90.6	-88.3	2970	3908	-30.5	-22.6	-90.6	-88.3	1.2	-1.2	-.

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 300 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	-39.4	-38.6	2676	7795	-14.7	-5.0	-1911.4	-998.4	179.5	-348.8	99.9
PARK	14.00	-25.1	-22.3	1911	5568	-13.1	-4.0	-1872.0	-959.8	165.8	-322.4	92.7
2	24.00	-77.7	-59.8	6078	12768	-12.8	-4.7	-1846.9	-937.5	156.3	-303.8	88.7
3	43.00	-111.5	-49.5	6398	12568	-17.4	-3.9	-1769.3	-877.7	139.1	-269.4	73.5
4	63.00	-64.8	-29.0	3199	5718	-20.3	-5.1	-1657.7	-828.1	122.0	-235.1	59.9
4A	73.00	-71.0	-27.5	3199	5169	-22.2	-5.3	-1592.9	-799.1	113.9	-218.9	52.6
5	83.00	-78.3	-27.1	3199	4443	-24.5	-6.1	-1522.0	-771.7	106.4	-203.3	46.2
6	93.00	-74.7	-29.9	2754	4176	-27.1	-7.2	-1443.7	-744.6	98.4	-188.5	39.6
7	103.00	-85.3	-36.3	4715	2962	-18.1	-12.2	-1369.0	-714.7	91.1	-174.4	31.2
8	113.00	-87.2	-33.3	4581	2670	-19.0	-12.5	-1283.7	-678.4	84.2	-161.2	23.3
9	123.00	-86.6	-35.2	4403	2513	-19.7	-14.0	-1196.5	-645.1	77.3	-148.2	16.4
10	133.00	-85.5	-37.7	4225	2379	-20.2	-15.8	-1109.9	-609.9	71.3	-137.2	10.4
11	143.00	-43.9	-31.6	1443	1621	-30.4	-19.5	-1024.5	-572.2	65.4	-126.5	4.2
12	153.00	-39.2	-32.0	1285	1489	-30.5	-21.5	-980.6	-540.6	59.8	-116.9	3.0
13	163.00	-35.0	-28.9	1100	1448	-31.8	-20.0	-941.3	-508.6	54.5	-106.9	2.4
14	173.00	-36.1	-28.3	1100	1448	-32.8	-19.5	-906.4	-479.6	49.6	-97.8	2.4
15	183.00	-37.3	-26.7	1100	1448	-33.9	-18.4	-870.3	-451.4	45.0	-88.8	2.4
16	193.00	-38.4	-25.1	1100	1448	-34.9	-17.3	-833.0	-424.7	40.6	-80.3	2.4
17	203.00	-39.6	-23.5	1100	1448	-36.0	-16.2	-794.5	-399.6	36.5	-72.4	2.4
18	213.00	-40.7	-22.4	1100	1448	-37.0	-15.5	-754.9	-376.2	32.6	-64.4	2.2
19	223.00	-41.6	-22.0	1100	1448	-37.8	-15.2	-714.3	-353.8	28.9	-57.0	2.2
20	233.00	-42.6	-21.7	1100	1448	-38.7	-15.0	-672.6	-331.8	25.5	-50.1	2.2
21	243.00	-43.5	-21.3	1100	1448	-39.6	-14.7	-630.1	-310.1	22.3	-43.6	2.2
22	253.00	-44.5	-21.0	1100	1448	-40.4	-14.5	-586.5	-288.8	19.3	-37.5	1.8
23	263.00	-45.2	-21.0	1100	1448	-41.1	-14.5	-542.0	-267.8	16.5	-31.9	1.6
24	273.00	-45.8	-21.1	1100	1448	-41.7	-14.6	-496.8	-246.8	13.9	-26.7	1.4
25	283.00	-46.4	-21.3	1100	1448	-42.2	-14.7	-451.0	-225.7	11.6	-21.9	1.2
26	293.00	-47.0	-21.4	1100	1448	-42.8	-14.8	-404.6	-204.4	9.4	-17.5	1.1
27	303.00	-47.6	-21.6	1100	1448	-43.3	-14.9	-357.5	-183.0	7.5	-13.8	.8
28	313.00	-47.4	-22.1	1100	1448	-43.0	-15.3	-310.6	-161.4	5.8	-10.5	.6
29	323.00	-47.1	-22.6	1100	1448	-42.8	-15.6	-262.6	-139.3	4.3	-7.6	.4
30	333.00	-46.9	-23.0	1100	1448	-42.6	-15.9	-215.5	-116.7	3.0	-5.3	.3
31	343.00	-69.9	-35.5	1650	2171	-42.4	-16.3	-168.6	-93.7	1.9	-3.3	.2
MECH	358.00	-98.6	-58.3	2970	3908	-33.2	-14.9	-98.6	-58.3	.8	-1.3	.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 310 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	-37.2	-31.8	2676	7795	-13.9	-4.1	-1970.2	-483.2	74.3	-357.1	101.9
PARK	14.00	-30.6	-17.7	1911	5568	-16.0	-3.2	-1932.9	-451.5	67.8	-329.7	95.5
2	24.00	-103.7	-44.3	6078	12768	-17.1	-3.5	-1902.3	-433.8	63.3	-310.6	91.7
3	43.00	-116.2	-27.7	6398	12568	-18.2	-2.2	-1798.6	-389.5	55.5	-275.4	73.3
4	63.00	-64.5	-16.1	3199	5718	-20.2	-2.8	-1682.5	-361.8	48.0	-240.6	60.0
4A	73.00	-69.6	-14.1	3199	5169	-21.7	-2.7	-1618.0	-345.7	44.5	-224.1	53.5
5	83.00	-77.4	-11.1	3199	4443	-24.2	-2.5	-1548.5	-331.6	41.1	-208.3	47.8
6	93.00	-72.2	-10.5	2754	4176	-26.2	-2.5	-1471.0	-320.5	37.8	-193.2	41.3
7	103.00	-88.0	-22.1	4715	2962	-18.7	-7.5	-1398.9	-310.0	34.7	-178.8	32.9
8	113.00	-88.4	-18.1	4581	2670	-19.3	-6.8	-1310.9	-287.9	31.7	-165.3	25.4
9	123.00	-87.5	-18.3	4403	2513	-19.9	-7.3	-1222.4	-269.7	28.9	-152.6	18.8
10	133.00	-87.0	-18.1	4225	2379	-20.6	-7.6	-1134.9	-251.4	26.3	-140.8	12.7
11	143.00	-42.9	-15.4	1443	1621	-29.8	-9.5	-1047.9	-233.3	23.9	-129.9	6.9
12	153.00	-39.3	-16.5	1285	1489	-30.6	-11.1	-1004.9	-217.9	21.6	-119.6	5.2
13	163.00	-34.9	-14.3	1100	1448	-31.7	-9.9	-965.6	-201.4	19.5	-109.8	5.1
14	173.00	-36.2	-14.0	1100	1448	-32.9	-9.7	-930.7	-187.1	17.6	-100.3	5.0
15	183.00	-37.8	-13.2	1100	1448	-34.4	-9.1	-894.5	-173.1	15.8	-91.2	4.9
16	193.00	-39.4	-12.4	1100	1448	-35.8	-8.6	-856.7	-159.8	14.1	-82.4	4.8
17	203.00	-40.9	-11.6	1100	1448	-37.2	-8.0	-817.3	-147.4	12.6	-74.0	4.6
18	213.00	-42.2	-11.0	1100	1448	-38.4	-7.6	-776.4	-135.8	11.1	-66.1	4.4
19	223.00	-43.1	-10.6	1100	1448	-39.1	-7.3	-734.2	-124.8	9.8	-58.5	4.2
20	233.00	-43.9	-10.3	1100	1448	-39.9	-7.1	-691.2	-114.2	8.6	-51.4	4.0
21	243.00	-44.8	-9.9	1100	1448	-40.7	-6.8	-647.2	-103.9	7.6	-44.7	3.7
22	253.00	-45.6	-9.5	1100	1448	-41.5	-6.6	-602.5	-94.0	6.6	-38.5	3.5
23	263.00	-46.4	-8.5	1100	1448	-42.2	-5.9	-556.8	-84.5	5.7	-32.7	3.2
24	273.00	-47.2	-7.2	1100	1448	-42.9	-5.0	-510.4	-76.0	4.9	-27.3	3.0
25	283.00	-47.9	-5.9	1100	1448	-43.6	-4.1	-463.3	-68.8	4.1	-22.5	2.8
26	293.00	-48.7	-4.6	1100	1448	-44.3	-3.2	-415.3	-62.9	3.5	-18.1	2.6
27	303.00	-49.3	-3.5	1100	1448	-44.8	-2.4	-366.6	-58.3	2.9	-14.2	2.4
28	313.00	-48.9	-4.4	1100	1448	-44.5	-3.0	-317.3	-54.8	2.3	-10.7	2.1
29	323.00	-48.5	-5.2	1100	1448	-44.1	-3.6	-268.4	-50.4	1.8	-7.8	1.8
30	333.00	-48.1	-6.1	1100	1448	-43.7	-4.2	-219.9	-45.2	1.3	-5.4	1.4
31	343.00	-71.3	-10.8	1650	2171	-43.2	-5.0	-171.9	-39.1	.9	-3.4	.7
MECH	358.00	-100.6	-28.3	2970	3908	-33.9	-7.2	-100.6	-28.3	.4	-1.4	

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 320 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	-38.5	-32.3	2676	7795	-14.4	-4.1	-2028.9	-169.9	21.9	-362.2	111.7
PARK	14.00	-31.4	-21.1	1911	5568	-16.4	-3.8	-1990.4	-137.6	19.8	-334.1	104.8
2	24.00	-110.6	-23.1	6078	12768	-18.2	-1.8	-1959.0	-116.5	18.5	-314.4	100.1
3	43.00	-125.6	-10.9	6398	12568	-19.6	-.9	-1848.4	-93.4	16.5	-278.2	81.4
4	63.00	-70.2	-7.7	3199	5718	-21.9	-1.3	-1722.8	-82.5	14.7	-242.5	66.9
4A	73.00	-76.7	-7.4	3199	5169	-24.0	-1.4	-1652.6	-74.9	14.0	-225.6	60.0
5	83.00	-85.7	-.4	3199	4443	-26.8	-.1	-1575.9	-67.5	13.2	-209.5	53.5
6	93.00	-78.1	7.7	2754	4176	-28.4	1.9	-1490.2	-67.1	12.6	-194.1	45.5
7	103.00	-99.6	-9.8	4715	2962	-21.1	-3.3	-1412.1	-74.8	11.9	-179.6	35.5
8	113.00	-97.5	-5.1	4581	2670	-21.3	-1.9	-1312.5	-65.1	11.2	-166.0	26.6
9	123.00	-94.6	-1.2	4403	2513	-21.5	-.5	-1215.0	-60.0	10.5	-153.7	18.8
10	133.00	-93.0	3.7	4225	2379	-22.0	1.6	-1120.4	-58.8	9.9	-141.7	11.4
11	143.00	-39.8	3.3	1443	1621	-27.6	2.0	-1027.4	-62.5	9.3	-130.9	4.4
12	153.00	-36.6	-.1	1285	1489	-28.5	-.1	-987.6	-65.8	8.7	-120.9	3.7
13	163.00	-33.9	-1.8	1100	1448	-30.8	-1.2	-951.0	-65.7	8.0	-111.2	3.2
14	173.00	-34.7	-2.5	1100	1448	-31.6	-1.7	-917.1	-63.9	7.4	-101.2	3.1
15	183.00	-35.5	-2.4	1100	1448	-32.3	-1.7	-882.3	-61.5	6.8	-92.8	3.1
16	193.00	-36.2	-2.3	1100	1448	-32.9	-1.6	-846.8	-59.1	6.2	-84.8	3.1
17	203.00	-37.0	-2.3	1100	1448	-33.6	-1.6	-810.6	-56.7	5.6	-75.9	3.0
18	213.00	-37.9	-2.3	1100	1448	-34.5	-1.6	-773.7	-54.5	5.0	-68.0	2.9
19	223.00	-39.2	-2.6	1100	1448	-35.6	-1.8	-735.8	-52.2	4.5	-60.4	2.9
20	233.00	-40.4	-2.9	1100	1448	-36.7	-2.0	-696.6	-49.6	4.0	-53.5	2.9
21	243.00	-41.7	-3.2	1100	1448	-37.9	-2.2	-656.2	-46.7	3.5	-46.3	2.9
22	253.00	-42.9	-3.5	1100	1448	-39.0	-2.4	-614.5	-43.5	3.1	-40.1	2.8
23	263.00	-44.3	-3.4	1100	1448	-40.3	-2.3	-571.6	-40.7	2.6	-34.2	2.6
24	273.00	-45.8	-3.1	1100	1448	-41.6	-2.1	-527.2	-36.7	2.3	-28.7	2.4
25	283.00	-47.3	-2.8	1100	1448	-43.0	-1.9	-481.5	-33.6	1.9	-23.7	2.3
26	293.00	-48.7	-2.6	1100	1448	-44.3	-1.8	-434.2	-30.8	1.6	-19.0	2.2
27	303.00	-50.1	-2.3	1100	1448	-45.5	-1.6	-385.5	-28.2	1.3	-15.4	1.9
28	313.00	-50.4	-2.7	1100	1448	-45.8	-1.8	-335.4	-25.9	1.0	-11.4	1.6
29	323.00	-50.7	-3.0	1100	1448	-46.1	-2.0	-285.1	-23.2	.8	-8.3	1.4
30	333.00	-51.0	-3.3	1100	1448	-46.3	-2.3	-234.4	-20.2	.6	-5.7	1.2
31	343.00	-77.0	-5.5	1650	2171	-46.7	-2.5	-183.4	-17.0	.4	-3.6	.9
MECH	358.00	-106.4	-11.5	2970	3908	-35.8	-2.9	-106.4	-11.5	.2	-1.4	.5

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 330 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	-40.9	-31.8	2676	7795	-15.3	-4.1	-2018.1	-80.2	13.3	-370.7	98.8
PARK	14.00	-24.9	-21.6	1911	5568	-13.0	-3.9	-1977.2	-48.4	12.4	-342.8	92.1
2	24.00	-77.1	-12.9	6078	12768	-12.7	-1.0	-1952.3	-26.7	12.0	-323.1	88.0
3	43.00	-115.4	-.6	6398	12568	-18.0	-.0	-1875.3	-13.8	11.6	-286.8	72.7
4	63.00	-66.9	-2.5	3199	5718	-20.9	-.4	-1759.9	-13.3	11.3	-250.4	59.3
4A	73.00	-74.5	-2.2	3199	5169	-23.3	-.4	-1693.0	-10.8	11.2	-233.1	52.8
5	83.00	-84.1	3.6	3199	4443	-26.3	.8	-1618.5	-8.6	11.1	-216.6	46.4
6	93.00	-77.0	12.8	2754	4176	-27.9	3.1	-1534.3	-12.2	11.0	-200.8	38.2
7	103.00	-101.5	-5.5	4715	2962	-21.5	-1.9	-1457.4	-25.0	10.8	-185.9	27.3
8	113.00	-99.2	.9	4581	2670	-21.6	.3	-1355.9	-19.5	10.6	-171.8	18.3
9	123.00	-96.1	6.1	4403	2513	-21.8	2.4	-1256.7	-20.4	10.4	-158.7	10.3
10	133.00	-94.8	12.6	4225	2379	-22.4	5.3	-1160.6	-26.4	10.2	-146.6	3.0
11	143.00	-41.6	12.0	1443	1621	-28.8	7.4	-1065.8	-39.0	9.8	-133.5	-4.7
12	153.00	-38.1	10.2	1285	1489	-29.7	6.8	-1024.3	-51.0	9.4	-125.1	-4.7
13	163.00	-35.2	3.8	1100	1448	-32.0	2.6	-986.2	-61.2	8.8	-115.0	-4.8
14	173.00	-35.9	1.6	1100	1448	-32.7	1.1	-951.0	-65.0	8.2	-105.3	-4.8
15	183.00	-36.6	.7	1100	1448	-33.3	.5	-915.1	-66.6	7.5	-96.0	-4.5
16	193.00	-37.3	-.3	1100	1448	-33.9	-.2	-878.4	-67.3	6.9	-87.0	-4.3
17	203.00	-38.0	-1.2	1100	1448	-34.6	-.8	-841.1	-67.0	6.2	-78.4	-4.0
18	213.00	-39.1	-2.1	1100	1448	-35.6	-1.5	-803.1	-65.8	5.5	-70.2	-3.7
19	223.00	-40.9	-2.9	1100	1448	-37.2	-2.0	-763.9	-63.6	4.9	-62.4	-3.4
20	233.00	-42.6	-3.7	1100	1448	-38.7	-2.6	-723.1	-60.7	4.3	-54.9	-3.1
21	243.00	-44.3	-4.5	1100	1448	-40.3	-3.1	-680.5	-57.1	3.7	-47.9	-2.8
22	253.00	-46.1	-5.3	1100	1448	-41.9	-3.7	-636.1	-52.6	3.1	-41.3	-2.6
23	263.00	-47.3	-5.3	1100	1448	-43.0	-3.7	-590.1	-47.3	2.6	-35.2	-2.2
24	273.00	-48.2	-5.0	1100	1448	-43.8	-3.4	-542.8	-42.0	2.2	-29.5	-1.9
25	283.00	-49.2	-4.6	1100	1448	-44.7	-3.2	-494.6	-37.0	1.8	-24.4	-1.6
26	293.00	-50.1	-4.3	1100	1448	-45.6	-3.0	-445.4	-32.4	1.4	-19.7	-1.3
27	303.00	-51.0	-4.0	1100	1448	-46.4	-2.7	-395.3	-28.1	1.1	-15.5	-1.0
28	313.00	-51.3	-3.7	1100	1448	-46.7	-2.6	-344.3	-24.2	.9	-11.8	-.8
29	323.00	-51.7	-3.4	1100	1448	-47.0	-2.4	-293.0	-20.5	.6	-8.6	-.6
30	333.00	-52.0	-3.2	1100	1448	-47.3	-2.2	-241.3	-17.0	.5	-5.9	-.4
31	343.00	-78.6	-4.3	1650	2171	-47.6	-2.0	-189.3	-13.8	.3	-3.7	-.2
MECH	358.00	-110.7	-9.5	2970	3908	-37.3	-2.4	-110.7	-9.5	.1	-1.5	-.6

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 340 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	-40.4	-25.2	2676	7795	-15.1	-3.2	-2063.5	52.1	1.2	-371.1	87.2
PARK	14.00	-32.0	-15.8	1911	5568	-16.8	-2.8	-2023.1	77.4	2.1	-342.5	82.7
2	24.00	-104.2	3.1	6078	12768	-17.2	.2	-1991.1	93.1	2.9	-322.4	79.7
3	43.00	-122.3	8.9	6398	12568	-19.1	.7	-1886.8	90.0	4.7	-285.6	62.4
4	63.00	-69.7	2.5	3199	5718	-21.8	.4	-1764.6	81.1	6.4	-249.1	49.0
4A	73.00	-76.4	1.7	3199	5169	-23.9	.3	-1694.9	78.6	7.2	-231.8	43.8
5	83.00	-86.0	8.8	3199	4443	-26.9	2.0	-1618.4	76.9	8.0	-215.2	37.8
6	93.00	-77.0	25.7	2754	4176	-28.0	6.2	-1532.4	68.1	8.7	-199.5	30.5
7	103.00	-100.9	6.3	4715	2962	-21.4	2.1	-1455.4	42.4	9.3	-184.5	20.6
8	113.00	-98.1	12.7	4581	2670	-21.4	4.8	-1354.5	36.1	9.6	-170.5	12.6
9	123.00	-96.4	16.1	4403	2513	-21.9	6.4	-1256.4	23.4	9.9	-157.4	4.6
10	133.00	-94.9	20.7	4225	2379	-22.5	8.7	-1160.0	7.3	10.1	-145.3	-2.3
11	143.00	-42.5	16.1	1443	1621	-29.5	9.9	-1065.1	-13.4	10.1	-134.2	-8.9
12	153.00	-38.9	13.9	1285	1489	-30.3	9.3	-1022.6	-29.5	9.9	-123.8	-9.2
13	163.00	-35.7	7.1	1100	1448	-32.5	4.9	-983.6	-43.4	9.5	-113.7	-9.9
14	173.00	-36.5	5.2	1100	1448	-33.2	3.6	-947.9	-50.5	9.0	-104.1	-8.9
15	183.00	-37.5	4.3	1100	1448	-34.1	3.0	-911.4	-55.7	8.5	-94.8	-8.6
16	193.00	-38.4	3.5	1100	1448	-34.9	2.4	-873.9	-60.0	7.9	-85.9	-8.8
17	203.00	-39.4	2.6	1100	1448	-35.8	1.8	-835.5	-63.5	7.3	-77.3	-8.7
18	213.00	-40.5	1.5	1100	1448	-36.8	1.0	-796.1	-66.1	6.6	-69.2	-7.7
19	223.00	-41.9	-.0	1100	1448	-38.1	-.0	-755.6	-67.6	6.0	-61.4	-7.4
20	233.00	-43.2	-1.6	1100	1448	-39.3	-1.1	-713.7	-67.5	5.3	-54.1	-6.5
21	243.00	-44.5	-3.1	1100	1448	-40.5	-2.1	-670.5	-66.0	4.6	-47.1	-6.1
22	253.00	-45.9	-4.6	1100	1448	-41.7	-3.2	-626.0	-62.9	4.0	-40.6	-5.7
23	263.00	-46.8	-5.1	1100	1448	-42.6	-3.5	-580.1	-58.3	3.4	-34.6	-5.2
24	273.00	-47.6	-5.1	1100	1448	-43.3	-3.6	-533.2	-53.2	2.8	-29.1	-4.8
25	283.00	-48.4	-5.2	1100	1448	-44.0	-3.6	-485.6	-48.0	2.3	-24.0	-4.4
26	293.00	-49.2	-5.2	1100	1448	-44.8	-3.6	-437.2	-42.8	1.9	-19.3	-3.9
27	303.00	-50.0	-5.3	1100	1448	-45.4	-3.6	-387.9	-37.6	1.5	-15.2	-3.5
28	313.00	-50.2	-5.1	1100	1448	-45.6	-3.5	-337.9	-32.3	1.1	-11.6	-3.0
29	323.00	-50.4	-4.9	1100	1448	-45.8	-3.4	-287.7	-27.3	.8	-8.5	-2.6
30	333.00	-50.6	-4.7	1100	1448	-46.0	-3.2	-237.3	-22.4	.6	-5.8	-2.2
31	343.00	-76.4	-6.6	1650	2171	-46.3	-3.1	-186.7	-17.7	.4	-3.7	-1.8
MECH	358.00	-110.3	-11.1	2970	3908	-37.1	-2.8	-110.3	-11.1	.1	-1.5	-1.2

TABLE 7. SHEAR AND MOMENT DIAGRAMS : HARRAH'S HOLIDAY INN, ATLANTIC CITY
WIND DIRECTION 350 CONFIGURATION A REFERENCE PRESSURE 48.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT FT	X-FORCE KIPS	Y-FORCE KIPS	X-AREA SQ FT	Y-AREA SQ FT	X-PRESS PSF	Y-PRESS PSF	X-SHEAR KIPS	Y-SHEAR KIPS	X-MOMENT	Y-MOMENT 1000-FT-KIPS	Z-MOMENT
PARK	0.00	-43.1	-9.0	2676	7795	-16.1	-1.2	-1933.1	317.6	-42.3	-343.8	65.4
PARK	14.00	-30.0	-1.8	1911	5568	-15.7	-.3	-1890.0	326.6	-37.8	-317.1	64.6
2	24.00	-88.9	26.5	6078	12768	-14.6	2.1	-1859.9	328.4	-34.5	-298.3	65.0
3	43.00	-118.8	24.7	6398	12568	-18.6	2.0	-1771.0	301.8	-28.5	-263.8	52.7
4	63.00	-70.8	14.9	3199	5718	-22.1	2.6	-1652.2	277.1	-22.7	-229.6	40.7
4A	73.00	-78.4	15.4	3199	5169	-24.5	3.0	-1581.4	262.2	-20.0	-213.4	36.2
5	83.00	-86.3	22.5	3199	4443	-27.0	5.1	-1503.0	246.7	-17.5	-198.0	32.0
6	93.00	-75.2	39.7	2754	4176	-27.3	9.5	-1416.7	224.3	-15.1	-183.4	25.7
7	103.00	-96.5	17.4	4715	2962	-20.5	5.9	-1341.5	184.6	-13.1	-169.6	16.5
8	113.00	-91.2	22.8	4581	2670	-19.9	8.5	-1245.0	167.2	-11.3	-156.7	9.1
9	123.00	-86.5	23.1	4403	2513	-19.6	9.2	-1153.7	144.4	-9.7	-144.7	2.8
10	133.00	-82.9	25.3	4225	2379	-19.6	10.6	-1067.3	121.3	-8.4	-133.6	-3.8
11	143.00	-40.0	17.1	1443	1621	-27.7	10.5	-984.4	96.0	-7.3	-123.7	-8.1
12	153.00	-36.6	13.5	1285	1489	-28.5	9.1	-944.4	78.9	-6.5	-113.7	-11.8
13	163.00	-34.4	7.7	1100	1448	-31.2	5.3	-907.8	65.4	-5.7	-104.4	-11.8
14	173.00	-35.0	6.3	1100	1448	-31.8	4.3	-873.4	57.7	-5.1	-95.5	-11.8
15	183.00	-35.8	5.7	1100	1448	-32.5	3.9	-838.4	51.4	-4.6	-86.9	-11.8
16	193.00	-36.5	5.0	1100	1448	-33.2	3.5	-802.6	45.7	-4.1	-78.7	-11.7
17	203.00	-37.2	4.4	1100	1448	-33.8	3.1	-766.1	40.7	-3.7	-70.9	-11.7
18	213.00	-37.9	3.7	1100	1448	-34.5	2.5	-728.9	36.3	-3.3	-63.4	-11.7
19	223.00	-38.7	2.7	1100	1448	-35.1	1.9	-691.0	32.6	-2.9	-56.3	-11.6
20	233.00	-39.4	1.8	1100	1448	-35.8	1.2	-652.3	29.8	-2.6	-49.3	-11.5
21	243.00	-40.1	.9	1100	1448	-36.4	.6	-613.0	28.0	-2.3	-43.3	-11.5
22	253.00	-40.8	-.1	1100	1448	-37.1	-.0	-572.9	27.2	-2.1	-37.3	-11.5
23	263.00	-41.8	-.3	1100	1448	-38.0	-.2	-532.1	27.2	-1.8	-31.8	-11.5
24	273.00	-43.0	1.1	1100	1448	-39.1	.8	-490.3	27.0	-1.5	-26.7	-11.4
25	283.00	-44.2	2.0	1100	1448	-40.2	1.4	-447.3	25.9	-1.2	-22.0	-11.4
26	293.00	-45.4	2.8	1100	1448	-41.3	2.0	-403.2	23.9	-1.0	-17.8	-11.3
27	303.00	-46.5	3.6	1100	1448	-42.2	2.5	-357.8	21.0	-.8	-14.0	-11.2
28	313.00	-46.6	3.2	1100	1448	-42.4	2.2	-311.3	17.5	-.6	-10.6	-11.2
29	323.00	-46.8	2.8	1100	1448	-42.6	2.0	-264.7	14.2	-.4	-7.7	-11.2
30	333.00	-47.0	2.5	1100	1448	-42.7	1.7	-217.8	11.4	-.3	-5.3	-11.2
31	343.00	-70.8	3.0	1650	2171	-42.9	1.4	-170.8	8.9	-.2	-3.4	-11.0
MECH	358.00	-100.0	5.9	2970	3908	-33.7	1.5	-100.0	5.9	-.1	-1.3	-11.0

HARRAH'S HOLIDAY INN, ATLANTIC CITY
PROJECT 7130 CONFIGURATION A
SCALE = 300 REF. PRESSURE = 48.0
GUST FACTOR = 1.32 STANDARD FLOOR HEIGHT = 10.00
NUMBER OF SIDES = 12 NO. OF FLOORS = 34

SIDE	ANGLE	Z-AXIS
1	270.0	16.920
2	270.0	3.920
3	0.0	4.000
4	90.0	8.400
5	90.0	-4.180
6	180.0	8.800
7	0.0	1.500
8	270.0	2.200
9	90.0	-1.500
10	90.0	2.200
11	270.0	-1.500
12	180.0	6.100

FLOOR #	LABEL	HEIGHT-FT
1	PARK	14.00
2	PARK	10.00
3	2	19.00
4	3	20.00
5	4	10.00
6	4A	10.00
7	5	10.00
8	6	10.00
9	7	10.00
10	8	10.00
11	9	10.00
12	10	10.00
13	11	10.00
14	12	10.00
15	13	10.00
16	14	10.00
17	15	10.00
18	16	10.00
19	17	10.00
20	18	10.00
21	19	10.00
22	20	10.00
23	21	10.00
24	22	10.00
25	23	10.00
26	24	10.00
27	25	10.00
28	26	10.00
29	27	10.00
30	28	10.00
31	29	10.00
32	30	10.00
33	31	15.00
34	MECH	27.00

APPENDIX A

PRESSURE DATA

Note: Pressure coefficients are defined in Section 4.3.

Pressure tap designation is explained in Figure 3.

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
0	1101	-.149	.095	.166	-.449
0	1102	-.132	.096	.197	-.431
0	1103	-.113	.097	.225	-.428
0	1104	-.085	.099	.252	-.396
0	1105	-.057	.106	.310	-.542
0	1106	-.129	.215	.409	-.891
0	1107	-.207	.265	.650	-1.247
0	1108	-.146	.093	.160	-.443
0	1109	-.102	.094	.241	-.391
0	1110	-.035	.098	.335	-.324
0	1111	.012	.104	.410	-.412
0	1112	.028	.154	.503	-.937
0	1113	-.133	.253	.580	-1.233
0	1114	-.158	.229	.698	-1.208
0	1115	-.137	.088	.173	-.433
0	1116	-.105	.089	.193	-.404
0	1117	-.037	.090	.256	-.402
0	1118	.011	.102	.349	-.450
0	1119	.003	.173	.405	-.943
0	1120	-.161	.247	.529	-1.040
0	1121	-.189	.225	.704	-.888
0	1122	-.150	.084	.150	-.441
0	1123	-.115	.082	.166	-.405
0	1124	-.048	.087	.250	-.402
0	1125	-.014	.110	.422	-.695
0	1126	-.050	.188	.492	-.920
0	1127	-.214	.244	.555	-1.296
0	1128	-.226	.221	.600	-1.071
0	1129	-.154	.085	.170	-.454
0	1130	-.129	.086	.159	-.450
0	1131	-.071	.090	.224	-.452
0	1132	-.042	.113	.309	-.638
0	1133	-.076	.170	.308	-.831
0	1134	-.204	.223	.413	-1.016
0	1135	-.219	.203	.460	-.939
0	1136	-.140	.084	.128	-.428
0	1137	-.090	.079	.174	-.356
0	1138	-.056	.086	.236	-.364
0	1139	-.028	.107	.322	-.498
0	1140	-.029	.147	.397	-.685
0	1141	-.108	.218	.573	-1.063
0	1142	-.148	.217	.624	-1.062
0	1143	-.063	.082	.225	-.325
0	1144	-.070	.084	.246	-.334
0	1145	-.055	.088	.279	-.365
0	1146	-.075	.104	.297	-.482
0	1147	-.077	.145	.394	-.642
0	1148	-.095	.172	.391	-.805
0	1149	-.115	.176	.406	-1.413
0	1150	-.044	.089	.275	-.332
0	1151	-.034	.093	.286	-.393
0	1152	-.152	.136	.410	-.627
0	1201	-.171	.098	.164	-.501
0	1202	-.174	.097	.198	-.486
0	1203	-.201	.095	.206	-.547
0	1204	-.178	.093	.173	-.620
0	1205	-.176	.094	.147	-.589
0	1206	-.173	.096	.153	-.575
0	1207	-.178	.096	.154	-.526
0	1208	-.175	.093	.112	-.498
0	1209	-.176	.095	.118	-.507
0	1210	-.204	.098	.161	-.515
0	1211	-.158	.094	.181	-.451
0	1212	-.180	.089	.084	-.469
0	1213	-.178	.090	.089	-.473
0	1214	-.185	.090	.110	-.486
0	1215	-.184	.091	.114	-.493
0	1216	-.180	.090	.111	-.486
0	1217	-.177	.091	.121	-.477
0	1218	-.172	.092	.120	-.500
0	1219	-.163	.089	.093	-.495
0	1220	-.148	.086	.103	-.496
0	1221	-.184	.094	.151	-.502
0	1222	-.145	.088	.130	-.513
0	1223	-.125	.083	.147	-.377
0	1224	-.181	.082	.094	-.478
0	1225	-.180	.082	.105	-.490
0	1226	-.175	.082	.108	-.458
0	1227	-.173	.082	.113	-.449
0	1228	-.205	.092	.060	-.574
0	1229	-.157	.087	.110	-.522
0	1230	-.185	.088	.106	-.458
0	1231	-.188	.091	.117	-.510
0	1232	-.185	.089	.121	-.460
0	1233	-.184	.089	.111	-.458
0	1234	-.174	.083	.100	-.478
0	1235	-.172	.084	.108	-.486
0	1236	-.170	.083	.118	-.479
0	1237	-.170	.086	.167	-.459
0	1238	-.155	.083	.193	-.440
0	1239	-.185	.082	.081	-.475
0	1240	-.181	.089	.128	-.528
0	1241	-.182	.091	.110	-.529
0	1242	-.179	.091	.097	-.554
0	1243	-.176	.091	.111	-.536
0	1244	-.168	.091	.147	-.495
0	1245	-.169	.092	.146	-.507
0	1246	-.212	.085	.100	-.510
0	1247	-.165	.082	.139	-.446
0	1248	-.182	.090	.113	-.501
0	1249	-.179	.092	.124	-.500
0	1250	-.173	.086	.110	-.480
0	1251	-.174	.089	.111	-.522
0	1252	-.168	.088	.108	-.502
0	1253	-.168	.089	.109	-.498
0	1254	-.178	.090	.127	-.469
0	1301	-.209	.100	.092	-.565
0	1302	-.213	.101	.102	-.567
0	1303	-.238	.104	.112	-.631
0	1304	-.230	.105	.213	-.675
0	1305	-.243	.104	.097	-.644
0	1306	-.250	.107	.063	-.716
0	1307	-.267	.115	.091	-.871
0	1308	-.203	.094	.099	-.527
0	1309	-.202	.100	.120	-.550
0	1310	-.209	.099	.102	-.556
0	1311	-.230	.099	.083	-.593
0	1312	-.220	.098	.100	-.584
0	1313	-.231	.096	.064	-.681
0	1314	-.237	.101	.069	-.683
0	1315	-.211	.089	.100	-.535
0	1316	-.196	.088	.099	-.512
0	1317	-.209	.088	.118	-.479
0	1318	-.216	.088	.104	-.495
0	1319	-.235	.088	.076	-.520
0	1320	-.229	.092	.079	-.576
0	1321	-.239	.101	.136	-.712
0	1322	-.210	.093	.162	-.564
0	1323	-.227	.093	.145	-.572
0	1324	-.216	.091	.154	-.564
0	1325	-.219	.090	.108	-.561
0	1326	-.218	.093	.145	-.583
0	1327	-.240	.097	.122	-.649
0	1328	-.227	.098	.128	-.605
0	1329	-.223	.097	.053	-.546
0	1330	-.231	.099	.036	-.567
0	1331	-.252	.099	.037	-.587
0	1332	-.248	.097	.058	-.621
0	1333	-.256	.090	.022	-.548
0	1334	-.267	.100	.024	-.640
0	1335	-.286	.099	.004	-.627
0	1336	-.237	.095	.047	-.645
0	1337	-.198	.092	.063	-.577
0	1338	-.210	.091	.074	-.670
0	1339	-.225	.092	.075	-.656
0	1340	-.216	.087	.097	-.570
0	1401	.175	.119	.604	-.213
0	1402	.051	.097	.463	-.332
0	1403	.088	.123	.559	-.515
0	1404	.204	.134	.714	-.218

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
0	1405	.174	.129	.677	-.216
0	1406	.110	.118	.516	-.236
0	1407	.066	.108	.437	-.265
0	1408	.011	.099	.385	-.327
0	1409	-.034	.096	.327	-.371
0	1410	.429	.154	.929	-.058
0	1411	.422	.156	.928	-.034
0	1412	.355	.150	.829	-.140
0	1413	.364	.149	.817	-.110
0	1414	.364	.147	.811	-.120
0	1415	.308	.139	.760	-.135
0	1416	.221	.129	.641	-.182
0	1417	.078	.106	.443	-.245
0	1418	-.022	.096	.302	-.372
0	1419	.414	.160	.990	-.040
0	1420	.446	.153	.997	.009
0	1421	.382	.157	.919	-.052
0	1423	.396	.157	.902	-.057
0	1424	.304	.149	.791	-.170
0	1425	.225	.138	.668	-.252
0	1426	.042	.115	.411	-.396
0	1427	-.045	.101	.307	-.429
0	1428	.378	.154	.924	-.096
0	1429	.386	.143	.848	-.051
0	1430	.322	.144	.795	-.067
0	1431	.313	.150	.817	-.099
0	1432	.305	.147	.813	-.093
0	1433	.275	.136	.834	-.058
0	1434	.190	.130	.629	-.193
0	1435	.018	.108	.439	-.351
0	1436	-.095	.097	.242	-.422
0	1437	.325	.142	.876	-.081
0	1438	.365	.134	.865	-.030
0	1439	.295	.139	.792	-.072
0	1440	.301	.149	.805	-.149
0	1441	.303	.148	.825	-.128
0	1442	.251	.139	.754	-.160
0	1443	.186	.125	.636	-.189
0	1444	.032	.106	.377	-.376
0	1445	-.066	.100	.270	-.459
0	1446	.280	.129	.742	-.091
0	1447	.292	.137	.838	-.059
0	1448	.241	.132	.734	-.202
0	1449	.252	.138	.701	-.232
0	1450	.236	.117	.684	-.136
0	1451	.193	.110	.610	-.168
0	1452	.123	.102	.486	-.230
0	1453	.053	.092	.345	-.285
0	1454	.021	.095	.351	-.302
0	1455	.198	.112	.686	-.272
0	1456	.185	.112	.659	-.155
0	1457	.199	.109	.661	-.117
0	1458	.210	.122	.689	-.201
0	1459	.221	.123	.669	-.316
0	1460	.171	.137	.730	-.349
0	1461	.109	.136	.690	-.407
0	1462	.074	.110	.658	-.355
0	1463	.080	.105	.636	-.303
0	1464	.298	.209	.982	-.188
0	1465	.217	.103	.556	-.122
0	1466	.191	.102	.511	-.127
0	1467	.201	.099	.517	-.109
0	1801	.151	.080	.418	-.085
0	1802	.115	.082	.436	-.141
0	1803	-.045	.080	.176	-.373
0	1804	-.131	.087	.157	-.432
0	1805	-.008	.086	.244	-.416
0	1806	.077	.086	.385	-.223
0	1807	.128	.098	.442	-.164
0	2101	-.174	.086	.130	-.527
0	2102	-.109	.082	.178	-.393
0	2103	.091	.086	.408	-.197
0	2104	.096	.151	.567	-.491
0	2105	-.211	.091	.105	-.704
0	2106	-.204	.093	.097	-.723
0	2107	-.127	.096	.224	-.450
0	2108	-.093	.095	.247	-.380
0	2109	-.213	.098	.111	-.637
0	2110	-.214	.101	.102	-.730
0	2111	-.090	.094	.204	-.408
0	2112	-.084	.097	.230	-.376
0	2113	.193	.113	.516	-.308
0	2114	.150	.094	.494	-.200
0	2115	.130	.087	.474	-.183
0	2116	-.238	.104	.063	-.603
0	2117	-.158	.086	.120	-.533
0	2118	-.129	.087	.165	-.530
0	2119	-.155	.090	.124	-.488
0	2120	-.148	.112	.199	-.767
0	2121	-.213	.192	.405	-.984
0	2122	-.076	.091	.283	-.402
0	2123	-.110	.078	.154	-.421
0	2124	.039	.106	.540	-.273
0	2125	.112	.132	.555	-.499
0	2126	-.091	.087	.199	-.390
0	2127	-.073	.083	.262	-.340
0	2128	-.109	.078	.155	-.412
0	2129	.151	.106	.601	-.197
0	2130	.133	.090	.428	-.160
0	2131	-.080	.084	.242	-.395
0	2132	-.095	.084	.244	-.410
0	2133	-.101	.085	.236	-.410
0	2134	-.112	.086	.207	-.427
0	2135	-.134	.094	.201	-.473
0	2136	-.228	.116	.263	-.729
0	2137	-.081	.083	.160	-.373
0	2138	-.229	.111	.069	-.736
0	2139	.155	.090	.457	-.122
0	2140	.090	.092	.416	-.218
0	2141	.085	.092	.400	-.197
0	2142	.089	.096	.419	-.262
0	2143	-.062	.079	.190	-.341
0	2144	-.076	.080	.206	-.357
0	2145	-.085	.080	.178	-.359
0	2146	-.114	.081	.156	-.544
0	2147	-.156	.100	.152	-.568
0	2148	-.050	.084	.246	-.375
0	2149	-.154	.093	.167	-.526
0	2150	-.065	.082	.257	-.329
0	2151	-.070	.081	.295	-.326
0	2152	-.104	.083	.272	-.391
0	2153	-.085	.085	.337	-.355
0	2154	-.150	.090	.313	-.452
0	2201	-.189	.085	.102	-.529
0	2202	-.187	.084	.142	-.531
0	2203	-.224	.087	.053	-.572
0	2204	-.204	.088	.097	-.572
0	2205	-.181	.088	.090	-.543
0	2206	-.186	.088	.092	-.552
0	2207	-.222	.088	.060	-.585
0	2208	-.197	.089	.083	-.550
0	2209	-.195	.083	.097	-.514
0	2210	-.182	.084	.122	-.494
0	2211	-.223	.089	.083	-.702
0	2212	-.207	.087	.078	-.481
0	2213	-.237	.085	.092	-.516
0	2214	-.232	.084	.047	-.514
0	2215	-.243	.084	.019	-.557
0	2216	-.221	.089	.109	-.504
0	2217	-.200	.099	.123	-.530
0	2218	-.217	.088	.049	-.548
0	2219	-.239	.096	.042	-.578
0	2220	-.140	.095	.168	-.568
0	2221	-.154	.077	.097	-.543
0	2222	-.195	.103	.124	-.803
0	2224	-.108	.084	.159	-.394
0	2225	-.135	.086	.129	-.472
0	2226	-.088	.086	.177	-.406
0	2227	-.086	.090	.218	-.392
0	2228	-.096	.095	.183	-.477

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
0	2229	-.069	.085	.197	-.347
0	2230	-.519	.072	-.393	-.678
0	2231	-.075	.087	.184	-.398
0	2232	-.081	.086	.193	-.442
0	2233	-.092	.085	.156	-.392
0	2234	-.052	.081	.204	-.347
0	2235	-.049	.081	.197	-.322
0	2236	-.059	.085	.204	-.337
0	2237	-.070	.085	.188	-.351
0	2238	-.085	.095	.178	-.448
0	2239	-.071	.083	.166	-.396
0	2240	-.082	.085	.171	-.422
0	2301	-.303	.101	-.002	-.669
0	2302	-.275	.101	.076	-.663
0	2303	-.073	.080	.250	-.414
0	2304	-.036	.081	.237	-.381
0	2305	-.059	.084	.228	-.445
0	2306	-.023	.079	.250	-.362
0	2307	-.038	.088	.257	-.391
0	2308	.013	.080	.281	-.267
0	2309	-.256	.090	.045	-.589
0	2310	-.144	.112	.188	-.701
0	2311	-.152	.099	.162	-.620
0	2312	-.221	.091	.056	-.583
0	2313	-.177	.087	.098	-.487
0	2314	-.274	.110	.040	-.781
0	2315	-.186	.093	.139	-.495
0	2401	-.235	.099	.104	-.605
0	2402	-.249	.099	.094	-.602
0	2403	-.267	.101	.059	-.701
0	2404	-.189	.082	.090	-.442
0	2405	-.068	.087	.215	-.345
0	2406	-.094	.091	.181	-.488
0	2407	-.274	.108	.064	-.647
0	2408	-.248	.104	.083	-.737
0	2409	-.212	.084	.073	-.489
0	2411	-.278	.096	.017	-.608
0	2412	-.236	.106	.123	-.762
0	2413	-.240	.094	.059	-.580
0	2414	-.213	.086	.087	-.520
0	2415	-.140	.100	.139	-.623
0	2416	-.163	.105	.167	-.511
0	2417	-.228	.097	.106	-.575
0	2418	-.224	.095	.070	-.565
0	2419	-.241	.099	.062	-.601
0	2420	-.236	.099	.080	-.577
0	2421	-.062	.084	.209	-.335
0	2422	-.059	.092	.243	-.451
0	2423	-.210	.101	.148	-.575
0	2424	-.206	.099	.101	-.558
0	2425	-.236	.103	.089	-.620
0	2426	-.202	.098	.138	-.527
0	2427	-.208	.092	.166	-.521
0	2428	-.042	.096	.287	-.449
0	2429	-.078	.156	.259	-.823
0	2430	-.220	.120	.148	-.707
0	2431	-.194	.100	.110	-.558
0	2432	-.200	.097	.141	-.636
0	2433	-.171	.091	.128	-.490
0	2434	-.143	.095	.154	-.464
0	2435	-.124	.091	.202	-.443
0	2436	-.066	.087	.238	-.342
0	2437	-.053	.085	.264	-.418
0	2438	-.080	.085	.229	-.435
0	2439	-.084	.081	.163	-.403
0	2440	-.237	.093	.035	-.531
0	2441	-.136	.090	.142	-.422
0	2442	-.097	.084	.168	-.413
0	2443	-.074	.087	.252	-.379
0	2444	-.201	.115	.086	-.734
0	2445	-.152	.100	.145	-.571
0	2446	-.178	.099	.115	-.559
0	2447	-.150	.100	.201	-.482
0	2448	-.085	.092	.283	-.413
0	2449	-.072	.082	.237	-.373
0	2450	-.157	.086	.131	-.434
0	2451	-.137	.087	.168	-.482
0	2501	-.256	.106	.111	-.596
0	2502	-.260	.103	.082	-.582
0	2503	-.023	.111	.522	-.387
0	2504	-.269	.115	.094	-.652
0	2505	-.068	.092	.244	-.377
0	2506	-.262	.097	.078	-.646
0	2507	-.305	.100	-.005	-.656
0	2508	.071	.114	.447	-.341
0	2509	-.088	.099	.304	-.514
0	2510	-.069	.096	.283	-.483
0	2511	-.229	.111	.148	-.781
0	2601	.145	.139	.813	-.292
0	2602	.134	.115	.581	-.184
0	2603	.082	.115	.545	-.246
0	2604	.096	.111	.579	-.234
0	2605	.034	.099	.443	-.285
0	2606	.154	.117	.673	-.196
0	2607	.183	.120	.679	-.271
0	2608	.176	.121	.719	-.316
0	2609	.158	.105	.529	-.176
0	2610	.133	.096	.474	-.177
0	2611	.060	.102	.509	-.249
0	2612	.005	.096	.348	-.331
0	2613	.113	.106	.554	-.237
0	2614	.255	.104	.642	-.126
0	2615	.069	.093	.390	-.321
0	2616	.107	.086	.439	-.212
0	2617	.091	.087	.421	-.250
0	2618	.064	.085	.397	-.263
0	2619	-.062	.092	.324	-.381
0	2620	.094	.092	.406	-.262
0	2621	.192	.099	.560	-.148
0	5102	-.025	.159	.646	-.749
0	5103	-.072	.098	.410	-.400
0	5104	-.014	.135	.535	-.636
0	5105	-.100	.096	.317	-.430
0	5106	-.031	.109	.304	-.463
0	5107	-.095	.093	.303	-.431
0	5108	-.043	.097	.312	-.355
0	5109	-.077	.131	.322	-.711
0	5110	.130	.126	.837	-.421
0	5111	-.088	.087	.213	-.378
0	5112	.074	.084	.376	-.206
0	5114	.176	.124	.680	-.203
0	5202	-.173	.086	.121	-.492
0	5203	-.177	.090	.179	-.447
0	5204	-.176	.086	.098	-.504
0	5301	.093	.155	.695	-.528
0	5302	.035	.126	.591	-.352
0	5303	.074	.132	.645	-.332
0	5304	.077	.127	.658	-.380
0	5305	-.032	.136	.412	-.525
0	5901	-.130	.094	.213	-.454
0	5902	-.153	.134	.302	-.749
0	6101	-.165	.094	.143	-.622
0	6102	-.086	.080	.170	-.375
0	6103	-.100	.088	.197	-.502
0	6104	-.080	.081	.202	-.322
0	6105	-.064	.088	.252	-.328
0	6106	-.038	.082	.254	-.301
0	6201	-.085	.081	.199	-.333
0	6301	-.015	.090	.366	-.334
0	6302	-.032	.094	.354	-.355
0	6901	-.117	.095	.199	-.572
0	7101	-.179	.096	.101	-.599
0	7102	-.150	.092	.117	-.488
0	7103	-.261	.132	.268	-.838
0	7104	-.131	.085	.117	-.479
0	7105	.019	.098	.413	-.271
0	7106	-.135	.084	.149	-.420
0	7201	.058	.107	.527	-.274
0	7301	-.125	.076	.170	-.401
0	9101	-.280	.105	.059	-.621

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
0	9102	-.010	.110	.291	-.434
0	9103	-.052	.101	.384	-.533
0	9104	.097	.119	.532	-.357
0	9105	-.269	.100	.022	-.639
0	9106	.003	.099	.441	-.395
0	9107	-.301	.097	-.010	-.654
0	9108	-.249	.102	.081	-.619
0	9109	-.279	.091	.035	-.632
0	9110	.064	.103	.483	-.227
0	9111	-.233	.089	.087	-.567
0	9112	-.143	.111	.264	-.562
0	9113	-.307	.101	.047	-.712
0	9114	-.281	.098	.069	-.639
0	9115	-.259	.098	.055	-.589
0	9116	-.224	.097	.083	-.569
0	9117	-.278	.103	.071	-.650
0	9118	-.002	.085	.296	-.348
0	9119	.033	.094	.364	-.328
0	9120	-.241	.097	.055	-.664
0	9121	-.224	.097	.067	-.613
0	9122	-.245	.104	.071	-.711
0	9123	-.062	.092	.307	-.425
0	9124	-.147	.136	.330	-.765
0	9125	-.156	.098	.280	-.537
0	9126	-.164	.115	.211	-.625
0	9201	-.093	.132	.270	-.590
0	9202	-.078	.091	.246	-.447
0	9203	-.095	.086	.177	-.418
0	9204	-.169	.094	.171	-.571
0	9205	-.140	.093	.208	-.462
0	9206	-.083	.091	.239	-.397
0	9207	-.194	.086	.083	-.498
0	9208	-.192	.089	.091	-.502
0	9209	-.204	.100	.149	-.568
0	9210	-.180	.103	.182	-.621
0	9211	-.133	.101	.234	-.507
0	9212	-.183	.094	.128	-.497
0	9213	-.093	.090	.187	-.521
0	9214	-.229	.104	.088	-.841
0	9215	-.209	.112	.160	-.927
0	9216	-.170	.111	.165	-.697
0	9217	-.094	.092	.238	-.473
0	9218	-.100	.088	.191	-.403
0	9219	-.204	.091	.083	-.525
0	9220	-.205	.096	.105	-.564
0	9221	-.207	.091	.128	-.622
0	9222	-.222	.110	.190	-.771
0	9223	-.114	.108	.318	-.496
0	9224	-.084	.096	.266	-.428
0	9225	-.204	.087	.046	-.550
0	9226	-.233	.091	.049	-.577
0	9227	-.246	.092	.161	-.573
0	9228	-.141	.108	.257	-.559
0	9229	-.203	.086	.057	-.579
0	9230	-.218	.109	.082	-.670
0	9231	-.125	.101	.213	-.534
0	9232	-.219	.094	.064	-.555
0	9233	-.226	.098	.090	-.594
0	9234	-.248	.097	.103	-.664
0	9235	-.149	.099	.162	-.577
0	9236	-.296	.103	.061	-.695
0	9237	-.154	.101	.165	-.577
0	9238	-.087	.092	.198	-.419
10	1101	-.103	.082	.210	-.413
10	1102	-.079	.085	.235	-.399
10	1103	-.047	.088	.263	-.377
10	1104	-.014	.092	.304	-.310
10	1105	.015	.111	.523	-.308
10	1106	.073	.137	.650	-.761
10	1107	.106	.200	.807	-.746
10	1108	-.109	.087	.264	-.373
10	1109	-.055	.087	.251	-.312
10	1110	.028	.094	.332	-.268
10	1111	.088	.100	.412	-.248
10	1112	.150	.111	.495	-.230
10	1113	.176	.199	.717	-.567
10	1114	.149	.227	.813	-.621
10	1115	-.112	.089	.276	-.428
10	1116	-.067	.091	.378	-.385
10	1117	.024	.092	.388	-.249
10	1118	.084	.101	.494	-.233
10	1119	.144	.116	.581	-.412
10	1120	.124	.212	.707	-.702
10	1121	.093	.242	1.062	-.747
10	1122	-.127	.092	.215	-.414
10	1123	-.082	.091	.266	-.386
10	1124	.001	.097	.374	-.412
10	1125	.081	.100	.439	-.313
10	1126	.139	.121	.562	-.669
10	1127	.122	.224	.712	-.749
10	1128	.092	.235	.798	-.689
10	1129	-.129	.086	.147	-.459
10	1130	-.093	.088	.266	-.447
10	1131	-.013	.094	.414	-.396
10	1132	.044	.103	.484	-.356
10	1133	.074	.108	.519	-.583
10	1134	.034	.199	.720	-.685
10	1135	.005	.210	.755	-.754
10	1136	-.126	.078	.119	-.376
10	1137	-.072	.073	.165	-.316
10	1138	-.030	.079	.234	-.304
10	1139	.000	.098	.392	-.426
10	1140	.024	.127	.493	-.684
10	1141	.002	.202	.653	-.861
10	1142	-.038	.209	.714	-.765
10	1143	-.025	.084	.248	-.318
10	1144	-.032	.085	.231	-.336
10	1145	-.011	.089	.264	-.384
10	1146	-.017	.107	.272	-.416
10	1147	-.025	.147	.527	-.469
10	1148	-.043	.159	.611	-.525
10	1149	-.047	.158	.660	-.672
10	1150	-.019	.086	.329	-.296
10	1151	-.002	.090	.294	-.332
10	1152	-.073	.136	.477	-.501
10	1201	-.149	.092	.178	-.464
10	1202	-.141	.089	.170	-.419
10	1203	-.162	.098	.222	-.538
10	1204	-.166	.106	.288	-.622
10	1205	-.168	.107	.253	-.745
10	1206	-.168	.102	.196	-.571
10	1207	-.172	.102	.199	-.515
10	1208	-.174	.094	.147	-.480
10	1209	-.175	.096	.152	-.497
10	1210	-.189	.089	.127	-.482
10	1211	-.137	.085	.156	-.419
10	1212	-.174	.095	.139	-.489
10	1213	-.177	.095	.130	-.523
10	1214	-.167	.085	.115	-.437
10	1215	-.169	.086	.111	-.442
10	1216	-.164	.085	.107	-.437
10	1217	-.159	.085	.114	-.433
10	1218	-.152	.081	.122	-.430
10	1219	-.150	.086	.124	-.449
10	1220	-.133	.084	.130	-.434
10	1221	-.164	.081	.127	-.473
10	1222	-.131	.083	.179	-.468
10	1223	-.114	.078	.157	-.357
10	1224	-.153	.085	.110	-.499
10	1225	-.153	.086	.109	-.511
10	1226	-.146	.085	.121	-.487
10	1227	-.144	.085	.129	-.483
10	1228	-.198	.089	.105	-.570
10	1229	-.147	.085	.132	-.501
10	1230	-.162	.077	.118	-.427
10	1231	-.166	.078	.135	-.426
10	1232	-.162	.077	.118	-.411
10	1233	-.159	.077	.107	-.407
10	1234	-.154	.084	.154	-.468
10	1235	-.152	.085	.155	-.449

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
10	1236	-.147	.084	.159	-.434
10	1237	-.168	.085	.115	-.546
10	1238	-.151	.082	.134	-.505
10	1239	-.176	.085	.088	-.562
10	1240	-.169	.079	.068	-.483
10	1241	-.170	.081	.077	-.483
10	1242	-.163	.080	.075	-.501
10	1243	-.159	.080	.085	-.499
10	1244	-.157	.083	.108	-.475
10	1245	-.157	.085	.110	-.483
10	1246	-.213	.084	.052	-.543
10	1247	-.164	.081	.099	-.488
10	1248	-.180	.082	.073	-.486
10	1249	-.180	.082	.074	-.476
10	1250	-.173	.081	.112	-.414
10	1251	-.169	.084	.136	-.421
10	1252	-.159	.082	.141	-.410
10	1253	-.157	.083	.147	-.423
10	1254	-.177	.086	.111	-.448
10	1301	-.182	.102	.151	-.583
10	1302	-.186	.102	.152	-.601
10	1303	-.218	.106	.151	-.567
10	1304	-.208	.109	.145	-.565
10	1305	-.206	.106	.100	-.773
10	1306	-.207	.110	.141	-.810
10	1307	-.229	.116	.135	-.675
10	1308	-.165	.096	.147	-.501
10	1309	-.180	.089	.157	-.430
10	1310	-.189	.089	.151	-.433
10	1311	-.217	.089	.122	-.474
10	1312	-.205	.090	.149	-.498
10	1313	-.204	.108	.188	-.640
10	1314	-.213	.113	.178	-.713
10	1315	-.190	.100	.105	-.590
10	1316	-.174	.098	.123	-.565
10	1317	-.185	.095	.106	-.536
10	1318	-.192	.095	.104	-.534
10	1319	-.214	.095	.085	-.535
10	1320	-.204	.098	.114	-.550
10	1321	-.210	.096	.170	-.550
10	1322	-.183	.086	.164	-.467
10	1323	-.204	.086	.136	-.485
10	1324	-.193	.085	.153	-.466
10	1325	-.203	.085	.069	-.480
10	1326	-.203	.088	.076	-.493
10	1327	-.227	.092	.061	-.536
10	1328	-.214	.093	.069	-.528
10	1329	-.205	.089	.079	-.558
10	1330	-.212	.092	.065	-.577
10	1331	-.241	.093	.071	-.637
10	1332	-.232	.091	.055	-.580
10	1333	-.244	.091	.104	-.521
10	1334	-.248	.096	.070	-.655
10	1335	-.269	.097	.053	-.632
10	1336	-.232	.091	.081	-.552
10	1337	-.183	.087	.132	-.503
10	1338	-.198	.086	.062	-.506
10	1339	-.204	.090	.110	-.587
10	1340	-.202	.084	.065	-.516
10	1401	.151	.120	.540	-.320
10	1402	.076	.106	.608	-.246
10	1403	.145	.132	.596	-.235
10	1404	.216	.146	.800	-.208
10	1405	.175	.139	.728	-.224
10	1406	.099	.129	.583	-.293
10	1407	.051	.119	.528	-.346
10	1408	-.027	.101	.335	-.343
10	1409	-.065	.098	.287	-.369
10	1410	.388	.148	.835	-.072
10	1411	.412	.150	.895	-.036
10	1412	.377	.165	.973	-.164
10	1413	.324	.158	.950	-.149
10	1414	.335	.136	.816	-.080
10	1415	.263	.124	.712	-.143
10	1416	.170	.113	.538	-.197
10	1417	.041	.093	.368	-.243
10	1418	-.054	.098	.251	-.349
10	1419	.395	.151	.907	-.106
10	1420	.437	.145	.922	-.072
10	1421	.400	.157	.982	-.170
10	1423	.319	.144	.736	-.136
10	1424	.285	.137	.929	-.144
10	1425	.186	.123	.747	-.212
10	1426	.000	.102	.400	-.338
10	1427	-.074	.092	.238	-.375
10	1428	.361	.146	.859	-.164
10	1429	.390	.140	.920	-.100
10	1430	.355	.148	.841	-.111
10	1431	.299	.148	.843	-.125
10	1432	.297	.142	.820	-.143
10	1433	.247	.127	.707	-.171
10	1434	.158	.114	.546	-.232
10	1435	-.011	.097	.357	-.331
10	1436	-.113	.092	.233	-.395
10	1437	.323	.140	.823	-.202
10	1438	.372	.134	.853	-.033
10	1439	.336	.138	.913	-.141
10	1440	.281	.146	.855	-.121
10	1441	.286	.141	.861	-.127
10	1442	.215	.127	.645	-.183
10	1443	.140	.110	.515	-.204
10	1444	-.015	.088	.294	-.286
10	1445	-.101	.085	.182	-.381
10	1446	.275	.133	.733	-.151
10	1447	.292	.127	.759	-.114
10	1448	.275	.130	.731	-.120
10	1449	.240	.128	.697	-.197
10	1450	.242	.125	.754	-.115
10	1451	.189	.115	.640	-.133
10	1452	.109	.105	.482	-.213
10	1453	.030	.093	.371	-.270
10	1454	-.013	.087	.279	-.341
10	1455	.224	.127	.760	-.157
10	1456	.211	.132	.764	-.146
10	1457	.232	.127	.757	-.104
10	1458	.222	.126	.668	-.206
10	1459	.236	.124	.666	-.159
10	1460	.176	.133	.612	-.303
10	1461	.106	.134	.601	-.415
10	1462	.038	.105	.404	-.273
10	1463	.049	.101	.397	-.253
10	1464	.289	.205	1.138	-.153
10	1465	.214	.102	.592	-.076
10	1466	.215	.114	.622	-.148
10	1467	.226	.110	.608	-.125
10	1801	.139	.082	.428	-.105
10	1802	.094	.079	.332	-.176
10	1803	-.037	.081	.231	-.315
10	1804	-.119	.086	.159	-.377
10	1805	-.007	.082	.245	-.363
10	1806	.071	.078	.402	-.195
10	1807	.119	.085	.411	-.156
10	2101	-.161	.084	.094	-.446
10	2102	-.076	.081	.229	-.357
10	2103	.095	.086	.413	-.219
10	2104	.160	.135	.704	-.454
10	2105	-.204	.089	.075	-.539
10	2106	-.197	.092	.084	-.529
10	2107	-.106	.094	.277	-.443
10	2108	-.062	.095	.305	-.404
10	2109	-.179	.094	.099	-.538
10	2110	-.182	.101	.164	-.624
10	2111	-.067	.085	.284	-.340
10	2112	-.049	.098	.340	-.394
10	2113	.199	.109	.587	-.166
10	2114	.136	.098	.454	-.174
10	2115	.119	.092	.468	-.192
10	2116	-.226	.100	.071	-.618
10	2117	-.135	.089	.147	-.563
10	2118	-.125	.090	.162	-.494

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
10	2119	-.160	.093	.109	-.585
10	2120	-.151	.121	.213	-.683
10	2121	-.170	.186	.483	-.849
10	2122	-.047	.098	.366	-.351
10	2123	-.105	.086	.179	-.403
10	2124	.028	.112	.408	-.317
10	2125	.111	.117	.464	-.360
10	2126	-.072	.094	.250	-.383
10	2127	-.050	.088	.284	-.338
10	2128	-.095	.083	.155	-.370
10	2129	.144	.097	.478	-.140
10	2130	.120	.099	.508	-.185
10	2131	-.073	.081	.177	-.376
10	2132	-.089	.082	.157	-.382
10	2133	-.082	.081	.180	-.374
10	2134	-.097	.080	.147	-.365
10	2135	-.114	.091	.169	-.483
10	2136	-.212	.123	.274	-.769
10	2137	-.063	.080	.230	-.337
10	2138	-.199	.109	.175	-.618
10	2139	.138	.097	.472	-.180
10	2140	.072	.100	.424	-.238
10	2141	.076	.090	.392	-.232
10	2142	.074	.090	.399	-.274
10	2143	-.053	.085	.310	-.318
10	2144	-.067	.086	.263	-.359
10	2145	-.062	.084	.339	-.323
10	2146	-.093	.084	.223	-.371
10	2147	-.124	.092	.264	-.479
10	2148	-.039	.083	.295	-.290
10	2149	-.114	.084	.281	-.373
10	2150	-.068	.082	.207	-.355
10	2151	-.058	.085	.248	-.373
10	2152	-.093	.086	.206	-.409
10	2153	-.063	.086	.232	-.377
10	2154	-.135	.090	.182	-.544
10	2201	-.182	.091	.140	-.466
10	2202	-.182	.090	.132	-.451
10	2203	-.216	.093	.117	-.507
10	2204	-.194	.092	.119	-.514
10	2205	-.173	.089	.109	-.465
10	2206	-.198	.091	.076	-.502
10	2207	-.226	.093	.077	-.519
10	2208	-.195	.090	.101	-.497
10	2209	-.189	.092	.135	-.466
10	2210	-.179	.093	.129	-.478
10	2211	-.217	.098	.127	-.594
10	2212	-.206	.097	.146	-.671
10	2213	-.237	.090	.036	-.573
10	2214	-.231	.090	.037	-.547
10	2215	-.240	.092	.079	-.591
10	2216	-.214	.091	.072	-.536
10	2217	-.190	.090	.139	-.485
10	2218	-.198	.085	.054	-.495
10	2219	-.242	.093	.034	-.611
10	2220	-.144	.099	.177	-.563
10	2221	-.191	.083	.042	-.465
10	2222	-.205	.111	.104	-.757
10	2224	-.099	.089	.260	-.439
10	2225	-.132	.091	.205	-.438
10	2226	-.082	.093	.276	-.391
10	2227	-.100	.093	.280	-.420
10	2228	-.124	.102	.270	-.516
10	2229	-.081	.093	.276	-.393
10	2230	-.295	.123	-.037	-.573
10	2231	-.084	.096	.289	-.409
10	2232	-.084	.090	.217	-.433
10	2233	-.101	.092	.185	-.409
10	2234	-.047	.087	.259	-.334
10	2235	-.057	.089	.236	-.334
10	2236	-.068	.085	.207	-.373
10	2237	-.074	.084	.194	-.348
10	2238	-.089	.088	.173	-.423
10	2239	-.073	.083	.191	-.373
10	2240	-.079	.081	.226	-.353
10	2301	-.283	.105	.040	-.727
10	2302	-.259	.104	.054	-.695
10	2303	-.079	.083	.246	-.387
10	2304	-.036	.083	.259	-.321
10	2305	-.049	.083	.222	-.409
10	2306	-.030	.086	.269	-.313
10	2307	-.055	.094	.229	-.395
10	2308	-.007	.084	.285	-.272
10	2309	-.238	.086	.015	-.557
10	2310	-.137	.122	.221	-.732
10	2311	-.158	.104	.138	-.659
10	2312	-.192	.082	.076	-.532
10	2313	-.140	.081	.123	-.462
10	2314	-.246	.105	.080	-.686
10	2315	-.165	.088	.111	-.494
10	2401	-.217	.090	.123	-.523
10	2402	-.234	.090	.114	-.541
10	2403	-.250	.091	.070	-.574
10	2404	-.194	.082	.080	-.490
10	2405	-.060	.085	.193	-.323
10	2406	-.101	.090	.165	-.523
10	2407	-.256	.096	.031	-.667
10	2408	-.239	.087	.044	-.540
10	2409	-.210	.082	.049	-.526
10	2411	-.270	.086	.014	-.617
10	2412	-.237	.089	.059	-.566
10	2413	-.239	.096	.117	-.563
10	2414	-.215	.082	.027	-.506
10	2415	-.142	.104	.182	-.484
10	2416	-.167	.102	.226	-.672
10	2417	-.210	.096	.161	-.602
10	2418	-.221	.096	.084	-.605
10	2419	-.248	.101	.076	-.629
10	2420	-.249	.100	.148	-.596
10	2421	-.069	.086	.220	-.452
10	2422	-.063	.100	.307	-.487
10	2423	-.214	.097	.082	-.612
10	2424	-.208	.095	.081	-.569
10	2425	-.242	.100	.041	-.617
10	2426	-.211	.099	.074	-.579
10	2427	-.203	.085	.117	-.497
10	2428	-.068	.100	.269	-.503
10	2429	-.128	.149	.322	-1.017
10	2430	-.202	.100	.127	-.755
10	2431	-.188	.091	.098	-.538
10	2432	-.187	.090	.115	-.534
10	2433	-.147	.086	.121	-.452
10	2434	-.099	.085	.227	-.403
10	2435	-.098	.083	.161	-.377
10	2436	-.062	.080	.223	-.338
10	2437	-.039	.078	.211	-.288
10	2438	-.071	.079	.195	-.334
10	2439	-.084	.088	.237	-.454
10	2440	-.211	.093	.077	-.495
10	2441	-.091	.086	.201	-.373
10	2442	-.076	.083	.224	-.418
10	2443	-.071	.082	.243	-.407
10	2444	-.164	.102	.145	-.552
10	2445	-.110	.094	.194	-.411
10	2446	-.138	.096	.170	-.451
10	2447	-.095	.094	.268	-.458
10	2448	-.066	.088	.227	-.353
10	2449	-.055	.082	.250	-.357
10	2450	-.131	.086	.177	-.451
10	2451	-.104	.094	.201	-.521
10	2501	-.225	.092	.086	-.604
10	2502	-.235	.086	.073	-.541
10	2503	-.049	.092	.288	-.425
10	2504	-.240	.097	.072	-.573
10	2505	-.073	.091	.263	-.383
10	2506	-.232	.102	.129	-.696
10	2507	-.271	.106	.108	-.676
10	2508	.061	.105	.422	-.295
10	2509	-.105	.092	.218	-.436
10	2510	-.083	.089	.250	-.403

APPENDIX A -- PRESSURE DATA: CONFIGURATION A: HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
10	2511	-.251	.098	.099	-.706
10	2601	.151	.130	.628	-.464
10	2602	.134	.099	.520	-.170
10	2603	.073	.102	.434	-.247
10	2604	.083	.101	.487	-.226
10	2605	.012	.087	.332	-.291
10	2606	.129	.106	.531	-.287
10	2607	.169	.118	.641	-.194
10	2608	.157	.115	.572	-.306
10	2609	.144	.102	.476	-.164
10	2610	.120	.093	.410	-.160
10	2611	.035	.094	.360	-.252
10	2612	-.019	.088	.336	-.352
10	2613	.097	.100	.462	-.219
10	2614	.254	.105	.629	-.191
10	2615	.059	.097	.398	-.345
10	2616	.099	.087	.412	-.210
10	2617	.086	.080	.368	-.161
10	2618	.056	.078	.339	-.198
10	2619	-.081	.084	.245	-.354
10	2620	.084	.085	.380	-.173
10	2621	.216	.104	.798	-.070
10	5102	.094	.162	.734	-.613
10	5103	-.013	.114	.367	-.434
10	5104	.078	.136	.598	-.422
10	5105	-.040	.113	.377	-.417
10	5106	.022	.121	.489	-.404
10	5107	-.069	.098	.477	-.508
10	5108	-.013	.107	.339	-.380
10	5109	-.027	.131	.327	-.692
10	5110	.167	.133	.830	-.376
10	5111	-.064	.092	.237	-.432
10	5112	.073	.084	.381	-.234
10	5114	.179	.119	.719	-.161
10	5202	-.168	.089	.156	-.573
10	5203	-.144	.080	.134	-.414
10	5204	-.173	.092	.147	-.558
10	5301	.010	.140	.594	-.488
10	5302	-.061	.114	.289	-.545
10	5303	.008	.113	.451	-.555
10	5304	.025	.097	.381	-.350
10	5305	-.112	.123	.273	-.583
10	5901	-.093	.096	.237	-.506
10	5902	-.237	.161	.244	-1.158
10	6101	-.145	.093	.145	-.550
10	6102	-.076	.081	.188	-.378
10	6103	-.081	.087	.248	-.447
10	6104	-.063	.079	.212	-.336
10	6105	-.051	.085	.242	-.343
10	6106	-.029	.078	.214	-.296

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
10	6201	-.074	.079	.181	-.346
10	6301	-.015	.085	.283	-.317
10	6302	-.022	.086	.301	-.294
10	6901	-.109	.086	.142	-.473
10	7101	-.156	.087	.118	-.521
10	7102	-.129	.084	.143	-.471
10	7103	-.257	.149	.212	-1.028
10	7104	-.119	.077	.157	-.354
10	7105	.027	.091	.497	-.286
10	7106	-.127	.077	.210	-.389
10	7201	.030	.098	.411	-.301
10	7301	-.119	.079	.143	-.483
10	9101	-.236	.107	.103	-.685
10	9102	-.033	.110	.377	-.469
10	9103	-.057	.109	.414	-.508
10	9104	.102	.122	.586	-.351
10	9105	-.229	.110	.130	-.691
10	9106	.001	.119	.393	-.435
10	9107	-.267	.109	.085	-.648
10	9108	-.227	.091	.064	-.594
10	9109	-.233	.091	.041	-.564
10	9110	.053	.094	.373	-.240
10	9111	-.193	.091	.084	-.493
10	9112	-.145	.117	.188	-.579
10	9113	-.258	.101	.088	-.609
10	9114	-.240	.091	.062	-.571
10	9115	-.258	.097	.051	-.637
10	9116	-.231	.097	.199	-.610
10	9117	-.282	.100	.048	-.675
10	9118	.006	.077	.267	-.261
10	9119	.030	.091	.410	-.236
10	9120	-.245	.098	.089	-.575
10	9121	-.227	.096	.132	-.604
10	9122	-.251	.099	.080	-.607
10	9123	-.054	.087	.238	-.394
10	9124	-.148	.131	.329	-.706
10	9125	-.151	.096	.260	-.563
10	9126	-.187	.098	.278	-.596
10	9201	-.012	.120	.431	-.484
10	9202	-.013	.085	.281	-.285
10	9203	-.057	.082	.270	-.318
10	9204	-.167	.088	.133	-.532
10	9205	-.125	.084	.155	-.481
10	9206	-.067	.078	.203	-.403
10	9207	-.186	.091	.137	-.541
10	9208	-.195	.093	.139	-.562
10	9209	-.183	.094	.149	-.559
10	9210	-.173	.105	.197	-.697
10	9211	-.114	.095	.236	-.426
10	9212	-.170	.090	.138	-.557

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
10	9213	-.098	.084	.196	-.381
10	9214	-.203	.105	.145	-.661
10	9215	-.172	.115	.372	-.979
10	9216	-.159	.103	.301	-.598
10	9217	-.111	.099	.224	-.605
10	9218	-.106	.092	.226	-.468
10	9219	-.191	.089	.122	-.575
10	9220	-.193	.091	.124	-.561
10	9221	-.210	.101	.126	-.660
10	9222	-.196	.115	.206	-.796
10	9223	-.094	.123	.389	-.912
10	9224	-.074	.099	.226	-.451
10	9225	-.209	.095	.100	-.555
10	9226	-.242	.101	.079	-.597
10	9227	-.225	.093	.061	-.651
10	9228	-.120	.108	.333	-.543
10	9229	-.213	.095	.111	-.521
10	9230	-.196	.106	.155	-.995
10	9231	-.119	.108	.251	-.643
10	9232	-.224	.102	.069	-.632
10	9233	-.227	.101	.088	-.612
10	9234	-.235	.099	.170	-.621
10	9235	-.146	.102	.240	-.520
10	9236	-.287	.106	.185	-.691
10	9237	-.141	.102	.225	-.490
10	9238	-.085	.092	.232	-.446
20	1101	-.075	.087	.219	-.388
20	1102	-.041	.093	.274	-.369
20	1103	.006	.098	.304	-.337
20	1104	.047	.105	.368	-.373
20	1105	.089	.118	.598	-.322
20	1106	.174	.137	.732	-.381
20	1107	.253	.154	.842	-.469
20	1108	-.080	.089	.193	-.367
20	1109	-.005	.096	.363	-.342
20	1110	.105	.113	.537	-.236
20	1111	.181	.126	.610	-.204
20	1112	.256	.142	.689	-.160
20	1113	.320	.156	.875	-.258
20	1114	.335	.179	.942	-.423
20	1115	-.081	.088	.231	-.438
20	1116	-.029	.092	.317	-.413
20	1117	.099	.106	.489	-.284
20	1118	.173	.120	.648	-.234
20	1119	.249	.134	.795	-.212
20	1120	.328	.163	.925	-.316
20	1121	.348	.179	.885	-.279
20	1122	-.101	.090	.187	-.457
20	1123	-.039	.091	.262	-.379
20	1124	.065	.103	.424	-.316

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
20	1125	.141	.122	.589	-.227
20	1126	.212	.138	.715	-.183
20	1127	.288	.168	.833	-.460
20	1128	.295	.194	.849	-.395
20	1129	-.120	.093	.205	-.455
20	1130	-.079	.095	.253	-.404
20	1131	.007	.095	.360	-.307
20	1132	.064	.100	.405	-.272
20	1133	.150	.117	.675	-.204
20	1134	.203	.160	.803	-.804
20	1135	.199	.193	.837	-.589
20	1136	-.118	.080	.120	-.370
20	1137	-.056	.075	.193	-.279
20	1138	-.009	.080	.304	-.269
20	1139	.031	.086	.450	-.235
20	1140	.062	.093	.476	-.231
20	1141	.083	.136	.590	-.445
20	1142	.038	.159	.571	-.678
20	1143	-.005	.084	.266	-.352
20	1144	-.011	.086	.266	-.386
20	1145	.013	.087	.313	-.329
20	1146	.015	.098	.326	-.396
20	1147	.032	.111	.632	-.455
20	1148	.017	.129	.534	-.455
20	1149	.017	.126	.491	-.497
20	1150	.003	.085	.431	-.280
20	1151	-.028	.084	.397	-.313
20	1152	-.026	.131	.505	-.418
20	1201	-.151	.099	.244	-.630
20	1202	-.133	.092	.226	-.503
20	1203	-.163	.105	.175	-.678
20	1204	-.178	.103	.142	-.624
20	1205	-.178	.101	.152	-.649
20	1206	-.175	.095	.134	-.506
20	1207	-.174	.094	.129	-.502
20	1208	-.174	.094	.139	-.539
20	1209	-.177	.096	.145	-.555
20	1210	-.205	.093	.152	-.661
20	1211	-.137	.088	.167	-.506
20	1212	-.176	.099	.138	-.539
20	1213	-.181	.097	.130	-.589
20	1214	-.167	.097	.179	-.503
20	1215	-.169	.097	.172	-.508
20	1216	-.160	.095	.157	-.494
20	1217	-.155	.094	.159	-.501
20	1218	-.150	.088	.105	-.447
20	1219	-.157	.085	.104	-.469
20	1220	-.132	.083	.104	-.422
20	1221	-.166	.096	.121	-.532
20	1222	-.124	.078	.144	-.375

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
20	1223	-.128	.083	.170	-.379
20	1224	-.164	.096	.115	-.472
20	1225	-.161	.097	.130	-.477
20	1226	-.150	.095	.128	-.464
20	1227	-.149	.096	.135	-.463
20	1228	-.217	.091	.052	-.503
20	1229	-.147	.085	.104	-.417
20	1230	-.160	.096	.120	-.466
20	1231	-.166	.096	.125	-.491
20	1232	-.161	.093	.126	-.484
20	1233	-.159	.092	.111	-.471
20	1234	-.169	.088	.111	-.551
20	1235	-.165	.090	.113	-.549
20	1236	-.158	.089	.113	-.534
20	1237	-.180	.088	.089	-.469
20	1238	-.157	.085	.115	-.441
20	1239	-.207	.092	.091	-.601
20	1240	-.199	.098	.110	-.474
20	1241	-.201	.100	.119	-.479
20	1242	-.188	.098	.123	-.453
20	1243	-.181	.098	.149	-.447
20	1244	-.181	.096	.193	-.477
20	1245	-.183	.098	.204	-.489
20	1246	-.230	.088	.029	-.538
20	1247	-.171	.085	.087	-.465
20	1248	-.212	.098	.098	-.532
20	1249	-.214	.098	.094	-.527
20	1250	-.202	.097	.108	-.507
20	1251	-.195	.100	.122	-.516
20	1252	-.177	.099	.143	-.493
20	1253	-.174	.099	.135	-.498
20	1254	-.186	.091	.093	-.453
20	1301	-.155	.092	.165	-.498
20	1302	-.165	.093	.159	-.497
20	1303	-.190	.096	.156	-.556
20	1304	-.175	.098	.176	-.592
20	1305	-.172	.098	.184	-.651
20	1306	-.182	.108	.120	-1.105
20	1307	-.203	.115	.116	-1.325
20	1308	-.147	.081	.091	-.435
20	1309	-.152	.085	.118	-.487
20	1310	-.164	.085	.102	-.498
20	1311	-.187	.086	.077	-.508
20	1312	-.173	.087	.096	-.510
20	1313	-.169	.092	.121	-.647
20	1314	-.180	.098	.108	-.914
20	1315	-.169	.086	.126	-.479
20	1316	-.154	.085	.129	-.464
20	1317	-.152	.087	.139	-.454
20	1318	-.165	.087	.134	-.457

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
20	1319	-.184	.088	.126	-.479
20	1320	-.170	.091	.144	-.510
20	1321	-.164	.093	.140	-.490
20	1322	-.155	.090	.131	-.442
20	1323	-.173	.090	.109	-.478
20	1324	-.162	.089	.101	-.441
20	1325	-.171	.092	.086	-.471
20	1326	-.178	.095	.097	-.506
20	1327	-.196	.096	.095	-.562
20	1328	-.182	.096	.114	-.550
20	1329	-.174	.090	.193	-.447
20	1330	-.184	.092	.191	-.458
20	1331	-.214	.092	.144	-.509
20	1332	-.206	.090	.106	-.498
20	1333	-.206	.093	.087	-.494
20	1334	-.208	.096	.114	-.543
20	1335	-.229	.098	.087	-.540
20	1336	-.214	.087	.067	-.617
20	1337	-.161	.083	.080	-.555
20	1338	-.181	.082	.076	-.482
20	1339	-.177	.080	.075	-.532
20	1340	-.181	.081	.067	-.505
20	1401	.098	.167	.617	-.465
20	1402	.117	.123	.624	-.309
20	1403	.122	.151	.510	-.493
20	1404	.171	.125	.641	-.254
20	1405	.122	.119	.531	-.271
20	1406	.046	.109	.453	-.312
20	1407	.007	.100	.368	-.324
20	1408	-.050	.092	.291	-.410
20	1409	-.081	.092	.264	-.450
20	1410	.313	.171	.807	-.367
20	1411	.337	.165	.840	-.268
20	1412	.268	.178	.848	-.383
20	1413	.240	.127	.781	-.204
20	1414	.252	.130	.663	-.180
20	1415	.175	.119	.578	-.232
20	1416	.092	.108	.481	-.314
20	1417	-.005	.090	.336	-.395
20	1418	-.067	.085	.231	-.387
20	1419	.306	.167	.774	-.265
20	1420	.365	.158	.859	-.195
20	1421	.326	.172	.886	-.443
20	1423	.248	.124	.648	-.268
20	1424	.192	.121	.625	-.172
20	1425	.108	.108	.519	-.212
20	1426	-.038	.092	.283	-.336
20	1427	-.084	.086	.217	-.376
20	1428	.301	.159	.792	-.228
20	1429	.339	.154	.845	-.256

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
20	1430	.290	.157	.866	-.271
20	1431	.218	.125	.611	-.223
20	1432	.218	.125	.617	-.228
20	1433	.173	.110	.537	-.223
20	1434	.103	.101	.549	-.184
20	1435	-.038	.091	.307	-.323
20	1436	-.114	.088	.164	-.388
20	1437	.286	.145	.786	-.280
20	1438	.335	.140	.922	-.123
20	1439	.276	.149	.797	-.288
20	1440	.211	.127	.626	-.232
20	1441	.216	.127	.631	-.246
20	1442	.153	.114	.506	-.274
20	1443	.091	.102	.411	-.297
20	1444	-.039	.081	.258	-.317
20	1445	-.111	.081	.202	-.376
20	1446	.264	.135	.735	-.168
20	1447	.293	.133	.805	-.183
20	1448	.232	.122	.738	-.179
20	1449	.184	.111	.632	-.115
20	1450	.191	.126	.707	-.208
20	1451	.137	.113	.573	-.250
20	1452	.063	.101	.404	-.287
20	1453	-.001	.090	.328	-.311
20	1454	-.022	.080	.249	-.271
20	1455	.204	.116	.601	-.543
20	1456	.187	.119	.628	-.153
20	1457	.215	.114	.594	-.135
20	1458	.211	.128	.788	-.144
20	1459	.226	.123	.760	-.115
20	1460	.140	.130	.564	-.276
20	1461	.068	.128	.495	-.335
20	1462	.028	.096	.367	-.365
20	1463	.042	.093	.364	-.332
20	1464	.287	.213	1.023	-.173
20	1465	.196	.099	.635	-.115
20	1466	.187	.102	.542	-.155
20	1467	.203	.099	.539	-.128
20	1801	.113	.080	.474	-.137
20	1802	.079	.085	.412	-.182
20	1803	-.033	.092	.242	-.322
20	1804	-.095	.092	.223	-.398
20	1805	.004	.078	.311	-.255
20	1806	.052	.079	.362	-.256
20	1807	.097	.088	.399	-.217
20	2101	-.156	.090	.168	-.451
20	2102	-.060	.089	.265	-.363
20	2103	.117	.099	.464	-.152
20	2104	.173	.137	.742	-.290
20	2105	-.208	.094	.110	-.517
20	2106	-.199	.095	.088	-.557
20	2107	-.085	.097	.240	-.393
20	2108	-.041	.097	.314	-.367
20	2109	-.146	.098	.272	-.529
20	2110	-.151	.106	.224	-.536
20	2111	-.044	.086	.253	-.382
20	2112	-.026	.099	.414	-.349
20	2113	.200	.114	.627	-.228
20	2114	.159	.114	.627	-.163
20	2115	.145	.107	.537	-.207
20	2116	-.191	.101	.148	-.603
20	2117	-.113	.083	.209	-.414
20	2118	-.123	.087	.176	-.457
20	2119	-.162	.095	.154	-.516
20	2120	-.121	.108	.228	-.558
20	2121	-.079	.170	.551	-.735
20	2122	-.012	.097	.364	-.335
20	2123	-.093	.083	.210	-.417
20	2124	.052	.131	.500	-.311
20	2125	.121	.117	.627	-.498
20	2126	-.049	.087	.250	-.393
20	2127	-.027	.080	.253	-.347
20	2128	-.070	.078	.191	-.414
20	2129	.148	.103	.497	-.145
20	2130	.107	.095	.426	-.220
20	2131	-.065	.079	.209	-.362
20	2132	-.082	.080	.182	-.384
20	2133	-.066	.079	.218	-.400
20	2134	-.088	.079	.161	-.403
20	2135	-.087	.089	.254	-.399
20	2136	-.189	.130	.257	-.772
20	2137	-.027	.084	.255	-.324
20	2138	-.129	.099	.226	-.621
20	2139	.119	.089	.421	-.192
20	2140	.044	.093	.341	-.279
20	2141	.052	.093	.424	-.289
20	2142	.050	.084	.315	-.233
20	2143	-.041	.080	.249	-.304
20	2144	-.056	.081	.226	-.346
20	2145	-.038	.079	.233	-.338
20	2146	-.067	.080	.191	-.333
20	2147	-.089	.082	.196	-.377
20	2148	-.043	.077	.208	-.307
20	2149	-.075	.078	.193	-.313
20	2150	-.044	.075	.193	-.310
20	2151	-.040	.080	.260	-.309
20	2152	-.067	.080	.271	-.363
20	2153	-.034	.080	.250	-.336
20	2154	-.120	.083	.187	-.458
20	2201	-.191	.088	.090	-.481
20	2202	-.193	.088	.080	-.498
20	2203	-.223	.090	.058	-.522
20	2204	-.199	.089	.080	-.506
20	2205	-.186	.091	.129	-.529
20	2206	-.208	.091	.077	-.547
20	2207	-.235	.092	.046	-.541
20	2208	-.211	.092	.106	-.572
20	2209	-.198	.093	.149	-.507
20	2210	-.194	.097	.170	-.541
20	2211	-.227	.099	.093	-.576
20	2212	-.219	.099	.106	-.592
20	2213	-.191	.090	.144	-.507
20	2214	-.197	.095	.159	-.527
20	2215	-.232	.102	.166	-.626
20	2216	-.219	.099	.159	-.633
20	2217	-.172	.096	.185	-.528
20	2218	-.147	.095	.164	-.519
20	2219	-.200	.100	.112	-.573
20	2220	-.075	.092	.242	-.427
20	2221	-.152	.086	.092	-.468
20	2222	-.166	.109	.181	-.674
20	2224	-.071	.083	.249	-.387
20	2225	-.100	.084	.245	-.422
20	2226	-.058	.084	.253	-.348
20	2227	-.082	.085	.221	-.367
20	2228	-.096	.087	.208	-.419
20	2229	-.063	.079	.216	-.352
20	2230	-.097	.086	.042	-.300
20	2231	-.066	.082	.200	-.396
20	2232	-.061	.088	.231	-.335
20	2233	-.079	.088	.184	-.351
20	2234	-.030	.085	.234	-.309
20	2235	-.048	.087	.208	-.351
20	2236	-.049	.080	.243	-.329
20	2237	-.058	.079	.230	-.366
20	2238	-.051	.079	.257	-.327
20	2239	-.055	.078	.248	-.309
20	2240	-.058	.080	.194	-.349
20	2301	-.235	.091	.053	-.559
20	2302	-.221	.088	.050	-.526
20	2303	-.073	.085	.255	-.365
20	2304	-.044	.083	.300	-.335
20	2305	-.053	.082	.297	-.358
20	2306	-.040	.086	.251	-.348
20	2307	-.066	.102	.283	-.583
20	2308	-.042	.087	.239	-.400
20	2309	-.207	.084	.056	-.519
20	2310	-.149	.110	.252	-.662
20	2311	-.193	.126	.169	-.837
20	2312	-.173	.093	.118	-.501

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
20	2313	-.115	.092	.202	-.452
20	2314	-.210	.113	.140	-.654
20	2315	-.128	.088	.216	-.462
20	2401	-.188	.098	.133	-.521
20	2402	-.205	.098	.130	-.544
20	2403	-.213	.097	.155	-.577
20	2404	-.198	.085	.065	-.513
20	2405	-.044	.083	.270	-.349
20	2406	-.087	.091	.299	-.414
20	2407	-.235	.089	.101	-.595
20	2408	-.221	.088	.156	-.545
20	2409	-.194	.082	.080	-.459
20	2411	-.249	.081	.129	-.557
20	2412	-.230	.088	.137	-.547
20	2413	-.216	.092	.069	-.515
20	2414	-.206	.084	.054	-.498
20	2415	-.177	.105	.121	-.583
20	2416	-.185	.097	.077	-.580
20	2417	-.217	.092	.053	-.629
20	2418	-.211	.090	.111	-.537
20	2419	-.245	.096	.061	-.618
20	2420	-.234	.101	.182	-.618
20	2421	-.065	.081	.184	-.441
20	2422	-.063	.095	.257	-.506
20	2423	-.201	.094	.088	-.511
20	2424	-.199	.093	.150	-.499
20	2425	-.220	.095	.126	-.579
20	2426	-.184	.094	.157	-.518
20	2427	-.160	.088	.112	-.506
20	2428	-.078	.103	.301	-.551
20	2429	-.145	.121	.366	-.712
20	2430	-.192	.095	.114	-.669
20	2431	-.171	.093	.127	-.513
20	2432	-.154	.091	.130	-.466
20	2433	-.118	.086	.135	-.448
20	2434	-.065	.086	.296	-.382
20	2435	-.067	.087	.209	-.337
20	2436	-.050	.082	.222	-.367
20	2437	-.036	.084	.243	-.294
20	2438	-.071	.088	.252	-.347
20	2439	-.082	.091	.195	-.450
20	2440	-.151	.092	.160	-.465
20	2441	-.055	.082	.214	-.346
20	2442	-.068	.086	.221	-.355
20	2443	-.073	.090	.204	-.391
20	2444	-.139	.107	.156	-.597
20	2445	-.089	.092	.224	-.462
20	2446	-.113	.096	.246	-.456
20	2447	-.040	.100	.328	-.380
20	2448	-.024	.105	.510	-.363

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
20	2449	-.029	.086	.269	-.340
20	2450	-.091	.081	.198	-.354
20	2451	-.059	.084	.281	-.335
20	2501	-.210	.094	.086	-.491
20	2502	-.210	.090	.119	-.502
20	2503	-.059	.090	.246	-.323
20	2504	-.222	.094	.101	-.496
20	2505	-.092	.088	.221	-.413
20	2506	-.228	.093	.119	-.543
20	2507	-.261	.097	.124	-.589
20	2508	.049	.098	.378	-.324
20	2509	-.112	.093	.222	-.414
20	2510	-.092	.092	.237	-.406
20	2511	-.233	.102	.074	-.636
20	2601	.056	.145	.497	-.590
20	2602	.095	.084	.382	-.174
20	2603	.025	.089	.369	-.329
20	2604	.059	.087	.378	-.225
20	2605	.009	.087	.297	-.309
20	2606	.119	.109	.519	-.251
20	2607	.172	.118	.634	-.212
20	2608	.094	.127	.544	-.483
20	2609	.102	.095	.580	-.215
20	2610	.097	.091	.443	-.209
20	2611	.014	.092	.466	-.317
20	2612	-.023	.084	.314	-.312
20	2613	.063	.099	.577	-.241
20	2614	.239	.103	.617	-.165
20	2615	.012	.094	.286	-.333
20	2616	.070	.085	.337	-.216
20	2617	.076	.083	.368	-.232
20	2618	.059	.080	.347	-.207
20	2619	-.068	.086	.238	-.356
20	2620	.098	.091	.413	-.240
20	2621	.213	.114	.636	-.138
20	5102	.160	.156	.807	-.380
20	5103	.049	.115	.447	-.319
20	5104	.146	.141	.778	-.312
20	5105	.005	.106	.377	-.358
20	5106	-.068	.119	.457	-.326
20	5107	-.049	.087	.285	-.399
20	5108	.020	.095	.368	-.305
20	5109	.034	.123	.441	-.465
20	5110	.204	.137	.746	-.205
20	5111	-.039	.092	.307	-.372
20	5112	.066	.085	.390	-.247
20	5114	.165	.115	.596	-.309
20	5202	-.136	.091	.144	-.529
20	5203	-.153	.083	.148	-.505
20	5204	-.156	.102	.158	-.619

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
20	5301	-.019	.145	.471	-.702
20	5302	-.091	.124	.260	-.721
20	5303	-.020	.129	.425	-.639
20	5304	.019	.095	.434	-.448
20	5305	-.098	.112	.283	-.638
20	5901	-.069	.094	.271	-.372
20	5902	-.257	.155	.256	-.986
20	6101	-.112	.086	.166	-.462
20	6102	-.057	.077	.210	-.346
20	6103	-.056	.082	.202	-.338
20	6104	-.047	.078	.216	-.321
20	6105	-.051	.081	.280	-.372
20	6106	-.025	.076	.230	-.320
20	6201	-.061	.080	.213	-.404
20	6301	-.011	.084	.319	-.317
20	6302	-.011	.091	.396	-.307
20	6901	-.090	.073	.181	-.451
20	7101	-.128	.077	.126	-.549
20	7102	-.117	.074	.087	-.402
20	7103	-.210	.133	.188	-.744
20	7104	-.104	.068	.207	-.332
20	7105	.007	.088	.338	-.280
20	7106	-.106	.076	.142	-.344
20	7201	-.001	.093	.423	-.258
20	7301	-.106	.074	.168	-.396
20	9101	-.214	.094	.112	-.640
20	9102	-.073	.105	.270	-.442
20	9103	-.061	.111	.295	-.485
20	9104	.111	.111	.540	-.238
20	9105	-.207	.106	.150	-.617
20	9106	.015	.111	.407	-.424
20	9107	-.247	.102	.133	-.576
20	9108	-.202	.100	.164	-.512
20	9109	-.214	.093	.089	-.493
20	9110	.029	.086	.297	-.244
20	9111	-.184	.092	.140	-.485
20	9112	-.059	.108	.251	-.539
20	9113	-.245	.099	.059	-.557
20	9114	-.227	.093	.056	-.517
20	9115	-.229	.085	.059	-.551
20	9116	-.212	.089	.074	-.483
20	9117	-.252	.089	.059	-.547
20	9118	.008	.079	.288	-.310
20	9119	.016	.085	.343	-.276
20	9120	-.217	.088	.062	-.518
20	9121	-.220	.091	.123	-.527
20	9122	-.230	.091	.080	-.614
20	9123	-.032	.090	.234	-.342
20	9124	-.141	.116	.259	-.594
20	9125	-.145	.092	.193	-.493

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
20	9126	-.178	.103	.155	-.772
20	9201	.027	.112	.397	-.491
20	9202	.016	.090	.438	-.277
20	9203	-.039	.086	.274	-.341
20	9204	-.141	.088	.153	-.526
20	9205	-.094	.085	.206	-.434
20	9206	-.038	.079	.209	-.332
20	9207	-.176	.089	.125	-.544
20	9208	-.197	.095	.103	-.810
20	9209	-.178	.095	.113	-.511
20	9210	-.139	.111	.284	-.603
20	9211	-.079	.086	.179	-.435
20	9212	-.185	.091	.103	-.513
20	9213	-.069	.082	.220	-.353
20	9214	-.166	.110	.229	-.783
20	9215	-.117	.104	.355	-.500
20	9216	-.100	.099	.304	-.467
20	9217	-.089	.089	.219	-.399
20	9218	-.085	.086	.178	-.395
20	9219	-.207	.091	.090	-.544
20	9220	-.211	.093	.064	-.547
20	9221	-.216	.096	.090	-.603
20	9222	-.145	.131	.278	-.767
20	9223	-.025	.101	.312	-.377
20	9224	-.051	.088	.256	-.352
20	9225	-.213	.089	.085	-.564
20	9226	-.240	.094	.072	-.632
20	9227	-.196	.093	.143	-.667
20	9228	-.070	.102	.265	-.436
20	9229	-.223	.091	.084	-.557
20	9230	-.167	.102	.183	-.593
20	9231	-.061	.111	.364	-.642
20	9232	-.219	.092	.054	-.640
20	9233	-.206	.093	.052	-.610
20	9234	-.196	.095	.084	-.575
20	9235	-.087	.097	.249	-.467
20	9236	-.236	.108	.086	-.646
20	9237	-.073	.095	.282	-.576
20	9238	-.063	.087	.184	-.394
30	1101	-.038	.103	.318	-.340
30	1102	.009	.109	.401	-.313
30	1103	.070	.115	.477	-.273
30	1104	.120	.123	.576	-.274
30	1105	.177	.113	.575	-.226
30	1106	.273	.128	.737	-.118
30	1107	.333	.139	.845	-.087
30	1108	-.050	.082	.304	-.354
30	1109	.042	.099	.391	-.327
30	1110	.167	.116	.593	-.221
30	1111	.247	.127	.716	-.143

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
30	1112	.322	.142	.856	-.060
30	1113	.413	.154	.889	-.117
30	1114	.395	.152	.865	-.125
30	1115	-.048	.086	.260	-.347
30	1116	.023	.093	.363	-.312
30	1117	.164	.105	.547	-.243
30	1118	.251	.121	.670	-.139
30	1119	.336	.137	.804	-.075
30	1120	.403	.156	.990	-.065
30	1121	.377	.161	1.089	-.098
30	1122	-.079	.096	.242	-.391
30	1123	-.004	.100	.353	-.308
30	1124	.116	.118	.539	-.225
30	1125	.190	.119	.711	-.161
30	1126	.251	.132	.805	-.156
30	1127	.300	.143	.857	-.147
30	1128	.287	.148	.785	-.422
30	1129	-.094	.095	.294	-.452
30	1130	-.041	.101	.348	-.411
30	1131	.059	.113	.547	-.313
30	1132	.115	.125	.670	-.274
30	1133	.178	.139	.737	-.217
30	1134	.199	.145	.771	-.364
30	1135	.187	.145	.749	-.428
30	1136	-.103	.086	.177	-.379
30	1137	-.039	.084	.241	-.328
30	1138	.007	.095	.363	-.354
30	1139	.055	.108	.593	-.243
30	1140	.076	.114	.664	-.226
30	1141	.104	.125	.686	-.419
30	1142	.076	.138	.644	-.499
30	1143	.022	.082	.297	-.260
30	1144	.014	.084	.290	-.275
30	1145	.034	.085	.313	-.253
30	1146	.026	.093	.357	-.303
30	1147	.042	.121	.425	-.535
30	1148	.021	.119	.450	-.693
30	1149	.035	.110	.501	-.318
30	1150	.047	.108	.458	-.264
30	1151	.047	.097	.486	-.242
30	1152	-.025	.113	.517	-.383
30	1201	-.170	.103	.228	-.658
30	1202	-.151	.094	.170	-.618
30	1203	-.177	.103	.127	-.609
30	1204	-.184	.111	.171	-.700
30	1205	-.186	.109	.171	-.640
30	1206	-.181	.103	.156	-.560
30	1207	-.178	.101	.166	-.555
30	1208	-.164	.089	.099	-.468
30	1209	-.166	.092	.099	-.480

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
30	1210	-.227	.095	.053	-.810
30	1211	-.152	.087	.117	-.503
30	1212	-.175	.093	.100	-.491
30	1213	-.174	.090	.102	-.454
30	1214	-.165	.096	.164	-.482
30	1215	-.165	.096	.168	-.485
30	1216	-.155	.095	.163	-.452
30	1217	-.151	.095	.173	-.448
30	1218	-.153	.085	.196	-.451
30	1219	-.175	.089	.087	-.603
30	1220	-.149	.087	.108	-.563
30	1221	-.191	.093	.103	-.602
30	1222	-.145	.077	.153	-.406
30	1223	-.131	.081	.164	-.430
30	1224	-.160	.086	.140	-.499
30	1225	-.156	.087	.146	-.480
30	1226	-.147	.086	.154	-.468
30	1227	-.145	.086	.162	-.470
30	1228	-.245	.094	.061	-.638
30	1229	-.166	.088	.143	-.565
30	1230	-.182	.096	.149	-.565
30	1231	-.180	.093	.124	-.556
30	1232	-.176	.090	.128	-.528
30	1233	-.170	.089	.141	-.514
30	1234	-.166	.096	.172	-.553
30	1235	-.162	.098	.158	-.582
30	1236	-.156	.097	.159	-.565
30	1237	-.209	.101	.093	-.612
30	1238	-.180	.098	.119	-.559
30	1239	-.225	.102	.160	-.621
30	1240	-.208	.088	.083	-.534
30	1241	-.210	.090	.093	-.550
30	1242	-.197	.086	.097	-.486
30	1243	-.183	.084	.140	-.502
30	1244	-.170	.096	.161	-.484
30	1245	-.171	.098	.167	-.488
30	1246	-.267	.103	.038	-.821
30	1247	-.201	.098	.102	-.593
30	1248	-.227	.101	.094	-.529
30	1249	-.230	.102	.101	-.597
30	1250	-.222	.092	.042	-.603
30	1251	-.209	.094	.055	-.566
30	1252	-.183	.092	.069	-.477
30	1253	-.176	.093	.091	-.482
30	1254	-.179	.085	.114	-.503
30	1301	-.140	.086	.132	-.444
30	1302	-.147	.087	.135	-.455
30	1303	-.169	.092	.167	-.533
30	1304	-.150	.095	.179	-.800
30	1305	-.139	.096	.218	-.558

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
30	1306	-.147	.096	.178	-.680
30	1307	-.165	.102	.168	-.972
30	1308	-.127	.079	.139	-.443
30	1309	-.128	.086	.178	-.475
30	1310	-.138	.086	.179	-.485
30	1311	-.156	.087	.171	-.495
30	1312	-.139	.087	.186	-.486
30	1313	-.132	.092	.144	-.448
30	1314	-.143	.094	.124	-.479
30	1315	-.142	.090	.159	-.417
30	1316	-.126	.089	.156	-.402
30	1317	-.133	.082	.141	-.384
30	1318	-.142	.082	.139	-.395
30	1319	-.157	.082	.114	-.419
30	1320	-.142	.083	.124	-.418
30	1321	-.147	.089	.178	-.485
30	1322	-.141	.087	.196	-.433
30	1323	-.157	.087	.181	-.442
30	1324	-.145	.086	.190	-.431
30	1325	-.140	.084	.178	-.455
30	1326	-.146	.086	.170	-.478
30	1327	-.161	.086	.131	-.543
30	1328	-.147	.087	.129	-.575
30	1329	-.145	.090	.135	-.466
30	1330	-.154	.092	.127	-.468
30	1331	-.178	.093	.081	-.485
30	1332	-.165	.092	.154	-.459
30	1333	-.175	.089	.167	-.501
30	1334	-.174	.091	.219	-.520
30	1335	-.195	.092	.241	-.549
30	1336	-.203	.102	.138	-.626
30	1337	-.155	.097	.171	-.548
30	1338	-.161	.091	.126	-.414
30	1339	-.148	.094	.161	-.530
30	1340	-.149	.088	.159	-.413
30	1401	-.118	.140	.433	-.566
30	1402	.044	.151	.614	-.470
30	1403	-.071	.160	.587	-.591
30	1404	.124	.119	.519	-.426
30	1405	.058	.107	.429	-.437
30	1406	-.011	.098	.393	-.328
30	1407	-.037	.093	.321	-.317
30	1408	-.077	.089	.187	-.364
30	1409	-.101	.090	.175	-.383
30	1410	.038	.184	.663	-.564
30	1411	.126	.183	.689	-.513
30	1412	.036	.196	.618	-.663
30	1413	.205	.150	.671	-.462
30	1414	.181	.112	.525	-.382
30	1415	.102	.097	.384	-.257
30	1416	.031	.090	.300	-.269
30	1417	-.041	.081	.226	-.316
30	1418	-.081	.092	.256	-.376
30	1419	.074	.182	.574	-.587
30	1420	.154	.183	.700	-.512
30	1421	.084	.199	.686	-.595
30	1423	.147	.130	.544	-.433
30	1424	.123	.106	.439	-.254
30	1425	.051	.097	.338	-.288
30	1426	-.071	.087	.188	-.362
30	1427	-.100	.085	.169	-.372
30	1428	.084	.175	.572	-.517
30	1429	.122	.179	.677	-.540
30	1430	.110	.195	.790	-.578
30	1431	.137	.148	.620	-.453
30	1432	.124	.138	.592	-.434
30	1433	.099	.116	.496	-.249
30	1434	.039	.092	.329	-.288
30	1435	-.059	.085	.278	-.395
30	1436	-.113	.084	.258	-.438
30	1437	.084	.165	.656	-.654
30	1438	.149	.156	.720	-.513
30	1439	.091	.171	.670	-.593
30	1440	.098	.129	.578	-.520
30	1441	.099	.127	.584	-.392
30	1442	.065	.111	.481	-.315
30	1443	.030	.099	.381	-.321
30	1444	-.062	.083	.218	-.377
30	1445	-.113	.084	.174	-.430
30	1446	.106	.138	.631	-.429
30	1447	.137	.131	.720	-.447
30	1448	.108	.128	.585	-.507
30	1449	.099	.110	.673	-.359
30	1450	.114	.109	.527	-.247
30	1451	.079	.103	.421	-.246
30	1452	.022	.097	.357	-.314
30	1453	-.023	.090	.315	-.346
30	1454	-.045	.090	.224	-.389
30	1455	.187	.118	.708	-.392
30	1456	.160	.122	.639	-.244
30	1457	.190	.116	.669	-.202
30	1458	.145	.126	.606	-.307
30	1459	.161	.116	.626	-.168
30	1460	.063	.119	.542	-.371
30	1461	.055	.106	.460	-.328
30	1462	.043	.102	.435	-.334
30	1463	.060	.099	.493	-.319
30	1464	.430	.228	.990	-.312
30	1465	.223	.112	.691	-.178
30	1466	.185	.107	.567	-.131
30	1467	.206	.105	.565	-.081
30	1801	.096	.072	.361	-.173
30	1802	.072	.078	.348	-.219
30	1803	-.038	.079	.214	-.324
30	1804	-.085	.079	.184	-.353
30	1805	.009	.075	.248	-.214
30	1806	.030	.079	.307	-.243
30	1807	.091	.089	.359	-.184
30	2101	-.161	.103	.157	-.478
30	2102	-.041	.105	.239	-.370
30	2103	.102	.104	.485	-.255
30	2104	.201	.140	.756	-.478
30	2105	-.212	.107	.143	-.548
30	2106	-.187	.108	.180	-.602
30	2107	-.057	.091	.232	-.380
30	2108	-.010	.095	.282	-.339
30	2109	-.081	.111	.398	-.500
30	2110	-.101	.108	.316	-.508
30	2111	-.009	.091	.302	-.307
30	2112	.023	.104	.393	-.371
30	2113	.160	.103	.548	-.244
30	2114	.127	.111	.501	-.168
30	2115	.141	.109	.523	-.137
30	2116	-.146	.093	.194	-.464
30	2117	-.066	.085	.227	-.370
30	2118	-.093	.090	.252	-.457
30	2119	-.149	.103	.125	-.556
30	2120	-.113	.100	.187	-.539
30	2121	-.095	.147	.565	-.685
30	2122	-.013	.091	.339	-.450
30	2123	-.061	.081	.208	-.365
30	2124	.078	.140	.569	-.345
30	2125	.152	.127	.628	-.341
30	2126	-.038	.081	.315	-.328
30	2127	-.001	.080	.295	-.326
30	2128	-.042	.077	.247	-.345
30	2129	.127	.091	.511	-.149
30	2130	.126	.100	.498	-.212
30	2131	-.050	.074	.200	-.307
30	2132	-.068	.074	.188	-.337
30	2133	-.051	.072	.215	-.286
30	2134	-.084	.074	.169	-.379
30	2135	-.074	.090	.243	-.416
30	2136	-.166	.119	.223	-.717
30	2137	-.012	.087	.303	-.333
30	2138	-.070	.097	.254	-.409
30	2139	.130	.093	.550	-.204
30	2140	.057	.099	.438	-.280
30	2141	.029	.090	.350	-.277
30	2142	.055	.083	.369	-.265

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
30	2143	-.041	.077	.232	-.327
30	2144	-.058	.078	.212	-.332
30	2145	-.033	.076	.239	-.295
30	2146	-.070	.076	.219	-.336
30	2147	-.078	.084	.191	-.366
30	2148	-.044	.083	.252	-.300
30	2149	-.057	.082	.231	-.305
30	2150	-.036	.082	.248	-.284
30	2151	-.025	.079	.231	-.288
30	2152	-.046	.080	.228	-.327
30	2153	-.013	.079	.258	-.281
30	2154	-.099	.084	.179	-.409
30	2201	-.200	.092	.175	-.546
30	2202	-.212	.092	.118	-.541
30	2203	-.227	.094	.137	-.575
30	2204	-.213	.092	.113	-.561
30	2205	-.192	.099	.106	-.622
30	2206	-.203	.103	.107	-.632
30	2207	-.230	.103	.080	-.645
30	2208	-.216	.101	.090	-.578
30	2209	-.213	.092	.056	-.543
30	2210	-.215	.096	.068	-.586
30	2211	-.239	.097	.109	-.666
30	2212	-.223	.098	.082	-.608
30	2213	-.156	.094	.192	-.495
30	2214	-.174	.102	.241	-.542
30	2215	-.224	.104	.250	-.664
30	2216	-.221	.100	.161	-.572
30	2217	-.146	.095	.192	-.441
30	2218	-.098	.083	.184	-.456
30	2219	-.151	.089	.150	-.521
30	2220	-.028	.082	.277	-.389
30	2221	-.085	.069	.147	-.364
30	2222	-.087	.091	.184	-.515
30	2224	-.041	.086	.278	-.315
30	2225	-.065	.085	.232	-.336
30	2226	-.023	.084	.291	-.302
30	2227	-.048	.085	.254	-.364
30	2228	-.047	.076	.202	-.329
30	2229	-.044	.073	.211	-.289
30	2230	.065	.083	.275	-.136
30	2231	-.041	.076	.221	-.299
30	2232	-.044	.072	.201	-.299
30	2233	-.063	.072	.176	-.285
30	2234	-.007	.069	.294	-.228
30	2235	-.029	.070	.309	-.269
30	2236	-.033	.078	.286	-.319
30	2237	-.048	.079	.263	-.316
30	2238	-.026	.076	.274	-.278
30	2239	-.040	.080	.271	-.307

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
30	2240	-.047	.085	.221	-.356
30	2301	-.201	.092	.106	-.511
30	2302	-.201	.090	.094	-.489
30	2303	-.069	.083	.197	-.334
30	2304	-.052	.081	.247	-.301
30	2305	-.077	.081	.214	-.342
30	2306	-.087	.086	.235	-.350
30	2307	-.132	.108	.195	-.545
30	2308	-.113	.090	.184	-.494
30	2309	-.181	.085	.107	-.526
30	2310	-.144	.098	.194	-.570
30	2311	-.172	.107	.152	-.680
30	2312	-.124	.085	.171	-.410
30	2313	-.060	.085	.218	-.357
30	2314	-.140	.098	.178	-.649
30	2315	-.082	.084	.177	-.369
30	2401	-.191	.089	.098	-.499
30	2402	-.209	.088	.082	-.501
30	2403	-.210	.088	.097	-.500
30	2404	-.221	.089	.088	-.535
30	2405	-.040	.077	.232	-.319
30	2406	-.067	.079	.223	-.315
30	2407	-.197	.100	.167	-.590
30	2408	-.194	.095	.175	-.521
30	2409	-.189	.087	.092	-.541
30	2411	-.215	.093	.111	-.529
30	2412	-.201	.096	.162	-.489
30	2413	-.188	.092	.128	-.487
30	2414	-.200	.090	.085	-.564
30	2415	-.167	.099	.206	-.646
30	2416	-.163	.090	.107	-.477
30	2417	-.187	.087	.091	-.485
30	2418	-.196	.095	.101	-.511
30	2419	-.217	.096	.099	-.566
30	2420	-.197	.096	.114	-.525
30	2421	-.044	.078	.206	-.316
30	2422	-.070	.087	.197	-.407
30	2423	-.182	.098	.143	-.515
30	2424	-.176	.097	.150	-.667
30	2425	-.183	.097	.164	-.498
30	2426	-.164	.100	.164	-.610
30	2427	-.104	.080	.154	-.395
30	2428	-.085	.090	.201	-.512
30	2429	-.113	.096	.252	-.526
30	2430	-.157	.099	.188	-.532
30	2431	-.133	.093	.135	-.450
30	2432	-.108	.091	.188	-.427
30	2433	-.068	.086	.194	-.354
30	2434	-.031	.086	.255	-.301
30	2435	-.019	.082	.246	-.308

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
30	2436	-.027	.080	.242	-.346
30	2437	-.003	.080	.272	-.298
30	2438	-.035	.083	.240	-.327
30	2439	-.039	.087	.196	-.420
30	2440	-.107	.082	.130	-.434
30	2441	-.022	.078	.258	-.301
30	2442	-.037	.081	.192	-.322
30	2443	-.039	.083	.289	-.326
30	2444	-.094	.091	.261	-.424
30	2445	-.056	.086	.257	-.374
30	2446	-.085	.090	.242	-.483
30	2447	-.011	.094	.408	-.409
30	2448	.001	.102	.441	-.448
30	2449	.006	.085	.354	-.370
30	2450	-.050	.078	.234	-.362
30	2451	-.022	.085	.273	-.332
30	2501	-.194	.099	.135	-.558
30	2502	-.207	.096	.157	-.591
30	2503	-.090	.100	.298	-.402
30	2504	-.205	.101	.137	-.628
30	2505	-.099	.090	.200	-.424
30	2506	-.215	.096	.092	-.540
30	2507	-.228	.097	.116	-.597
30	2508	.008	.101	.351	-.299
30	2509	-.107	.095	.234	-.406
30	2510	-.094	.093	.210	-.389
30	2511	-.200	.091	.103	-.544
30	2601	-.007	.163	.544	-.735
30	2602	.072	.091	.456	-.273
30	2603	-.001	.090	.366	-.281
30	2604	.036	.088	.413	-.249
30	2605	-.004	.086	.294	-.304
30	2606	.090	.110	.510	-.254
30	2607	.162	.118	.607	-.189
30	2608	.035	.152	.497	-.784
30	2609	.069	.089	.392	-.237
30	2610	.065	.083	.481	-.210
30	2611	-.015	.089	.362	-.336
30	2612	-.025	.084	.275	-.359
30	2613	.072	.102	.578	-.219
30	2614	.264	.111	.729	-.169
30	2615	-.023	.095	.283	-.399
30	2616	.055	.081	.338	-.219
30	2617	.049	.087	.357	-.257
30	2618	.042	.086	.352	-.274
30	2619	-.077	.092	.258	-.433
30	2620	.081	.096	.410	-.268
30	2621	.212	.128	.720	-.114
30	5102	.260	.154	.827	-.232
30	5103	.110	.110	.583	-.298

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
30	5104	.234	.145	.713	-.252
30	5105	.046	.100	.422	-.314
30	5106	.139	.138	.798	-.264
30	5107	-.034	.083	.310	-.319
30	5108	.020	.093	.502	-.392
30	5109	.037	.106	.461	-.570
30	5110	.165	.133	.745	-.283
30	5111	-.020	.089	.297	-.421
30	5112	.051	.084	.347	-.276
30	5114	.122	.103	.512	-.264
30	5202	-.103	.088	.163	-.504
30	5203	-.113	.080	.187	-.412
30	5204	-.127	.100	.142	-.602
30	5301	.015	.148	.477	-.625
30	5302	-.095	.136	.333	-.707
30	5303	-.056	.132	.317	-.835
30	5304	-.004	.099	.476	-.413
30	5305	-.097	.112	.352	-.619
30	5901	-.044	.100	.351	-.407
30	5902	-.254	.155	.225	-.989
30	6101	-.069	.085	.204	-.395
30	6102	-.025	.079	.230	-.285
30	6103	-.037	.081	.235	-.335
30	6104	-.030	.082	.320	-.328
30	6105	-.059	.085	.273	-.373
30	6106	-.012	.080	.299	-.303
30	6201	-.040	.085	.336	-.385
30	6301	-.004	.083	.317	-.307
30	6302	-.023	.083	.327	-.314
30	6901	-.051	.081	.221	-.388
30	7101	-.088	.082	.156	-.391
30	7102	-.090	.081	.167	-.427
30	7103	-.122	.128	.299	-.706
30	7104	-.072	.076	.165	-.385
30	7105	-.008	.090	.407	-.297
30	7106	-.085	.077	.188	-.346
30	7201	-.019	.085	.410	-.285
30	7301	-.091	.080	.179	-.397
30	9101	-.228	.099	.053	-.587
30	9102	-.139	.121	.320	-.593
30	9103	-.119	.130	.293	-.541
30	9104	.061	.124	.658	-.443
30	9105	-.218	.103	.141	-.612
30	9106	-.030	.113	.379	-.486
30	9107	-.245	.100	.099	-.642
30	9108	-.195	.095	.119	-.498
30	9109	-.198	.103	.138	-.500
30	9110	.005	.082	.285	-.333
30	9111	-.184	.101	.185	-.478
30	9112	-.048	.096	.230	-.486

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
30	9113	-.227	.110	.157	-.539
30	9114	-.218	.101	.097	-.525
30	9115	-.209	.096	.125	-.505
30	9116	-.196	.100	.168	-.614
30	9117	-.215	.098	.210	-.567
30	9118	-.011	.083	.220	-.341
30	9119	-.014	.089	.293	-.344
30	9120	-.198	.099	.179	-.530
30	9121	-.199	.099	.095	-.548
30	9122	-.183	.101	.117	-.534
30	9123	-.008	.092	.260	-.348
30	9124	-.118	.102	.311	-.571
30	9125	-.139	.091	.166	-.506
30	9126	-.173	.100	.159	-.594
30	9201	.004	.113	.450	-.381
30	9202	.067	.109	.476	-.294
30	9203	-.006	.095	.416	-.290
30	9204	-.097	.085	.189	-.397
30	9205	-.061	.078	.223	-.369
30	9206	-.008	.075	.277	-.298
30	9207	-.183	.098	.152	-.484
30	9208	-.205	.102	.164	-.595
30	9209	-.141	.100	.183	-.546
30	9210	-.085	.101	.233	-.481
30	9211	-.069	.077	.184	-.337
30	9212	-.195	.097	.123	-.530
30	9213	-.047	.081	.201	-.338
30	9214	-.099	.106	.294	-.512
30	9215	-.049	.094	.291	-.371
30	9216	-.059	.085	.280	-.336
30	9217	-.056	.087	.250	-.311
30	9218	-.063	.086	.226	-.314
30	9219	-.229	.097	.079	-.579
30	9220	-.221	.100	.084	-.602
30	9221	-.213	.097	.108	-.557
30	9222	-.051	.119	.401	-.623
30	9223	-.026	.088	.297	-.284
30	9224	-.027	.082	.268	-.271
30	9225	-.219	.093	.102	-.525
30	9226	-.231	.099	.084	-.634
30	9227	-.161	.112	.248	-.661
30	9228	.005	.090	.380	-.266
30	9229	-.226	.093	.099	-.616
30	9230	-.085	.095	.224	-.551
30	9231	-.015	.079	.286	-.290
30	9232	-.233	.102	.077	-.644
30	9233	-.188	.101	.123	-.542
30	9234	-.155	.100	.133	-.546
30	9235	-.011	.086	.278	-.295
30	9236	-.156	.098	.176	-.554

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
30	9237	-.006	.087	.295	-.310
30	9238	-.028	.081	.258	-.294
40	1101	-.003	.106	.502	-.347
40	1102	.045	.114	.572	-.317
40	1103	.101	.119	.515	-.335
40	1104	.146	.125	.568	-.385
40	1105	.225	.132	.711	-.164
40	1106	.295	.138	.734	-.185
40	1107	.320	.142	.772	-.202
40	1108	-.024	.098	.344	-.409
40	1109	.074	.104	.453	-.276
40	1110	.213	.126	.632	-.196
40	1111	.301	.140	.753	-.139
40	1112	.378	.156	.870	-.166
40	1113	.402	.150	1.004	-.090
40	1114	.338	.144	.881	-.236
40	1115	-.039	.090	.264	-.310
40	1116	.035	.094	.329	-.284
40	1117	.189	.113	.606	-.239
40	1118	.282	.129	.736	-.139
40	1119	.357	.144	.887	-.118
40	1120	.379	.152	.978	-.137
40	1121	.327	.147	.778	-.174
40	1122	-.059	.096	.283	-.363
40	1123	.014	.098	.382	-.309
40	1124	.145	.110	.540	-.254
40	1125	.243	.125	.697	-.179
40	1126	.315	.148	.832	-.209
40	1127	.328	.159	1.019	-.184
40	1128	.260	.151	.932	-.209
40	1129	-.085	.089	.182	-.384
40	1130	-.025	.094	.267	-.369
40	1131	.089	.108	.470	-.291
40	1132	.164	.127	.633	-.207
40	1133	.206	.151	.694	-.215
40	1134	.210	.166	.771	-.225
40	1135	.166	.156	.668	-.270
40	1136	-.092	.087	.193	-.387
40	1137	-.022	.083	.255	-.286
40	1138	.038	.092	.377	-.265
40	1139	.073	.110	.529	-.240
40	1140	.096	.126	.599	-.246
40	1141	.125	.136	.748	-.229
40	1142	.105	.136	.774	-.309
40	1143	.059	.091	.381	-.269
40	1144	.055	.094	.383	-.275
40	1145	.078	.098	.421	-.290
40	1146	.069	.111	.442	-.331
40	1147	.051	.128	.452	-.597
40	1148	.016	.114	.444	-.623

APPENDIX A -- PRESSURE DATA: CONFIGURATION A: HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
40	1149	.034	.100	.460	-.537
40	1150	.105	.101	.471	-.240
40	1151	.079	.102	.474	-.257
40	1152	.014	.096	.562	-.286
40	1201	-.159	.109	.280	-.584
40	1202	-.143	.100	.300	-.537
40	1203	-.191	.123	.189	-.666
40	1204	-.191	.122	.186	-.804
40	1205	-.191	.119	.184	-.778
40	1206	-.186	.108	.171	-.704
40	1207	-.180	.105	.186	-.774
40	1208	-.161	.097	.197	-.497
40	1209	-.163	.099	.235	-.530
40	1210	-.217	.102	.133	-.646
40	1211	-.142	.093	.191	-.555
40	1212	-.181	.106	.226	-.542
40	1213	-.173	.101	.222	-.546
40	1214	-.180	.098	.114	-.585
40	1215	-.173	.096	.141	-.512
40	1216	-.165	.094	.154	-.538
40	1217	-.156	.091	.160	-.505
40	1218	-.142	.096	.179	-.473
40	1219	-.182	.091	.090	-.512
40	1220	-.159	.088	.120	-.460
40	1221	-.190	.101	.148	-.574
40	1222	-.152	.092	.119	-.493
40	1223	-.129	.087	.149	-.436
40	1224	-.162	.101	.204	-.516
40	1225	-.153	.101	.180	-.485
40	1226	-.147	.101	.177	-.457
40	1227	-.143	.100	.192	-.449
40	1228	-.253	.096	.034	-.574
40	1229	-.177	.090	.096	-.485
40	1230	-.185	.101	.142	-.514
40	1231	-.180	.099	.140	-.474
40	1232	-.180	.097	.146	-.471
40	1233	-.164	.092	.174	-.452
40	1234	-.147	.088	.132	-.457
40	1235	-.140	.090	.162	-.438
40	1236	-.141	.089	.148	-.431
40	1237	-.191	.095	.081	-.605
40	1238	-.166	.093	.086	-.561
40	1239	-.201	.097	.108	-.511
40	1240	-.192	.101	.195	-.569
40	1241	-.193	.102	.192	-.590
40	1242	-.185	.098	.167	-.496
40	1243	-.169	.096	.135	-.492
40	1244	-.166	.095	.117	-.485
40	1245	-.166	.097	.126	-.493
40	1246	-.243	.100	.035	-.722
40	1247	-.177	.093	.087	-.489
40	1248	-.210	.102	.076	-.542
40	1249	-.203	.100	.105	-.515
40	1250	-.201	.091	.079	-.559
40	1251	-.201	.093	.073	-.566
40	1252	-.185	.090	.080	-.509
40	1253	-.178	.091	.075	-.522
40	1254	-.168	.092	.132	-.482
40	1301	-.109	.087	.187	-.378
40	1302	-.119	.089	.187	-.391
40	1303	-.131	.094	.205	-.440
40	1304	-.112	.094	.174	-.630
40	1305	-.109	.097	.184	-.520
40	1306	-.128	.094	.176	-.507
40	1307	-.143	.098	.161	-.560
40	1308	-.100	.086	.189	-.409
40	1309	-.100	.086	.151	-.394
40	1310	-.110	.085	.146	-.402
40	1311	-.120	.085	.138	-.407
40	1312	-.109	.086	.149	-.405
40	1313	-.119	.090	.184	-.511
40	1314	-.138	.093	.168	-.534
40	1315	-.116	.086	.169	-.419
40	1316	-.104	.085	.178	-.402
40	1317	-.107	.086	.156	-.438
40	1318	-.117	.087	.147	-.450
40	1319	-.130	.088	.149	-.457
40	1320	-.126	.089	.149	-.457
40	1321	-.130	.086	.121	-.415
40	1322	-.109	.086	.147	-.420
40	1323	-.120	.085	.135	-.433
40	1324	-.112	.084	.143	-.410
40	1325	-.110	.079	.190	-.370
40	1326	-.117	.082	.177	-.383
40	1327	-.134	.081	.169	-.392
40	1328	-.133	.082	.181	-.385
40	1329	-.110	.085	.151	-.394
40	1330	-.119	.086	.140	-.423
40	1331	-.138	.087	.119	-.431
40	1332	-.123	.087	.148	-.426
40	1333	-.118	.080	.213	-.367
40	1334	-.124	.080	.215	-.385
40	1335	-.147	.081	.194	-.398
40	1336	-.164	.089	.164	-.552
40	1337	-.117	.085	.196	-.490
40	1338	-.128	.087	.261	-.408
40	1339	-.105	.080	.167	-.429
40	1340	-.111	.084	.251	-.389
40	1401	-.220	.105	.148	-.650
40	1402	-.130	.130	.450	-.571
40	1403	-.214	.113	.313	-.733
40	1404	.012	.145	.460	-.540
40	1405	-.021	.111	.400	-.510
40	1406	-.051	.088	.307	-.422
40	1407	-.062	.085	.252	-.424
40	1408	-.082	.082	.230	-.399
40	1409	-.096	.085	.227	-.423
40	1410	-.180	.128	.221	-.724
40	1411	-.135	.151	.492	-.577
40	1412	-.181	.147	.432	-.652
40	1413	.015	.195	.629	-.673
40	1414	.057	.146	.463	-.611
40	1415	.030	.088	.332	-.441
40	1416	-.015	.081	.267	-.306
40	1417	-.052	.079	.228	-.354
40	1418	-.081	.075	.186	-.317
40	1419	-.163	.143	.444	-.614
40	1420	-.100	.152	.527	-.531
40	1421	-.145	.151	.325	-.692
40	1423	.008	.144	.365	-.689
40	1424	.037	.090	.349	-.333
40	1425	-.006	.083	.288	-.256
40	1426	-.082	.078	.160	-.365
40	1427	-.093	.078	.149	-.374
40	1428	-.140	.147	.392	-.635
40	1429	-.100	.144	.479	-.580
40	1430	-.140	.149	.357	-.653
40	1431	-.024	.158	.416	-.540
40	1432	-.013	.130	.361	-.549
40	1433	.013	.086	.265	-.393
40	1434	-.012	.082	.277	-.354
40	1435	-.074	.079	.179	-.324
40	1436	-.109	.079	.157	-.363
40	1437	-.105	.138	.323	-.600
40	1438	-.037	.135	.367	-.476
40	1439	-.098	.152	.430	-.675
40	1440	-.002	.120	.418	-.441
40	1441	.004	.110	.415	-.411
40	1442	-.008	.091	.294	-.296
40	1443	-.020	.086	.263	-.293
40	1444	-.069	.086	.241	-.325
40	1445	-.095	.088	.232	-.355
40	1446	-.040	.133	.331	-.592
40	1447	.019	.123	.472	-.479
40	1448	-.026	.132	.355	-.518
40	1449	.030	.105	.493	-.416
40	1450	.030	.097	.330	-.427
40	1451	-.000	.092	.342	-.397
40	1452	-.035	.089	.292	-.320
40	1453	-.046	.085	.255	-.314

APPENDIX A -- PRESSURE DATA: CONFIGURATION A) HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
40	1454	-.059	.084	.204	-.348
40	1455	.086	.106	.481	-.351
40	1456	.043	.105	.438	-.355
40	1457	.080	.099	.453	-.331
40	1458	.022	.109	.424	-.356
40	1459	.053	.101	.433	-.361
40	1460	-.026	.111	.364	-.402
40	1461	-.008	.107	.390	-.397
40	1462	-.005	.088	.274	-.348
40	1463	.008	.087	.264	-.340
40	1464	.399	.200	1.012	-.293
40	1465	.137	.090	.437	-.147
40	1466	.138	.094	.455	-.209
40	1467	.155	.092	.469	-.176
40	1801	.079	.075	.353	-.184
40	1802	.055	.077	.292	-.217
40	1803	-.043	.076	.208	-.358
40	1804	-.072	.080	.169	-.387
40	1805	.007	.079	.260	-.257
40	1806	.018	.077	.276	-.267
40	1807	.069	.079	.348	-.214
40	2101	-.155	.092	.147	-.497
40	2102	-.027	.087	.238	-.357
40	2103	.022	.100	.440	-.377
40	2104	.119	.159	.766	-.288
40	2105	-.194	.097	.151	-.626
40	2106	-.153	.097	.189	-.531
40	2107	-.037	.083	.256	-.320
40	2108	.001	.084	.351	-.289
40	2109	-.041	.123	.367	-.479
40	2110	-.060	.110	.362	-.453
40	2111	.026	.089	.332	-.275
40	2112	.038	.088	.395	-.234
40	2113	.065	.090	.367	-.261
40	2114	.034	.086	.378	-.295
40	2115	.058	.088	.356	-.242
40	2116	-.099	.091	.170	-.437
40	2117	-.032	.086	.236	-.418
40	2118	-.051	.085	.256	-.371
40	2119	-.071	.088	.214	-.428
40	2120	-.096	.093	.199	-.496
40	2121	-.066	.113	.569	-.444
40	2122	-.007	.089	.301	-.337
40	2123	-.056	.094	.221	-.456
40	2124	-.020	.125	.400	-.413
40	2125	.140	.115	.588	-.281
40	2126	-.013	.094	.405	-.289
40	2127	.035	.096	.642	-.251
40	2128	-.027	.089	.257	-.288
40	2129	.061	.083	.351	-.219

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
40	2130	.062	.083	.500	-.184
40	2131	-.045	.078	.221	-.338
40	2132	-.060	.079	.198	-.347
40	2133	-.021	.076	.238	-.291
40	2134	-.058	.077	.187	-.325
40	2135	-.060	.083	.251	-.331
40	2136	-.104	.092	.237	-.586
40	2137	.013	.089	.349	-.292
40	2138	-.048	.083	.262	-.316
40	2139	.083	.080	.421	-.158
40	2140	.008	.088	.379	-.295
40	2141	-.013	.083	.340	-.350
40	2142	.051	.089	.390	-.248
40	2143	-.045	.073	.228	-.305
40	2144	-.059	.074	.216	-.317
40	2145	-.020	.072	.247	-.259
40	2146	-.056	.075	.227	-.317
40	2147	-.059	.077	.257	-.357
40	2148	-.060	.078	.218	-.339
40	2149	-.030	.074	.262	-.316
40	2150	-.016	.077	.359	-.293
40	2151	.000	.080	.372	-.263
40	2152	-.033	.077	.285	-.290
40	2153	-.018	.073	.281	-.253
40	2154	-.069	.075	.232	-.352
40	2201	-.186	.093	.108	-.548
40	2202	-.201	.092	.083	-.554
40	2203	-.209	.093	.095	-.585
40	2204	-.213	.099	.073	-.662
40	2205	-.198	.108	.171	-.652
40	2206	-.152	.101	.166	-.632
40	2207	-.177	.099	.194	-.562
40	2208	-.214	.111	.154	-.689
40	2209	-.213	.107	.134	-.588
40	2210	-.216	.106	.116	-.612
40	2211	-.225	.112	.101	-.680
40	2212	-.190	.111	.206	-.618
40	2213	-.085	.091	.341	-.415
40	2214	-.092	.098	.319	-.480
40	2215	-.162	.097	.230	-.625
40	2216	-.180	.094	.202	-.563
40	2217	-.102	.089	.218	-.463
40	2218	-.058	.080	.225	-.315
40	2219	-.098	.083	.195	-.550
40	2220	-.009	.083	.286	-.308
40	2221	-.053	.068	.195	-.277
40	2222	-.050	.094	.204	-.546
40	2224	-.007	.088	.429	-.277
40	2225	-.034	.087	.290	-.317
40	2226	.007	.080	.270	-.272

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
40	2227	-.026	.083	.256	-.295
40	2228	-.031	.087	.263	-.435
40	2229	-.035	.085	.196	-.381
40	2230	-.056	.061	.104	-.195
40	2231	-.038	.090	.249	-.385
40	2232	-.034	.084	.260	-.442
40	2233	-.059	.085	.221	-.500
40	2234	.011	.078	.281	-.230
40	2235	-.020	.080	.256	-.272
40	2236	-.020	.084	.265	-.322
40	2237	-.034	.085	.262	-.353
40	2238	-.012	.081	.286	-.306
40	2239	-.020	.084	.306	-.302
40	2240	-.036	.085	.228	-.330
40	2301	-.147	.088	.125	-.420
40	2302	-.163	.091	.136	-.616
40	2303	-.058	.077	.215	-.308
40	2304	-.045	.077	.202	-.295
40	2305	-.072	.080	.180	-.351
40	2306	-.076	.083	.256	-.409
40	2307	-.110	.100	.224	-.594
40	2308	-.097	.091	.223	-.408
40	2309	-.164	.088	.127	-.480
40	2310	-.082	.083	.225	-.400
40	2311	-.134	.101	.164	-.632
40	2312	-.083	.084	.200	-.383
40	2313	-.026	.085	.239	-.301
40	2314	-.094	.091	.195	-.441
40	2315	-.051	.081	.267	-.301
40	2401	-.128	.082	.151	-.416
40	2402	-.149	.081	.105	-.439
40	2403	-.157	.081	.101	-.446
40	2404	-.222	.092	.068	-.562
40	2405	-.034	.078	.237	-.294
40	2406	-.057	.079	.226	-.347
40	2407	-.130	.091	.164	-.476
40	2408	-.140	.089	.171	-.436
40	2409	-.174	.092	.139	-.512
40	2411	-.148	.084	.112	-.444
40	2412	-.141	.088	.151	-.447
40	2413	-.151	.099	.188	-.513
40	2414	-.174	.093	.136	-.479
40	2415	-.113	.088	.199	-.571
40	2416	-.120	.080	.112	-.391
40	2417	-.139	.079	.103	-.399
40	2418	-.152	.101	.147	-.576
40	2419	-.162	.099	.115	-.754
40	2420	-.119	.099	.213	-.475
40	2421	-.027	.071	.214	-.245
40	2422	-.061	.076	.203	-.299

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
40	2423	-.126	.095	.243	-.462
40	2424	-.125	.095	.229	-.462
40	2425	-.128	.096	.227	-.447
40	2426	-.122	.099	.239	-.450
40	2427	-.054	.077	.213	-.330
40	2428	-.060	.078	.190	-.399
40	2429	-.051	.084	.233	-.428
40	2430	-.096	.088	.195	-.439
40	2431	-.089	.082	.208	-.391
40	2432	-.069	.082	.198	-.348
40	2433	-.033	.078	.254	-.289
40	2434	-.007	.081	.291	-.283
40	2435	-.002	.080	.239	-.273
40	2436	-.001	.075	.231	-.277
40	2437	.014	.078	.255	-.237
40	2438	-.014	.079	.217	-.277
40	2439	-.013	.078	.265	-.312
40	2440	-.065	.080	.220	-.393
40	2441	.006	.075	.281	-.299
40	2442	-.012	.077	.277	-.321
40	2443	-.006	.078	.239	-.258
40	2444	-.054	.082	.198	-.342
40	2445	-.026	.078	.211	-.301
40	2446	-.053	.080	.185	-.327
40	2447	-.010	.081	.279	-.290
40	2448	-.002	.080	.342	-.256
40	2449	.022	.077	.306	-.253
40	2450	-.022	.073	.232	-.279
40	2451	.020	.076	.298	-.253
40	2501	-.139	.093	.182	-.463
40	2502	-.162	.089	.162	-.521
40	2503	-.092	.092	.249	-.437
40	2504	-.144	.095	.175	-.532
40	2505	-.084	.089	.210	-.390
40	2506	-.172	.094	.116	-.552
40	2507	-.152	.098	.139	-.637
40	2508	-.034	.099	.319	-.352
40	2509	-.089	.089	.214	-.446
40	2510	-.077	.088	.221	-.455
40	2511	-.120	.093	.199	-.436
40	2601	-.006	.133	.453	-.547
40	2602	.049	.088	.416	-.242
40	2603	-.016	.077	.257	-.289
40	2604	.027	.076	.296	-.242
40	2605	-.008	.081	.302	-.291
40	2606	.027	.085	.349	-.253
40	2607	.065	.104	.495	-.229
40	2608	.071	.116	.436	-.478
40	2609	.051	.086	.390	-.282
40	2610	.049	.081	.379	-.273
40	2611	-.028	.086	.337	-.416
40	2612	-.016	.082	.349	-.335
40	2613	.036	.084	.306	-.269
40	2614	.195	.100	.550	-.130
40	2615	-.028	.090	.331	-.387
40	2616	.040	.079	.265	-.246
40	2617	.046	.076	.310	-.233
40	2618	.043	.073	.308	-.215
40	2619	-.064	.079	.233	-.367
40	2620	.060	.082	.377	-.241
40	2621	.128	.096	.517	-.214
40	5102	.219	.136	.811	-.157
40	5103	.079	.101	.574	-.266
40	5104	.202	.125	.747	-.187
40	5105	.034	.094	.369	-.262
40	5106	.110	.123	.662	-.270
40	5107	-.018	.080	.286	-.295
40	5108	.011	.088	.308	-.347
40	5109	.020	.098	.395	-.324
40	5110	.142	.116	.672	-.197
40	5111	-.012	.082	.290	-.340
40	5112	.036	.079	.263	-.240
40	5114	.144	.114	.593	-.173
40	5202	-.057	.080	.217	-.308
40	5203	-.056	.084	.235	-.306
40	5204	-.072	.086	.180	-.493
40	5301	.024	.156	.551	-.760
40	5302	-.074	.128	.342	-.668
40	5303	-.036	.111	.357	-.617
40	5304	.001	.091	.350	-.319
40	5305	-.080	.105	.269	-.532
40	5901	-.026	.108	.453	-.671
40	5902	-.244	.157	.208	-.923
40	6101	-.040	.084	.273	-.339
40	6102	-.017	.082	.289	-.341
40	6103	-.034	.079	.271	-.323
40	6104	-.021	.076	.256	-.293
40	6105	-.073	.079	.205	-.347
40	6106	-.004	.076	.253	-.274
40	6201	-.028	.081	.261	-.306
40	6301	-.016	.084	.260	-.316
40	6302	-.038	.082	.219	-.351
40	6901	-.033	.081	.219	-.326
40	7101	-.060	.077	.199	-.350
40	7102	-.060	.078	.204	-.374
40	7103	-.065	.106	.254	-.551
40	7104	-.047	.073	.191	-.304
40	7105	-.037	.090	.285	-.317
40	7106	-.057	.082	.212	-.322
40	7201	-.029	.087	.336	-.309
40	7301	-.066	.085	.174	-.429
40	9101	-.245	.106	.070	-.673
40	9102	-.099	.139	.376	-.704
40	9103	-.162	.128	.267	-.689
40	9104	-.037	.107	.340	-.419
40	9105	-.208	.110	.151	-.586
40	9106	-.081	.114	.260	-.480
40	9107	-.212	.106	.121	-.570
40	9108	-.135	.091	.178	-.530
40	9109	-.138	.084	.117	-.534
40	9110	-.030	.075	.230	-.322
40	9111	-.131	.085	.130	-.464
40	9112	-.035	.090	.256	-.427
40	9113	-.149	.092	.139	-.550
40	9114	-.159	.086	.111	-.589
40	9115	-.166	.090	.177	-.565
40	9116	-.148	.088	.102	-.467
40	9117	-.164	.089	.174	-.521
40	9118	-.027	.081	.262	-.334
40	9119	-.034	.082	.241	-.307
40	9120	-.151	.091	.141	-.466
40	9121	-.152	.095	.153	-.602
40	9122	-.113	.090	.184	-.452
40	9123	.006	.087	.291	-.303
40	9124	-.079	.087	.257	-.403
40	9125	-.108	.094	.197	-.518
40	9126	-.134	.100	.180	-.543
40	9201	-.037	.115	.400	-.434
40	9202	.108	.106	.529	-.212
40	9203	.011	.091	.348	-.316
40	9204	-.081	.101	.266	-.704
40	9205	-.026	.087	.243	-.309
40	9206	.022	.085	.305	-.264
40	9207	-.174	.097	.134	-.552
40	9208	-.186	.102	.137	-.723
40	9209	-.097	.093	.181	-.429
40	9210	-.034	.098	.286	-.502
40	9211	-.049	.082	.223	-.417
40	9212	-.182	.095	.094	-.601
40	9213	-.044	.084	.251	-.340
40	9214	-.063	.104	.329	-.478
40	9215	-.003	.092	.392	-.362
40	9216	-.037	.084	.282	-.419
40	9217	-.038	.082	.276	-.326
40	9218	-.051	.087	.275	-.344
40	9219	-.207	.091	.066	-.554
40	9220	-.200	.097	.107	-.580
40	9221	-.166	.106	.220	-.506
40	9222	-.010	.098	.405	-.449
40	9223	-.019	.082	.234	-.288

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
40	9224	-.005	.078	.333	-.279
40	9225	-.187	.104	.199	-.540
40	9226	-.180	.108	.192	-.574
40	9227	-.073	.104	.366	-.468
40	9228	.020	.079	.296	-.272
40	9229	-.203	.104	.185	-.579
40	9230	-.029	.084	.240	-.363
40	9231	-.002	.081	.391	-.266
40	9232	-.200	.112	.165	-.583
40	9233	-.129	.100	.170	-.498
40	9234	-.102	.104	.316	-.611
40	9235	.004	.079	.357	-.305
40	9236	-.114	.092	.157	-.488
40	9237	.006	.081	.312	-.297
40	9238	-.008	.084	.341	-.435
50	1101	.014	.142	.552	-.428
50	1102	.061	.150	.738	-.408
50	1103	.113	.153	.693	-.385
50	1104	.161	.156	.738	-.330
50	1105	.198	.161	.740	-.435
50	1106	.256	.164	.779	-.284
50	1107	.263	.169	.797	-.370
50	1108	-.033	.107	.436	-.476
50	1109	.054	.113	.498	-.355
50	1110	.165	.131	.646	-.261
50	1111	.238	.146	.787	-.256
50	1112	.311	.162	.882	-.245
50	1113	.351	.184	.909	-.260
50	1114	.285	.175	.817	-.373
50	1115	-.052	.100	.357	-.414
50	1116	.010	.103	.427	-.300
50	1117	.144	.119	.600	-.213
50	1118	.225	.136	.635	-.161
50	1119	.296	.152	.744	-.229
50	1120	.322	.165	.865	-.245
50	1121	.262	.166	.832	-.288
50	1122	-.067	.091	.270	-.440
50	1123	-.013	.093	.284	-.362
50	1124	.088	.110	.445	-.258
50	1125	.147	.118	.616	-.240
50	1126	.209	.140	.725	-.240
50	1127	.236	.155	.748	-.308
50	1128	.186	.152	.804	-.338
50	1129	-.083	.096	.236	-.470
50	1130	-.036	.097	.367	-.375
50	1131	.043	.108	.438	-.249
50	1132	.105	.124	.584	-.276
50	1133	.171	.142	.668	-.328
50	1134	.194	.161	.752	-.490
50	1135	.152	.155	.729	-.891
50	1136	-.088	.105	.237	-.641
50	1137	-.028	.092	.266	-.465
50	1138	.008	.094	.310	-.596
50	1139	.029	.103	.457	-.413
50	1140	.045	.110	.523	-.352
50	1141	.075	.118	.574	-.284
50	1142	.063	.124	.624	-.358
50	1143	.041	.083	.298	-.279
50	1144	.034	.085	.307	-.284
50	1145	.038	.088	.302	-.341
50	1146	.023	.096	.346	-.392
50	1147	.030	.106	.416	-.852
50	1148	-.000	.096	.595	-.506
50	1149	.002	.087	.413	-.362
50	1150	.056	.099	.406	-.237
50	1151	.044	.094	.449	-.289
50	1152	.008	.088	.407	-.267
50	1201	-.125	.129	.285	-.681
50	1202	-.124	.114	.234	-.548
50	1203	-.169	.126	.222	-.712
50	1204	-.174	.147	.248	-.923
50	1205	-.173	.146	.271	-.811
50	1206	-.181	.138	.343	-.903
50	1207	-.183	.137	.256	-.733
50	1208	-.162	.113	.205	-.693
50	1209	-.162	.113	.198	-.666
50	1210	-.198	.123	.201	-.644
50	1211	-.117	.103	.205	-.472
50	1212	-.142	.103	.205	-.590
50	1213	-.145	.105	.201	-.600
50	1214	-.144	.112	.223	-.780
50	1215	-.160	.121	.268	-.683
50	1216	-.165	.123	.322	-.789
50	1217	-.151	.117	.329	-.697
50	1218	-.140	.107	.178	-.539
50	1219	-.145	.104	.207	-.458
50	1220	-.123	.098	.160	-.424
50	1221	-.150	.106	.210	-.681
50	1222	-.129	.098	.218	-.518
50	1223	-.117	.101	.236	-.453
50	1224	-.146	.106	.237	-.632
50	1225	-.143	.108	.216	-.591
50	1226	-.137	.103	.193	-.561
50	1227	-.130	.102	.201	-.534
50	1228	-.221	.106	.075	-.630
50	1229	-.139	.096	.128	-.536
50	1230	-.155	.106	.175	-.586
50	1231	-.163	.107	.189	-.543
50	1232	-.165	.104	.189	-.500
50	1233	-.159	.100	.157	-.546
50	1234	-.144	.102	.158	-.607
50	1235	-.135	.101	.174	-.572
50	1236	-.135	.099	.194	-.564
50	1237	-.161	.119	.186	-.594
50	1238	-.126	.105	.179	-.493
50	1239	-.160	.103	.182	-.586
50	1240	-.169	.107	.150	-.573
50	1241	-.171	.107	.162	-.529
50	1242	-.189	.111	.157	-.694
50	1243	-.183	.112	.170	-.620
50	1244	-.155	.110	.176	-.994
50	1245	-.153	.110	.182	-.957
50	1246	-.177	.117	.201	-.619
50	1247	-.106	.104	.223	-.511
50	1248	-.115	.093	.166	-.416
50	1249	-.122	.096	.184	-.513
50	1250	-.136	.103	.176	-.566
50	1251	-.162	.115	.189	-.709
50	1252	-.177	.121	.192	-.687
50	1253	-.183	.137	.159	-1.028
50	1254	-.174	.131	.205	-1.025
50	1301	-.068	.089	.221	-.376
50	1302	-.077	.090	.210	-.396
50	1303	-.077	.090	.210	-.415
50	1304	-.069	.088	.230	-.705
50	1305	-.071	.088	.229	-.402
50	1306	-.091	.091	.244	-.482
50	1307	-.099	.096	.244	-.520
50	1308	-.066	.080	.220	-.347
50	1309	-.066	.091	.251	-.378
50	1310	-.075	.090	.245	-.386
50	1311	-.080	.089	.248	-.377
50	1312	-.078	.090	.266	-.378
50	1313	-.085	.087	.192	-.372
50	1314	-.108	.093	.192	-.436
50	1315	-.074	.083	.228	-.351
50	1316	-.067	.082	.235	-.344
50	1317	-.070	.081	.222	-.313
50	1318	-.082	.081	.215	-.330
50	1319	-.090	.081	.192	-.333
50	1320	-.096	.084	.184	-.360
50	1321	-.107	.090	.177	-.437
50	1322	-.074	.086	.218	-.380
50	1323	-.078	.085	.197	-.375
50	1324	-.075	.084	.196	-.374
50	1325	-.071	.078	.168	-.404
50	1326	-.085	.080	.148	-.446
50	1327	-.103	.081	.138	-.442
50	1328	-.109	.083	.147	-.433
50	1329	-.063	.084	.164	-.478

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
50	1330	-.074	.086	.163	-.486
50	1331	-.086	.085	.149	-.395
50	1332	-.074	.082	.148	-.376
50	1333	-.070	.080	.172	-.385
50	1334	-.091	.083	.142	-.440
50	1335	-.110	.087	.131	-.432
50	1336	-.121	.096	.188	-.602
50	1337	-.073	.092	.229	-.492
50	1338	-.068	.089	.200	-.389
50	1339	-.058	.087	.252	-.341
50	1340	-.054	.087	.226	-.338
50	1401	-.258	.119	.137	-.876
50	1402	-.188	.129	.329	-.590
50	1403	-.228	.128	.255	-.719
50	1404	-.057	.150	.396	-.618
50	1405	-.061	.118	.380	-.579
50	1406	-.055	.091	.267	-.458
50	1407	-.054	.091	.240	-.411
50	1408	-.058	.089	.228	-.512
50	1409	-.068	.092	.238	-.514
50	1410	-.235	.126	.185	-.671
50	1411	-.201	.138	.428	-.720
50	1412	-.231	.141	.363	-.714
50	1413	-.079	.183	.537	-.610
50	1414	-.021	.139	.360	-.522
50	1415	-.005	.088	.274	-.336
50	1416	-.027	.080	.241	-.327
50	1417	-.041	.078	.190	-.337
50	1418	-.057	.083	.232	-.380
50	1419	-.220	.141	.321	-.761
50	1420	-.153	.146	.397	-.741
50	1421	-.201	.155	.388	-.825
50	1423	-.053	.137	.326	-.590
50	1424	.004	.090	.413	-.340
50	1425	-.021	.083	.381	-.327
50	1426	-.060	.080	.280	-.310
50	1427	-.061	.080	.266	-.309
50	1428	-.190	.142	.303	-.762
50	1429	-.140	.149	.486	-.840
50	1430	-.150	.146	.364	-.818
50	1431	-.039	.150	.502	-.759
50	1432	-.031	.122	.382	-.763
50	1433	-.008	.084	.270	-.338
50	1434	-.022	.082	.268	-.297
50	1435	-.058	.080	.227	-.377
50	1436	-.073	.078	.181	-.384
50	1437	-.152	.141	.342	-.887
50	1438	-.075	.139	.589	-.573
50	1439	-.147	.133	.324	-.648
50	1440	-.025	.129	.370	-.605
50	1441	-.024	.112	.316	-.603
50	1442	-.026	.085	.254	-.326
50	1443	-.028	.081	.233	-.293
50	1444	-.046	.084	.234	-.307
50	1445	-.059	.085	.229	-.322
50	1446	-.089	.131	.524	-.739
50	1447	-.017	.127	.561	-.510
50	1448	-.060	.135	.506	-.554
50	1449	-.004	.111	.345	-.368
50	1450	-.003	.094	.267	-.386
50	1451	-.020	.087	.280	-.341
50	1452	-.036	.083	.228	-.329
50	1453	-.029	.081	.231	-.309
50	1454	-.028	.086	.283	-.369
50	1455	-.014	.092	.381	-.470
50	1456	-.059	.096	.279	-.469
50	1457	-.011	.091	.310	-.457
50	1458	-.023	.093	.300	-.334
50	1459	-.009	.095	.294	-.412
50	1460	-.076	.100	.274	-.483
50	1461	-.030	.094	.313	-.358
50	1462	-.022	.091	.428	-.316
50	1463	-.014	.091	.422	-.335
50	1464	.117	.197	.836	-.306
50	1465	.023	.087	.435	-.240
50	1466	.009	.082	.322	-.274
50	1467	.023	.080	.339	-.246
50	1801	.036	.074	.277	-.177
50	1802	.010	.075	.251	-.222
50	1803	-.031	.075	.210	-.305
50	1804	-.049	.076	.201	-.326
50	1805	-.004	.077	.238	-.274
50	1806	.002	.073	.229	-.258
50	1807	.015	.072	.268	-.224
50	2101	-.158	.150	.288	-1.307
50	2102	-.016	.095	.288	-.416
50	2103	.024	.119	.781	-.353
50	2104	-.045	.117	.493	-.432
50	2105	-.098	.122	.345	-.528
50	2106	-.048	.104	.320	-.541
50	2107	-.005	.087	.301	-.265
50	2108	.017	.087	.330	-.265
50	2109	-.009	.095	.341	-.305
50	2110	-.021	.090	.344	-.359
50	2111	.020	.084	.324	-.269
50	2112	.046	.091	.392	-.226
50	2113	-.009	.091	.292	-.321
50	2114	-.014	.093	.415	-.311
50	2115	.028	.101	.669	-.259
50	2116	-.060	.096	.357	-.422
50	2117	-.036	.087	.332	-.384
50	2118	-.053	.084	.309	-.380
50	2119	-.039	.074	.201	-.360
50	2120	-.059	.073	.154	-.318
50	2121	.021	.088	.442	-.283
50	2122	.002	.076	.240	-.257
50	2123	-.063	.085	.210	-.400
50	2124	-.061	.108	.468	-.422
50	2125	.005	.086	.335	-.281
50	2126	.030	.098	.396	-.267
50	2127	.092	.102	.571	-.206
50	2128	.006	.084	.296	-.269
50	2129	-.004	.082	.272	-.275
50	2130	-.013	.082	.366	-.315
50	2131	-.048	.082	.237	-.308
50	2132	-.065	.083	.222	-.342
50	2133	-.021	.079	.261	-.257
50	2134	-.041	.079	.239	-.274
50	2135	-.036	.082	.277	-.297
50	2136	-.043	.090	.269	-.348
50	2137	.034	.085	.343	-.214
50	2138	-.029	.082	.252	-.298
50	2139	-.006	.074	.226	-.261
50	2140	-.075	.083	.198	-.341
50	2141	-.027	.084	.287	-.370
50	2142	-.004	.087	.317	-.298
50	2143	-.035	.077	.217	-.305
50	2144	-.051	.078	.198	-.327
50	2145	-.012	.075	.228	-.281
50	2146	-.036	.075	.199	-.300
50	2147	-.037	.079	.196	-.263
50	2148	-.056	.081	.195	-.289
50	2149	-.008	.077	.217	-.228
50	2150	-.005	.083	.403	-.253
50	2151	.026	.091	.403	-.263
50	2152	-.005	.092	.393	-.291
50	2153	-.001	.081	.287	-.261
50	2154	-.032	.085	.258	-.301
50	2201	-.107	.103	.229	-.419
50	2202	-.122	.097	.179	-.451
50	2203	-.109	.098	.300	-.467
50	2204	-.166	.112	.181	-.759
50	2205	-.187	.146	.199	-1.205
50	2206	-.032	.099	.310	-.411
50	2207	-.060	.098	.256	-.447
50	2208	-.121	.109	.270	-.577
50	2209	-.144	.116	.173	-.613
50	2210	-.136	.116	.187	-.592
50	2211	-.116	.107	.194	-.526
50	2212	-.083	.096	.195	-.449

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
50	2213	-.017	.084	.267	-.283
50	2214	-.019	.087	.319	-.309
50	2215	-.046	.090	.242	-.371
50	2216	-.068	.090	.236	-.395
50	2217	-.030	.087	.270	-.334
50	2218	-.020	.083	.276	-.406
50	2219	-.054	.080	.231	-.319
50	2220	.008	.084	.326	-.349
50	2221	-.021	.067	.234	-.301
50	2222	.003	.082	.270	-.324
50	2224	.036	.090	.407	-.230
50	2225	-.007	.087	.319	-.268
50	2226	.027	.074	.300	-.223
50	2227	-.011	.076	.273	-.277
50	2228	-.016	.080	.280	-.300
50	2229	-.021	.076	.266	-.310
50	2230	.177	.044	.258	.037
50	2231	-.022	.080	.261	-.345
50	2232	-.016	.081	.253	-.359
50	2233	-.044	.083	.260	-.395
50	2234	.024	.074	.297	-.252
50	2235	-.006	.076	.267	-.301
50	2236	-.009	.087	.304	-.273
50	2237	-.023	.088	.296	-.298
50	2238	-.014	.083	.301	-.272
50	2239	-.006	.087	.336	-.287
50	2240	-.023	.086	.259	-.366
50	2301	-.098	.083	.227	-.459
50	2302	-.102	.086	.231	-.443
50	2303	-.040	.078	.247	-.335
50	2304	-.018	.077	.270	-.327
50	2305	-.041	.078	.281	-.329
50	2306	-.037	.087	.249	-.334
50	2307	-.051	.091	.217	-.359
50	2308	-.059	.097	.325	-.532
50	2309	-.088	.081	.183	-.402
50	2310	-.039	.087	.290	-.364
50	2311	-.069	.092	.217	-.588
50	2312	-.024	.080	.270	-.302
50	2313	.011	.078	.325	-.274
50	2314	-.021	.081	.286	-.298
50	2315	-.018	.079	.246	-.283
50	2401	-.079	.086	.173	-.406
50	2402	-.091	.084	.163	-.412
50	2403	-.097	.086	.153	-.429
50	2404	-.143	.090	.190	-.472
50	2405	-.023	.079	.227	-.290
50	2406	-.038	.079	.235	-.281
50	2407	-.089	.097	.230	-.411
50	2408	-.095	.092	.203	-.450
50	2409	-.068	.086	.246	-.351
50	2411	-.101	.091	.223	-.437
50	2412	-.091	.091	.215	-.394
50	2413	-.080	.089	.230	-.351
50	2414	-.059	.079	.250	-.323
50	2415	-.060	.082	.195	-.333
50	2416	-.062	.080	.215	-.312
50	2417	-.073	.081	.198	-.365
50	2418	-.093	.099	.207	-.489
50	2419	-.081	.092	.208	-.373
50	2420	-.052	.088	.238	-.348
50	2421	-.005	.076	.243	-.298
50	2422	-.038	.078	.237	-.351
50	2423	-.061	.095	.281	-.383
50	2424	-.058	.093	.253	-.392
50	2425	-.058	.094	.269	-.389
50	2426	-.045	.094	.268	-.357
50	2427	-.016	.078	.268	-.267
50	2428	-.033	.081	.249	-.291
50	2429	-.007	.081	.284	-.267
50	2430	-.029	.079	.296	-.315
50	2431	-.020	.079	.232	-.277
50	2432	-.015	.079	.258	-.273
50	2433	.008	.077	.249	-.226
50	2434	-.002	.079	.254	-.254
50	2435	-.001	.078	.232	-.260
50	2436	.005	.074	.263	-.264
50	2437	.017	.076	.246	-.262
50	2438	-.013	.077	.231	-.277
50	2439	-.008	.077	.225	-.271
50	2440	-.020	.078	.228	-.287
50	2441	.017	.076	.262	-.233
50	2442	-.004	.076	.222	-.267
50	2443	-.001	.082	.285	-.334
50	2444	-.035	.088	.248	-.375
50	2445	-.010	.085	.270	-.331
50	2446	-.033	.086	.253	-.378
50	2447	.005	.076	.272	-.239
50	2448	.015	.077	.290	-.227
50	2449	.035	.073	.304	-.206
50	2450	.002	.072	.237	-.248
50	2451	.051	.074	.305	-.247
50	2501	-.092	.094	.216	-.416
50	2502	-.099	.089	.224	-.425
50	2503	-.058	.086	.229	-.361
50	2504	-.096	.095	.224	-.439
50	2505	-.061	.091	.218	-.400
50	2506	-.092	.098	.193	-.404
50	2507	-.103	.096	.176	-.462
50	2508	-.056	.100	.322	-.406
50	2509	-.060	.093	.250	-.375
50	2510	-.052	.091	.247	-.403
50	2511	-.041	.078	.223	-.291
50	2601	-.075	.106	.385	-.512
50	2602	.004	.089	.328	-.280
50	2603	-.048	.087	.252	-.371
50	2604	.014	.085	.344	-.379
50	2605	-.006	.084	.339	-.312
50	2606	.007	.089	.321	-.324
50	2607	-.042	.096	.291	-.400
50	2608	.005	.107	.384	-.471
50	2609	.025	.087	.363	-.263
50	2610	.043	.082	.368	-.222
50	2611	-.026	.088	.277	-.324
50	2612	-.001	.083	.311	-.301
50	2613	-.007	.086	.256	-.309
50	2614	.101	.085	.382	-.260
50	2615	-.050	.093	.261	-.418
50	2616	.014	.084	.251	-.306
50	2617	.014	.085	.330	-.306
50	2618	.025	.083	.313	-.268
50	2619	-.059	.088	.238	-.391
50	2620	.001	.082	.269	-.324
50	2621	.011	.089	.303	-.286
50	5102	.132	.127	.737	-.233
50	5103	.055	.098	.419	-.274
50	5104	.116	.110	.604	-.239
50	5105	.029	.090	.474	-.267
50	5106	.075	.108	.489	-.247
50	5107	.001	.075	.296	-.264
50	5108	.018	.080	.321	-.255
50	5109	.034	.094	.343	-.326
50	5110	.104	.102	.528	-.207
50	5111	.006	.081	.274	-.279
50	5112	.033	.077	.271	-.239
50	5114	.097	.097	.472	-.248
50	5202	-.026	.075	.203	-.340
50	5203	-.019	.074	.241	-.290
50	5204	-.020	.077	.227	-.376
50	5301	-.045	.136	.356	-.681
50	5302	-.053	.101	.282	-.483
50	5303	-.018	.096	.320	-.704
50	5304	.010	.086	.357	-.400
50	5305	-.003	.089	.383	-.423
50	5901	-.001	.106	.366	-.376
50	5902	-.100	.121	.316	-.630
50	6101	-.032	.079	.260	-.471
50	6102	-.010	.076	.288	-.243
50	6103	-.014	.076	.277	-.253
50	6104	-.009	.076	.266	-.259

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
50	6105	-.046	.079	.255	-.302
50	6106	.012	.077	.308	-.239
50	6201	-.018	.079	.298	-.332
50	6301	-.012	.075	.323	-.310
50	6302	-.020	.074	.263	-.312
50	6901	-.015	.082	.236	-.382
50	7101	-.034	.076	.241	-.345
50	7102	-.041	.078	.242	-.328
50	7103	-.043	.080	.195	-.357
50	7104	-.029	.073	.230	-.286
50	7105	-.049	.074	.191	-.360
50	7106	-.034	.071	.206	-.363
50	7201	-.027	.075	.236	-.329
50	7301	-.027	.077	.220	-.267
50	9101	-.219	.113	.187	-.657
50	9102	-.067	.101	.284	-.466
50	9103	-.128	.104	.226	-.449
50	9104	-.040	.095	.261	-.461
50	9105	-.188	.135	.205	-.627
50	9106	-.042	.104	.277	-.592
50	9107	-.155	.121	.228	-.569
50	9108	-.091	.094	.217	-.416
50	9109	-.092	.089	.179	-.369
50	9110	-.034	.083	.239	-.354
50	9111	-.090	.092	.182	-.412
50	9112	-.037	.085	.251	-.455
50	9113	-.102	.099	.186	-.442
50	9114	-.105	.092	.162	-.398
50	9115	-.095	.083	.214	-.429
50	9116	-.092	.090	.188	-.574
50	9117	-.093	.081	.216	-.351
50	9118	-.005	.078	.279	-.302
50	9119	-.018	.081	.293	-.313
50	9120	-.095	.092	.212	-.473
50	9121	-.077	.090	.195	-.398
50	9122	-.053	.088	.226	-.415
50	9123	-.001	.091	.314	-.340
50	9124	-.042	.088	.253	-.392
50	9125	-.047	.091	.234	-.470
50	9126	-.055	.091	.259	-.367
50	9201	-.032	.091	.279	-.355
50	9202	.087	.103	.484	-.259
50	9203	.017	.089	.349	-.273
50	9204	-.021	.100	.305	-.471
50	9205	-.007	.089	.308	-.317
50	9206	.036	.084	.296	-.250
50	9207	-.180	.130	.249	-1.081
50	9208	-.089	.110	.253	-.508
50	9209	-.033	.087	.282	-.386
50	9210	-.014	.089	.307	-.388

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
50	9211	-.063	.088	.190	-.398
50	9212	-.167	.120	.171	-.883
50	9213	-.036	.082	.277	-.314
50	9214	-.044	.086	.345	-.408
50	9215	.008	.081	.328	-.304
50	9216	-.024	.084	.346	-.376
50	9217	-.029	.089	.303	-.313
50	9218	-.038	.091	.354	-.334
50	9219	-.161	.101	.154	-.590
50	9220	-.132	.107	.215	-.633
50	9221	-.064	.095	.330	-.403
50	9222	.004	.088	.301	-.322
50	9223	-.004	.090	.342	-.319
50	9224	.004	.086	.281	-.325
50	9225	-.088	.106	.268	-.435
50	9226	-.065	.097	.345	-.434
50	9227	-.017	.092	.328	-.437
50	9228	.027	.083	.315	-.254
50	9229	-.124	.118	.290	-.524
50	9230	-.003	.076	.229	-.268
50	9231	.008	.085	.322	-.290
50	9232	-.077	.101	.295	-.465
50	9233	-.036	.087	.270	-.388
50	9234	-.025	.090	.285	-.316
50	9235	.021	.084	.320	-.271
50	9236	-.074	.089	.192	-.377
50	9237	.027	.088	.318	-.277
50	9238	.014	.089	.313	-.300
60	1101	.054	.206	.911	-.761
60	1102	.091	.204	.911	-.763
60	1103	.084	.176	1.019	-.481
60	1104	.080	.162	.774	-.704
60	1105	.085	.163	.827	-.418
60	1106	.095	.176	.930	-.547
60	1107	.088	.190	1.068	-.539
60	1108	-.016	.170	.695	-.566
60	1109	.078	.175	.718	-.514
60	1110	.130	.153	.786	-.268
60	1111	.141	.142	.664	-.259
60	1112	.159	.149	.796	-.286
60	1113	.152	.171	.818	-.799
60	1114	.088	.181	.761	-1.319
60	1115	-.020	.162	.645	-.565
60	1116	.043	.151	.705	-.396
60	1117	.095	.120	.624	-.319
60	1118	.116	.126	.645	-.324
60	1119	.133	.149	.721	-.333
60	1120	.140	.189	.837	-.393
60	1121	.110	.197	.912	-.546
60	1122	-.038	.156	.486	-.686

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
60	1123	.013	.138	.479	-.513
60	1124	.059	.121	.542	-.362
60	1125	.079	.126	.568	-.325
60	1126	.085	.146	.678	-.372
60	1127	.069	.175	.865	-.423
60	1128	.035	.182	.777	-.569
60	1129	-.012	.147	.684	-.700
60	1130	.029	.133	.714	-.620
60	1131	.040	.111	.464	-.528
60	1132	.033	.108	.576	-.434
60	1133	.021	.118	.557	-.436
60	1134	-.008	.138	.728	-.547
60	1135	-.044	.148	.795	-.681
60	1136	-.000	.116	.612	-.634
60	1137	.035	.094	.417	-.390
60	1138	.030	.090	.322	-.322
60	1139	.028	.088	.334	-.267
60	1140	.002	.089	.336	-.288
60	1141	-.020	.090	.411	-.516
60	1142	-.051	.096	.423	-.779
60	1143	.051	.086	.428	-.256
60	1144	.053	.088	.435	-.266
60	1145	.076	.088	.497	-.441
60	1146	.068	.094	.536	-.453
60	1147	.049	.107	.383	-.380
60	1148	-.020	.097	.331	-.367
60	1149	-.035	.086	.275	-.337
60	1150	.084	.101	.506	-.323
60	1151	.073	.090	.403	-.256
60	1152	.041	.085	.348	-.246
60	1201	-.033	.129	.510	-.680
60	1202	-.060	.099	.261	-.472
60	1203	-.101	.115	.308	-.617
60	1204	-.095	.130	.334	-.757
60	1205	-.098	.132	.363	-.755
60	1206	-.132	.142	.387	-.775
60	1207	-.179	.160	.354	-.815
60	1208	-.245	.179	.399	-1.170
60	1209	-.279	.208	.408	-1.755
60	1210	-.097	.120	.449	-.572
60	1211	-.054	.095	.237	-.389
60	1212	-.079	.105	.273	-.516
60	1213	-.083	.113	.277	-.756
60	1214	-.088	.106	.274	-.553
60	1215	-.123	.129	.287	-.646
60	1216	-.190	.162	.339	-.961
60	1217	-.248	.186	.359	-1.296
60	1218	-.254	.188	.316	-1.231
60	1219	-.051	.110	.360	-.466
60	1220	-.043	.097	.312	-.416

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
60	1221	-.076	.098	.283	-.441
60	1222	-.070	.096	.220	-.502
60	1223	-.045	.100	.281	-.435
60	1224	-.117	.132	.482	-.548
60	1225	-.171	.169	.367	-.907
60	1226	-.242	.203	.328	-1.546
60	1227	-.247	.197	.323	-1.388
60	1228	-.102	.115	.346	-.514
60	1229	-.049	.095	.277	-.426
60	1230	-.063	.094	.257	-.402
60	1231	-.072	.104	.279	-.591
60	1232	-.079	.104	.268	-.542
60	1233	-.097	.120	.310	-.581
60	1234	-.141	.154	.316	-.997
60	1235	-.215	.203	.343	-1.572
60	1236	-.235	.193	.281	-1.485
60	1237	-.022	.100	.321	-.390
60	1238	-.024	.089	.238	-.372
60	1239	-.050	.091	.273	-.453
60	1240	-.055	.106	.279	-.556
60	1241	-.056	.109	.316	-.549
60	1242	-.077	.122	.302	-.595
60	1243	-.107	.150	.304	-1.212
60	1244	-.181	.203	.366	-1.672
60	1245	-.211	.206	.357	-1.749
60	1246	-.034	.114	.452	-.399
60	1247	.000	.093	.295	-.338
60	1248	-.032	.096	.307	-.406
60	1249	-.016	.099	.319	-.353
60	1250	-.011	.099	.274	-.367
60	1251	-.023	.109	.308	-.541
60	1252	-.037	.137	.428	-.845
60	1253	-.078	.182	.383	-1.361
60	1254	-.086	.221	.409	-1.273
60	1301	-.075	.093	.222	-.436
60	1302	-.084	.094	.214	-.455
60	1303	-.079	.090	.213	-.426
60	1304	-.074	.088	.212	-.477
60	1305	-.063	.086	.269	-.434
60	1306	-.076	.086	.211	-.398
60	1307	-.074	.088	.231	-.412
60	1308	-.070	.082	.227	-.372
60	1309	-.069	.081	.242	-.337
60	1310	-.077	.079	.230	-.363
60	1311	-.074	.077	.192	-.322
60	1312	-.073	.079	.205	-.313
60	1313	-.076	.084	.218	-.462
60	1314	-.087	.088	.216	-.512
60	1315	-.076	.081	.238	-.440
60	1316	-.073	.080	.225	-.445
60	1317	-.074	.078	.207	-.346
60	1318	-.081	.077	.206	-.351
60	1319	-.081	.076	.219	-.365
60	1320	-.080	.079	.218	-.374
60	1321	-.080	.092	.234	-.493
60	1322	-.083	.091	.212	-.433
60	1323	-.082	.089	.200	-.434
60	1324	-.081	.086	.207	-.373
60	1325	-.076	.075	.152	-.355
60	1326	-.085	.078	.157	-.401
60	1327	-.084	.079	.158	-.386
60	1328	-.082	.081	.171	-.385
60	1329	-.073	.091	.201	-.519
60	1330	-.085	.092	.202	-.492
60	1331	-.084	.087	.187	-.433
60	1332	-.067	.083	.196	-.347
60	1333	-.076	.083	.195	-.348
60	1334	-.099	.093	.175	-.605
60	1335	-.094	.093	.179	-.661
60	1336	-.101	.089	.199	-.492
60	1337	-.053	.084	.233	-.421
60	1338	-.052	.082	.233	-.354
60	1339	-.043	.082	.284	-.347
60	1340	-.037	.084	.266	-.364
60	1401	-.261	.157	.209	-1.246
60	1402	-.178	.163	.350	-.892
60	1403	-.200	.146	.371	-.902
60	1404	-.114	.165	.395	-1.246
60	1405	-.118	.144	.325	-1.180
60	1406	-.092	.108	.286	-.703
60	1407	-.071	.100	.269	-.535
60	1408	-.060	.085	.186	-.390
60	1409	-.069	.087	.171	-.422
60	1410	-.220	.145	.237	-.809
60	1411	-.178	.144	.338	-.748
60	1412	-.207	.145	.335	-.761
60	1413	-.114	.172	.412	-.783
60	1414	-.102	.157	.499	-.725
60	1415	-.068	.114	.380	-.557
60	1416	-.056	.097	.242	-.427
60	1417	-.055	.090	.228	-.421
60	1418	-.058	.082	.209	-.350
60	1419	-.208	.151	.307	-.953
60	1420	-.142	.153	.384	-.843
60	1421	-.184	.159	.295	-1.237
60	1423	-.080	.141	.339	-.785
60	1424	-.055	.112	.331	-.688
60	1425	-.055	.095	.273	-.500
60	1426	-.067	.085	.258	-.384
60	1427	-.068	.085	.264	-.427
60	1428	-.172	.153	.363	-1.051
60	1429	-.126	.159	.618	-.912
60	1430	-.154	.163	.425	-1.235
60	1431	-.090	.164	.439	-1.059
60	1432	-.086	.147	.331	-1.153
60	1433	-.061	.112	.308	-.790
60	1434	-.045	.093	.233	-.543
60	1435	-.064	.086	.204	-.437
60	1436	-.074	.084	.191	-.454
60	1437	-.132	.134	.317	-1.065
60	1438	-.073	.135	.439	-.971
60	1439	-.118	.145	.414	-1.483
60	1440	-.076	.126	.354	-.887
60	1441	-.079	.120	.338	-.860
60	1442	-.064	.098	.238	-.514
60	1443	-.050	.089	.409	-.510
60	1444	-.058	.089	.286	-.401
60	1445	-.072	.091	.276	-.422
60	1446	-.102	.115	.343	-.845
60	1447	-.086	.104	.313	-.635
60	1448	-.108	.106	.516	-.706
60	1449	-.092	.103	.430	-.446
60	1450	-.078	.100	.331	-.562
60	1451	-.074	.095	.215	-.437
60	1452	-.067	.089	.222	-.354
60	1453	-.053	.086	.209	-.322
60	1454	-.049	.090	.246	-.356
60	1455	-.061	.096	.285	-.585
60	1456	-.129	.101	.259	-.570
60	1457	-.075	.096	.210	-.628
60	1458	-.080	.093	.366	-.500
60	1459	-.067	.093	.375	-.406
60	1460	-.110	.098	.373	-.495
60	1461	-.040	.089	.223	-.340
60	1462	-.023	.089	.378	-.324
60	1463	-.019	.091	.390	-.394
60	1464	.147	.225	.827	-.343
60	1465	-.005	.082	.316	-.262
60	1466	-.010	.081	.282	-.276
60	1467	.000	.078	.287	-.279
60	1801	.009	.076	.328	-.236
60	1802	-.012	.076	.283	-.258
60	1803	-.027	.084	.300	-.289
60	1804	-.046	.085	.305	-.326
60	1805	-.026	.076	.252	-.335
60	1806	-.021	.078	.245	-.277
60	1807	-.003	.078	.293	-.308
60	2101	.048	.172	.653	-1.347
60	2102	.038	.104	.511	-.295
60	2103	.014	.116	.541	-.364

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
60	2104	-.044	.129	.559	-.421
60	2105	.027	.119	.589	-.549
60	2106	-.003	.105	.407	-.499
60	2107	-.001	.096	.330	-.387
60	2108	.033	.096	.315	-.386
60	2109	-.000	.093	.347	-.366
60	2110	-.023	.084	.281	-.281
60	2111	.010	.090	.474	-.320
60	2112	.055	.099	.407	-.288
60	2113	-.061	.095	.256	-.523
60	2114	-.009	.092	.373	-.380
60	2115	.019	.091	.425	-.289
60	2116	-.046	.094	.411	-.376
60	2117	-.009	.078	.273	-.309
60	2118	-.040	.080	.252	-.333
60	2119	-.035	.088	.274	-.318
60	2120	-.054	.086	.226	-.460
60	2121	-.002	.093	.470	-.350
60	2122	-.006	.088	.372	-.301
60	2123	-.041	.080	.252	-.307
60	2124	-.053	.097	.397	-.399
60	2125	-.009	.087	.356	-.296
60	2126	.054	.103	.424	-.274
60	2127	.095	.098	.568	-.216
60	2128	.020	.086	.414	-.291
60	2129	-.027	.082	.217	-.344
60	2130	-.011	.087	.479	-.344
60	2131	-.033	.087	.339	-.311
60	2132	-.050	.088	.320	-.325
60	2133	-.007	.085	.354	-.278
60	2134	-.041	.087	.340	-.328
60	2135	-.039	.085	.212	-.377
60	2136	-.053	.087	.207	-.394
60	2137	.031	.081	.273	-.253
60	2138	-.040	.082	.238	-.367
60	2139	-.015	.079	.275	-.300
60	2140	-.074	.087	.281	-.384
60	2141	-.024	.083	.269	-.284
60	2142	-.021	.084	.244	-.275
60	2143	-.028	.079	.293	-.334
60	2144	-.044	.080	.279	-.353
60	2145	-.000	.077	.310	-.297
60	2146	-.033	.079	.289	-.333
60	2147	-.035	.075	.216	-.343
60	2148	-.048	.078	.214	-.318
60	2149	.002	.073	.255	-.282
60	2150	.006	.080	.279	-.266
60	2151	.030	.085	.356	-.281
60	2152	-.000	.085	.336	-.307
60	2153	-.002	.078	.292	-.289

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
60	2154	-.025	.080	.241	-.332
60	2201	.064	.105	.539	-.347
60	2202	.021	.095	.428	-.291
60	2203	.033	.096	.466	-.252
60	2204	-.013	.091	.417	-.447
60	2205	.012	.115	.438	-.521
60	2206	.015	.098	.405	-.320
60	2207	.026	.094	.345	-.303
60	2208	-.008	.090	.324	-.275
60	2209	-.012	.093	.274	-.409
60	2210	-.013	.107	.354	-.465
60	2211	-.013	.090	.237	-.325
60	2212	-.007	.090	.265	-.306
60	2213	.002	.089	.354	-.337
60	2214	.014	.092	.355	-.320
60	2215	-.002	.091	.371	-.340
60	2216	-.024	.089	.323	-.349
60	2217	-.019	.091	.272	-.386
60	2218	-.008	.089	.259	-.335
60	2219	-.040	.085	.247	-.329
60	2220	.014	.089	.329	-.286
60	2221	-.010	.072	.257	-.250
60	2222	.023	.085	.306	-.323
60	2224	.052	.095	.484	-.279
60	2225	.001	.092	.378	-.362
60	2226	.027	.079	.260	-.263
60	2227	-.010	.082	.222	-.334
60	2228	-.012	.087	.284	-.318
60	2229	-.023	.084	.258	-.343
60	2230	.009	.083	.201	-.181
60	2231	-.013	.086	.261	-.328
60	2232	.000	.083	.282	-.315
60	2233	-.030	.085	.262	-.360
60	2234	.024	.077	.279	-.302
60	2235	-.004	.079	.287	-.314
60	2236	-.001	.080	.266	-.312
60	2237	-.013	.082	.269	-.328
60	2238	-.021	.080	.249	-.311
60	2239	.002	.080	.291	-.319
60	2240	-.006	.084	.299	-.371
60	2301	-.085	.085	.228	-.402
60	2302	-.072	.089	.253	-.399
60	2303	-.020	.082	.275	-.321
60	2304	-.002	.082	.283	-.342
60	2305	-.029	.084	.278	-.376
60	2306	-.040	.087	.323	-.380
60	2307	-.045	.094	.314	-.387
60	2308	-.038	.117	.378	-.520
60	2309	-.059	.088	.235	-.454
60	2310	-.021	.081	.269	-.309

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
60	2311	-.030	.084	.275	-.337
60	2312	-.019	.086	.285	-.384
60	2313	.009	.082	.317	-.234
60	2314	-.007	.083	.256	-.282
60	2315	-.014	.077	.235	-.297
60	2401	-.092	.093	.224	-.436
60	2402	-.083	.085	.186	-.388
60	2403	-.072	.088	.187	-.400
60	2404	-.034	.097	.285	-.457
60	2405	-.022	.083	.290	-.309
60	2406	-.028	.083	.278	-.302
60	2407	-.076	.086	.201	-.353
60	2408	-.062	.085	.224	-.399
60	2409	.025	.089	.330	-.307
60	2411	-.067	.079	.162	-.309
60	2412	-.050	.081	.205	-.317
60	2413	-.051	.091	.260	-.372
60	2414	-.007	.089	.304	-.283
60	2415	-.026	.081	.271	-.292
60	2416	-.032	.078	.222	-.394
60	2417	-.036	.078	.195	-.398
60	2418	-.056	.088	.259	-.374
60	2419	-.042	.086	.255	-.351
60	2420	-.043	.087	.248	-.353
60	2421	-.003	.075	.228	-.258
60	2422	-.017	.076	.204	-.292
60	2423	-.026	.090	.248	-.322
60	2424	-.028	.090	.262	-.319
60	2425	-.030	.091	.268	-.360
60	2426	-.033	.091	.257	-.385
60	2427	-.014	.078	.296	-.359
60	2428	-.017	.076	.290	-.298
60	2429	.004	.077	.309	-.305
60	2430	-.012	.079	.274	-.296
60	2431	-.013	.081	.263	-.293
60	2432	-.013	.082	.261	-.332
60	2433	.007	.080	.276	-.275
60	2434	-.005	.081	.250	-.292
60	2435	-.013	.078	.263	-.261
60	2436	-.021	.077	.235	-.278
60	2437	-.004	.076	.279	-.254
60	2438	-.030	.076	.251	-.271
60	2439	-.025	.079	.258	-.272
60	2440	-.011	.078	.273	-.258
60	2441	.012	.076	.286	-.232
60	2442	-.017	.076	.252	-.259
60	2443	-.022	.079	.227	-.247
60	2444	-.014	.081	.227	-.258
60	2445	.012	.079	.248	-.217
60	2446	-.005	.079	.230	-.235

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
60	2447	.010	.078	.294	-.292
60	2448	.011	.077	.287	-.297
60	2449	.023	.075	.268	-.273
60	2450	.001	.074	.247	-.283
60	2451	.059	.077	.312	-.185
60	2501	-.105	.101	.200	-.474
60	2502	-.073	.097	.221	-.378
60	2503	-.059	.092	.270	-.370
60	2504	-.084	.095	.256	-.474
60	2505	-.061	.090	.222	-.347
60	2506	-.058	.091	.268	-.394
60	2507	-.083	.095	.215	-.416
60	2508	-.070	.095	.227	-.382
60	2509	-.042	.089	.242	-.356
60	2510	-.036	.088	.263	-.347
60	2511	-.035	.083	.261	-.293
60	2601	-.133	.103	.208	-.799
60	2602	-.035	.087	.337	-.380
60	2603	-.080	.086	.277	-.354
60	2604	-.014	.086	.259	-.318
60	2605	-.014	.087	.343	-.389
60	2606	-.010	.085	.308	-.313
60	2607	-.088	.095	.268	-.454
60	2608	-.051	.090	.249	-.478
60	2609	-.034	.083	.254	-.324
60	2610	-.008	.081	.313	-.284
60	2611	-.072	.086	.309	-.348
60	2612	-.013	.081	.342	-.268
60	2613	-.027	.080	.228	-.335
60	2614	.072	.085	.339	-.287
60	2615	-.109	.092	.172	-.468
60	2616	-.036	.079	.225	-.355
60	2617	-.027	.082	.229	-.303
60	2618	-.006	.080	.262	-.268
60	2619	-.071	.086	.225	-.335
60	2620	-.009	.078	.268	-.267
60	2621	-.007	.081	.271	-.291
60	5102	.039	.110	.603	-.333
60	5103	.014	.084	.377	-.266
60	5104	.037	.096	.536	-.253
60	5105	.005	.080	.317	-.297
60	5106	.014	.085	.489	-.238
60	5107	-.001	.075	.262	-.239
60	5108	.000	.076	.258	-.231
60	5109	.002	.083	.321	-.323
60	5110	-.014	.083	.261	-.350
60	5111	-.003	.080	.270	-.281
60	5112	.002	.080	.283	-.335
60	5114	-.012	.075	.221	-.264
60	5202	-.027	.079	.290	-.289
60	5203	-.016	.077	.233	-.278
60	5204	-.008	.072	.296	-.250
60	5301	-.015	.092	.336	-.392
60	5302	-.027	.084	.267	-.411
60	5303	-.015	.079	.272	-.334
60	5304	-.012	.080	.296	-.275
60	5305	.018	.081	.330	-.253
60	5901	.010	.094	.427	-.254
60	5902	-.012	.074	.276	-.341
60	6101	-.038	.075	.193	-.334
60	6102	-.022	.071	.197	-.278
60	6103	-.031	.071	.190	-.289
60	6104	-.034	.075	.245	-.375
60	6105	-.056	.077	.205	-.373
60	6106	.019	.074	.275	-.288
60	6201	-.024	.078	.263	-.355
60	6301	-.019	.076	.225	-.335
60	6302	-.024	.076	.206	-.343
60	6901	-.022	.077	.233	-.310
60	7101	-.042	.080	.215	-.500
60	7102	-.058	.081	.218	-.317
60	7103	-.014	.078	.242	-.288
60	7104	-.007	.077	.309	-.260
60	7105	-.017	.080	.243	-.269
60	7106	-.011	.078	.260	-.258
60	7201	-.053	.087	.253	-.382
60	7301	-.034	.079	.185	-.427
60	9101	-.172	.113	.249	-.566
60	9102	-.079	.109	.330	-.635
60	9103	-.091	.118	.359	-.586
60	9104	-.066	.104	.316	-.421
60	9105	-.123	.119	.329	-.564
60	9106	-.024	.100	.303	-.577
60	9107	-.112	.100	.237	-.440
60	9108	-.103	.096	.246	-.562
60	9109	-.076	.076	.210	-.370
60	9110	-.036	.087	.278	-.380
60	9111	-.081	.076	.192	-.426
60	9112	-.037	.085	.310	-.334
60	9113	-.078	.080	.230	-.494
60	9114	-.065	.079	.228	-.410
60	9115	-.058	.096	.275	-.452
60	9116	-.057	.090	.281	-.392
60	9117	-.060	.095	.278	-.426
60	9118	.004	.079	.277	-.301
60	9119	-.012	.080	.258	-.316
60	9120	-.056	.091	.281	-.366
60	9121	-.042	.082	.238	-.345
60	9122	-.043	.085	.255	-.329
60	9123	-.002	.083	.304	-.326
60	9124	-.020	.081	.231	-.356
60	9125	-.007	.082	.269	-.337
60	9126	-.023	.085	.219	-.333
60	9201	.029	.101	.376	-.365
60	9202	.119	.105	.559	-.301
60	9203	.015	.091	.449	-.258
60	9204	-.015	.087	.259	-.360
60	9205	.000	.086	.305	-.300
60	9206	.036	.080	.314	-.236
60	9207	-.011	.172	.494	-.904
60	9208	-.005	.106	.457	-.360
60	9209	-.011	.092	.398	-.301
60	9210	-.023	.091	.303	-.369
60	9211	-.067	.088	.238	-.399
60	9212	-.019	.099	.295	-.378
60	9213	-.035	.083	.210	-.339
60	9214	-.026	.090	.276	-.354
60	9215	.017	.085	.287	-.292
60	9216	-.026	.084	.224	-.340
60	9217	-.029	.082	.218	-.337
60	9218	-.042	.082	.225	-.332
60	9219	.004	.103	.388	-.438
60	9220	-.008	.092	.281	-.339
60	9221	-.024	.081	.269	-.340
60	9222	.014	.082	.287	-.407
60	9223	-.010	.082	.295	-.303
60	9224	-.010	.075	.267	-.391
60	9225	.018	.090	.346	-.339
60	9226	-.010	.083	.262	-.332
60	9227	.015	.086	.364	-.345
60	9228	.026	.075	.268	-.323
60	9229	.034	.097	.485	-.349
60	9230	.013	.080	.283	-.274
60	9231	.002	.083	.281	-.294
60	9232	.017	.094	.367	-.281
60	9233	.011	.089	.351	-.297
60	9234	.012	.095	.406	-.315
60	9235	.027	.085	.370	-.241
60	9236	-.068	.092	.314	-.385
60	9237	.033	.089	.351	-.244
60	9238	.012	.090	.288	-.264
70	1101	.226	.299	1.208	-.865
70	1102	.268	.305	1.316	-.816
70	1103	.179	.277	1.244	-1.250
70	1104	.128	.253	1.163	-.686
70	1105	.075	.240	1.036	-.719
70	1106	.016	.227	.892	-.695
70	1107	-.034	.231	1.021	-.860
70	1108	.177	.272	1.002	-.717
70	1109	.314	.303	1.589	-.592

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
70	1110	.320	.276	1.311	-.573
70	1111	.250	.243	1.120	-.597
70	1112	.187	.216	.951	-.513
70	1113	.059	.225	.923	-.608
70	1114	-.082	.231	.889	-.766
70	1115	.202	.297	1.048	-.832
70	1116	.306	.300	1.144	-.598
70	1117	.301	.256	1.223	-.562
70	1118	.221	.217	1.035	-.484
70	1119	.126	.189	1.114	-.445
70	1120	-.003	.184	.905	-.541
70	1121	-.107	.197	.999	-.765
70	1122	.248	.270	1.017	-1.054
70	1123	.349	.264	1.160	-.686
70	1124	.312	.227	.988	-.441
70	1125	.200	.195	.980	-.445
70	1126	.105	.171	.753	-.517
70	1127	-.051	.162	.833	-.600
70	1128	-.139	.167	.716	-.723
70	1129	.246	.250	1.123	-.756
70	1130	.322	.252	1.216	-.592
70	1131	.276	.224	1.126	-.460
70	1132	.194	.200	.993	-.578
70	1133	.089	.174	.766	-.457
70	1134	-.054	.150	.466	-.648
70	1135	-.153	.145	.348	-.839
70	1136	.076	.181	.880	-.791
70	1137	.104	.175	.847	-.579
70	1138	.130	.177	.784	-.454
70	1139	.122	.166	.829	-.474
70	1140	.089	.156	.691	-.499
70	1141	-.032	.139	.472	-.497
70	1142	-.114	.132	.353	-.571
70	1143	.121	.150	.644	-.469
70	1144	.150	.152	.652	-.452
70	1145	.223	.153	.858	-.240
70	1146	.258	.155	.873	-.285
70	1147	.223	.160	.944	-.357
70	1148	.066	.163	.736	-.508
70	1149	-.054	.146	.590	-.635
70	1150	.231	.165	.875	-.302
70	1151	.265	.166	1.050	-.284
70	1152	.150	.145	.834	-.449
70	1201	-.000	.160	.684	-.577
70	1202	-.092	.136	.293	-.559
70	1203	-.129	.157	.341	-.797
70	1204	-.107	.150	.399	-.583
70	1205	-.110	.151	.383	-.600
70	1206	-.159	.155	.296	-.835
70	1207	-.222	.186	.307	-1.231
70	1208	-.446	.251	.266	-1.527
70	1209	-.508	.295	.433	-2.262
70	1210	-.080	.167	.592	-.640
70	1211	-.069	.119	.383	-.518
70	1212	-.102	.133	.315	-.618
70	1213	-.087	.136	.330	-.781
70	1214	-.088	.149	.406	-.656
70	1215	-.108	.168	.406	-.831
70	1216	-.229	.221	.407	-1.113
70	1217	-.441	.293	.464	-1.769
70	1218	-.435	.275	.451	-2.073
70	1219	-.014	.142	.637	-.503
70	1220	-.036	.124	.405	-.439
70	1221	-.077	.141	.372	-.687
70	1222	-.077	.131	.364	-.611
70	1223	-.020	.132	.395	-.515
70	1224	-.081	.165	.609	-.659
70	1225	-.166	.216	.489	-1.101
70	1226	-.417	.306	.431	-1.991
70	1227	-.430	.296	.494	-2.247
70	1228	-.102	.149	.521	-.724
70	1229	-.040	.123	.419	-.498
70	1230	-.060	.122	.350	-.478
70	1231	-.056	.126	.350	-.526
70	1232	-.067	.128	.363	-.514
70	1233	-.055	.144	.406	-.609
70	1234	-.114	.207	.442	-1.204
70	1235	-.388	.326	.416	-2.303
70	1236	-.468	.319	.414	-2.483
70	1237	.028	.146	.808	-.445
70	1238	.011	.130	.532	-.438
70	1239	-.023	.133	.389	-.495
70	1240	-.015	.123	.406	-.478
70	1241	-.010	.128	.415	-.466
70	1242	-.014	.137	.437	-.498
70	1243	-.020	.159	.551	-.669
70	1244	-.269	.283	.589	-1.567
70	1245	-.375	.282	.600	-1.806
70	1246	.084	.212	.884	-.546
70	1247	.074	.141	.595	-.413
70	1248	.011	.138	.501	-.429
70	1249	.049	.136	.495	-.447
70	1250	.061	.137	.595	-.429
70	1251	.050	.145	.617	-.550
70	1252	.080	.169	.609	-.583
70	1253	.013	.238	.686	-1.941
70	1254	-.053	.279	.890	-1.384
70	1301	-.166	.135	.293	-.739
70	1302	-.163	.132	.281	-.571
70	1303	-.158	.127	.280	-.882
70	1304	-.143	.125	.283	-.902
70	1305	-.134	.129	.282	-.639
70	1306	-.139	.127	.316	-.673
70	1307	-.142	.130	.319	-.703
70	1308	-.168	.131	.234	-.705
70	1309	-.168	.133	.257	-.627
70	1310	-.162	.128	.213	-.621
70	1311	-.161	.126	.194	-.643
70	1312	-.152	.128	.230	-.614
70	1313	-.156	.131	.279	-.595
70	1314	-.159	.132	.284	-.604
70	1315	-.198	.139	.276	-.765
70	1316	-.183	.133	.267	-.688
70	1317	-.166	.117	.160	-.576
70	1318	-.160	.116	.172	-.564
70	1319	-.161	.116	.182	-.585
70	1320	-.154	.118	.205	-.616
70	1321	-.161	.123	.219	-.580
70	1322	-.197	.138	.367	-1.126
70	1323	-.188	.129	.333	-.680
70	1324	-.166	.120	.298	-.616
70	1325	-.150	.119	.211	-.503
70	1326	-.148	.122	.236	-.525
70	1327	-.149	.121	.212	-.550
70	1328	-.140	.121	.219	-.539
70	1329	-.180	.135	.228	-.776
70	1330	-.164	.128	.242	-.626
70	1331	-.151	.120	.239	-.527
70	1332	-.134	.119	.304	-.525
70	1333	-.135	.121	.305	-.564
70	1334	-.134	.123	.320	-.576
70	1335	-.129	.123	.317	-.587
70	1336	-.253	.132	.202	-.647
70	1337	-.155	.120	.260	-.528
70	1338	-.136	.121	.287	-.516
70	1339	-.136	.122	.280	-.541
70	1340	-.104	.123	.328	-.527
70	1401	-.405	.226	.192	-1.954
70	1402	-.379	.227	.495	-1.853
70	1403	-.392	.247	.267	-2.052
70	1404	-.362	.268	.391	-2.065
70	1405	-.347	.253	.306	-1.663
70	1406	-.286	.210	.361	-1.485
70	1407	-.216	.184	.275	-1.262
70	1408	-.188	.169	.402	-1.265
70	1409	-.184	.171	.406	-1.270
70	1410	-.371	.193	.178	-1.354
70	1411	-.375	.208	.193	-1.337
70	1412	-.414	.229	.601	-1.627
70	1413	-.378	.253	.622	-1.449

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
70	1414	-.349	.240	.380	-1.196
70	1415	-.267	.203	.331	-1.032
70	1416	-.206	.168	.291	-1.036
70	1417	-.172	.150	.301	-.929
70	1418	-.177	.152	.383	-.899
70	1419	-.341	.202	.252	-1.261
70	1420	-.325	.199	.263	-1.121
70	1421	-.360	.220	.456	-1.813
70	1423	-.299	.186	.423	-1.027
70	1424	-.281	.200	.480	-1.167
70	1425	-.221	.165	.359	-.938
70	1426	-.201	.149	.279	-.672
70	1427	-.196	.150	.246	-.774
70	1428	-.284	.185	.243	-1.175
70	1429	-.278	.167	.234	-1.090
70	1430	-.315	.199	.294	-1.259
70	1431	-.303	.205	.327	-1.352
70	1432	-.306	.202	.336	-1.453
70	1433	-.263	.175	.267	-.926
70	1434	-.223	.169	.399	-.932
70	1435	-.209	.170	.330	-1.126
70	1436	-.224	.172	.273	-1.141
70	1437	-.251	.146	.169	-.979
70	1438	-.237	.144	.199	-1.070
70	1439	-.277	.185	.282	-2.125
70	1440	-.262	.166	.300	-1.215
70	1441	-.261	.170	.314	-1.395
70	1442	-.259	.155	.243	-.842
70	1443	-.224	.147	.275	-.748
70	1444	-.239	.171	.268	-.984
70	1445	-.245	.173	.294	-.968
70	1446	-.243	.140	.192	-.782
70	1447	-.243	.142	.262	-.954
70	1448	-.260	.155	.320	-1.147
70	1449	-.249	.157	.326	-1.228
70	1450	-.243	.139	.174	-1.022
70	1451	-.237	.142	.181	-.843
70	1452	-.235	.139	.186	-.829
70	1453	-.213	.137	.211	-.723
70	1454	-.255	.152	.229	-.858
70	1455	-.271	.174	.237	-1.239
70	1456	-.418	.185	.096	-1.212
70	1457	-.307	.173	.177	-1.065
70	1458	-.312	.184	.218	-1.827
70	1459	-.284	.182	.183	-1.776
70	1460	-.380	.207	.175	-1.705
70	1461	-.227	.175	.274	-1.050
70	1462	-.183	.170	.378	-.988
70	1463	-.167	.166	.477	-.993
70	1464	.273	.368	1.221	-.707
70	1465	-.118	.122	.264	-.572
70	1466	-.080	.118	.325	-.495
70	1467	-.070	.112	.304	-.476
70	1801	-.062	.118	.393	-.477
70	1802	-.072	.118	.334	-.479
70	1803	-.107	.127	.299	-.567
70	1804	-.111	.129	.289	-.602
70	1805	-.111	.121	.310	-.606
70	1806	-.112	.114	.267	-.522
70	1807	-.079	.113	.286	-.433
70	2101	.308	.232	1.204	-.404
70	2102	.034	.188	.711	-.687
70	2103	.027	.172	.604	-1.138
70	2104	-.191	.145	.355	-.756
70	2105	.024	.194	.860	-.618
70	2106	-.062	.168	.729	-.651
70	2107	-.071	.156	.411	-.711
70	2108	.042	.161	.611	-.573
70	2109	-.062	.138	.509	-.536
70	2110	-.050	.129	.413	-.426
70	2111	-.015	.123	.443	-.468
70	2112	.146	.166	.853	-.359
70	2113	-.272	.149	.217	-1.203
70	2114	.061	.156	.576	-.498
70	2115	.024	.141	.508	-.516
70	2116	-.128	.139	.314	-.578
70	2117	-.138	.130	.289	-.574
70	2118	-.113	.134	.334	-.703
70	2119	-.114	.140	.318	-.963
70	2120	-.135	.156	.317	-1.179
70	2121	-.154	.160	.366	-1.067
70	2122	-.035	.147	.580	-.698
70	2123	-.125	.133	.363	-.583
70	2124	-.122	.138	.401	-.636
70	2125	-.084	.119	.391	-.468
70	2126	.104	.164	.782	-.417
70	2127	.058	.147	.656	-.450
70	2128	.034	.142	.579	-.453
70	2129	-.090	.139	.458	-.661
70	2130	-.046	.128	.428	-.453
70	2131	-.111	.125	.325	-.536
70	2132	-.113	.124	.325	-.516
70	2133	-.115	.127	.350	-.503
70	2134	-.102	.130	.342	-.577
70	2135	-.125	.148	.326	-.899
70	2136	-.129	.140	.342	-.810
70	2137	-.017	.130	.399	-.408
70	2138	-.114	.125	.322	-.550
70	2139	-.086	.123	.333	-.535
70	2140	-.178	.137	.283	-.705
70	2141	-.058	.133	.429	-.577
70	2142	-.086	.133	.368	-.621
70	2143	-.109	.130	.305	-.608
70	2144	-.111	.131	.320	-.618
70	2145	-.115	.133	.290	-.641
70	2146	-.098	.133	.322	-.616
70	2147	-.105	.131	.302	-.573
70	2148	-.108	.125	.289	-.554
70	2149	-.096	.130	.369	-.574
70	2150	-.033	.141	.443	-.638
70	2151	.056	.138	.539	-.387
70	2152	.036	.136	.502	-.412
70	2153	-.112	.131	.329	-.569
70	2154	-.073	.131	.307	-.512
70	2201	.225	.183	.943	-.410
70	2202	.131	.168	.747	-.423
70	2203	.131	.168	.662	-.465
70	2204	.027	.153	.565	-.467
70	2205	.088	.175	.770	-.828
70	2206	-.018	.142	.504	-.482
70	2207	.046	.143	.573	-.427
70	2208	-.010	.137	.429	-.409
70	2209	-.007	.146	.562	-.561
70	2210	-.044	.160	.663	-.666
70	2211	-.022	.142	.446	-.533
70	2212	-.022	.135	.405	-.477
70	2213	-.038	.121	.393	-.562
70	2214	.004	.121	.494	-.456
70	2215	-.016	.118	.421	-.467
70	2216	-.039	.120	.379	-.516
70	2217	-.067	.141	.335	-.556
70	2218	-.118	.148	.369	-.653
70	2219	-.103	.132	.306	-.572
70	2220	-.013	.129	.411	-.439
70	2221	-.029	.106	.273	-.394
70	2222	-.049	.133	.354	-.539
70	2224	.059	.153	.702	-.544
70	2225	-.039	.164	.479	-.885
70	2226	-.029	.142	.449	-.442
70	2227	-.033	.137	.431	-.530
70	2228	-.036	.126	.422	-.454
70	2229	-.052	.120	.357	-.420
70	2230	-.477	.208	.009	-.834
70	2231	-.037	.123	.395	-.481
70	2232	-.026	.141	.414	-.492
70	2233	-.054	.147	.437	-.523
70	2234	-.055	.140	.359	-.527
70	2235	-.029	.138	.388	-.509
70	2236	-.029	.119	.355	-.435
70	2237	-.013	.120	.389	-.429

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
70	2238	-.130	.123	.271	-.558
70	2239	-.020	.121	.362	-.476
70	2240	-.071	.143	.380	-.696
70	2301	-.170	.122	.219	-.551
70	2302	-.164	.130	.223	-.667
70	2303	-.094	.127	.305	-.532
70	2304	-.107	.128	.331	-.556
70	2305	-.163	.141	.347	-.680
70	2306	-.183	.153	.366	-.744
70	2307	-.071	.151	.520	-.767
70	2308	.139	.192	1.072	-.463
70	2309	-.169	.144	.396	-.648
70	2310	-.108	.123	.318	-.606
70	2311	-.097	.120	.369	-.518
70	2312	-.075	.121	.438	-.516
70	2313	-.054	.117	.419	-.492
70	2314	-.059	.118	.449	-.487
70	2315	-.069	.117	.386	-.447
70	2401	-.172	.141	.258	-.629
70	2402	-.153	.139	.266	-.598
70	2403	-.156	.148	.314	-.657
70	2404	.039	.146	.499	-.428
70	2405	-.091	.125	.407	-.544
70	2406	-.084	.123	.415	-.516
70	2407	-.166	.134	.290	-.594
70	2408	-.162	.141	.264	-.603
70	2409	.000	.148	.468	-.603
70	2411	-.153	.129	.256	-.578
70	2412	-.138	.132	.316	-.543
70	2413	-.158	.147	.397	-.724
70	2414	-.036	.141	.415	-.544
70	2415	-.101	.122	.412	-.582
70	2416	-.101	.129	.328	-.590
70	2417	-.104	.128	.347	-.580
70	2418	-.148	.134	.331	-.632
70	2419	-.127	.137	.382	-.557
70	2420	-.133	.142	.377	-.624
70	2421	-.066	.125	.325	-.565
70	2422	-.079	.126	.325	-.568
70	2423	-.081	.127	.296	-.481
70	2424	-.098	.129	.324	-.533
70	2425	-.099	.131	.328	-.539
70	2426	-.108	.133	.294	-.573
70	2427	-.074	.118	.358	-.502
70	2428	-.079	.117	.330	-.476
70	2429	-.068	.116	.321	-.465
70	2430	-.073	.114	.295	-.460
70	2431	-.071	.125	.324	-.479
70	2432	-.072	.125	.328	-.460
70	2433	-.048	.123	.366	-.463

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
70	2434	-.065	.123	.355	-.449
70	2435	-.072	.120	.363	-.499
70	2436	-.107	.115	.271	-.521
70	2437	-.086	.118	.369	-.510
70	2438	-.104	.120	.356	-.538
70	2439	-.113	.121	.303	-.479
70	2440	-.056	.119	.328	-.459
70	2441	-.057	.116	.336	-.446
70	2442	-.098	.118	.294	-.480
70	2443	-.106	.122	.285	-.541
70	2444	-.069	.122	.326	-.465
70	2445	-.072	.119	.314	-.463
70	2446	-.074	.119	.302	-.466
70	2447	-.064	.122	.332	-.475
70	2448	-.057	.124	.373	-.488
70	2449	-.047	.122	.380	-.465
70	2450	-.056	.121	.369	-.469
70	2451	.038	.119	.407	-.343
70	2501	-.189	.136	.311	-.835
70	2502	-.167	.138	.308	-.692
70	2503	-.220	.146	.204	-.902
70	2504	-.176	.130	.305	-.659
70	2505	-.181	.130	.200	-.865
70	2506	-.171	.138	.237	-.722
70	2507	-.171	.123	.184	-.820
70	2508	-.192	.146	.255	-.832
70	2509	-.133	.132	.311	-.647
70	2510	-.124	.133	.286	-.672
70	2511	-.115	.121	.291	-.558
70	2601	-.226	.141	.281	-.977
70	2602	-.114	.126	.352	-.667
70	2603	-.222	.142	.272	-.869
70	2604	-.105	.130	.359	-.771
70	2605	-.101	.121	.283	-.590
70	2606	-.086	.119	.366	-.470
70	2607	-.298	.136	.113	-.822
70	2608	-.107	.113	.264	-.490
70	2609	-.123	.122	.223	-.567
70	2610	-.079	.118	.293	-.511
70	2611	-.198	.134	.248	-.670
70	2612	-.085	.122	.284	-.526
70	2613	-.107	.120	.328	-.517
70	2614	.020	.132	.542	-.443
70	2615	-.245	.140	.283	-.917
70	2616	-.142	.126	.275	-.602
70	2617	-.111	.132	.352	-.503
70	2618	-.065	.127	.382	-.476
70	2619	-.186	.145	.324	-.698
70	2620	-.067	.130	.363	-.463
70	2621	-.088	.121	.310	-.488

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
70	5102	-.041	.128	.435	-.549
70	5103	-.060	.127	.389	-.593
70	5104	-.034	.127	.551	-.482
70	5105	-.062	.132	.394	-.518
70	5106	-.024	.122	.591	-.355
70	5107	-.079	.119	.317	-.458
70	5108	-.068	.115	.337	-.561
70	5109	-.065	.118	.335	-.480
70	5110	-.075	.116	.369	-.465
70	5111	-.071	.117	.370	-.497
70	5112	-.073	.114	.361	-.450
70	5114	-.090	.109	.240	-.449
70	5202	-.067	.137	.511	-.506
70	5203	-.079	.113	.305	-.487
70	5204	-.068	.111	.361	-.472
70	5301	-.054	.118	.390	-.483
70	5302	-.074	.119	.329	-.645
70	5303	-.071	.121	.294	-.469
70	5304	-.069	.121	.286	-.483
70	5305	-.069	.120	.335	-.462
70	5901	-.063	.125	.357	-.498
70	5902	-.069	.116	.267	-.468
70	6101	-.104	.120	.267	-.768
70	6102	-.099	.115	.254	-.489
70	6103	-.107	.113	.214	-.490
70	6104	-.102	.112	.343	-.471
70	6105	-.135	.115	.327	-.540
70	6106	-.042	.116	.373	-.482
70	6201	-.076	.119	.342	-.487
70	6301	-.095	.111	.300	-.505
70	6302	-.097	.109	.297	-.495
70	6901	-.091	.118	.418	-.761
70	7101	-.120	.127	.347	-.628
70	7102	-.151	.140	.392	-.648
70	7103	-.074	.128	.470	-.495
70	7104	-.053	.125	.364	-.465
70	7105	-.051	.128	.461	-.457
70	7106	-.090	.129	.459	-.518
70	7201	-.131	.129	.379	-.576
70	7301	-.134	.148	.309	-.664
70	9101	-.370	.174	.107	-1.213
70	9102	-.025	.148	.583	-.655
70	9103	.025	.199	.864	-.564
70	9104	-.141	.218	.607	-1.291
70	9105	-.322	.192	.310	-1.051
70	9106	.050	.159	.729	-.409
70	9107	-.295	.168	.288	-.924
70	9108	-.159	.123	.286	-.588
70	9109	-.157	.126	.281	-.574
70	9110	-.200	.180	.366	-1.136

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
70	9111	-.158	.121	.243	-.566
70	9112	-.124	.135	.344	-.700
70	9113	-.168	.123	.213	-.628
70	9114	-.149	.128	.288	-.530
70	9115	-.157	.137	.344	-.668
70	9116	-.141	.121	.276	-.586
70	9117	-.154	.136	.306	-.653
70	9118	-.064	.125	.355	-.565
70	9119	-.092	.130	.332	-1.057
70	9120	-.129	.122	.292	-.606
70	9121	-.120	.122	.317	-.561
70	9122	-.130	.132	.377	-.622
70	9123	-.064	.138	.421	-.487
70	9124	-.110	.136	.351	-.558
70	9125	-.094	.127	.357	-.498
70	9126	-.119	.147	.383	-.882
70	9201	.202	.177	.837	-.460
70	9202	.304	.204	1.008	-.362
70	9203	-.026	.150	.489	-.573
70	9204	-.084	.144	.352	-.527
70	9205	-.011	.148	.545	-.652
70	9206	-.032	.136	.417	-.514
70	9207	.195	.218	.872	-.914
70	9208	-.024	.167	.710	-.533
70	9209	-.069	.130	.370	-.552
70	9210	-.064	.136	.508	-.567
70	9211	-.143	.143	.254	-.711
70	9212	.005	.149	.503	-.452
70	9213	-.093	.140	.356	-.556
70	9214	-.048	.139	.442	-.537
70	9215	-.062	.143	.414	-.547
70	9216	-.080	.140	.375	-.537
70	9217	-.077	.123	.326	-.551
70	9218	-.072	.125	.331	-.470
70	9219	.120	.148	.707	-.398
70	9220	-.001	.138	.434	-.472
70	9221	-.041	.128	.450	-.419
70	9222	-.057	.126	.353	-.494
70	9223	-.064	.120	.350	-.525
70	9224	-.062	.124	.396	-.547
70	9225	.040	.157	.724	-.482
70	9226	-.031	.134	.511	-.427
70	9227	.002	.129	.427	-.462
70	9228	-.018	.121	.412	-.490
70	9229	.119	.155	.754	-.386
70	9230	-.021	.117	.305	-.489
70	9231	-.047	.114	.360	-.438
70	9232	.016	.146	.531	-.431
70	9233	-.004	.133	.474	-.424
70	9234	-.014	.133	.466	-.440

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
70	9235	-.010	.124	.427	-.458
70	9236	-.151	.138	.398	-.652
70	9237	.002	.131	.423	-.463
70	9238	-.041	.115	.365	-.484
80	1101	.437	.164	1.080	-.286
80	1102	.467	.166	1.104	-.220
80	1103	.345	.161	.927	-.291
80	1104	.296	.162	.896	-.418
80	1105	.230	.178	.969	-.376
80	1106	.098	.178	.921	-.505
80	1107	.006	.179	.786	-.637
80	1108	.465	.171	1.030	-.317
80	1109	.613	.184	1.258	-.063
80	1110	.616	.184	1.235	-.118
80	1111	.523	.184	1.288	-.314
80	1112	.401	.184	1.390	-.372
80	1113	.159	.184	.802	-.425
80	1114	-.076	.171	.539	-.653
80	1115	.496	.172	1.081	-.190
80	1116	.628	.174	1.203	-.031
80	1117	.633	.178	1.259	.028
80	1118	.533	.172	1.110	-.101
80	1119	.380	.161	.977	-.161
80	1120	.112	.147	.637	-.453
80	1121	-.048	.144	.483	-.728
80	1122	.413	.182	1.059	-.632
80	1123	.529	.188	1.101	-.226
80	1124	.521	.185	1.102	-.123
80	1125	.458	.175	1.150	-.101
80	1126	.326	.166	.892	-.230
80	1127	.057	.150	.575	-.437
80	1128	-.114	.142	.386	-.608
80	1129	.285	.191	.952	-.499
80	1130	.327	.191	.962	-.301
80	1131	.280	.187	.921	-.368
80	1132	.238	.179	.916	-.401
80	1133	.178	.170	.814	-.402
80	1134	-.025	.154	.614	-.513
80	1135	-.181	.144	.403	-.628
80	1136	-.041	.251	.648	-1.314
80	1137	-.006	.169	.610	-1.042
80	1138	-.006	.151	.602	-.512
80	1139	.008	.148	.598	-.420
80	1140	-.011	.151	.588	-.503
80	1141	-.128	.151	.450	-.607
80	1142	-.213	.146	.313	-.812
80	1143	.022	.159	.508	-.652
80	1144	.058	.163	.575	-.490
80	1145	.182	.160	.768	-.437
80	1146	.249	.156	.906	-.321

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
80	1147	.236	.162	.851	-.341
80	1148	.039	.190	.619	-.748
80	1149	-.104	.180	.429	-.932
80	1150	.167	.169	.917	-.347
80	1151	.330	.183	1.042	-.259
80	1152	.199	.159	.916	-.274
80	1201	.168	.193	.903	-.456
80	1202	-.160	.144	.344	-.686
80	1203	-.222	.173	.310	-.799
80	1204	-.137	.150	.360	-.669
80	1205	-.131	.146	.358	-.643
80	1206	-.127	.142	.356	-.680
80	1207	-.153	.173	.378	-.807
80	1208	-.491	.189	.256	-1.581
80	1209	-.487	.191	.131	-2.019
80	1210	.012	.165	.749	-.458
80	1211	-.044	.121	.365	-.405
80	1212	-.084	.132	.324	-.530
80	1213	-.063	.131	.335	-.522
80	1214	-.046	.130	.389	-.488
80	1215	-.001	.143	.454	-.588
80	1216	-.116	.247	.553	-1.360
80	1217	-.449	.196	.281	-1.486
80	1218	-.410	.192	.190	-2.108
80	1219	.020	.134	.639	-.390
80	1220	-.003	.119	.401	-.399
80	1221	-.039	.129	.403	-.497
80	1222	-.034	.125	.404	-.443
80	1223	.040	.126	.477	-.520
80	1224	.032	.151	.518	-.554
80	1225	-.052	.256	.566	-1.037
80	1226	-.375	.221	.624	-1.271
80	1227	-.346	.208	.411	-1.282
80	1228	-.074	.141	.418	-.555
80	1229	-.005	.120	.398	-.393
80	1230	-.023	.114	.373	-.431
80	1231	-.012	.117	.400	-.445
80	1232	-.006	.117	.416	-.507
80	1233	.052	.130	.464	-.644
80	1234	.025	.241	.597	-1.126
80	1235	-.330	.273	.634	-1.589
80	1236	-.347	.243	.567	-1.527
80	1237	.068	.127	.526	-.396
80	1238	.047	.112	.487	-.388
80	1239	.026	.137	.523	-.391
80	1240	.039	.128	.438	-.487
80	1241	.056	.133	.477	-.511
80	1242	.102	.142	.530	-.585
80	1243	.123	.180	.622	-.811
80	1244	-.155	.334	.834	-1.486

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
80	1245	-.243	.308	.932	-1.677
80	1246	.232	.206	1.174	-.453
80	1247	.150	.127	.604	-.326
80	1248	.055	.149	.638	-.516
80	1249	.104	.146	.622	-.489
80	1250	.132	.133	.562	-.412
80	1251	.156	.144	.609	-.429
80	1252	.230	.169	.757	-.564
80	1253	.200	.229	.847	-1.200
80	1254	.177	.204	.768	-1.033
80	1301	-.310	.180	.259	-1.333
80	1302	-.288	.166	.260	-1.109
80	1303	-.239	.144	.271	-1.113
80	1304	-.215	.140	.233	-1.493
80	1305	-.219	.140	.266	-1.234
80	1306	-.214	.132	.228	-.789
80	1307	-.208	.133	.231	-.803
80	1308	-.300	.156	.306	-.921
80	1309	-.271	.149	.236	-.907
80	1310	-.234	.134	.205	-.651
80	1311	-.220	.126	.247	-.601
80	1312	-.215	.126	.283	-.599
80	1313	-.221	.128	.216	-.640
80	1314	-.218	.129	.221	-.647
80	1315	-.301	.138	.106	-.865
80	1316	-.271	.131	.169	-.785
80	1317	-.238	.129	.166	-.762
80	1318	-.229	.129	.184	-.756
80	1319	-.225	.129	.209	-.746
80	1320	-.218	.129	.225	-.742
80	1321	-.215	.131	.250	-.648
80	1322	-.286	.143	.160	-.907
80	1323	-.255	.136	.184	-.816
80	1324	-.233	.130	.195	-.708
80	1325	-.242	.125	.180	-.594
80	1326	-.239	.128	.188	-.615
80	1327	-.231	.127	.184	-.592
80	1328	-.226	.128	.187	-.590
80	1329	-.315	.136	.147	-.839
80	1330	-.271	.131	.155	-.739
80	1331	-.236	.126	.189	-.633
80	1332	-.235	.130	.159	-.701
80	1333	-.268	.126	.180	-.680
80	1334	-.262	.130	.207	-.709
80	1335	-.248	.130	.225	-.689
80	1336	-.367	.145	.102	-.837
80	1337	-.254	.133	.166	-.695
80	1338	-.246	.127	.197	-.788
80	1339	-.272	.143	.215	-.786
80	1340	-.235	.137	.250	-.802

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
80	1401	-.351	.153	.125	-.893
80	1402	-.376	.153	.111	-.874
80	1403	-.378	.154	.175	-1.245
80	1404	-.369	.176	.178	-1.188
80	1405	-.373	.184	.207	-1.259
80	1406	-.395	.197	.303	-1.231
80	1407	-.392	.209	.260	-1.334
80	1408	-.385	.235	.304	-1.514
80	1409	-.394	.260	.309	-1.770
80	1410	-.325	.151	.140	-.986
80	1411	-.324	.146	.137	-.843
80	1412	-.329	.152	.123	-.973
80	1413	-.334	.157	.124	-1.029
80	1414	-.344	.157	.269	-.985
80	1415	-.356	.168	.257	-1.053
80	1416	-.359	.172	.206	-1.158
80	1417	-.391	.213	.210	-1.417
80	1418	-.379	.220	.255	-1.757
80	1419	-.304	.140	.132	-.767
80	1420	-.298	.140	.144	-.769
80	1421	-.290	.151	.176	-.957
80	1423	-.311	.136	.235	-.730
80	1424	-.344	.160	.148	-.921
80	1425	-.367	.162	.163	-.970
80	1426	-.410	.190	.146	-1.288
80	1427	-.416	.195	.142	-1.262
80	1428	-.306	.139	.123	-.718
80	1429	-.303	.136	.179	-.738
80	1430	-.307	.138	.223	-.829
80	1431	-.313	.142	.226	-.836
80	1432	-.320	.141	.198	-.822
80	1433	-.337	.145	.180	-.825
80	1434	-.351	.141	.089	-.891
80	1435	-.387	.158	.115	-1.130
80	1436	-.399	.161	.085	-1.076
80	1437	-.329	.140	.130	-.818
80	1438	-.317	.139	.141	-.793
80	1439	-.322	.135	.093	-.873
80	1440	-.339	.143	.201	-.867
80	1441	-.344	.147	.249	-.914
80	1442	-.371	.150	.174	-1.013
80	1443	-.387	.155	.096	-1.182
80	1444	-.459	.177	.024	-1.228
80	1445	-.462	.178	.028	-1.200
80	1446	-.337	.150	.134	-1.029
80	1447	-.316	.152	.164	-.834
80	1448	-.361	.146	.095	-.908
80	1449	-.377	.152	.098	-.931
80	1450	-.364	.144	.115	-.834
80	1451	-.386	.159	.120	-1.310

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
80	1452	-.406	.169	.093	-1.730
80	1453	-.373	.161	.268	-1.288
80	1454	-.356	.159	.160	-1.077
80	1455	-.372	.197	.211	-1.355
80	1456	-.520	.207	.102	-1.517
80	1457	-.411	.201	.180	-1.497
80	1458	-.473	.213	.154	-1.575
80	1459	-.443	.210	.188	-1.564
80	1460	-.520	.242	.122	-1.905
80	1461	-.320	.197	.353	-1.099
80	1462	-.256	.189	.320	-1.114
80	1463	-.226	.187	.301	-1.239
80	1464	.216	.358	1.253	-.754
80	1465	-.187	.149	.291	-.724
80	1466	-.091	.147	.386	-.622
80	1467	-.089	.140	.360	-.598
80	1801	-.079	.117	.304	-.446
80	1802	-.076	.115	.377	-.485
80	1803	-.153	.129	.292	-.588
80	1804	-.135	.131	.345	-.580
80	1805	-.124	.125	.316	-.542
80	1806	-.131	.128	.306	-.658
80	1807	-.099	.119	.281	-.482
80	2101	.367	.213	1.136	-.454
80	2102	-.136	.185	.385	-1.092
80	2103	.001	.210	.682	-1.403
80	2104	-.208	.162	.354	-.960
80	2105	.124	.212	.807	-.657
80	2106	.047	.172	.714	-.483
80	2107	-.163	.164	.374	-1.144
80	2108	-.080	.176	.499	-.874
80	2109	.050	.152	.568	-.419
80	2110	.049	.154	.689	-.440
80	2111	-.031	.126	.428	-.530
80	2112	.053	.167	.595	-.533
80	2113	-.373	.193	.609	-1.200
80	2114	.050	.162	.545	-.583
80	2115	-.057	.170	.519	-.863
80	2116	-.045	.143	.436	-.510
80	2117	-.205	.140	.233	-.750
80	2118	-.142	.138	.299	-.629
80	2119	-.139	.120	.239	-.545
80	2120	-.140	.117	.286	-.550
80	2121	-.146	.132	.327	-.685
80	2122	.144	.177	.711	-.489
80	2123	-.153	.125	.302	-.570
80	2124	-.190	.155	.266	-.736
80	2125	-.132	.132	.276	-.578
80	2126	.113	.179	.818	-.366
80	2127	.026	.133	.801	-.445

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
80	2128	.221	.195	.922	-.333
80	2129	-.095	.169	.505	-.853
80	2130	-.084	.134	.337	-.556
80	2131	-.162	.137	.301	-.640
80	2132	-.165	.137	.300	-.639
80	2133	-.152	.137	.321	-.567
80	2134	-.133	.136	.349	-.564
80	2135	-.128	.120	.307	-.533
80	2136	-.135	.120	.243	-.530
80	2137	.005	.130	.542	-.399
80	2138	-.157	.124	.256	-.601
80	2139	-.131	.143	.364	-.817
80	2140	-.208	.154	.287	-.800
80	2141	-.072	.133	.436	-.516
80	2142	-.115	.133	.446	-.697
80	2143	-.162	.116	.206	-.567
80	2144	-.165	.116	.200	-.547
80	2145	-.158	.116	.210	-.527
80	2146	-.129	.113	.228	-.497
80	2147	-.127	.121	.347	-.551
80	2148	-.155	.122	.342	-.591
80	2149	-.124	.121	.352	-.560
80	2150	-.038	.136	.464	-.589
80	2151	.089	.130	.626	-.392
80	2152	.169	.161	.762	-.371
80	2153	-.151	.123	.290	-.566
80	2154	-.104	.121	.319	-.569
80	2201	.314	.164	.893	-.281
80	2202	.259	.155	.855	-.264
80	2203	.221	.147	.733	-.278
80	2204	.144	.141	.802	-.469
80	2205	.235	.189	1.063	-.426
80	2206	.051	.150	.690	-.622
80	2207	.147	.140	.643	-.435
80	2208	.129	.136	.574	-.392
80	2209	.110	.150	.592	-.437
80	2210	.043	.175	.609	-.547
80	2211	.065	.138	.535	-.412
80	2212	.038	.131	.622	-.440
80	2213	-.030	.145	.569	-.478
80	2214	.042	.140	.512	-.455
80	2215	.017	.137	.422	-.456
80	2216	.020	.134	.458	-.422
80	2217	.059	.144	.507	-.381
80	2218	.015	.157	.608	-.529
80	2219	-.067	.132	.441	-.470
80	2220	-.031	.123	.390	-.412
80	2221	-.040	.103	.292	-.324
80	2222	-.062	.131	.409	-.600
80	2224	.013	.148	.560	-.605
80	2225	-.111	.174	.390	-.794
80	2226	-.019	.127	.393	-.413
80	2227	-.026	.123	.352	-.492
80	2228	-.029	.129	.456	-.485
80	2229	-.057	.120	.315	-.538
80	2230	-.400	.095	-.178	-.617
80	2231	-.036	.125	.451	-.505
80	2232	-.033	.133	.470	-.582
80	2233	-.089	.147	.301	-.740
80	2234	-.051	.121	.341	-.513
80	2235	-.024	.121	.411	-.471
80	2236	-.028	.125	.413	-.433
80	2237	-.010	.127	.472	-.447
80	2238	-.126	.130	.257	-.595
80	2239	-.037	.135	.355	-.527
80	2240	-.104	.140	.350	-.610
80	2301	-.309	.161	.129	-.969
80	2302	-.272	.160	.211	-1.087
80	2303	-.116	.132	.412	-.586
80	2304	-.180	.145	.422	-.850
80	2305	-.281	.179	.364	-1.241
80	2306	-.303	.189	.345	-.997
80	2307	-.073	.180	.708	-.815
80	2308	.161	.227	1.033	-.599
80	2309	-.261	.154	.253	-.946
80	2310	-.156	.134	.283	-.744
80	2311	-.130	.122	.353	-.560
80	2312	-.097	.117	.336	-.508
80	2313	-.075	.115	.354	-.475
80	2314	-.076	.113	.345	-.436
80	2315	-.084	.118	.357	-.458
80	2401	-.283	.138	.164	-.799
80	2402	-.273	.136	.140	-.746
80	2403	-.279	.150	.166	-.869
80	2404	.151	.146	.589	-.387
80	2405	-.099	.122	.309	-.505
80	2406	-.087	.121	.317	-.488
80	2407	-.280	.131	.169	-.849
80	2408	-.260	.140	.236	-.893
80	2409	.090	.146	.585	-.504
80	2411	-.276	.128	.120	-.952
80	2412	-.217	.128	.240	-.671
80	2413	-.243	.173	.322	-.962
80	2414	.038	.134	.515	-.487
80	2415	-.138	.126	.280	-.623
80	2416	-.122	.120	.309	-.562
80	2417	-.127	.118	.422	-.577
80	2418	-.226	.154	.297	-.816
80	2419	-.184	.155	.329	-.715
80	2420	-.198	.158	.346	-.755
80	2421	-.086	.113	.313	-.525
80	2422	-.090	.113	.294	-.531
80	2423	-.122	.136	.370	-.583
80	2424	-.147	.137	.366	-.571
80	2425	-.143	.136	.338	-.553
80	2426	-.160	.136	.341	-.571
80	2427	-.106	.131	.354	-.595
80	2428	-.089	.129	.411	-.562
80	2429	-.097	.132	.328	-.546
80	2430	-.103	.120	.278	-.479
80	2431	-.102	.123	.289	-.612
80	2432	-.098	.121	.273	-.574
80	2433	-.075	.119	.290	-.561
80	2434	-.094	.118	.253	-.566
80	2435	-.097	.115	.362	-.482
80	2436	-.130	.119	.267	-.612
80	2437	-.114	.114	.334	-.516
80	2438	-.132	.115	.307	-.539
80	2439	-.154	.120	.185	-.543
80	2440	-.066	.120	.288	-.422
80	2441	-.092	.118	.254	-.461
80	2442	-.130	.118	.240	-.509
80	2443	-.132	.125	.342	-.528
80	2444	-.101	.129	.357	-.525
80	2445	-.092	.125	.349	-.502
80	2446	-.090	.124	.359	-.496
80	2447	-.077	.128	.347	-.454
80	2448	-.072	.128	.354	-.439
80	2449	-.068	.128	.355	-.438
80	2450	-.072	.126	.321	-.436
80	2451	.023	.120	.487	-.380
80	2501	-.299	.145	.121	-.778
80	2502	-.308	.167	.225	-1.029
80	2503	-.352	.168	.125	-1.218
80	2504	-.307	.146	.122	-.814
80	2505	-.297	.150	.187	-.824
80	2506	-.276	.163	.194	-1.435
80	2507	-.316	.151	.186	-1.122
80	2508	-.323	.173	.211	-.925
80	2509	-.229	.155	.357	-.767
80	2510	-.206	.155	.393	-.796
80	2511	-.163	.129	.245	-.639
80	2601	-.362	.199	.303	-1.431
80	2602	-.192	.156	.305	-.914
80	2603	-.247	.167	.280	-1.066
80	2604	-.127	.166	.435	-1.078
80	2605	-.114	.140	.347	-.724
80	2606	-.121	.134	.333	-.630
80	2607	-.444	.174	.123	-1.142
80	2608	-.179	.150	.305	-1.008

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
80	2609	-.149	.126	.274	-.595
80	2610	-.090	.120	.301	-.525
80	2611	-.202	.131	.257	-.640
80	2612	-.085	.120	.323	-.498
80	2613	-.139	.126	.276	-.571
80	2614	-.032	.150	.423	-.656
80	2615	-.295	.171	.190	-1.073
80	2616	-.141	.127	.296	-.664
80	2617	-.119	.115	.233	-.542
80	2618	-.075	.110	.270	-.491
80	2619	-.191	.124	.182	-.654
80	2620	-.082	.117	.275	-.537
80	2621	-.108	.137	.308	-.533
80	5102	-.068	.142	.441	-.661
80	5103	-.077	.185	.507	-1.444
80	5104	-.057	.138	.578	-.571
80	5105	-.052	.163	.659	-.644
80	5106	-.047	.129	.547	-.476
80	5107	-.103	.124	.312	-.674
80	5108	-.084	.118	.298	-.505
80	5109	-.081	.117	.359	-.490
80	5110	-.078	.114	.343	-.534
80	5111	-.081	.110	.335	-.454
80	5112	-.078	.111	.314	-.463
80	5114	-.090	.126	.302	-.506
80	5202	-.040	.176	.679	-.645
80	5203	-.099	.131	.455	-.612
80	5204	-.091	.120	.337	-.563
80	5301	-.090	.141	.412	-.630
80	5302	-.081	.132	.469	-.549
80	5303	-.076	.120	.401	-.759
80	5304	-.063	.117	.321	-.508
80	5305	-.050	.116	.340	-.396
80	5901	-.111	.166	.464	-.787
80	5902	-.078	.116	.306	-.546
80	6101	-.202	.122	.226	-.732
80	6102	-.178	.113	.272	-.555
80	6103	-.191	.116	.235	-.648
80	6104	-.169	.116	.216	-.572
80	6105	-.176	.118	.239	-.558
80	6106	-.058	.118	.339	-.415
80	6201	-.061	.115	.309	-.467
80	6301	-.144	.123	.283	-.535
80	6302	-.145	.122	.290	-.530
80	6901	-.162	.126	.317	-.569
80	7101	-.149	.134	.289	-.668
80	7102	-.166	.138	.332	-.678
80	7103	-.093	.122	.336	-.509
80	7104	-.081	.135	.471	-.496
80	7105	-.059	.118	.375	-.519
80	7106	-.130	.118	.276	-.560
80	7201	-.156	.134	.296	-.704
80	7301	-.146	.139	.358	-.649
80	9101	-.469	.160	.062	-1.164
80	9102	.002	.179	.596	-.697
80	9103	.138	.251	1.128	-.692
80	9104	-.068	.272	.697	-1.363
80	9105	-.448	.167	.139	-1.048
80	9106	.131	.187	.814	-.593
80	9107	-.462	.175	.164	-1.110
80	9108	-.277	.135	.167	-.698
80	9109	-.312	.162	.252	-.897
80	9110	-.319	.185	.299	-1.792
80	9111	-.280	.146	.252	-.790
80	9112	-.212	.175	.443	-.950
80	9113	-.282	.147	.265	-.900
80	9114	-.257	.158	.241	-.811
80	9115	-.266	.161	.319	-.821
80	9116	-.244	.139	.231	-.726
80	9117	-.254	.159	.296	-.900
80	9118	-.098	.131	.395	-.815
80	9119	-.129	.148	.376	-1.258
80	9120	-.232	.144	.217	-.896
80	9121	-.185	.133	.249	-.594
80	9122	-.211	.146	.242	-.663
80	9123	-.079	.148	.450	-.587
80	9124	-.150	.148	.328	-.807
80	9125	-.142	.135	.326	-.584
80	9126	-.170	.149	.330	-.804
80	9201	.300	.188	1.032	-.287
80	9202	.304	.221	1.322	-.294
80	9203	-.088	.160	.449	-.625
80	9204	-.046	.135	.379	-.550
80	9205	-.030	.157	.517	-.703
80	9206	-.024	.130	.582	-.493
80	9207	.371	.222	1.234	-.270
80	9208	.096	.195	.898	-.559
80	9209	.059	.154	.691	-.444
80	9210	-.088	.143	.454	-.575
80	9211	-.129	.126	.331	-.613
80	9212	.158	.186	1.071	-.481
80	9213	-.082	.134	.393	-.627
80	9214	.049	.146	.530	-.472
80	9215	-.046	.137	.401	-.537
80	9216	-.076	.132	.368	-.585
80	9217	-.073	.133	.376	-.650
80	9218	-.064	.136	.385	-.639
80	9219	.251	.165	.945	-.267
80	9220	.106	.151	.739	-.393
80	9221	.021	.135	.523	-.437
80	9222	-.032	.138	.461	-.550
80	9223	-.084	.131	.350	-.567
80	9224	-.072	.117	.333	-.452
80	9225	.141	.163	.731	-.522
80	9226	.034	.138	.459	-.477
80	9227	.059	.121	.446	-.364
80	9228	-.034	.114	.334	-.379
80	9229	.195	.163	.935	-.347
80	9230	-.023	.115	.361	-.389
80	9231	-.063	.129	.341	-.505
80	9232	.103	.160	.608	-.373
80	9233	.056	.143	.534	-.414
80	9234	.022	.128	.407	-.479
80	9235	-.023	.113	.344	-.383
80	9236	-.169	.133	.254	-.618
80	9237	-.015	.120	.358	-.411
80	9238	-.033	.128	.407	-.483
90	1101	.504	.169	1.090	-.083
90	1102	.460	.169	1.008	-.167
90	1103	.290	.154	.782	-.325
90	1104	.226	.148	.691	-.354
90	1105	.165	.156	.795	-.356
90	1106	.042	.147	.591	-.407
90	1107	-.024	.145	.505	-.469
90	1108	.608	.175	1.219	.075
90	1109	.665	.187	1.374	.092
90	1110	.578	.185	1.302	.022
90	1111	.472	.178	1.190	-.069
90	1112	.351	.171	.980	-.175
90	1113	.113	.143	.572	-.302
90	1114	-.082	.133	.319	-.493
90	1115	.605	.166	1.401	.086
90	1116	.636	.170	1.393	.121
90	1117	.570	.164	1.119	.039
90	1118	.449	.158	.949	-.031
90	1119	.307	.148	.789	-.140
90	1120	.058	.135	.497	-.366
90	1121	-.079	.132	.455	-.475
90	1122	.580	.185	1.337	-.407
90	1123	.574	.182	1.258	-.057
90	1124	.453	.172	1.065	-.034
90	1125	.333	.161	.855	-.171
90	1126	.198	.157	.706	-.271
90	1127	-.023	.142	.430	-.473
90	1128	-.160	.135	.242	-.596
90	1129	.437	.193	1.247	-.572
90	1130	.397	.174	1.196	-.205
90	1131	.248	.157	.904	-.307
90	1132	.140	.151	.711	-.383
90	1133	.047	.150	.566	-.444

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
90	1134	-.132	.144	.401	-.600
90	1135	-.229	.136	.251	-.671
90	1136	-.139	.231	.646	-.999
90	1137	.088	.215	.598	-.892
90	1138	.074	.132	.508	-.367
90	1139	.010	.121	.428	-.464
90	1140	-.059	.123	.379	-.548
90	1141	-.186	.124	.274	-.676
90	1142	-.245	.124	.187	-.736
90	1143	.026	.147	.598	-.418
90	1144	.165	.146	.771	-.345
90	1145	.169	.140	.724	-.485
90	1146	.167	.138	.700	-.265
90	1147	.147	.148	.729	-.420
90	1148	-.067	.168	.545	-.572
90	1149	-.188	.152	.353	-.725
90	1150	.172	.157	.826	-.261
90	1151	.173	.154	.844	-.292
90	1152	.071	.146	.766	-.444
90	1201	.346	.184	1.049	-.403
90	1202	-.215	.138	.249	-.676
90	1203	-.333	.152	.258	-.964
90	1204	-.142	.136	.272	-.600
90	1205	-.112	.135	.301	-.580
90	1206	-.050	.132	.339	-.533
90	1207	-.002	.132	.404	-.500
90	1208	-.050	.236	.682	-.866
90	1209	-.119	.227	.817	-.912
90	1210	.090	.157	.815	-.490
90	1211	-.005	.127	.424	-.523
90	1212	-.034	.145	.375	-.490
90	1213	-.015	.144	.407	-.472
90	1214	.012	.117	.402	-.387
90	1215	.095	.123	.505	-.341
90	1216	.176	.129	.601	-.382
90	1217	.019	.255	.717	-1.021
90	1218	.005	.235	.806	-.729
90	1219	.032	.122	.444	-.329
90	1220	.028	.119	.419	-.328
90	1221	.008	.124	.427	-.432
90	1222	.017	.124	.438	-.371
90	1223	.167	.123	.551	-.325
90	1224	.149	.139	.640	-.305
90	1225	.233	.148	.790	-.367
90	1226	.098	.273	.967	-.822
90	1227	.074	.248	1.047	-.777
90	1228	.045	.122	.450	-.319
90	1229	.043	.118	.430	-.313
90	1230	.040	.135	.481	-.414
90	1231	.054	.137	.495	-.424

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
90	1232	.086	.136	.527	-.393
90	1233	.193	.140	.626	-.298
90	1234	.303	.141	.724	-.199
90	1235	.300	.225	.918	-.724
90	1236	.242	.238	.937	-.566
90	1237	.113	.131	.553	-.327
90	1238	.087	.125	.481	-.346
90	1239	.094	.127	.497	-.361
90	1240	.124	.130	.560	-.330
90	1241	.153	.135	.623	-.320
90	1242	.274	.143	.795	-.191
90	1243	.392	.154	.944	-.085
90	1244	.432	.175	1.025	-.406
90	1245	.412	.212	1.109	-.606
90	1246	.543	.204	1.378	-.177
90	1247	.209	.132	.690	-.213
90	1248	.113	.138	.617	-.339
90	1249	.190	.133	.658	-.231
90	1250	.227	.130	.619	-.281
90	1251	.302	.140	.771	-.251
90	1252	.455	.157	.973	-.179
90	1253	.525	.179	1.155	-.184
90	1254	.477	.184	1.115	-.083
90	1301	-.310	.151	.234	-1.110
90	1302	-.297	.149	.253	-1.527
90	1303	-.245	.139	.279	-.858
90	1304	-.275	.137	.262	-.964
90	1305	-.289	.126	.132	-.745
90	1306	-.273	.121	.172	-.697
90	1307	-.226	.119	.208	-.633
90	1308	-.288	.125	.100	-.782
90	1309	-.291	.130	.117	-.726
90	1310	-.287	.127	.097	-.694
90	1311	-.247	.121	.110	-.628
90	1312	-.273	.125	.107	-.673
90	1313	-.282	.122	.077	-.737
90	1314	-.281	.123	.089	-.737
90	1315	-.270	.118	.115	-.703
90	1316	-.286	.120	.135	-.703
90	1317	-.288	.130	.087	-.724
90	1318	-.290	.130	.086	-.724
90	1319	-.248	.125	.104	-.675
90	1320	-.271	.128	.100	-.713
90	1321	-.284	.124	.133	-.715
90	1322	-.329	.128	.076	-.690
90	1323	-.269	.120	.119	-.630
90	1324	-.290	.121	.123	-.683
90	1325	-.308	.128	.122	-.727
90	1326	-.305	.131	.139	-.736
90	1327	-.247	.125	.177	-.681

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
90	1328	-.271	.128	.165	-.710
90	1329	-.350	.131	.098	-.857
90	1330	-.323	.130	.133	-.835
90	1331	-.250	.124	.141	-.776
90	1332	-.277	.129	.171	-.715
90	1333	-.324	.134	.143	-.915
90	1334	-.319	.135	.144	-.875
90	1335	-.258	.128	.175	-.790
90	1336	-.275	.122	.184	-.667
90	1337	-.286	.123	.162	-.683
90	1338	-.279	.132	.149	-.713
90	1339	-.311	.128	.146	-.873
90	1340	-.272	.136	.188	-.798
90	1401	-.289	.127	.249	-.697
90	1402	-.239	.122	.343	-.625
90	1403	-.301	.128	.143	-.840
90	1404	-.298	.135	.146	-.827
90	1405	-.299	.136	.152	-.810
90	1406	-.275	.131	.209	-.735
90	1407	-.318	.138	.231	-.804
90	1408	-.347	.154	.146	-1.132
90	1409	-.354	.165	.203	-1.281
90	1410	-.256	.123	.173	-.663
90	1411	-.262	.133	.143	-.723
90	1412	-.246	.124	.195	-.796
90	1413	-.276	.127	.166	-.873
90	1414	-.295	.131	.197	-.718
90	1415	-.308	.134	.235	-.793
90	1416	-.285	.132	.248	-.774
90	1417	-.340	.148	.194	-1.000
90	1418	-.342	.145	.050	-1.236
90	1419	-.283	.134	.144	-.730
90	1420	-.203	.126	.200	-.625
90	1421	-.284	.130	.143	-.715
90	1423	-.273	.129	.159	-.680
90	1424	-.324	.131	.082	-.846
90	1425	-.342	.131	.078	-.848
90	1426	-.333	.136	.160	-.853
90	1427	-.372	.141	.130	-.881
90	1428	-.294	.131	.139	-.701
90	1429	-.296	.128	.079	-.722
90	1430	-.310	.131	.151	-.889
90	1431	-.317	.133	.138	-.890
90	1432	-.280	.128	.157	-.830
90	1433	-.321	.133	.147	-.895
90	1434	-.354	.132	.148	-.852
90	1435	-.379	.140	.083	-.916
90	1436	-.344	.136	.112	-.993
90	1437	-.339	.135	.062	-.780
90	1438	-.248	.127	.140	-.670

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
90	1439	-.324	.130	.153	-.771
90	1440	-.345	.126	.024	-.807
90	1441	-.346	.129	.027	-.827
90	1442	-.320	.125	.029	-.780
90	1443	-.362	.129	.011	-.863
90	1444	-.399	.152	.071	-.911
90	1445	-.397	.153	.076	-.888
90	1446	-.322	.139	.093	-.836
90	1447	-.302	.140	.161	-.758
90	1448	-.296	.142	.147	-.731
90	1449	-.334	.146	.114	-.800
90	1450	-.347	.141	.240	-.809
90	1451	-.363	.148	.264	-1.036
90	1452	-.338	.145	.268	-1.001
90	1453	-.369	.150	.234	-1.091
90	1454	-.369	.136	.048	-.837
90	1455	-.341	.148	.156	-.983
90	1456	-.352	.147	.100	-.859
90	1457	-.363	.149	.097	-.891
90	1458	-.366	.155	.098	-.913
90	1459	-.366	.156	.115	-.959
90	1460	-.364	.165	.147	-1.109
90	1461	-.341	.164	.161	-1.117
90	1462	-.313	.156	.243	-1.177
90	1463	-.328	.160	.284	-1.136
90	1464	.319	.295	1.104	-.624
90	1465	-.213	.124	.161	-.623
90	1466	-.182	.124	.201	-.642
90	1467	-.199	.121	.171	-.627
90	1801	-.114	.122	.365	-.579
90	1802	-.177	.129	.194	-.634
90	1803	-.165	.141	.303	-.686
90	1804	-.107	.146	.358	-.625
90	1805	-.171	.125	.290	-.649
90	1806	-.271	.151	.164	-.871
90	1807	-.179	.123	.216	-.610
90	2101	.557	.187	1.439	-.051
90	2102	.076	.178	.662	-.663
90	2103	.064	.216	.713	-1.102
90	2104	-.221	.188	.408	-1.013
90	2105	.477	.182	1.179	-.037
90	2106	.403	.179	1.120	-.107
90	2107	.179	.150	.694	-.432
90	2108	.201	.145	.717	-.301
90	2109	.264	.163	1.019	-.277
90	2110	.103	.153	.741	-.468
90	2111	.222	.163	.830	-.883
90	2112	.263	.150	.860	-.372
90	2113	-.340	.141	.100	-1.037
90	2114	-.031	.216	.708	-.821

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
90	2115	.017	.165	.546	-.829
90	2116	.206	.155	.785	-.337
90	2117	-.408	.184	.117	-1.139
90	2118	-.353	.190	.176	-1.351
90	2119	-.177	.145	.388	-.859
90	2120	-.160	.132	.355	-.701
90	2121	-.180	.139	.398	-.759
90	2122	.054	.180	.837	-.479
90	2123	-.426	.215	.230	-1.397
90	2124	-.083	.154	.412	-.598
90	2125	-.273	.161	.228	-.863
90	2126	-.039	.143	.469	-.438
90	2127	.053	.155	.516	-.514
90	2128	.222	.209	.963	-.384
90	2129	-.225	.157	.355	-.782
90	2130	-.116	.169	.404	-.732
90	2131	-.194	.142	.241	-.656
90	2132	-.204	.143	.233	-.681
90	2133	-.222	.141	.221	-.719
90	2134	-.195	.138	.295	-.688
90	2135	-.177	.144	.328	-.617
90	2136	-.195	.143	.270	-.632
90	2137	.039	.154	.496	-.481
90	2138	-.211	.143	.219	-.649
90	2139	-.215	.141	.226	-.725
90	2140	-.176	.165	.423	-.779
90	2141	-.164	.170	.516	-.795
90	2142	-.247	.195	.495	-.958
90	2143	-.185	.131	.298	-.630
90	2144	-.190	.134	.241	-.636
90	2145	-.177	.131	.376	-.613
90	2146	-.142	.127	.327	-.633
90	2147	-.193	.129	.271	-.706
90	2148	-.158	.125	.297	-.629
90	2149	-.128	.127	.342	-.587
90	2150	.084	.156	.654	-.501
90	2151	.083	.144	.733	-.494
90	2152	.203	.194	.929	-.374
90	2153	-.199	.136	.293	-.679
90	2154	-.167	.141	.327	-.620
90	2201	.400	.154	.971	-.097
90	2202	.386	.159	1.006	-.097
90	2203	.319	.149	.790	-.158
90	2204	.253	.141	.686	-.221
90	2205	.518	.186	1.217	-.023
90	2206	.096	.166	.906	-.406
90	2207	.235	.150	.762	-.211
90	2208	.205	.142	.809	-.254
90	2209	.235	.155	.789	-.231
90	2210	.428	.180	1.046	-.140

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
90	2211	.086	.154	.603	-.428
90	2212	.057	.149	.531	-.491
90	2213	-.044	.140	.484	-.502
90	2214	.085	.137	.512	-.355
90	2215	.034	.133	.449	-.378
90	2216	-.020	.131	.352	-.410
90	2217	.240	.168	.796	-.322
90	2218	.209	.191	.975	-.306
90	2219	.087	.183	.796	-.511
90	2220	-.059	.136	.363	-.512
90	2221	-.039	.113	.317	-.385
90	2222	-.052	.133	.336	-.544
90	2224	.029	.154	.614	-.540
90	2225	-.056	.148	.430	-.554
90	2226	-.023	.139	.508	-.506
90	2227	-.020	.134	.430	-.484
90	2228	-.009	.136	.469	-.537
90	2229	-.042	.130	.458	-.520
90	2230	.246	.089	.456	.040
90	2231	-.005	.134	.507	-.535
90	2232	.015	.129	.487	-.590
90	2233	-.035	.147	.454	-.593
90	2234	-.040	.125	.438	-.468
90	2235	-.002	.124	.500	-.444
90	2236	-.000	.132	.416	-.504
90	2237	.031	.137	.480	-.455
90	2238	-.108	.131	.341	-.620
90	2239	.019	.142	.487	-.449
90	2240	-.046	.161	.382	-.693
90	2301	-.325	.143	.158	-1.007
90	2302	-.303	.137	.090	-.766
90	2303	-.232	.138	.203	-.716
90	2304	-.220	.135	.213	-.821
90	2305	-.341	.153	.139	-1.072
90	2306	-.340	.165	.154	-1.000
90	2307	-.233	.181	.348	-.950
90	2308	.269	.210	.962	-.463
90	2309	-.337	.136	.065	-.800
90	2310	-.225	.132	.231	-.694
90	2311	-.206	.137	.256	-.796
90	2312	-.167	.134	.264	-.632
90	2313	-.076	.123	.303	-.458
90	2314	-.137	.129	.273	-.540
90	2315	-.105	.127	.332	-.481
90	2401	-.308	.146	.163	-.776
90	2402	-.299	.146	.172	-.798
90	2403	-.290	.149	.181	-.779
90	2404	.219	.148	.723	-.347
90	2405	-.186	.131	.354	-.673
90	2406	-.201	.137	.319	-.687

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
90	2407	-.328	.135	.094	-.771
90	2408	-.320	.137	.171	-.799
90	2409	.153	.144	.646	-.396
90	2411	-.320	.129	.068	-.708
90	2412	-.291	.135	.168	-.752
90	2413	-.337	.140	.110	-1.006
90	2414	.068	.139	.558	-.399
90	2415	-.204	.131	.360	-.712
90	2416	-.214	.125	.186	-.652
90	2417	-.245	.128	.183	-.705
90	2418	-.285	.128	.147	-.825
90	2419	-.270	.141	.172	-1.020
90	2420	-.329	.152	.166	-.949
90	2421	-.141	.116	.245	-.592
90	2422	-.194	.123	.225	-.689
90	2423	-.222	.127	.176	-.666
90	2424	-.244	.130	.147	-.749
90	2425	-.224	.132	.196	-.719
90	2426	-.287	.137	.149	-.788
90	2427	-.176	.131	.275	-.611
90	2428	-.199	.132	.246	-.634
90	2429	-.137	.125	.279	-.515
90	2430	-.169	.122	.344	-.606
90	2431	-.173	.127	.300	-.588
90	2432	-.172	.126	.280	-.548
90	2433	-.060	.118	.381	-.429
90	2434	-.156	.122	.271	-.555
90	2435	-.164	.123	.231	-.592
90	2436	-.189	.119	.182	-.628
90	2437	-.141	.119	.242	-.525
90	2438	-.210	.126	.197	-.626
90	2439	-.246	.127	.184	-.678
90	2440	-.082	.128	.376	-.471
90	2441	-.103	.120	.307	-.545
90	2442	-.199	.124	.233	-.632
90	2443	-.204	.129	.268	-.685
90	2444	-.221	.141	.338	-.758
90	2445	-.140	.130	.361	-.603
90	2446	-.204	.136	.314	-.672
90	2447	-.169	.127	.304	-.603
90	2448	-.145	.127	.309	-.590
90	2449	-.071	.120	.393	-.513
90	2450	-.060	.125	.346	-.539
90	2451	-.000	.123	.397	-.385
90	2501	-.328	.142	.112	-.859
90	2502	-.316	.147	.139	-.809
90	2503	-.356	.147	.083	-.876
90	2504	-.347	.142	.085	-.830
90	2505	-.326	.134	.087	-.810
90	2506	-.329	.135	.130	-.769
90	2507	-.342	.134	.035	-.817
90	2508	-.336	.143	.098	-.895
90	2509	-.309	.145	.149	-.818
90	2510	-.299	.146	.141	-.868
90	2511	-.251	.134	.184	-.742
90	2601	-.446	.199	.174	-1.447
90	2602	-.405	.179	.224	-1.038
90	2603	-.278	.153	.171	-1.024
90	2604	-.229	.136	.234	-.816
90	2605	-.196	.125	.280	-.773
90	2606	-.172	.122	.427	-.598
90	2607	-.265	.125	.192	-.671
90	2608	-.417	.182	.231	-1.204
90	2609	-.397	.176	.128	-1.056
90	2610	-.273	.135	.223	-.753
90	2611	-.220	.124	.184	-.643
90	2612	-.195	.120	.253	-.635
90	2613	-.197	.128	.343	-.604
90	2614	-.085	.138	.408	-.603
90	2615	-.515	.284	.254	-1.971
90	2616	-.349	.207	.229	-1.658
90	2617	-.202	.140	.277	-.649
90	2618	-.168	.132	.266	-.598
90	2619	-.164	.133	.247	-.600
90	2620	-.176	.131	.259	-.750
90	2621	-.200	.127	.264	-.657
90	5102	-.166	.132	.390	-.640
90	5103	-.228	.211	.317	-1.597
90	5104	-.168	.125	.227	-.638
90	5105	-.174	.176	.859	-1.032
90	5106	-.166	.119	.298	-.554
90	5107	-.173	.129	.387	-.761
90	5108	-.170	.119	.320	-.632
90	5109	-.174	.128	.289	-.682
90	5110	-.125	.124	.308	-.531
90	5111	-.163	.112	.302	-.546
90	5112	-.140	.114	.267	-.513
90	5114	-.089	.136	.454	-.619
90	5202	-.073	.215	.883	-.840
90	5203	-.149	.128	.266	-.622
90	5204	-.146	.119	.302	-.529
90	5301	-.146	.127	.370	-.587
90	5302	-.145	.128	.312	-.697
90	5303	-.151	.124	.238	-1.283
90	5304	-.118	.123	.316	-.632
90	5305	-.036	.133	.450	-.470
90	5901	-.170	.181	.419	-.974
90	5902	-.160	.124	.273	-.651
90	6101	-.342	.132	.097	-.958
90	6102	-.322	.126	.120	-.799
90	6103	-.323	.131	.159	-.969
90	6104	-.329	.134	.118	-.907
90	6105	-.259	.131	.161	-.698
90	6106	-.082	.133	.439	-.534
90	6201	-.070	.127	.349	-.590
90	6301	-.320	.120	.079	-.678
90	6302	-.275	.119	.128	-.709
90	6901	-.327	.140	.131	-.775
90	7101	-.232	.145	.314	-.862
90	7102	-.233	.156	.448	-.941
90	7103	-.159	.137	.263	-.618
90	7104	-.058	.161	.497	-.619
90	7105	-.112	.135	.308	-.536
90	7106	-.129	.134	.344	-.582
90	7201	-.237	.142	.216	-.887
90	7301	-.265	.147	.371	-.878
90	9101	-.382	.140	.056	-.861
90	9102	.049	.170	.697	-.704
90	9103	.143	.277	.929	-.942
90	9104	-.405	.189	.264	-1.281
90	9105	-.354	.149	.185	-.974
90	9106	-.094	.211	.643	-.881
90	9107	-.335	.140	.215	-.790
90	9108	-.292	.133	.155	-.706
90	9109	-.316	.129	.137	-.752
90	9110	-.354	.158	.236	-1.015
90	9111	-.297	.123	.139	-.663
90	9112	-.327	.176	.241	-1.430
90	9113	-.326	.127	.136	-.722
90	9114	-.301	.128	.144	-.701
90	9115	-.332	.140	.134	-.817
90	9116	-.300	.132	.101	-.749
90	9117	-.336	.144	.138	-.815
90	9118	-.146	.127	.291	-.757
90	9119	-.240	.141	.244	-.839
90	9120	-.284	.132	.114	-.748
90	9121	-.274	.156	.210	-.842
90	9122	-.339	.176	.209	-.973
90	9123	-.217	.139	.213	-.881
90	9124	-.255	.136	.183	-.833
90	9125	-.198	.124	.211	-.650
90	9126	-.358	.175	.165	-1.018
90	9201	.111	.190	1.018	-.429
90	9202	.222	.178	.845	-.281
90	9203	.212	.166	.821	-.326
90	9204	.138	.165	.930	-.441
90	9205	-.084	.160	.476	-.824
90	9206	-.013	.143	.477	-.544
90	9207	.581	.178	1.219	-.045
90	9208	.451	.173	1.005	-.084

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
90	9209	-.255	.168	.857	-.201
90	9210	-.040	.153	.410	-.715
90	9211	-.100	.135	.308	-.558
90	9212	.306	.152	1.043	-.188
90	9213	-.071	.126	.331	-.576
90	9214	.037	.131	.458	-.479
90	9215	-.041	.122	.394	-.575
90	9216	-.049	.120	.401	-.564
90	9217	-.054	.135	.407	-.457
90	9218	-.035	.137	.361	-.501
90	9219	.328	.149	.932	-.160
90	9220	.170	.138	.739	-.304
90	9221	-.022	.147	.476	-.516
90	9222	-.025	.132	.387	-.502
90	9223	-.087	.133	.455	-.498
90	9224	-.080	.127	.428	-.471
90	9225	.234	.160	.817	-.293
90	9226	.065	.148	.540	-.414
90	9227	.058	.133	.571	-.394
90	9228	.022	.120	.439	-.341
90	9229	.290	.157	.876	-.182
90	9230	-.025	.118	.425	-.417
90	9231	-.076	.118	.322	-.498
90	9232	.178	.163	.684	-.369
90	9233	.090	.152	.682	-.340
90	9234	.070	.129	.478	-.386
90	9235	-.043	.120	.439	-.507
90	9236	-.139	.127	.328	-.663
90	9237	-.031	.123	.427	-.543
90	9238	-.029	.126	.320	-.591
100	1101	.438	.184	1.086	-.159
100	1102	.348	.173	.961	-.192
100	1103	.171	.150	.687	-.287
100	1104	.104	.144	.605	-.351
100	1105	.060	.140	.525	-.392
100	1106	-.053	.130	.401	-.482
100	1107	-.099	.128	.361	-.555
100	1108	.644	.187	1.300	-.015
100	1109	.553	.188	1.160	-.048
100	1110	.410	.170	.870	-.165
100	1111	.307	.155	.758	-.224
100	1112	.197	.145	.625	-.342
100	1113	.027	.125	.440	-.365
100	1114	-.138	.121	.249	-.543
100	1115	.619	.184	1.278	-.138
100	1116	.587	.177	1.227	.065
100	1117	.438	.167	1.044	-.054
100	1118	.311	.159	.928	-.180
100	1119	.184	.148	.792	-.285
100	1120	-.021	.135	.527	-.442
100	1121	-.126	.126	.257	-.562
100	1122	.511	.211	1.195	-.364
100	1123	.493	.178	1.159	-.195
100	1124	.353	.157	.947	-.159
100	1125	.243	.151	.797	-.300
100	1126	.107	.146	.648	-.443
100	1127	-.087	.132	.376	-.584
100	1128	-.202	.128	.231	-.661
100	1129	.260	.263	.905	-.560
100	1130	.304	.222	.840	-.584
100	1131	.204	.149	.672	-.263
100	1132	.092	.141	.555	-.356
100	1133	-.016	.126	.399	-.461
100	1134	-.182	.121	.226	-.671
100	1135	-.257	.119	.128	-.746
100	1136	-.187	.166	.462	-.904
100	1137	-.113	.235	.627	-.712
100	1138	.068	.127	.451	-.354
100	1139	.001	.121	.427	-.446
100	1140	-.084	.120	.318	-.576
100	1141	-.218	.121	.176	-.723
100	1142	-.268	.122	.134	-.769
100	1143	-.045	.143	.397	-.611
100	1144	.113	.143	.613	-.373
100	1145	.101	.135	.547	-.326
100	1146	.083	.128	.495	-.355
100	1147	.042	.134	.506	-.570
100	1148	-.169	.152	.299	-.739
100	1149	-.256	.140	.238	-.779
100	1150	.119	.149	.709	-.494
100	1151	.094	.144	.634	-.378
100	1152	-.008	.122	.447	-.516
100	1201	.445	.188	1.278	-.190
100	1202	-.245	.126	.246	-.761
100	1203	-.375	.136	.117	-.848
100	1204	-.119	.136	.337	-.566
100	1205	-.075	.139	.408	-.540
100	1206	.015	.139	.515	-.448
100	1207	.080	.143	.618	-.408
100	1208	.234	.156	.877	-.355
100	1209	.283	.201	1.039	-.491
100	1210	.273	.198	1.134	-.317
100	1211	.059	.121	.472	-.401
100	1212	.019	.124	.475	-.414
100	1213	.052	.125	.504	-.384
100	1214	.090	.129	.492	-.367
100	1215	.203	.136	.622	-.239
100	1216	.317	.142	.736	-.128
100	1217	.454	.175	.916	-.417
100	1218	.495	.227	1.157	-.334
100	1219	.083	.130	.698	-.366
100	1220	.082	.125	.486	-.379
100	1221	.079	.139	.668	-.505
100	1222	.068	.124	.568	-.323
100	1223	.230	.128	.740	-.231
100	1224	.256	.154	.767	-.232
100	1225	.368	.165	.929	-.148
100	1226	.486	.189	1.103	-.316
100	1227	.501	.214	1.190	-.256
100	1228	.093	.129	.776	-.393
100	1229	.092	.125	.487	-.384
100	1230	.109	.131	.572	-.420
100	1231	.130	.135	.609	-.417
100	1232	.176	.136	.653	-.365
100	1233	.318	.145	.833	-.229
100	1234	.412	.141	.909	-.004
100	1235	.529	.156	1.061	.054
100	1236	.556	.168	1.161	-.051
100	1237	.143	.129	.798	-.257
100	1238	.123	.118	.494	-.246
100	1239	.122	.124	.538	-.253
100	1240	.162	.137	.668	-.298
100	1241	.194	.143	.726	-.304
100	1242	.333	.152	.925	-.187
100	1243	.461	.163	1.129	-.080
100	1244	.531	.160	1.077	-.070
100	1245	.531	.166	1.104	-.122
100	1246	.548	.193	1.216	-.056
100	1247	.234	.123	.626	-.130
100	1248	.143	.138	.639	-.321
100	1249	.218	.137	.773	-.226
100	1250	.268	.138	.763	-.182
100	1251	.342	.150	.858	-.122
100	1252	.495	.165	.990	-.045
100	1253	.549	.184	1.039	-.035
100	1254	.438	.171	.939	-.074
100	1301	-.304	.150	.147	-1.245
100	1302	-.297	.146	.179	-1.220
100	1303	-.259	.128	.156	-.711
100	1304	-.296	.126	.099	-.732
100	1305	-.309	.127	.118	-.879
100	1306	-.300	.123	.128	-.820
100	1307	-.254	.121	.161	-.764
100	1308	-.287	.129	.149	-.773
100	1309	-.278	.130	.197	-.832
100	1310	-.287	.127	.163	-.809
100	1311	-.252	.120	.176	-.712
100	1312	-.273	.124	.172	-.724
100	1313	-.291	.130	.191	-.722
100	1314	-.291	.132	.197	-.730

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
100	1315	-.263	.130	.162	-.637
100	1316	-.286	.130	.120	-.667
100	1317	-.297	.127	.074	-.717
100	1318	-.300	.127	.081	-.713
100	1319	-.258	.123	.113	-.642
100	1320	-.280	.127	.104	-.666
100	1321	-.279	.138	.170	-.909
100	1322	-.299	.142	.187	-.857
100	1323	-.253	.134	.199	-.818
100	1324	-.281	.134	.164	-.867
100	1325	-.311	.126	.155	-.788
100	1326	-.315	.129	.168	-.815
100	1327	-.276	.124	.187	-.769
100	1328	-.300	.127	.169	-.805
100	1329	-.344	.122	.046	-.743
100	1330	-.332	.123	.075	-.743
100	1331	-.282	.119	.095	-.668
100	1332	-.312	.123	.066	-.708
100	1333	-.336	.129	.100	-.763
100	1334	-.334	.131	.094	-.802
100	1335	-.291	.127	.130	-.727
100	1336	-.338	.133	.102	-.776
100	1337	-.346	.133	.110	-.764
100	1338	-.344	.127	.130	-.834
100	1339	-.359	.133	.063	-.805
100	1340	-.289	.125	.210	-.782
100	1401	-.284	.128	.124	-.694
100	1402	-.246	.125	.160	-.633
100	1403	-.301	.136	.140	-.753
100	1404	-.286	.131	.229	-.826
100	1405	-.287	.133	.229	-.850
100	1406	-.256	.127	.243	-.750
100	1407	-.286	.134	.224	-.775
100	1408	-.316	.146	.133	-1.002
100	1409	-.323	.154	.134	-1.233
100	1410	-.247	.124	.175	-.625
100	1411	-.250	.133	.175	-.696
100	1412	-.238	.125	.152	-.642
100	1413	-.266	.128	.127	-.680
100	1414	-.271	.123	.109	-.700
100	1415	-.280	.125	.123	-.722
100	1416	-.249	.121	.109	-.685
100	1417	-.283	.127	.128	-.778
100	1418	-.300	.137	.147	-.820
100	1419	-.267	.135	.167	-.769
100	1420	-.196	.128	.209	-.670
100	1421	-.268	.133	.171	-.660
100	1423	-.258	.123	.180	-.641
100	1424	-.293	.120	.134	-.684
100	1425	-.303	.122	.137	-.700
100	1426	-.272	.120	.175	-.671
100	1427	-.302	.125	.177	-.727
100	1428	-.283	.133	.120	-.755
100	1429	-.275	.121	.170	-.702
100	1430	-.289	.132	.120	-.689
100	1431	-.296	.134	.121	-.708
100	1432	-.259	.129	.138	-.652
100	1433	-.297	.130	.107	-.703
100	1434	-.305	.127	.169	-.713
100	1435	-.320	.132	.141	-.738
100	1436	-.288	.130	.164	-.701
100	1437	-.320	.124	.127	-.766
100	1438	-.240	.118	.182	-.651
100	1439	-.291	.125	.177	-.670
100	1440	-.336	.120	-.017	-.733
100	1441	-.340	.124	-.000	-.754
100	1442	-.321	.119	.011	-.701
100	1443	-.367	.122	.003	-.776
100	1444	-.376	.124	.109	-.794
100	1445	-.379	.126	.088	-.799
100	1446	-.306	.123	.119	-.716
100	1447	-.297	.125	.153	-.698
100	1448	-.277	.116	.142	-.665
100	1449	-.316	.120	.123	-.698
100	1450	-.327	.123	.107	-.743
100	1451	-.347	.130	.112	-.785
100	1452	-.332	.123	.109	-.732
100	1453	-.356	.123	.115	-.753
100	1454	-.357	.117	.070	-.784
100	1455	-.303	.119	.092	-.730
100	1456	-.312	.120	.089	-.723
100	1457	-.309	.120	.085	-.724
100	1458	-.338	.136	.202	-.858
100	1459	-.341	.136	.173	-.850
100	1460	-.347	.140	.189	-.840
100	1461	-.341	.135	.188	-.796
100	1462	-.317	.133	.128	-.745
100	1463	-.331	.135	.105	-.784
100	1464	-.041	.281	.970	-.708
100	1465	-.240	.128	.222	-.659
100	1466	-.201	.122	.225	-.646
100	1467	-.234	.119	.152	-.677
100	1801	-.128	.119	.235	-.517
100	1802	-.193	.122	.179	-.680
100	1803	-.144	.141	.332	-.609
100	1804	-.111	.147	.472	-.563
100	1805	-.225	.122	.178	-.619
100	1806	-.246	.130	.218	-.755
100	1807	-.224	.122	.128	-.645
100	2101	.601	.181	1.149	.002
100	2102	.061	.184	.707	-.570
100	2103	.072	.169	.584	-.803
100	2104	-.177	.159	.384	-.864
100	2105	.484	.194	1.144	-.129
100	2106	.363	.195	1.154	-.333
100	2107	.155	.190	.832	-.419
100	2108	.174	.172	.790	-.369
100	2109	.163	.174	1.043	-.445
100	2110	.040	.152	.614	-.410
100	2111	.203	.165	.966	-.334
100	2112	.227	.176	.835	-.299
100	2113	-.327	.129	.103	-.694
100	2114	-.218	.178	.523	-.972
100	2115	-.034	.162	.503	-.586
100	2116	.118	.173	.716	-.504
100	2117	-.225	.174	.313	-1.121
100	2118	-.355	.204	.185	-1.214
100	2119	-.273	.165	.177	-1.061
100	2120	-.210	.129	.177	-.692
100	2121	-.217	.126	.180	-.637
100	2122	-.026	.129	.366	-.503
100	2123	-.226	.170	.322	-.861
100	2124	-.135	.150	.338	-.732
100	2125	-.268	.148	.249	-.961
100	2126	-.056	.149	.413	-.484
100	2127	.100	.165	.714	-.382
100	2128	.118	.183	.861	-.416
100	2129	-.277	.127	.138	-.860
100	2130	-.238	.154	.306	-.766
100	2131	-.158	.125	.306	-.564
100	2132	-.161	.125	.276	-.599
100	2133	-.159	.125	.287	-.594
100	2134	-.204	.131	.212	-.702
100	2135	-.237	.142	.327	-.925
100	2136	-.236	.135	.297	-.741
100	2137	.084	.142	.689	-.489
100	2138	-.182	.128	.296	-.668
100	2139	-.281	.126	.131	-.695
100	2140	-.260	.134	.210	-.808
100	2141	-.266	.134	.202	-.774
100	2142	-.213	.165	.344	-.909
100	2143	-.151	.132	.332	-.580
100	2144	-.155	.132	.310	-.577
100	2145	-.143	.130	.322	-.597
100	2146	-.138	.133	.390	-.608
100	2147	-.220	.149	.254	-.824
100	2148	-.146	.130	.278	-.589
100	2149	-.132	.138	.347	-.651
100	2150	.160	.147	.591	-.427
100	2151	.088	.138	.500	-.448

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
100	2152	.132	.196	.894	-.400
100	2153	-.176	.130	.201	-.669
100	2154	-.202	.137	.207	-.708
100	2201	.423	.160	.958	-.125
100	2202	.432	.166	1.068	-.153
100	2203	.345	.161	.895	-.189
100	2204	.283	.154	.762	-.199
100	2205	.510	.186	1.017	-.097
100	2206	.083	.187	.709	-.531
100	2207	.230	.166	.767	-.330
100	2208	.215	.157	.717	-.301
100	2209	.257	.151	.860	-.251
100	2210	.414	.198	1.013	-.265
100	2211	.116	.147	.832	-.409
100	2212	.072	.144	.648	-.490
100	2213	-.093	.139	.495	-.590
100	2214	.047	.135	.487	-.460
100	2215	-.001	.129	.460	-.401
100	2216	-.028	.131	.453	-.432
100	2217	.177	.173	.867	-.433
100	2218	.089	.182	.908	-.489
100	2219	.052	.194	.912	-.523
100	2220	-.059	.133	.411	-.506
100	2221	-.023	.108	.345	-.428
100	2222	-.049	.128	.356	-.486
100	2224	.081	.147	.717	-.352
100	2225	-.042	.138	.456	-.608
100	2226	-.030	.130	.514	-.447
100	2227	-.008	.129	.577	-.481
100	2228	.018	.121	.518	-.370
100	2229	-.013	.113	.444	-.391
100	2230	.175	.247	.700	-.242
100	2231	.035	.119	.482	-.359
100	2232	.064	.124	.497	-.333
100	2233	.050	.141	.498	-.433
100	2234	-.011	.124	.472	-.403
100	2235	.040	.125	.486	-.367
100	2236	.045	.122	.439	-.353
100	2237	.096	.124	.520	-.312
100	2238	-.076	.123	.335	-.524
100	2239	.092	.124	.510	-.521
100	2240	.052	.134	.411	-.596
100	2301	-.405	.143	.144	-.903
100	2302	-.413	.147	.145	-.885
100	2303	-.265	.130	.156	-.875
100	2304	-.225	.120	.177	-.602
100	2305	-.340	.130	.075	-.791
100	2306	-.364	.138	.153	-.948
100	2307	-.317	.142	.225	-.837
100	2308	.137	.195	.859	-.428
100	2309	-.401	.147	.084	-.995
100	2310	-.252	.135	.210	-.697
100	2311	-.223	.132	.221	-.768
100	2312	-.200	.129	.256	-.614
100	2313	-.110	.120	.298	-.482
100	2314	-.169	.126	.227	-.572
100	2315	-.125	.116	.235	-.579
100	2401	-.365	.140	.170	-.831
100	2402	-.366	.142	.171	-.845
100	2403	-.383	.146	.157	-.856
100	2404	.255	.147	.772	-.177
100	2405	-.205	.135	.440	-.675
100	2406	-.233	.140	.225	-.711
100	2407	-.361	.129	.076	-.758
100	2408	-.405	.133	.054	-.909
100	2409	.166	.144	.712	-.296
100	2411	-.352	.121	.032	-.739
100	2412	-.382	.134	.046	-.894
100	2413	-.431	.153	.038	-1.081
100	2414	.068	.144	.588	-.461
100	2415	-.220	.126	.208	-.699
100	2416	-.233	.122	.226	-.693
100	2417	-.277	.127	.176	-.754
100	2418	-.336	.139	.115	-.849
100	2419	-.369	.160	.224	-1.091
100	2420	-.398	.169	.143	-1.008
100	2421	-.141	.125	.248	-.540
100	2422	-.190	.126	.240	-.650
100	2423	-.272	.145	.214	-.844
100	2424	-.289	.147	.211	-.879
100	2425	-.246	.153	.294	-.829
100	2426	-.341	.154	.251	-.924
100	2427	-.232	.123	.262	-.640
100	2428	-.216	.121	.159	-.676
100	2429	-.182	.116	.186	-.544
100	2430	-.235	.123	.148	-.683
100	2431	-.217	.131	.257	-.634
100	2432	-.222	.129	.224	-.634
100	2433	-.088	.122	.339	-.464
100	2434	-.205	.127	.218	-.575
100	2435	-.211	.123	.156	-.678
100	2436	-.235	.114	.212	-.632
100	2437	-.194	.116	.148	-.683
100	2438	-.256	.121	.111	-.722
100	2439	-.299	.121	.156	-.688
100	2440	-.072	.125	.381	-.508
100	2441	-.147	.113	.280	-.582
100	2442	-.237	.117	.164	-.631
100	2443	-.254	.119	.227	-.654
100	2444	-.203	.128	.241	-.674
100	2445	-.135	.118	.363	-.550
100	2446	-.196	.121	.315	-.622
100	2447	-.171	.120	.217	-.666
100	2448	-.135	.129	.298	-.653
100	2449	-.076	.120	.287	-.589
100	2450	-.019	.127	.408	-.601
100	2451	-.019	.118	.348	-.404
100	2501	-.357	.120	.049	-.804
100	2502	-.381	.128	.042	-.833
100	2503	-.375	.119	-.014	-.821
100	2504	-.368	.120	.050	-.809
100	2505	-.351	.131	.105	-.747
100	2506	-.432	.152	.056	-.975
100	2507	-.362	.135	.104	-.795
100	2508	-.371	.136	.104	-.821
100	2509	-.346	.136	.095	-.859
100	2510	-.341	.136	.084	-.876
100	2511	-.311	.135	.136	-.909
100	2601	-.309	.157	.251	-.976
100	2602	-.330	.171	.205	-1.262
100	2603	-.263	.145	.264	-1.154
100	2604	-.251	.128	.157	-.923
100	2605	-.251	.133	.173	-.837
100	2606	-.195	.120	.241	-.581
100	2607	-.290	.123	.132	-.723
100	2608	-.344	.153	.218	-.831
100	2609	-.367	.159	.143	-.986
100	2610	-.234	.138	.244	-.628
100	2611	-.230	.133	.182	-.633
100	2612	-.242	.143	.182	-.931
100	2613	-.226	.126	.229	-.680
100	2614	-.124	.129	.356	-.583
100	2615	-.407	.196	.158	-1.304
100	2616	-.297	.166	.337	-1.075
100	2617	-.212	.138	.239	-.702
100	2618	-.223	.133	.191	-.646
100	2619	-.240	.136	.205	-.889
100	2620	-.219	.125	.280	-.618
100	2621	-.232	.128	.218	-.646
100	5102	-.170	.142	.312	-.796
100	5103	-.183	.300	.525	-1.436
100	5104	-.180	.128	.235	-.707
100	5105	.012	.221	.852	-.893
100	5106	-.178	.120	.250	-.650
100	5107	-.353	.194	.191	-1.363
100	5108	-.238	.135	.168	-.692
100	5109	-.184	.130	.269	-.630
100	5110	-.189	.134	.304	-.686
100	5111	-.218	.127	.249	-.732
100	5112	-.182	.127	.235	-.598

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
100	5114	-.143	.122	.234	-.616
100	5202	.116	.223	.868	-.598
100	5203	-.184	.159	.347	-.719
100	5204	-.159	.122	.229	-.669
100	5301	-.177	.129	.232	-.660
100	5302	-.158	.128	.263	-.687
100	5303	-.154	.119	.224	-.631
100	5304	-.176	.119	.217	-.569
100	5305	-.147	.115	.229	-.572
100	5901	.022	.198	.762	-.917
100	5902	-.208	.144	.282	-.914
100	6101	-.439	.144	.026	-1.108
100	6102	-.438	.142	.003	-1.097
100	6103	-.285	.139	.194	-.832
100	6104	-.383	.140	.042	-.913
100	6105	-.211	.125	.228	-.789
100	6106	-.021	.125	.411	-.587
100	6201	-.069	.140	.534	-.534
100	6301	-.393	.124	.041	-.796
100	6302	-.315	.125	.044	-.819
100	6901	-.357	.160	.087	-1.191
100	7101	-.296	.142	.117	-.957
100	7102	-.320	.144	.415	-.857
100	7103	-.176	.124	.297	-.607
100	7104	.013	.150	.595	-.629
100	7105	-.135	.130	.337	-.657
100	7106	-.089	.125	.381	-.511
100	7201	-.276	.124	.229	-.713
100	7301	-.298	.134	.191	-.987
100	9101	-.398	.147	.058	-.924
100	9102	-.031	.163	.510	-.759
100	9103	-.217	.239	.765	-.884
100	9104	-.397	.160	.135	-1.145
100	9105	-.310	.147	.239	-.789
100	9106	-.300	.173	.340	-.874
100	9107	-.343	.136	.082	-.821
100	9108	-.362	.136	.087	-.763
100	9109	-.386	.138	.000	-.882
100	9110	-.351	.130	.113	-.823
100	9111	-.372	.135	.054	-.892
100	9112	-.356	.133	.073	-.879
100	9113	-.373	.136	.034	-.850
100	9114	-.403	.142	.002	-.906
100	9115	-.429	.149	.045	-.967
100	9116	-.379	.137	.072	-.857
100	9117	-.443	.156	.055	-1.050
100	9118	-.208	.114	.145	-.576
100	9119	-.299	.122	.070	-.710
100	9120	-.353	.135	.069	-.838
100	9121	-.373	.154	.116	-.849

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
100	9122	-.403	.179	.299	-1.054
100	9123	-.328	.146	.092	-.862
100	9124	-.290	.143	.147	-.854
100	9125	-.257	.133	.157	-.713
100	9126	-.464	.199	.119	-1.179
100	9201	.008	.132	.467	-.447
100	9202	.177	.146	.745	-.305
100	9203	.184	.153	.827	-.288
100	9204	.029	.159	.607	-.477
100	9205	-.079	.143	.424	-.517
100	9206	.009	.140	.440	-.443
100	9207	.577	.185	1.313	.011
100	9208	.407	.189	1.021	-.298
100	9209	.195	.175	.850	-.378
100	9210	-.009	.136	.488	-.486
100	9211	-.115	.137	.304	-.510
100	9212	.337	.158	.912	-.199
100	9213	-.024	.152	.472	-.604
100	9214	.033	.160	.551	-.592
100	9215	-.025	.150	.458	-.483
100	9216	-.042	.144	.447	-.516
100	9217	-.031	.132	.420	-.448
100	9218	-.001	.131	.425	-.428
100	9219	.388	.154	.906	-.127
100	9220	.195	.144	.777	-.320
100	9221	-.011	.148	.531	-.583
100	9222	-.026	.131	.416	-.426
100	9223	-.108	.131	.323	-.542
100	9224	-.080	.124	.327	-.493
100	9225	.260	.172	.941	-.298
100	9226	.059	.151	.595	-.439
100	9227	.064	.120	.531	-.365
100	9228	.017	.116	.401	-.409
100	9229	.306	.166	.855	-.291
100	9230	-.033	.116	.365	-.428
100	9231	-.091	.121	.327	-.527
100	9232	.172	.174	.777	-.469
100	9233	.060	.159	.577	-.566
100	9234	.029	.150	.652	-.620
100	9235	-.050	.127	.363	-.620
100	9236	-.149	.136	.329	-.699
100	9237	-.030	.131	.402	-.591
100	9238	-.042	.131	.371	-.471
110	1101	.124	.237	.766	-.656
110	1102	.140	.183	.694	-.709
110	1103	.035	.134	.469	-.424
110	1104	-.023	.130	.400	-.506
110	1105	-.061	.143	.421	-.662
110	1106	-.147	.137	.307	-.728
110	1107	-.179	.138	.289	-.765

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
110	1108	.298	.276	1.190	-.553
110	1109	.299	.258	1.058	-.800
110	1110	.246	.166	.871	-.344
110	1111	.154	.156	.734	-.394
110	1112	.058	.150	.616	-.490
110	1113	-.076	.137	.443	-.502
110	1114	-.197	.134	.320	-.628
110	1115	.257	.282	1.003	-.625
110	1116	.283	.273	.947	-.722
110	1117	.269	.161	.763	-.269
110	1118	.155	.152	.658	-.310
110	1119	.044	.141	.549	-.388
110	1120	-.125	.132	.368	-.523
110	1121	-.193	.119	.240	-.583
110	1122	.068	.267	.980	-1.004
110	1123	.105	.286	.863	-1.078
110	1124	.204	.142	.694	-.278
110	1125	.101	.139	.598	-.361
110	1126	-.011	.137	.441	-.502
110	1127	-.163	.130	.213	-.625
110	1128	-.252	.131	.159	-.714
110	1129	-.169	.290	.930	-1.083
110	1130	-.131	.345	.875	-1.384
110	1131	.112	.168	.682	-.791
110	1132	.015	.145	.533	-.477
110	1133	-.096	.126	.305	-.464
110	1134	-.238	.124	.162	-.611
110	1135	-.303	.124	.100	-.686
110	1136	-.316	.160	.367	-1.077
110	1137	-.334	.168	.414	-1.011
110	1138	-.092	.178	.595	-.746
110	1139	-.085	.132	.379	-.612
110	1140	-.140	.121	.250	-.595
110	1141	-.263	.119	.125	-.723
110	1142	-.304	.118	.096	-.753
110	1143	-.152	.149	.394	-.737
110	1144	-.013	.150	.593	-.541
110	1145	-.030	.143	.532	-.484
110	1146	-.031	.136	.488	-.460
110	1147	-.078	.148	.475	-.574
110	1148	-.265	.146	.274	-.788
110	1149	-.330	.135	.218	-.795
110	1150	-.008	.147	.546	-.497
110	1151	-.012	.145	.509	-.543
110	1152	-.081	.129	.327	-.532
110	1201	.418	.177	1.092	-.154
110	1202	-.227	.127	.175	-.646
110	1203	-.399	.138	.027	-.862
110	1204	-.073	.139	.374	-.568
110	1205	-.018	.142	.443	-.495

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
110	1206	.084	.144	.577	-.369
110	1207	.151	.152	.724	-.382
110	1208	.374	.162	.880	-.143
110	1209	.451	.175	1.035	-.097
110	1210	.523	.211	1.263	-.126
110	1211	.148	.120	.727	-.259
110	1212	.070	.127	.476	-.395
110	1213	.141	.131	.524	-.329
110	1214	.198	.146	.685	-.286
110	1215	.335	.160	.869	-.175
110	1216	.463	.170	1.017	-.048
110	1217	.603	.186	1.238	.032
110	1218	.639	.177	1.192	.098
110	1219	.215	.143	.742	-.283
110	1220	.185	.128	.693	-.277
110	1221	.159	.129	.594	-.278
110	1222	.166	.146	.627	-.307
110	1223	.308	.123	.750	-.104
110	1224	.390	.160	.878	-.106
110	1225	.518	.174	1.064	-.016
110	1226	.632	.186	1.261	.111
110	1227	.630	.193	1.337	.089
110	1228	.206	.139	.826	-.263
110	1229	.194	.128	.682	-.265
110	1230	.174	.134	.575	-.269
110	1231	.205	.138	.635	-.247
110	1232	.255	.140	.697	-.200
110	1233	.401	.152	.902	-.063
110	1234	.542	.171	1.208	.033
110	1235	.626	.181	1.316	.021
110	1236	.597	.184	1.262	-.054
110	1237	.232	.161	.803	-.350
110	1238	.205	.149	.670	-.303
110	1239	.197	.147	.726	-.308
110	1240	.236	.148	.758	-.310
110	1241	.276	.156	.843	-.277
110	1242	.422	.167	.979	-.130
110	1243	.532	.180	1.065	-.055
110	1244	.574	.195	1.243	-.114
110	1245	.499	.208	1.298	-.211
110	1246	.584	.212	1.444	-.203
110	1247	.300	.156	.880	-.222
110	1248	.207	.144	.679	-.263
110	1249	.294	.149	.867	-.205
110	1250	.318	.156	.764	-.195
110	1251	.401	.169	.905	-.189
110	1252	.508	.183	1.067	-.141
110	1253	.470	.196	1.055	-.175
110	1254	.291	.178	.978	-.228
110	1301	-.352	.149	.213	-.915
110	1302	-.346	.146	.202	-.948
110	1303	-.311	.131	.165	-.725
110	1304	-.326	.131	.173	-.735
110	1305	-.317	.126	.111	-.730
110	1306	-.304	.123	.103	-.700
110	1307	-.268	.122	.142	-.663
110	1308	-.331	.128	.071	-.757
110	1309	-.342	.141	.114	-.826
110	1310	-.326	.136	.123	-.802
110	1311	-.286	.131	.159	-.735
110	1312	-.300	.134	.158	-.729
110	1313	-.311	.128	.205	-.822
110	1314	-.309	.129	.209	-.804
110	1315	-.315	.128	.176	-.881
110	1316	-.331	.128	.137	-.829
110	1317	-.321	.121	.189	-.703
110	1318	-.316	.122	.222	-.723
110	1319	-.276	.118	.231	-.654
110	1320	-.294	.121	.219	-.686
110	1321	-.302	.132	.135	-.766
110	1322	-.340	.136	.090	-.747
110	1323	-.299	.128	.109	-.694
110	1324	-.320	.127	.105	-.749
110	1325	-.329	.123	.108	-.749
110	1326	-.332	.127	.126	-.791
110	1327	-.297	.122	.147	-.724
110	1328	-.318	.125	.130	-.752
110	1329	-.349	.129	.227	-.778
110	1330	-.346	.130	.223	-.757
110	1331	-.329	.125	.182	-.700
110	1332	-.374	.129	.140	-.777
110	1333	-.388	.126	.079	-.834
110	1334	-.385	.128	.065	-.813
110	1335	-.345	.124	.081	-.772
110	1336	-.392	.124	-.003	-.828
110	1337	-.399	.125	-.012	-.812
110	1338	-.407	.124	-.055	-.877
110	1339	-.426	.126	-.028	-.879
110	1340	-.345	.122	.023	-.722
110	1401	-.293	.135	.132	-.784
110	1402	-.262	.132	.138	-.726
110	1403	-.309	.128	.137	-.742
110	1404	-.306	.130	.125	-.808
110	1405	-.307	.131	.131	-.817
110	1406	-.270	.128	.134	-.783
110	1407	-.286	.135	.153	-.754
110	1408	-.309	.138	.138	-.872
110	1409	-.321	.144	.150	-1.199
110	1410	-.257	.131	.137	-.753
110	1411	-.262	.119	.170	-.629
110	1412	-.252	.123	.129	-.674
110	1413	-.277	.125	.119	-.701
110	1414	-.292	.123	.125	-.771
110	1415	-.298	.125	.147	-.774
110	1416	-.266	.122	.175	-.700
110	1417	-.294	.126	.133	-.717
110	1418	-.305	.125	.108	-.768
110	1419	-.269	.121	.220	-.653
110	1420	-.210	.115	.220	-.574
110	1421	-.283	.123	.089	-.723
110	1423	-.271	.122	.140	-.687
110	1424	-.301	.125	.133	-.727
110	1425	-.304	.127	.131	-.745
110	1426	-.265	.124	.142	-.677
110	1427	-.294	.126	.148	-.711
110	1428	-.293	.121	.119	-.673
110	1429	-.296	.114	.113	-.666
110	1430	-.303	.123	.163	-.735
110	1431	-.309	.125	.171	-.740
110	1432	-.276	.121	.195	-.694
110	1433	-.310	.124	.168	-.735
110	1434	-.332	.124	.096	-.754
110	1435	-.331	.126	.095	-.776
110	1436	-.297	.122	.111	-.741
110	1437	-.343	.118	.065	-.732
110	1438	-.271	.112	.118	-.635
110	1439	-.333	.120	.130	-.763
110	1440	-.326	.117	.034	-.759
110	1441	-.330	.121	.044	-.776
110	1442	-.311	.117	.055	-.746
110	1443	-.342	.120	.029	-.797
110	1444	-.366	.125	.082	-.810
110	1445	-.372	.128	.074	-.813
110	1446	-.333	.117	.076	-.715
110	1447	-.328	.122	.112	-.707
110	1448	-.298	.120	.139	-.746
110	1449	-.342	.122	.115	-.795
110	1450	-.367	.129	.036	-.811
110	1451	-.402	.138	-.010	-.839
110	1452	-.379	.134	.047	-.810
110	1453	-.392	.134	-.007	-.907
110	1454	-.384	.119	.014	-.806
110	1455	-.335	.122	.044	-.801
110	1456	-.347	.123	.036	-.822
110	1457	-.341	.122	.043	-.787
110	1458	-.376	.128	.029	-.846
110	1459	-.373	.128	.039	-.834
110	1460	-.389	.134	.076	-.869
110	1461	-.393	.127	.030	-.882
110	1462	-.362	.122	.041	-.797

APPENDIX A -- PRESSURE DATA: CONFIGURATION A: HARRAH'S HOLIDAY INN, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
110	1463	-.375	.124	.027	-.832
110	1464	-.142	.249	.856	-.765
110	1465	-.279	.121	.105	-.699
110	1466	-.238	.130	.268	-.723
110	1467	-.266	.127	.235	-.732
110	1801	-.159	.121	.329	-.581
110	1802	-.213	.116	.158	-.618
110	1803	-.137	.137	.329	-.604
110	1804	-.104	.141	.359	-.579
110	1805	-.289	.136	.149	-.753
110	1806	-.274	.131	.188	-.721
110	1807	-.271	.122	.186	-.678
110	2101	.536	.171	1.104	-.058
110	2102	-.212	.189	.396	-.989
110	2103	-.028	.164	.605	-.643
110	2104	-.164	.131	.296	-.672
110	2105	.407	.165	1.041	-.146
110	2106	.324	.158	.875	-.186
110	2107	-.020	.161	.523	-.609
110	2108	.020	.147	.513	-.567
110	2109	.167	.153	.624	-.395
110	2110	.133	.154	.607	-.426
110	2111	.062	.170	.647	-.593
110	2112	.080	.139	.568	-.358
110	2113	-.351	.123	.080	-.789
110	2114	-.267	.153	.273	-.761
110	2115	-.160	.161	.382	-.785
110	2116	.107	.148	.589	-.509
110	2117	-.255	.145	.227	-.723
110	2118	-.225	.149	.228	-.797
110	2119	-.213	.142	.182	-1.033
110	2120	-.215	.126	.145	-.830
110	2121	-.241	.127	.171	-.724
110	2122	.007	.132	.428	-.431
110	2123	-.249	.155	.359	-.897
110	2124	-.233	.147	.331	-.793
110	2125	-.210	.131	.230	-.704
110	2126	.011	.133	.522	-.497
110	2127	.100	.134	.569	-.330
110	2128	.004	.145	.537	-.443
110	2129	-.298	.124	.191	-.687
110	2130	-.298	.131	.125	-.734
110	2131	-.162	.129	.249	-.607
110	2132	-.168	.129	.250	-.587
110	2133	-.151	.129	.261	-.579
110	2134	-.176	.131	.234	-.578
110	2135	-.229	.133	.228	-.707
110	2136	-.265	.126	.185	-.743
110	2137	.126	.130	.526	-.268
110	2138	-.197	.124	.274	-.619

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
110	2139	-.312	.120	.057	-.736
110	2140	-.311	.125	.068	-.747
110	2141	-.324	.121	.085	-.866
110	2142	-.260	.133	.225	-.739
110	2143	-.142	.129	.338	-.715
110	2144	-.147	.130	.318	-.739
110	2145	-.134	.127	.309	-.625
110	2146	-.114	.129	.391	-.562
110	2147	-.193	.129	.318	-.647
110	2148	-.145	.121	.260	-.525
110	2149	-.134	.126	.352	-.527
110	2150	.199	.146	.767	-.305
110	2151	.069	.131	.462	-.467
110	2152	-.023	.148	.622	-.545
110	2153	-.184	.131	.239	-.717
110	2154	-.251	.133	.302	-.843
110	2201	.402	.159	.949	-.140
110	2202	.464	.172	1.060	-.071
110	2203	.357	.162	.881	-.168
110	2204	.335	.153	.897	-.204
110	2205	.496	.179	1.104	.008
110	2206	.131	.186	.739	-.473
110	2207	.254	.161	.898	-.311
110	2208	.281	.148	.756	-.226
110	2209	.326	.151	.869	-.230
110	2210	.364	.174	.997	-.332
110	2211	.185	.148	.794	-.387
110	2212	.123	.145	.800	-.396
110	2213	-.076	.148	.527	-.649
110	2214	.064	.140	.598	-.474
110	2215	.015	.138	.554	-.545
110	2216	.044	.140	.623	-.554
110	2217	.160	.147	.727	-.331
110	2218	.124	.185	1.104	-.532
110	2219	.040	.164	.706	-.548
110	2220	-.035	.133	.425	-.490
110	2221	.025	.107	.380	-.308
110	2222	.002	.130	.627	-.421
110	2224	.152	.160	.704	-.540
110	2225	.109	.167	.694	-.474
110	2226	-.015	.146	.543	-.695
110	2227	.019	.146	.526	-.643
110	2228	.058	.130	.534	-.369
110	2229	.042	.123	.483	-.351
110	2230	-.956	.145	-.560	-1.201
110	2231	.122	.133	.615	-.337
110	2232	.135	.140	.609	-.375
110	2233	.162	.157	.701	-.536
110	2234	.033	.132	.441	-.443
110	2235	.099	.135	.515	-.378

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
110	2236	.096	.129	.566	-.358
110	2237	.145	.127	.571	-.247
110	2238	-.028	.131	.441	-.440
110	2239	.145	.127	.569	-.256
110	2240	.159	.138	.671	-.427
110	2301	-.459	.135	.040	-.899
110	2302	-.456	.137	-.004	-.895
110	2303	-.273	.138	.249	-.798
110	2304	-.243	.119	.115	-.630
110	2305	-.331	.121	.039	-.753
110	2306	-.372	.129	.039	-.848
110	2307	-.366	.133	.056	-.892
110	2308	.007	.159	.577	-.604
110	2309	-.447	.139	-.018	-.921
110	2310	-.237	.141	.389	-.852
110	2311	-.222	.145	.333	-.704
110	2312	-.214	.134	.214	-.749
110	2313	-.137	.125	.281	-.628
110	2314	-.170	.134	.277	-.696
110	2315	-.131	.123	.307	-.527
110	2401	-.400	.120	.036	-.842
110	2402	-.422	.123	.039	-.851
110	2403	-.438	.126	.021	-.890
110	2404	.331	.142	.777	-.151
110	2405	-.279	.142	.357	-.762
110	2406	-.346	.150	.164	-.953
110	2407	-.388	.130	.101	-.818
110	2408	-.447	.135	.091	-.890
110	2409	.221	.139	.671	-.266
110	2411	-.395	.123	.084	-.787
110	2412	-.426	.138	.042	-.895
110	2413	-.498	.146	-.045	-1.082
110	2414	.121	.138	.625	-.424
110	2415	-.245	.138	.221	-.735
110	2416	-.248	.121	.189	-.654
110	2417	-.291	.120	.191	-.694
110	2418	-.346	.142	.084	-.913
110	2419	-.413	.157	.051	-1.163
110	2420	-.426	.162	.241	-1.066
110	2421	-.195	.117	.416	-.567
110	2422	-.249	.126	.191	-.845
110	2423	-.275	.146	.262	-.719
110	2424	-.257	.149	.312	-.768
110	2425	-.228	.147	.303	-.758
110	2426	-.363	.142	.075	-.796
110	2427	-.256	.126	.170	-.707
110	2428	-.252	.125	.143	-.679
110	2429	-.212	.122	.185	-.602
110	2430	-.268	.126	.186	-.693
110	2431	-.216	.138	.230	-.654