

EVALUATION OF THE PERFORMANCE
CHARACTERISTICS OF TURBINE-TYPE
FLOWMETERS

by

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INTRODUCTION

The purpose of this report is to discuss performance characteristics of various sizes of turbine meters manufactured by three flowmeter companies, Potter Aeronautical, Fischer and Porter, and Waugh. The specific performance characteristics discussed are linearity, range, accuracy and repeatability. Sizes of meters tested ranged from 3/16 to 6 1/2-in. Potter meters, 1/2, 3/4 and 2-in. Fischer and Porter meters and 3/4 and 2-in. Waugh meters.

Linearity

Linearity of a turbine flowmeter is a term used to describe the relationship between the rotating speed of the turbine (frequency) and discharge. It is dependent upon the geometry of the turbine, bearing resistance to the rotor and properties of the fluid flowing through the meter. A flowmeter that exhibits linearity is simple to use because the slope of the frequency-discharge curve is constant and a single calibration factor, K , can be used to determine the relative discharge for any output frequency of the meter.

Range

Linearity of turbine flowmeters is limited practically because of the limitations of the mechanical components of the meter. Bearing friction and energy losses at low discharges and separation and cavitation at high discharges are the principal limitations. The range of discharges between a minimum and maximum discharge displaying linearity is termed the range of the meter.

Accuracy

Accuracy is used to describe the deviation of indicated discharge from actual discharge.

Repeatability

Repeatability is a characteristic which describes how consistently the frequency-discharge relationships can be repeated.

EXPERIMENTAL DATA AND DISCUSSION OF RESULTS

Data used to evaluate the performance characteristics of various flowmeters were obtained from tests made on flowmeters provided by the Martin Company and tested in the Hydraulics Laboratory of Colorado State University. Flowmeters manufactured by the Potter Aeronautical, Fischer and Porter and Waugh Companies were studied.

Potter Aeronautical Flowmeters

Experimental data for Potter meters were obtained for flowmeters ranging in sizes from 3/16 to 6 1/2 inches in diameter. Various models, and where possible, a number of different meters of the same model were used to describe performance characteristics.

Figure 1 in Appendix A shows a typical calibration curve for a 3/16-in. meter. The curve of frequency as a function of discharge (f-G curve) shows a linear relationship. Because of the scale of the coordinates of the graph, it is not easy to determine the accuracy nor the range of the meter. Therefore, a curve of the calibration factor K, as a function of discharge (K-G curve) is shown above the f-G curve. (The abscissa of this curve could be frequency as well as discharge because of the linearity of the flowmeter. For convenience of this curve, discharge is used as the abscissa.)

The dimensions of K are cycles per gallon (c.p.g.). The value of K is the slope of a line (multiplied by 60) connecting a specific point of the frequency-discharge curve with the origin of coordinates. If the calibration curve included the origin, K of each point could be averaged to determine a single value, \bar{K} , which would be the average calibration factor for the meter.

As shown in Figure 1, the calibration curve passes very nearly through the origin. However, the curve of calibration factors (K -G curve) shows that an average linear line through all the points determined on the calibration curve does not include the origin as a significant point. Considerable deviation in the values of K are observed for the lower discharges.

According to these performance curves, the characteristics of the model 3/16-308 Potter Aeronautical Flowmeter are:

The average calibration factor of the meter is $\bar{K} = 24,000$ c.p.g. The flowmeter is linear in a range of 0.25 to 1.006 g.p.m. (the maximum discharge calibrated) with an accuracy of ± 1.0 per cent. Repeatability is within 0.2 per cent.

As already discussed, by definition \bar{K} assumes the origin as a significant point. As noted in Figure 1 however the origin is not a significant point in the linear relationship (that is, at frequency = 0, discharge = some finite quantity). Hence, the fact that an average calibration factor \bar{K} can be used for a range of discharges is only because of the proximity of the origin to the calibration curve. When values of K are determined for the large discharges, the difference between K and the slope of a linear function which best fits the calibration data, is very small. In order to show the difference, a linear function was calculated from the measured data used to plot Fig. 1. The function was of the form

$$f = MG + F_0$$

where

f = frequency in cycles per second

M = slope of the line

G = discharge in gallons per minute

F_0 = intercept of the function with the curve $G = 0$.

The computed results were:

$$M = 411.45$$

$$F_0 = -2.38 \text{ c.p.s.}$$

or, converting M to cycles per gallon,

$$M' = 24,228 \text{ c.p.g.}$$

In a range of 0.25 to 1.0 g.p.m. the accuracy is ± 1.3 per cent. The data of Nov. 7, 1959, give:

$$M' = 24,240 \text{ c.p.g.}$$

$$F_0 = -2.22 \text{ c.p.s.}$$

Accuracy in this case is also within ± 1.3 per cent in a range of 0.25 to 1.0 g.p.m.

Comparisons of the two methods describing Potter flowmeter performance characteristics show that although there is error in the assumption which enables use of \bar{K} as the calibration factor for the meter, its use enables greater accuracy in determining discharge than does M' within a specified meter range. The lower limit of the meter range is arbitrarily set at the discharge when the accuracy of the meter is exceeded.

The curves of Fig. 1 are only for a model 3/16-308 flowmeter, serial No. GLMD-10. Fig. 2 shows comparative curves of calibration factor K for different meters of the same model. Note that the values of \bar{K} differ for each meter.

Figs. 3 through 15 show performance curves of flow meter models 3/8-405, 1/2-308, 3/4-80, 3/4-308, 1 1/2-354A, 2-353,

3-349, 4-317, 4-353, 4 1/2-317, 5 1/2-317, 6-353, and 6 1/2-317 respectively. Comparative performance of various meters of the same model are shown in Figures 16 to 27. These performance curves show that the frequency-discharge curve of all the meters tested pass very nearly through the origin of coordinates. Because of this significant meter characteristic, it is more advantageous to use the calibration factor \bar{K} and to limit the meter range, than it is to apply a linear function if an accuracy less than ± 1.0 per cent is required. Each flowmeter exhibits different characteristics depending upon both size and model. The smaller sizes are generally more variable between different meters than the larger sizes, but in all cases the variance requires that each flowmeter be calibrated separately. It is to be noted further in Figs. 3 to 15 that the same meter recalibrated after some amount of use, shows differences in the average calibration factor. Therefore, it would appear desirable to recalibrate meters from time to time to establish a new calibration curve so that the required accuracy can be maintained.

Fischer and Porter Flowmeters

Experimental data for Fischer and Porter flowmeters were obtained for meters 1/2, 3/4, and 2-inches in size. Performance curves for these meters are shown in Figs. 28 to 31 of Appendix B. There is considerable variation in the value of K for each point calibrated for the 1/2-inch meter of Fig. 28. Because of the constant change in the values of K with discharge, there is no average value of \bar{K} applicable to any range of discharge. Using the concept of calibration factor K , it would be necessary to use a specific K for each frequency output. Note also the difference in meter performance at a different fluid temperature. The values of M' and F_0 are also shown on the Figure. Using these values and the calibration of December 26, 1957, the variations between the measured values and the linear function are ± 3.0 per cent in a range of 1 to 10 g.p.m.

The performance curves for the flowmeter model 10C1505, size 3/4-23 are shown in Fig. 29. Using calibration factor K , linear operation exists in a flow range from 4.5 to 20 g.p.m. with an accuracy of ± 1.0 per cent. The average calibration factor \bar{K} is 1505 c.p.g. For the same calibration data $M' = 1507.9$ c.p.g. and $F_0 = .27$ c.p.s. With an accuracy of ± 0.9 per cent in a flow range of 2.4 to 23 g.p.m. The performance characteristics shown in Fig. 29 are with water as the metered fluid. The performance characteristics of the same meter using hydraulic oil of larger kinematic viscosity than water, are shown in Fig. 30. Comparison of meter performance with water and oil shows that the viscosity of the metered fluid has considerable effect. (The effect of viscosity are discussed in a separate report). For this meter, an increase in the viscosity decreased the range and decreased frequency output. For the hydraulic oil

$$\begin{aligned}\bar{K} &= 1505 \text{ c.p.g. in a range from 10 to 22 g.p.m.,} \\ M' &= 1536.34 \text{ c.p.g. and } F_0 = -12.42 \text{ c.p.s. in a range} \\ &\text{from 4 to 24 g.p.m.}\end{aligned}$$

The accuracy of the meter using the linear function for measuring hydraulic oil is ± 2.0 per cent.

The performance curves of a model 10C1505 2-inch Fischer and Porter meter are shown in Fig. 31. The general characteristics discussed for the 1/2 and 3/4-inch meter pertains also to the 2-inch flowmeter.

Waugh Meters

Performance characteristics of Waugh meters were determined for the 3/4 and 2-inch meters. Fig. 32 of Appendix C shows frequency-discharge and K -discharge curves for a 3/4 inch meter model MT110-2511. The calibrating fluid was hydraulic oil at 100°F. Note that because the f - G curve is displaced from the origin of coordinates, the values of K change significantly and constantly with

discharge. The value of M and F_0 are 1753.4 c.p.g. and -8.08 c.f.s. respectively. Accuracy of the meter is within ± 0.5 per cent using the linear relationship in a flow range of 3.8 to 26 g.p.m. A single factor \bar{K} cannot be applied to the meter; either specific values of K for different discharges, or values of M' and F_0 could be used for calculation of discharge. Fig. 33 shows similar characteristics for a 2-inch flowmeter.

SUMMARY AND CONCLUSIONS

Turbine-type flowmeters were tested for performance characteristics. In a specific flow range and within a specified accuracy, all the flowmeters show linearity between frequency output and discharge. Either of two methods may be used to determine a single calibration factor for a turbine meter. One method is to use an average value \bar{K} which may be determined from a curve of K as a function of either discharge or frequency output. The value of K is the slope of an imaginary line from the origin of coordinates to the points on the f - G curve. The second method is to determine by linear regression, a line to fit the set of measured data. Constants M' and F_0 of the linear relationship could then be used to calculate the discharge from measured frequency.

The results of the study shows that for Potter Aeronautical flowmeters of the sizes tested, the first method is perhaps superior if an accuracy of ± 1.0 per cent is required. This applies particularly to the small meters. For the larger meters, either method will give satisfactory results.

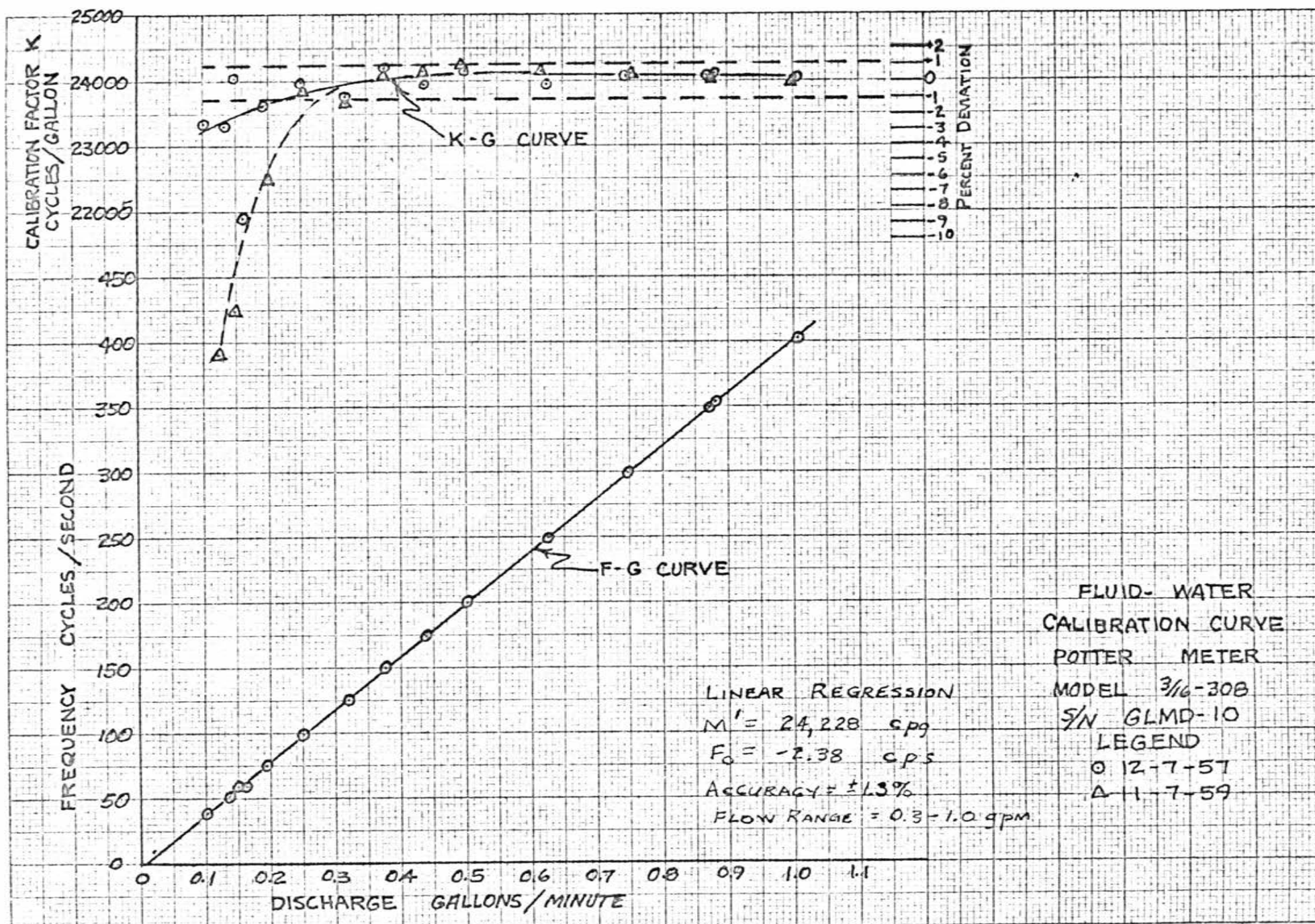
Use of an average calibration factor \bar{K} limits the range for sizes 1/2 and 3/4-inch Fischer and Porter flowmeters. The linear expression for the calibration curve will extend the range of the meter, but with sacrifice of accuracy. In this case, the only recourse is to use different values of K for each meter frequency

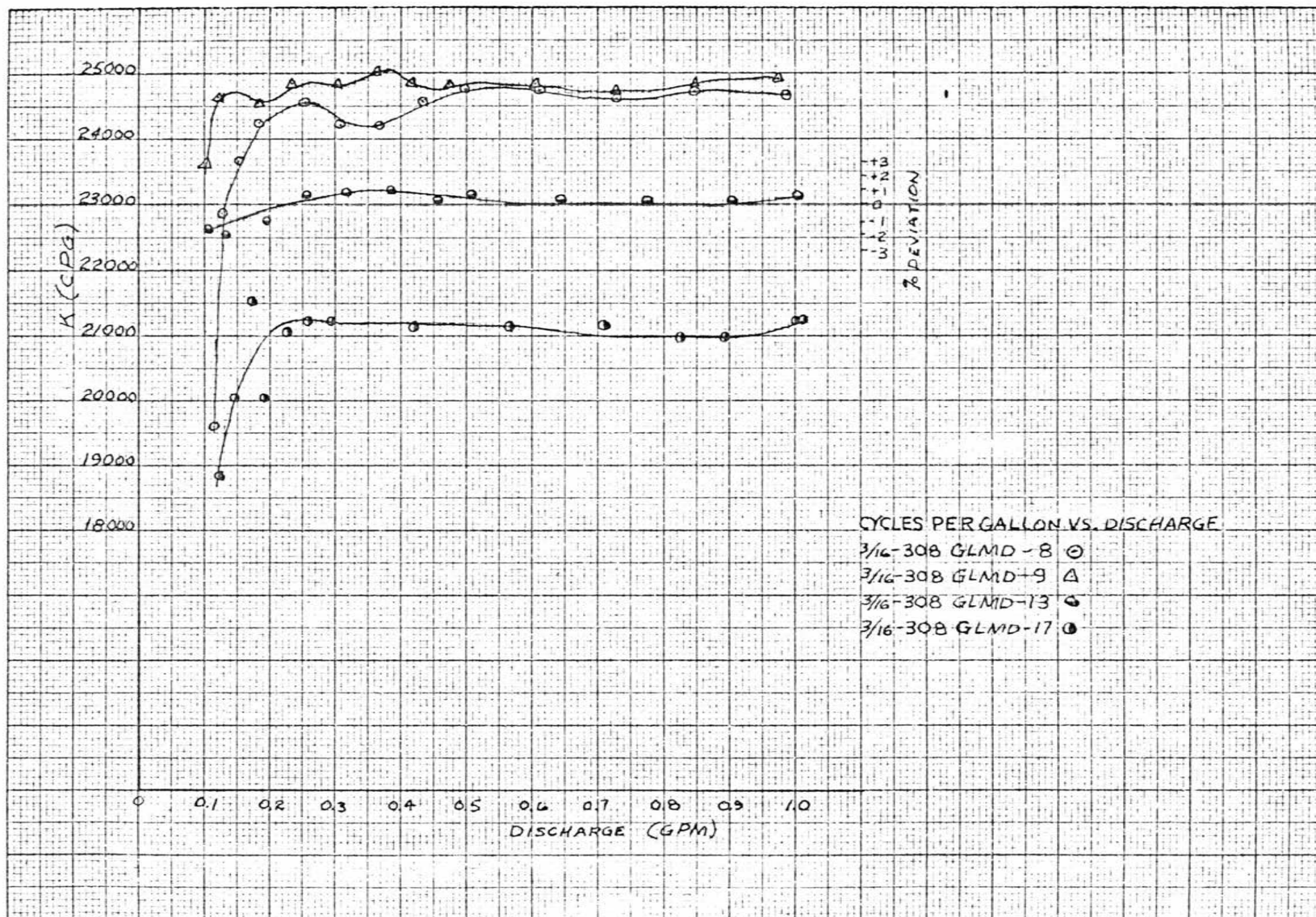
to determine the discharge. Either \bar{K} or the linear expression may be used for the 2-inch Fischer and Porter meter.

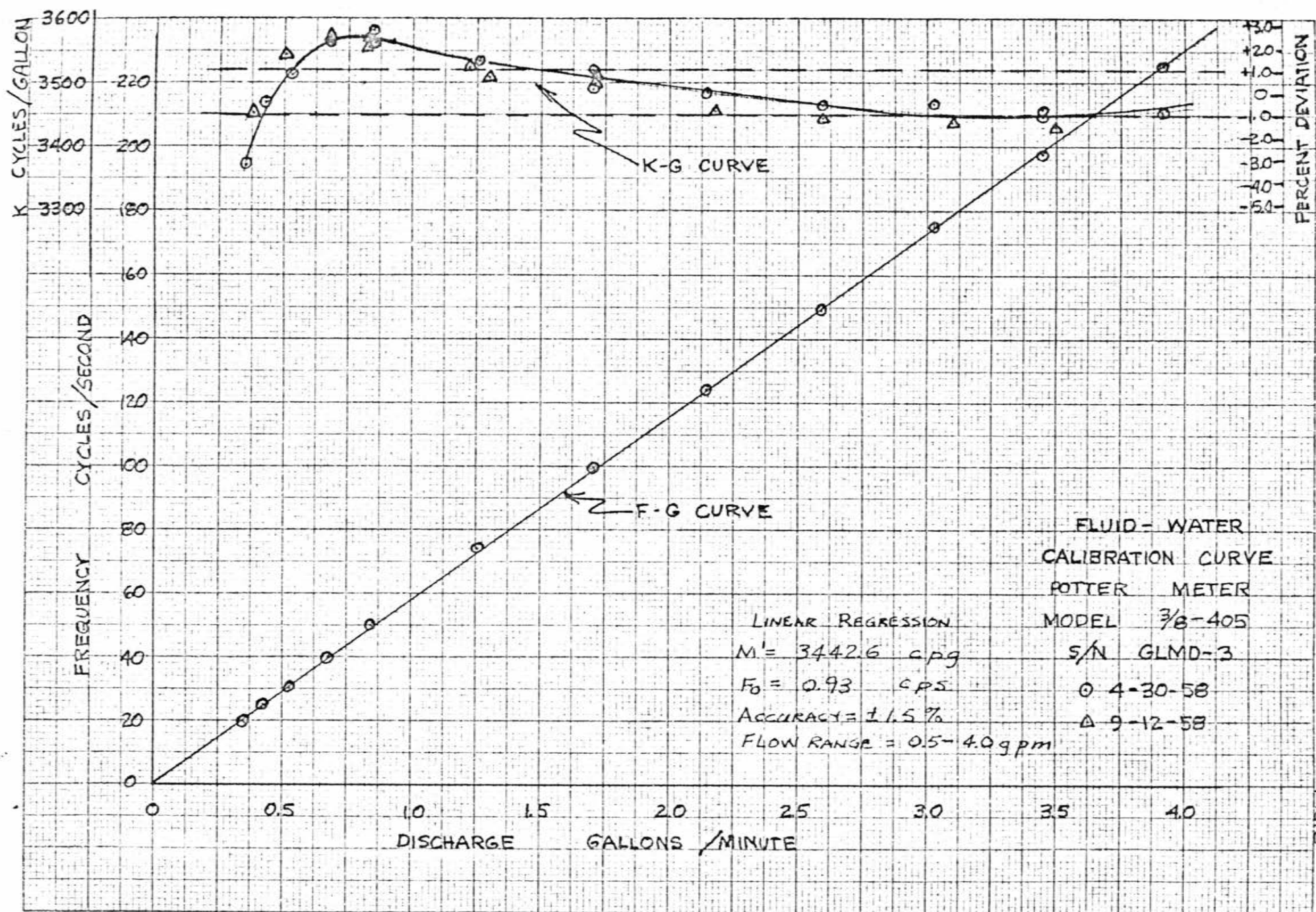
The Waugh flowmeters of 3/4 and 2-inch sizes tested show linear characteristics. The linear function results in a wider range for the 3/4-inch meter than use of \bar{K} . Either method will give discharge measurements within ± 1 per cent for the 2-inch meter.

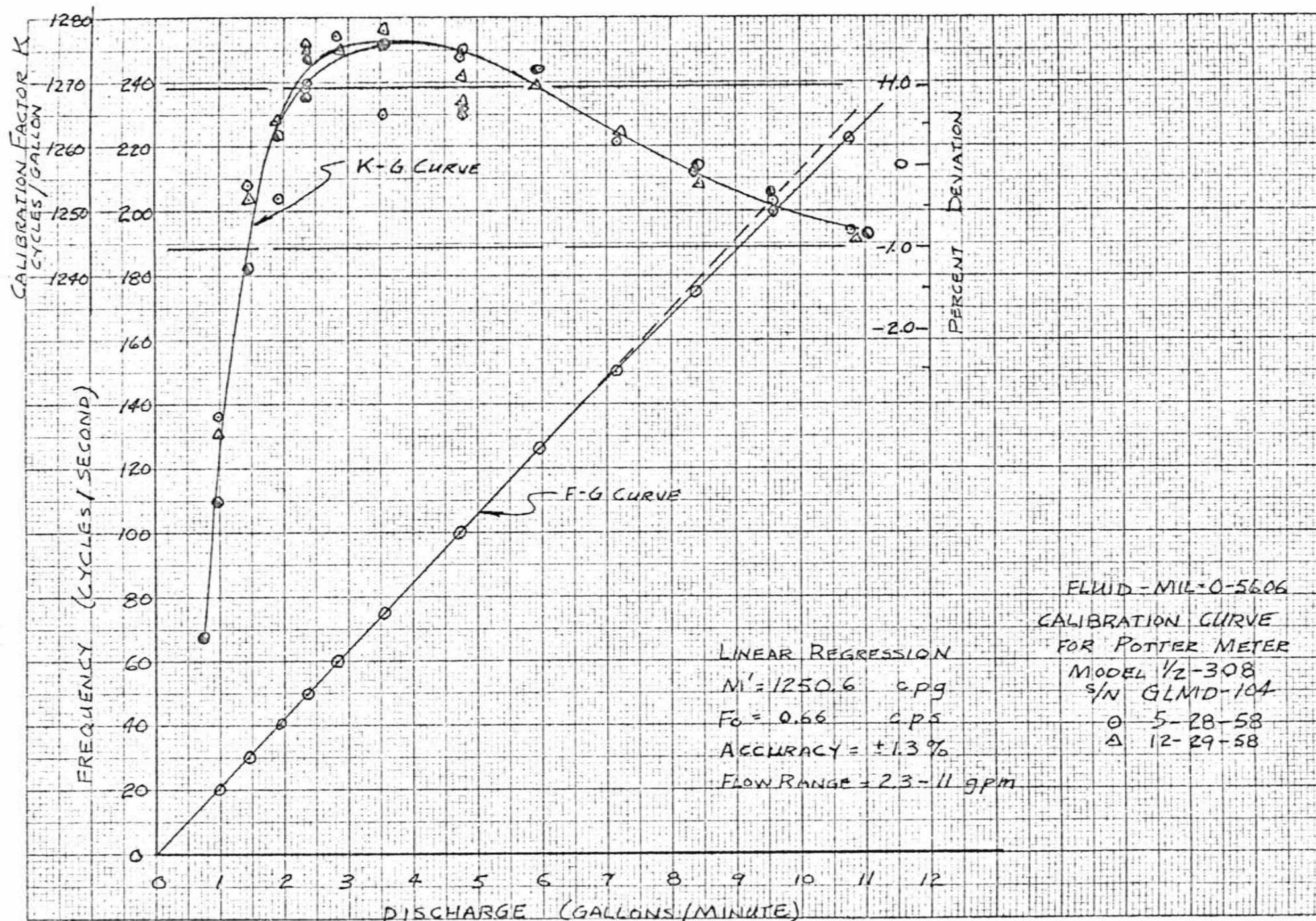
APPENDIX A

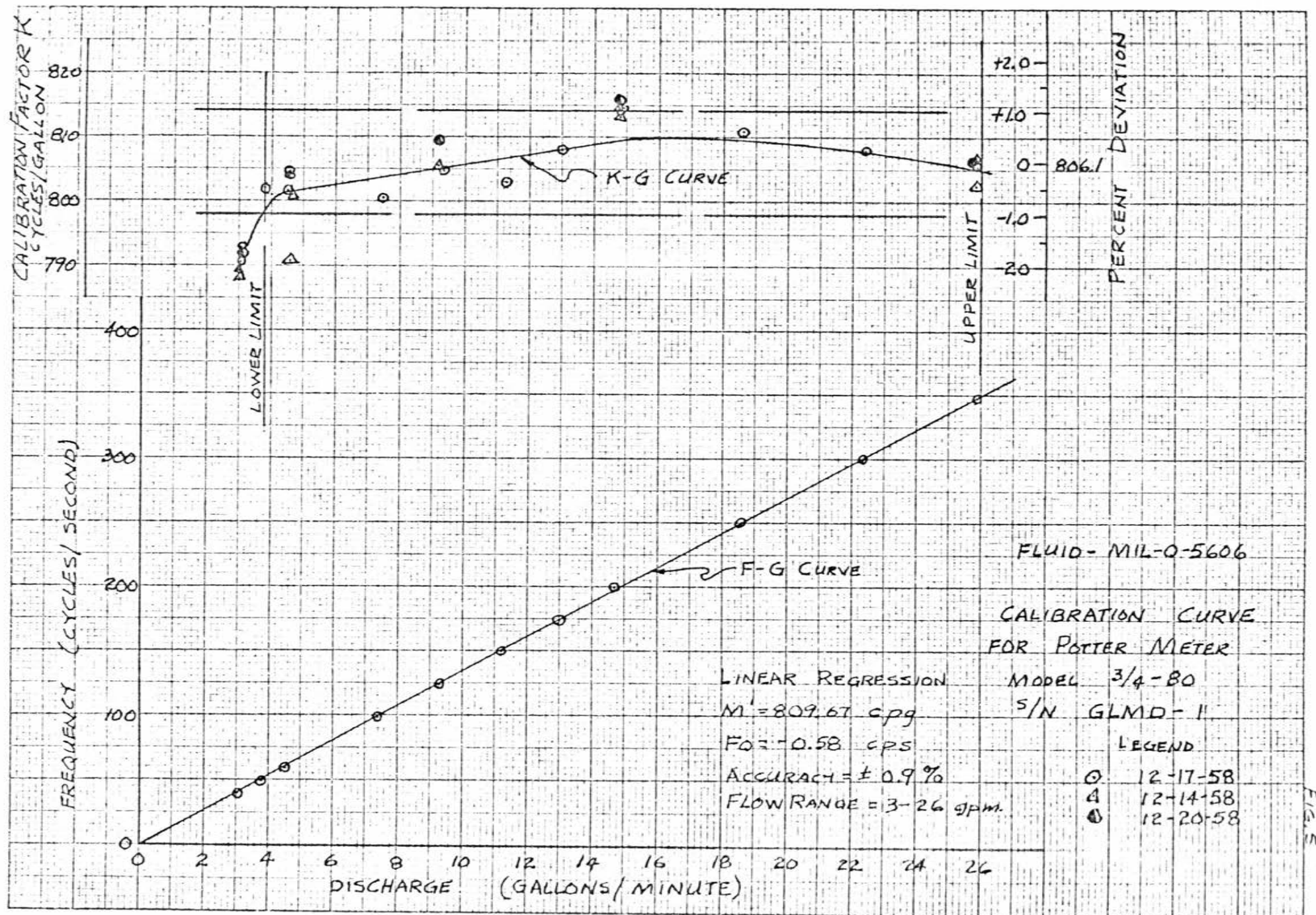
POTTER AERONAUTICAL FLOWMETERS

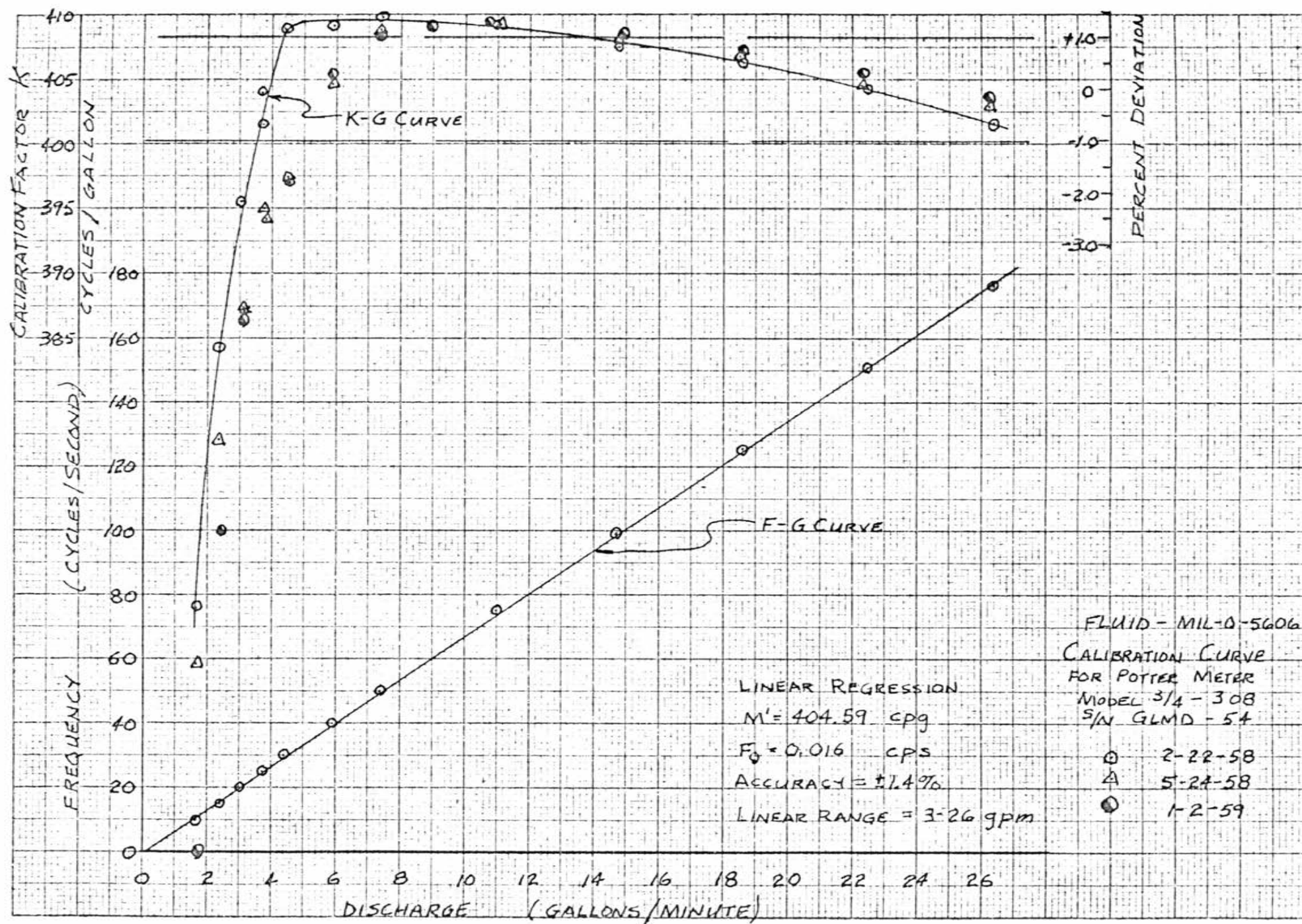


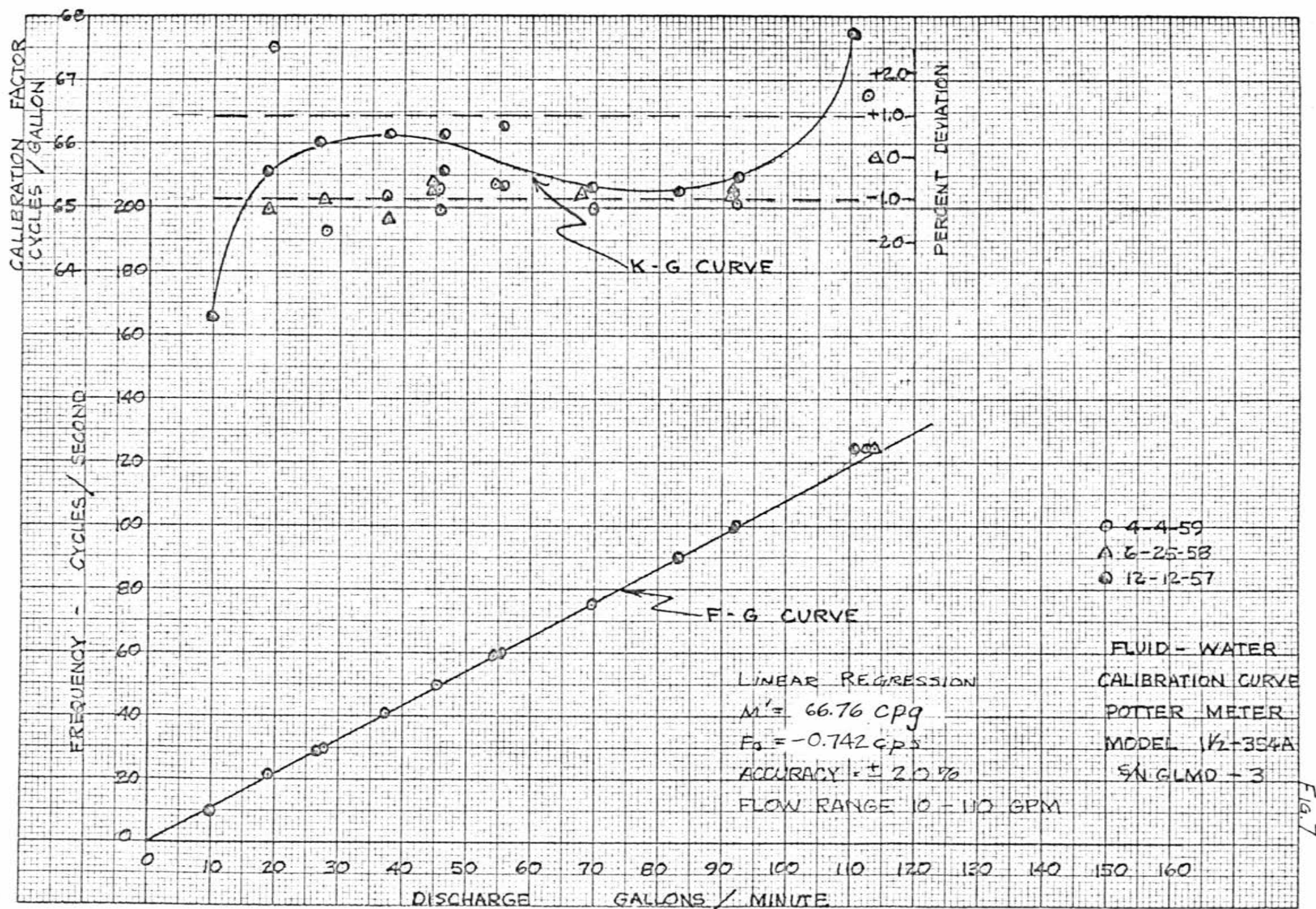


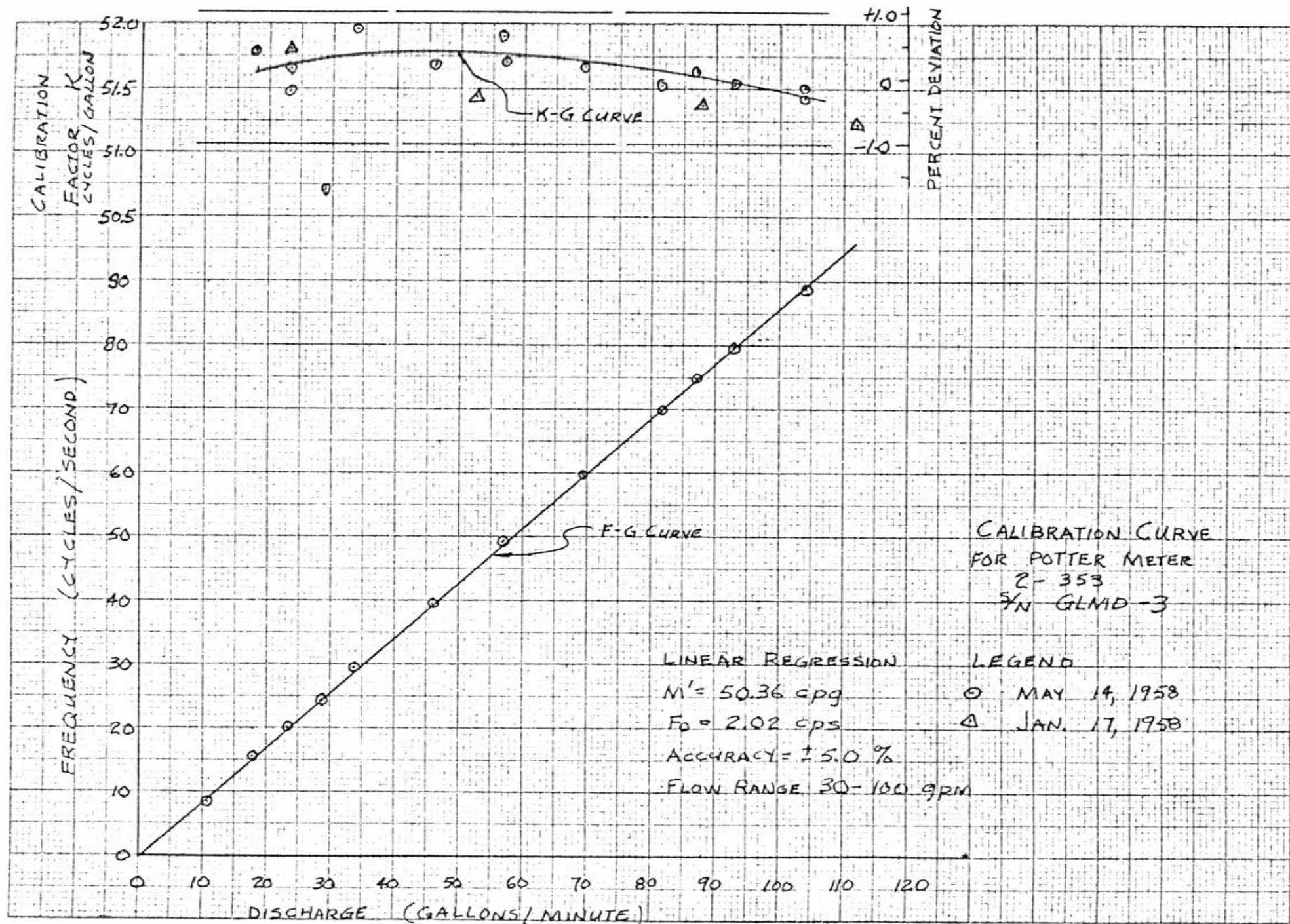


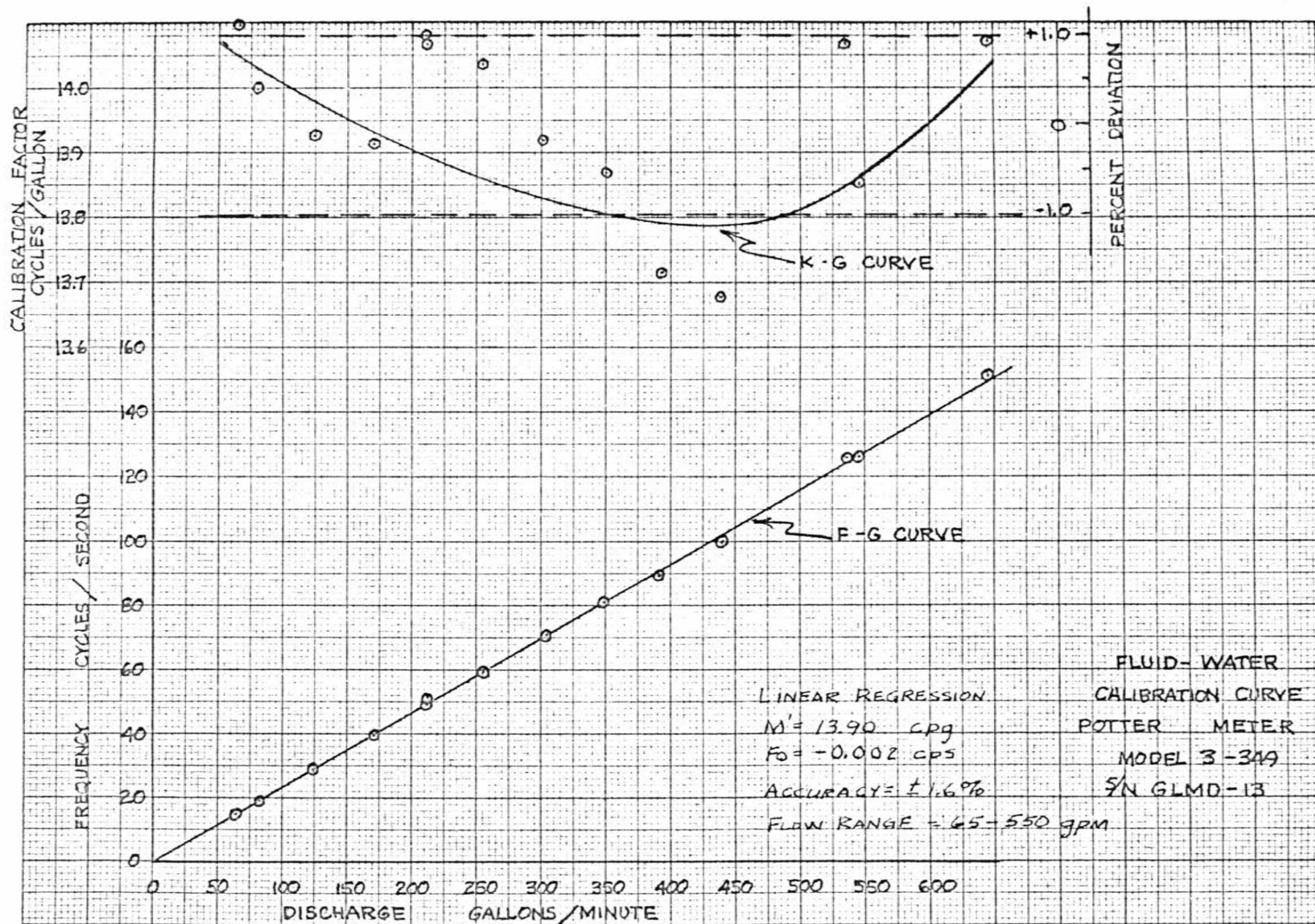


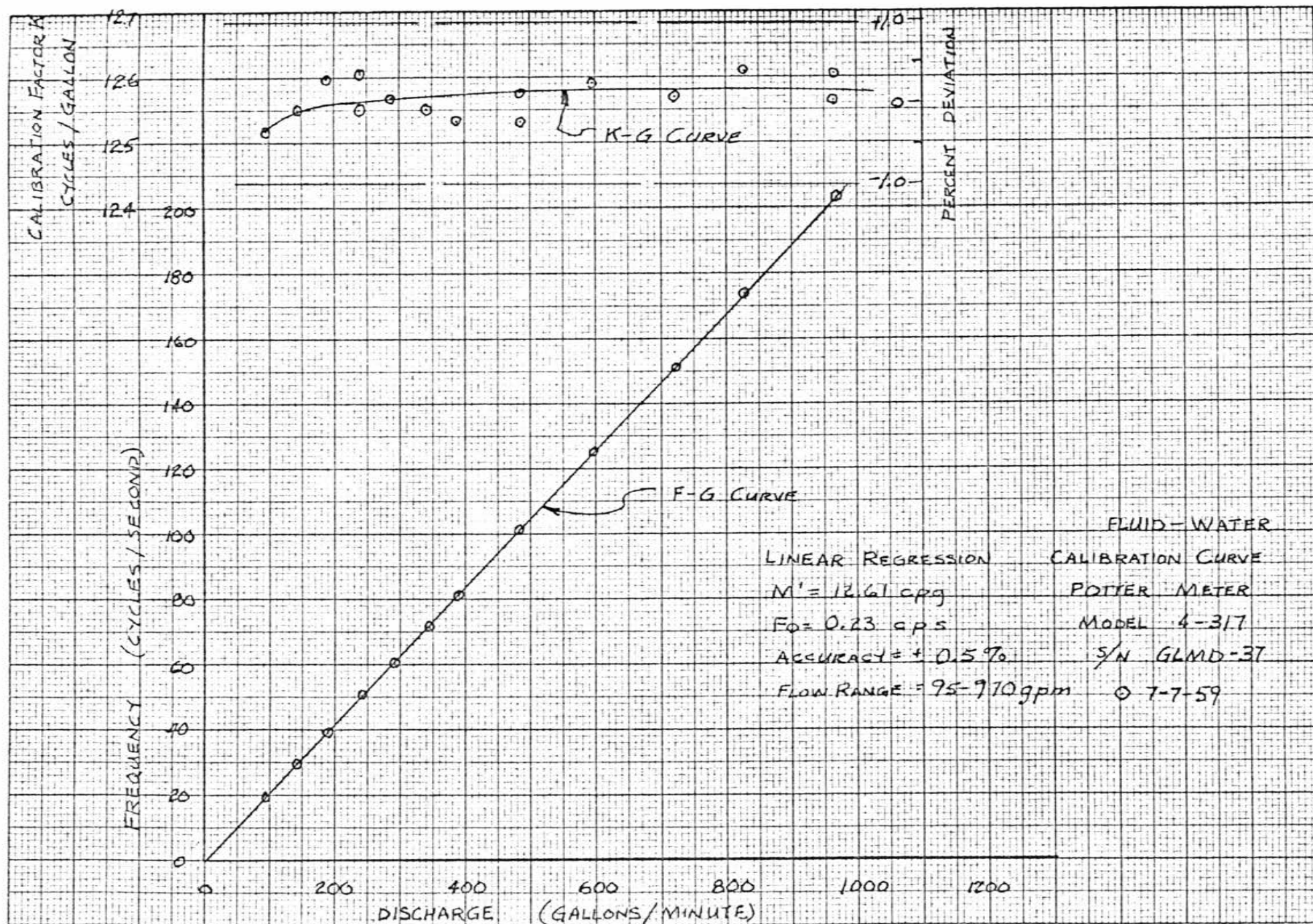


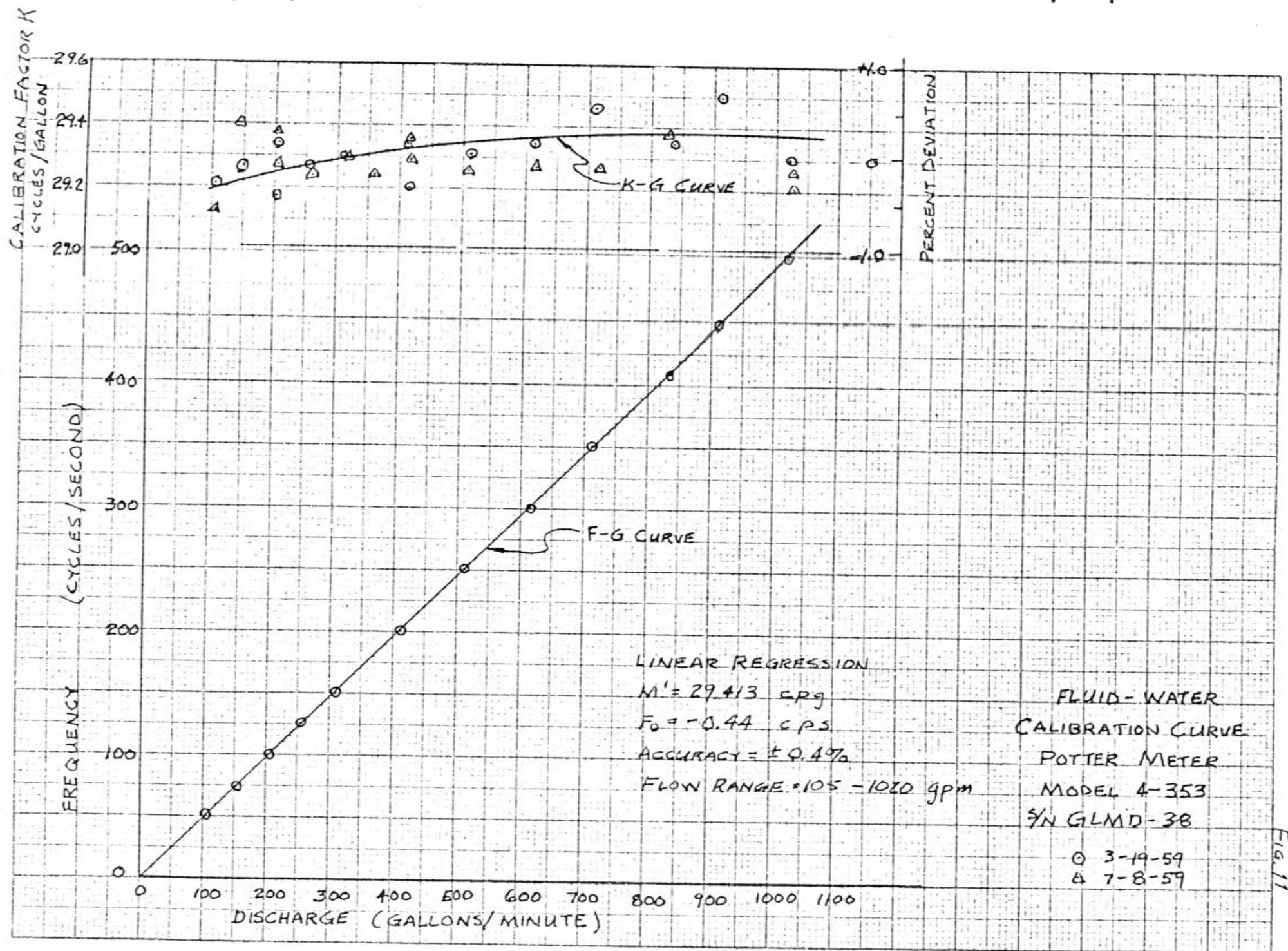


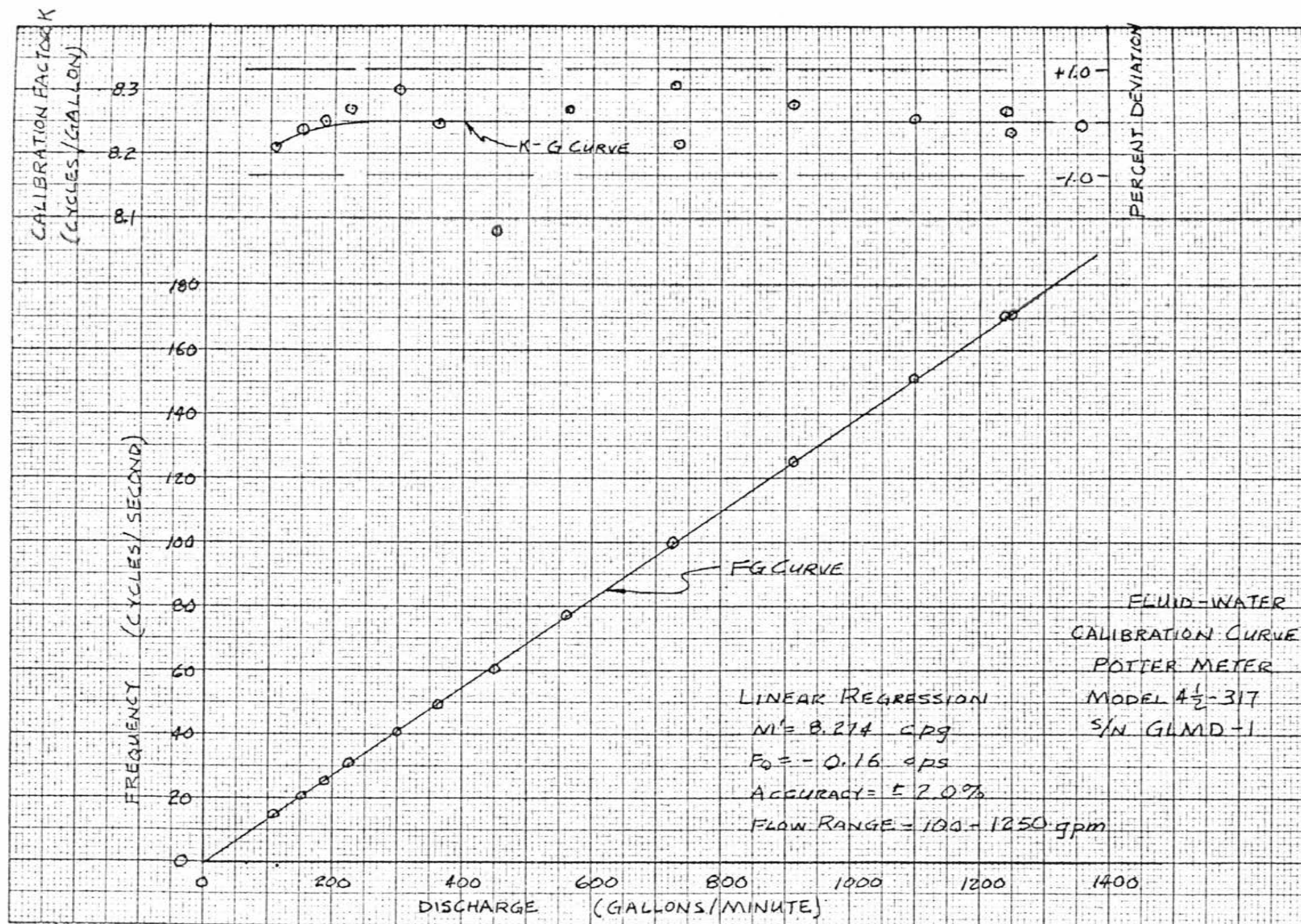


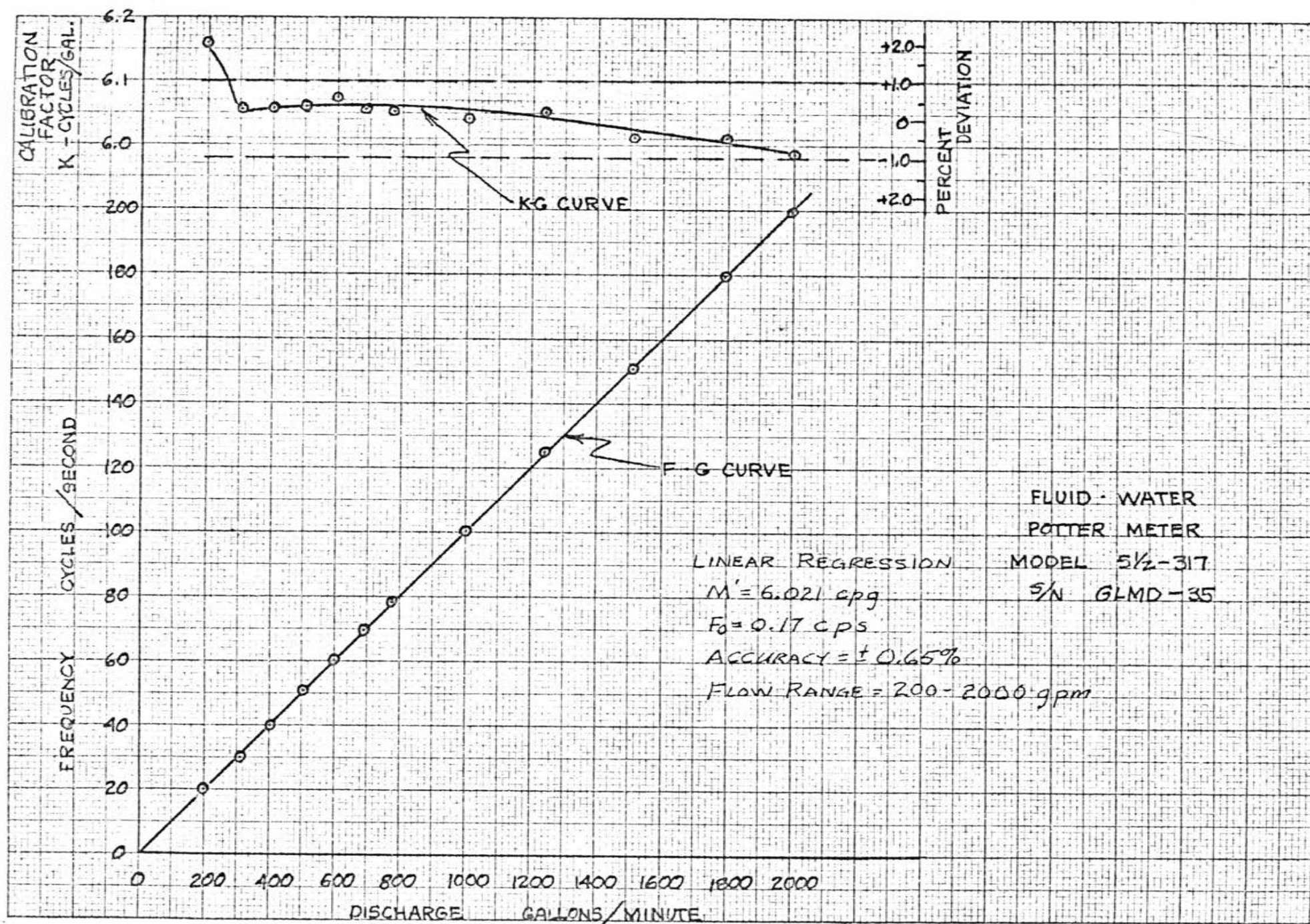












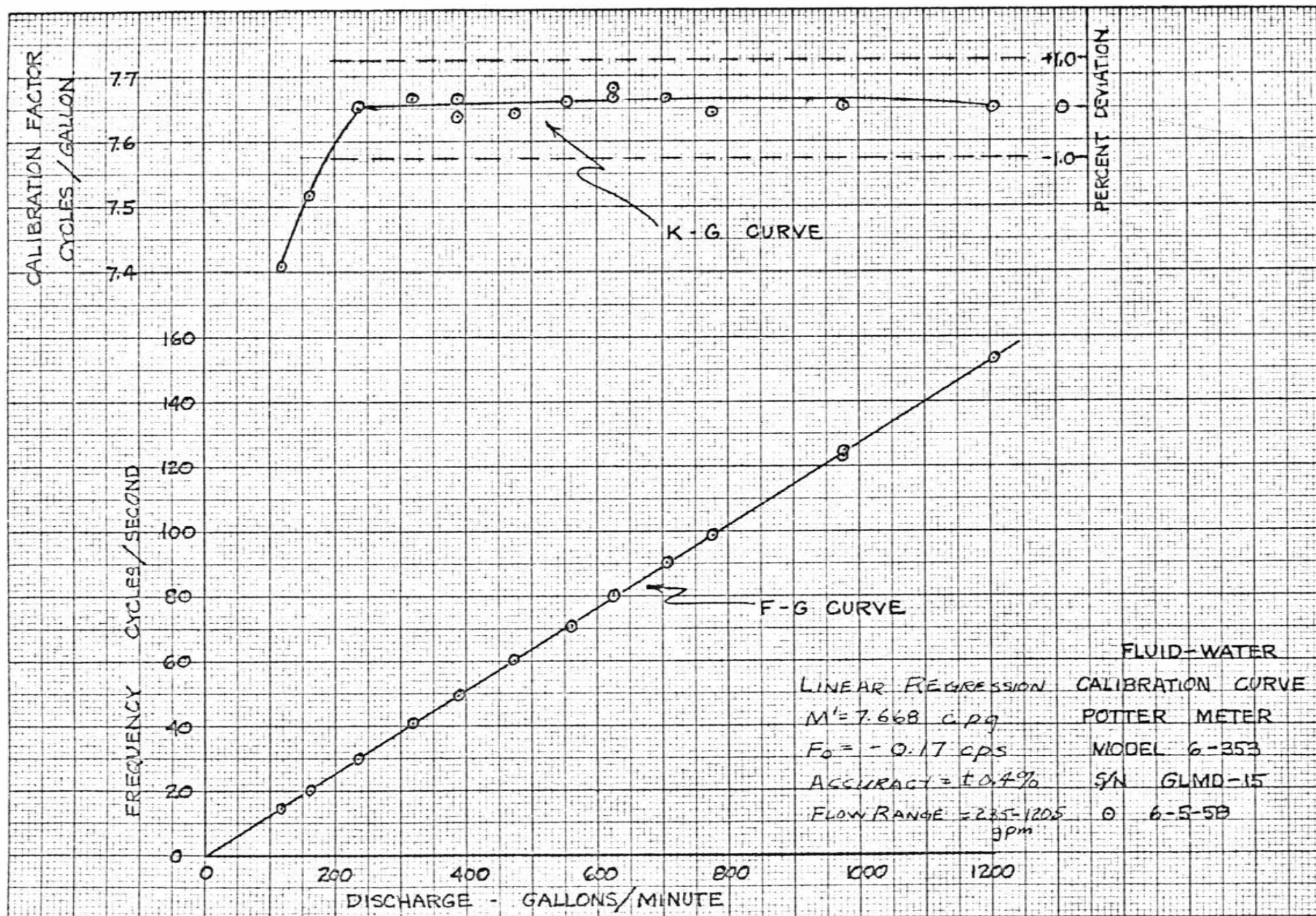
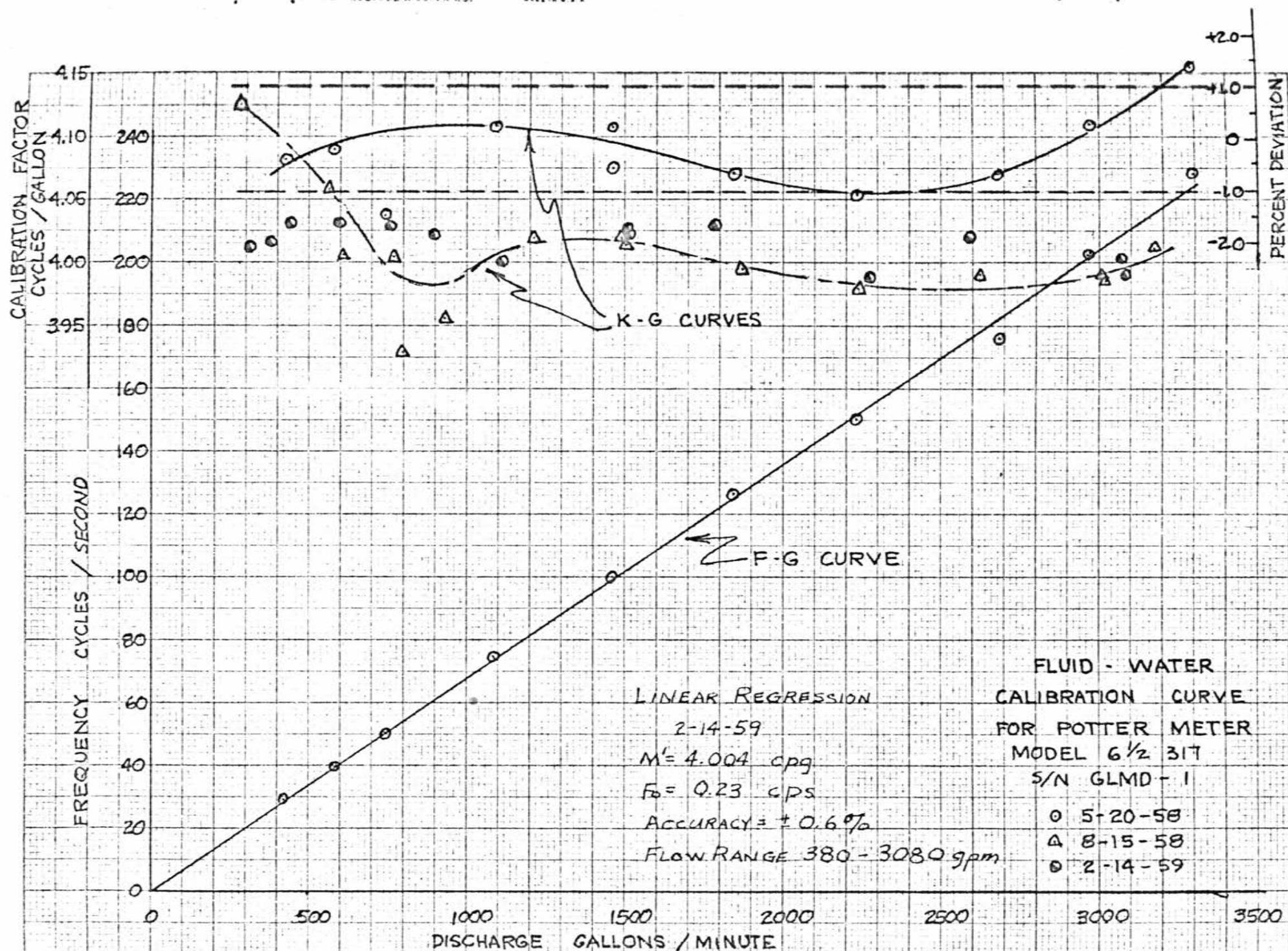
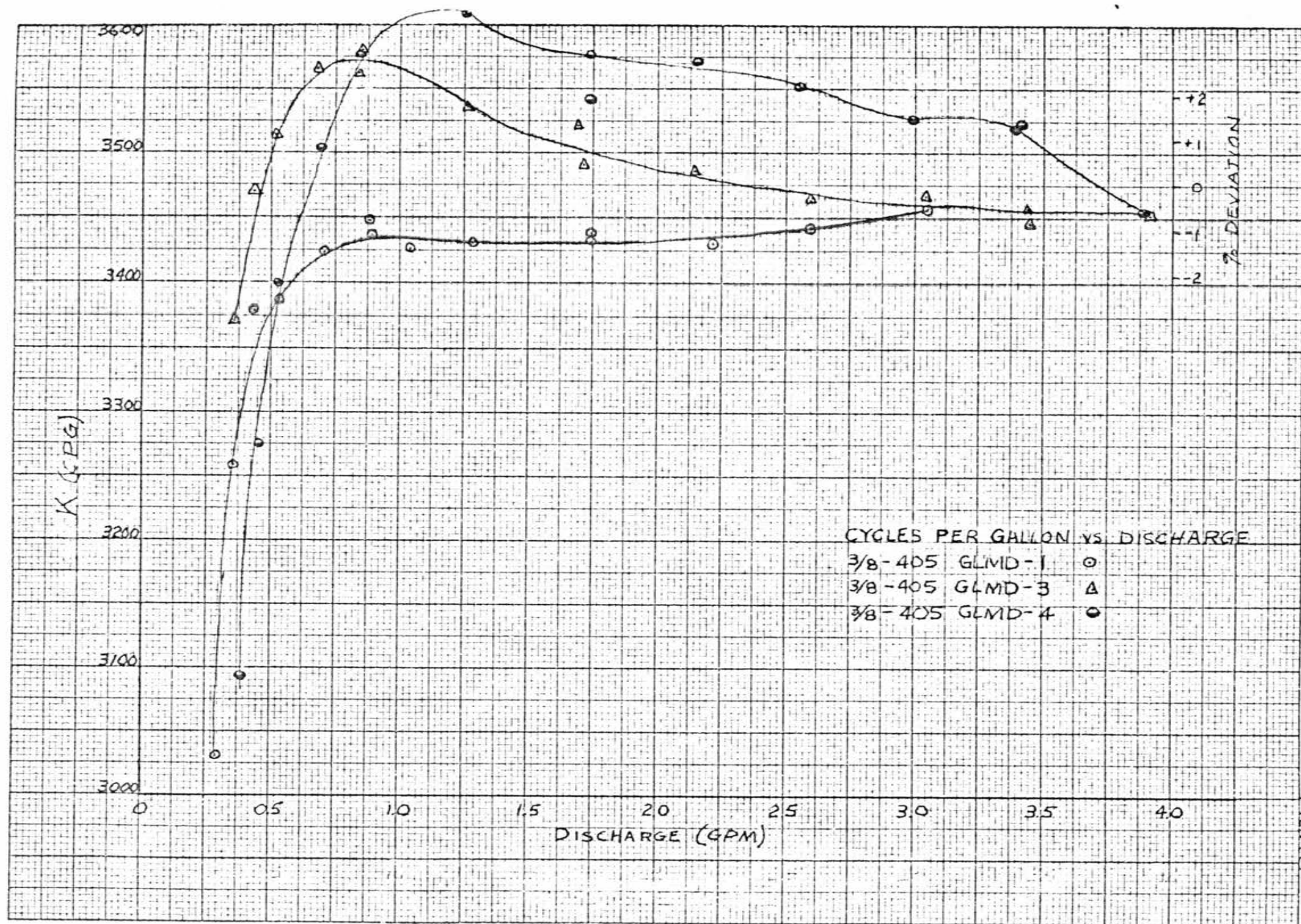


Fig. 14





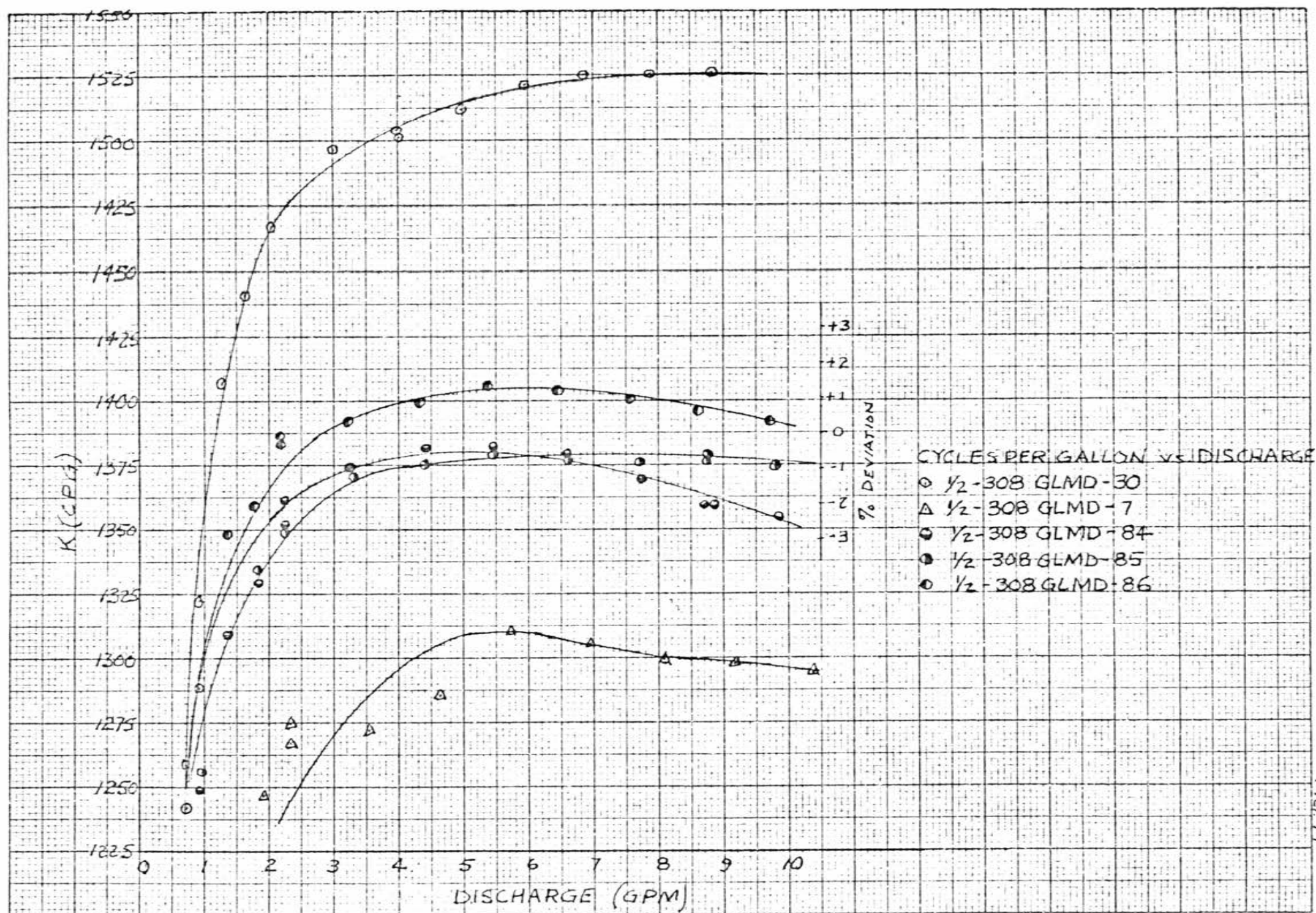
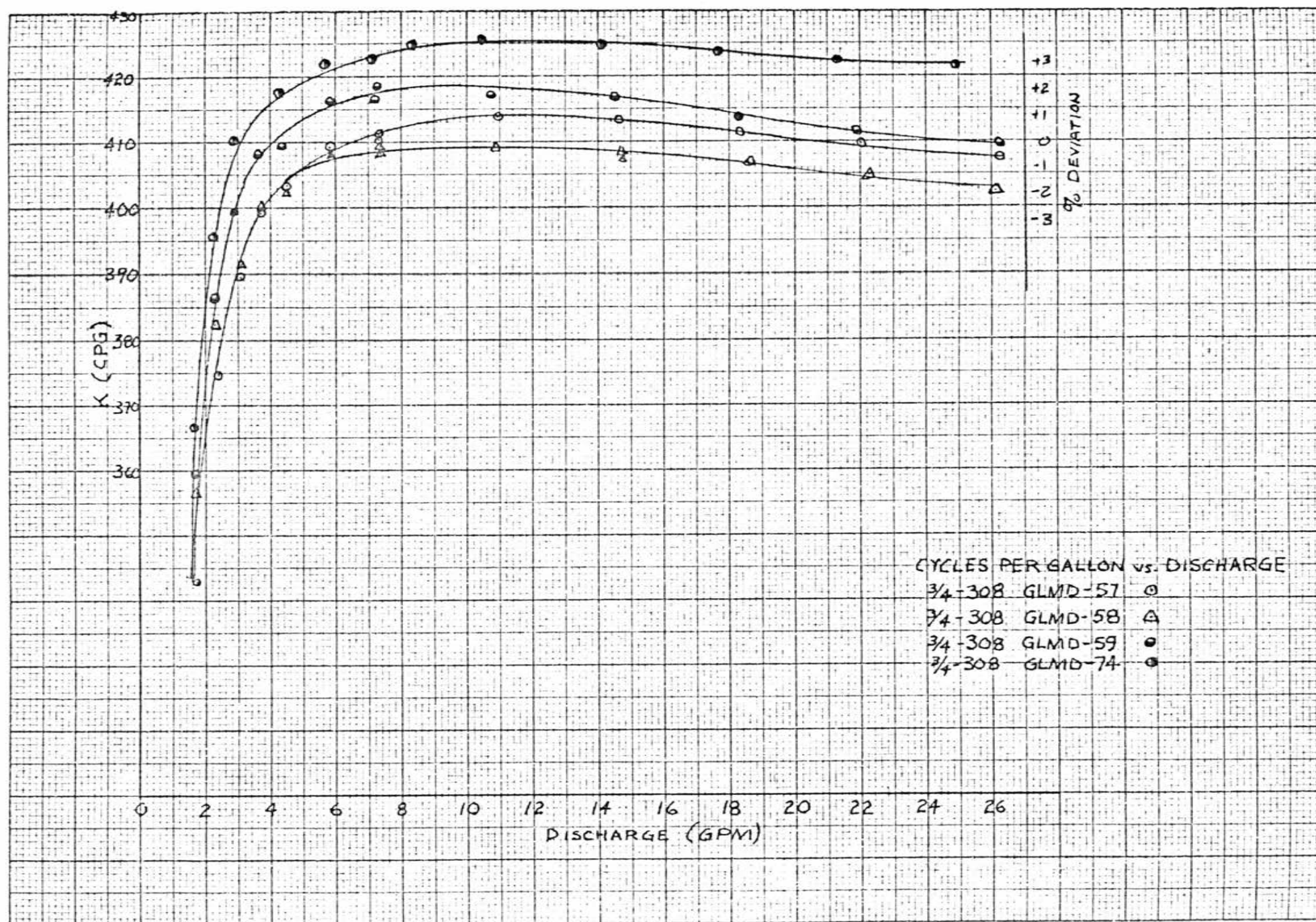


Fig. 17



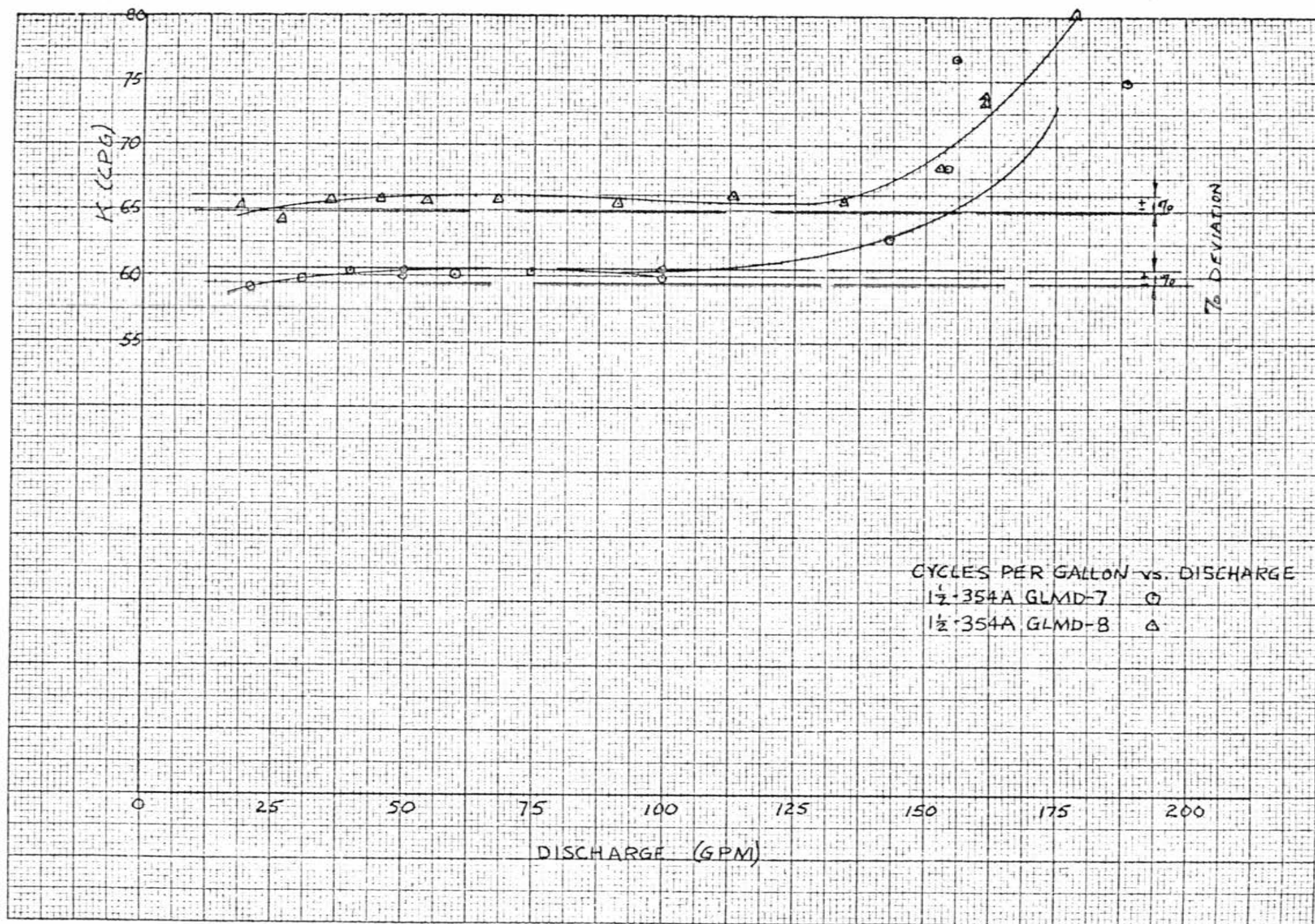
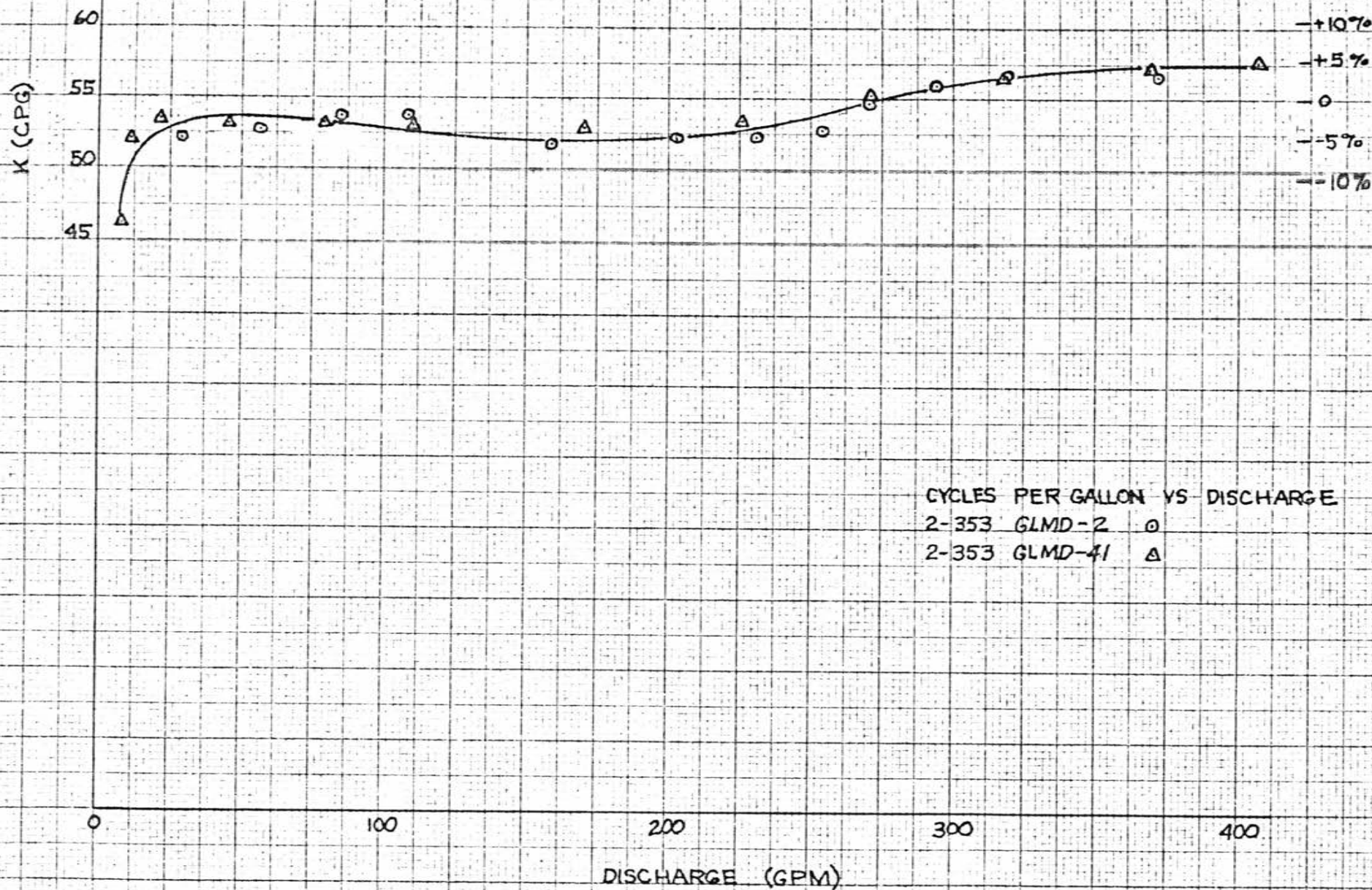
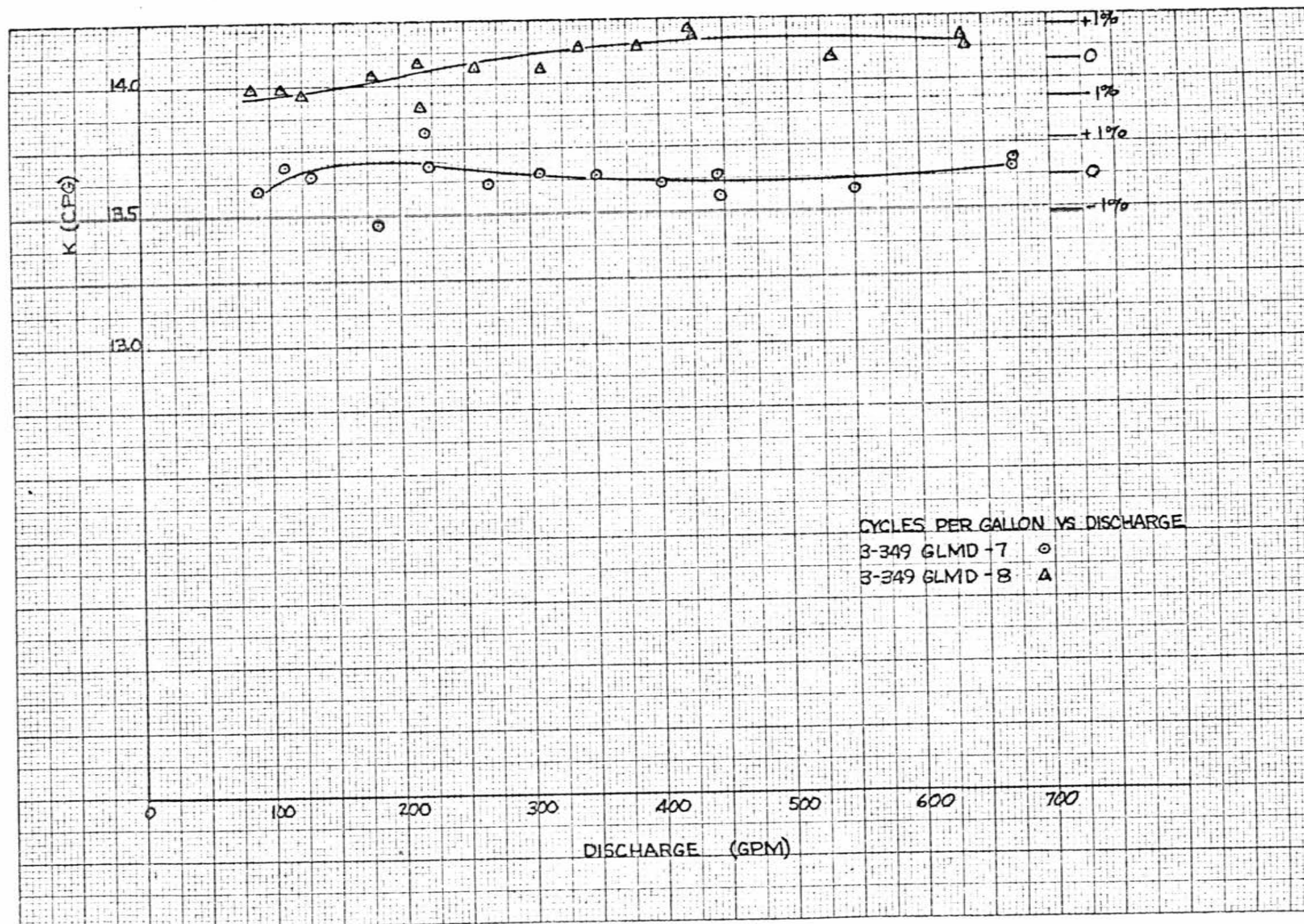
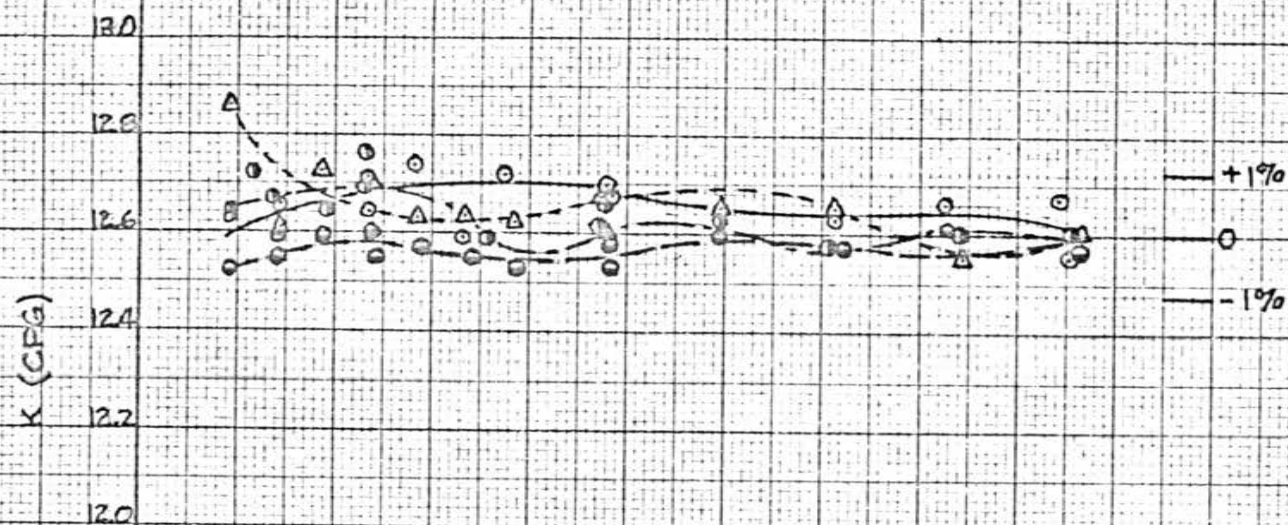


Fig. 19





CYCLES PER GALLON VS DISCHARGE
3-349 GLMD-7 ○
3-349 GLMD-8 Δ



CYCLES PER GALLON VS DISCHARGE

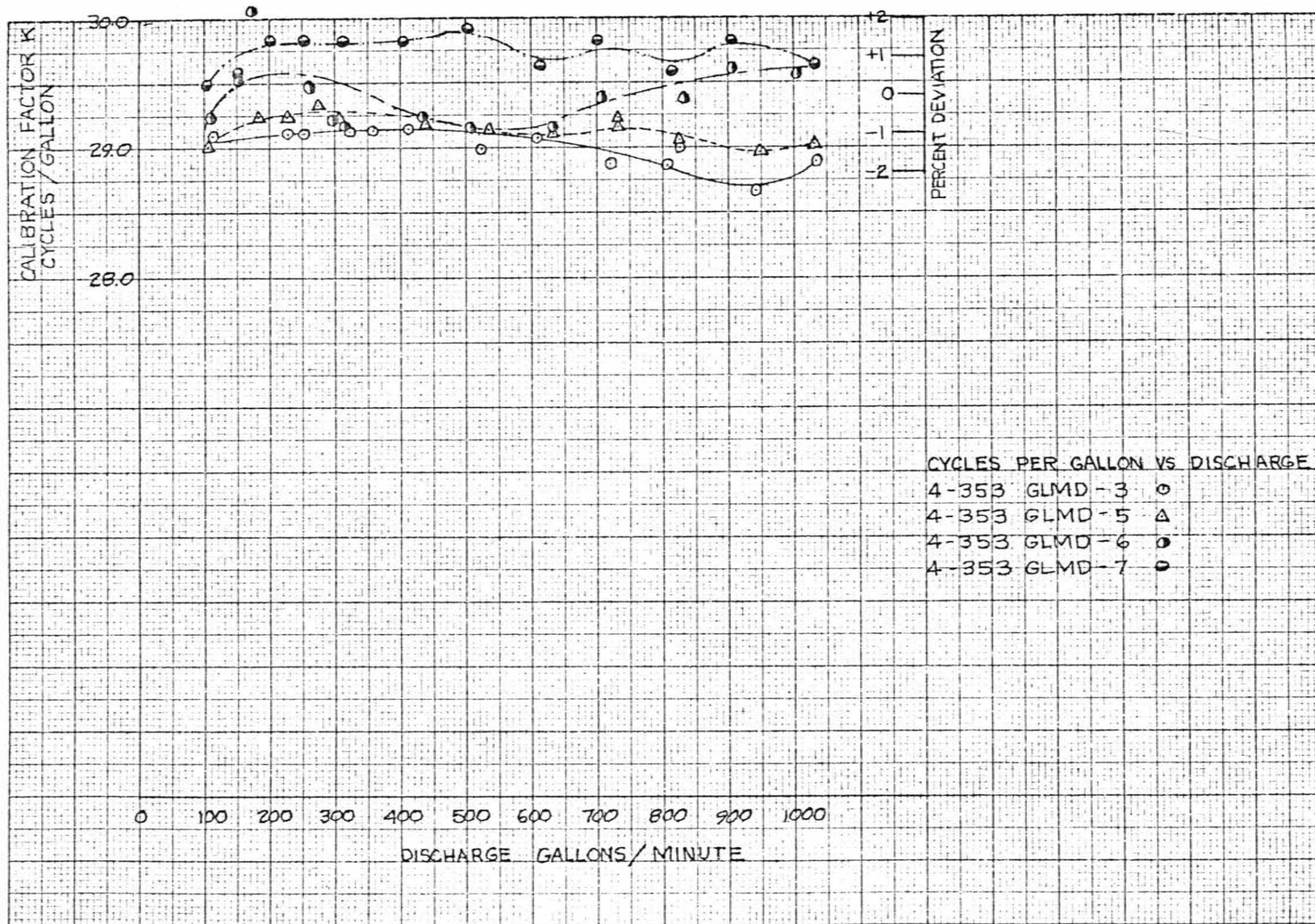
4-317 GLMD - 1 ○

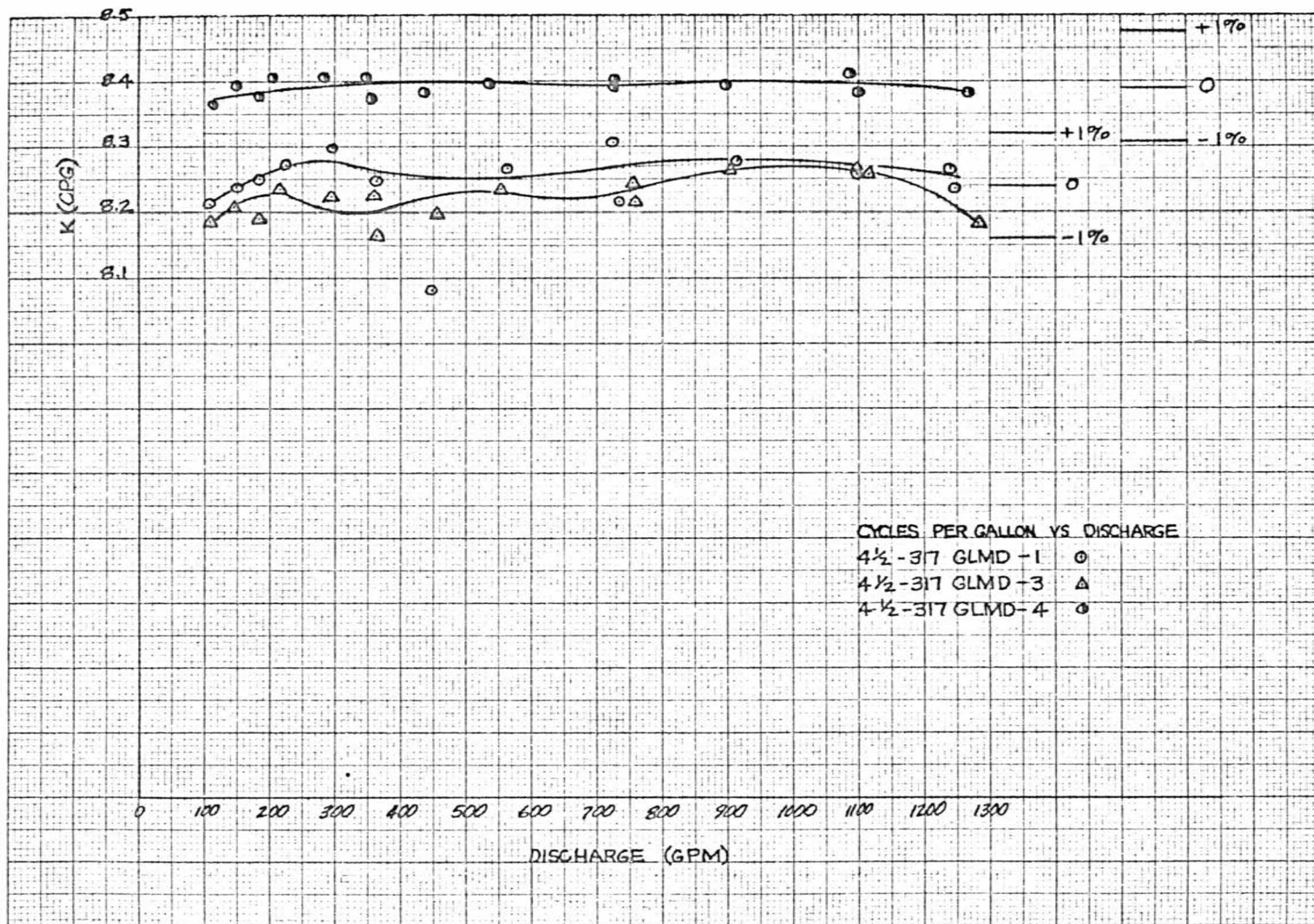
4-317 GLMD - 11 △

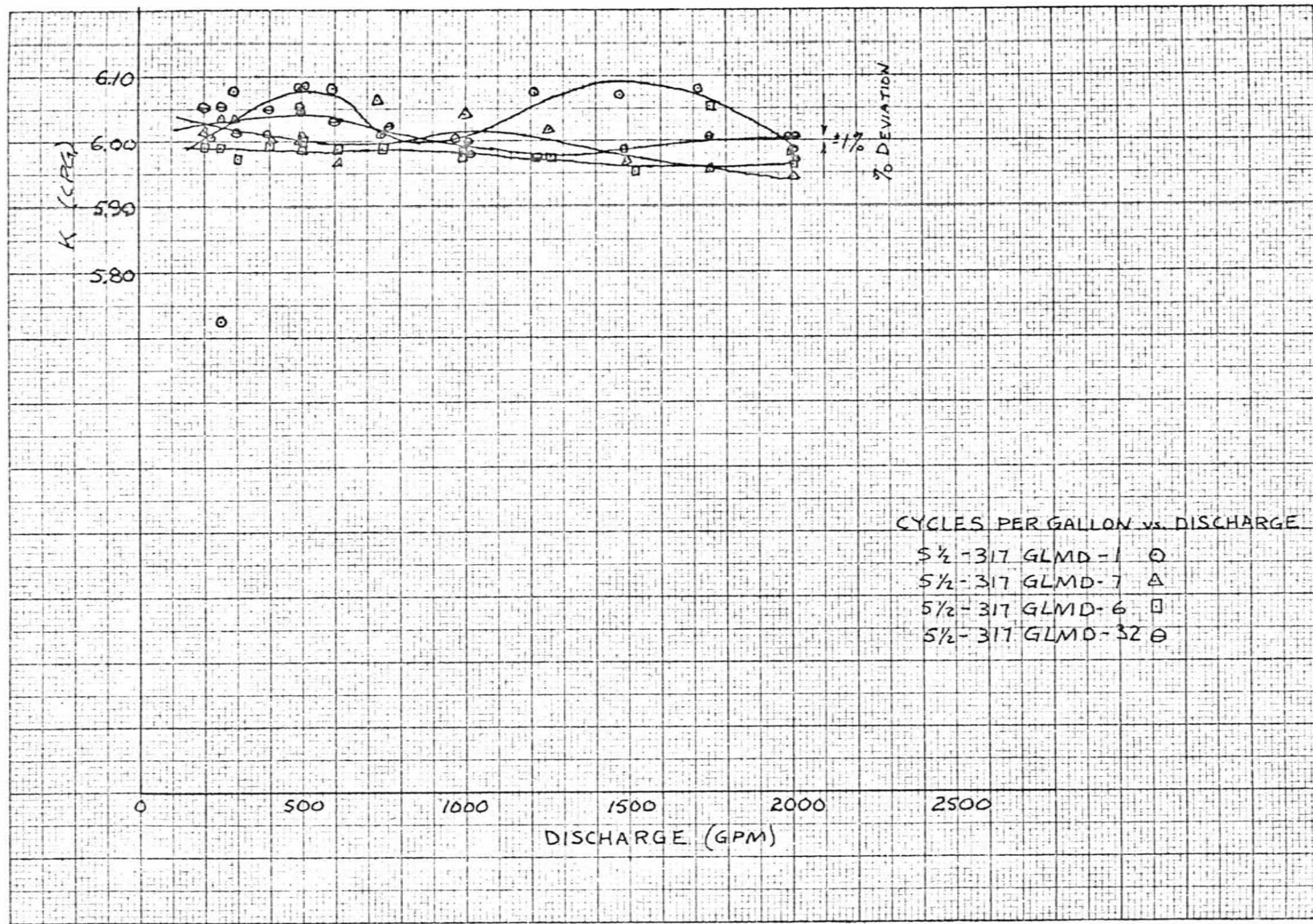
4-317 GLMD - 19 ●

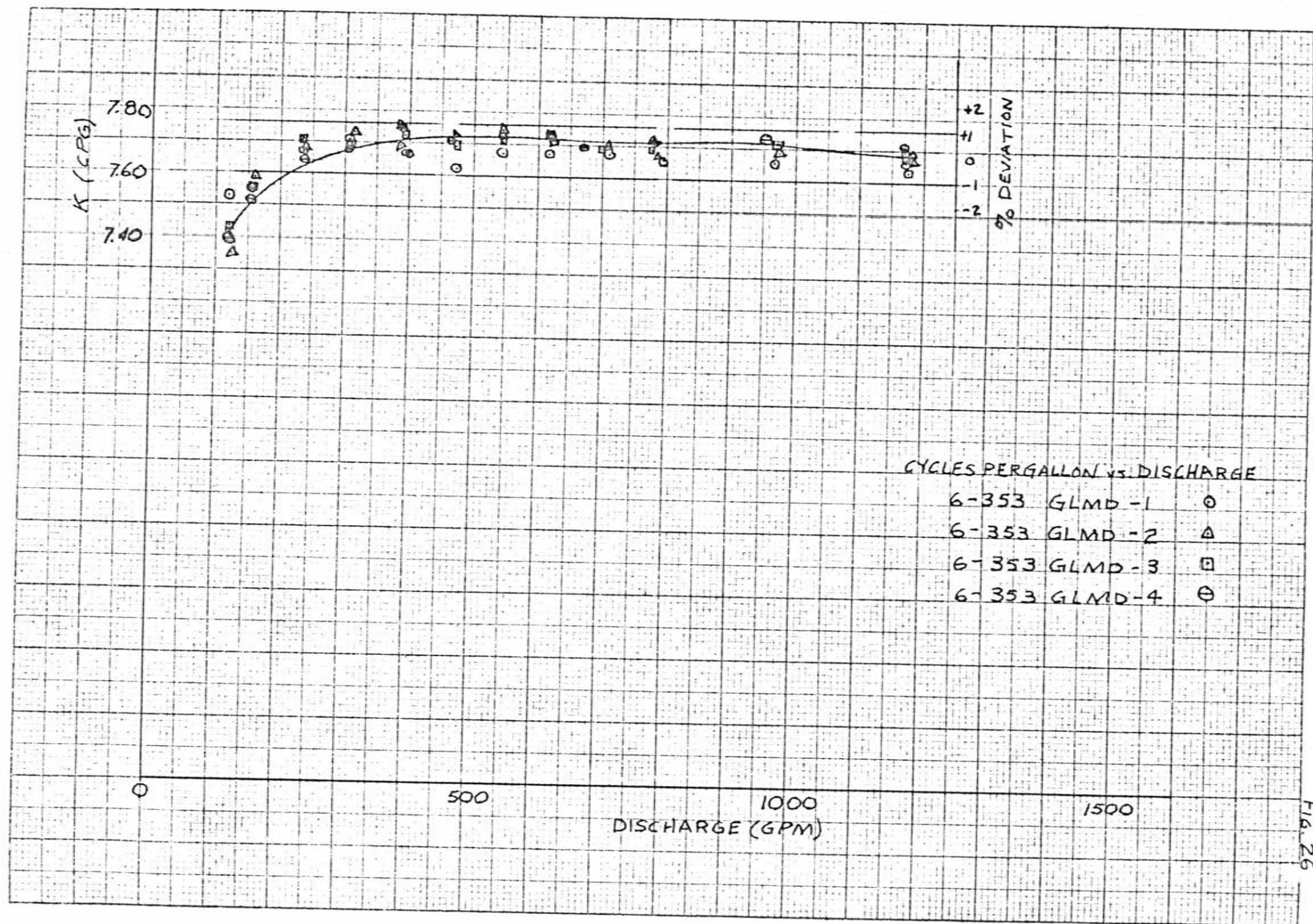
4-317 GLMD - 37 ◆

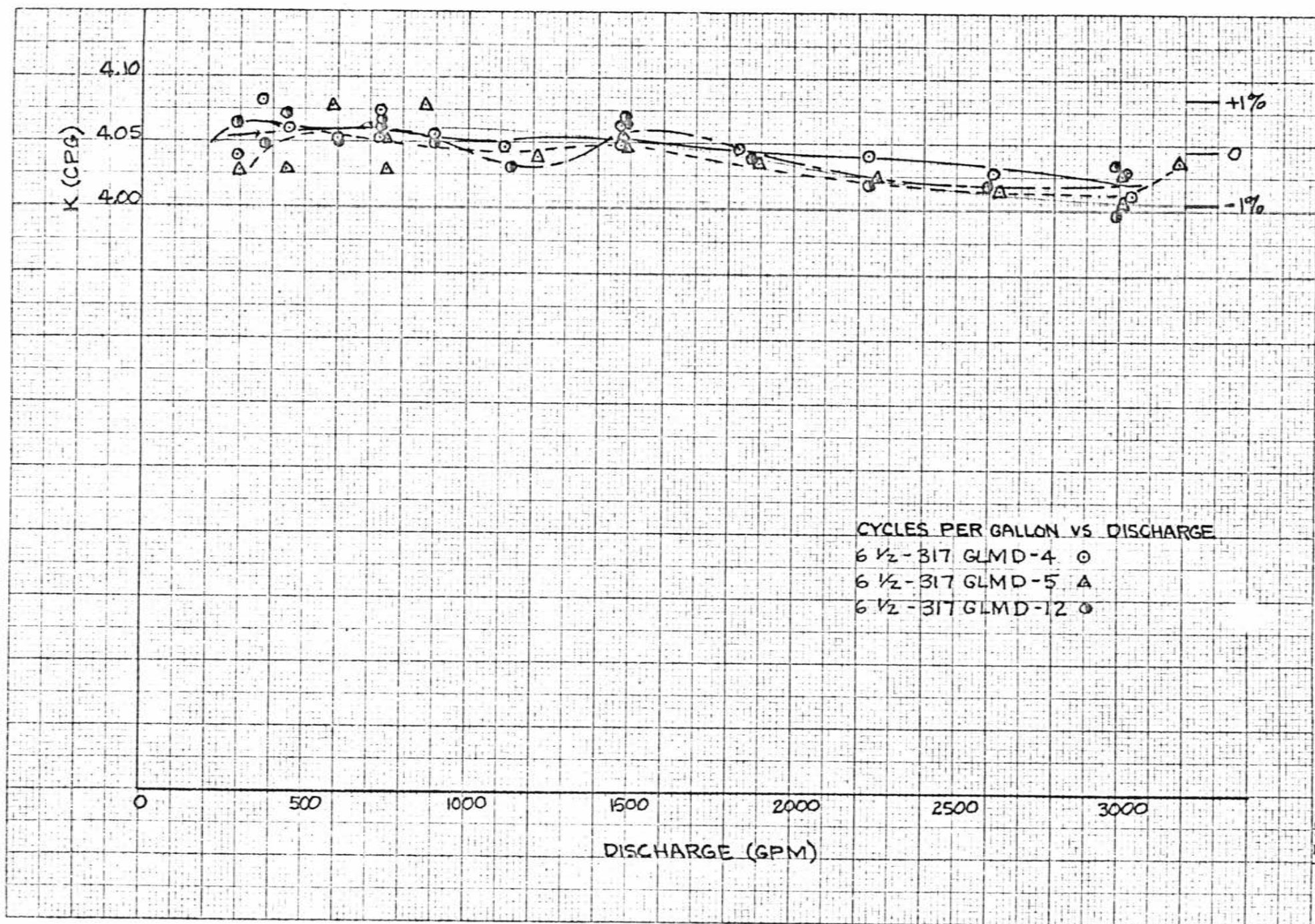
DISCHARGE (GPM)





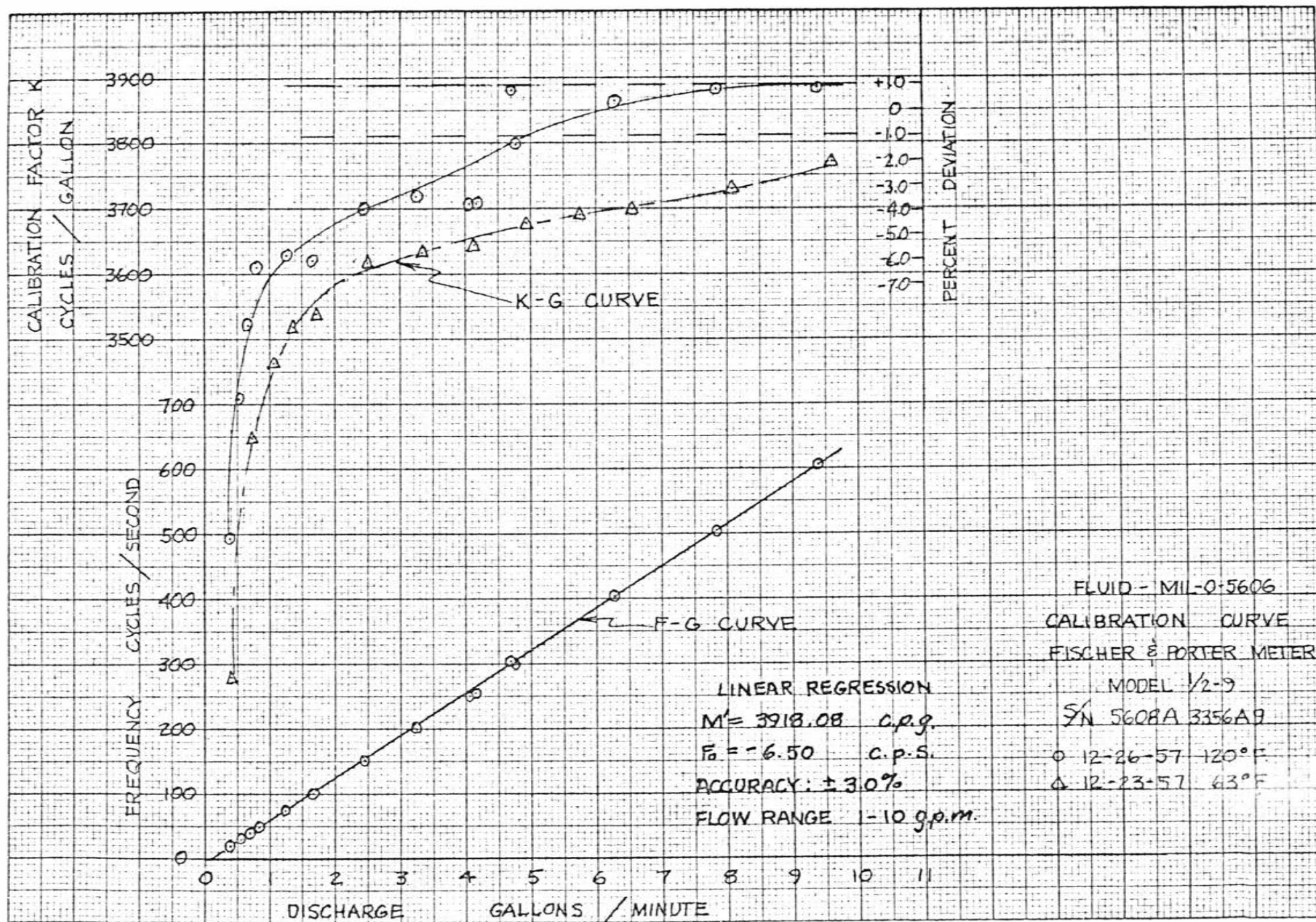






APPENDIX B

FISCHER AND PORTER FLOWMETERS



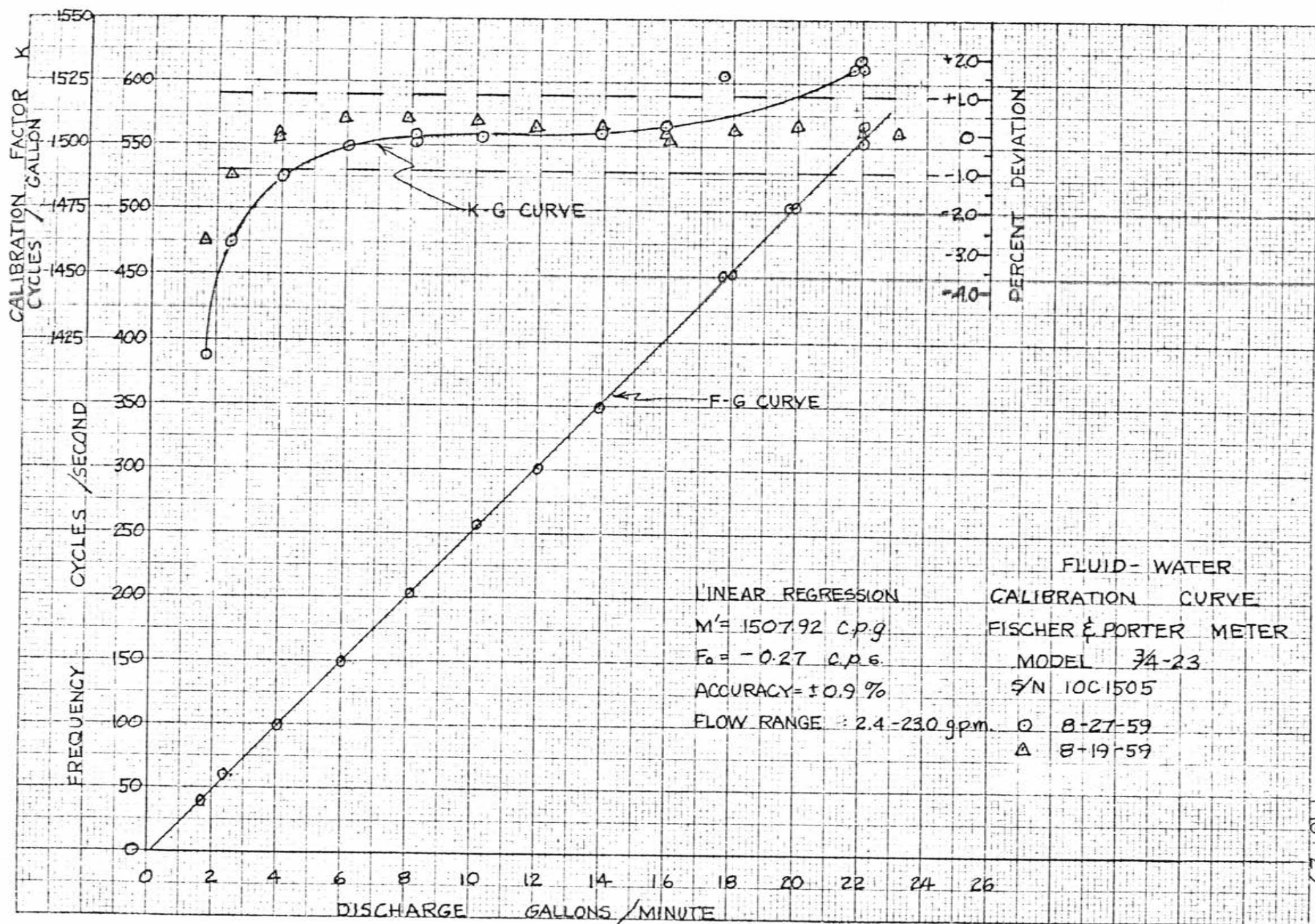
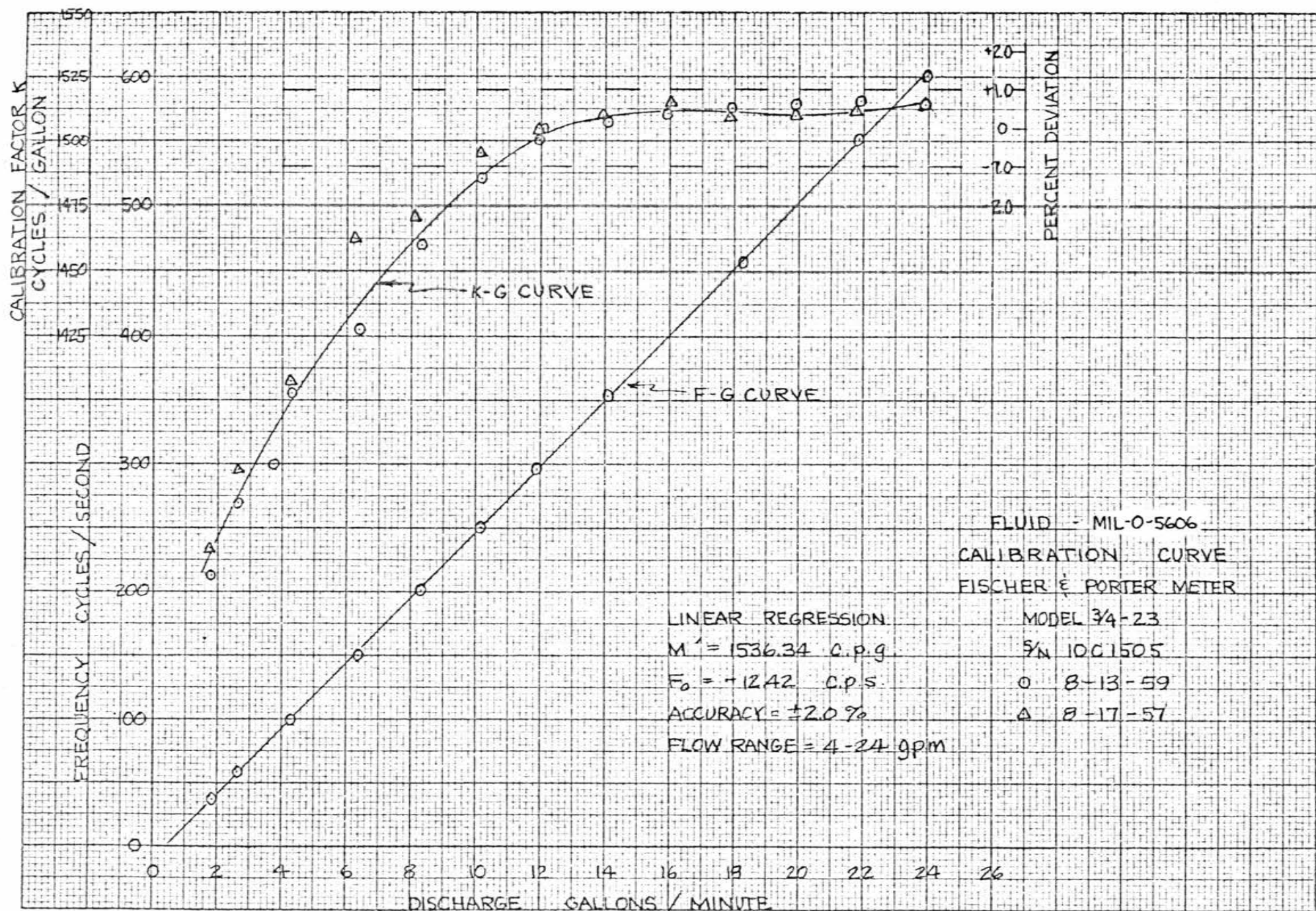
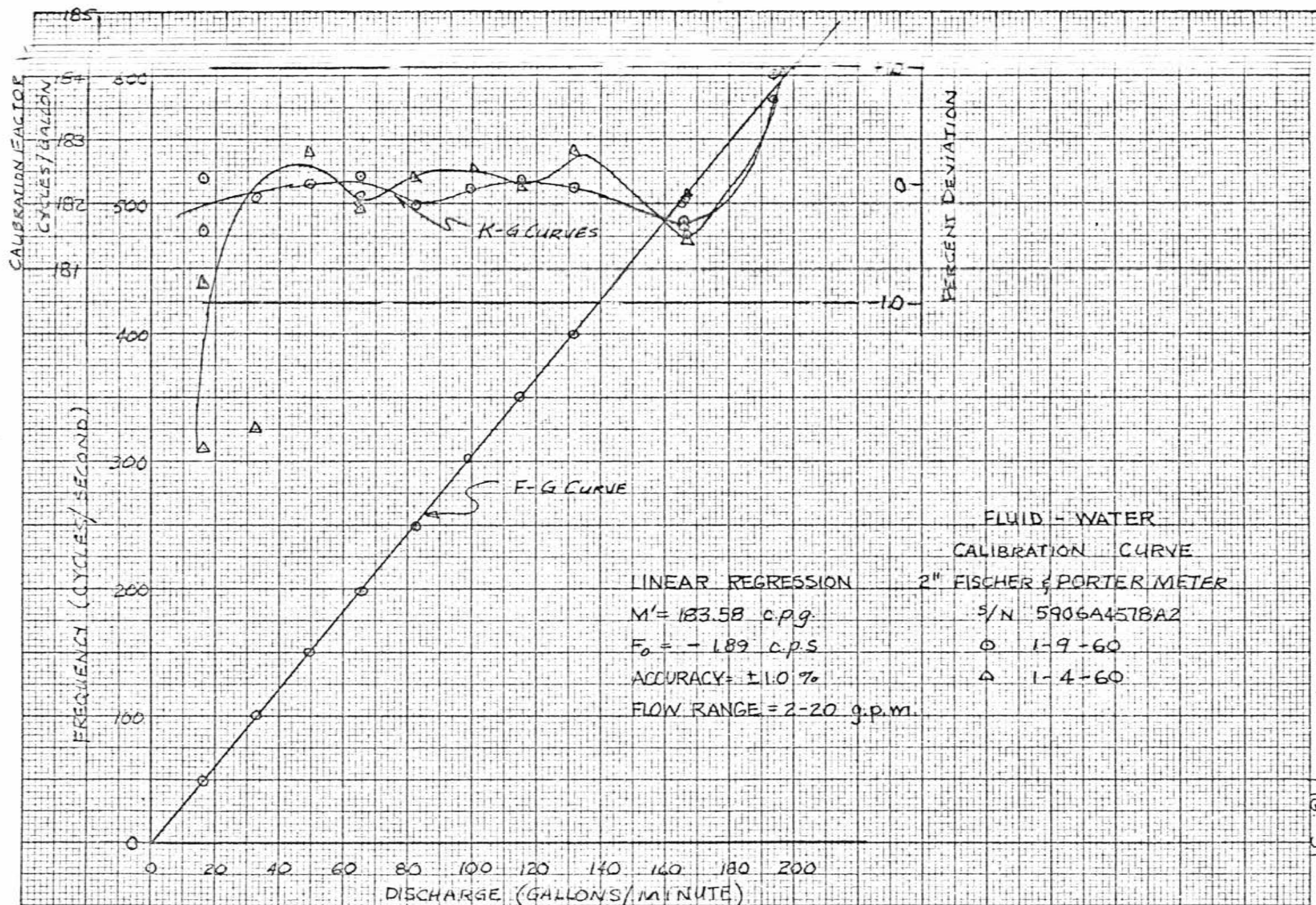


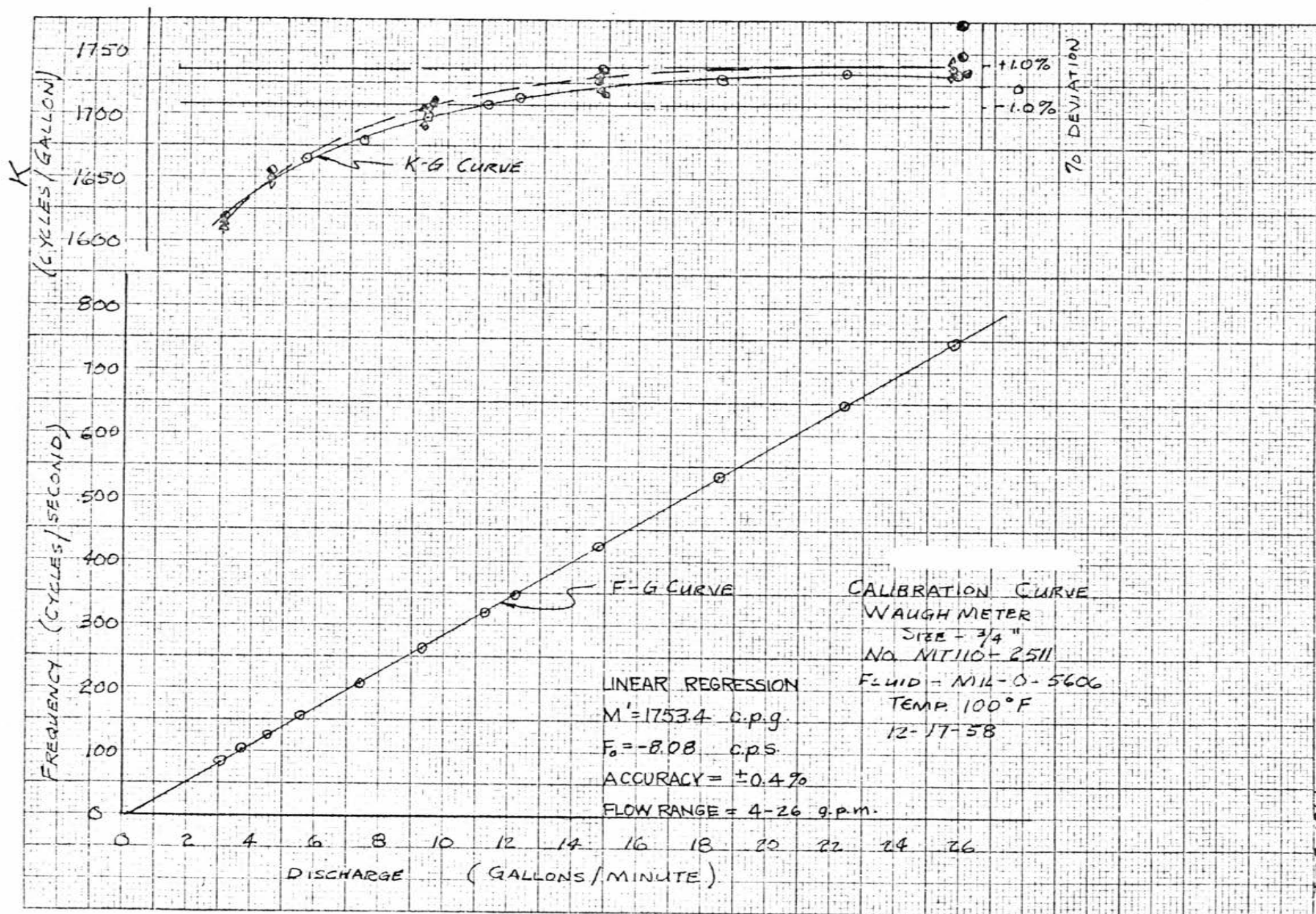
FIG. 29





APPENDIX C

WAUGH FLOWMETERS



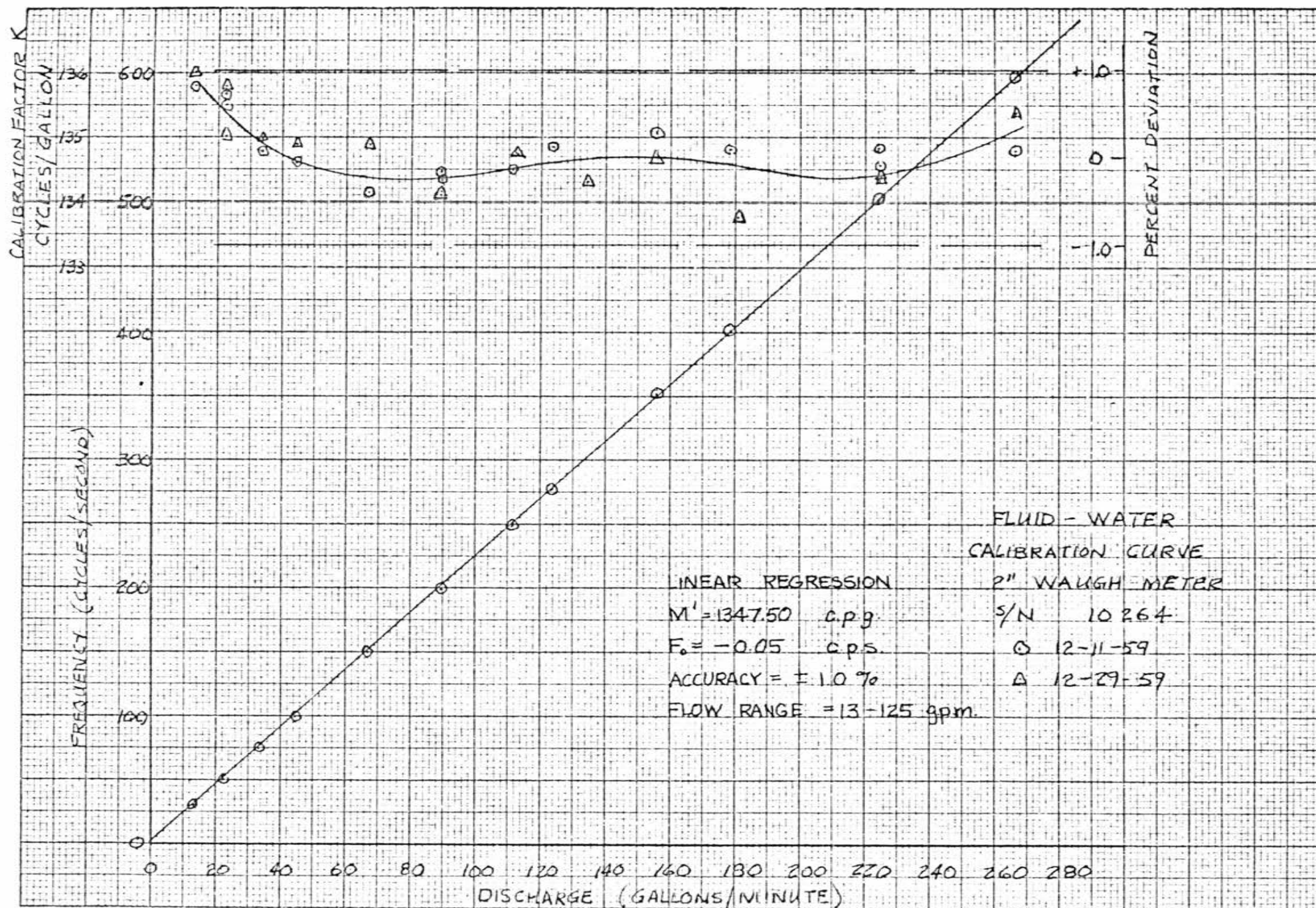


FIG. 33