WIND-TUNNEL STUDY OF LPC MANDALAY, LAS COLINAS, TEXAS

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LIST OF SYMBOLS

Symbol	Definition
U	Local mean velocity
D	Characteristic dimension (building height, width, etc.)
ν, ρ	Kinematic viscosity and density of approach flow
$\frac{UD}{\nu}$	Reynolds number
E	Mean voltage
A, B, n	Constants
U_{rms}	Root-mean-square of fluctuating velocity
E_{rms}	Root-mean-square of fluctuating voltage
U_∞	Reference mean velocity outside the boundary layer
X, Y	Horizontal coordinates
Z	Height above surface
δ	Height of boundary layer
T_u	Turbulence intensity $\frac{U_{rms}}{U_\infty}$ or $\frac{U_{rms}}{U}$
$C_{p_{mean}}$	Mean pressure coefficient $\frac{(p-p_\infty)_{mean}}{0.5\ \rho\ U_\infty^2}$
$C_{p_{rms}}$	Root-mean-square pressure coefficient, $\frac{(p-p_\infty) - (p-p_\infty)_{mean\ rms}}{0.5\ \rho\ U_\infty^2}$
$C_{p_{max}}$	Peak maximum pressure coefficient, $\frac{(p-p_\infty)_{max}}{0.5\ \rho\ U_\infty^2}$
$C_{p_{min}}$	Peak minimum pressure coefficient, $\frac{(p-p_\infty)_{min}}{0.5\ \rho\ U_\infty^2}$
$(\ )_{min}$	Minimum value during data record
$(\ )_{max}$	Minimum value during data record

LIST OF SYMBOLS (continued)

Symbol	Definition
P	Fluctuating pressure at a pressure tap on the structure
P_∞	Static pressure in the wind tunnel above the model
F_x, F_y	Forces in X, Y direction
A_R	Reference area
CF_X	Force coefficient, X direction, $\frac{F_X}{A_R \; 0.5 \; \rho \; U_\infty^2}$
CF_Y	Force coefficient, Y direction, $\frac{F_Y}{A_R \; 0.5 \; \rho \; U_\infty^2}$

1. INTRODUCTION

1.1 General

A significant characteristic of modern building design is lighter cladding and more flexible frames. These features produce an increased vulnerability of glass and cladding to wind damage and result in larger deflections of the building frame. In addition, increased use of pedestrian plazas at the base of the buildings has brought about a need to consider the effects of wind and gustiness in the design of these areas.

The building geometry itself may increase or decrease wind loading on the structure. Wind forces may be modified by nearby structures which can produce beneficial shielding or adverse increases in loading. Overestimating loads results in uneconomical design; underestimating may result in cladding or window failures. Tall structures have historically produced unpleasant wind and turbulence conditions at their bases. The intensity and frequency of objectionable winds in pedestrian areas is influenced both by the structure shape and by the shape and position of adjacent structures.

Techniques have been developed for wind-tunnel modeling of proposed structures which allow the prediction of wind pressures on cladding and windows, overall structural loading, and also wind velocities and gusts in pedestrian areas adjacent to the building. Information on sidewalk-level gustiness allows plaza areas to be protected by design changes before the structure is constructed. Accurate knowledge of the intensity and distribution of the pressures on the structure permits adequate but economical selection of cladding strength to meet selected maximum design winds and overall wind loads for the design of the frame for flexural control.

Modeling of the aerodynamic loading on a structure requires special consideration of flow conditions in order to guarantee similitude between model and prototype. A detailed discussion of the similarity requirements and their wind-tunnel implementation can be found in references (1), (2) and (3). In general, the requirements are that the model and prototype be geometrically similar, that the approach mean velocity at the building site have a vertical profile shape similar to the full-scale flow, that the turbulence characteristics of the flows be similar, and that the Reynolds number for the model and prototype be equal.

These criteria are satisfied by constructing a scale model of the structure and its surroundings and performing the wind tests in a wind tunnel specifically designed to model atmospheric boundary-layer flows. Reynolds number similarity requires that the quantity UD/ν be similar for model and prototype. Since ν, the kinematic viscosity of air, is identical for both, Reynolds numbers cannot be made precisely equal with reasonable wind velocities. To accomplish this the air velocity in the wind tunnel would have to be as large as the model scale factor times the prototype wind velocity, a velocity which would introduce unacceptable compressibility effects. However, for sufficiently high Reynolds numbers ($>2\times10^4$) the pressure coefficient at any location on the structure will be essentially constant for a large range of Reynolds numbers. Typical values encountered are 10^7-10^8 for the full-scale and 10^5-10^6 for the wind-tunnel model. In this range acceptable flow similarity is achieved without precise Reynolds number equality.

1.2 The Wind-Tunnel Test

The wind-engineering study is performed on a building or building group modeled at scales ranging from 1:150 to 1:400. The building model is constructed of clear plastic fastened together with screws. The structure is modeled in detail to provide accurate flow patterns in the wind passing over the building surfaces. The building under test is often located in a surrounding where nearby buildings or terrain may provide beneficial shielding or adverse wind loading. To achieve similarity in wind effects the area surrounding the test building is also modeled. A flow visualization study is first made (smoke is used to make the air currents visible) to define overall flow patterns and identify regions where local flow features might cause difficulties in building curtain-wall design or produce pedestrian discomfort.

The test model, equipped with pressure taps (200 to 600 or more), is exposed to an appropriately modeled atmospheric wind in the wind tunnel and the fluctuating pressure at each tap measured electronically. The model, and the modeled area, are rotated 10 or 15 degrees and another set of data recorded for each pressure tap. Normally, 24 or 36 sets of data (360 degrees of turning) are taken; however, when flow visualization or recorded data indicate high pressure regions of small azimuthal extent, data is obtained in smaller azimuthal steps.

Data are recorded, analyzed and processed by an on-line computerized data-acquisition system. Pressure coefficients of several types are calculated by the computer for each reading on each piezometer tap and are printed in tabular form as computer readout. Using wind data applicable to the building site, representative wind velocities are selected for combination with measured pressures on the building model.

Integration of test data with wind data results in prediction of peak local wind pressures for design of glass or cladding and may include overall forces and moments on the structure (by floor if desired) for design of the structural frame. Pressure contours are drawn on the developed building surfaces showing the intensity and distribution of peak wind loads on the building. These results may be used to divide the building into zones where lighter or heavier cladding or glass may be desirable.

Based on the visualization (smoke) tests and on a knowledge of heavy pedestrian use areas, a dozen or more locations may be chosen at the base of the building where wind velocities can be measured to determine the relative comfort or discomfort of pedestrians in plaza areas near building entrances, near building corners, or on sidewalks. Usually a reference pedestrian position is also tested to determine whether the wind environment in the building area is better or worse than the environment a block or so away in an undisturbed area.

The following pages discuss in greater detail the procedures followed, the equipment and data collecting and processing methods used. In addition, the data presentation format is explained and the implications of the data are discussed.

2. EXPERIMENTAL CONFIGURATION

2.1 Wind Tunnel

Wind-engineering studies are performed in the Fluid Dynamics and Diffusion Laboratory at Colorado State University (Figure 1). Three large wind tunnels are available for wind loading studies depending on the detailed requirements of the study. The wind tunnel used for this investigation is shown in Figure 2. All tunnels have a flexible roof adjustable in height to maintain a zero pressure gradient along the test section. The mean velocity can be adjusted continuously in each tunnel to the maximum velocity available.

2.2 Model

In order to obtain an accurate assessment of local pressures using piezometer taps, models are constructed to the largest scale that does not produce significant blockage in the wind-tunnel test section. The models are constructed of 1/2-in. thick Lucite plastic and fastened together with metal screws. Significant variations in the building surface, such as mullions, are machined into the plastic surface. Piezometer taps (1/16 in. diameter) are drilled normal to the exterior vertical surfaces in rows at several or more elevations between the bottom and top of the building. Similarly, taps are placed in the roof and on any sloping, protruding, or otherwise distinctive features of the building that might need investigation.

Pressure tap locations are chosen so that the entire surface of the building can be investigated for pressure loading and at the same time permit critical examination of areas where experience has shown that maximum wind effects may be expected to occur. Locations of the pressure taps for this study are shown in Figure 3. Dimensions are given

both for full-scale building (in ft) and for model (in in.). The pressure tap numbers are shown adjacent to the taps.

The pressure tests are sometimes made in two stages. In the first stage measurements are made on the initial distribution of pressure taps. If it becomes apparent from the data that the loading on the building is being influenced by some unsuspected geometry of the building or adjacent structures, additional pressure taps are installed in the critical areas. The locations of the taps are selected so that the maximum loading can be detected and the area over which this loading is acting can be defined. Any added taps are also shown in Figure 3.

A circular area 750 to 2000 ft in radius depending on model scale and characteristics of the surrounding buildings and terrain is modeled in detail. Structures within the modeled region are made from styrofoam and cut to the individual building geometries. They are mounted on the turntable in their proper locations. Significant terrain features are included as needed. The model is mounted on a turntable (Figure 2) near the downwind end of the test section. Any buildings or terrain features which do not fit on the turntable are placed on removable pieces which are placed upwind of the turntable for appropriate wind directions. A plan view of the building and its surroundings is shown in Figure 4. Geometric configurations are specified along with the data configuration in Table 1. The turntable is calibrated to indicate azimuthal orientation to 0.1 degree.

The region upstream from the modeled area is covered with a randomized roughness constructed using various sized cubes placed on the floor of the wind tunnel. Different roughness sizes may be used for different wind directions. Spires are installed at the test-section entrance to

provide a thicker boundary layer than would otherwise be available. The thicker boundary layer permits a somewhat larger scale model than would otherwise be possible. The spires are approximately triangularly shaped pieces of 1/2-in. thick plywood 6 in. wide at the base and 1 in. wide at the top, extending from the floor to the top of the test section. They are placed so that the broad side intercepts the flow. A barrier approximately 8 in. high is placed on the test-section floor downstream of the spires to aid in development of the boundary-layer flow.

The distribution of the roughness cubes and the spires in the roughened area was designed to provide a boundary-layer thickness of approximately 4 ft, a velocity profile power-law exponent similar to that expected to occur in the region approaching the modeled area for each wind direction (a number of wind directions may have the same approach roughness). Photographs of the completed model in the wind tunnel are shown in Figure 5. The wind-tunnel ceiling is adjusted after placement of the model to obtain a zero pressure gradient along the test section.

3. INSTRUMENTATION AND DATA ACQUISITION

3.1 Flow Visualization

Making the air flow visible in the vicinity of the model is helpful (a) in understanding and interpreting mean and fluctuating pressures, (b) in defining zones of separated flow and reattachment and zones of vortex formation where pressure coefficients may be expected to be high, and (c) in indicating areas where pedestrian discomfort may be a problem. Titanium tetrachloride smoke is released from sources on and near the model to make the flow lines visible to the eye and to make it possible to obtain motion picture records of the tests. Conclusions obtained from these smoke studies are discussed in Sections 4.1 and 5.1.

3.2 Pressures

Mean and fluctuating pressures are measured at each of the pressure taps on the model structure. Data are obtained for 24 or 36 wind directions, rotating the entire model assembly in a complete circle. Seventy-six pieces of 1/16 in. I.D. plastic tubing are used to connect pressure ports to four 48 tap pressure switches mounted under the model. The switch and tubing were designed to minimize the attenuation of pressure fluctuations across the switch. Each of the measurement ports is directed in turn by the switch to one of four pressure transducers mounted close to the switch. Four pressure input taps not used for transmitting building surface pressures are connected to a common tube leading outside the wind tunnel. This arrangement provides both a means of performing in-place calibration of the transducers and, by connecting this tube to a pitot tube mounted inside the wind tunnel, a means of automatically monitoring the tunnel speed. The switch is operated by means of a computer activated motor. The computer-controlled motor

steps the switch into each of the 20 required positions. The computer keeps track of switch position but a digital readout of position is provided at the wind tunnel.

The pressure transducers used are Setra differential transducers (Model 237) with a 0.10 psid range. Reference pressures are obtained by connecting the reference sides of the four transducers, using plastic tubing, to the static side of a pitot-static tube mounted in the wind tunnel free stream above the model building. In this way the transducer measures the instantaneous difference between the local pressures on the surface of the building and the static pressure in the free stream above the model.

Output from the pressure transducers is fed to an on-line data acquisition system consisting of a Hewlett-Packard 21 MX computer, disk unit, card reader, printer, Digi-Data digital tape drive and a Preston Scientific analog-to-digital converter. The data are processed immediately into pressure coefficient form as described in Section 4.3 and stored for printout or further analysis.

All four transducers are recorded simultaneously for 16 seconds at a 250 sample-per-second rate. The results of an experiment to determine the length of record required to obtain stable mean and rms (root-mean-square) pressures and to determine the overall accuracy of the pressure data acquisition system is shown in Figure 6. A typical pressure port record was integrated for a number of different time periods to obtain the data shown. Examination of a large number of pressure taps showed

that the overall accuracy for a 16-second period is, in pressure coefficient form, 0.03 for mean pressures, 0.1 for peak pressures, and 0.01 for rms pressures. Pressure coefficients are defined in Section 4.3.

3.3 Velocity

Mean velocity and turbulence intensity profiles are measured upstream of the model to determine that an approach boundary-layer flow appropriate to the site has been established. Tests are made at one wind velocity in the tunnel. This velocity is well above that required to produce Reynolds number similarity between the model and the prototype as discussed in Section 1.1.

In addition, mean velocity and turbulence intensity measurements are made 5 to 7 ft (prototype) above the surface at a dozen or more locations on and near the building for 16 wind directions. The measurement locations are shown on Figure 4. The surface measurements are indicative of the wind environment to which a pedestrian at the measurement location would be subjected. The locations are chosen to determine the degree of pedestrian comfort or discomfort at the building corners where relatively severe conditions frequently are found, near building entrances and on adjacent sidewalks where pedestrian traffic is heavy, and in open plaza areas. In most studies a reference pedestrian position, located about a block away, is also tested. These data are helpful in evaluating the degree of pedestrian comfort or discomfort in the proposed plaza area in terms of the undisturbed environment in the immediate vicinity.

Measurements are made with a single hot-wire anemometer mounted with its axis vertical. The instrumentation used is a Thermo Systems constant temperature anemometer (Model 1050) with a 0.001 in. diameter

platinum film sensing element 0.020 in. long. Output is directed to the on-line data acquisition system for analysis.

Calibration of the hot-wire anemometer is performed by comparing output with the pitot-static tube in the wind tunnel. The calibration data fit to a variable exponent King's Law relationship of the form

$$E^2 = A + BU^n$$

where E is the hot-wire output voltage, U the velocity and A, B, and n are coefficients selected to fit the data. The above relationship was used to determine the mean velocity at measurement points using the measured mean voltage. The fluctuating velocity in the form U_{rms} (root-mean-square velocity) was obtained from

$$U_{rms} = \frac{2\ E\ E_{rms}}{B\ n\ U^{n-1}}$$

where E_{rms} is the root-mean-square voltage output from the anemometer. For interpretation all turbulence measurements for pedestrian winds were divided by the mean velocity outside the boundary-layer U_∞. Turbulence intensity in velocity profile measurements used the local mean velocity.

4. RESULTS

4.1 Flow Visualization

A film is included as part of this report showing the characteristics of flow about the structure using smoke to make the flow visible. Flow visualization experiments were conducted at selected locations for various configurations. Several features can be noted from the visualization. As with all large structures, wind approaching the building is deflected down to the plaza level, up over the structure and around the sides. A description of the smoke test results emphasizing flow patterns of concern relative to possible high-wind load areas and pedestrian comfort is given in Section 5.1.

4.2 Velocity

Velocity and turbulence profiles are shown in Figure 7. Profiles were taken upstream from the model which are characteristic of the boundary layer approaching the model and at the building site with building removed. The boundary-layer thickness, δ, is shown in Figure 7. The corresponding prototype value of δ for this study is also shown in the figure. This value was established as a reasonable height for this study. The mean velocity profile approaching the modeled area has the form

$$\frac{U}{U_\infty} = \left(\frac{z}{\delta}\right)^n .$$

The exponent n for the approach flow established for this study is shown in Figure 7.

Profiles of longitudinal turbulence intensity in the flow approaching the modeled area are shown in Figure 7. The turbulence intensities are appropriate for the approach mean velocity profile selected. For the velocity profiles, turbulence intensity is defined as the root-

mean-square about the mean of the longitudinal velocity fluctuations divided by the local mean velocity U,

$$Tu = \frac{U_{rms}}{U} .$$

Velocity data obtained at each of the pedestrian measurement locations shown in Figure 4 are listed in Table 2 as mean velocity U/U_∞, turbulence intensity U_{rms}/U_∞, and largest effective gust

$$U_{pk} = \frac{U + 3U_{rms}}{U_\infty} .$$

These data are plotted in polar form in Figure 8. Measurements were taken 5 to 7 ft above the ground surface. An analysis of these wind data is given in Section 5.2.

To enable a quantitative assessment of the wind environment, the wind-tunnel data were combined with wind frequency and direction information obtained at the local airport. Table 3 shows wind frequency by direction and magnitude obtained from summaries published by the National Weather Service. These data, usually obtained at an elevation of about 30-40 ft, were converted to velocities at the reference velocity height for the wind-tunnel measurements and combined with the wind-tunnel data to obtain cumulative probability distributions (percent time a given velocity is exceeded) for wind velocity at each measuring location. The percentage times were summed by wind direction to obtain a percent time exceeded at each measuring position independent of wind direction (but accounting for the fact that the wind blows from different directions with varying frequency). These results are plotted in Figure 9.

Interpretation of Figure 9 is aided by a description of the effects of wind of various magnitudes on people. The earliest quantitative description of wind effects was established by Sir Francis Beaufort in

1806 for use at sea and is still in use today. Several recent investigators have added to the knowledge of wind effects on pedestrians. These investigations along with suggested criteria for acceptance have been summarized by Penwarden and Wise (4) and Melbourne (5). The Beaufort scale (from ref. 4), based on mean velocity only, is reproduced as Table 4 including qualitative descriptions of wind effects. Table 4 suggests that mean wind speeds below 12 mph are of minor concern and that mean speeds above 24 mph are definitely inconvenient. Quantitative criteria for acceptance from reference (5) are superimposed as dashed lines on Figure 9. The peak gust curves shown in Figure 9 are the percent of time during which a short gust of the stated magnitude could occur (say about one of these gusts per hour). Implications of the data plotted in Figure 9 are presented in Section 5.2.

Because some pedestrian wind measuring positions are purposely chosen at sites where the smoke tests showed large velocities of small spacial extent, the general wind environment about the structure may be less severe than one might infer from a strict analysis of Table 2 and Figure 9.

4.3 Pressures

For each of the pressure taps examined at each wind direction, the data record is analyzed to obtain four separate pressure coefficients. The first is the mean pressure coefficient

$$C_{p_{mean}} = \frac{(p-p_\infty)_{mean}}{0.5\ \rho\ U_\infty^2}$$

where the symbols are defined in the List of Symbols. It represents the mean of the instantaneous pressure difference between the building pressure tap and the static pressure in the wind tunnel above the building model, nondimensionalized by the dynamic pressure

$$0.5\ \rho\ U_\infty^2$$

at the reference velocity position. This relationship produces a dimensionless coefficient which indicates that the mean pressure difference between building and ambient wind at a given point on the structure is some fraction less or some fraction greater than the undisturbed wind dynamic pressure near the upper edge of the boundary layer. Using the measured coefficient, prototype mean pressure values for any wind velocity may be calculated.

The magnitude of the fluctuating pressure is obtained by the rms pressure coefficient

$$C_{p_{rms}} = \frac{\left((p-p_\infty) - (p-p_\infty)_{mean}\right)_{rms}}{0.5\ \rho\ U_\infty^2}$$

in which the numerator is the root-mean-square of the instantaneous pressure difference about the mean.

If the pressure fluctuations followed a Gaussian probability distribution, no additional data would be required to predict the frequency with which any given pressure level would be observed. However, the pressure fluctuations do not, in general, follow a Gaussian probability distribution so that additional information is required to show the extreme values of pressure expected. The peak maximum and peak minimum pressure coefficients are used to determine these values:

$$C_{p_{max}} = \frac{(p-p_\infty)_{max}}{0.5\ \rho\ U_\infty^2}$$

$$C_{p_{min}} = \frac{(p-p_\infty)_{min}}{0.5\ \rho\ U_\infty^2}$$

the values of $p-p_\infty$ which were digitized at 250 samples per second for 16 seconds, representing about one hour of time in the full-scale, are examined individually by the computer to obtain the most positive and

most negative values during the 16-second period. These are converted to $C_{p_{max}}$ and $C_{p_{min}}$ by nondimensionalizing with the free stream dynamic pressure.

The four pressure coefficients are calculated by the on-line data acquisition system computer and tabulated along with the approach wind azimuth in degrees from true north. The list of coefficients is included as Appendices A-F. The pressure tap code numbers used in the appendices are explained in Figure 3.

To determine the largest peak loads acting at any point on the structure for cladding design purposes, the pressure coefficients for all wind directions were searched to obtain, at each pressure tap, the largest peak positive and peak negative pressure coefficients. Table 6 lists the larger values and associated wind directions. Included in Section 5.3 is an analysis of the coefficients of Table 6 including the maximum values obtained and where they occurred on the building.

The pressure coefficients of Table 6 can be converted to full-scale loads by multiplication by a suitable reference pressure selected for the field site. This reference pressure is represented in the equations for pressure coefficients by the $0.5\ \rho\ U_\infty^2$ denominator. This value is the dynamic pressure associated with an hourly mean wind at the reference velocity measurement position at the edge of the boundary layer. In general, the method of arriving at a design reference pressure for a particular site involves selection of a design wind velocity, translation of the velocity to an hourly mean wind at the reference velocity location and conversion to a reference pressure. Selection of the design velocity can be made from statistical analysis of extreme wind data or selected from wind maps contained in the proposed wind loading

code ANSI A58.1 of the American National Standards Institute (6). The calculation of reference pressure for this study is shown in Table 5. The factor used in Table 5 to reduce gust winds to hourly mean winds was obtained from reference (7).

The reference pressure associated with the design hourly mean velocity at the reference velocity location can be used directly with the peak-pressure coefficients to obtain peak local design wind loads for cladding design. Local, instantaneous peak loads on the full-scale building suitable for cladding design were computed by multiplying the reference pressure of Table 5 by the peak coefficients of Table 6 and are listed as peak pressures in that table. The maximum psf loads given at each tap location are the largest peak positive and peak negative values found in the tests. For ease in visualizing the loads on the structure, contours of equal peak pressures for cladding load shown in Table 6 have been plotted on developed elevation views of the structure, Figure 10. If a data point which is taken in the basic model configuration is retaken in a resolution configuration, the data are averaged in preparing Figure 10. For control of water infiltration from outsite to inside, the largest positive (inward acting) pressure at each tap location is tabulated in Table 6.

For glass design pressures, a glass load factor is used to account for the different duration between measured peak pressures and the one minute loading commonly used in glass design charts. The design pressure used for glass is normally less than the peak pressures used for cladding design because of the static fatigue property of glass which can withstand higher pressures for short duration loads than for long duration loads. Recent research (8) indicates that the period of appli-

cation of the peak pressures reported herein is about 5-10 seconds or less. If a glass design is based on these peak-pressure values, then a glass strength associated with this duration load should be used. Because glass design charts are normally based on some alternate load duration--usually one minute--then some reduction in peak loads should be made. An estimate of a load reduction factor can be obtained from an empirical relation of glass strength as a function of load duration. Current glass selection charts showing glass strength as a function of load duration (9) and older references (10) indicate the following load reduction factors:

	ref.(9)	ref.(10)
annealed float	0.80	0.81
heat strengthened	0.94	
tempered	0.97	0.98

Loadings appropriate for glass design can be computed by multiplying the peak-pressure loads of Table 6 by these load factors.

4.4 Forces and Moments

Force coefficients in the horizontal X and Y directions and moment coefficients about the X, Y, and Z axes with the origin at ground level at the base of the building with Z axis vertical may be computed for all wind directions tested by integration of mean pressures on the building. Overall forces and moments acting on the full-scale building due to wind loading which are useful in designing the structural framing of the proposed building may be obtained from use of these coefficients.

Force coefficients were computed for each floor for each wind direction using the equations shown below.

$$CF_X = \frac{F_X}{A_R \; 0.5 \; \rho \; U_\infty^2} \qquad CF_Y = \frac{F_Y}{A_R \; 0.5 \; \rho \; U_\infty^2}$$

Terms and symbols used in the equations are defined in the List of Symbols and the axes are defined for the building in Figure 12. Force coefficients CF_X and CF_Y were computed for the horizontal forces acting along the X and Y axes using the mean pressure coefficient at each pressure tap. A_R represents a constant reference area for nondimensionalization of the forces and moments.

The total forces acting on the full-scale building for each floor and wind direction were computed by multiplying the above coefficients by the appropriate full-scale reference area, by the reference pressure of Table 5, and by a gust load factor selected for an appropriate wind gust duration. The gust load factor, shown in Table 5, was selected to increase the loads from an hourly mean load to that of a gust whose duration would be sufficient for its effect to be fully felt by the structure. A table of gust load factors for various gust durations is incorporated in Table 5 so that force and moment data of Table 7 may be adjusted to a different load duration if desired.

The forces obtained at each floor were used to obtain load, shear, and moment diagrams for the building for each wind direction. The shear diagram, in kips, was obtained by algebraic sum of all forces in each coordinate direction acting above the floor of interest. The load diagram, in psf, was obtained by dividing the shear values by their contributing areas (listed in Table 7). The moment diagram, in 1000 ft-kips, was obtained by integration of the shear values so that the moment due to forces acting above the floor level of interest was calculated. The sign of the moment was established by the right-hand rule about an X', Y' axis through the floor of interest. Moments about the Z axis

were calculated by considering the displacement of forces in the X and Y directions from the Z axis shown in Figure 12. Eccentricities were computed such that the product of the Y force and X eccentricity minus the product of the X force and Y eccentricity equaled the Z moment. Load, shear, and moment diagrams are shown in Figure 13 for several wind directions.

5. DISCUSSION

5.1 Flow Visualization

Flow patterns identified with smoke showed that largest pressures would most likely be found near corners of the tower. These pressures are due to flow separation phenomena. Flow separation occurs when the wind is unable to turn a sharp corner on the building and separates from the surface. Elevated negative (outward acting) pressures are often found under the separated flow near the point of separation. High velocity and large curvature in the separated flow contribute to the local elevated pressures. Flow visualization showed high velocity flow separation at the building corners at several elevations along the corners. Elevated pressures may thus be found anywhere along the corners.

The tower had the effect of deflecting higher velocity winds from upper elevations on the tower down to ground level. These high winds impinged on the lower balconies and the garage connecting links of the LPC Mandalay Towers (LPCMT) for some wind directions. For this reason, wind pressures on the lower balconies and the garage connecting links may be higher than those measured at roof level of the structure. For some wind directions the tower was shielded by the adjacent tower and should have low wind loads. The adjacent tower deflected accelerated winds onto the tower under consideration, a situation which can increase local wind loads near corners.

Winds in pedestrian areas at ground level were largest near corners of the two towers. These winds were due to the downward deflection of higher velocity winds from near the tops of the towers. Winds on pedestrian walks at the corners of either tower (Tower I or Tower II)

appeared high for some wind directions due to the deflected winds explained previously. The wind velocity in pedestrian areas about the base of the towers appeared to be fairly high near all corners of the towers--particularly at the corner adjacent to the other tower. At location 7 (see Figure 4), a high velocity was observed for a range of northeasterly through southeasterly and southwesterly through northeasterly wind directions due to wind flow channeled between the two towers.

5.2 Pedestrian Winds

Figure 4a shows the 28 locations selected for investigation of pedestrian wind comfort for the twin-tower configuration. Figure 4b shows the 20 locations selected for the single-tower configuration. Location 26 was chosen as a comparison location whose wind should be only slightly modified by the LPCMT. Location 5 was positioned under building overhangs.

Table 2 and Figure 8 show that the largest mean velocities were measured at locations 2, 7, 8 and 19 with values of 70 to 84 percent of U_∞, the velocity at gradient height of 1200 ft, for the twin-tower configuration. For the single-tower configuration, the largest mean velocities occurred at locations 2, 6, 7, 10 and 19 with values of 70 to 89 percent of U_∞. These velocities can be compared to 40 to 45 percent which might be found in an open-country environment. The largest gust velocities, represented by the mean plus 3 rms as discussed in Section 4.2, were measured at locations 1, 2 and 10 with values of 121 to 133 percent of U_∞. Values above about 120 percent are rather large in comparison with values of 80 to 90 percent in an open-country environment.

Velocity data of Table 2 integrated with local wind data listed in Table 3 are shown in Figure 9. Based on the data of this figure, mean

winds at pedestrian locations 2, 7, 8, 10, 18, 19, 21, 22, 24 and 26 exceed the published acceptability limit for the twin-tower configuration. Gust winds for the above locations were within the acceptable level except locations 7 and 10 which exceed the acceptability limit approximately 7 percent of the time. Because the mean wind acceptance criteria for LPCMT were calculated for an urban location with turbulence larger than that found at LPCMT (the Dallas area is known as a windy environment, it may be that the actual acceptability criteria are somewhat higher than those used in this report), the mean winds at all locations except 7 and 10 are probably acceptable as is. Locations 7 and 10 will, however, not be comfortable. Location 7 was expected to be unacceptable from flow visualization since a channeled flow was formed by the presence of the two towers. Gust winds at location 10 were high because of concentration of winds deflected by Tower 1.

Mean winds at pedestrian locations 1, 2, 4, 6, 7, 10, 16 and 17 exceed the published acceptability limit for the single-tower configuration. Gust winds for these locations were within the acceptable level except locations 2, 6, 7 and 10 which exceed the acceptability limit approximately 3 to 10 percent of the time. For the same reason mentioned before, the mean winds at most locations except 7 and 10 are probably acceptable but not always comfortable for walking.

Location 26 is an existing location which should be reasonably undisturbed by the presence of LPCMT. It appeared that location 26 was as windy as other locations in the new construction geometry. Therefore, LPCMT will increase winds only at some corners at the base of the towers such as locations 7, 10 and 19. All other pedestrian locations,

such as east and west plazas, will have winds similar to the nearby existing environment.

5.3 Wind Loads

Table 6 shows the largest peak pressure coefficients and corresponding loads measured on the building for each pressure tap location. Data configurations are identified in Table 1. Data are identified by configuration in Table 6a and represent peak pressure and corresponding azimuth angle obtained at each pressure tap location. Table 6b tabulates the greatest pressure magnitudes and associated pressure tap locations for different configurations. Pressure coefficient data for all configurations, taps, and wind directions are contained in the appendices. Only the highest pressure at each tap for selected configurations are presented in Table 6.

The largest pressures obtained on Tower I were -51 to -65 psf on the roof and south side of the building for the twin-tower configuration. The largest cladding pressures on Tower I alone ranged up to -65 psf and were located near the southwest corner of the tower. The greatest pressure magnitudes on Tower I were little affected by the presence of Tower II and its linked structures. The largest pressures obtained on Tower II were -51 to -64 psf on the roof and west side of the building for the twin-tower configuration. The largest pressures on Tower II cladding ranged up to -64 psf and were located near the southeast corner of the tower.

Figure 10 shows the distribution of peak negative and peak positive pressures over the surface of Tower I and II. Most of the area of the two towers had peak negative pressures less than -40 psf with higher

pressures restricted to limited areas. Typical peak positive pressures were less than +30 psf with largest values extending up to 40 psf.

The wind pressures shown in Table 6 and Figure 10 represent external pressures. Internal pressures on buildings may be controlled by the air handling system in combination with infiltration through the curtainwall and any openings in the curtainwall associated with operable doors or windows which are left open during a wind storm. Internal pressures for this complex can reasonably be assumed to be controlled primarily by infiltration and the air handling system. Values of ±5 psf are reasonable for internal pressures. Figure 11 shows elevations of both towers blocked into rectangular regions with internal pressures included.

Figure 13 shows frame pressure, shear and moment distributions plotted from Table 7 for the largest base shears in the x and y coordinate directions on the new tower. The coordinate system is shown in Figure 12. For wind direction 20 degrees where the x shear reached its maximum, the y shear remained at a magnitude approximately 60 percent of the x shear for Tower I under the twin-tower configuration. For Tower II of the twin-tower configuration the result remained quite similar except the wind direction changed to 90 degrees. For Tower I of the single-tower configuration, x shear reached its maximum at wind direction 10 degrees and the y shear became rather insignificant with a magnitude of less than 10 percent of the x shear. As shown on the summary page of Table 7, the torsional moments were moderate but tended to be largest simultaneously with large base shears.

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9. PPG Glass Thickness Recommendations to Meet Architects' Specified 1-Minute Wind Load, Pittsburgh Plate Glass Industries, April 1979.

10. Shand, E. B., "Glass Engineering Handbook," Second Edition, McGraw-Hill, New York, 1958, p. 51.

FIGURES

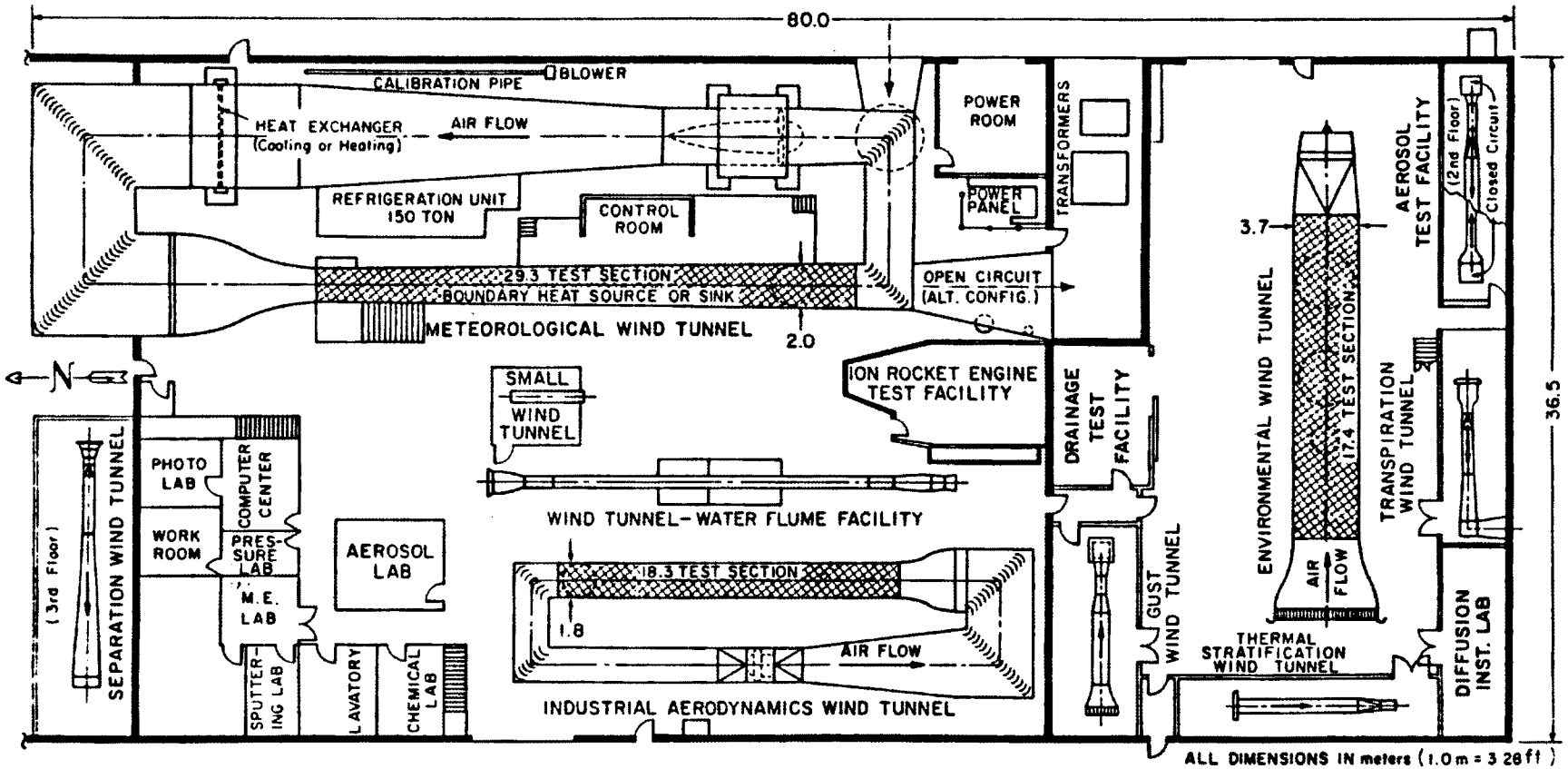
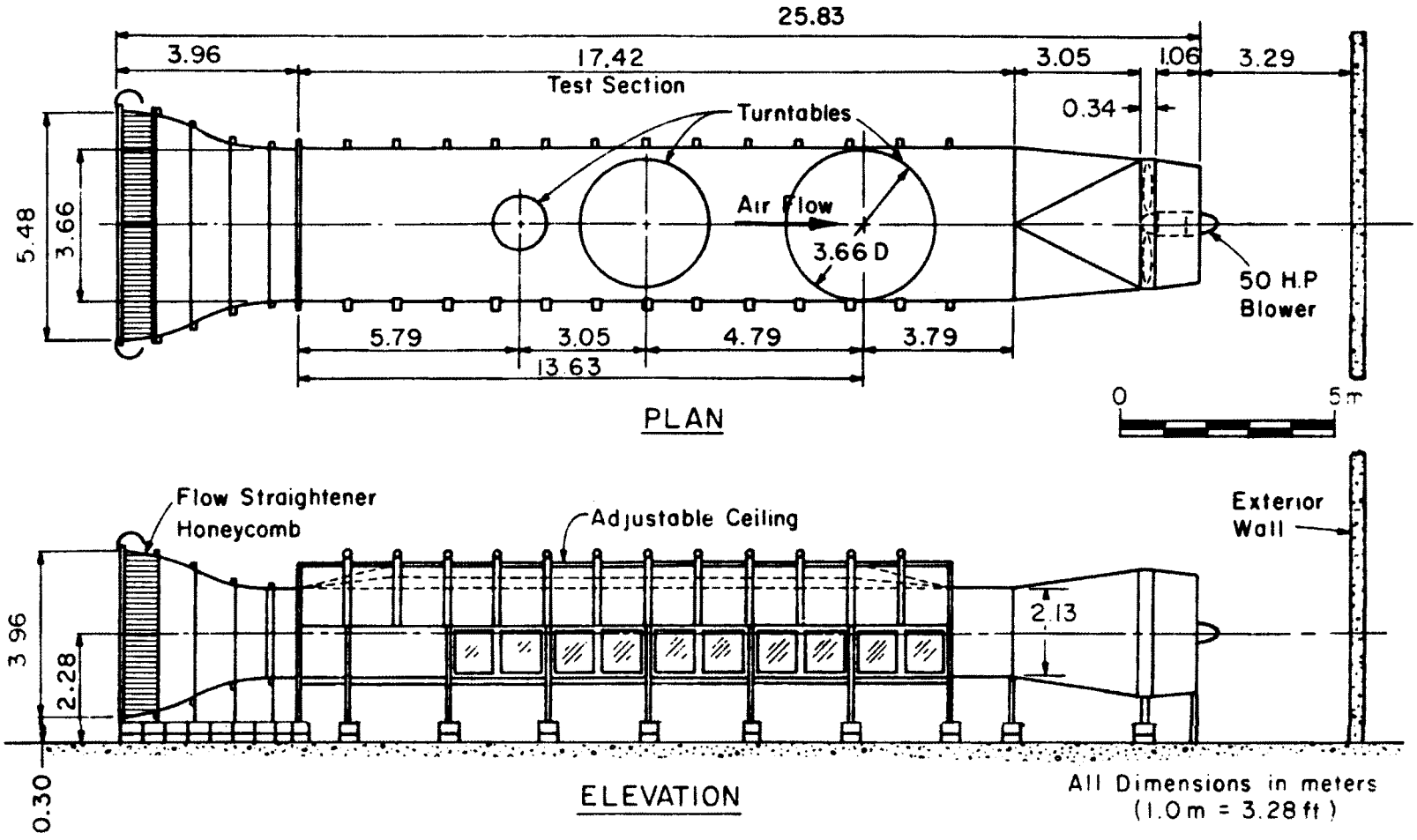
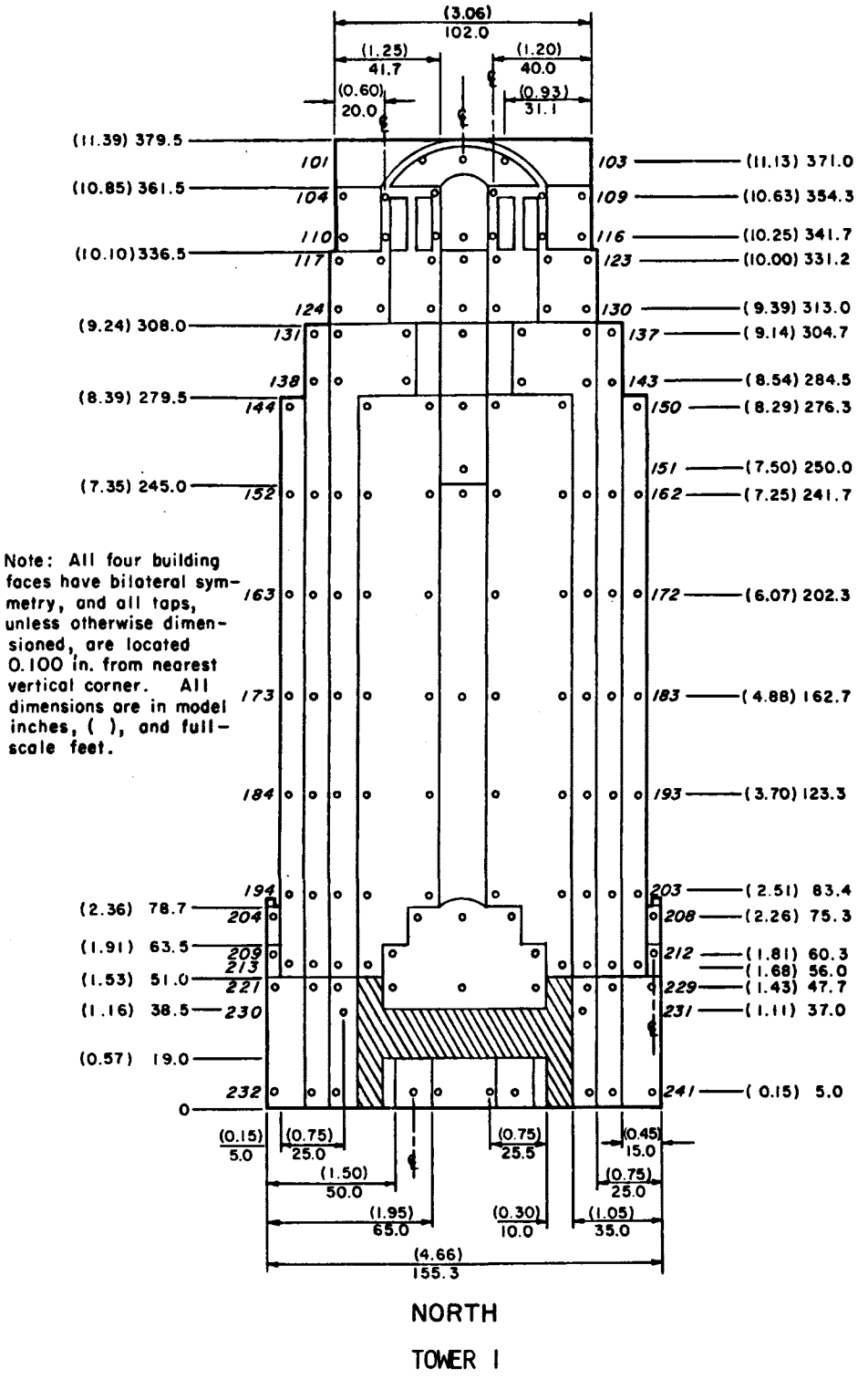


Figure 1. Fluid Dynamics and Diffusion Laboratory, Colorado State University



Environmental Wind Tunnel, Fluid Dynamics and Diffusion Laboratory, Colorado State University

Figure 2. Wind Tunnel Configuration



Note: All four building faces have bilateral symmetry, and all taps, unless otherwise dimensioned, are located 0.100 in. from nearest vertical corner. All dimensions are in model inches, ( ), and full-scale feet.

Figure 3a. Pressure Tap Locations

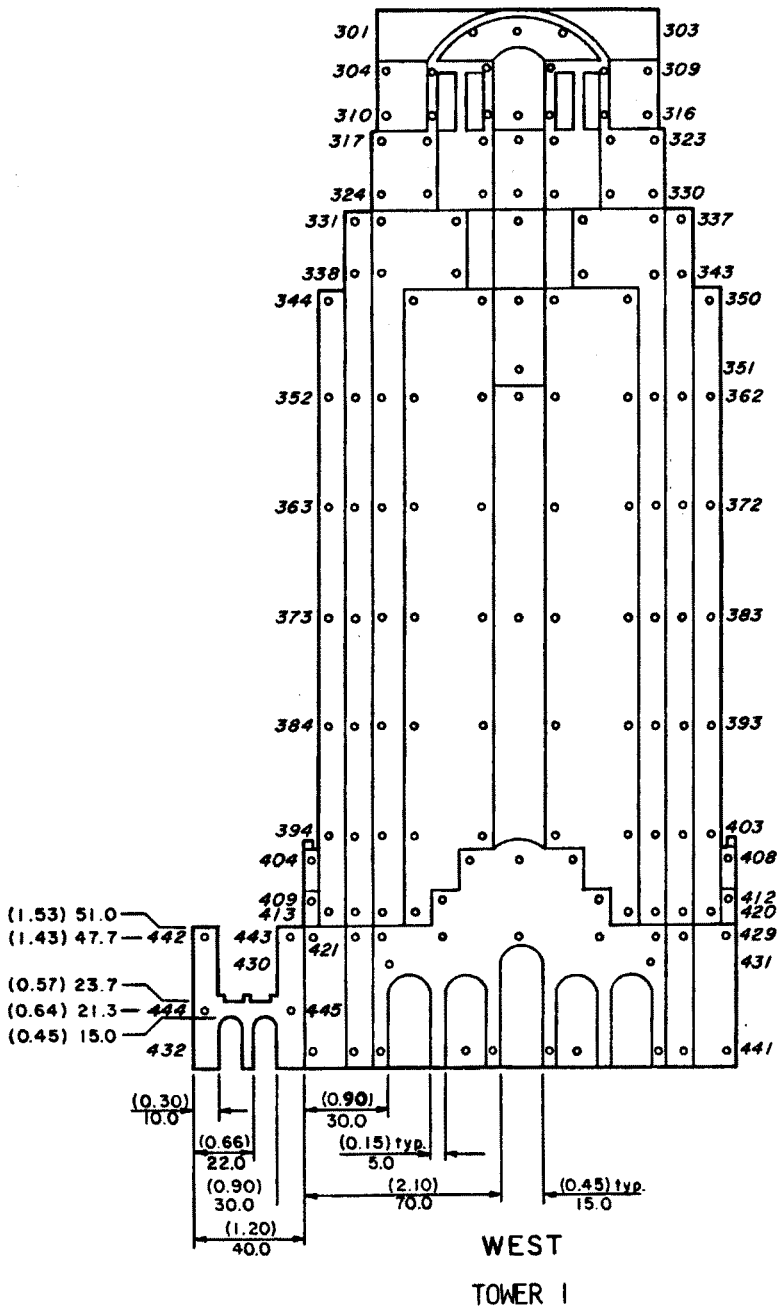


Figure 3b. Pressure Tap Locations

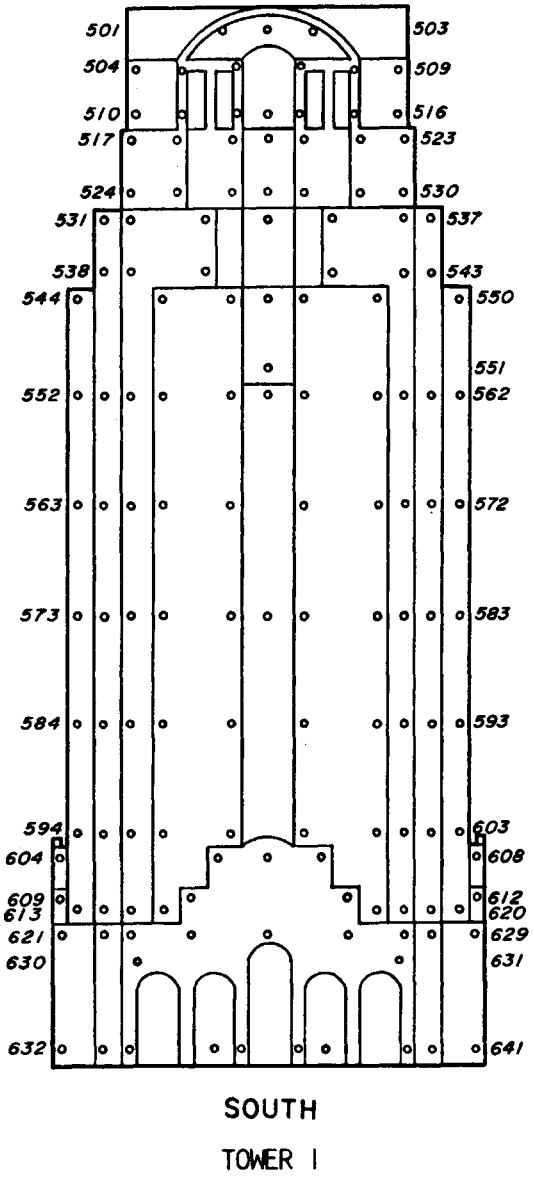


Figure 3c. Pressure Tap Locations

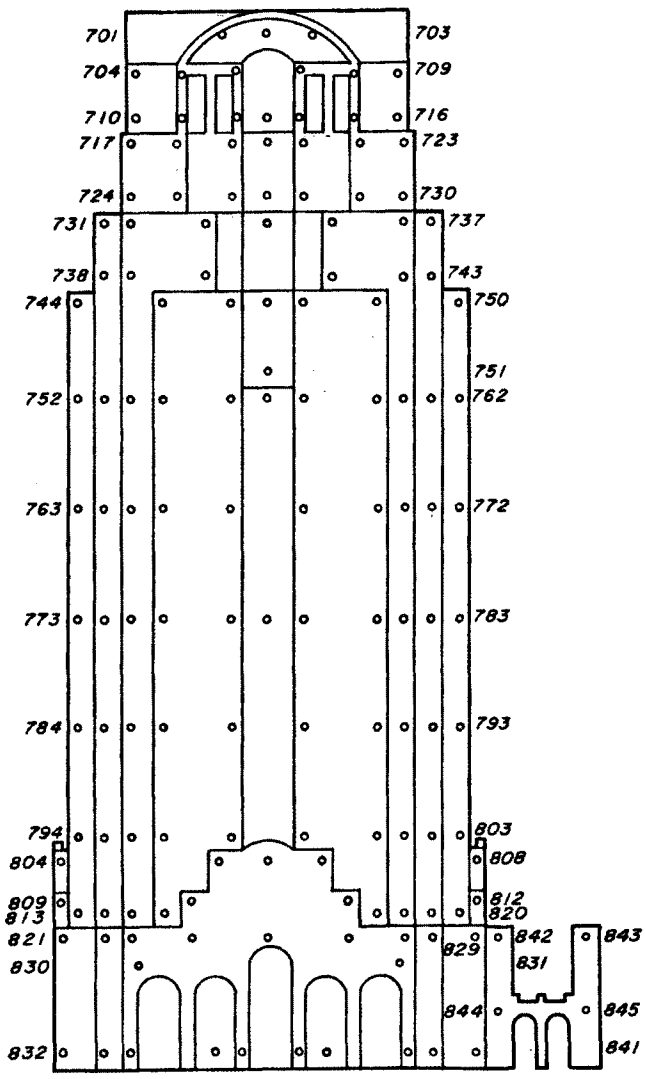
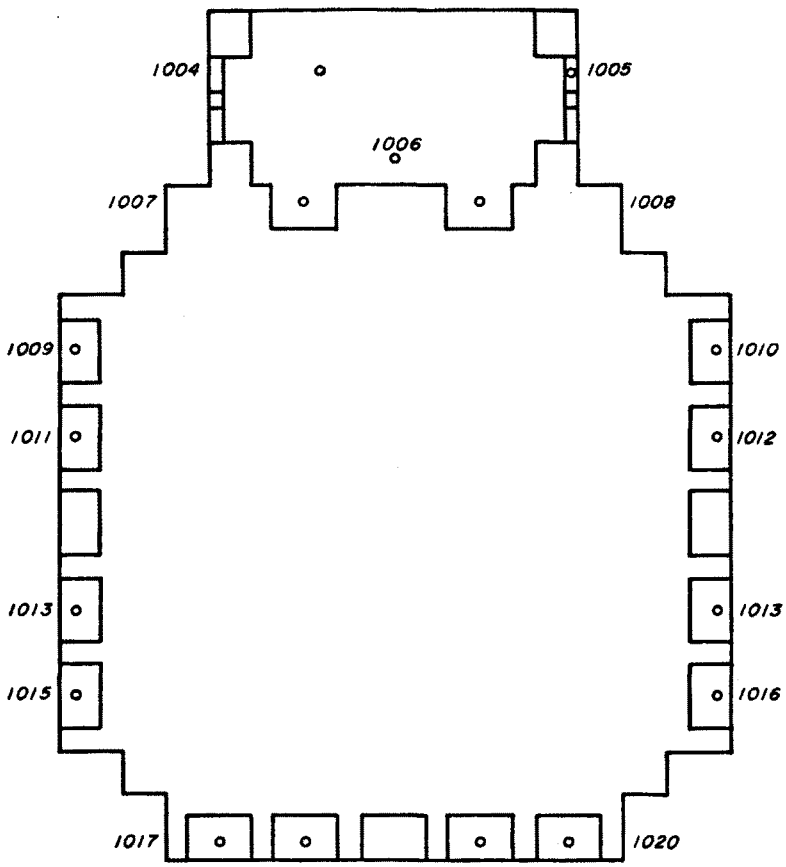


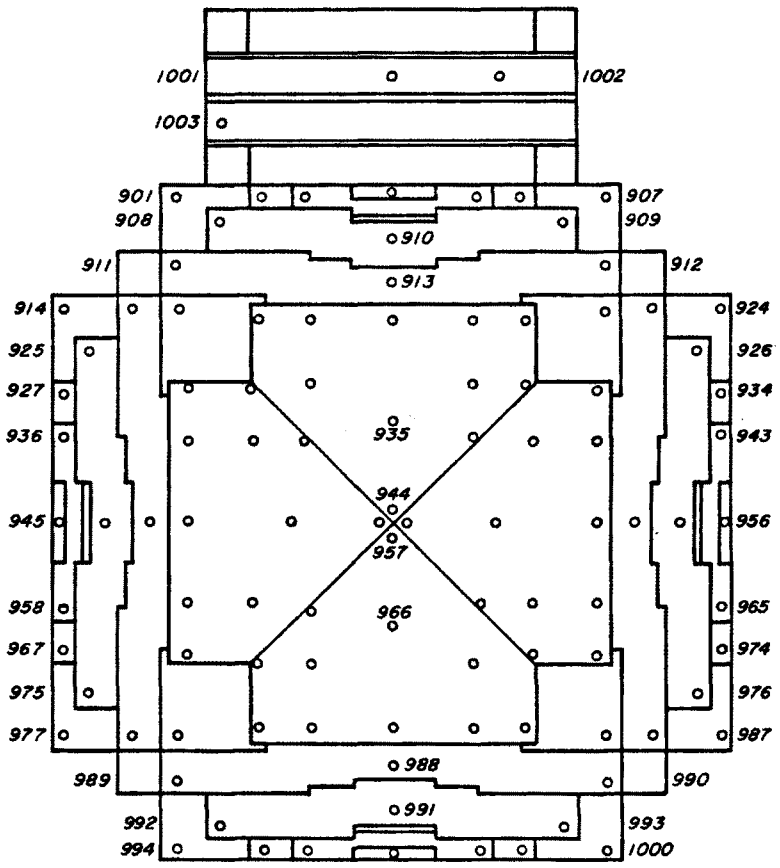
Figure 3d. Pressure Tap Locations



TOWER I

SOFFIT

Figure 3e. Pressure Tap Locations



TOWER I

ROOF

Figure 3f. Pressure Tap Locations

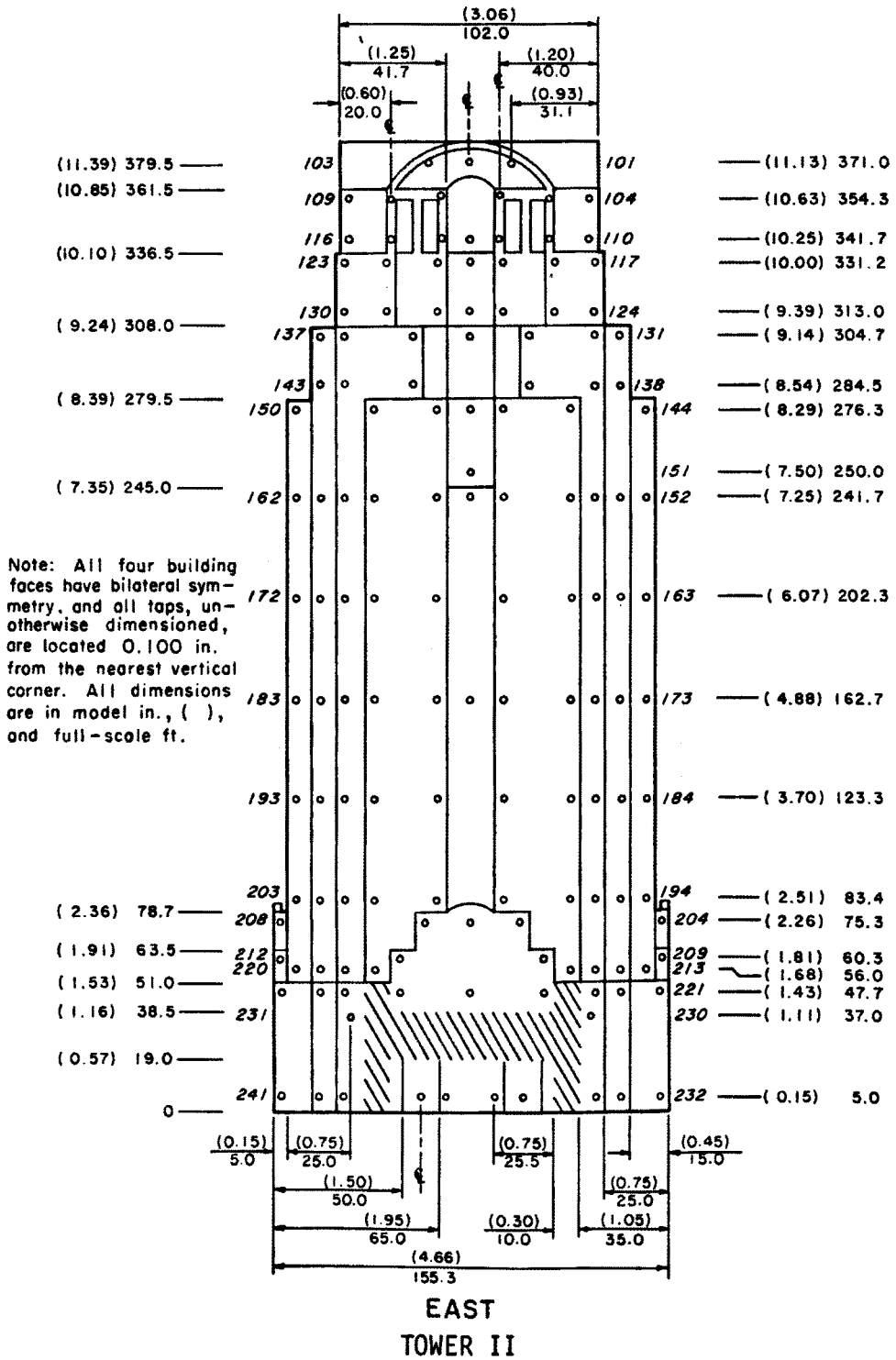
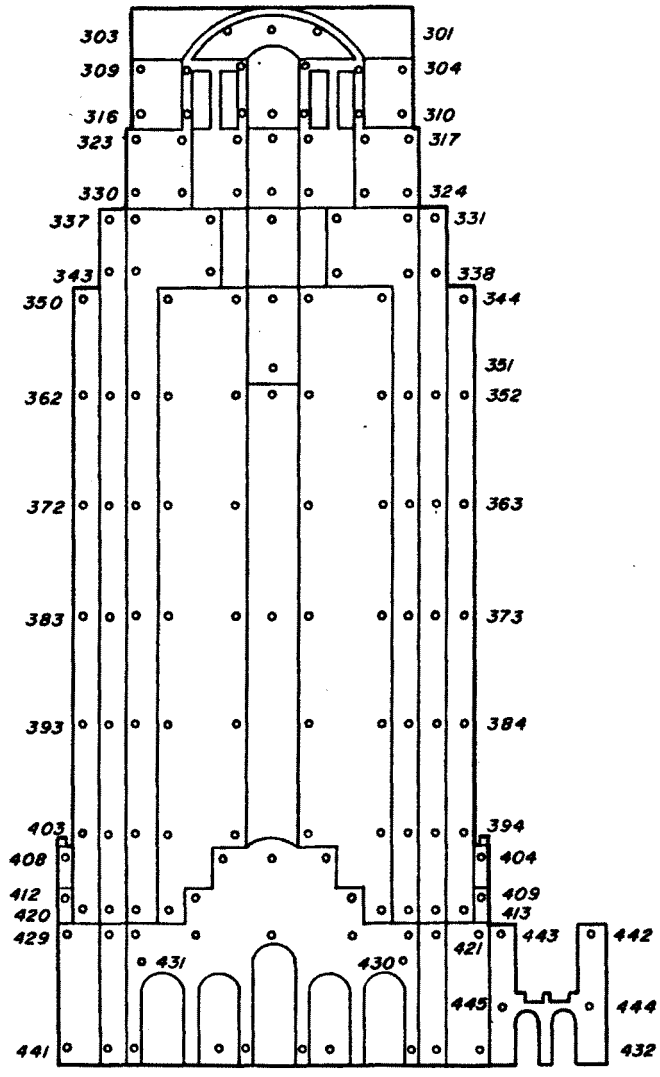


Figure 3g. Pressure Tap Locations



SOUTH
TOWER II

Figure 3h. Pressure Tap Locations

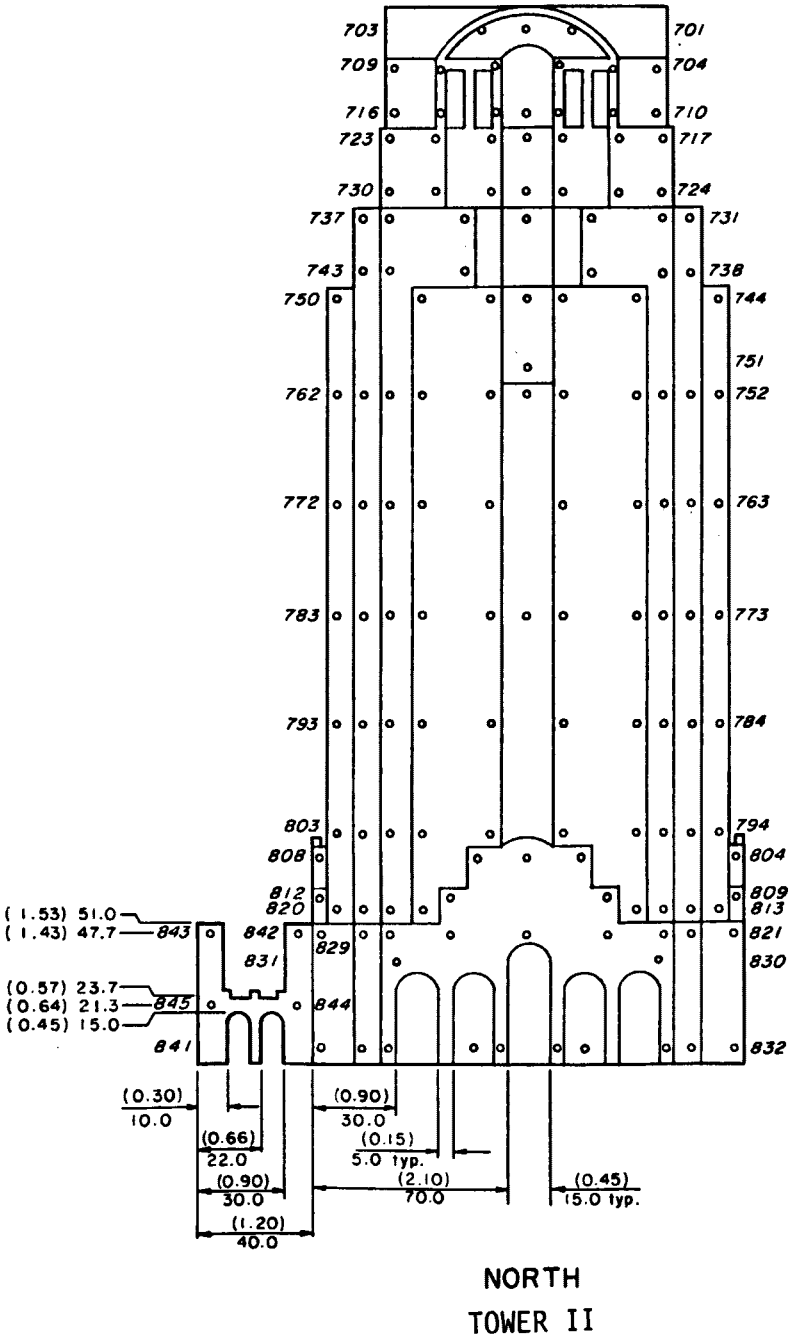
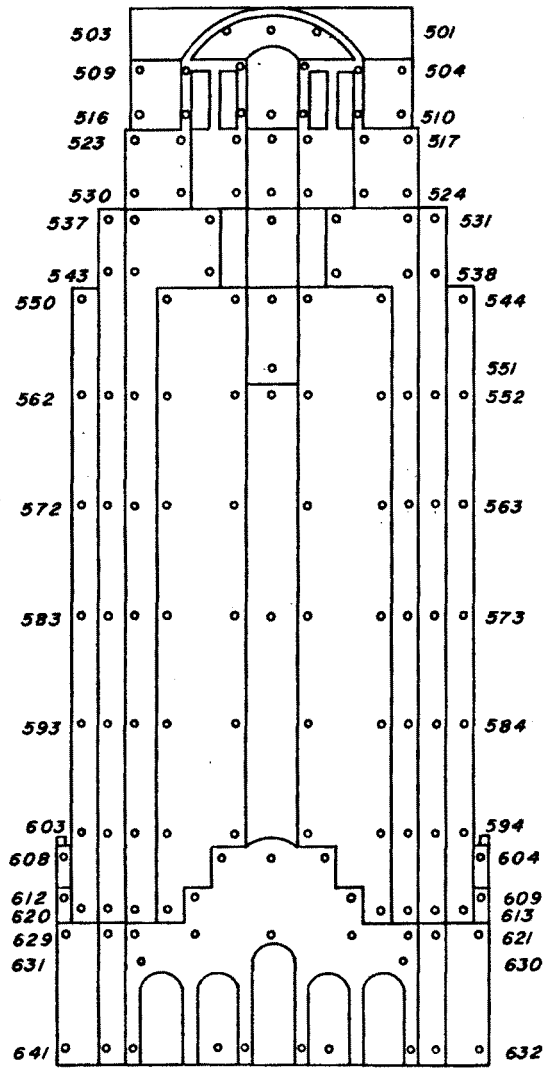
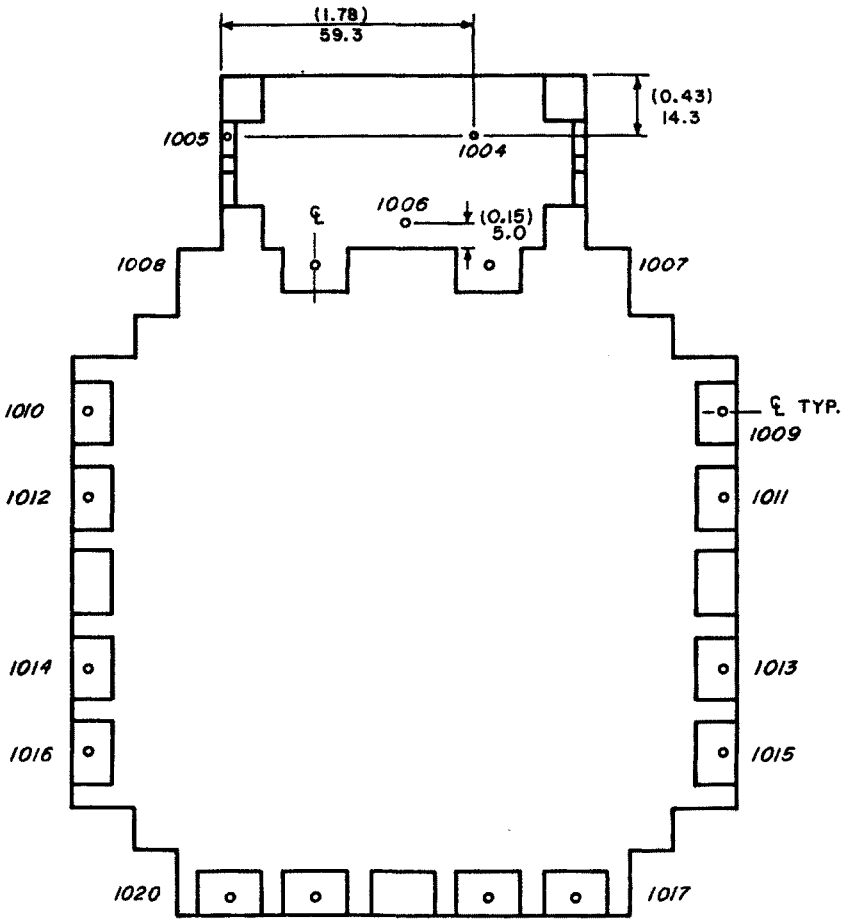


Figure 3i. Pressure Tap Locations



WEST
TOWER II

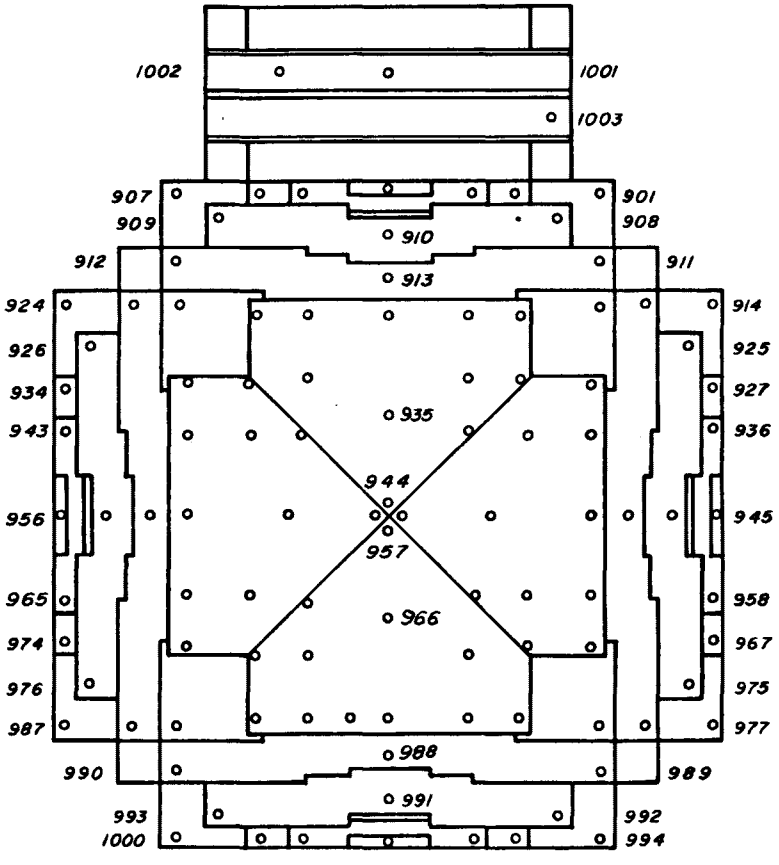
Figure 3j. Pressure Tap Locations



SOFFIT

TOWER II

Figure 3k. Pressure Tap Locations



ROOF

TOWER II

Figure 31. Pressure Tap Locations

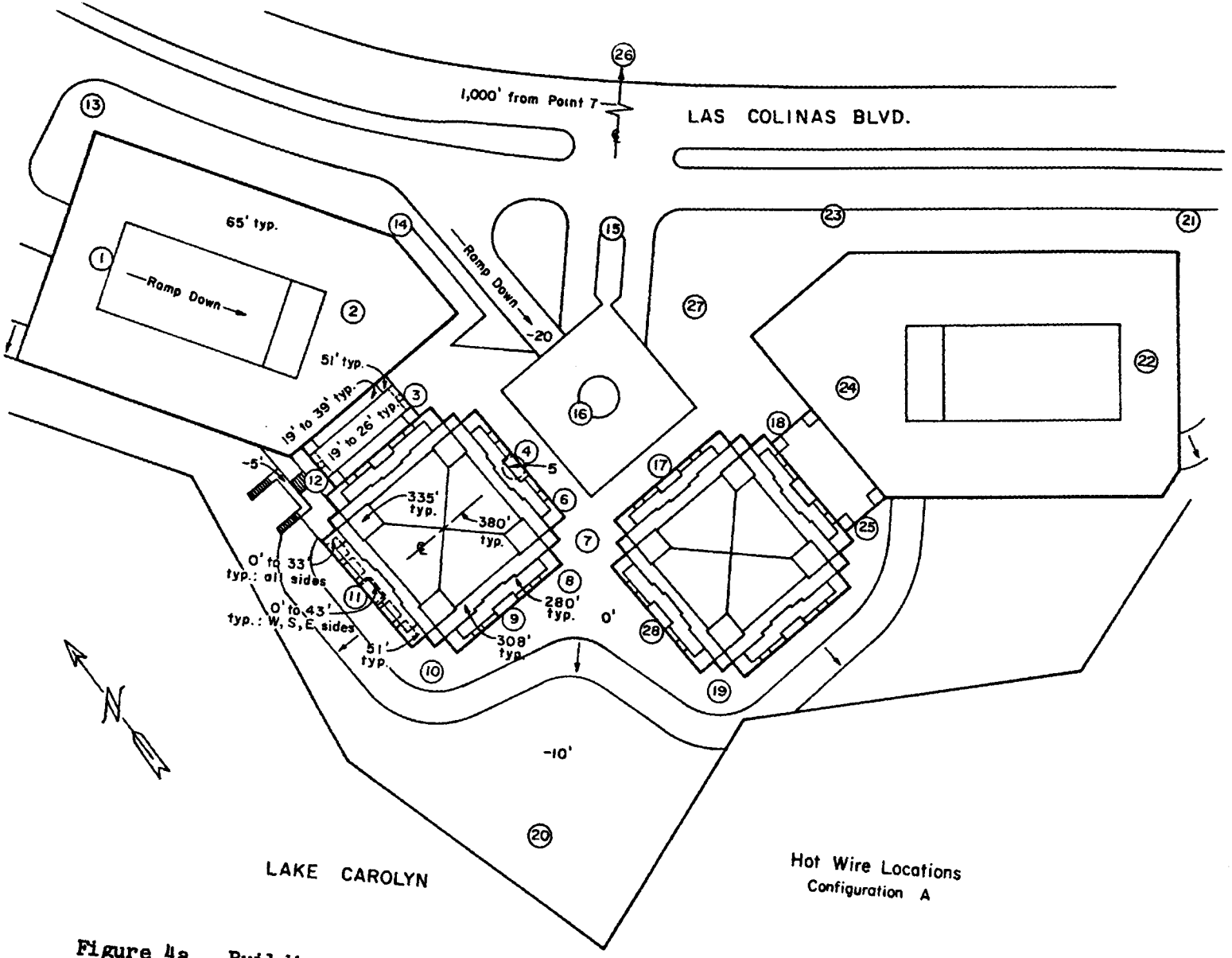


Figure 4a. Building Location and Pedestrian Wind Velocity Measuring Positions

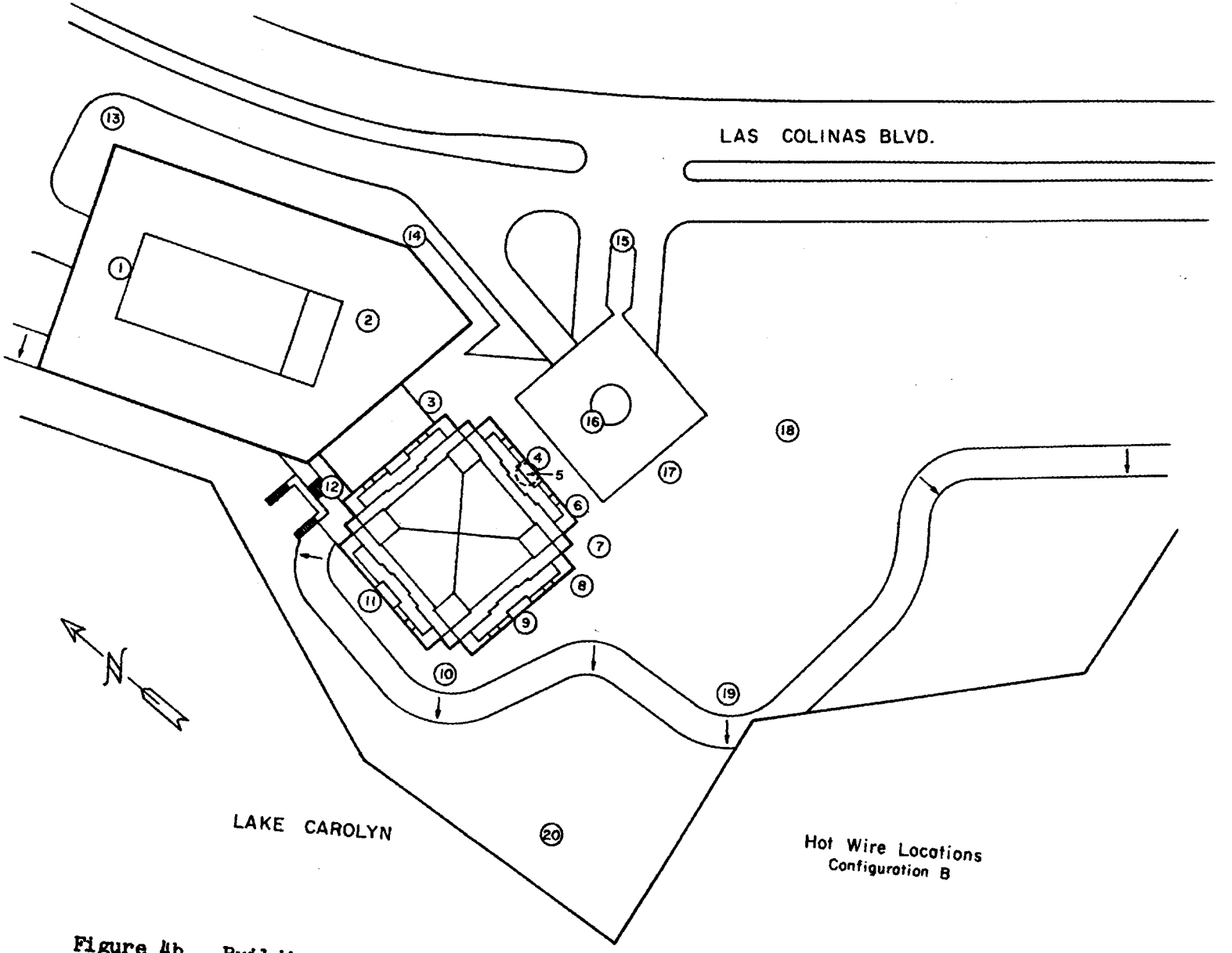
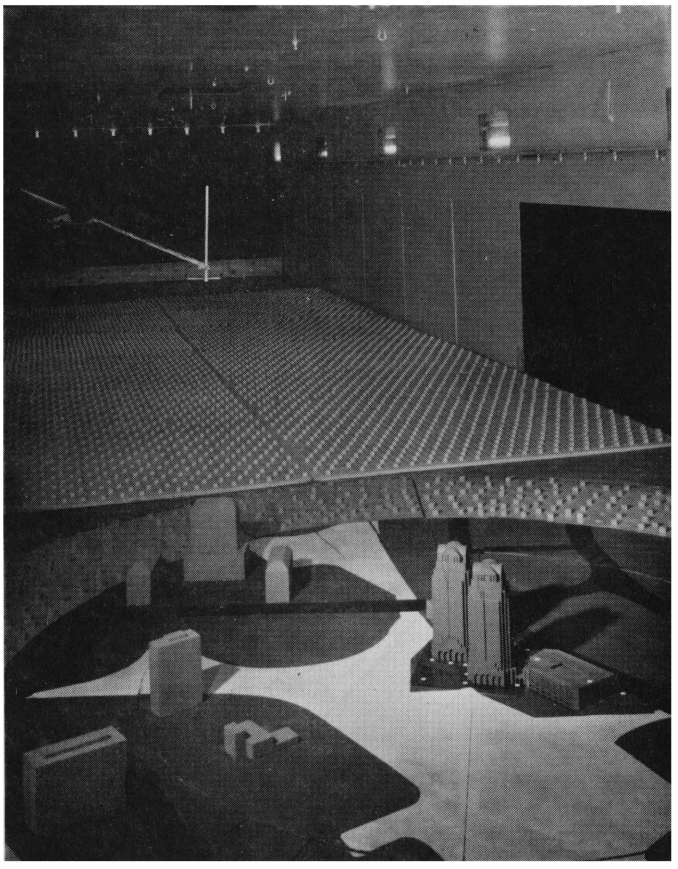


Figure 4b. Building Location and Pedestrian Wind Velocity Measuring Positions



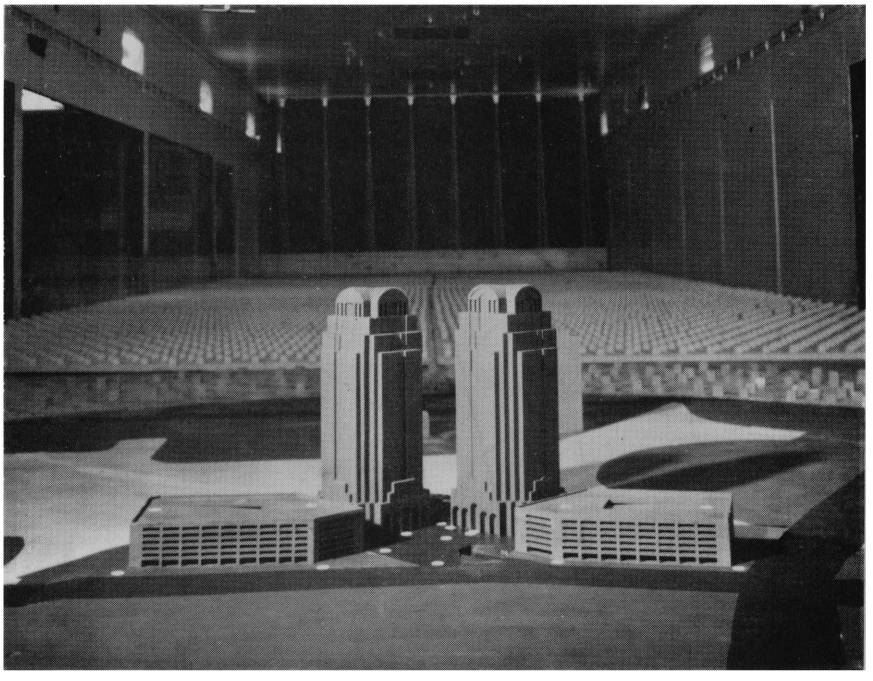


Figure 5a. Completed Model in Wind Tunnel

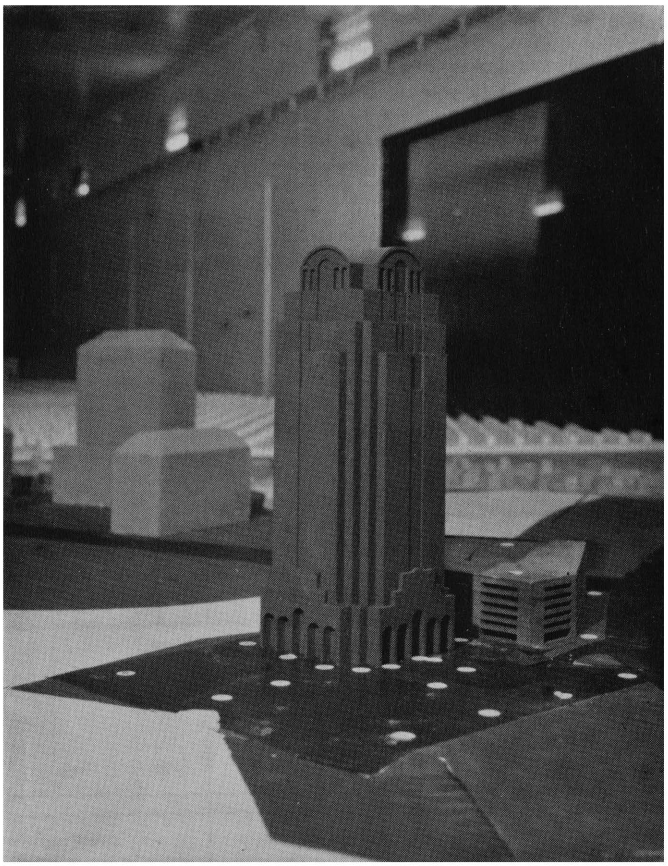


Figure 5b. Completed Model in Wind Tunnel

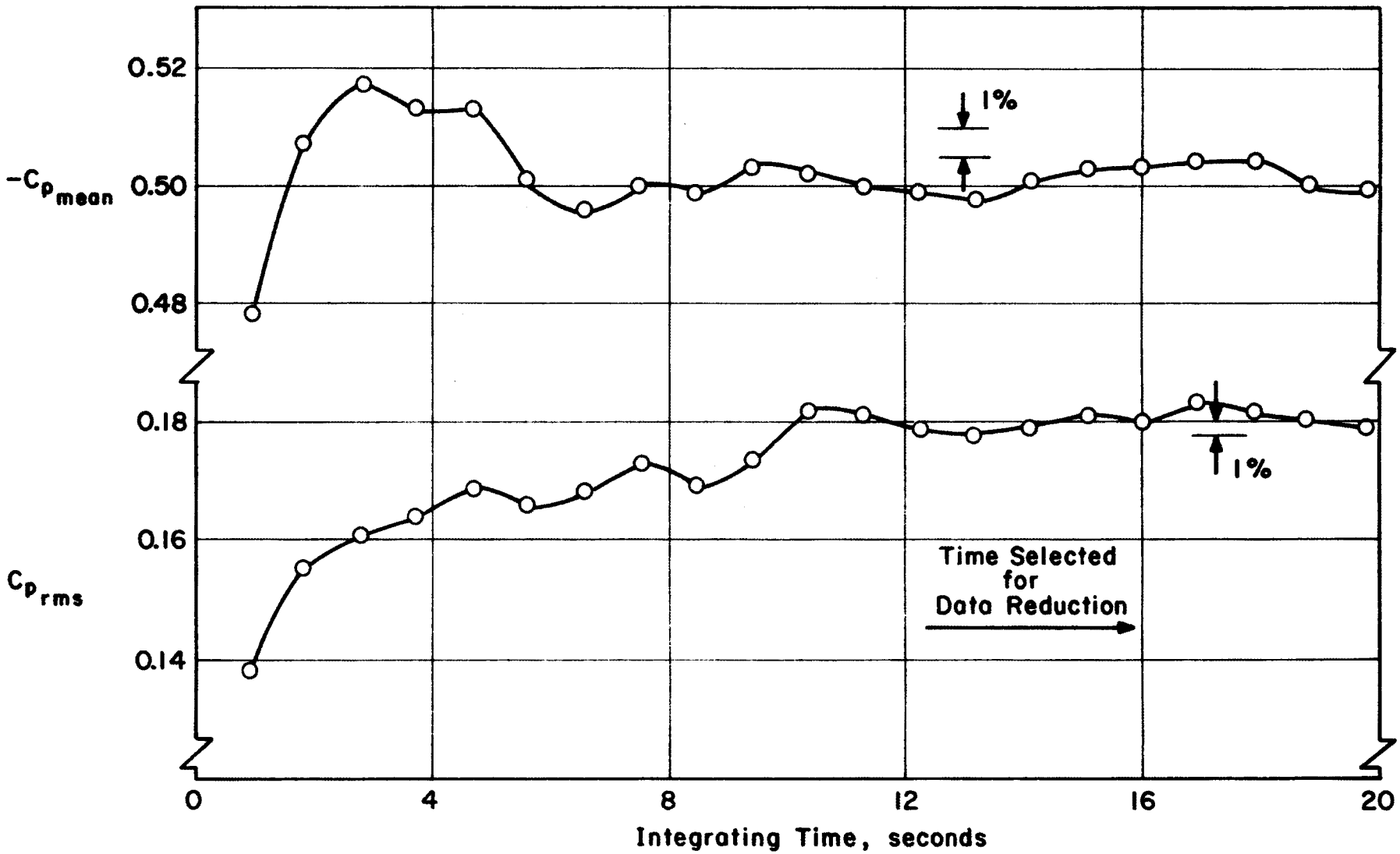


Figure 6. Data Sampling Time Verification

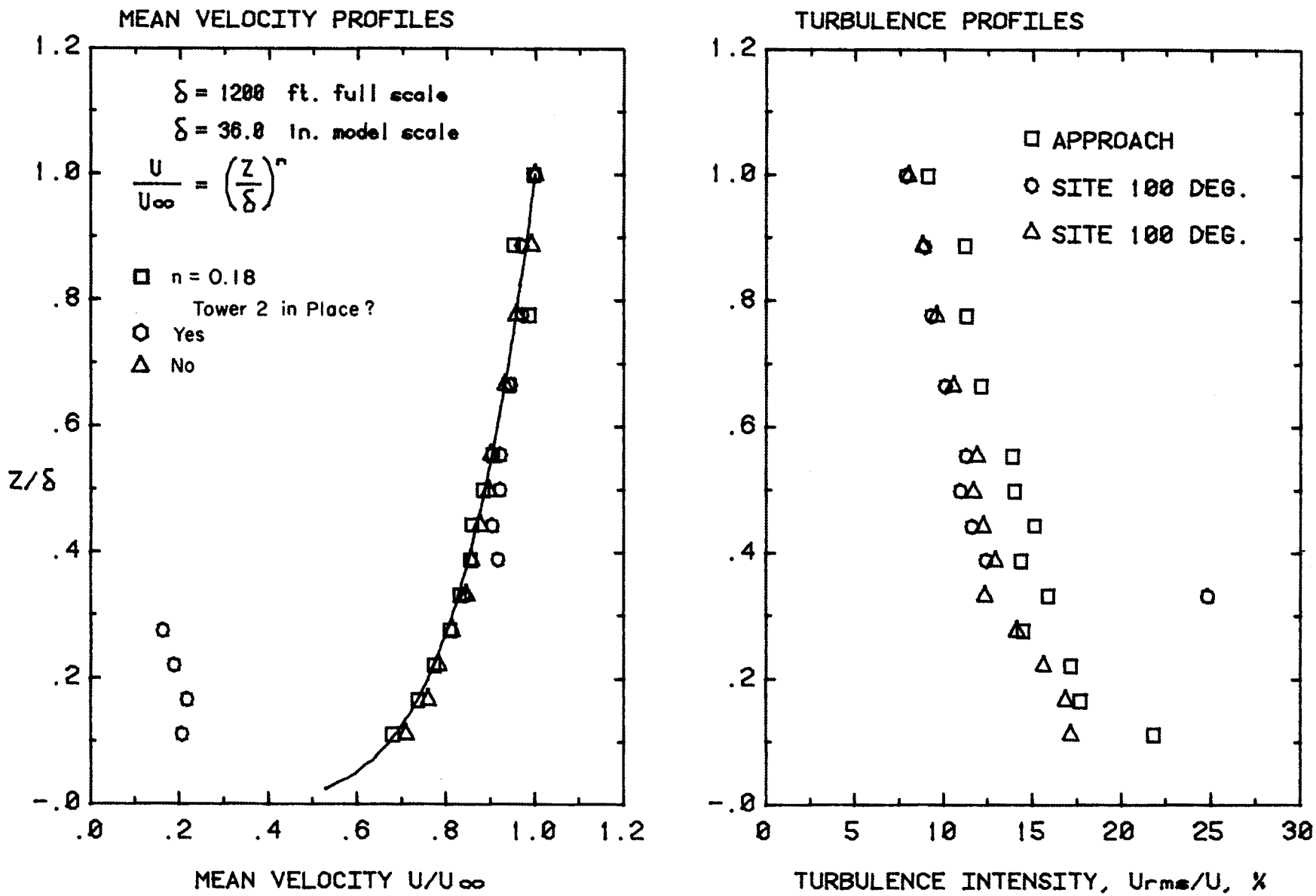


Figure 7. Mean Velocity and Turbulence Profiles Approaching the Model.

TOWER II IN PLACE

CONFIGURATION G

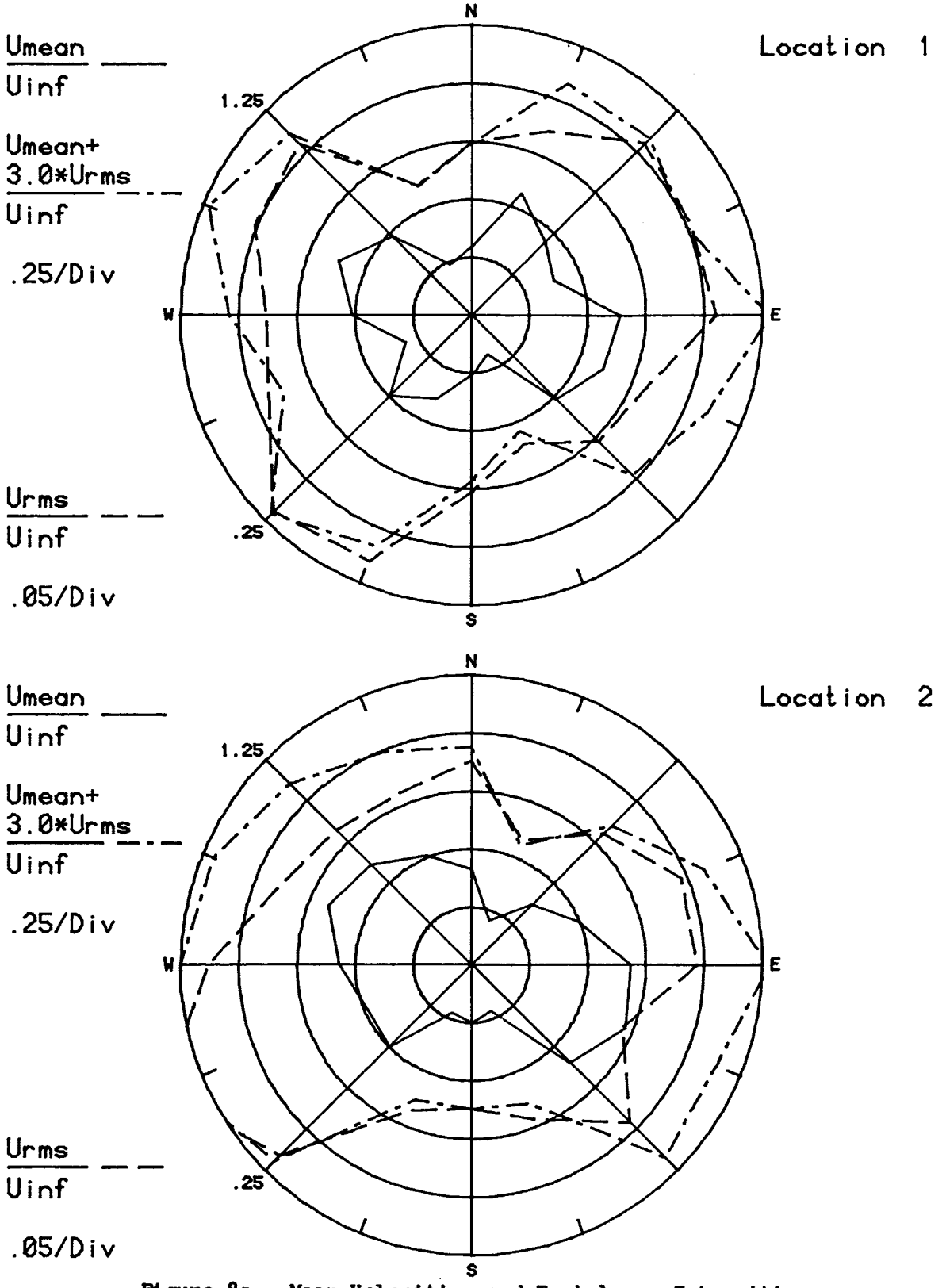
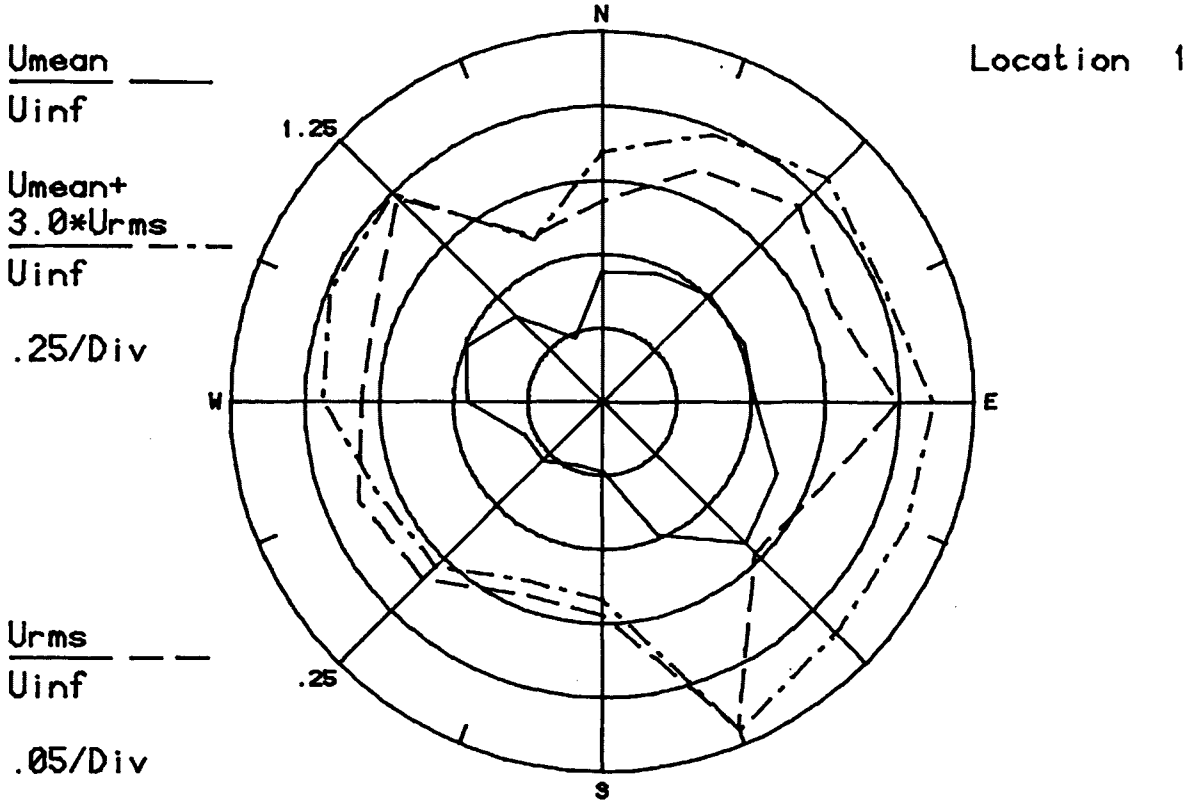


Figure 8a. Mean Velocities and Turbulence Intensities at Pedestrian Locations 1 and 2

TOWER II OUT

CONFIGURATION H



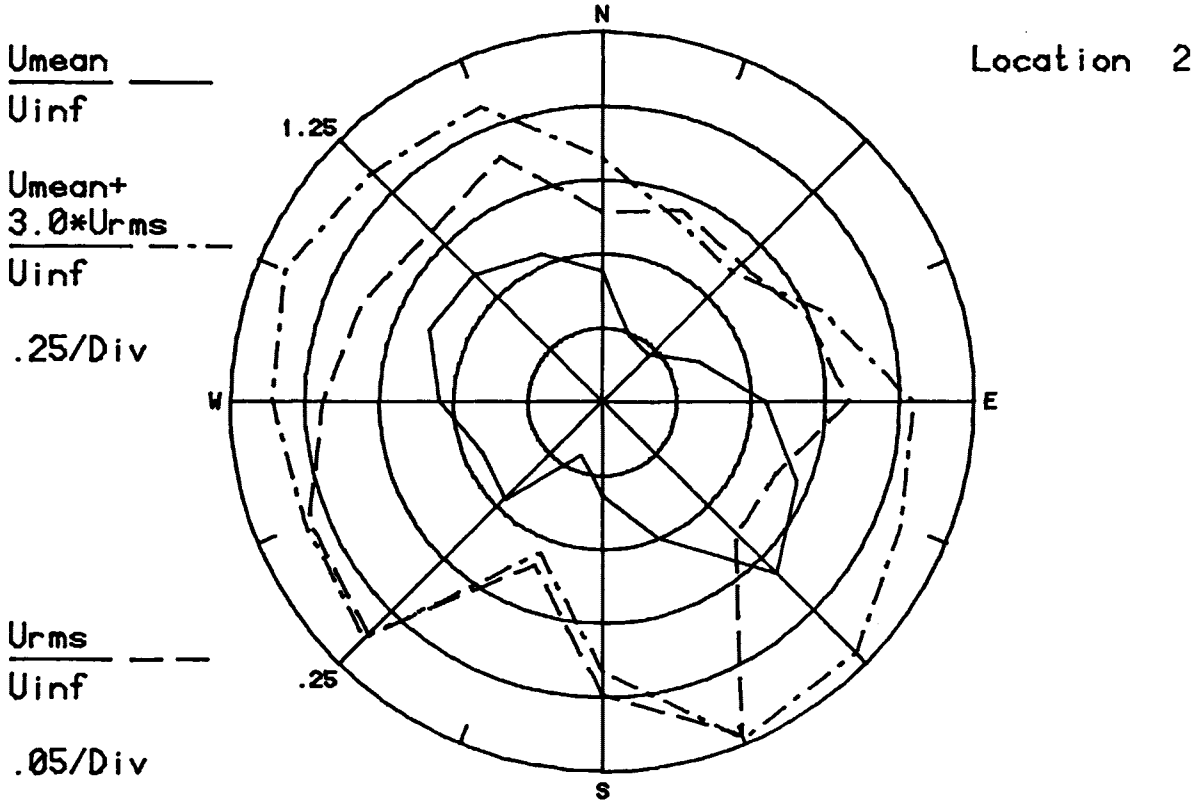


Figure 8b. Mean Velocities and Turbulence Intensities at Pedestrian Locations 1 and 2

TOWER II IN PLACE
CONFIGURATION G

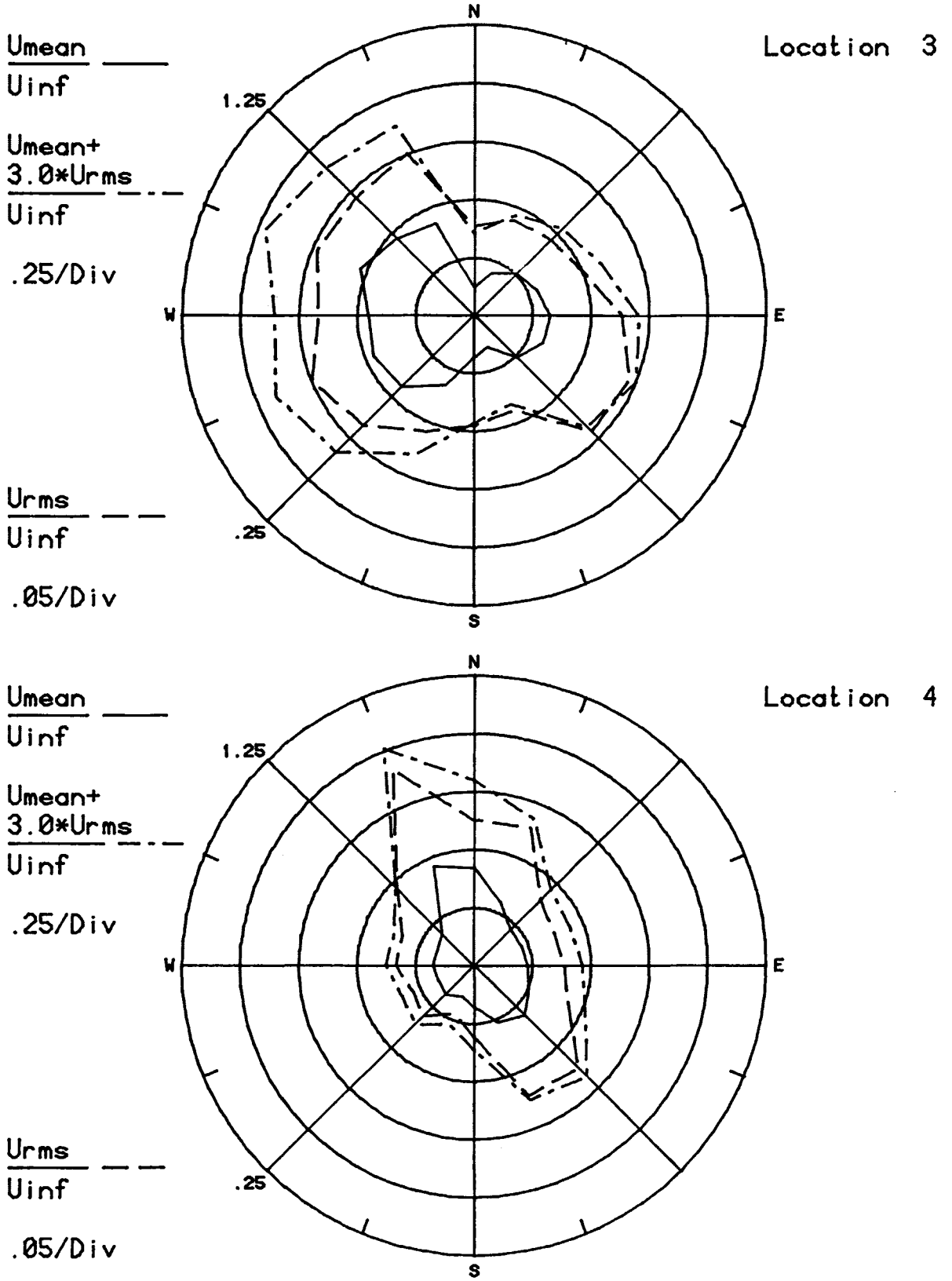
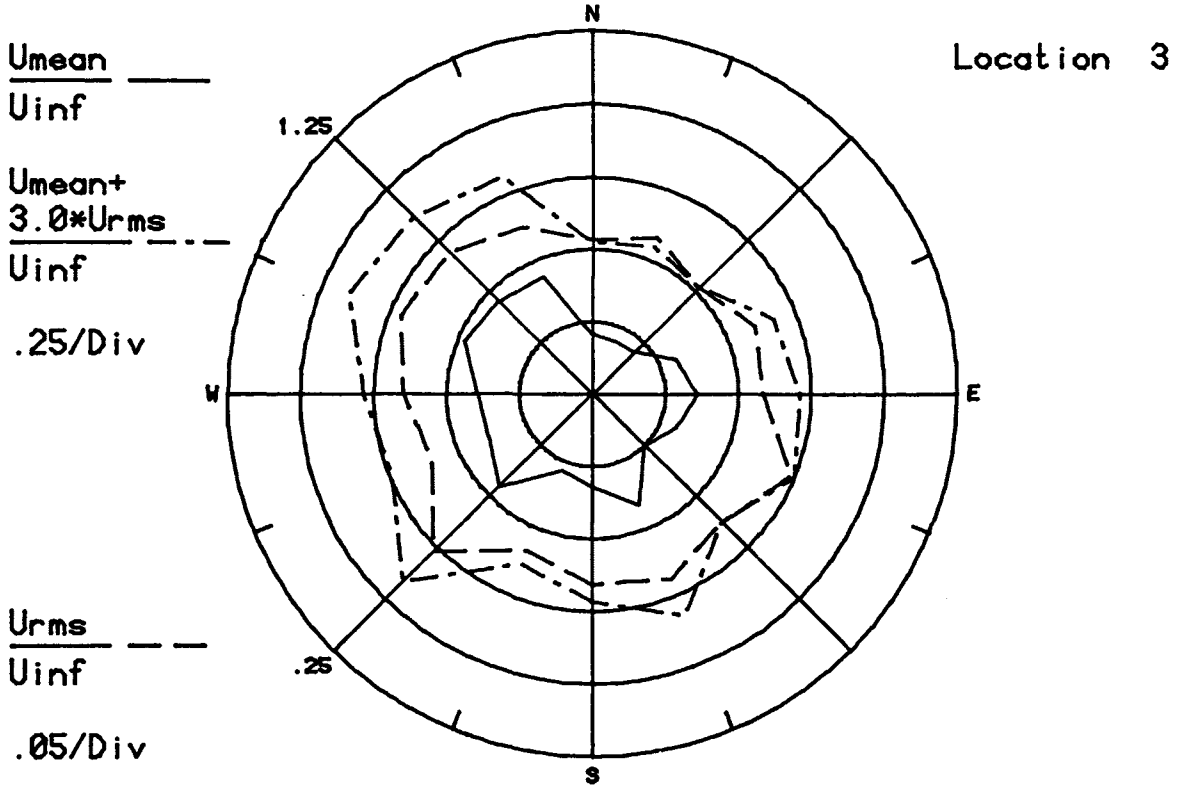


Figure 8c. Mean Velocities and Turbulence Intensities at Pedestrian Locations 3 and 4

TOWER II OUT

CONFIGURATION H



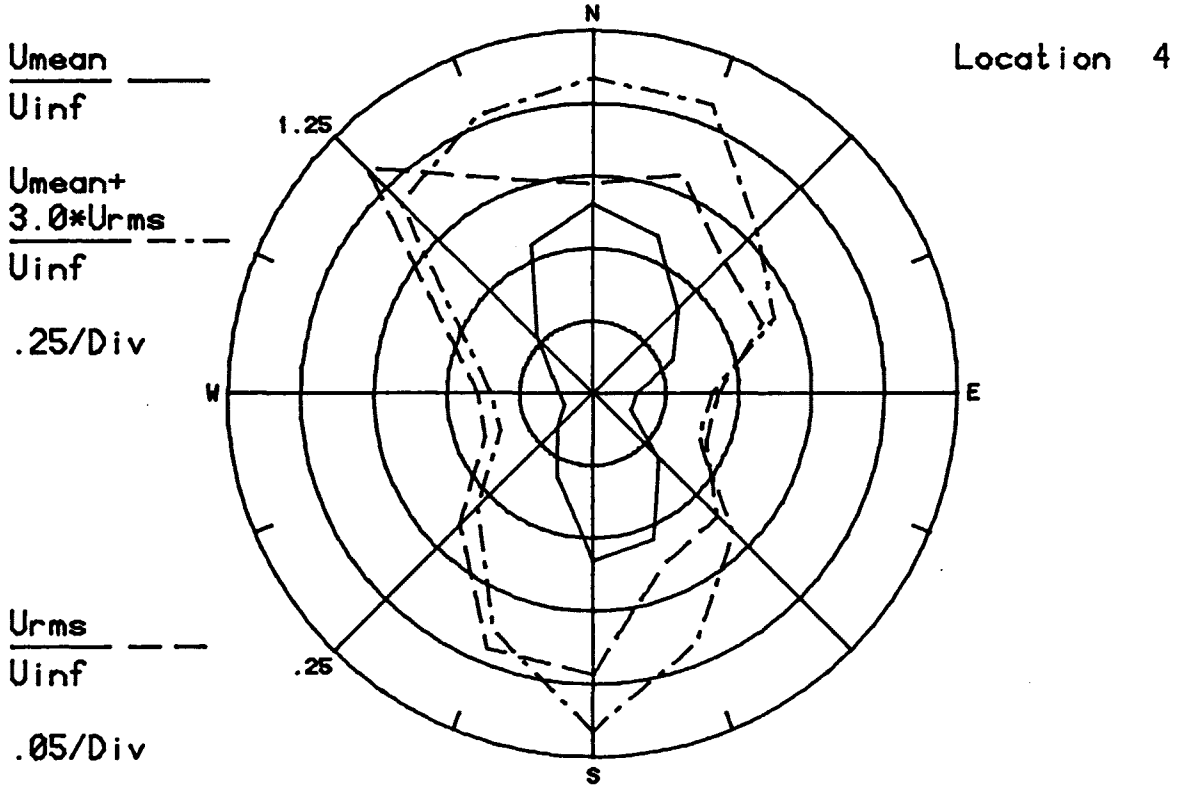


Figure 8d. Mean Velocities and Turbulence Intensities at Pedestrian Locations 3 and 4

TOWER II IN PLACE

CONFIGURATION G

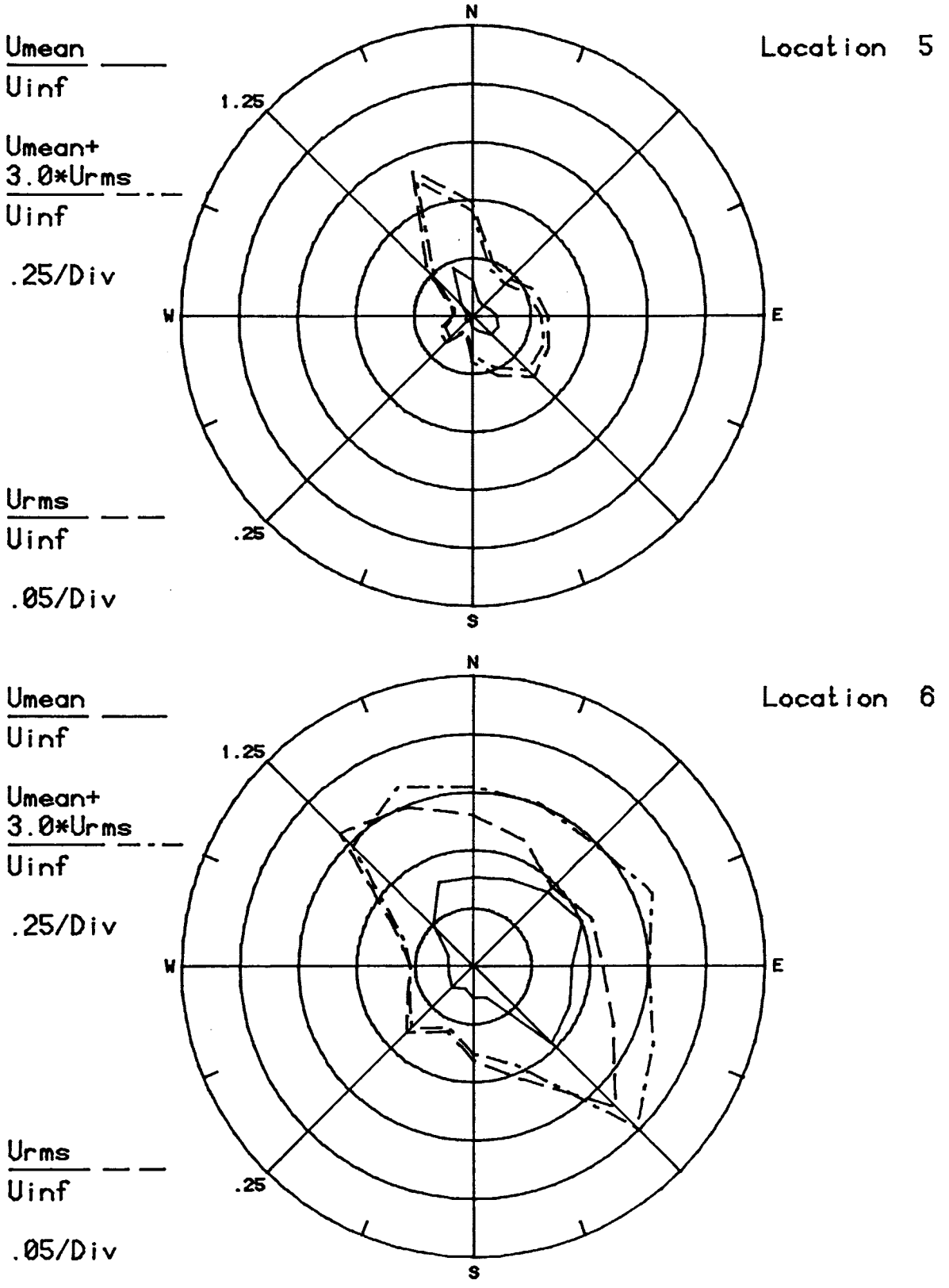


Figure 8e. Mean Velocities and Turbulence Intensities at Pedestrian Locations 5 and 6

TOWER II OUT

CONFIGURATION H

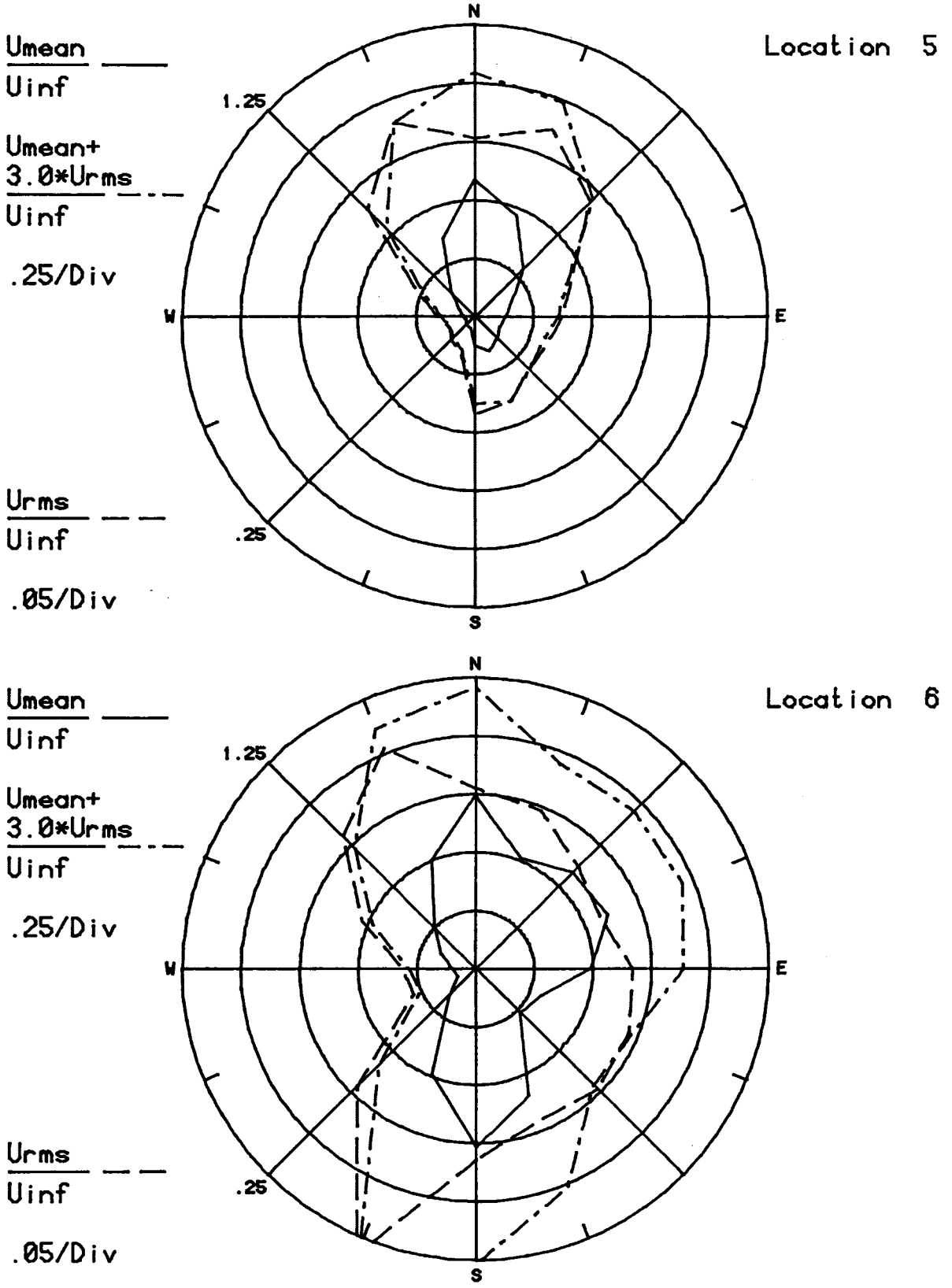
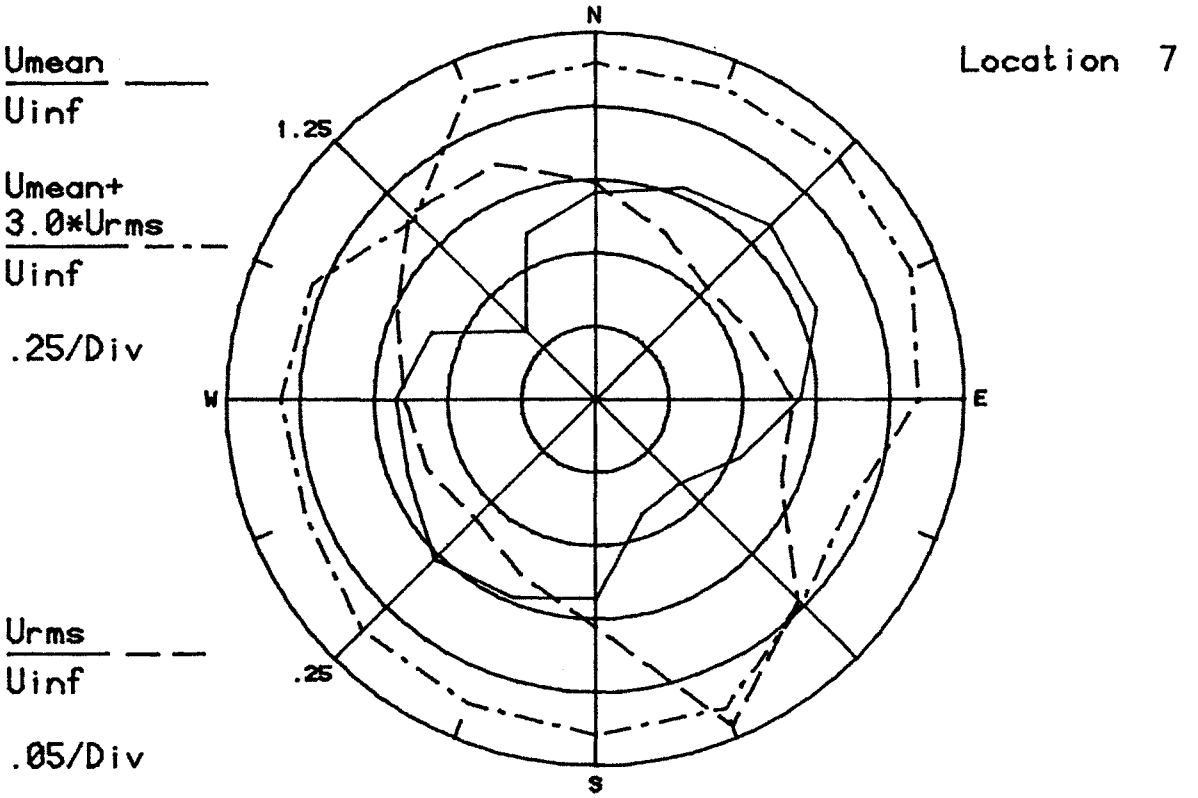


Figure 8f. Mean Velocities and Turbulence Intensities at Pedestrian Locations 5 and 6

TOWER II IN PLACE
CONFIGURATION G



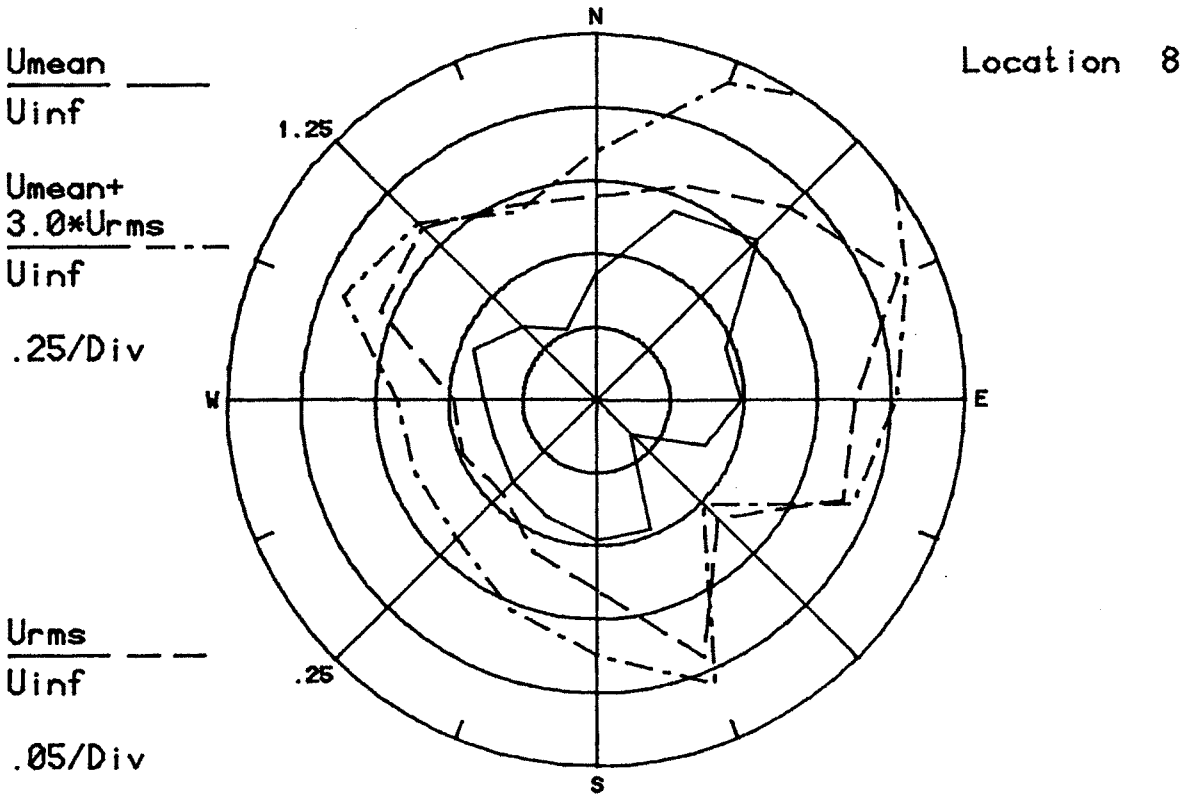
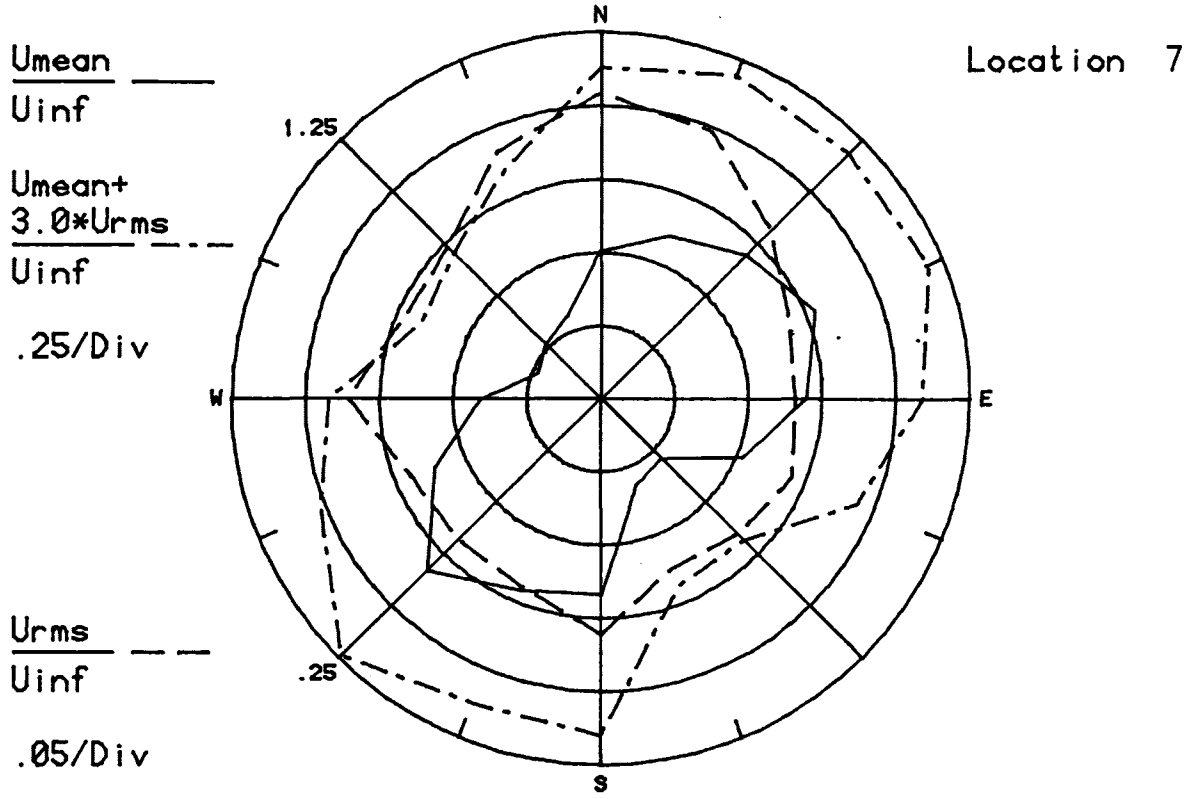


Figure 8g. Mean Velocities and Turbulence Intensities at Pedestrian Locations 7 and 8

TOWER II OUT

CONFIGURATION H



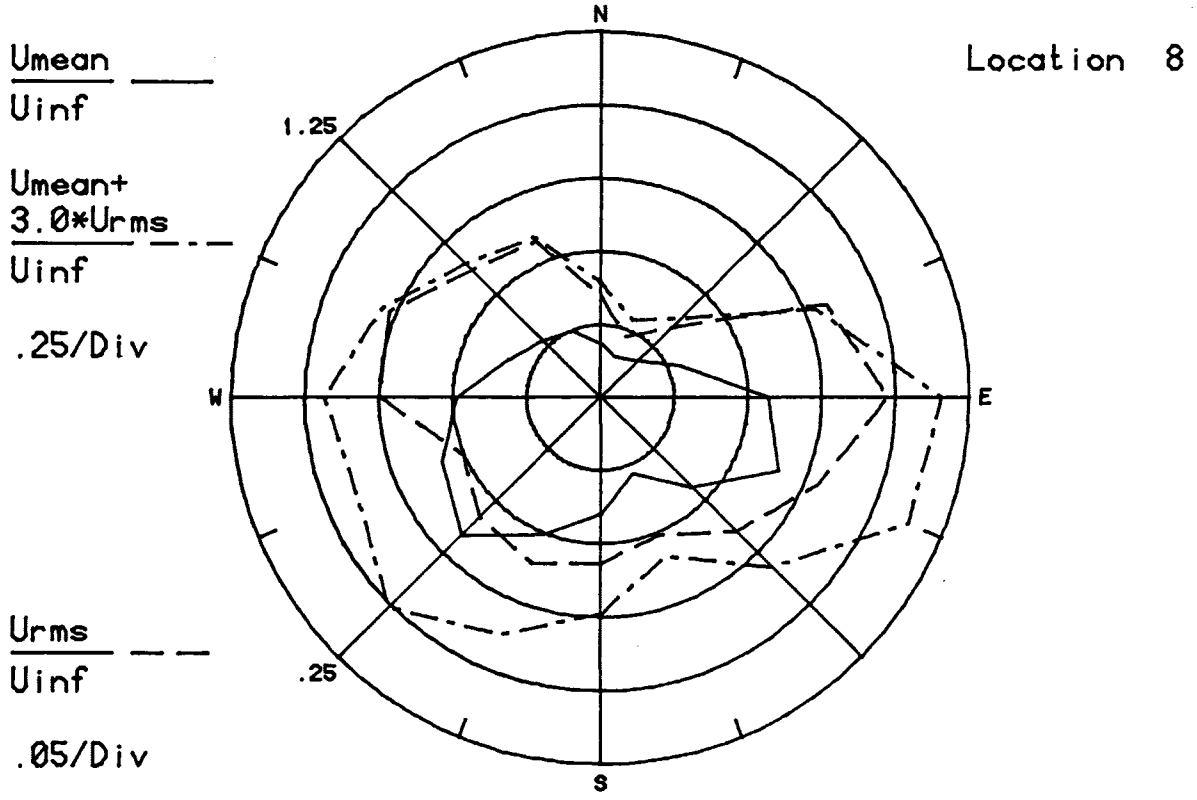


Figure 8h. Mean Velocities and Turbulence Intensities at Pedestrian Locations 7 and 8

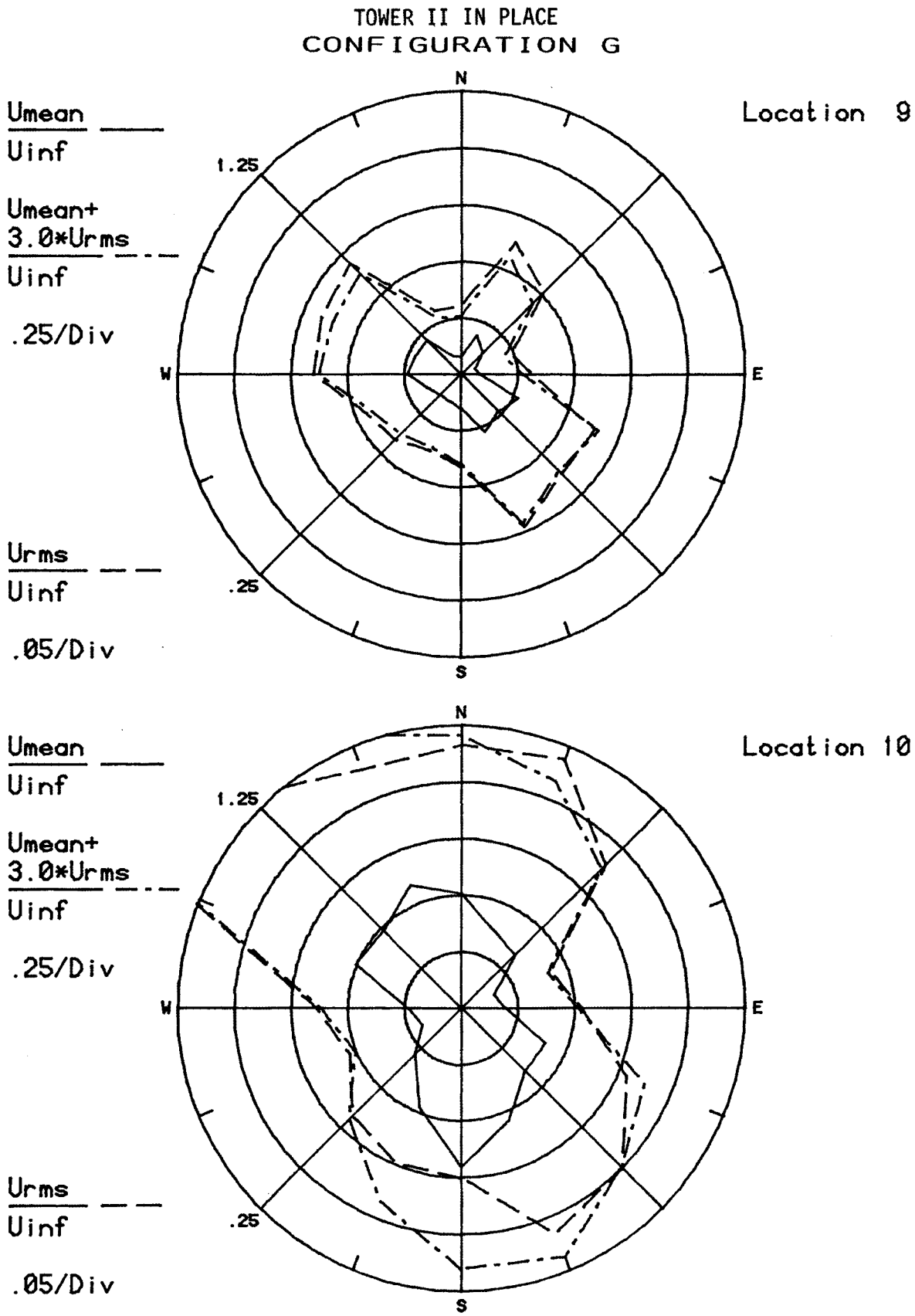


Figure 8i. Mean Velocities and Turbulence Intensities at Pedestrian Locations 9 and 10

TOWER II OUT
CONFIGURATION H

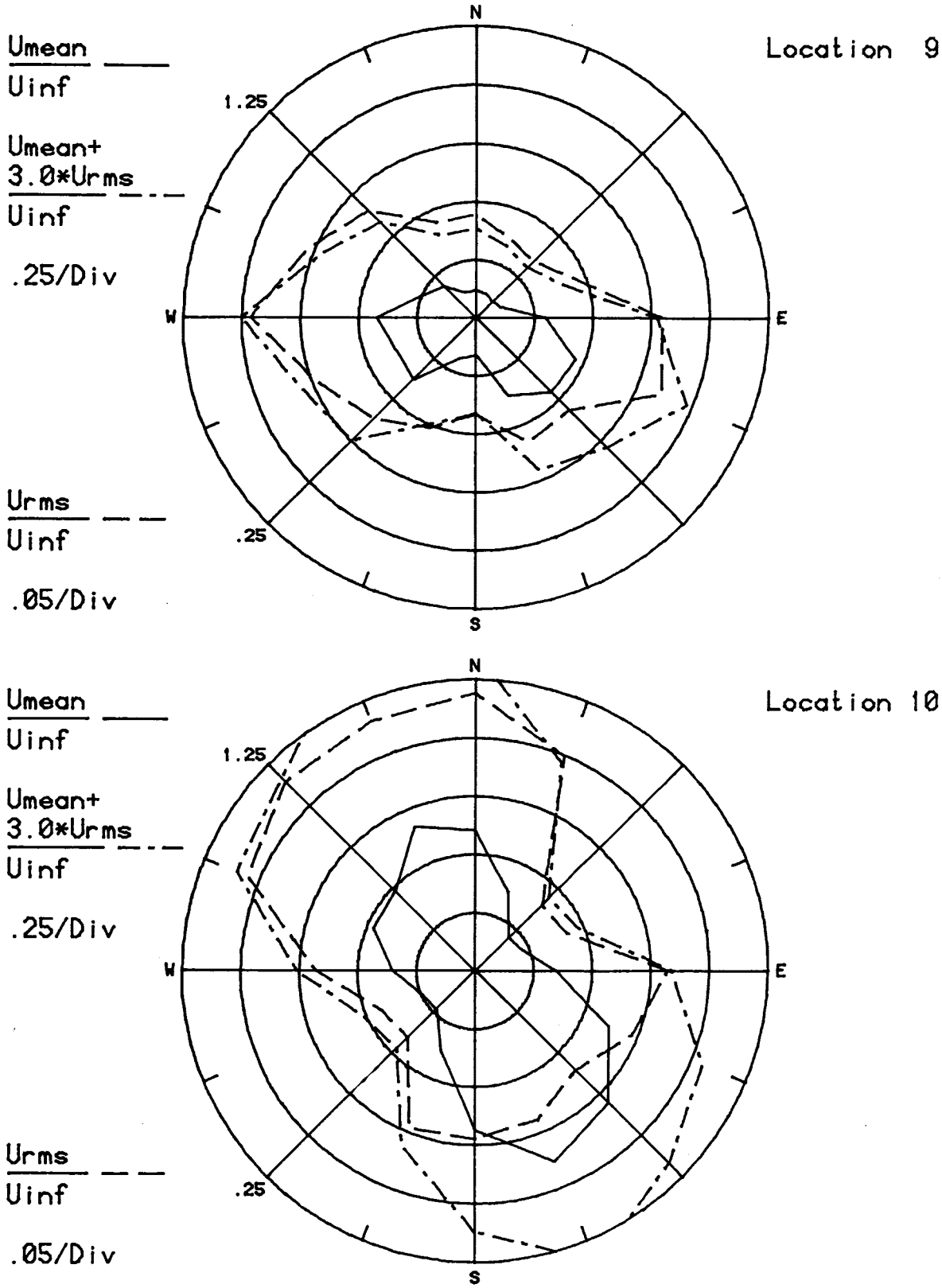
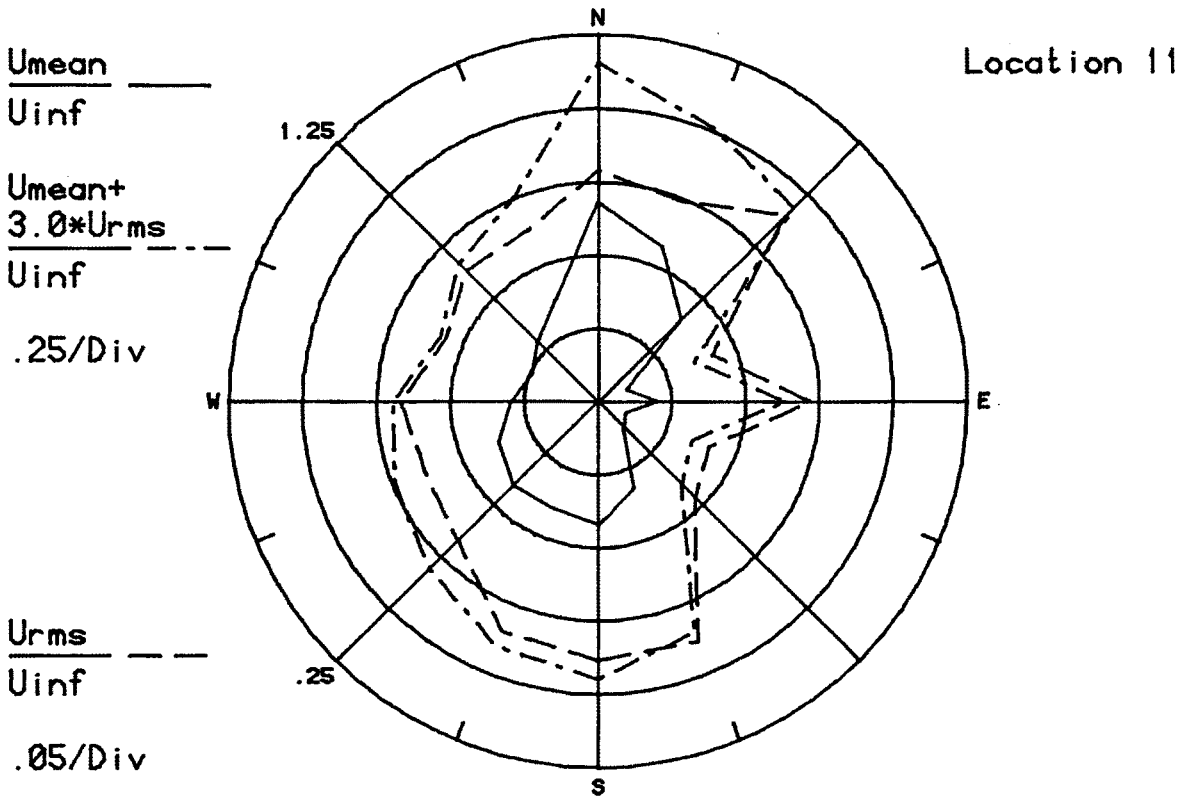


Figure 8j. Mean Velocities and Turbulence Intensities at Pedestrian Locations 9 and 10

TOWER II IN PLACE
CONFIGURATION G



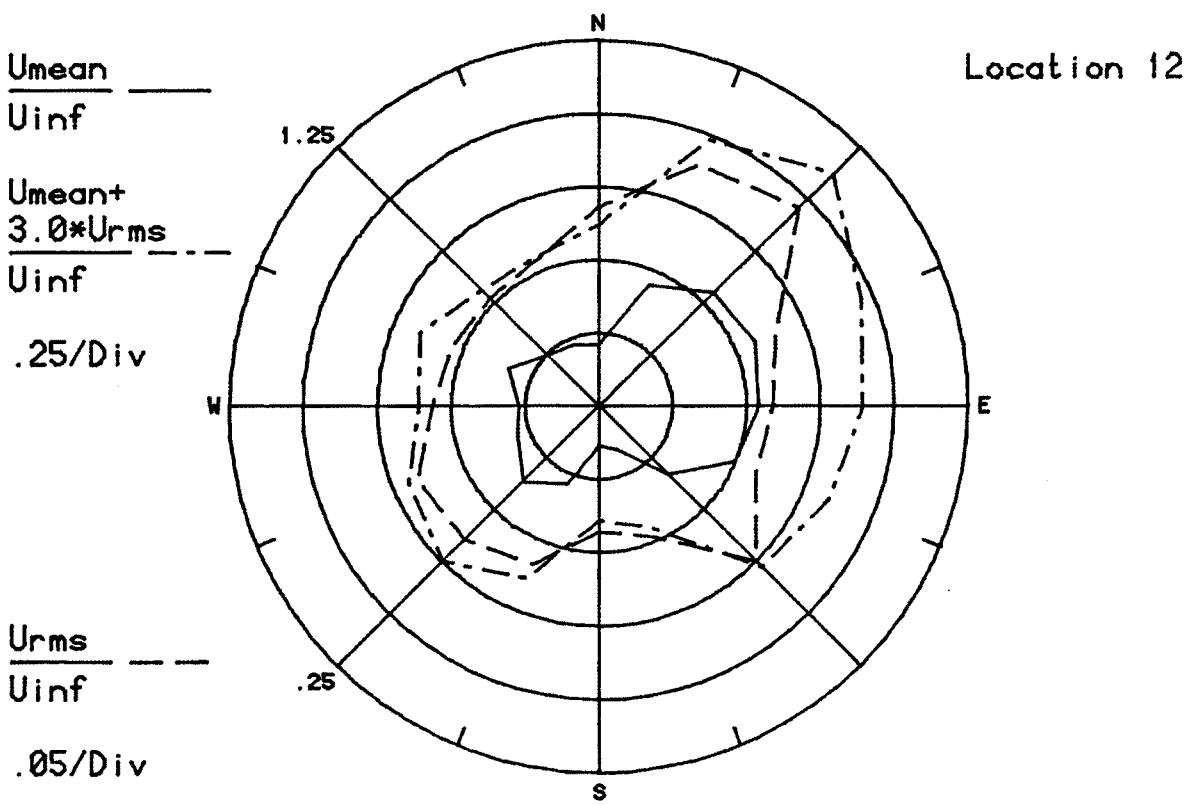
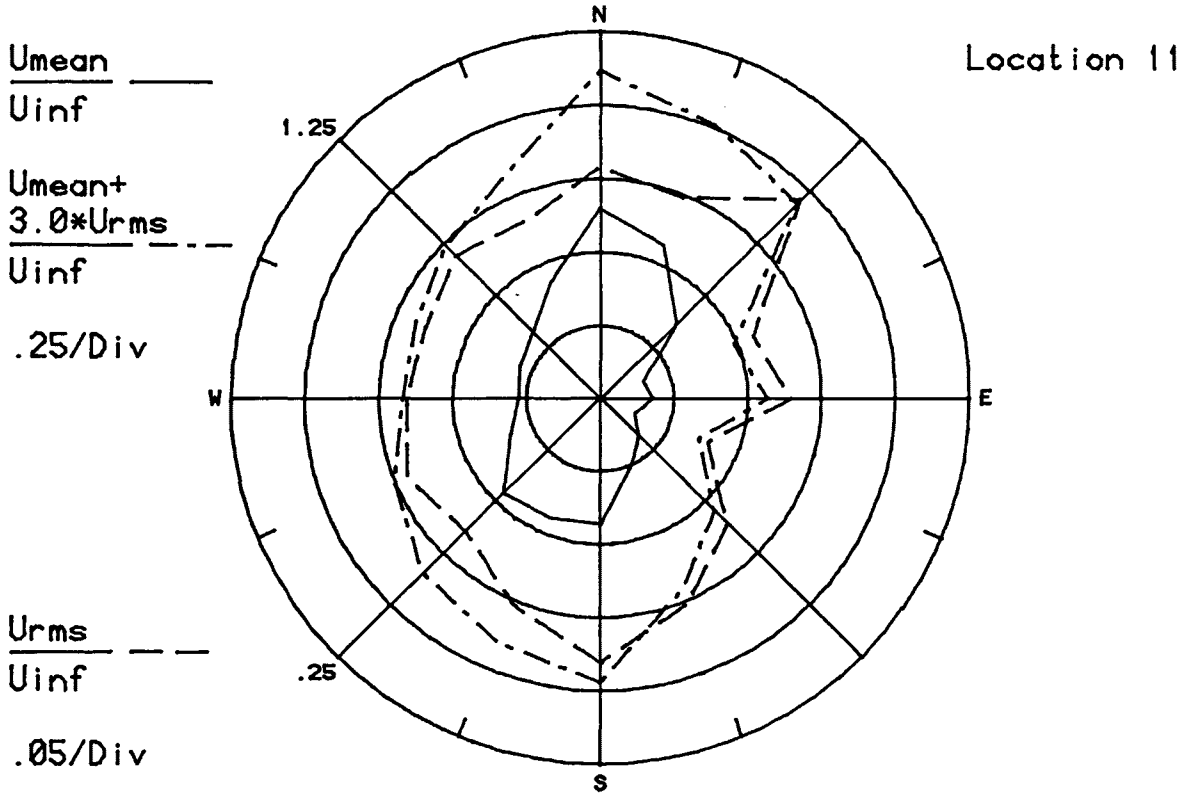


Figure 8k. Mean Velocities and Turbulence Intensities at Pedestrian Locations 11 and 12

TOWER II OUT

CONFIGURATION H



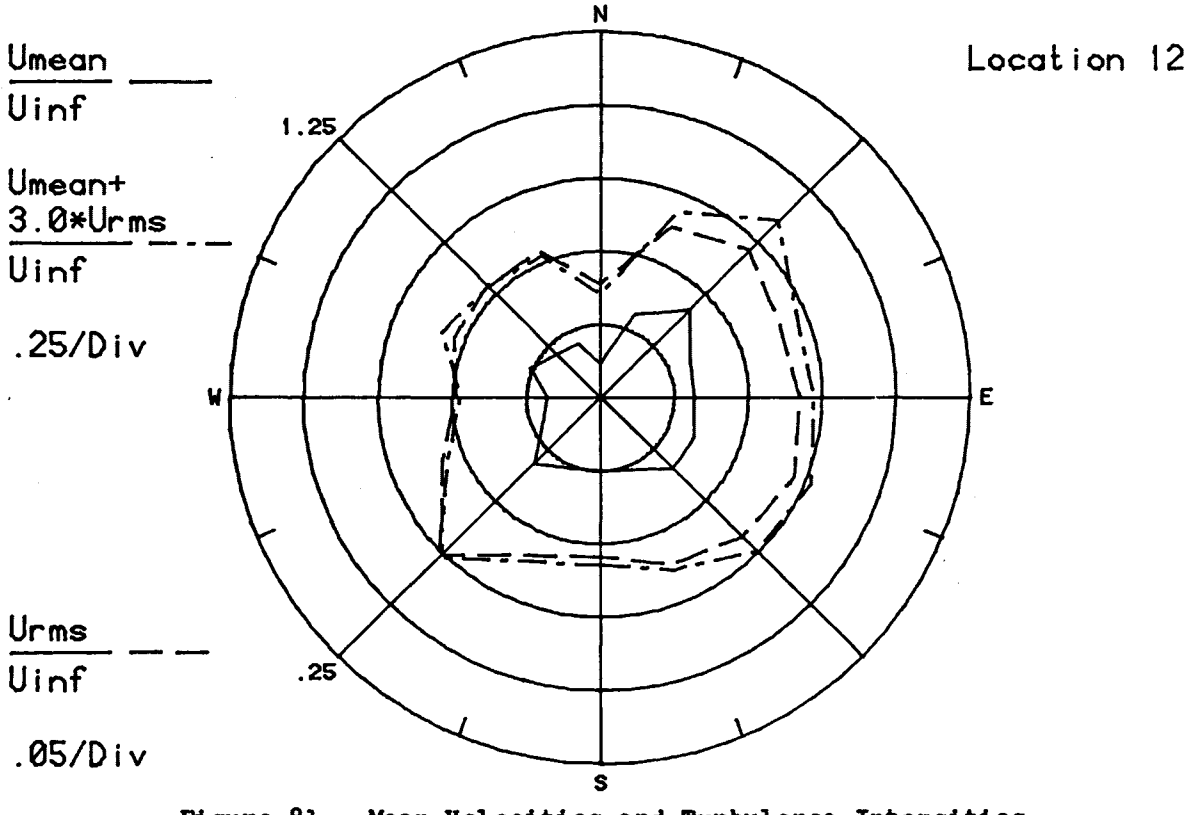
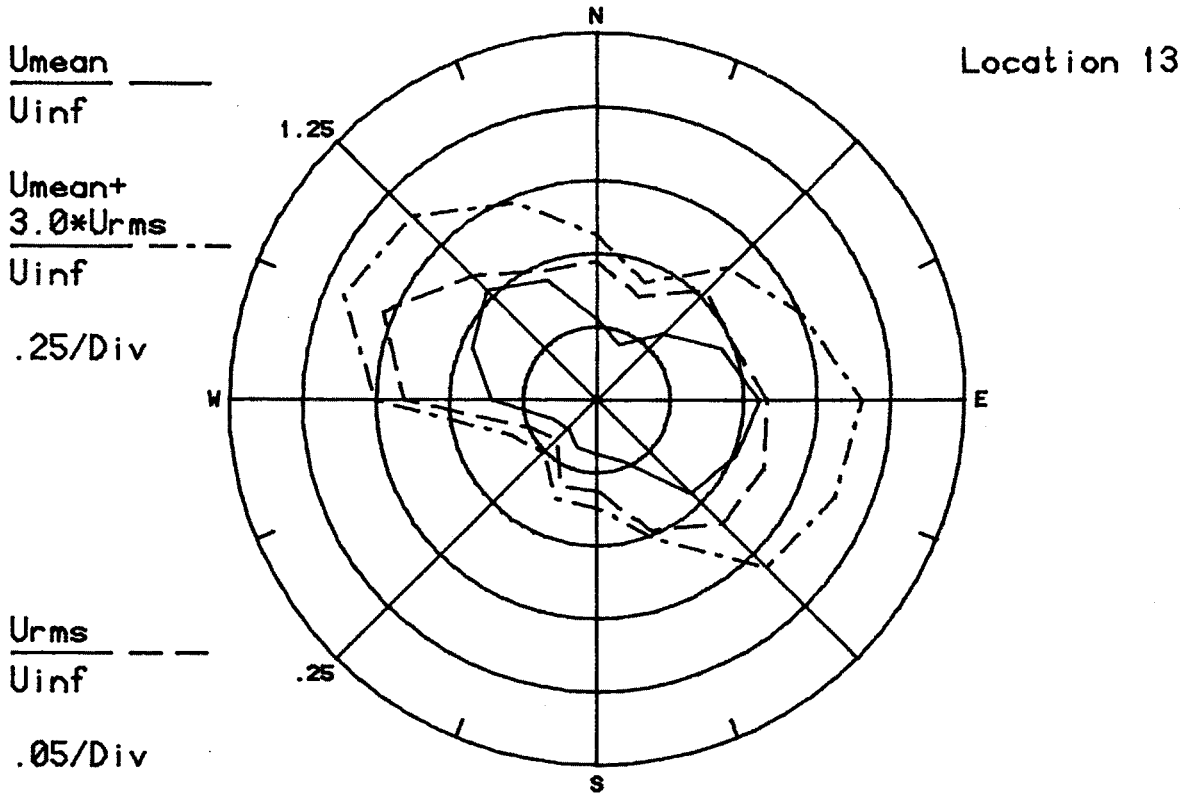


Figure 81. Mean Velocities and Turbulence Intensities at Pedestrian Locations 11 and 12

TOWER II IN PLACE

CONFIGURATION G



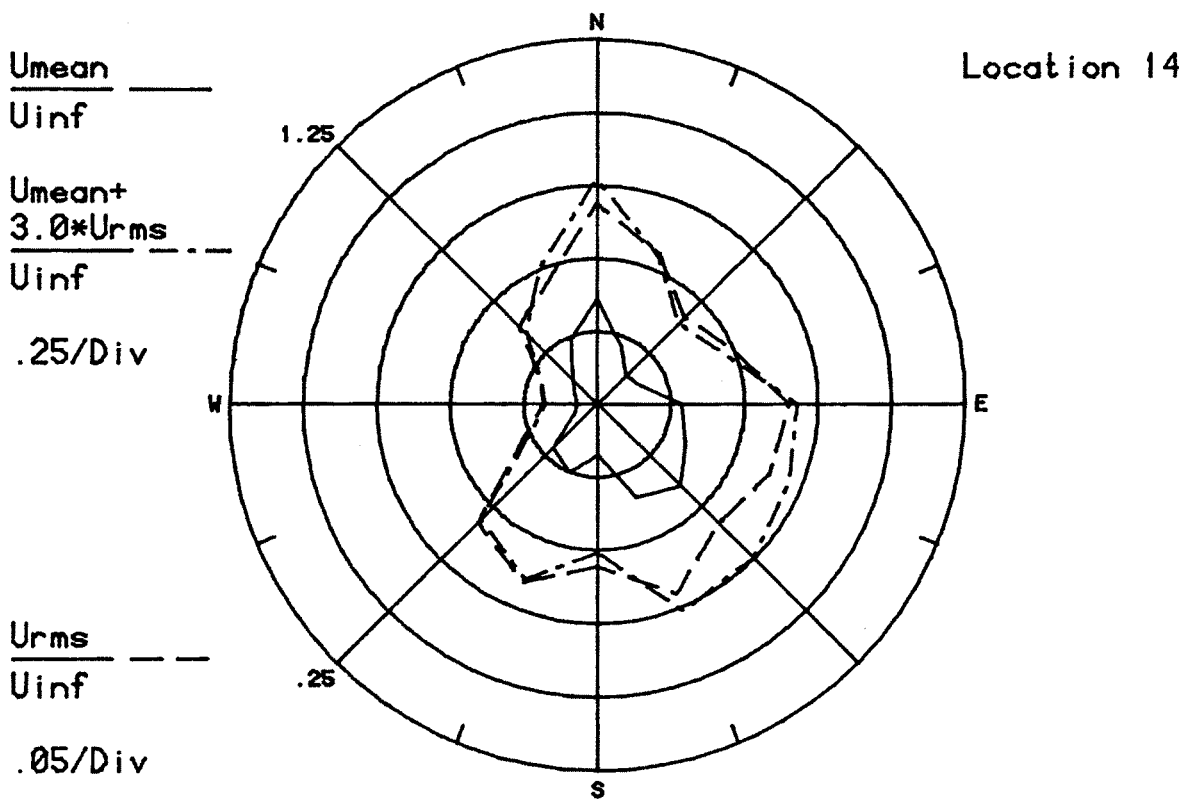
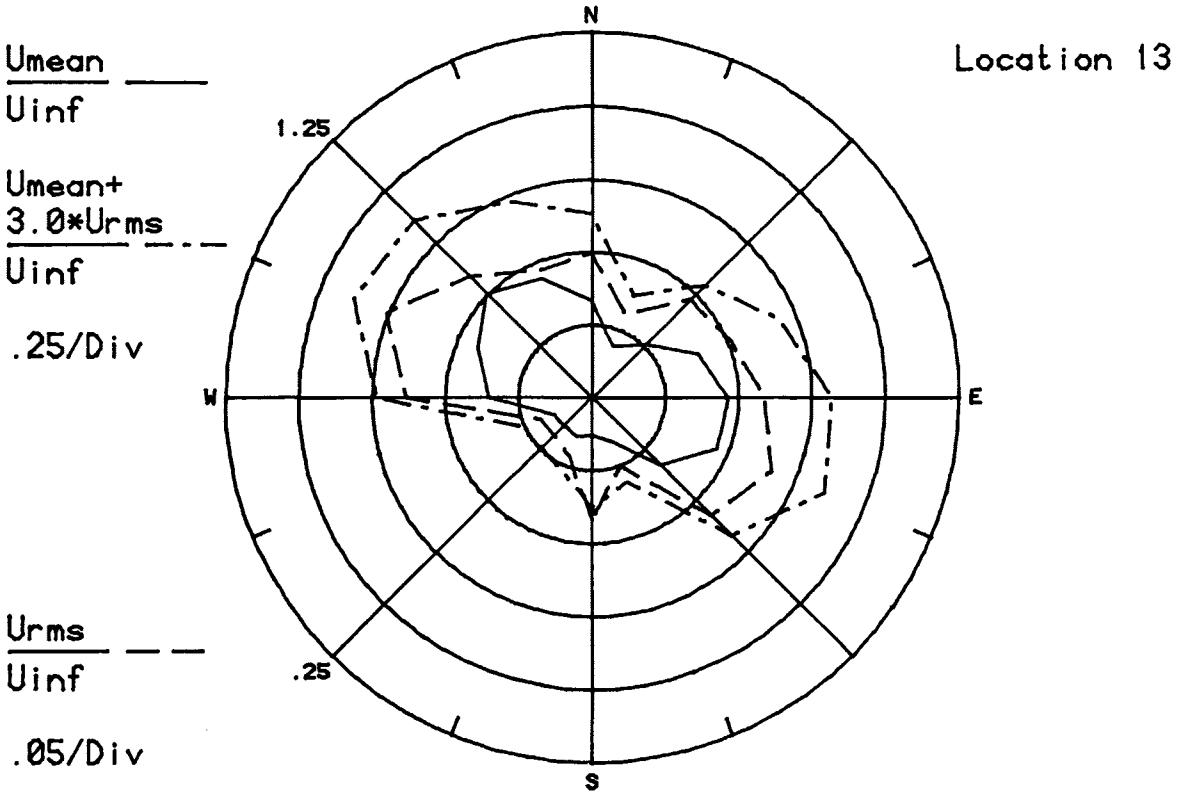


Figure 8m. Mean Velocities and Turbulence Intensities at Pedestrian Locations 13 and 14

TOWER II OUT

CONFIGURATION H



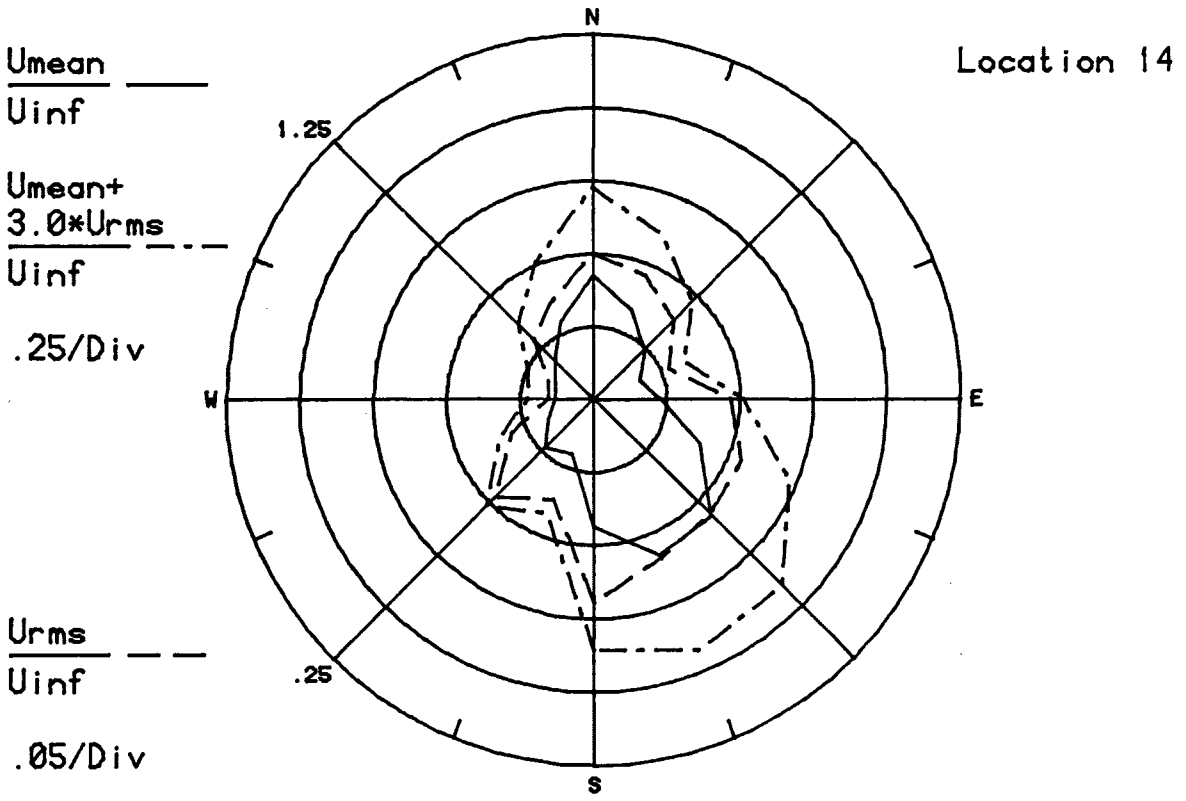
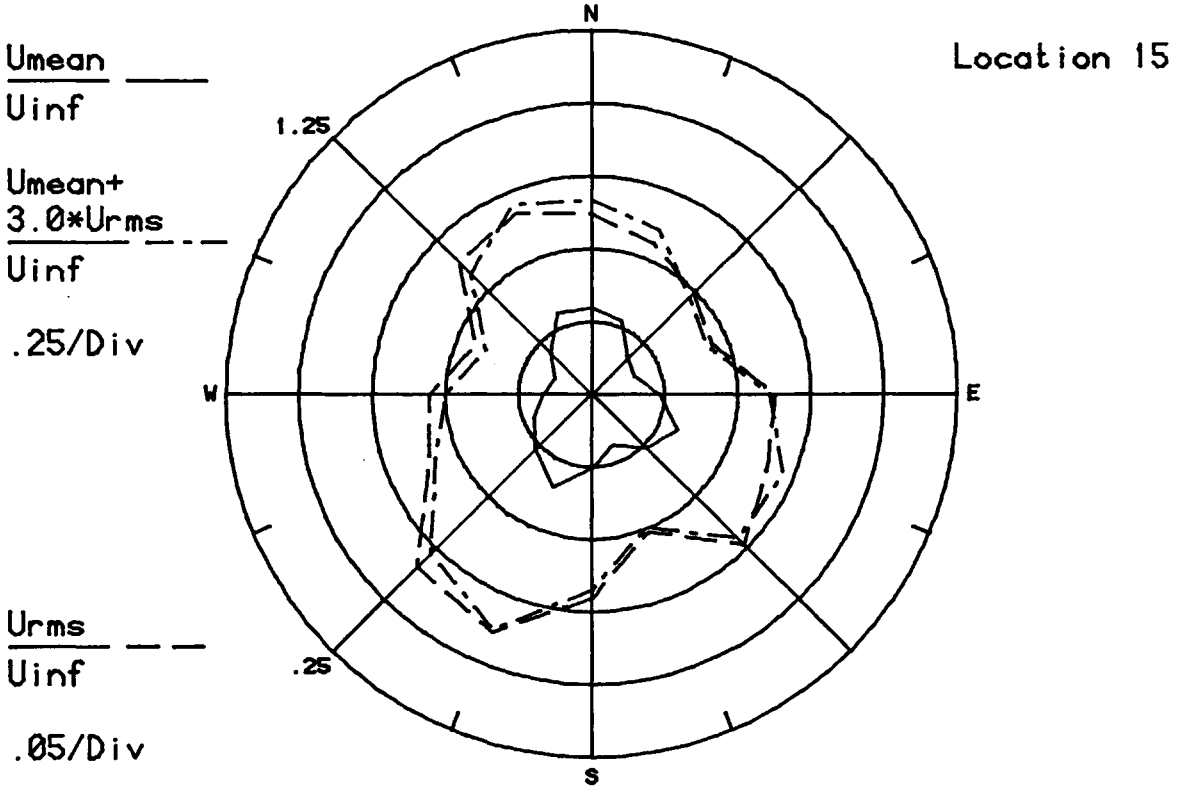


Figure 8n. Mean Velocities and Turbulence Intensities at Pedestrian Locations 13 and 14

TOWER II IN PLACE

CONFIGURATION G



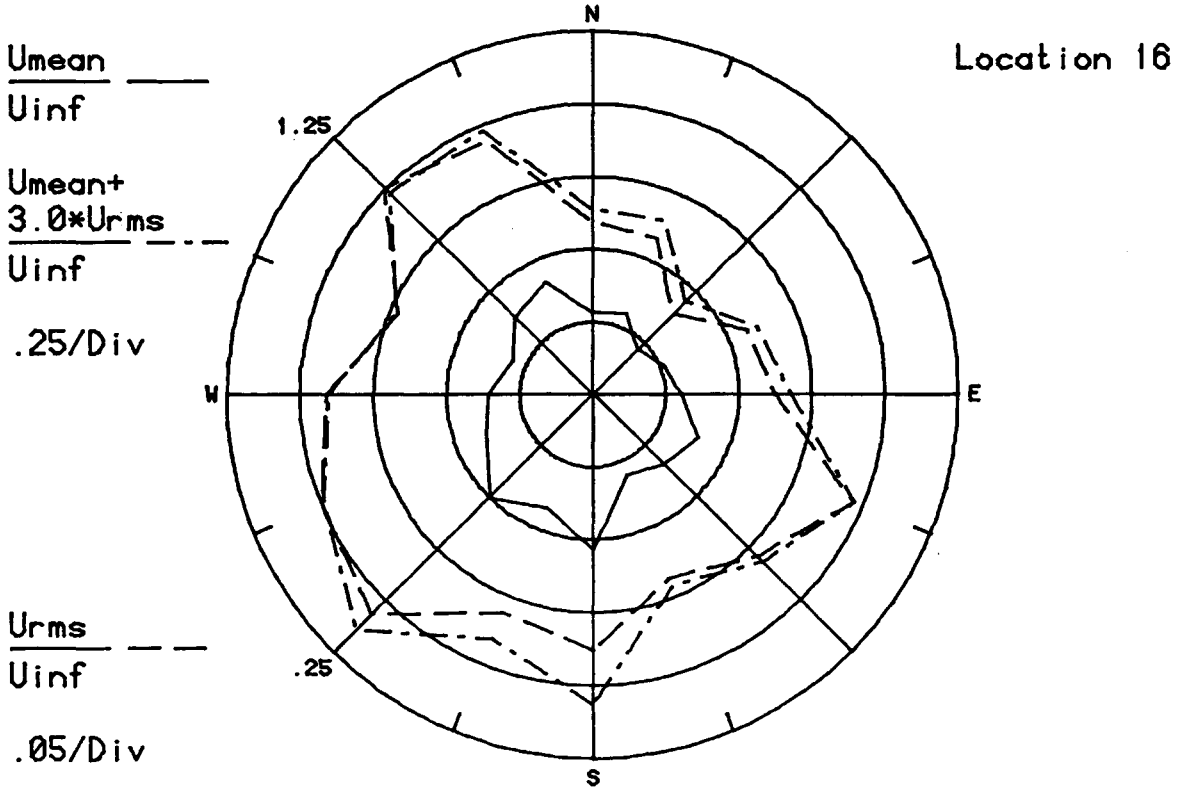


Figure 8o. Mean Velocities and Turbulence Intensities at Pedestrian Locations 15 and 16

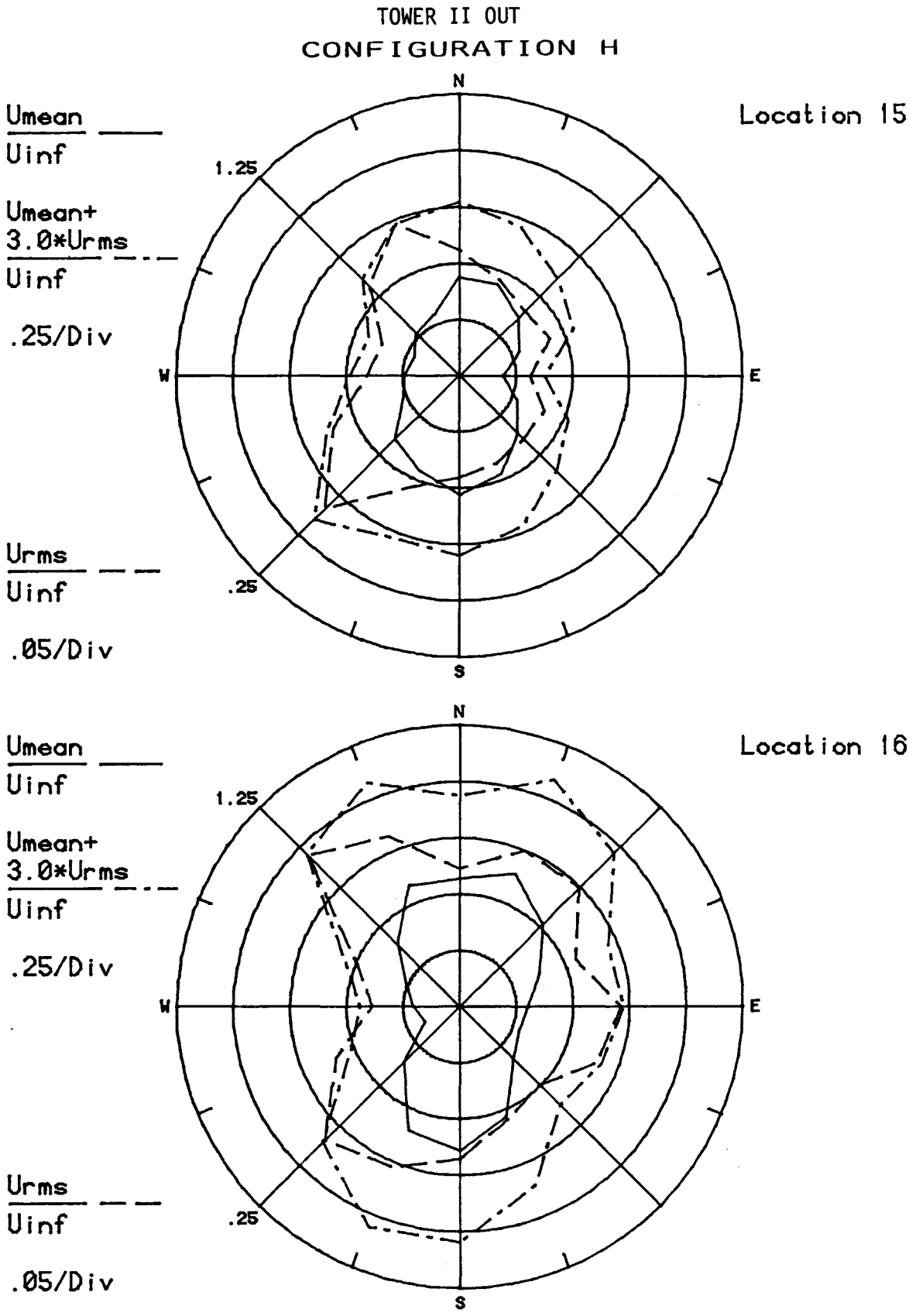


Figure 8p. Mean Velocities and Turbulence Intensities at Pedestrian Locations 15 and 16

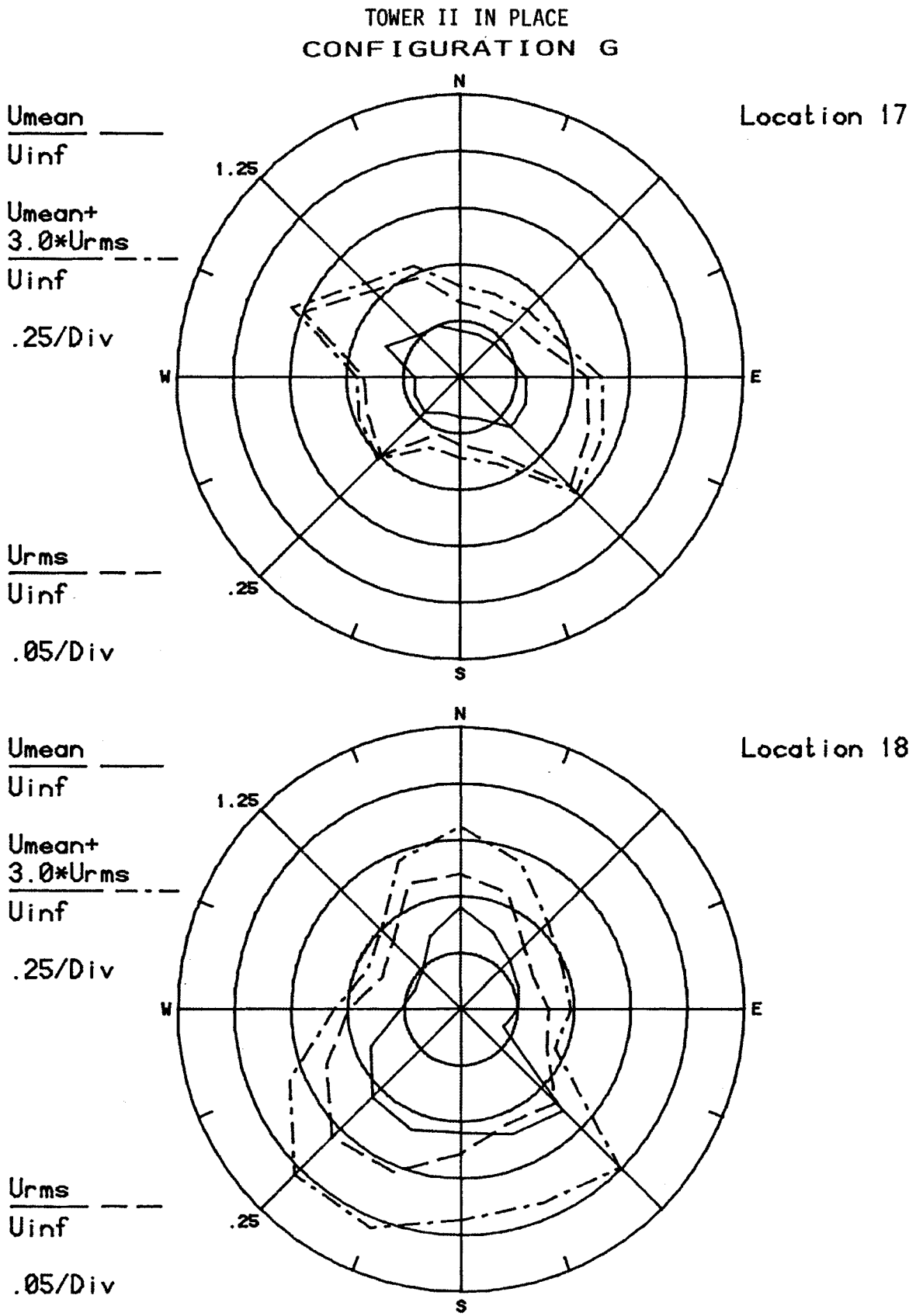


Figure 8q. Mean Velocities and Turbulence Intensities at Pedestrian Locations 17 and 18

TOWER II OUT

CONFIGURATION H

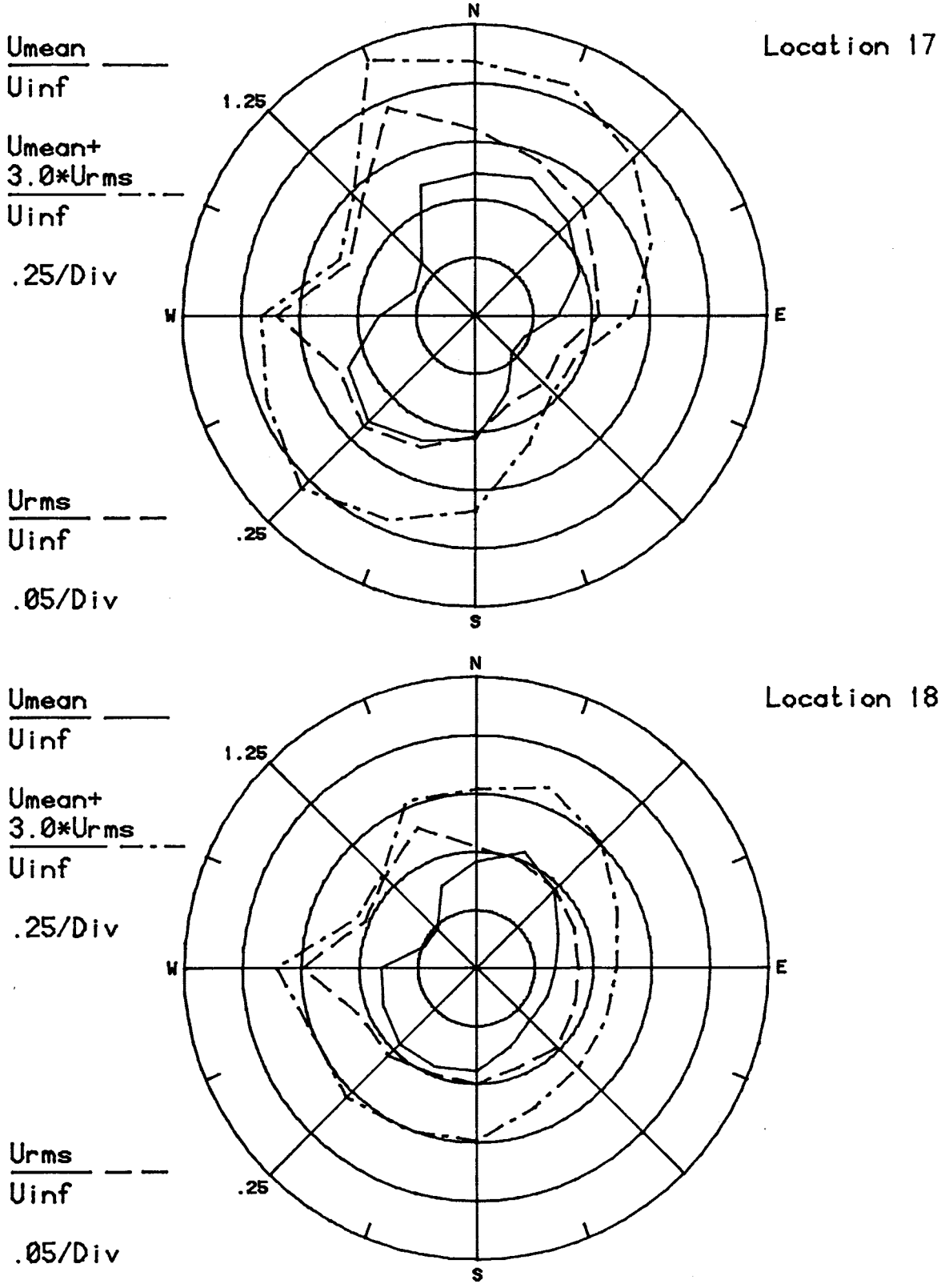


Figure 8r. Mean Velocities and Turbulence Intensities at Pedestrian Locations 17 and 18

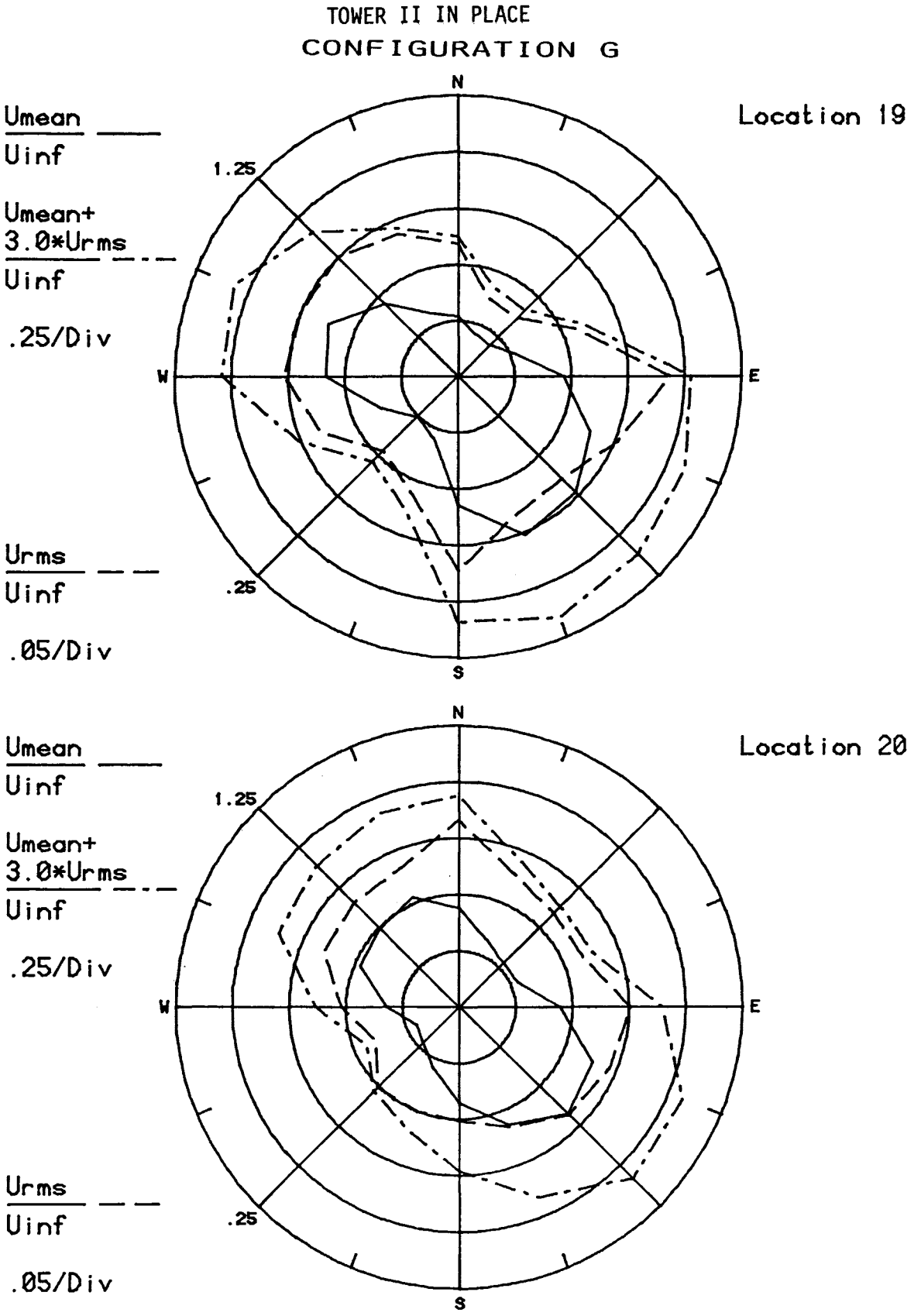


Figure 8s. Mean Velocities and Turbulence Intensities at Pedestrian Locations 19 and 20

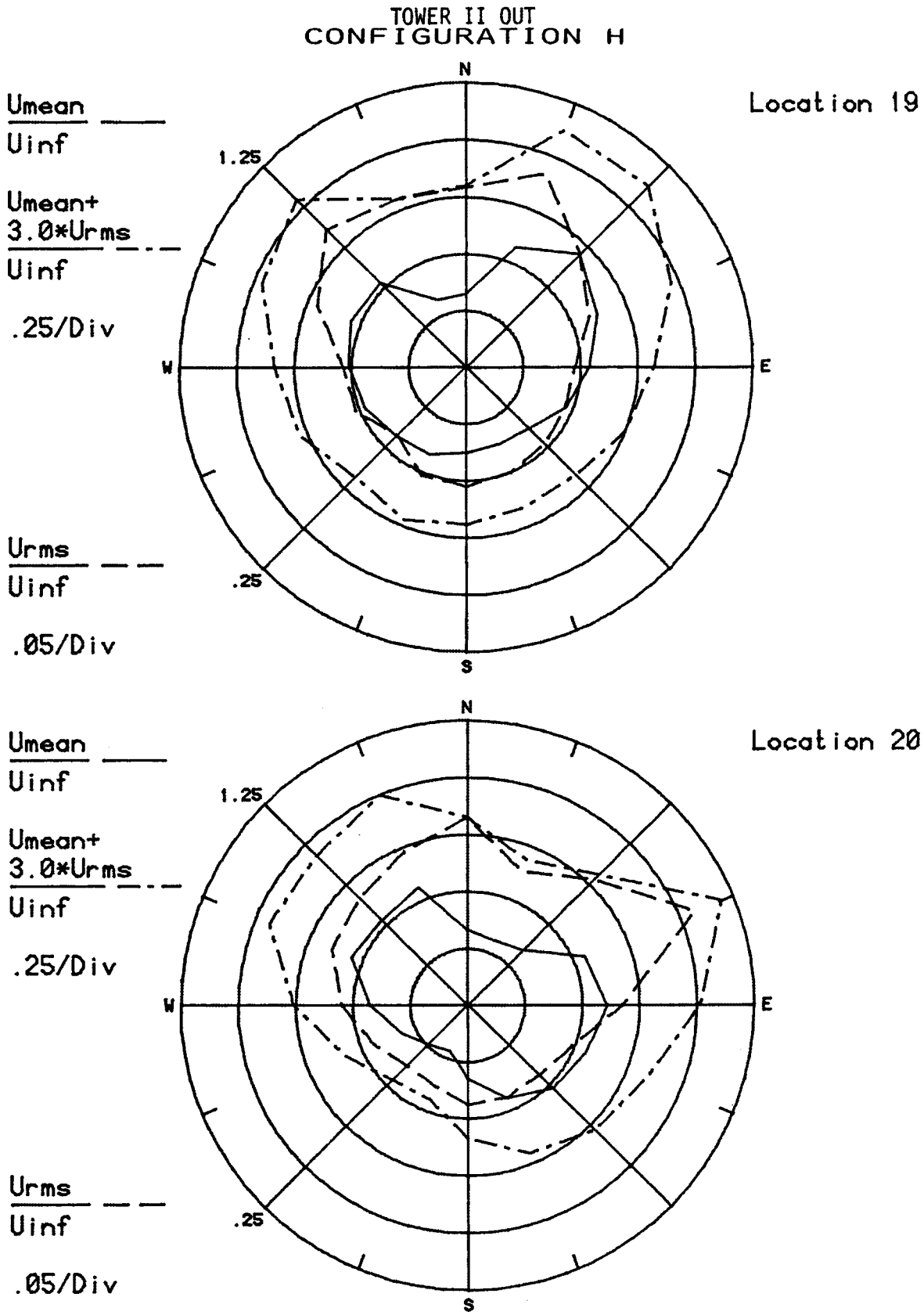
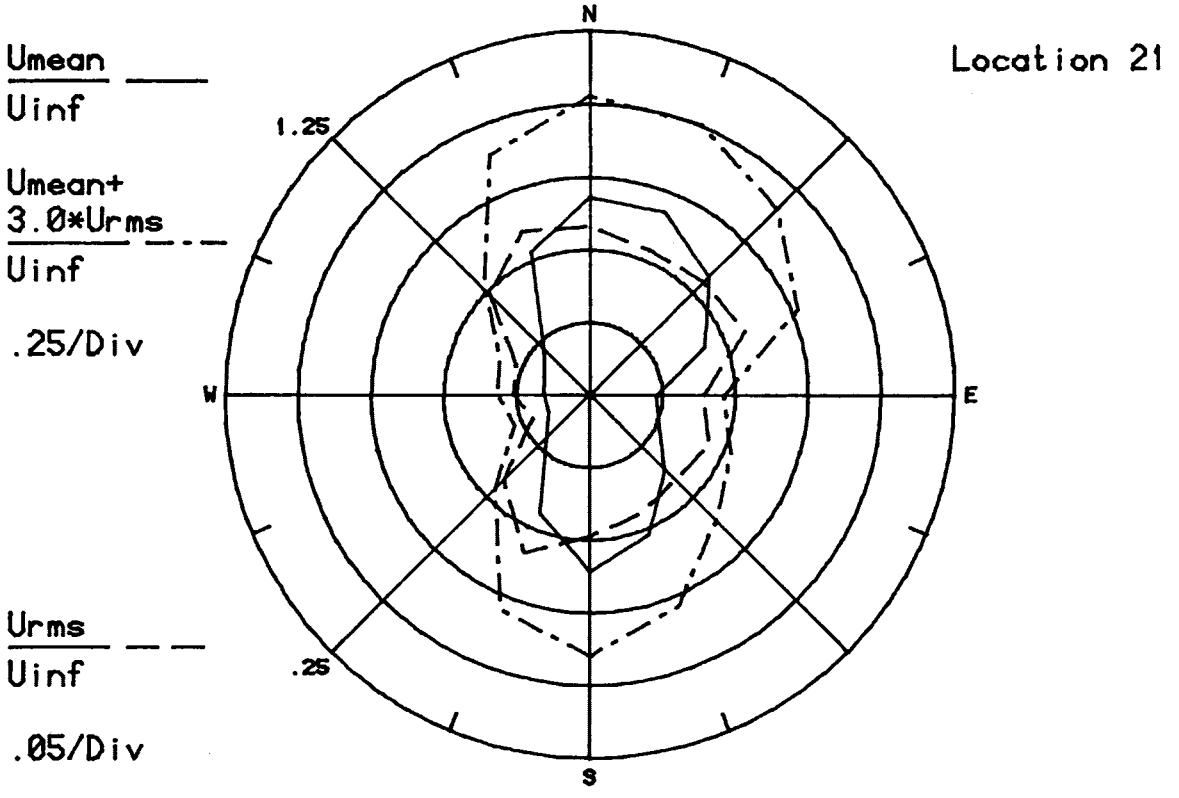


Figure 8t. Mean Velocities and Turbulence Intensities at Pedestrian Locations 19 and 20

TOWER II IN PLACE

CONFIGURATION G



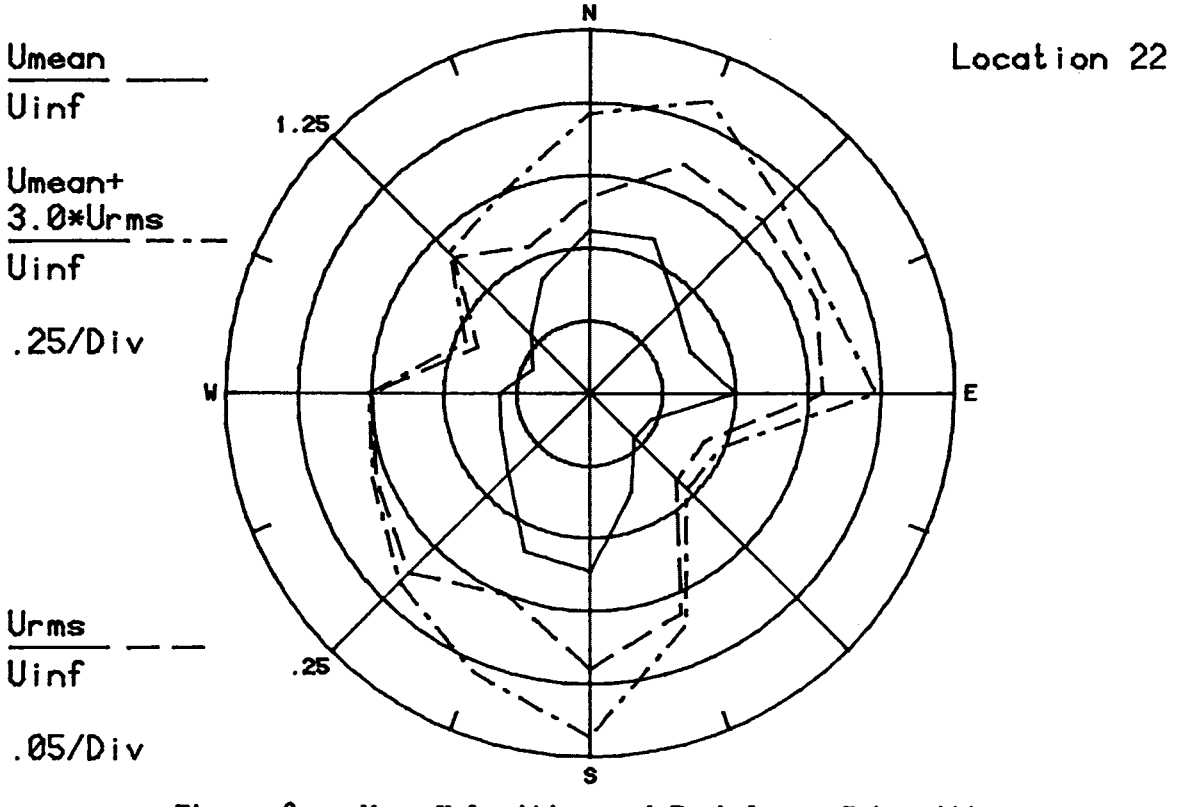
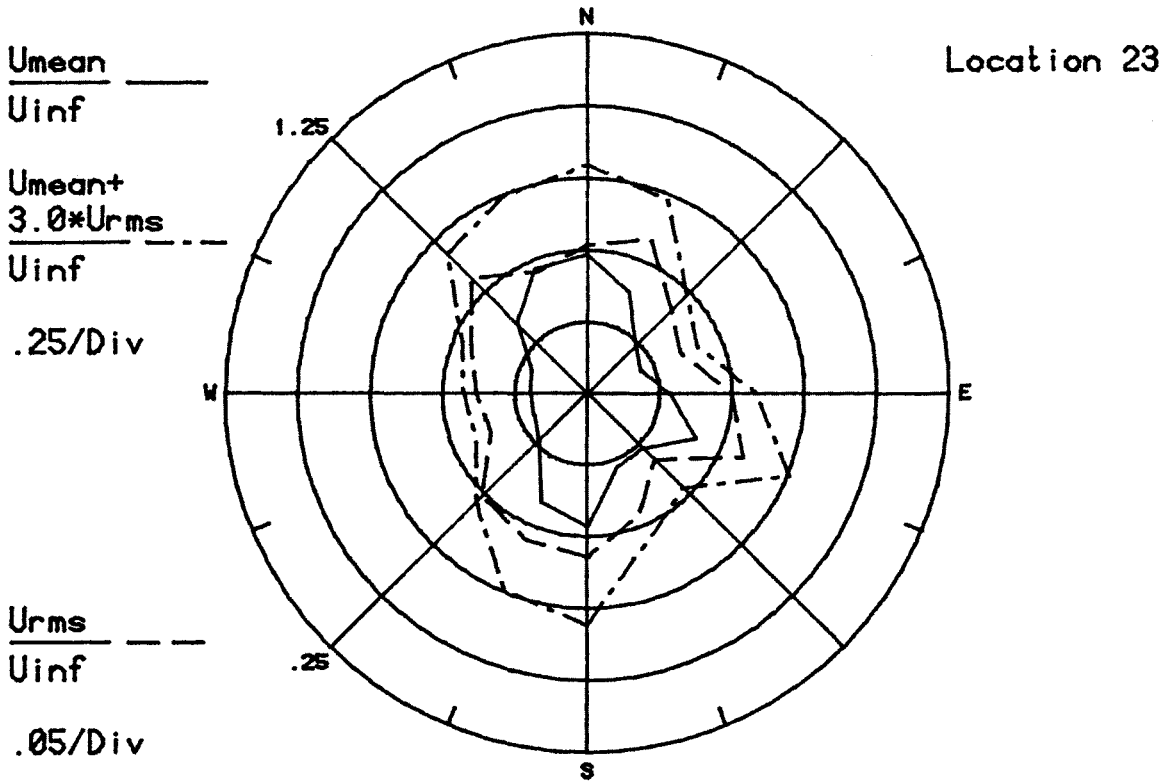


Figure 8u. Mean Velocities and Turbulence Intensities at Pedestrian Locations 21 and 22

TOWER II IN PLACE

CONFIGURATION G



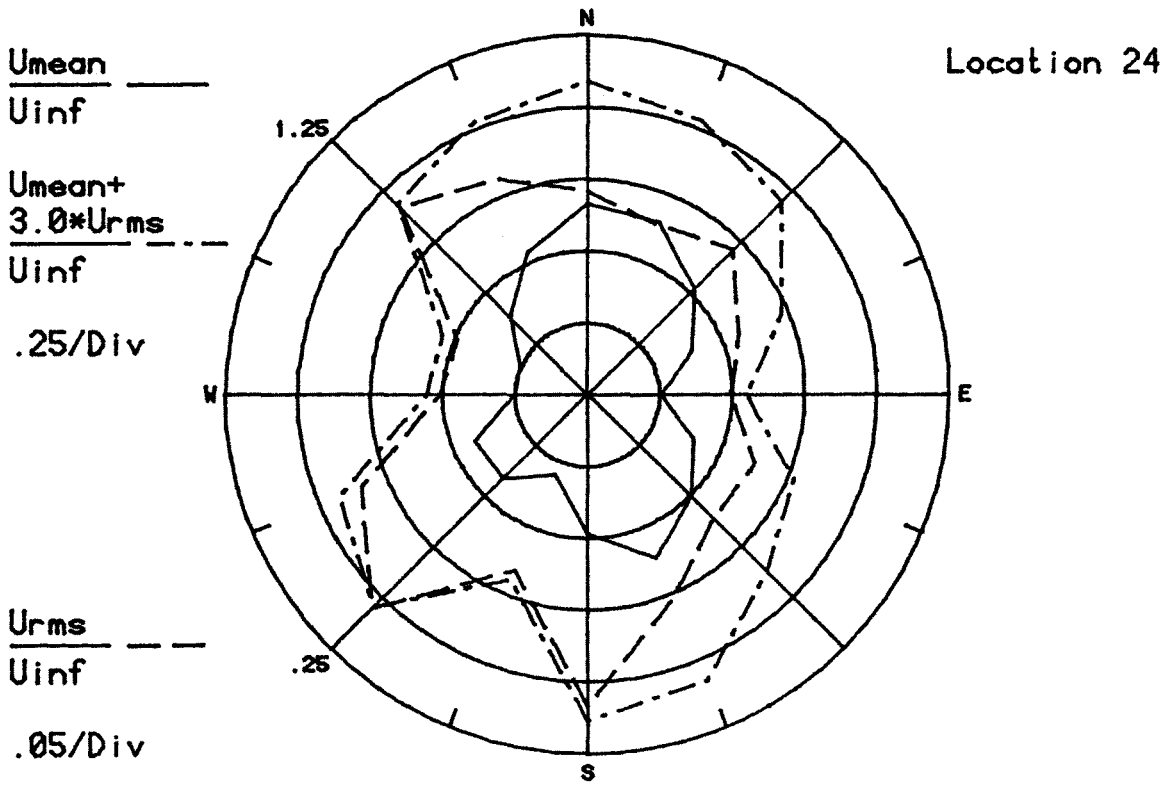
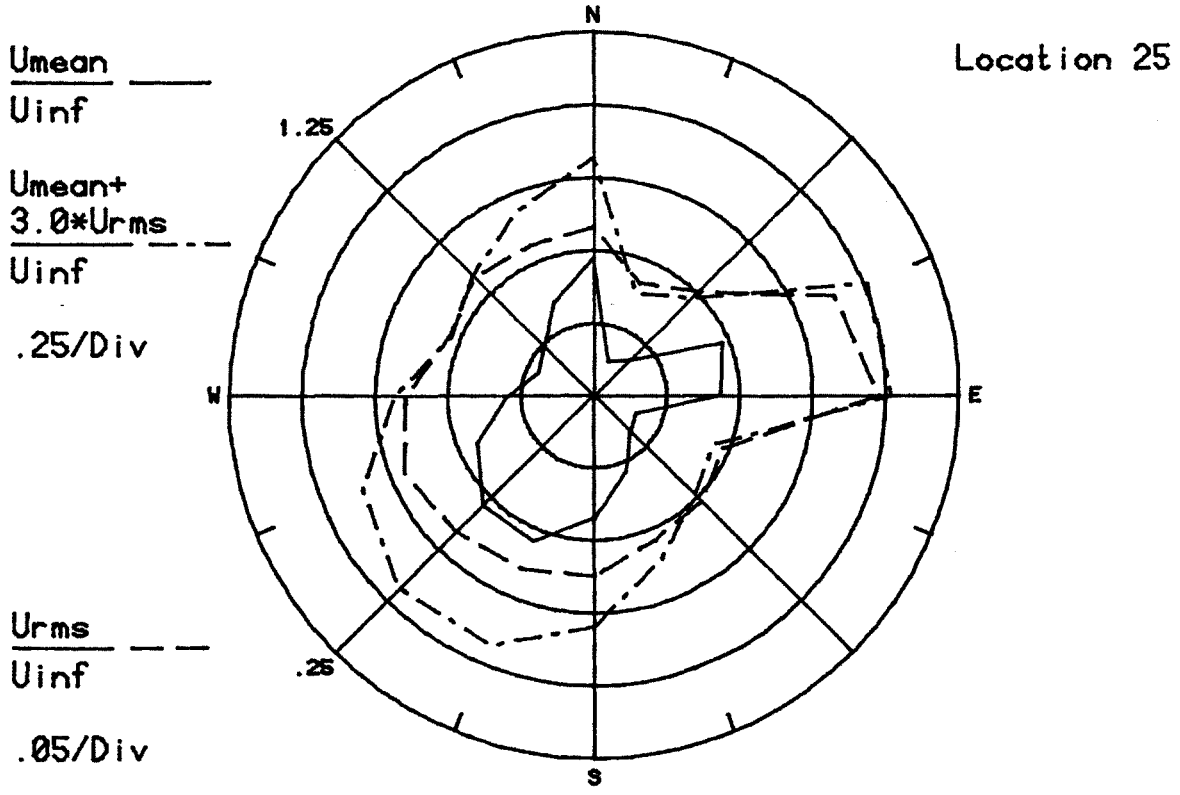


Figure 8v. Mean Velocities and Turbulence Intensities at Pedestrian Locations 23 and 24

TOWER II IN PLACE

CONFIGURATION G



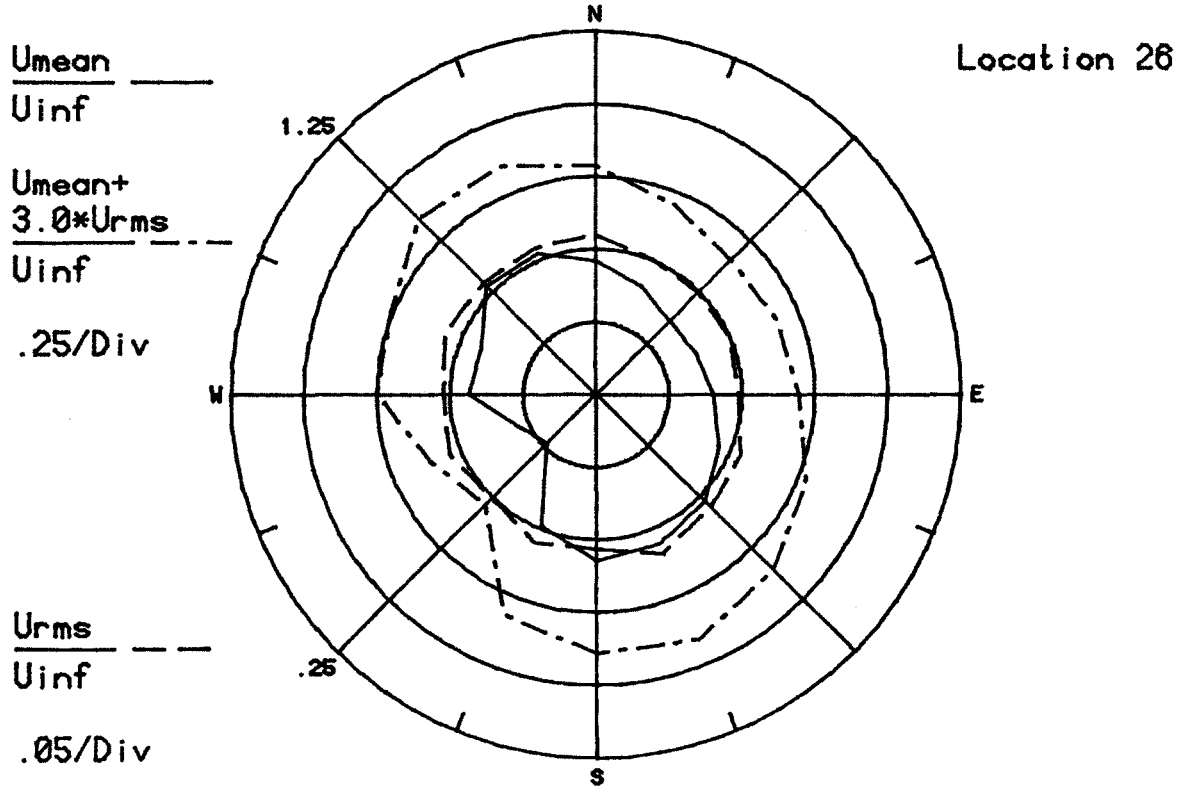
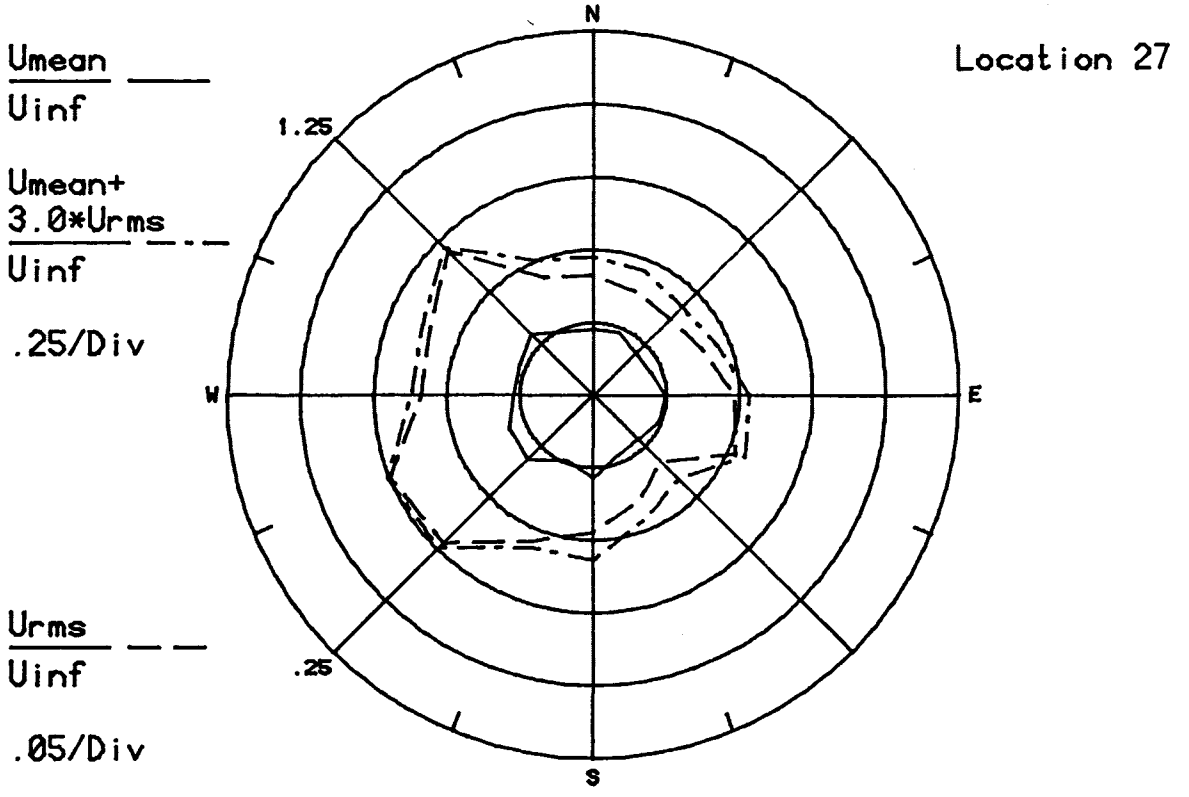


Figure 8w. Mean Velocities and Turbulence Intensities at Pedestrian Locations 25 and 26

TOWER II IN PLACE

CONFIGURATION G



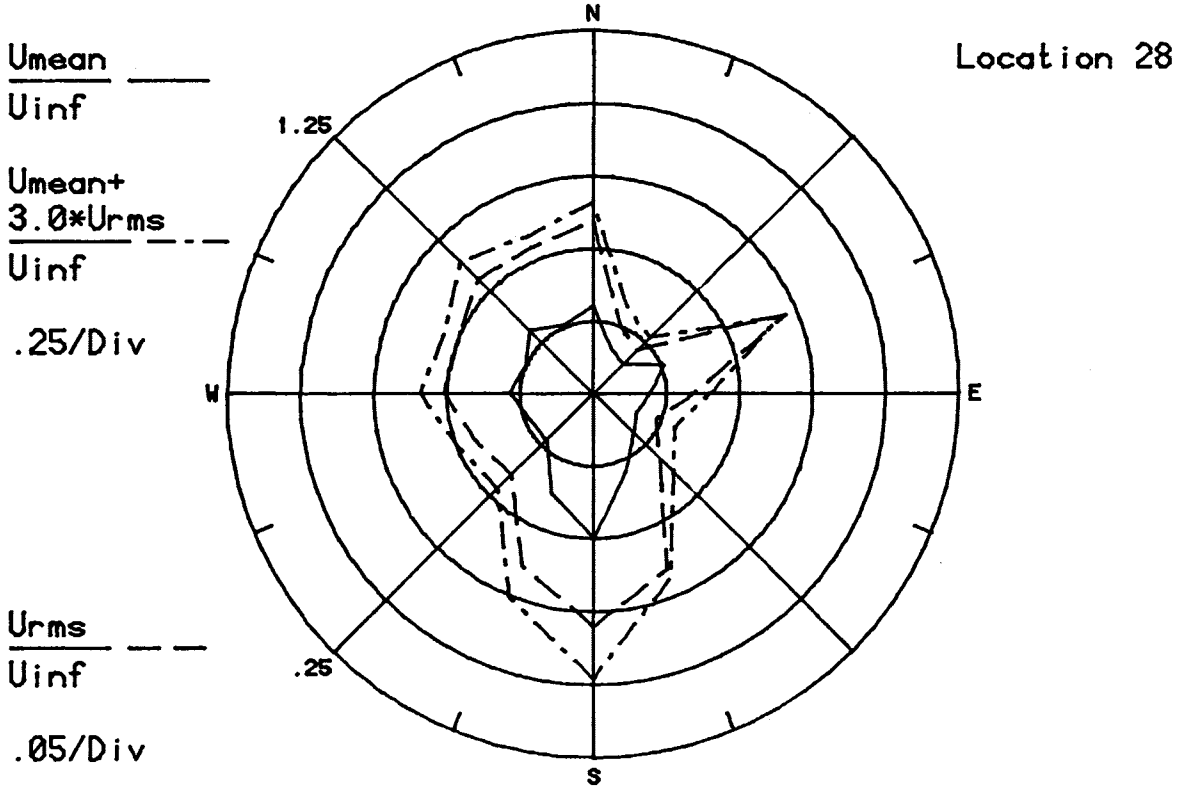


Figure 8x. Mean Velocities and Turbulence Intensities at Pedestrian Locations 27 and 28

TOWER II IN PLACE

CONFIGURATION G

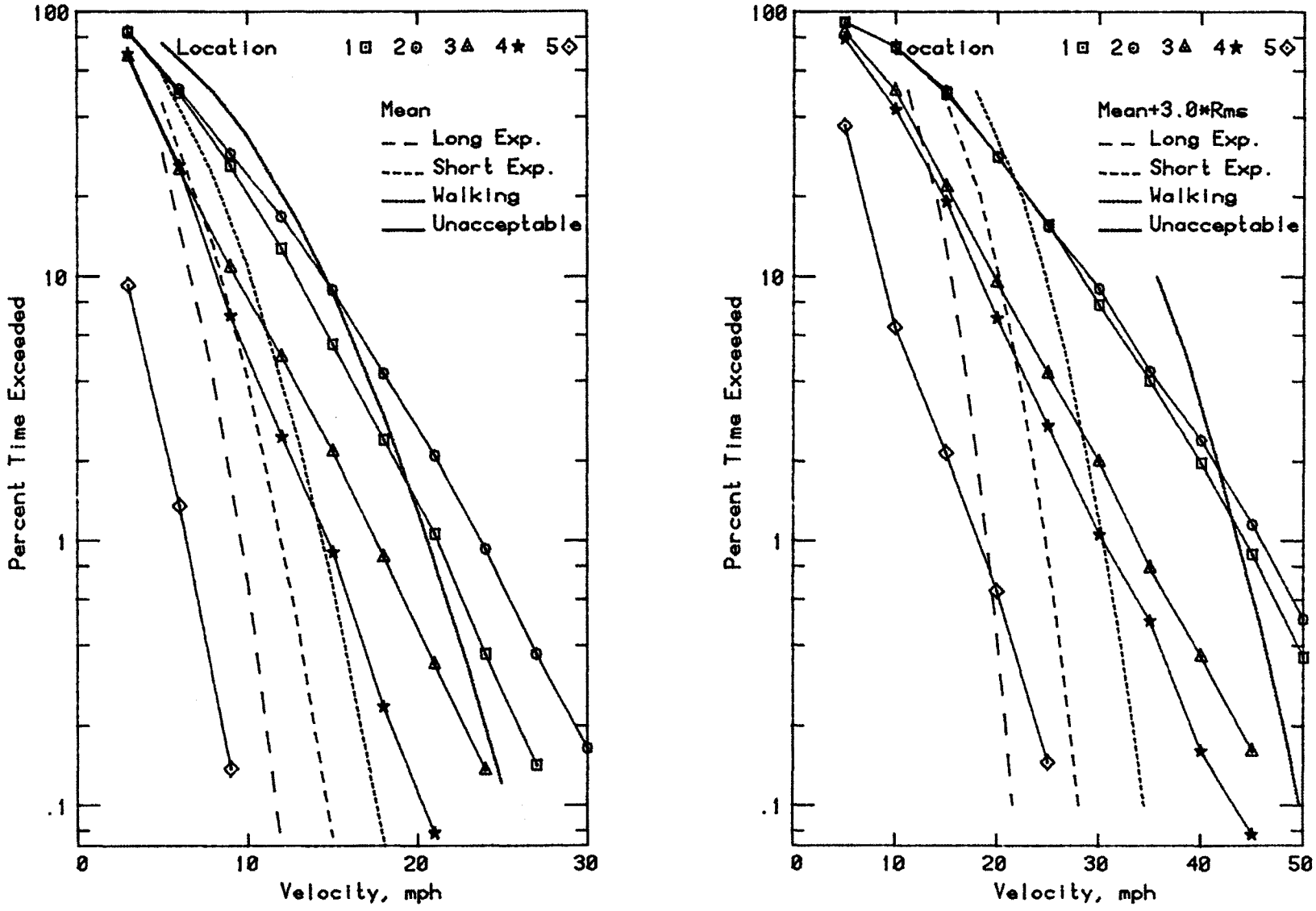


Figure 9a. Wind Velocity Probabilities for Pedestrian Locations

TOWER II OUT

CONFIGURATION H

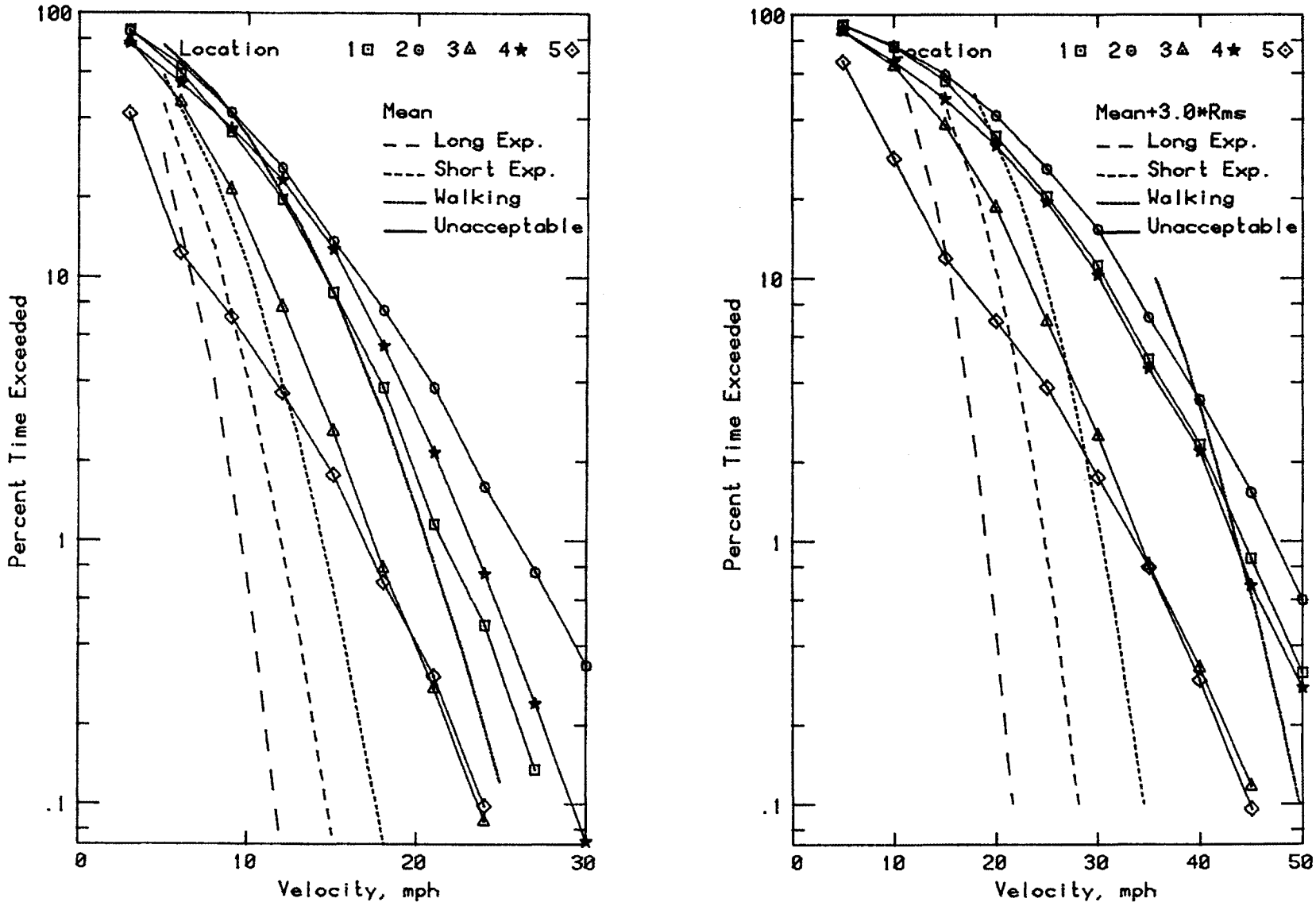


Figure 9b. Wind Velocity Probabilities for Pedestrian Locations

TOWER II IN PLACE
CONFIGURATION G

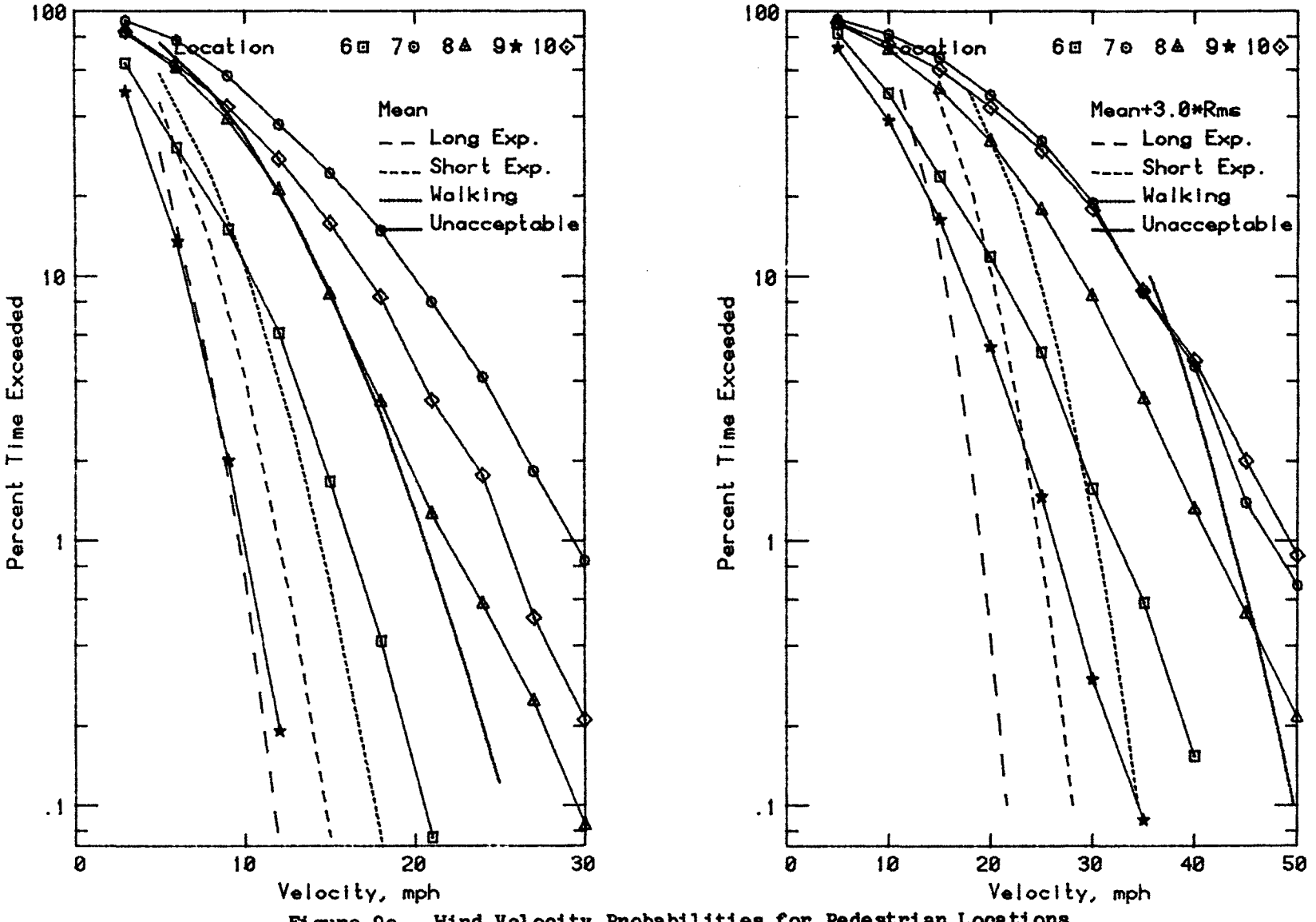


Figure 9c. Wind Velocity Probabilities for Pedestrian Locations

TOWER II OUT

CONFIGURATION H

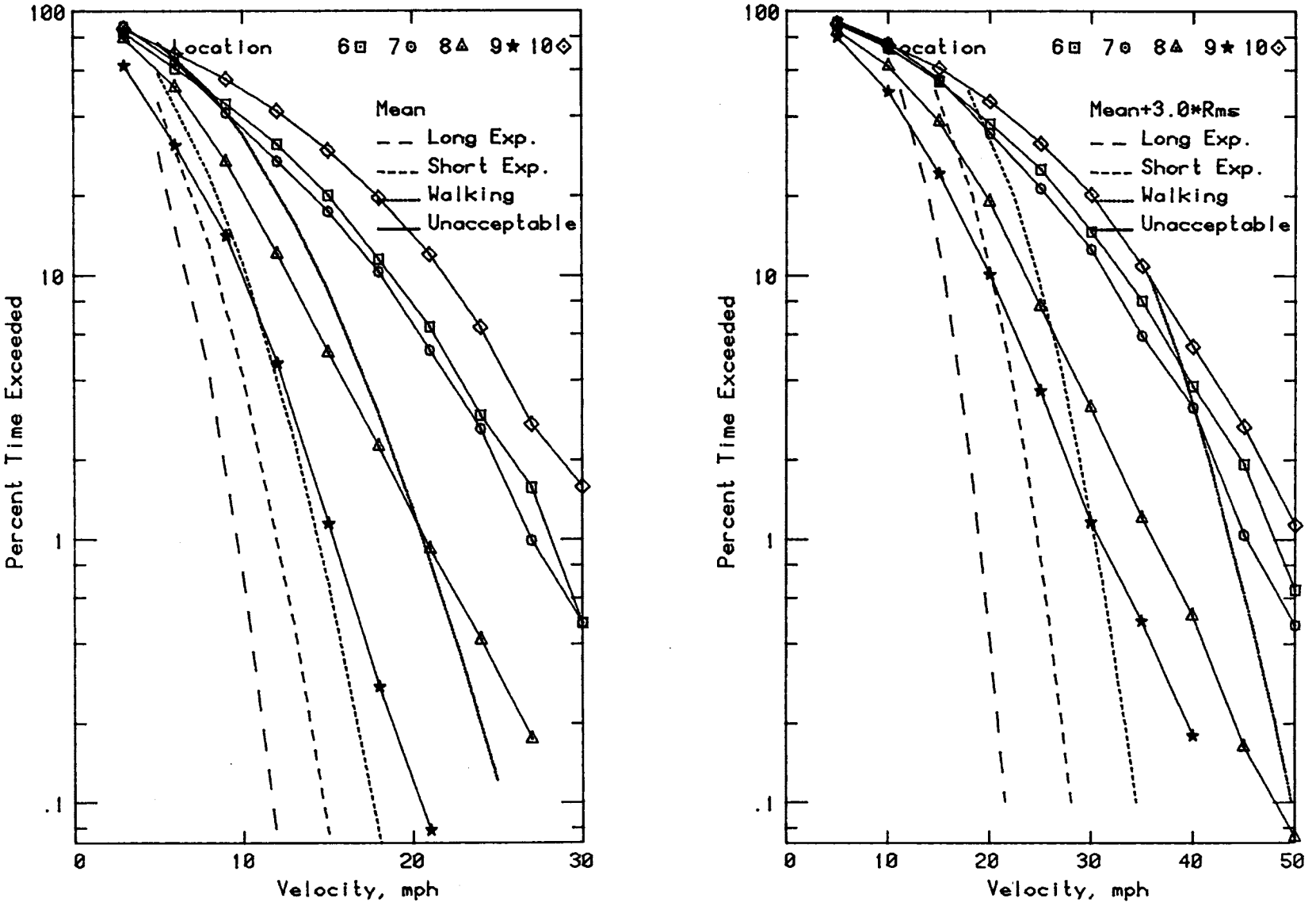


Figure 9d. Wind Velocity Probabilities for Pedestrian Locations

TOWER II IN PLACE

CONFIGURATION G

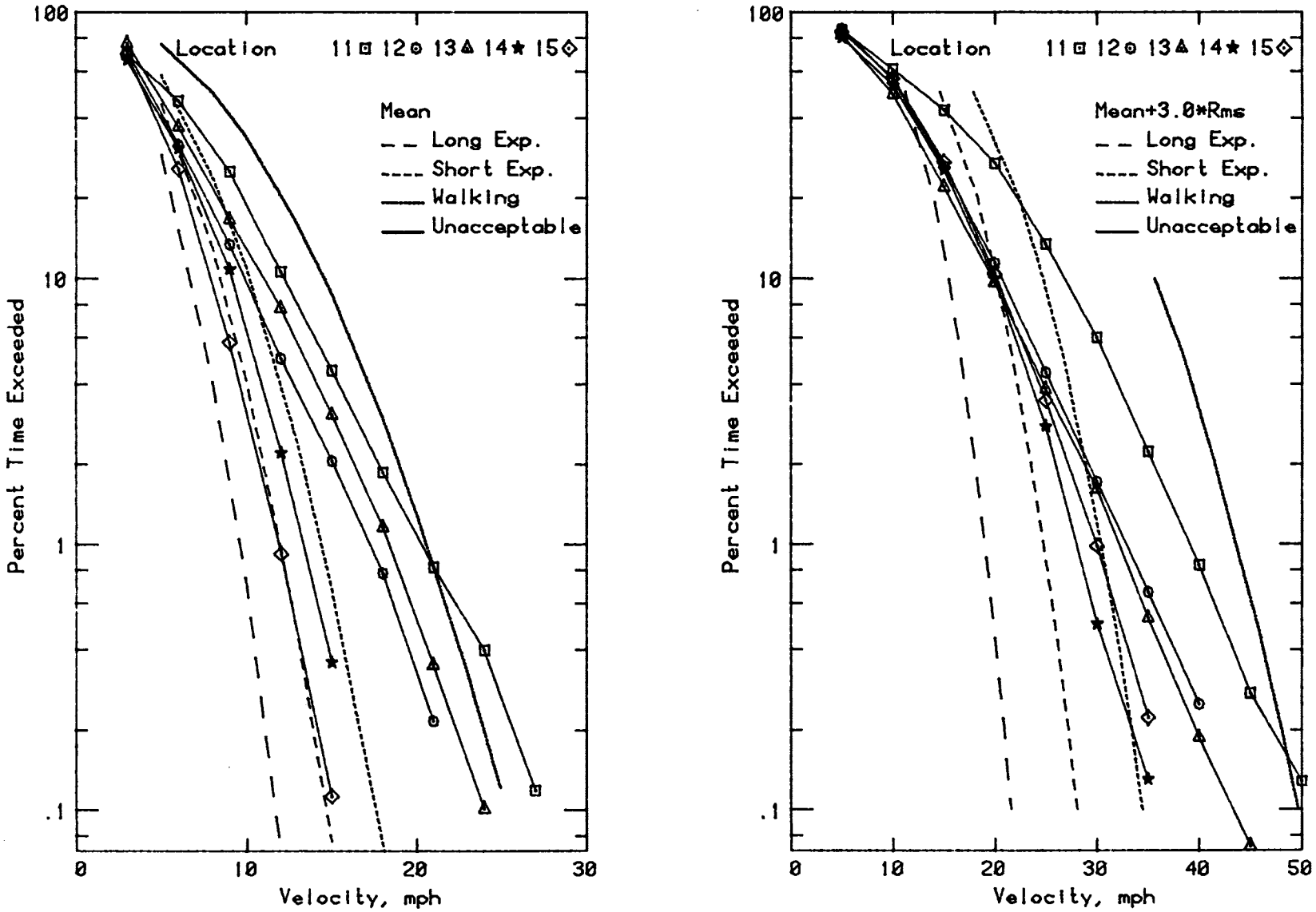


Figure 9e. Wind Velocity Probabilities for Pedestrian Locations

TOWER II OUT

CONFIGURATION H

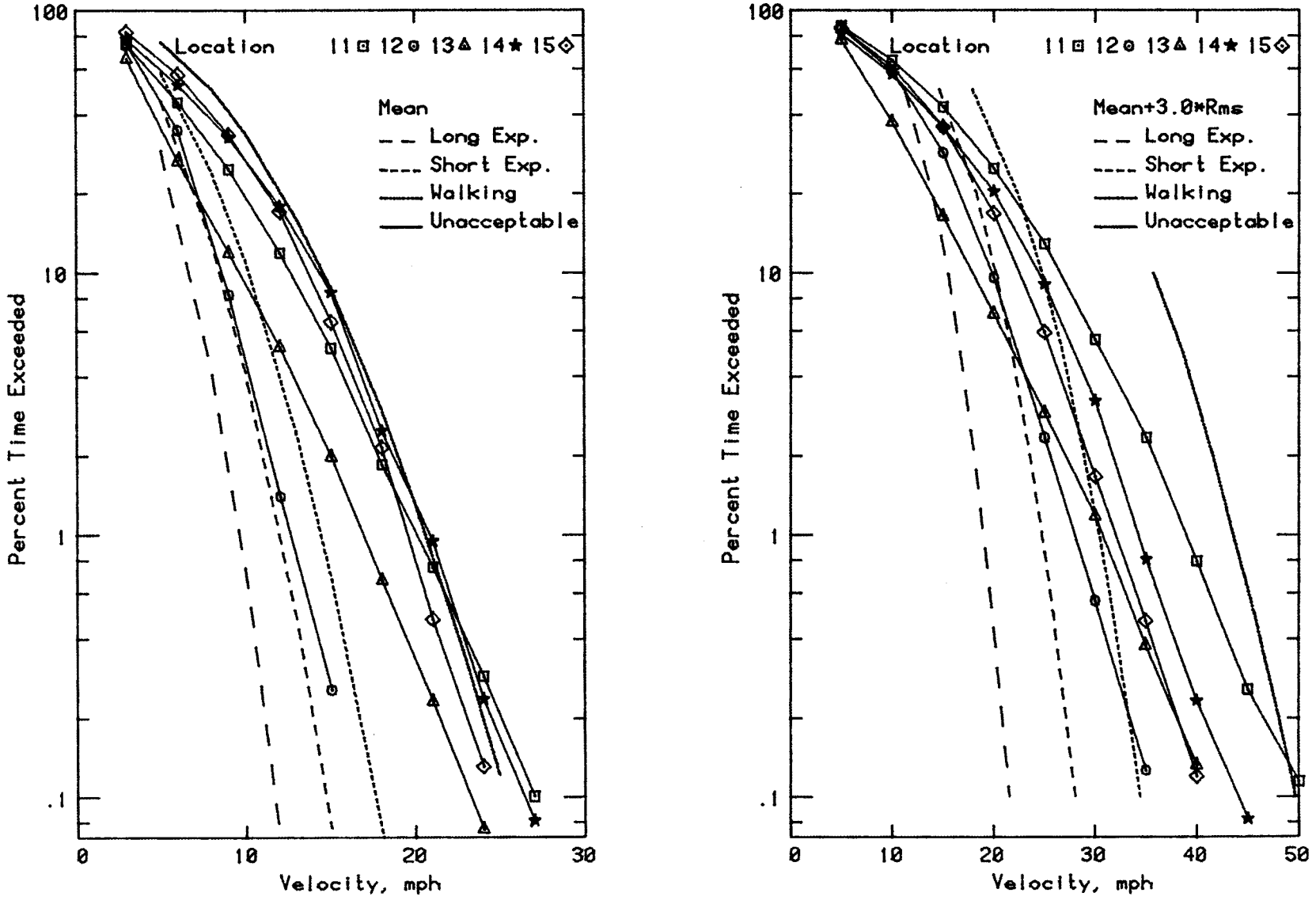


Figure 9f. Wind Velocity Probabilities for Pedestrian Locations

TOWER II IN PLACE

CONFIGURATION G

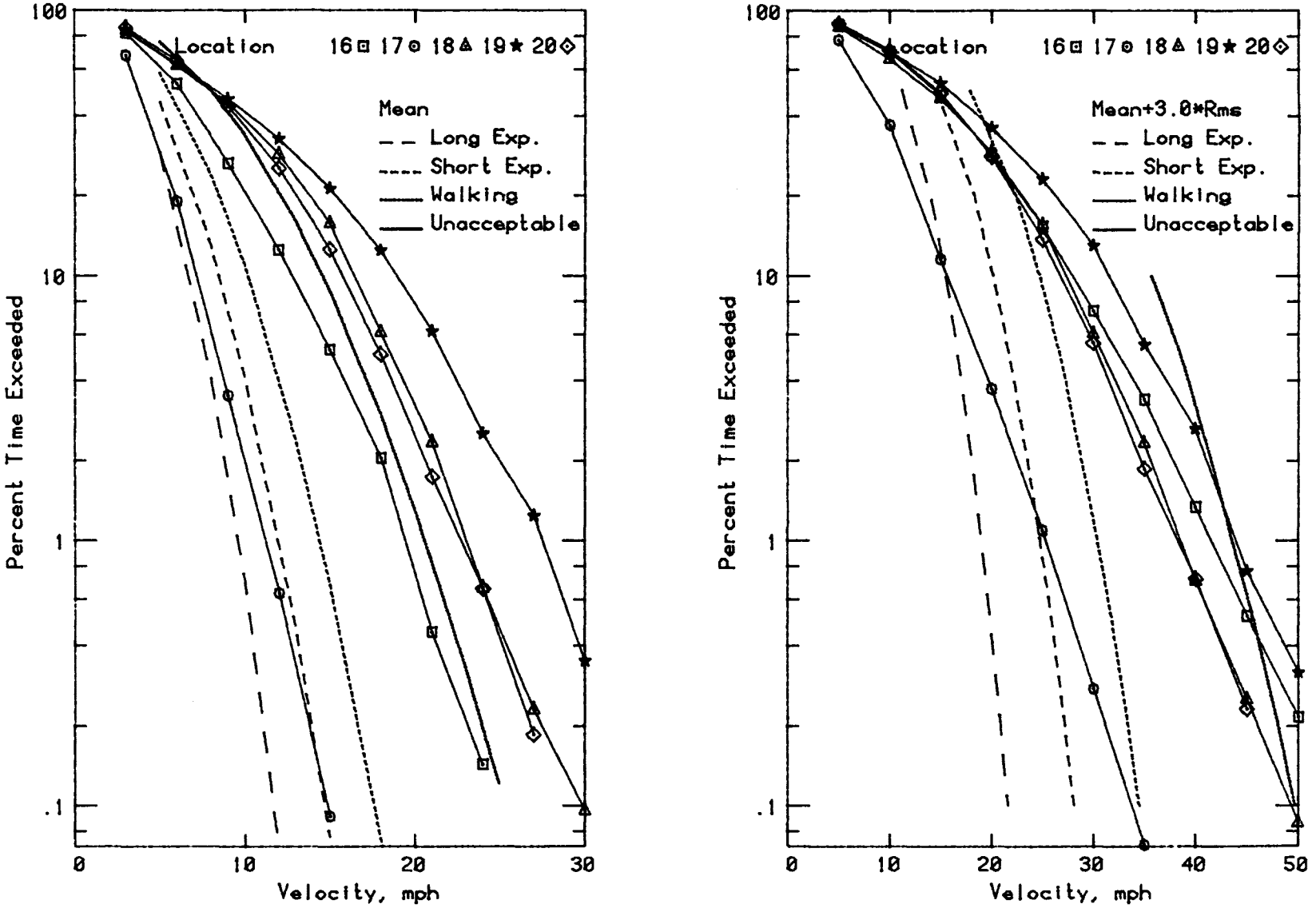


Figure 9g. Wind Velocity Probabilities for Pedestrian Locations

TOWER II OUT
CONFIGURATION H

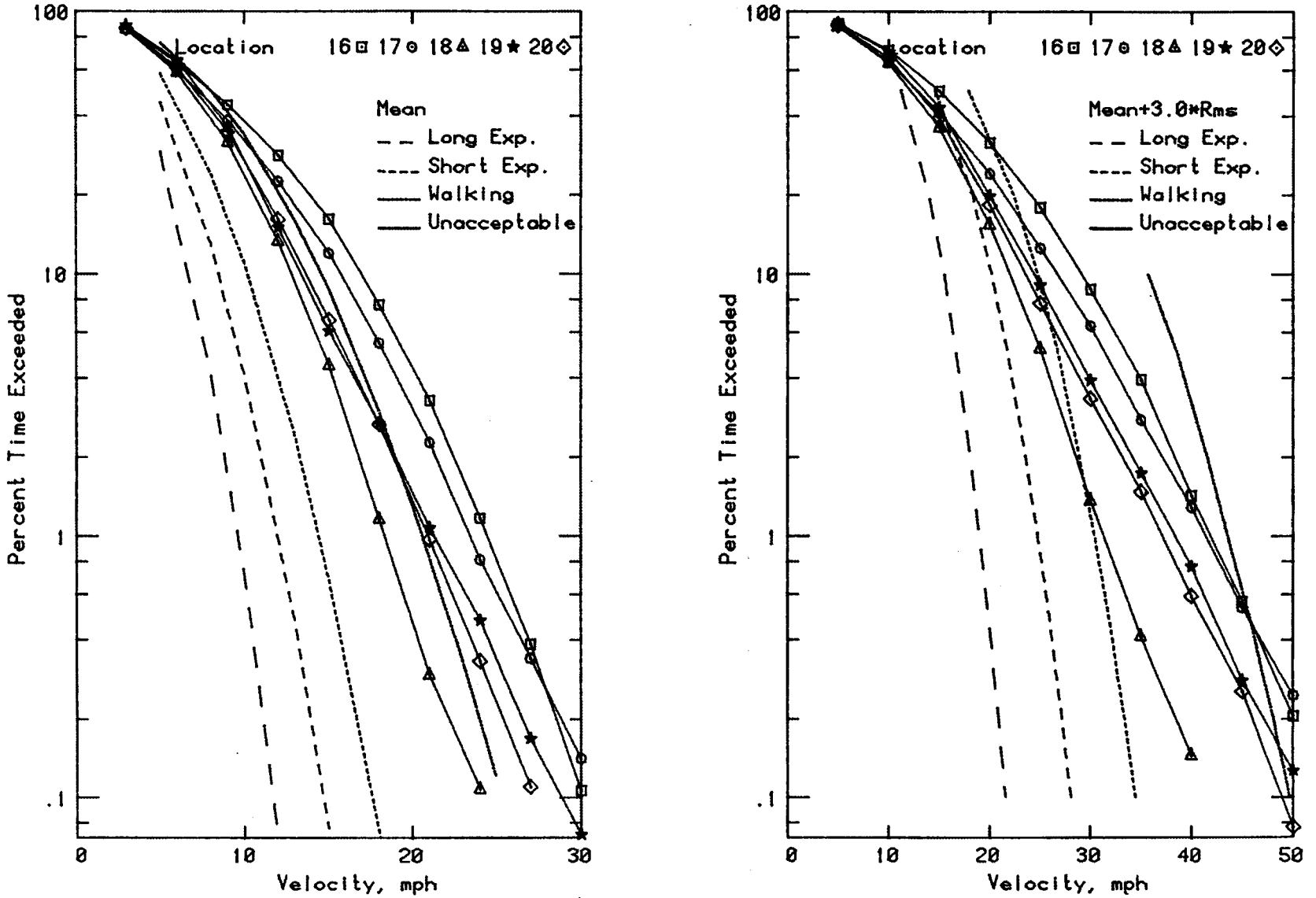


Figure 9h. Wind Velocity Probabilities for Pedestrian Locations

TOWER II IN PLACE

CONFIGURATION G

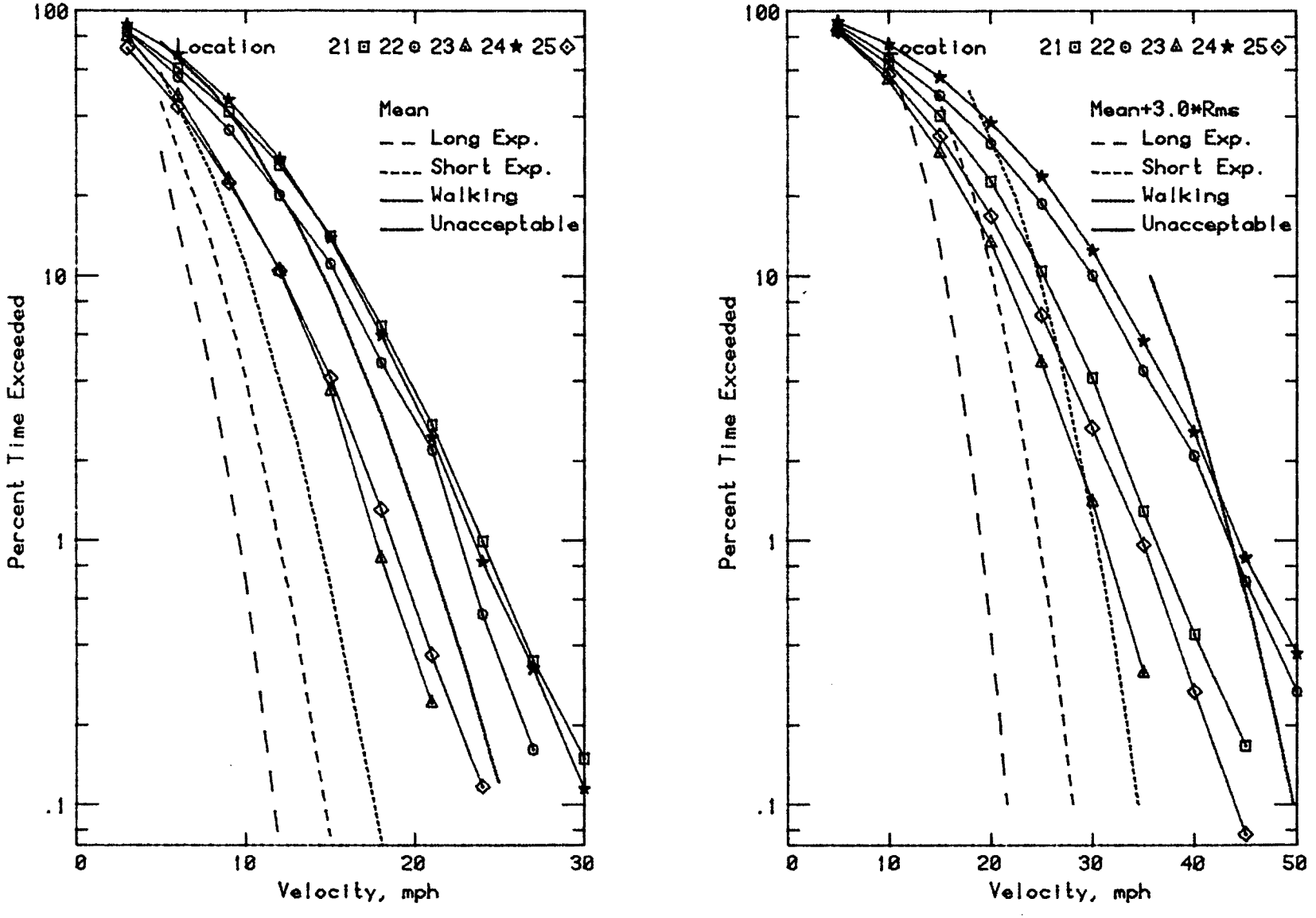


Figure 9i. Wind Velocity Probabilities for Pedestrian Locations

TOWER II OUT

CONFIGURATION G

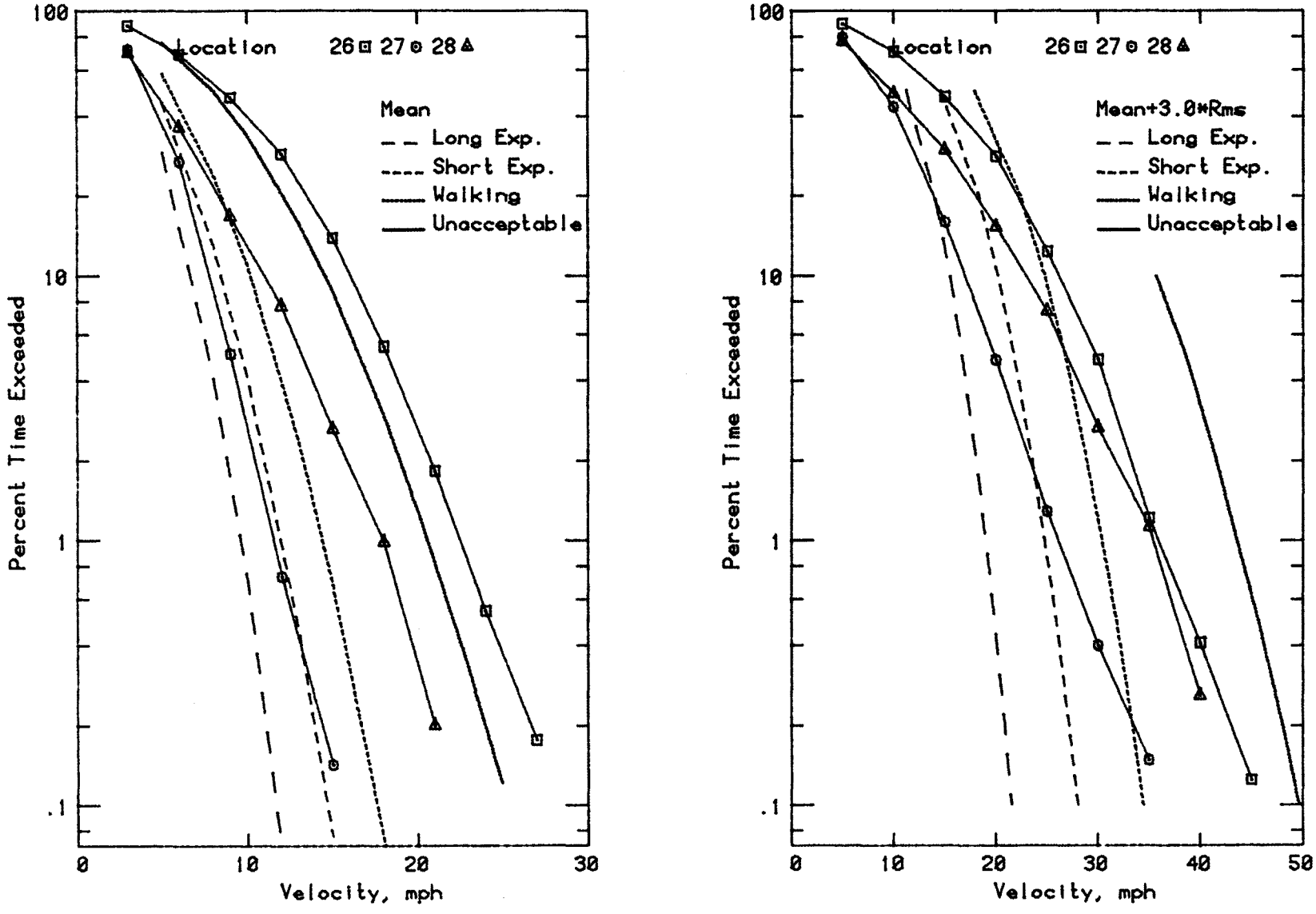
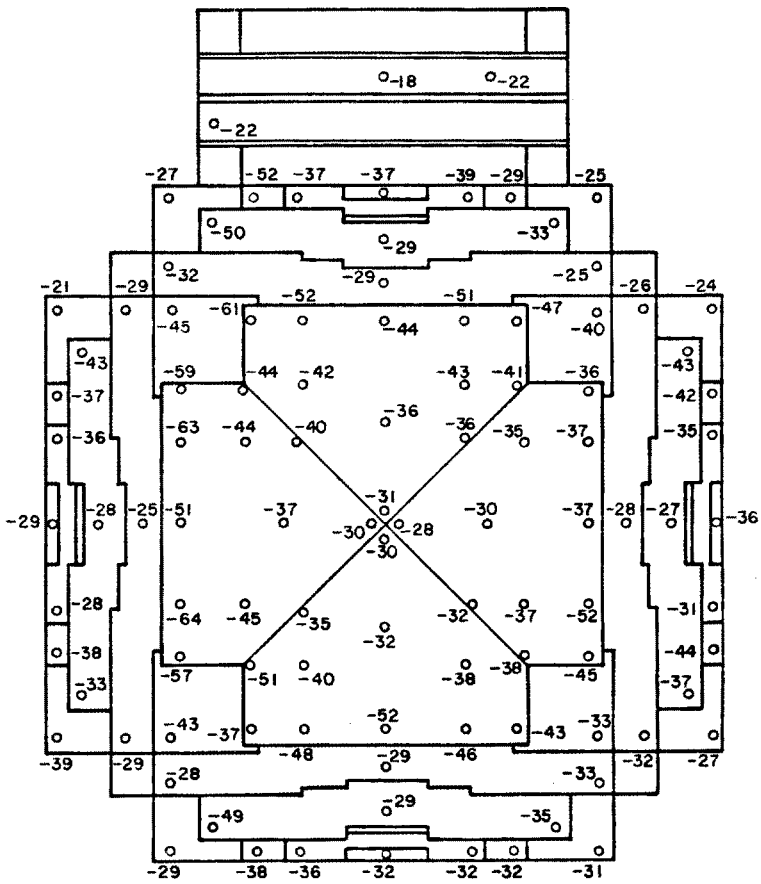


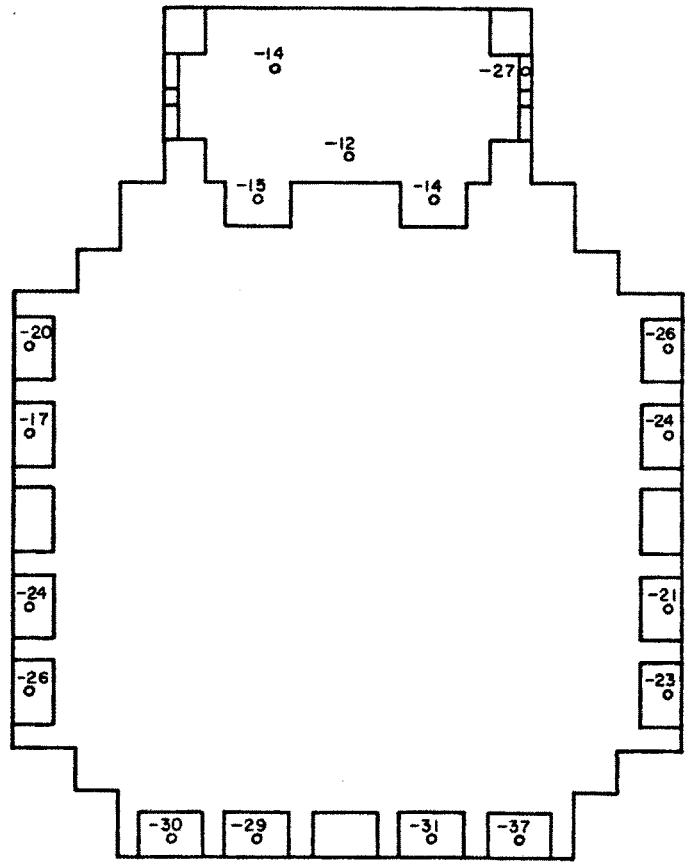
Figure 9j. Wind Velocity Probabilities for Pedestrian Locations



TOWER I

ROOF
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
NEGATIVE LOADS ACT OUTWARD
WORST CASE OF CONFIGURATIONS A AND B

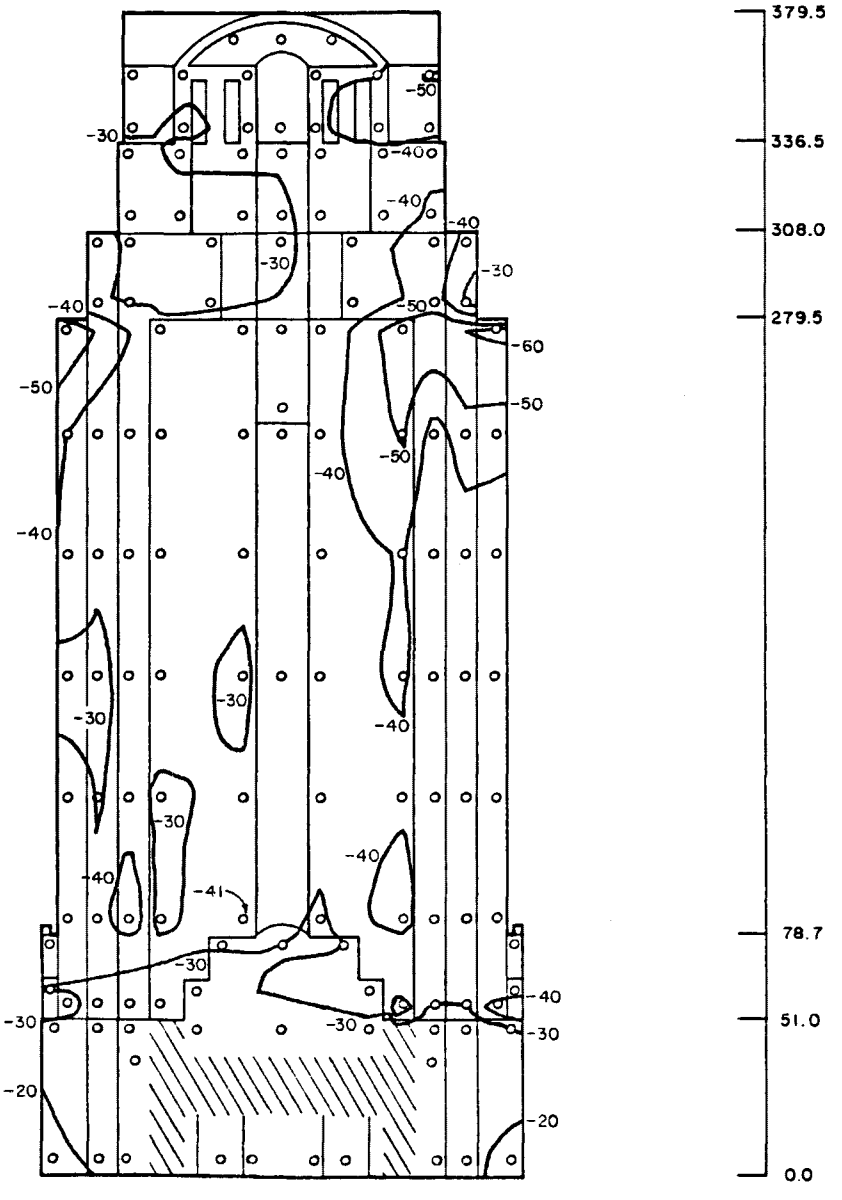
Figure 10a. Peak Pressure Contours on the Building for Cladding Loads



TOWER I

SOFFIT
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
NEGATIVE LOADS ACT OUTWARD
WORST CASE OF CONFIGURATIONS A AND B

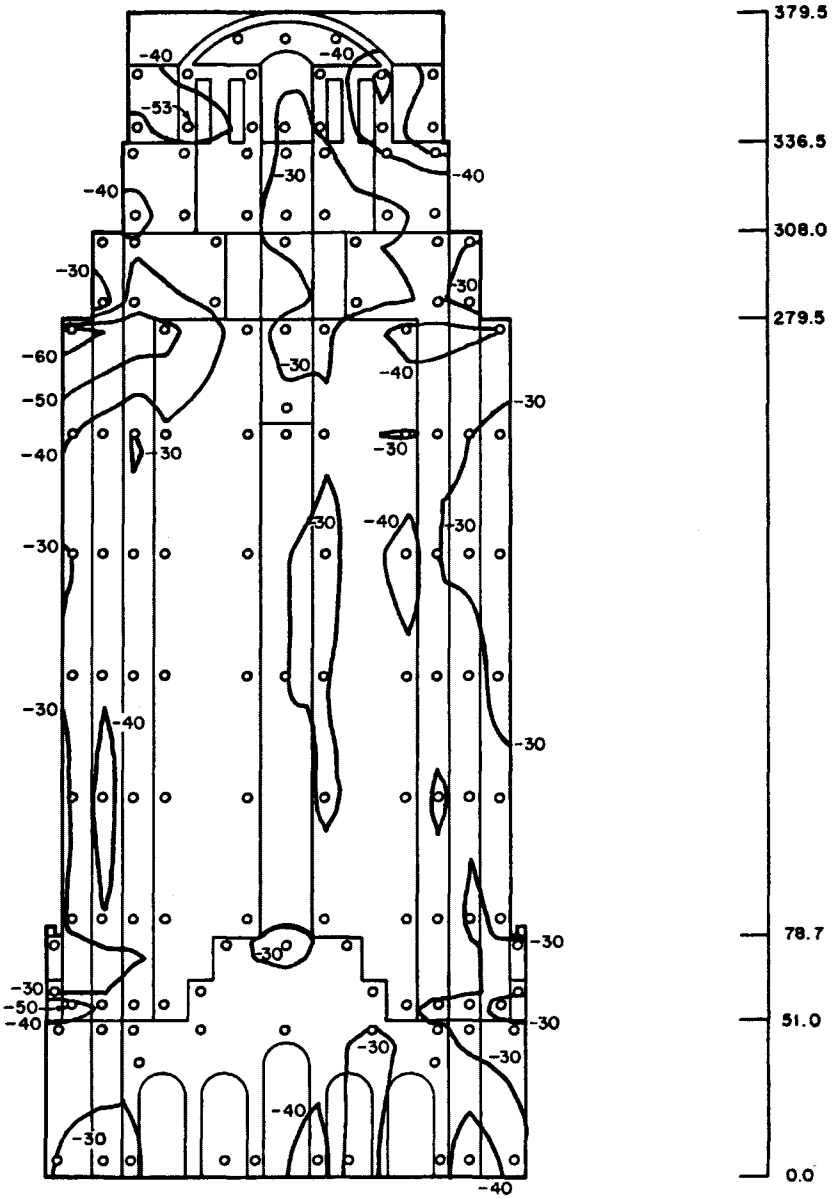
Figure 10b. Peak Pressure Contours on the Building for Cladding Loads



TOWER I

NORTH ELEVATION
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
NEGATIVE LOADS ACT OUTWARD
WORST CASE OF CONFIGURATIONS A AND B

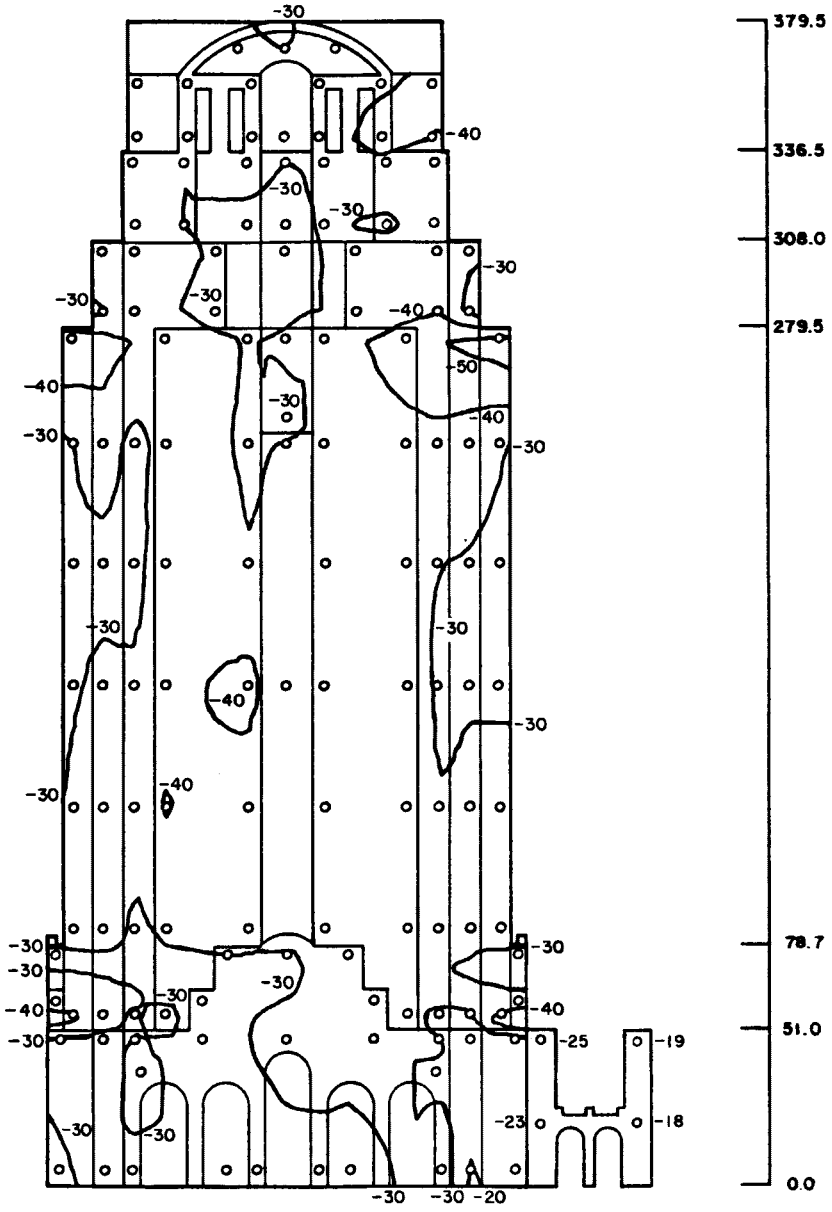
Figure 10c. Peak Pressure Contours on the Building for Cladding Loads



TOWER I

SOUTH ELEVATION
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
NEGATIVE LOADS ACT OUTWARD
WORST CASE OF CONFIGURATIONS A AND B

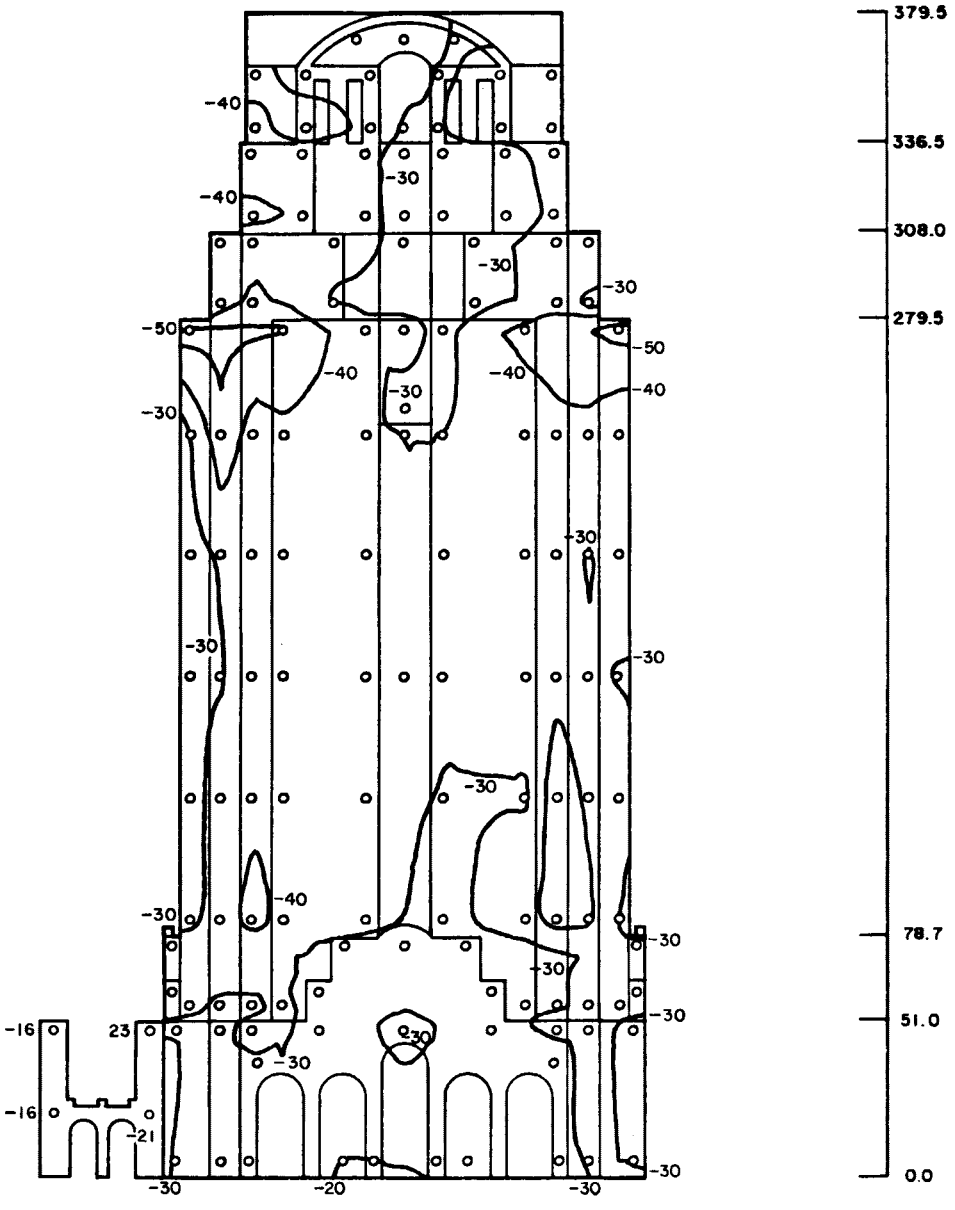
Figure 10d. Peak Pressure Contours on the Building for Cladding Loads



TOWER I

EAST ELEVATION
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
NEGATIVE LOADS ACT OUTWARD
WORST CASE OF CONFIGURATIONS A AND B

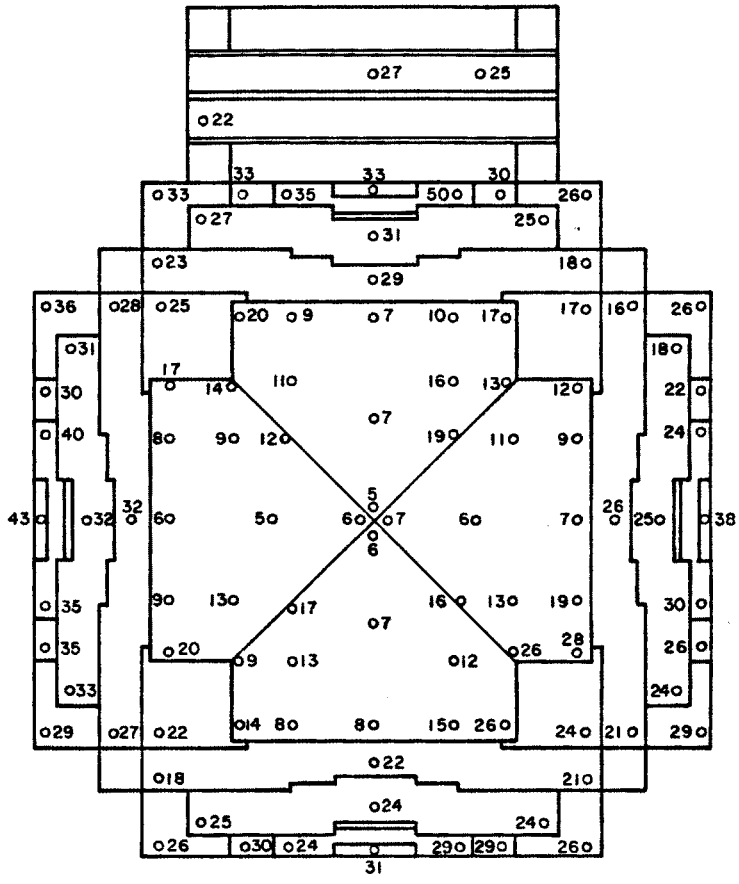
Figure 10e. Peak Pressure Contours on the Building for Cladding Loads



TOWER I

WEST ELEVATION
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
NEGATIVE LOADS ACT OUTWARD
WORST CASE OF CONFIGURATIONS A AND B

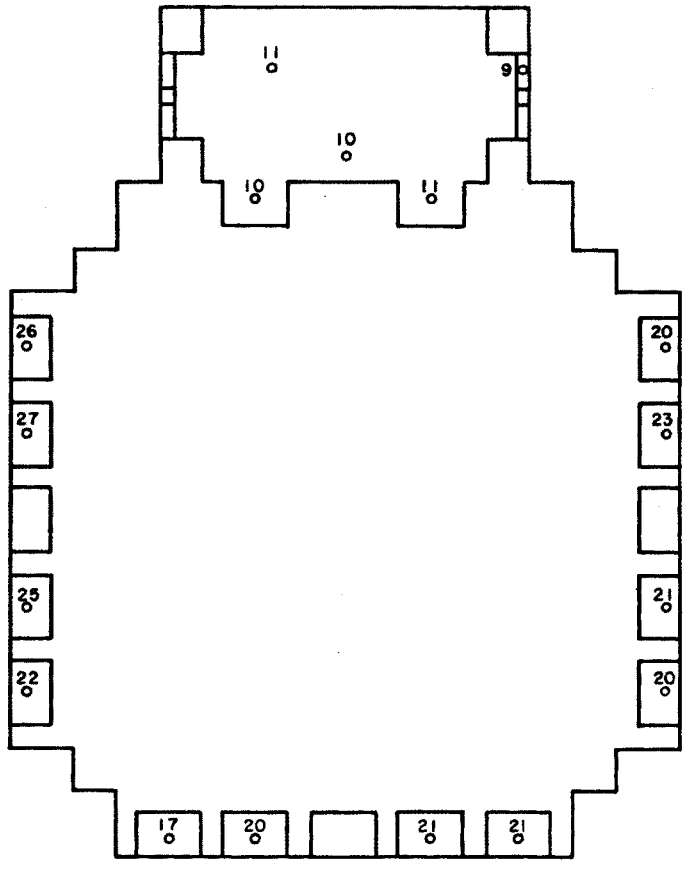
Figure 10f. Peak Pressure Contours on the Building for Cladding Loads



TOWER I

ROOF
PEAK POSITIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
POSITIVE LOADS ACT INWARD
WORST CASE OF CONFIGURATIONS A AND B

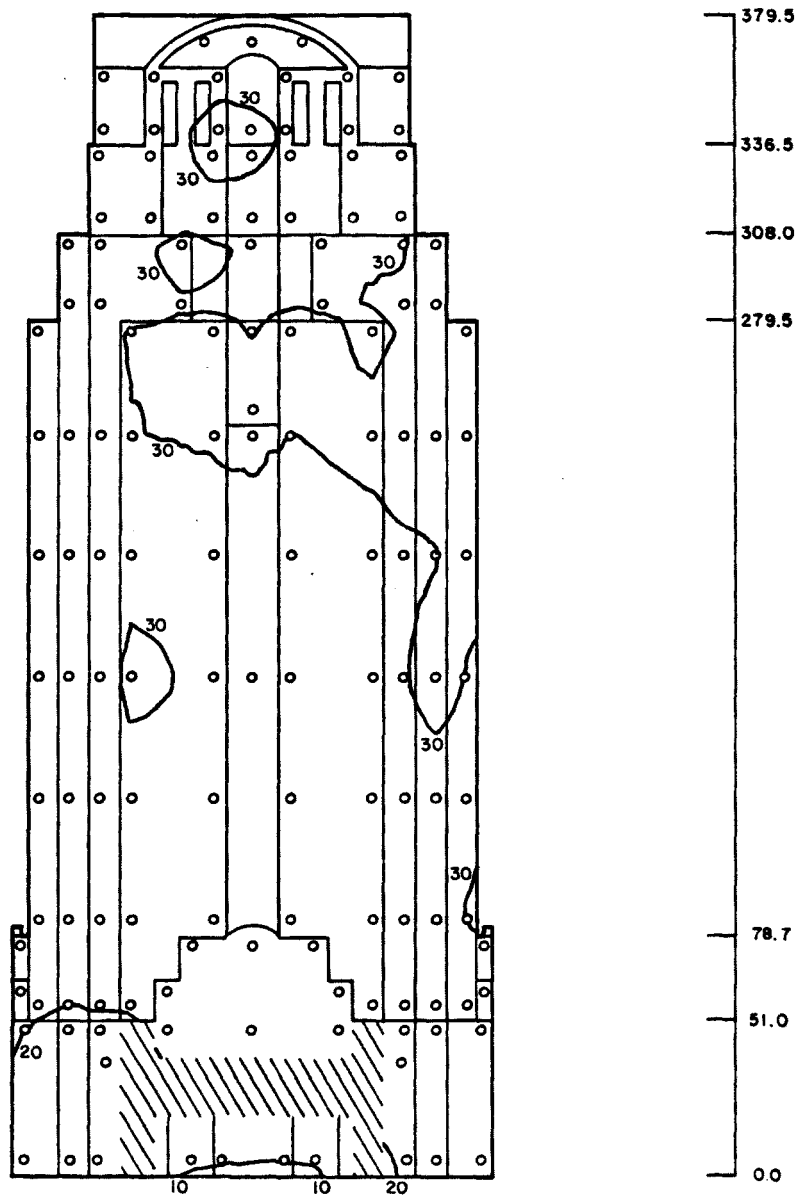
Figure 10g. Peak Pressure Contours on the Building for Cladding Loads



TOWER I

SOFFIT
PEAK POSITIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
POSITIVE LOADS ACT INWARD
WORST CASE OF CONFIGURATIONS A AND B

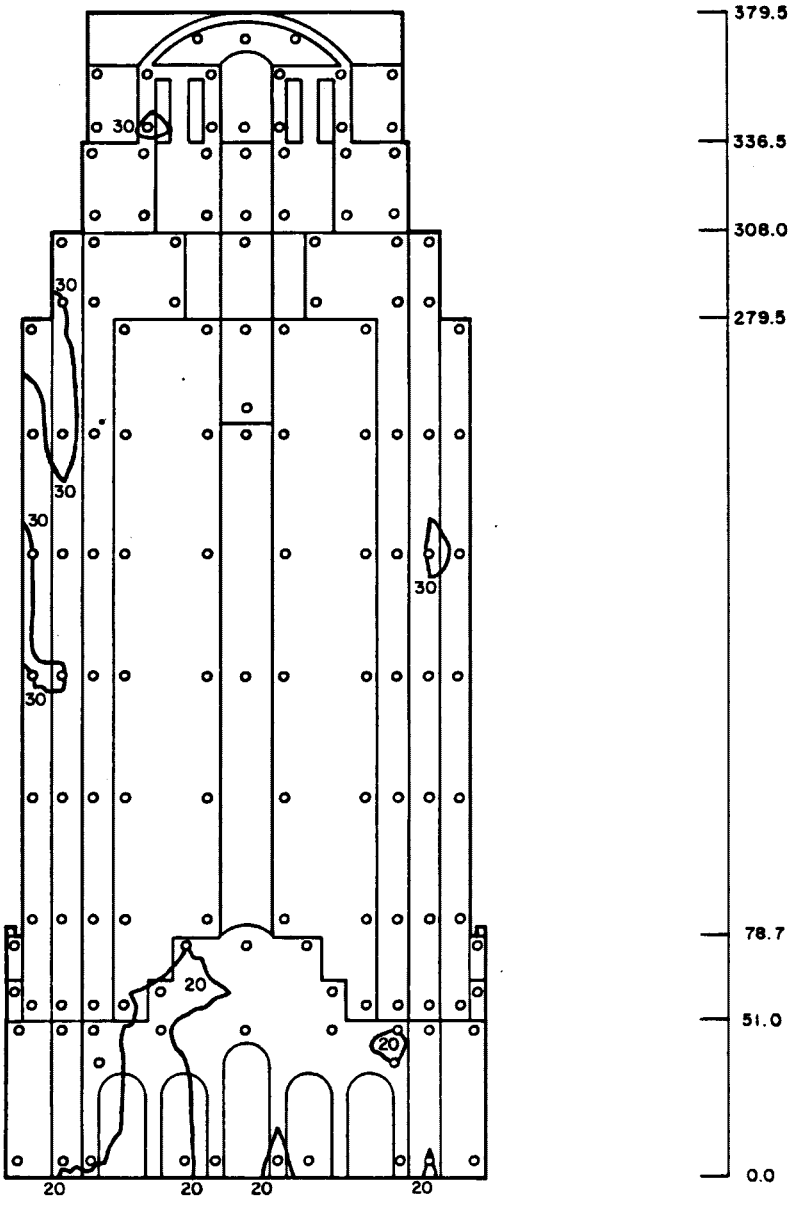
Figure 10h. Peak Pressure Contours on the Building for Cladding Loads



TOWER I

NORTH ELEVATION
PEAK POSITIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
POSITIVE LOADS ACT INWARD
WORST CASE OF CONFIGURATIONS A AND B

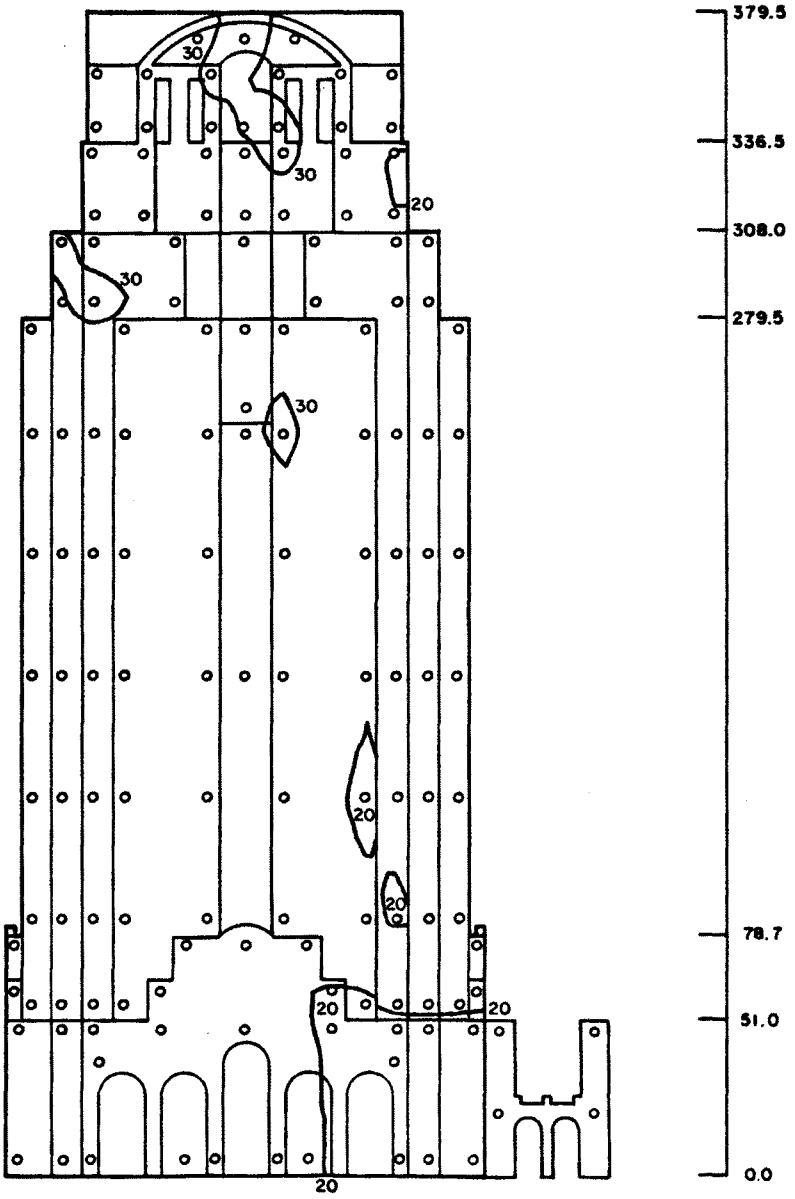
Figure 10i. Peak Pressure Contours on the Building for Cladding Loads



TOWER I

SOUTH ELEVATION
PEAK POSITIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
POSITIVE LOADS ACT INWARD
WORST CASE OF CONFIGURATIONS A AND B

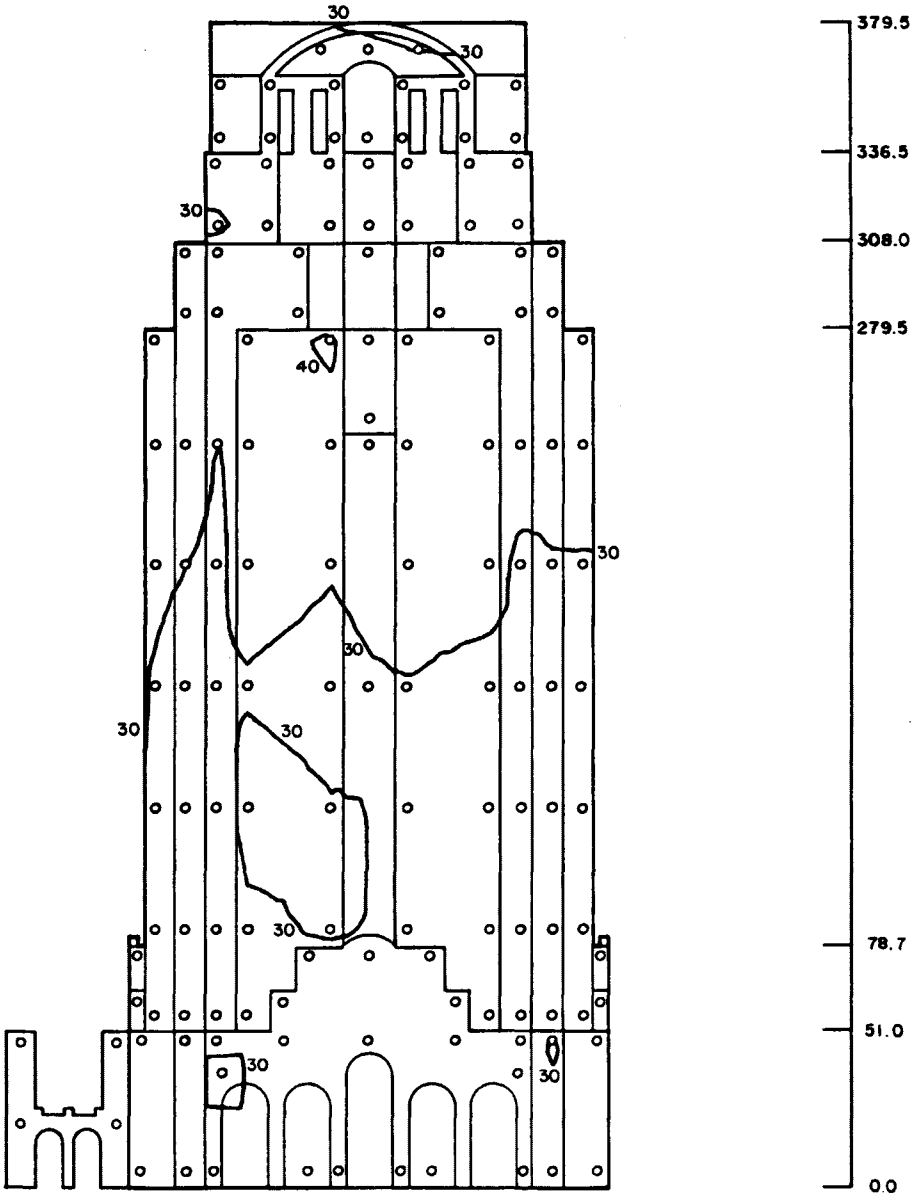
Figure 10j. Peak Pressure Contours on the Building for Cladding Loads



TOWER I

EAST ELEVATION
PEAK POSITIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
POSITIVE LOADS ACT INWARD
WORST CASE OF CONFIGURATIONS A AND B

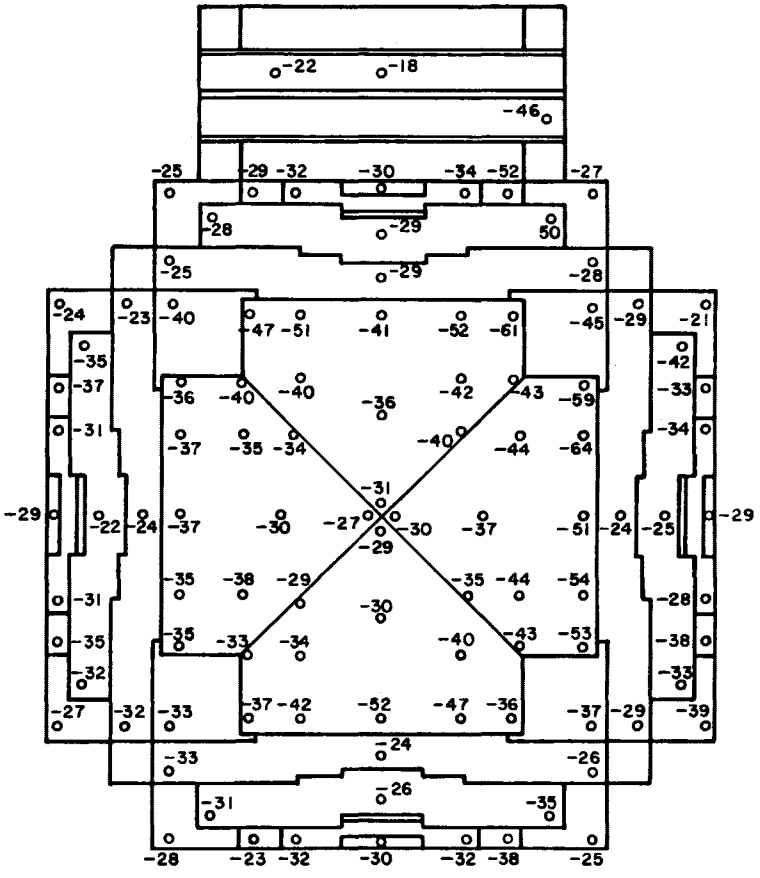
Figure 10k. Peak Pressure Contours on the Building for Cladding Loads



TOWER I

WEST ELEVATION
PEAK POSITIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
POSITIVE LOADS ACT INWARD
WORST CASE OF CONFIGURATIONS A AND B

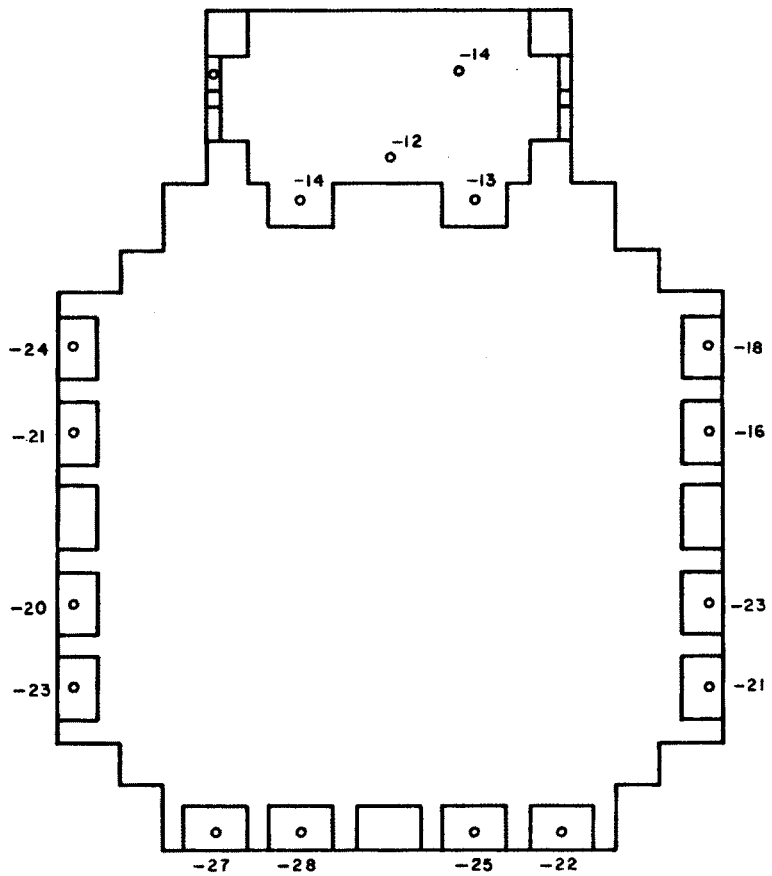
Figure 101. Peak Pressure Contours on the Building for Cladding Loads



<u>Tower II</u>

ROOF
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
NEGATIVE LOADS ACT OUTWARD

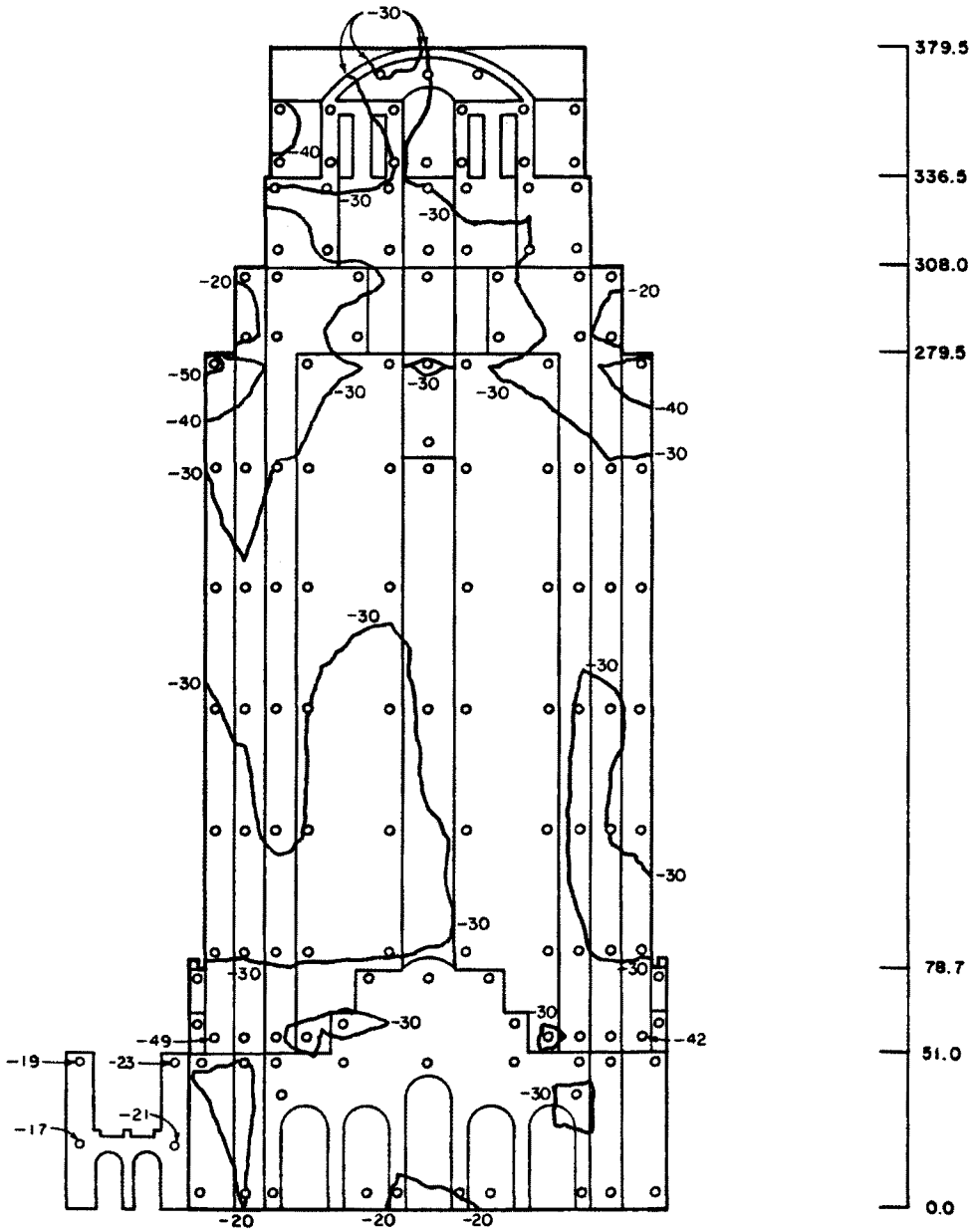
Figure 10m. Peak Pressure Contours on the Building for Cladding Loads



Tower II

SOFFIT
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
NEGATIVE LOADS ACT OUTWARD

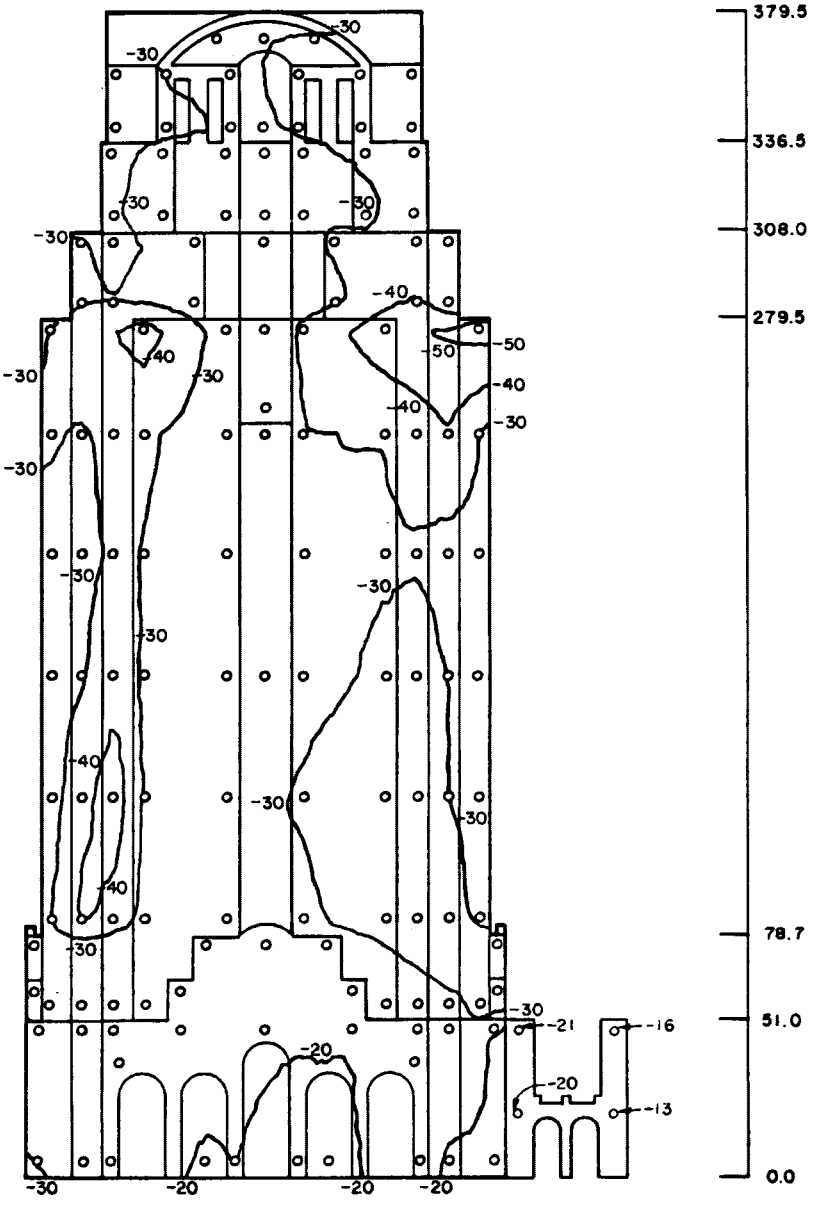
Figure 10n. Peak Pressure Contours on the Building for Cladding Loads



Tower II

NORTH
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
NEGATIVE LOADS ACT OUTWARD

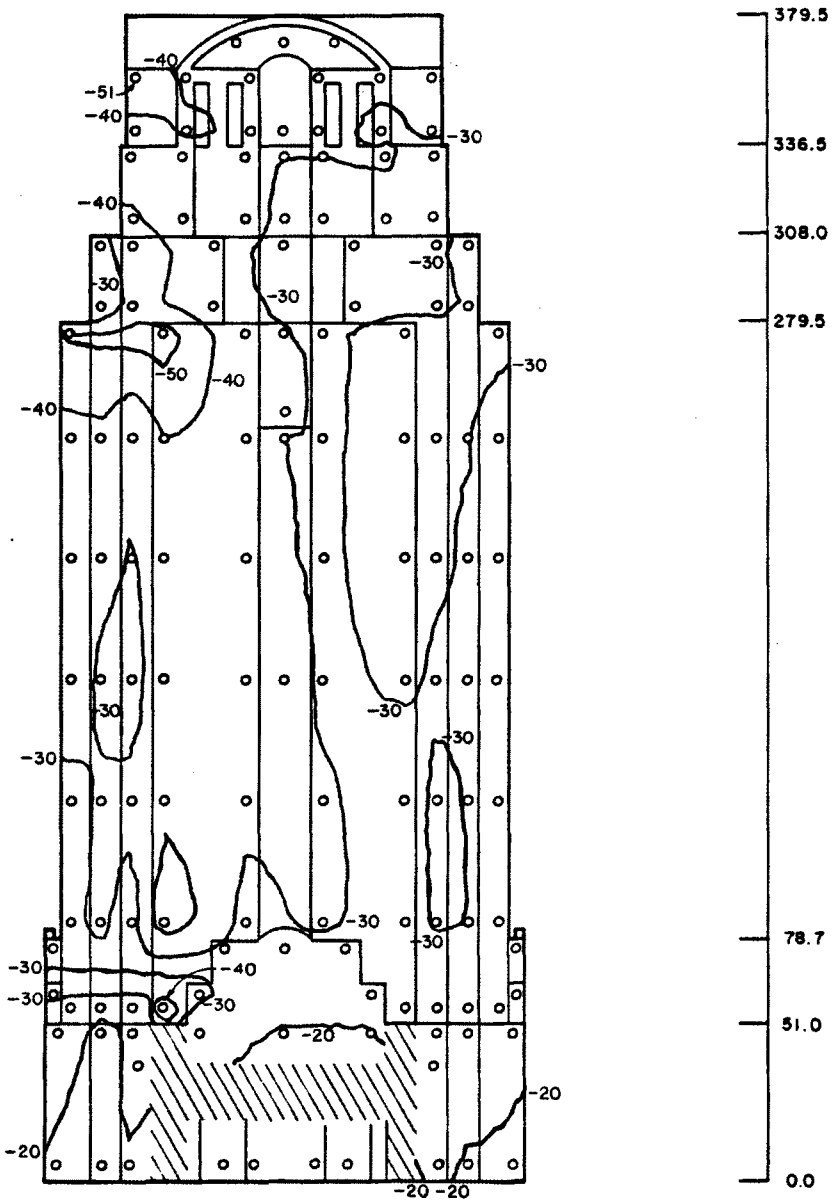
Figure 10o. Peak Pressure Contours on the Building for Cladding Loads



Tower II

SOUTH
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
NEGATIVE LOADS ACT OUTWARD

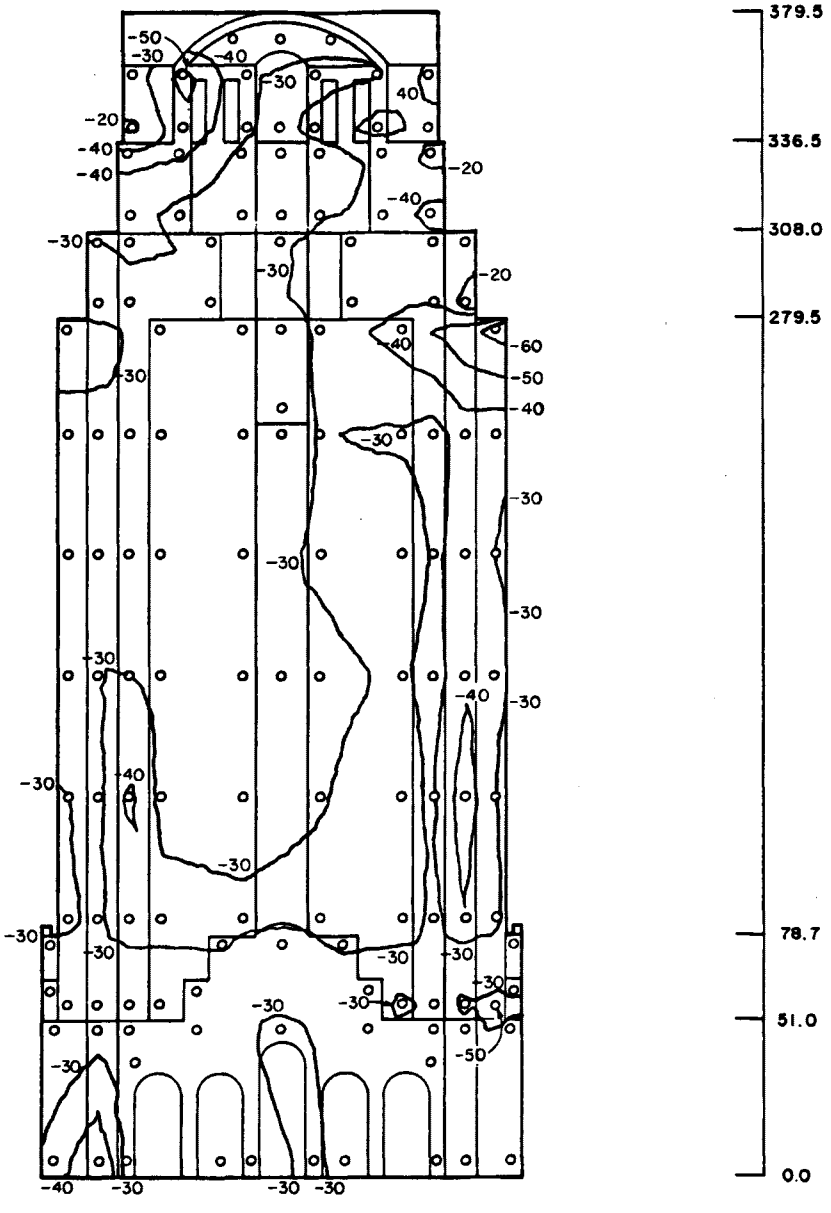
Figure 10p. Peak Pressure Contours on the Building for Cladding Loads



Tower II

EAST
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
NEGATIVE LOADS ACT OUTWARD

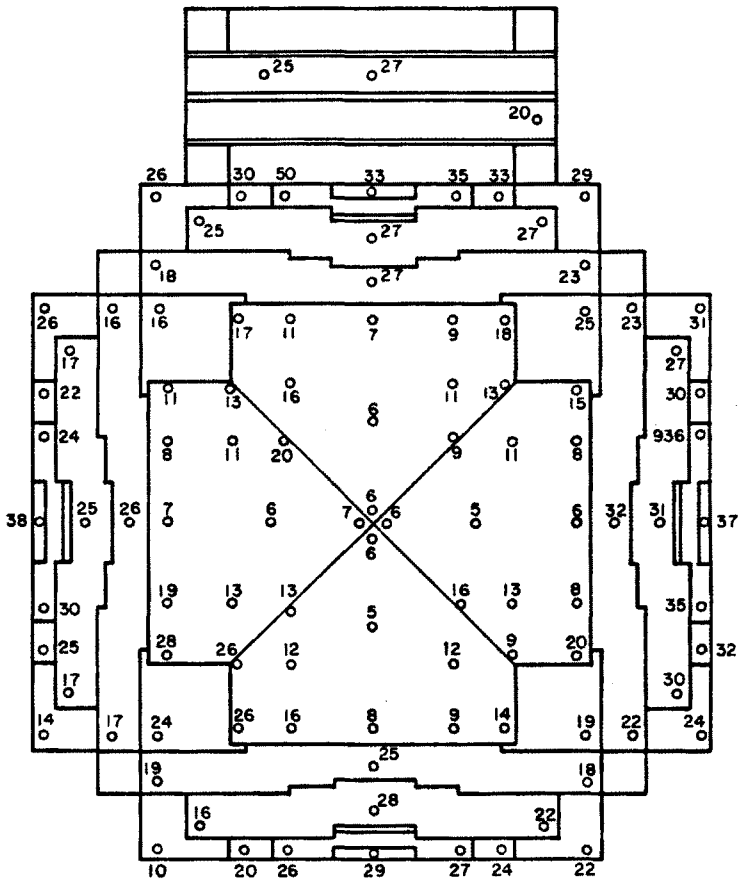
Figure 10q. Peak Pressure Contours on the Building for Cladding Loads



Tower II

WEST
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
NEGATIVE LOADS ACT OUTWARD

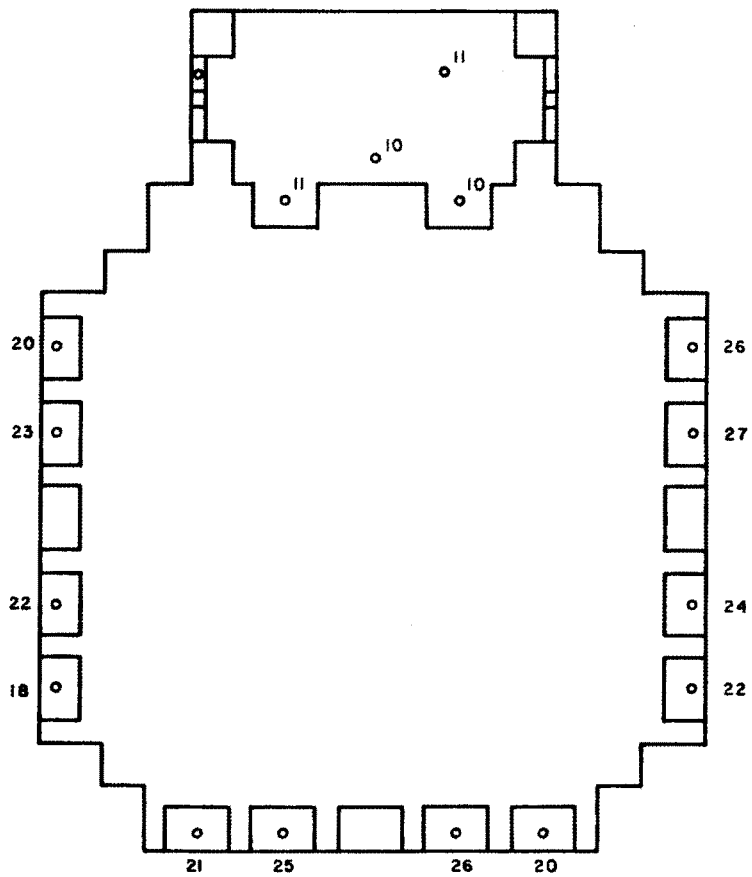
Figure 10r. Peak Pressure Contours on the Building for Cladding Loads



Tower II

ROOF
PEAK POSITIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
POSITIVE LOADS ACT INWARD

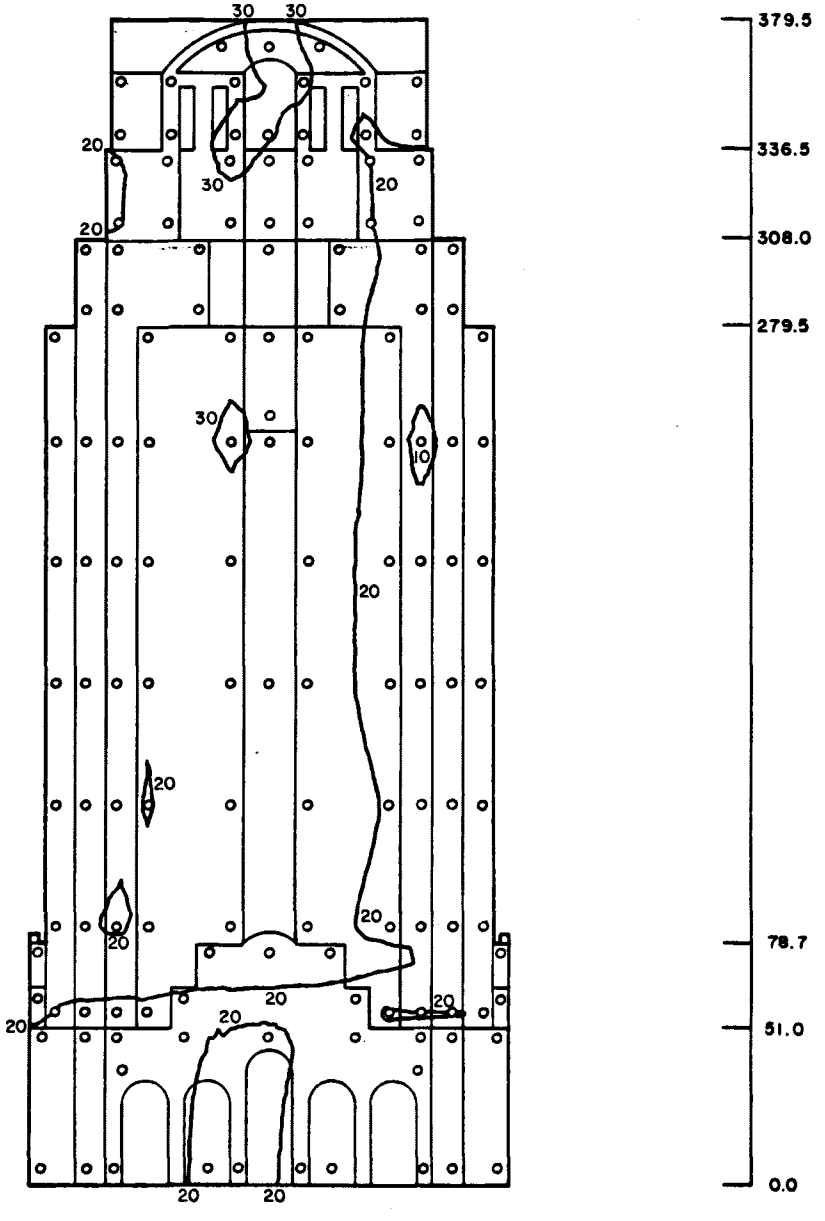
Figure 10s. Peak Pressure Contours on the Building for Cladding Loads



Tower II

SOFFIT
PEAK POSITIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
POSITIVE LOADS ACT INWARD

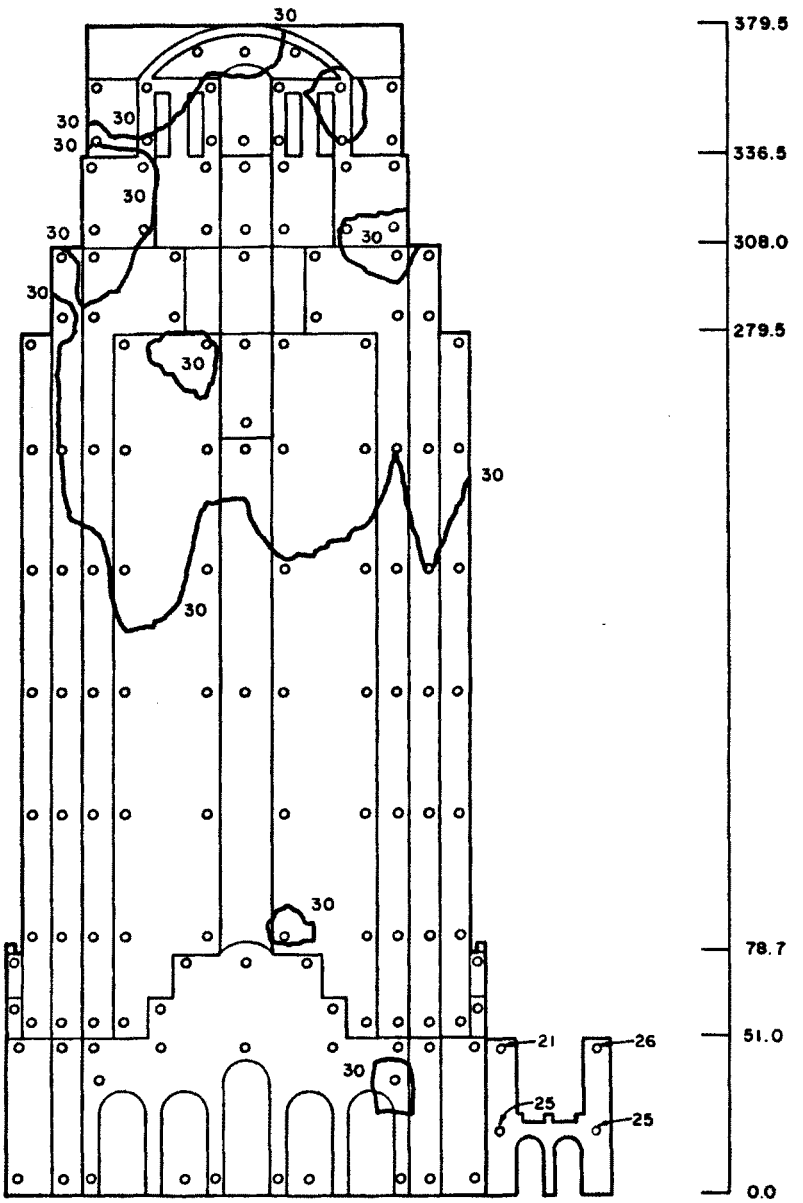
Figure 10t. Peak Pressure Contours on the Building for Cladding Loads



Tower II

NORTH
PEAK POSITIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
POSITIVE LOADS ACT INWARD

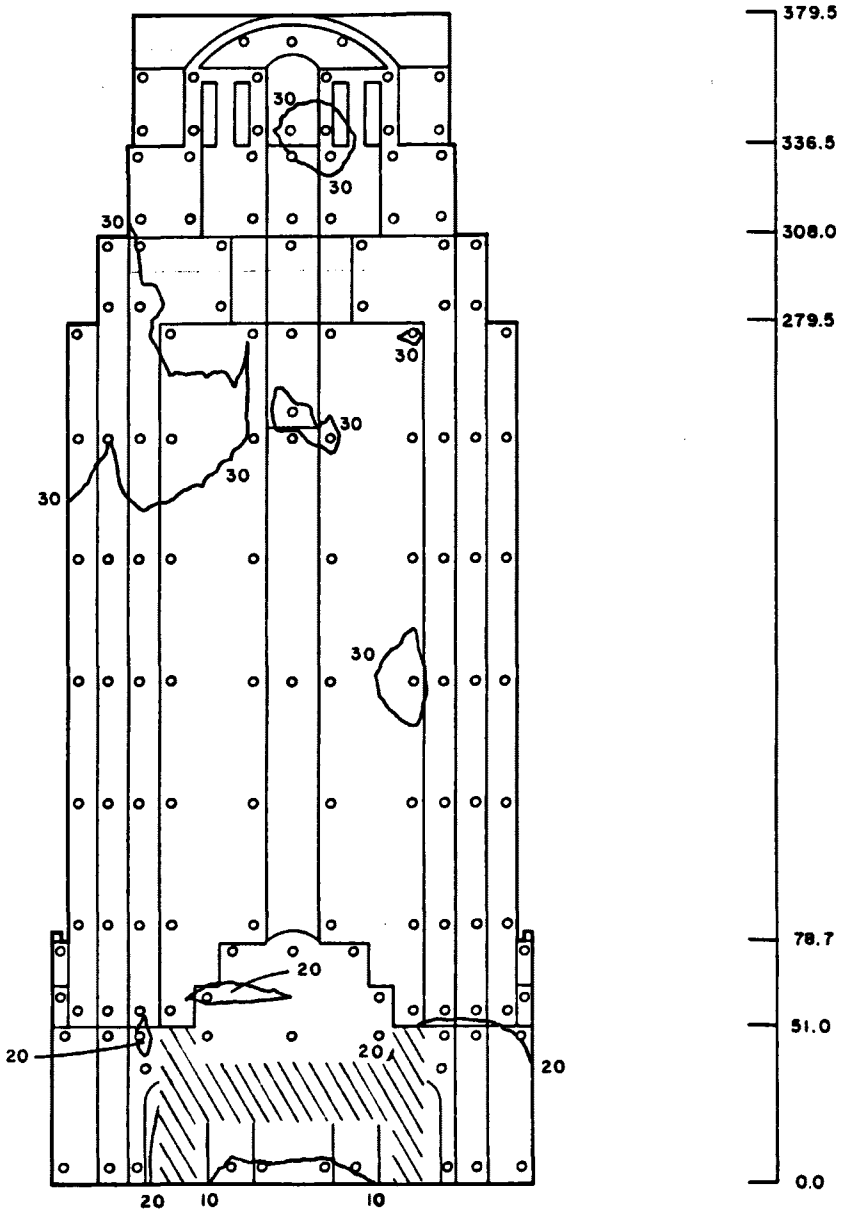
Figure 10u. Peak Pressure Contours on the Building for Cladding Loads



Tower II

SOUTH
PEAK POSITIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
POSITIVE LOADS ACT INWARD

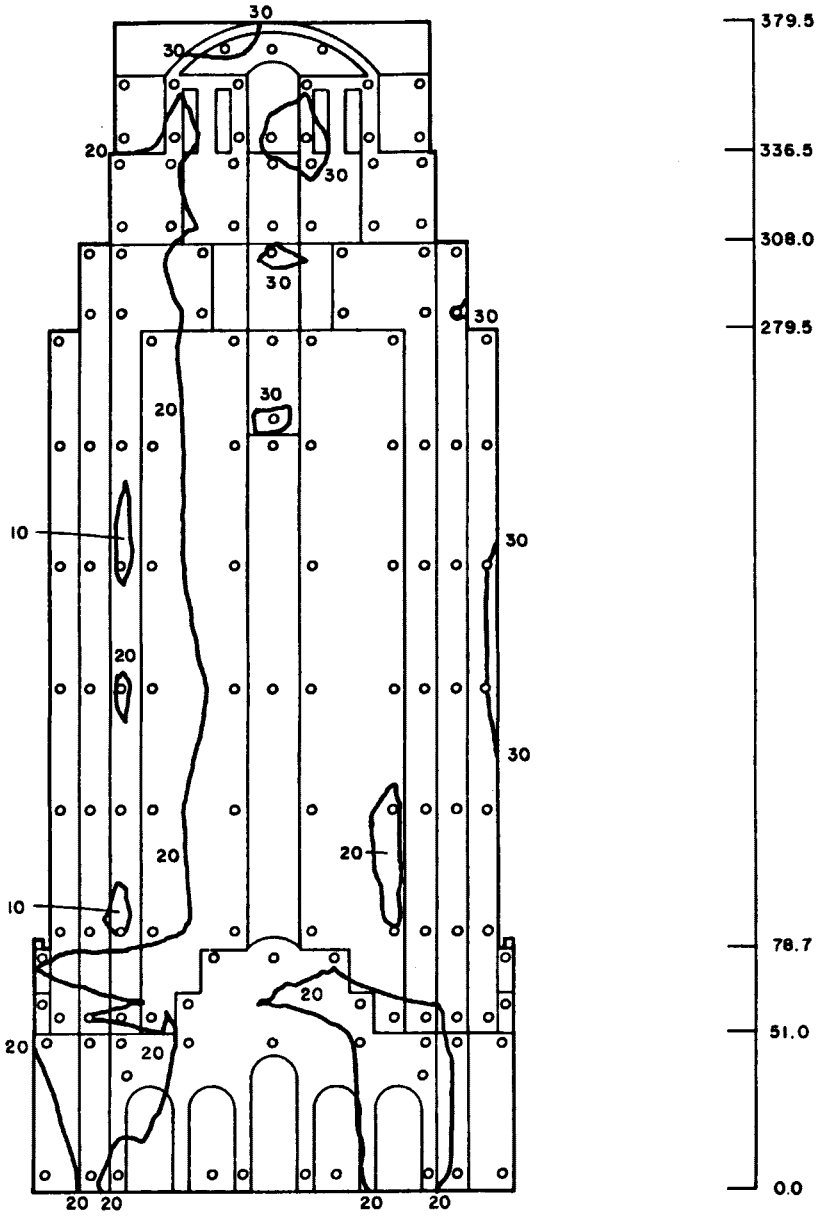
Figure 10v. Peak Pressure Contours on the Building for Cladding Loads



Tower II

EAST
PEAK POSITIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
POSITIVE LOADS ACT INWARD

Figure 10w. Peak Pressure Contours on the Building for Cladding Loads



<u>Tower II</u>

WEST
PEAK POSITIVE CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND
POSITIVE LOADS ACT INWARD

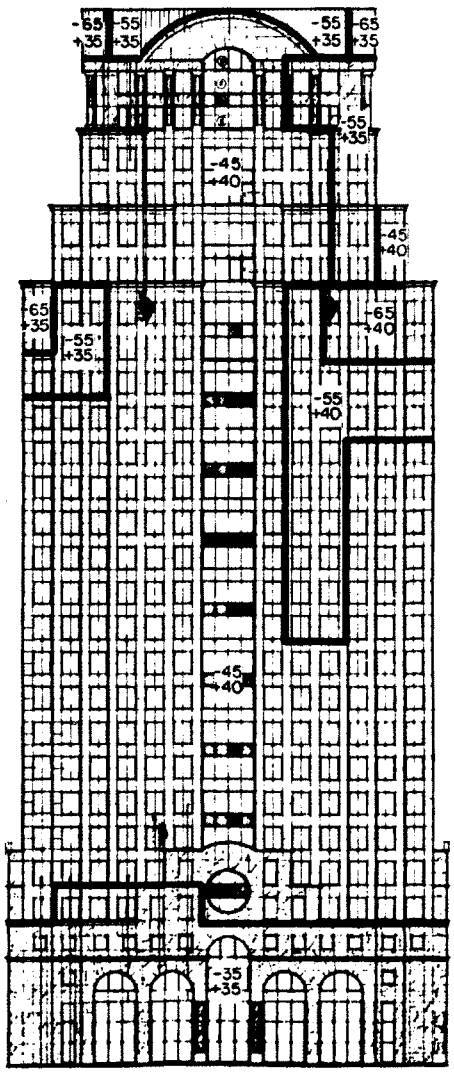
Figure 10x. Peak Pressure Contours on the Building for Cladding Loads

PEAK CLADDING PRESSURE ZONES, PSF

100 - Year Winds

Zones Include Internal Pressures of ±5 psf

February 1986

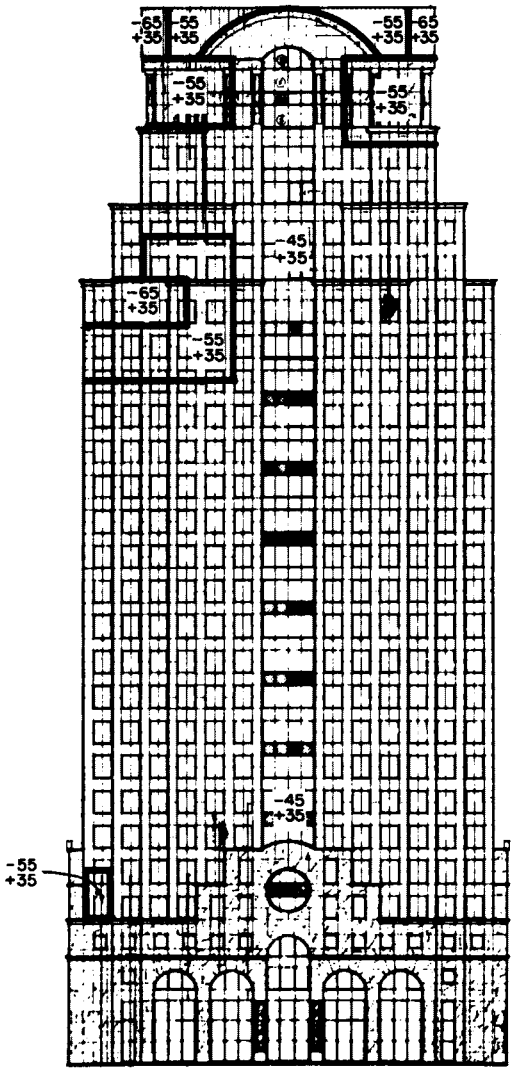


Tower I

NORTH

Figure 11a. Peak Pressure Cladding Zones

February 1986

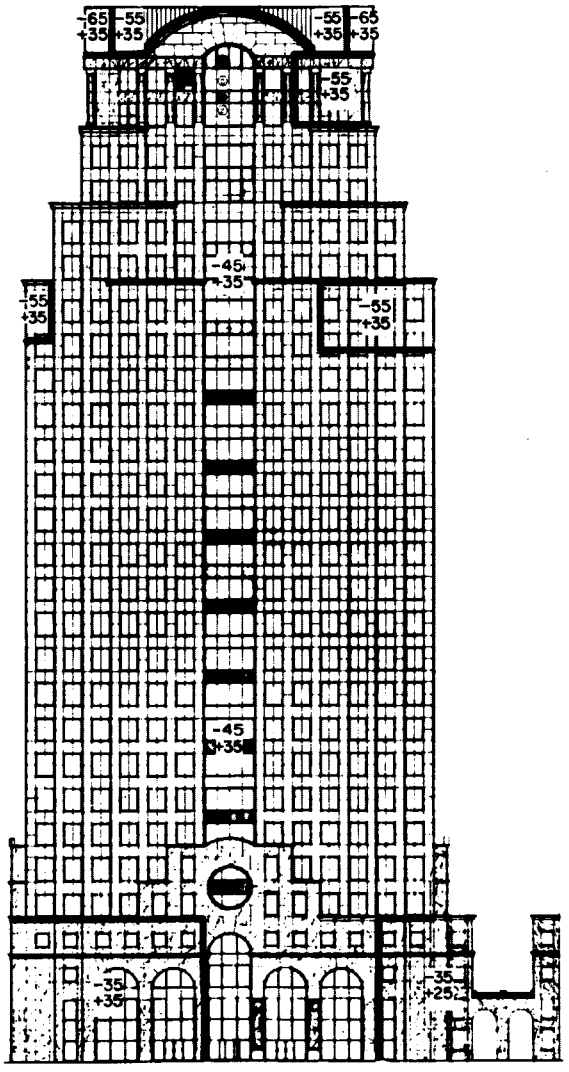


Tower I

SOUTH

Figure 11b. Peak Pressure Cladding Zones

February 1986

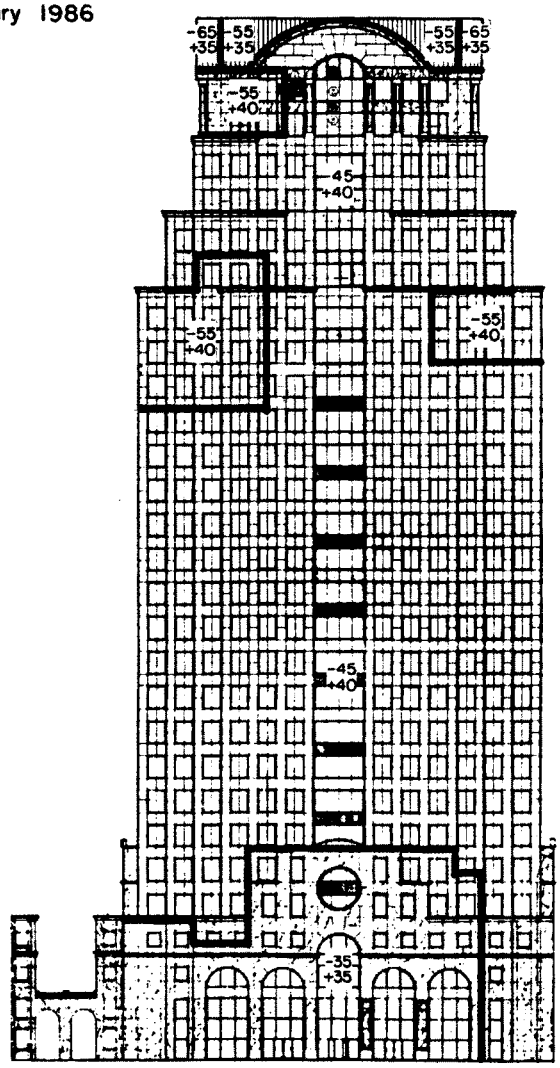


Tower I

EAST

Figure 11c. Peak Pressure Cladding Zones

February 1986

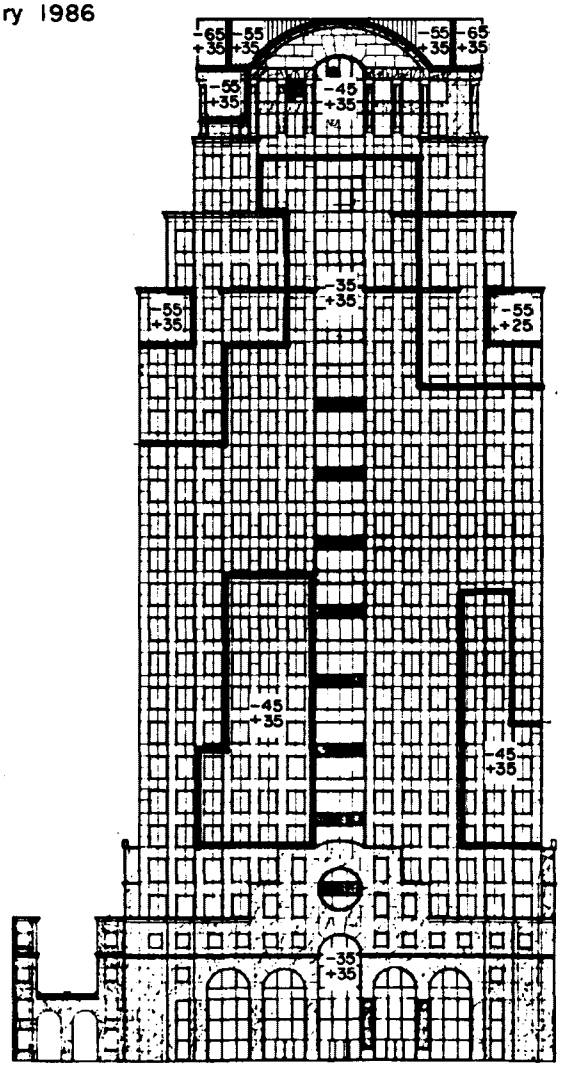


Tower I

WEST

Figure 11d. Peak Pressure Cladding Zones

February 1986

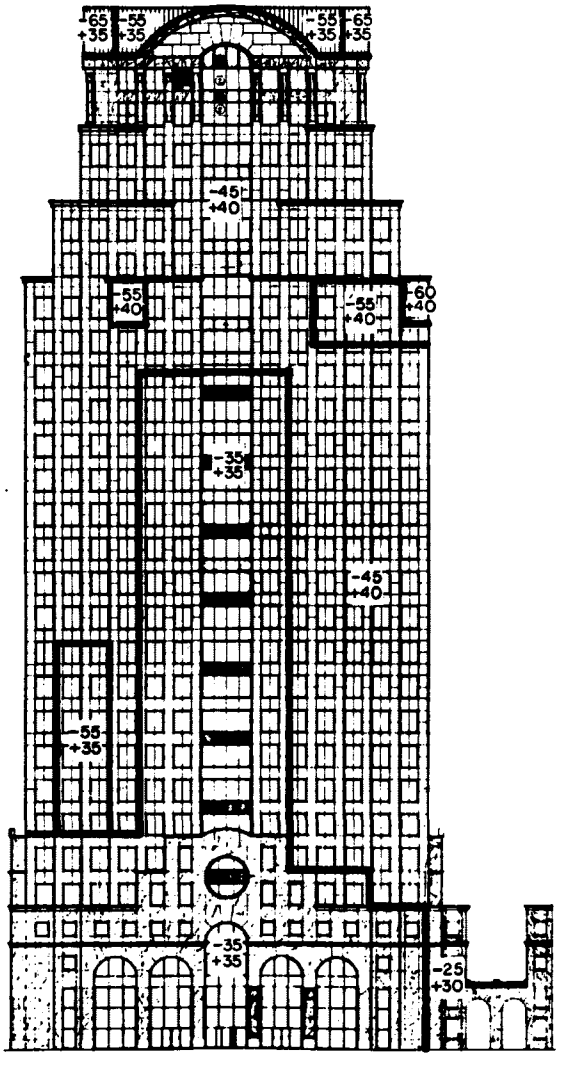


Tower II

NORTH

Figure 11e. Peak Pressure Cladding Zones

February 1986

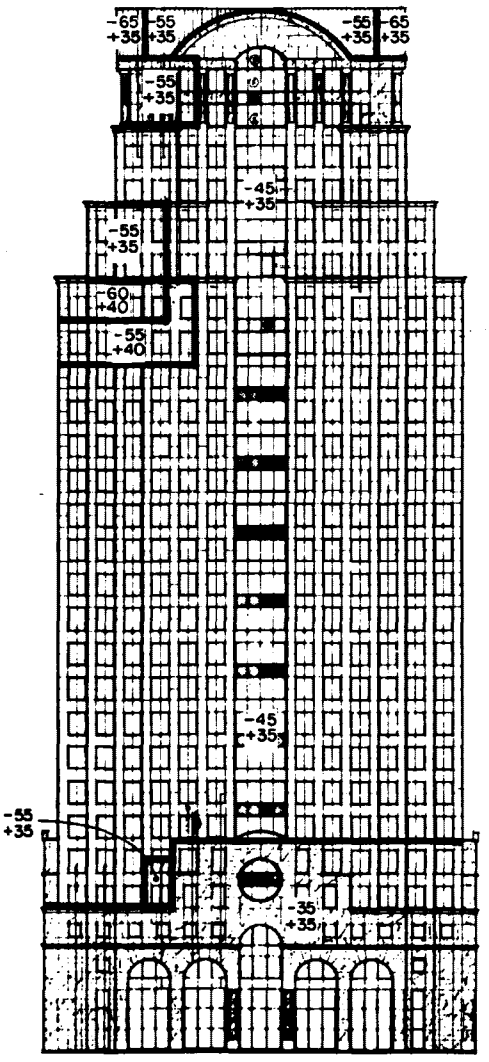


Tower II

SOUTH

Figure 11f. Peak Pressure Cladding Zones

February 1986

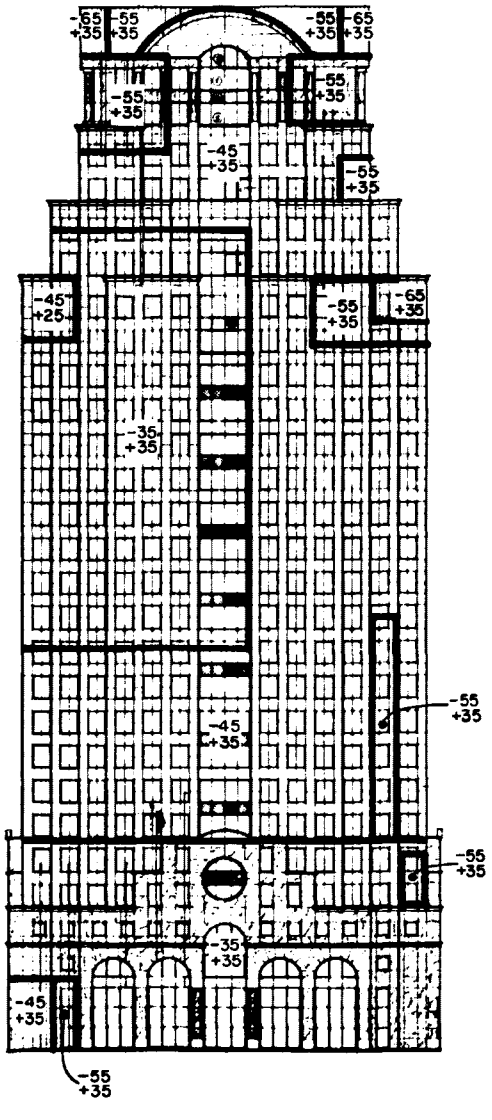


Tower II

EAST

Figure 11g. Peak Pressure Cladding Zones

February 1986



Tower II

WEST

Figure 11h. Peak Pressure Cladding Zones

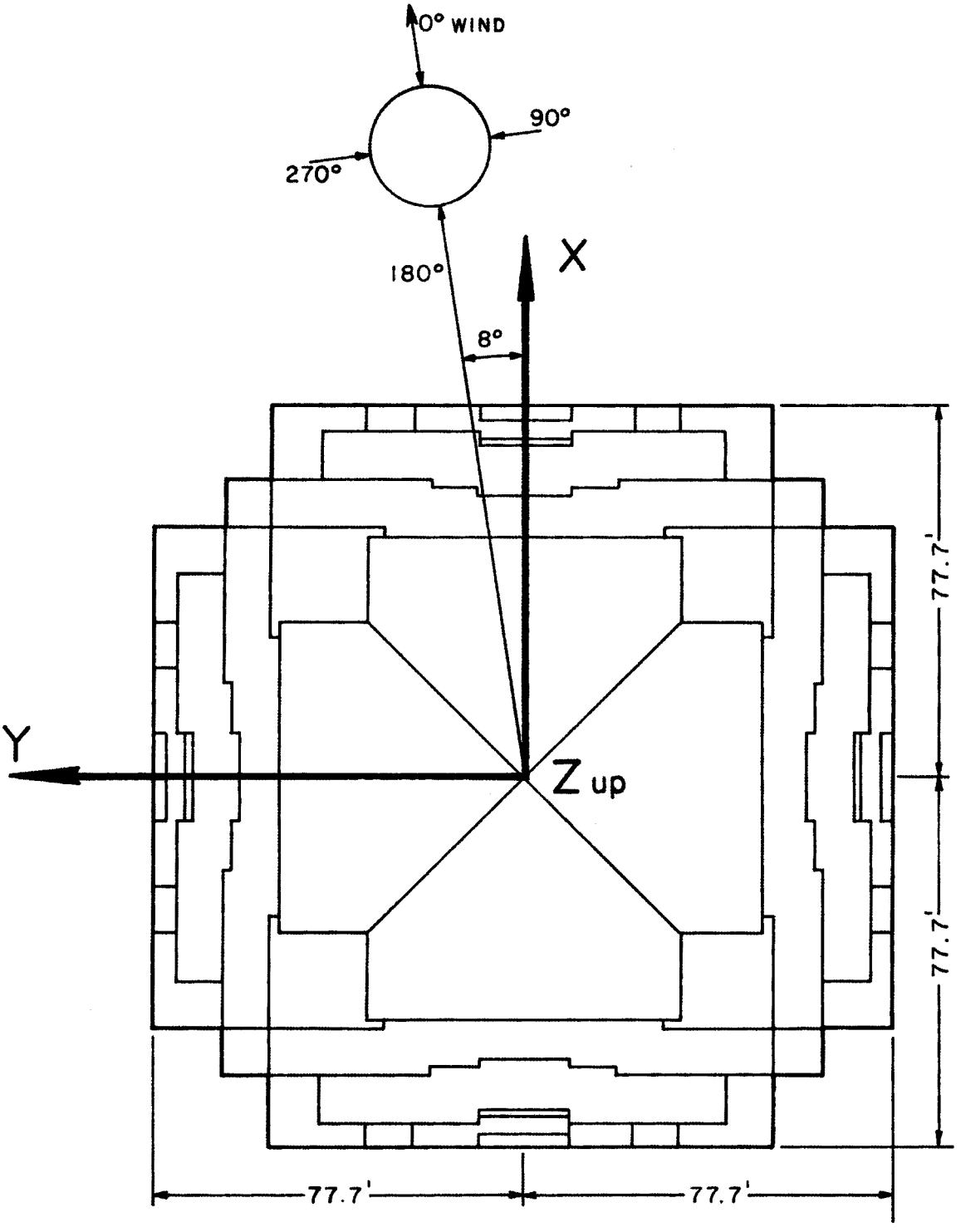


Figure 12. Coordinate System for Forces and Moments

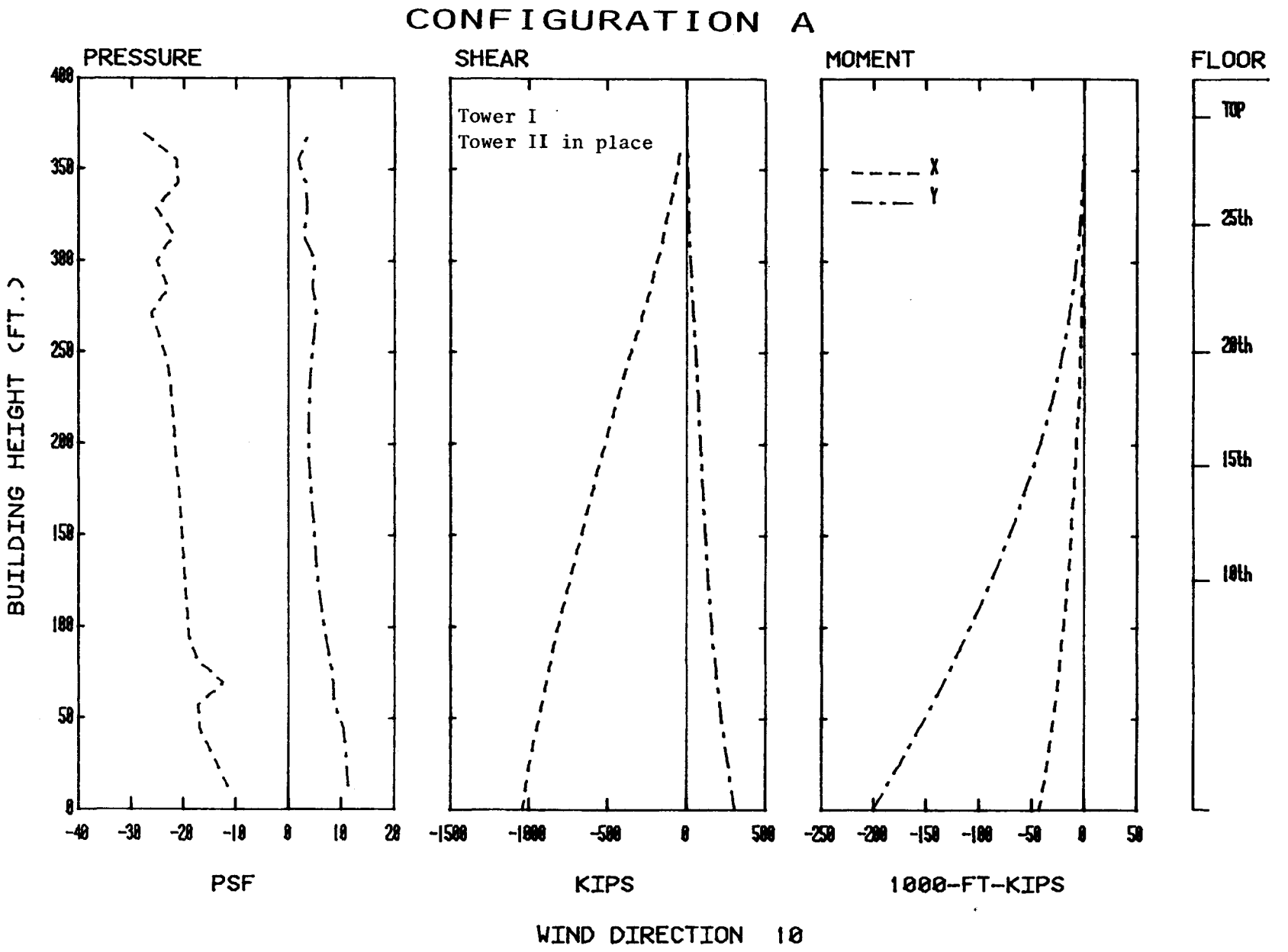


Figure 13a. Load, Shear, and Moment Diagrams for Selected Wind Directions

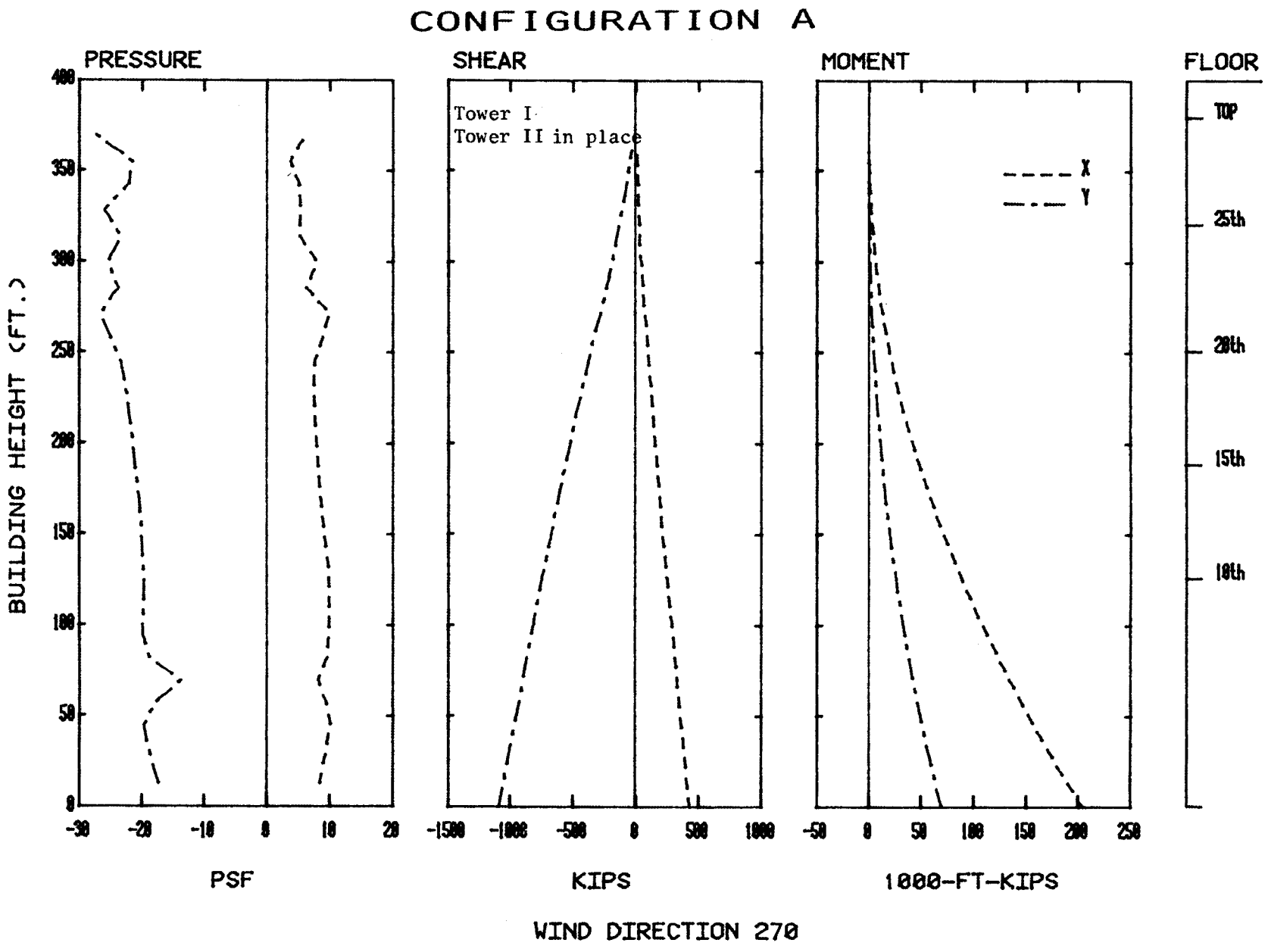


Figure 13b. Load, Shear, and Moment Diagrams for Selected Wind Directions

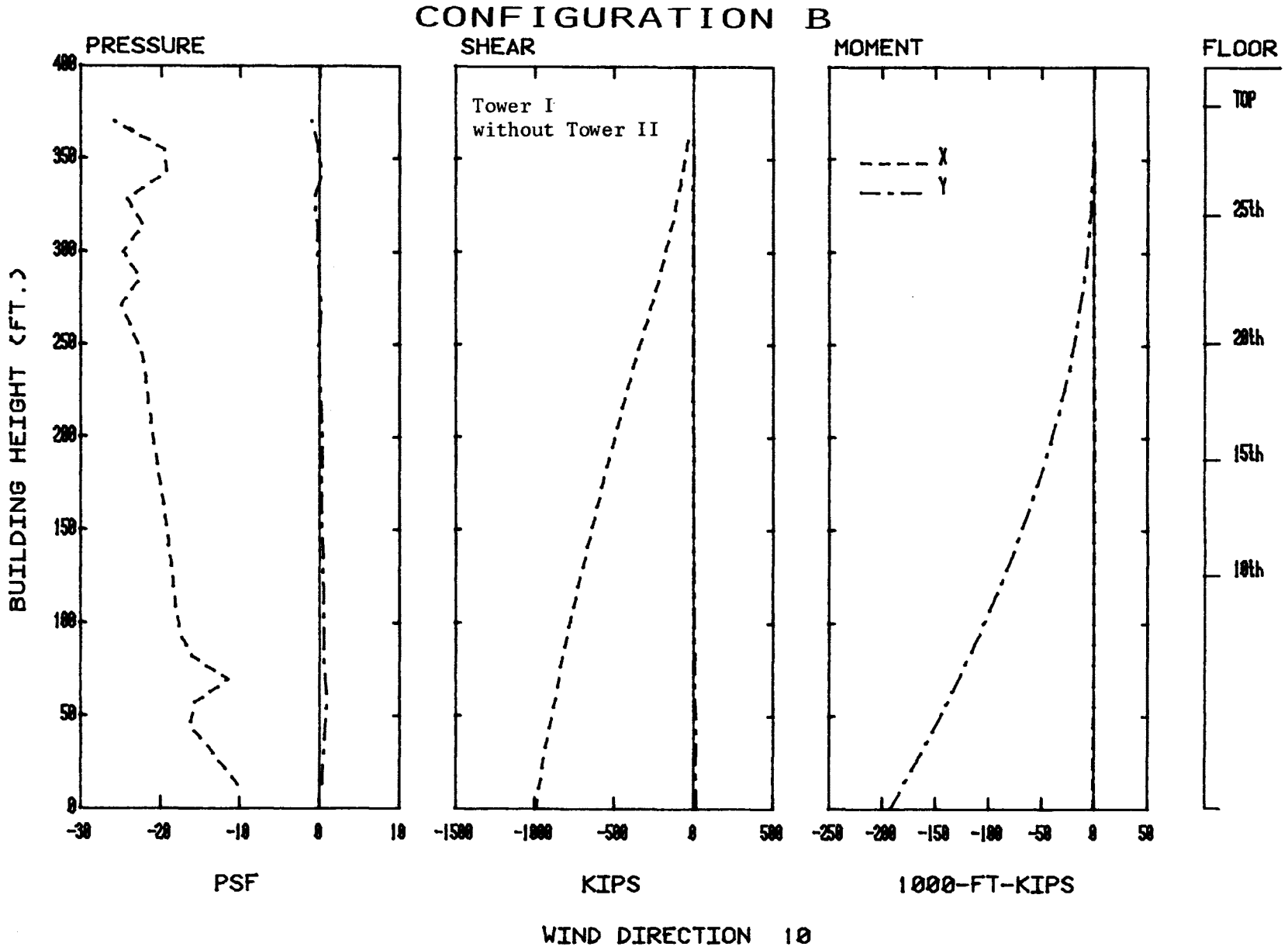


Figure 13c. Load, Shear, and Moment Diagrams for Selected Wind Directions

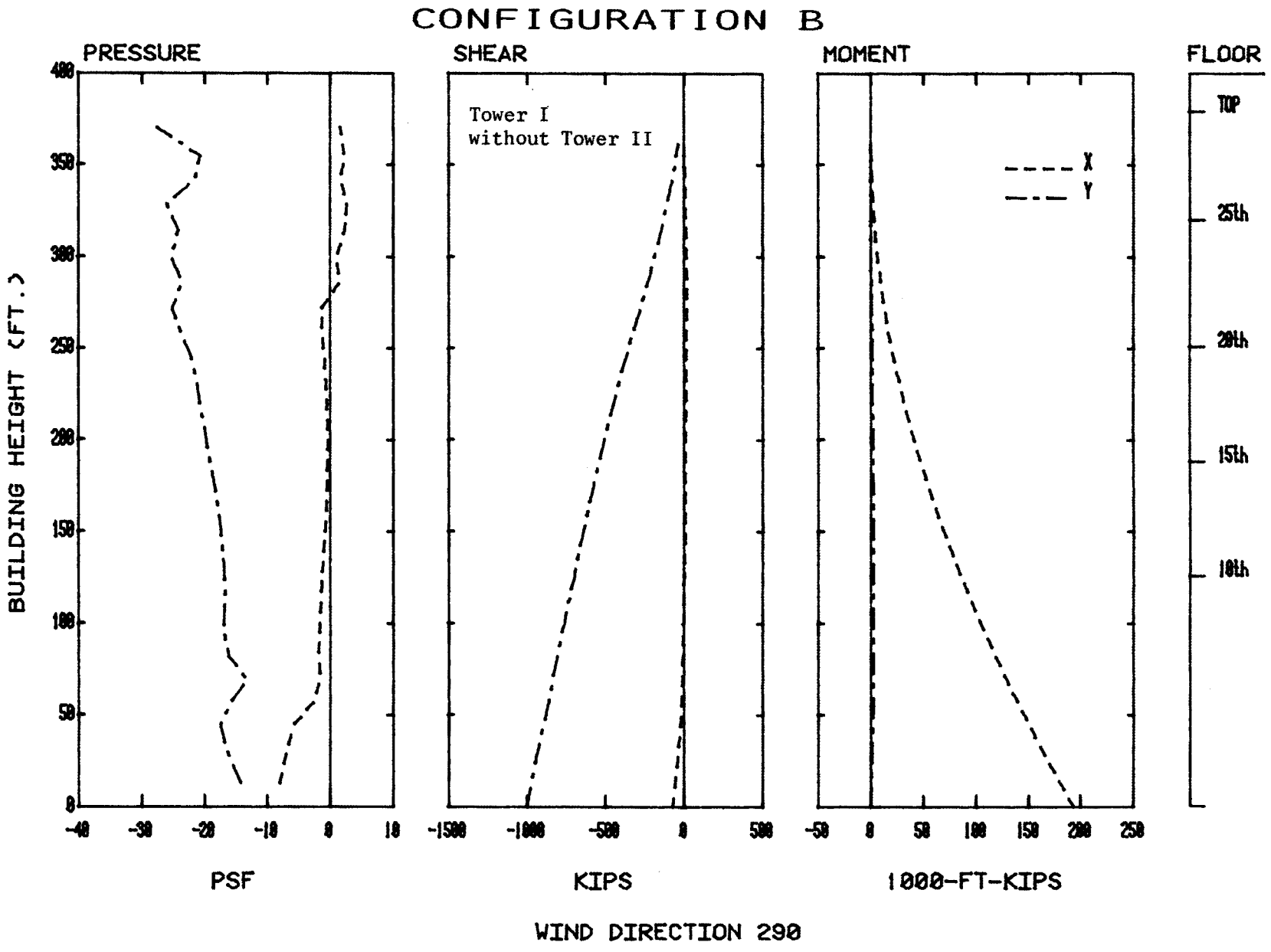


Figure 13d. Load, Shear, and Moment Diagrams for Selected Wind Directions

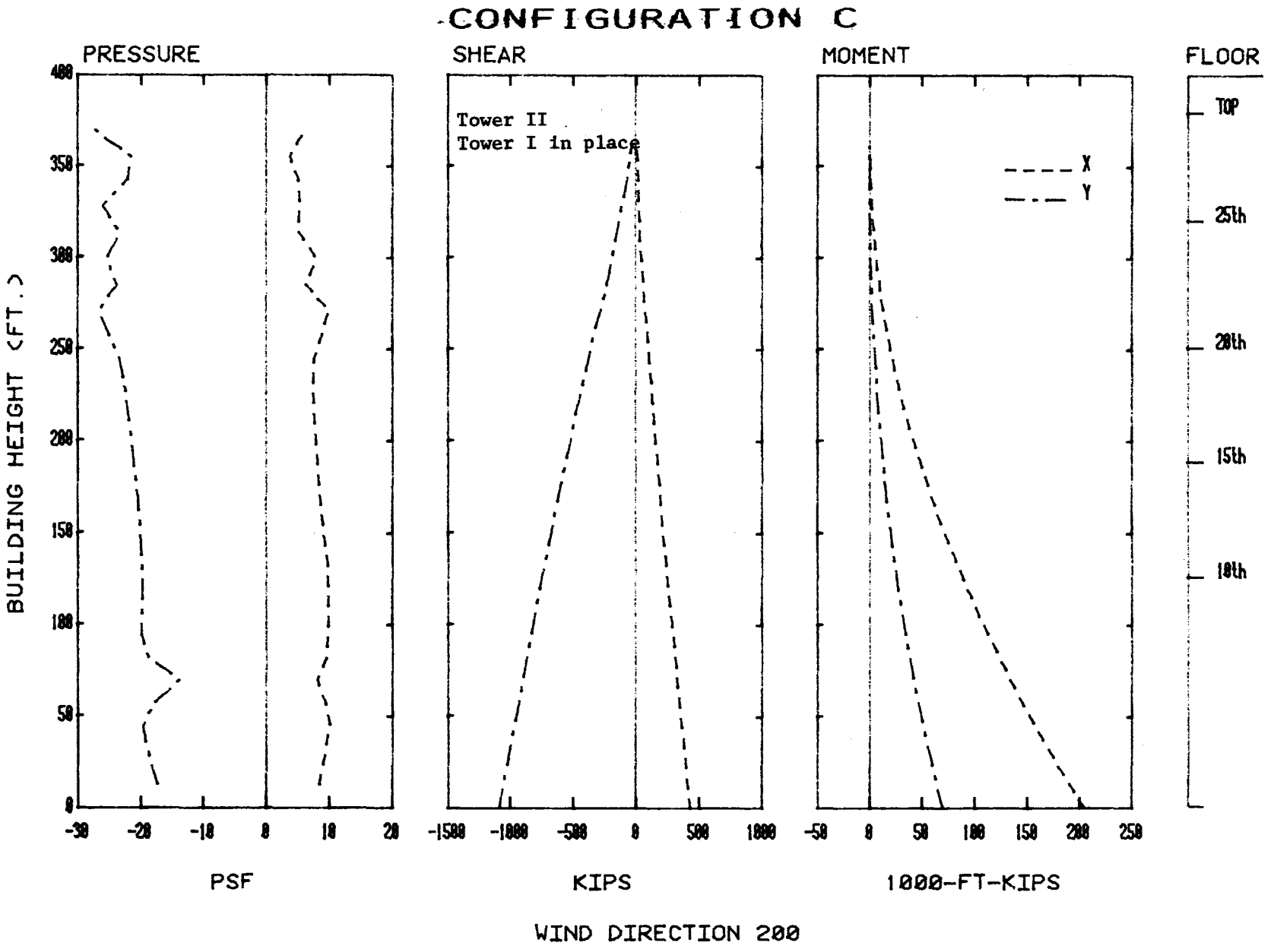


Figure 13e. Load, Shear, and Moment Diagrams for Selected Wind Directions

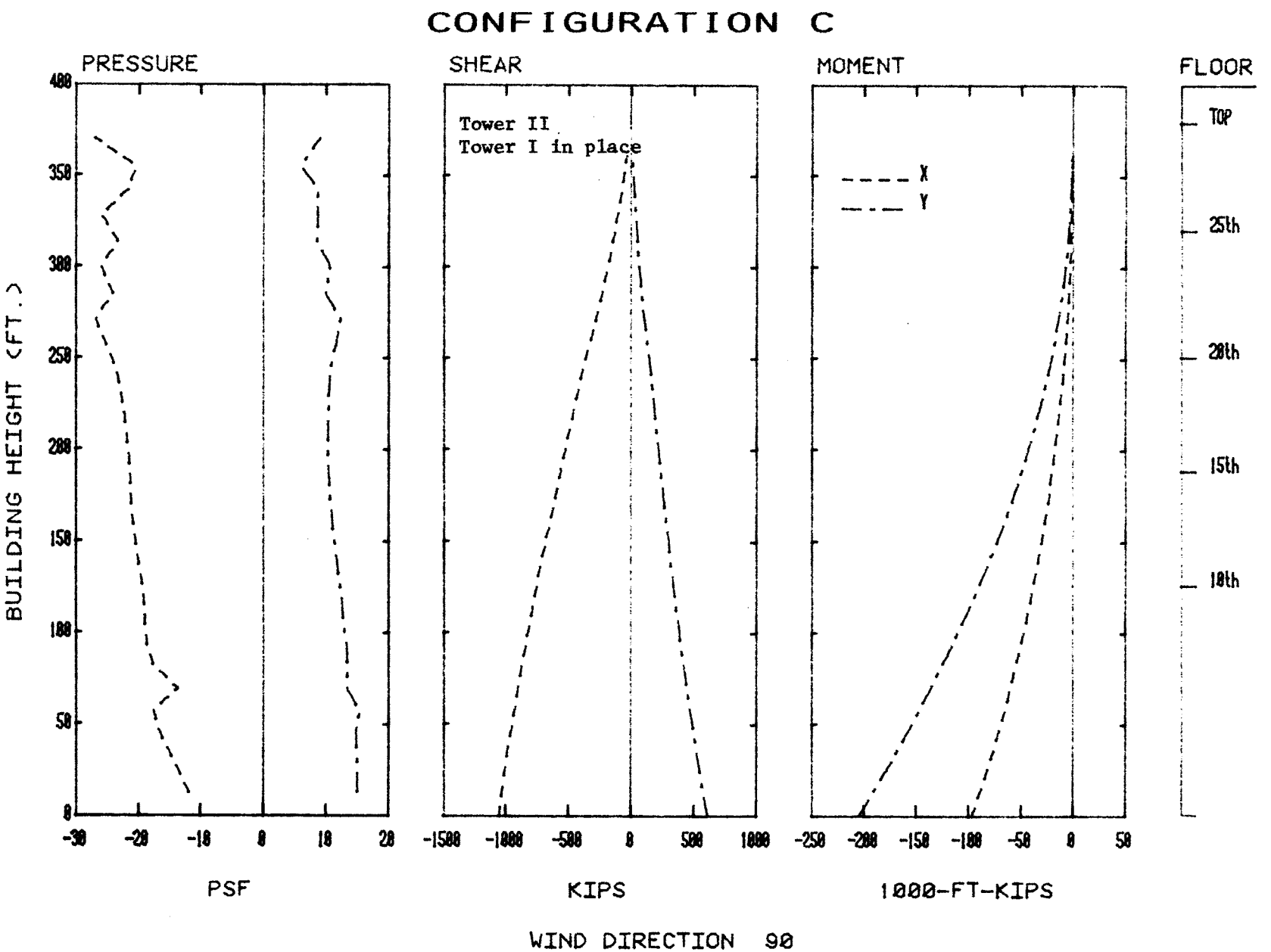


Figure 13f. Load, Shear, and Moment Diagrams for Selected Wind Directions

TABLES

TABLE 1

DATA CONFIGURATIONS

Configuration A:

Geometry - Towers I and II in place.

Pressures - Data measured for 36 wind directions, in 10-degree increments from 0, for all tap locations on Tower I.

Configuration B:

Geometry - Tower I in place.

Pressures - Data measured for 36 wind directions, in 10-degree increments from 0, for all tap locations on Tower I.

Configuration C:

Geometry - Towers I and II in place.

Pressures - Data measured for 36 wind directions, in 10-degree increments from 0, for all tap locations on Tower II.

Configuration D:

Geometry - Towers I and II in place.

Pressures - Data measured in 2-degree increments to both sides of selected wind directions for selected taps on Tower I where large pressure peaks were observed in Configuration A. Taps were selected to obtain the largest peak pressures on the structure.

Configuration E:

Geometry - Tower I in place.

Pressures - Data measured in 2-degree increments to both sides of selected wind directions for selected taps on Tower I where large pressure peaks were observed in Configuration B. Taps were selected to obtain the largest peak pressures on the structure.

Configuration F:

Geometry - Towers I and II in place.

Pressures - Data measured in 2-degree increments to both sides of selected wind directions for selected taps on Tower II where large pressure peaks were observed in Configuration C. Taps were selected to obtain the largest peak pressures on the structure.

TABLE 1 (Con't)

Configuration G:

Geometry - Towers I and II in place.

Velocities - Pedestrian winds measured for 16 wind directions, in 22.5-degree increments from 0, for locations 1-28 (Figure 4).

Configuration H:

Geometry - Tower I in place.

Velocities - Pedestrian winds measured for 16 wind directions, in 22.5-degree increments from 0, for locations 1-20 (Figure 4).

Configuration W:

Pressures - Worst case of Configurations A and B.

TABLE 2 PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

CONFIGURATION G

LOCATION 1

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U(3.0*RMS/UR (PERCENT)
0.00	29.4	14.9	74.0
22.50	52.5	17.1	107.9
45.00	45.1	21.0	108.1
67.50	30.6	20.4	99.8
90.00	63.7	21.0	126.0
112.50	60.0	16.3	109.8
135.00	51.2	15.4	97.5
157.50	10.6	12.0	54.2
180.00	25.8	15.3	71.8
202.50	39.0	23.0	107.9
225.00	49.3	24.0	121.2
247.50	30.6	19.0	87.0
270.00	51.3	17.6	104.1
292.50	61.0	20.2	122.3
315.00	47.9	20.9	110.6
337.50	24.0	12.1	60.2

LOCATION

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U(3.0*RMS/UR (PERCENT)
0.00	41.3	17.6	94.0
22.50	20.7	11.8	55.5
45.00	36.9	16.0	84.9
67.50	49.4	19.5	100.0
90.00	60.2	19.4	126.5
112.50	71.5	14.0	113.3
135.00	59.8	19.2	117.5
157.50	21.5	14.4	64.0
180.00	24.9	12.4	62.4
202.50	22.0	13.5	62.8
225.00	49.5	23.2	119.3
247.50	49.0	27.0	130.0
270.00	57.0	22.6	124.7
292.50	52.6	17.8	110.9
315.00	51.0	16.4	110.2
337.50	51.2	16.0	99.3

LOCATION 3

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U(3.0*RMS/UR (PERCENT)
0.00	12.2	7.7	35.3
22.50	19.9	8.6	46.4
45.00	28.7	7.2	52.0
67.50	20.7	10.0	50.3
90.00	32.5	12.7	70.3
112.50	31.6	14.4	74.8
135.00	25.8	14.1	67.6
157.50	14.0	9.9	41.5
180.00	17.7	9.5	46.2
202.50	32.4	10.8	64.8
225.00	43.3	13.4	83.5
247.50	40.7	15.0	91.9
270.00	45.3	13.3	85.2
292.50	50.1	14.6	99.0
315.00	46.8	14.3	89.6
337.50	42.8	15.0	87.8

LOCATION 4

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U(3.0*RMS/UR (PERCENT)
0.00	42.3	12.5	79.8
22.50	29.9	10.9	59.0
45.00	24.3	8.1	49.5
67.50	22.1	7.4	44.4
90.00	23.0	7.0	42.3
112.50	25.8	8.7	51.4
135.00	30.4	12.3	60.4
157.50	26.4	12.1	62.2
180.00	17.8	6.2	39.7
202.50	14.2	4.4	28.5
225.00	17.1	6.1	35.4
247.50	16.5	5.7	33.9
270.00	17.5	6.7	37.6
292.50	17.0	6.6	39.8
315.00	16.3	9.3	47.3
337.50	43.2	18.2	100.0

TABLE 2 -- PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

CONFIGURATION G

LOCATION 5

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U[3.0*RMS/UR (PERCENT)
0.00	15.6	9.8	45.2
22.50	7.0	4.8	21.5
45.00	6.2	4.5	19.6
67.50	7.9	5.8	25.2
90.00	10.2	6.5	29.7
112.50	12.0	7.1	33.3
135.00	11.2	7.4	33.5
157.50	7.1	5.6	23.8
180.00	5.0	4.0	17.0
202.50	2.1	1.5	6.7
225.00	3.7	3.2	13.3
247.50	3.4	3.2	12.9
270.00	2.6	1.8	7.6
292.50	2.7	1.9	8.4
315.00	6.5	5.5	22.9
337.50	22.3	13.5	62.7

LOCATION 6

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U[3.0*RMS/UR (PERCENT)
0.00	38.2	13.0	77.3
22.50	40.6	11.7	75.6
45.00	45.1	9.6	74.0
67.50	50.4	10.9	83.2
90.00	42.0	11.1	75.4
112.50	44.6	13.0	83.6
135.00	47.3	17.2	98.9
157.50	14.5	10.6	46.1
180.00	12.4	9.2	37.9
202.50	10.2	6.1	29.4
225.00	13.0	8.1	37.3
247.50	11.4	6.1	29.7
270.00	10.7	5.4	26.8
292.50	11.0	7.0	32.0
315.00	24.3	16.2	73.0
337.50	39.1	14.0	83.5

LOCATION 7

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U[3.0*RMS/UR (PERCENT)
0.00	70.4	14.7	114.6
22.50	70.0	12.3	114.0
45.00	84.0	10.7	116.3
67.50	81.2	11.6	115.9
90.00	69.4	13.4	109.5
112.50	52.5	13.7	93.4
135.00	40.5	19.5	98.9
157.50	41.9	24.1	114.2
180.00	67.9	15.6	114.6
202.50	73.1	13.1	112.3
225.00	77.0	11.5	111.5
247.50	68.6	12.4	105.7
270.00	67.8	12.9	102.6
292.50	59.9	14.5	103.4
315.00	33.0	17.9	86.6
337.50	61.1	17.3	113.1

LOCATION 8

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U[3.0*RMS/UR (PERCENT)
0.00	43.1	13.8	84.7
22.50	67.7	15.8	117.0
45.00	77.1	18.5	132.7
67.50	67.3	22.2	113.9
90.00	49.2	17.6	101.8
112.50	39.8	18.1	94.0
135.00	16.5	11.5	51.1
157.50	48.0	19.0	105.0
180.00	48.0	13.0	87.1
202.50	43.5	11.3	77.3
225.00	40.0	9.0	67.0
247.50	36.9	9.8	66.3
270.00	38.4	9.7	67.6
292.50	45.3	15.8	92.8
315.00	35.3	16.6	85.2
337.50	26.2	14.4	69.4

TABLE 2 - PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

CONFIGURATION G

LOCATION 9

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U[3.0*RMS/UR (PERCENT)
0.00	7.8	6.0	25.9
22.50	18.4	12.6	50.1
45.00	13.6	10.3	44.5
67.50	6.2	4.0	20.5
90.00	8.2	6.3	27.0
112.50	27.2	12.7	65.4
135.00	23.1	12.5	60.6
157.50	27.4	14.6	71.3
180.00	15.3	8.2	39.9
202.50	12.9	7.3	34.8
225.00	13.0	8.2	37.6
247.50	15.6	9.0	42.7
270.00	23.7	13.0	62.6
292.50	21.6	13.2	61.3
315.00	21.3	13.8	62.8
337.50	8.7	6.1	27.1

LOCATION 10

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U[3.0*RMS/UR (PERCENT)
0.00	50.7	23.2	120.3
22.50	37.2	23.8	108.7
45.00	33.5	18.0	87.6
67.50	15.6	8.5	41.2
90.00	17.5	10.6	51.3
112.50	40.0	15.7	87.2
135.00	37.5	20.0	99.5
157.50	54.1	21.5	118.7
180.00	70.0	15.0	115.1
202.50	48.1	14.8	92.7
225.00	27.3	13.6	70.0
247.50	18.7	10.6	50.5
270.00	23.9	12.8	62.1
292.50	50.3	25.7	125.4
315.00	48.1	25.8	125.6
337.50	50.8	22.8	127.2

LOCATION 11

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U[3.0*RMS/UR (PERCENT)
0.00	68.1	15.8	115.4
22.50	57.1	14.8	101.3
45.00	40.0	17.5	93.8
67.50	10.3	8.3	35.2
90.00	20.3	14.4	63.5
112.50	10.0	8.1	34.3
135.00	12.3	9.2	40.0
157.50	32.1	17.7	85.3
180.00	41.7	17.7	94.8
202.50	39.4	17.0	90.3
225.00	40.4	13.4	80.7
247.50	34.5	12.6	74.5
270.00	29.5	13.3	69.5
292.50	24.3	11.1	57.7
315.00	28.7	12.6	66.6
337.50	37.5	12.6	75.1

LOCATION 12

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U[3.0*RMS/UR (PERCENT)
0.00	21.1	13.6	61.9
22.50	44.9	17.8	98.4
45.00	55.0	19.2	112.5
67.50	57.2	13.0	96.1
90.00	54.1	11.8	89.4
112.50	47.3	11.5	83.9
135.00	32.9	14.9	77.7
157.50	15.7	7.7	44.8
180.00	13.6	8.6	39.4
202.50	28.9	11.7	63.7
225.00	34.5	12.9	74.0
247.50	29.7	13.3	69.6
270.00	27.1	11.2	60.8
292.50	33.4	10.7	65.4
315.00	24.7	10.4	55.9
337.50	22.5	10.8	55.0

TABLE 2 PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

CONFIGURATION G

LOCATION 13

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U(3.0*RMS/UR (PERCENT)
0.00	28.0	9.4	56.3
22.50	20.5	7.6	43.4
45.00	31.7	10.5	63.3
67.50	45.0	10.0	75.9
90.00	55.3	11.6	90.2
112.50	50.7	12.3	87.5
135.00	45.1	12.1	81.3
157.50	22.6	9.7	51.7
180.00	18.4	6.2	37.1
202.50	17.5	6.4	38.8
225.00	13.9	3.9	25.5
247.50	16.7	5.0	31.7
270.00	36.0	13.1	75.3
292.50	45.9	15.7	92.9
315.00	52.8	11.9	88.6
337.50	44.2	9.5	72.7

LOCATION 14

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U(3.0*RMS/UR (PERCENT)
0.00	35.9	13.8	77.1
22.50	21.5	11.1	54.8
45.00	13.8	8.4	39.1
67.50	16.3	9.9	46.0
90.00	20.8	13.0	67.9
112.50	32.5	12.6	70.4
135.00	37.7	11.6	74.5
157.50	34.5	14.0	76.5
180.00	17.6	11.1	51.0
202.50	25.1	13.2	64.7
225.00	21.5	11.5	56.0
247.50	8.5	5.2	24.1
270.00	6.8	3.6	17.7
292.50	8.4	4.1	20.8
315.00	11.9	7.5	34.5
337.50	23.9	8.9	50.7

LOCATION 15

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U(3.0*RMS/UR (PERCENT)
0.00	29.6	12.4	66.7
22.50	27.5	11.8	60.9
45.00	17.8	9.6	47.5
67.50	16.0	8.9	42.7
90.00	23.3	12.5	60.9
112.50	31.9	13.0	71.0
135.00	26.3	14.7	70.4
157.50	18.8	10.2	48.5
180.00	25.3	14.1	67.4
202.50	34.5	17.7	87.7
225.00	27.3	16.8	77.8
247.50	21.7	12.0	57.7
270.00	16.5	11.1	49.8
292.50	13.4	8.6	39.2
315.00	19.9	12.8	58.3
337.50	30.0	13.4	70.2

LOCATION 16

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U(3.0*RMS/UR (PERCENT)
0.00	28.1	11.9	63.7
22.50	22.9	11.6	64.7
45.00	21.7	7.8	45.0
67.50	26.3	11.5	60.7
90.00	30.4	12.5	67.8
112.50	38.9	15.3	96.8
135.00	34.1	15.8	81.5
157.50	30.2	13.7	71.3
180.00	53.5	17.6	106.1
202.50	42.2	16.1	90.6
225.00	50.0	21.4	114.1
247.50	39.5	20.0	99.4
270.00	35.7	18.2	90.2
292.50	27.5	14.4	72.6
315.00	37.6	20.1	97.8
337.50	41.5	18.9	98.1

TABLE 2 PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

CONFIGURATION G

LOCATION 17

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U(3.0*RMS/UR (PERCENT)
0.00	20.5	6.6	40.3
22.50	20.5	6.4	37.7
45.00	21.4	6.0	41.9
67.50	22.0	7.5	45.0
90.00	26.1	11.5	63.0
112.50	31.2	12.3	60.2
135.00	31.2	13.7	72.3
157.50	19.0	7.2	41.5
180.00	17.6	6.0	35.7
202.50	17.2	5.5	33.7
225.00	21.9	9.9	51.5
247.50	21.6	8.9	48.2
270.00	20.0	8.4	45.3
292.50	35.6	15.0	80.5
315.00	26.2	10.8	58.7
337.50	24.7	9.5	53.3

LOCATION 18

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U(3.0*RMS/UR (PERCENT)
0.00	45.0	12.0	80.9
22.50	37.0	11.1	70.2
45.00	30.6	9.0	54.5
67.50	27.5	7.9	48.6
90.00	25.2	7.7	48.4
112.50	20.2	8.2	44.9
135.00	33.8	11.8	99.3
157.50	60.0	11.0	92.9
180.00	54.9	12.9	93.4
202.50	57.7	15.6	104.4
225.00	55.4	14.1	103.5
247.50	43.2	12.8	81.7
270.00	26.1	9.9	55.7
292.50	22.1	7.5	44.5
315.00	23.9	8.5	49.3
337.50	35.2	12.0	71.2

LOCATION 19

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U(3.0*RMS/UR (PERCENT)
0.00	26.9	11.0	62.3
22.50	20.4	7.4	42.6
45.00	19.8	7.3	41.7
67.50	26.9	11.1	60.1
90.00	46.5	18.7	102.7
112.50	62.7	15.2	100.2
135.00	73.1	12.9	111.9
157.50	76.0	13.3	115.9
180.00	57.4	17.3	109.2
202.50	29.4	11.1	62.8
225.00	25.5	9.4	53.6
247.50	36.6	13.0	75.7
270.00	50.2	15.3	104.2
292.50	61.6	15.0	106.5
315.00	45.6	15.0	90.6
337.50	30.4	13.7	71.5

LOCATION 20

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U(3.0*RMS/UR (PERCENT)
0.00	44.0	16.6	93.7
22.50	32.3	12.8	70.6
45.00	27.9	11.8	63.3
67.50	28.3	11.8	63.7
90.00	44.4	15.1	89.7
112.50	63.6	14.3	106.6
135.00	67.3	13.6	100.0
157.50	56.7	11.6	91.6
180.00	42.6	10.1	73.1
202.50	29.5	10.0	59.6
225.00	26.7	10.2	53.2
247.50	20.4	7.9	44.2
270.00	32.0	10.4	63.2
292.50	47.5	12.9	86.1
315.00	49.3	13.1	88.5
337.50	52.6	13.3	92.6

TABLE 2 PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

CONFIGURATION G

LOCATION 21

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	67.8	11.6	102.6
22.50	68.0	10.8	100.3
45.00	57.9	11.0	90.9
67.50	42.6	11.6	77.4
90.00	22.8	7.8	46.2
112.50	25.7	8.9	52.4
135.00	36.2	8.3	61.1
157.50	52.1	8.9	78.9
180.00	60.6	9.7	89.8
202.50	44.6	11.0	79.0
225.00	21.0	8.3	45.9
247.50	15.1	4.2	27.7
270.00	15.8	5.2	31.4
292.50	16.8	5.5	33.2
315.00	22.2	9.6	51.1
337.50	53.0	12.1	89.4

LOCATION 22

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	55.8	13.4	96.0
22.50	57.5	17.0	108.5
45.00	42.5	16.7	92.7
67.50	37.5	16.8	87.9
90.00	50.2	16.0	98.3
112.50	22.9	8.6	48.6
135.00	21.5	8.4	46.8
157.50	37.0	16.4	86.2
180.00	61.3	18.9	118.0
202.50	59.0	15.0	104.0
225.00	39.6	17.5	92.2
247.50	33.0	15.8	80.4
270.00	31.0	14.9	75.7
292.50	21.0	8.3	46.0
315.00	28.5	13.2	68.1
337.50	42.6	10.9	75.3

LOCATION 23

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	48.3	10.3	79.3
22.50	38.2	11.6	73.1
45.00	24.1	8.2	48.7
67.50	20.2	7.1	41.5
90.00	28.4	10.0	58.4
112.50	40.8	11.7	75.9
135.00	27.1	6.6	46.8
157.50	27.6	9.3	55.5
180.00	46.5	11.4	80.0
202.50	41.3	11.1	74.5
225.00	23.6	10.2	54.3
247.50	18.9	7.6	41.5
270.00	19.6	7.7	42.7
292.50	20.7	8.6	46.6
315.00	34.5	11.3	68.3
337.50	46.8	9.1	74.2

LOCATION 24

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	66.4	14.1	108.7
22.50	64.8	12.7	103.1
45.00	52.4	14.2	95.1
67.50	38.7	11.3	72.6
90.00	25.3	9.9	55.0
112.50	37.6	12.5	77.0
135.00	50.5	12.3	87.3
157.50	61.5	15.4	107.7
180.00	48.3	21.7	113.3
202.50	30.1	13.2	69.8
225.00	41.3	21.1	104.5
247.50	42.1	16.9	92.7
270.00	24.8	10.2	55.3
292.50	25.1	9.7	54.2
315.00	38.0	18.4	93.1
337.50	53.9	16.2	102.5

TABLE 2 -- PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

CONFIGURATION G

LOCATION 25

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	47.0	11.6	81.7
22.50	13.0	8.4	38.0
45.00	17.2	10.1	47.5
67.50	47.7	17.9	101.2
90.00	43.3	19.5	101.9
112.50	15.7	9.5	44.4
135.00	17.6	10.4	48.8
157.50	20.2	10.8	60.7
180.00	42.2	12.5	77.6
202.50	54.2	13.0	93.1
225.00	53.9	13.3	93.9
247.50	42.5	14.0	85.5
270.00	29.5	12.8	68.1
292.50	20.8	10.7	52.9
315.00	24.0	11.5	58.6
337.50	34.8	11.2	68.5

LOCATION 26

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	45.8	10.9	78.6
22.50	40.4	10.0	70.5
45.00	35.7	9.9	65.4
67.50	37.3	10.0	67.7
90.00	40.3	9.8	69.6
112.50	45.7	10.7	77.9
135.00	52.3	11.1	85.5
157.50	55.7	11.3	91.3
180.00	57.2	10.6	89.1
202.50	49.0	11.0	82.1
225.00	23.6	10.1	53.9
247.50	28.5	10.9	61.0
270.00	43.7	10.4	75.0
292.50	42.4	11.1	75.7
315.00	52.9	10.9	85.5
337.50	52.3	10.9	84.9

LOCATION 27

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	22.8	8.2	47.4
22.50	23.2	7.6	46.2
45.00	20.7	7.4	42.9
67.50	21.3	8.1	45.6
90.00	24.6	9.8	53.5
112.50	24.1	10.6	55.8
135.00	21.5	6.5	41.1
157.50	22.4	8.0	46.4
180.00	28.4	9.5	56.9
202.50	24.1	10.9	56.8
225.00	31.1	14.4	74.4
247.50	31.0	15.0	75.9
270.00	26.9	11.7	62.1
292.50	26.8	12.0	62.9
315.00	29.6	14.0	71.6
337.50	23.8	8.7	50.0

LOCATION 28

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	30.3	11.8	65.8
22.50	16.4	5.0	31.4
45.00	14.5	4.3	27.3
67.50	25.9	14.3	68.7
90.00	19.2	6.9	40.0
112.50	16.1	4.6	30.0
135.00	19.3	6.4	38.6
157.50	29.3	13.1	68.7
180.00	49.8	16.0	97.8
202.50	37.3	12.8	75.6
225.00	22.3	7.9	46.3
247.50	23.5	8.7	49.5
270.00	28.5	10.2	59.0
292.50	24.9	10.0	54.8
315.00	30.9	11.1	64.2
337.50	26.0	10.9	58.7

TABLE 2 PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

CONFIGURATION G

** GREATEST VALUES **

UMEAN/UINF (PERCENT)

LOC	AZ	MEAN	RMS	M13.0RMS
7	45.0	84.0	10.7	116.3
7	67.5	81.2	11.6	115.9
7	22.5	78.0	12.3	114.0
8	45.0	77.1	10.5	132.7
7	225.0	77.0	11.5	111.5
19	157.5	76.0	13.3	115.9
7	202.5	73.1	13.1	112.3
19	135.0	73.1	12.9	111.9
2	112.5	71.5	14.0	113.6
7	0.0	70.4	14.7	114.6

URMS/UINF (PERCENT)

LOC	AZ	MEAN	RMS	M13.0RMS
2	247.5	49.0	27.0	130.0
10	315.0	40.1	25.8	125.6
10	292.5	50.3	25.7	127.4
7	157.5	41.9	24.1	114.2
1	225.0	49.3	24.0	121.2
10	22.5	37.3	23.8	108.7
2	225.0	49.7	23.2	119.3
10	0.0	50.7	23.2	120.3
1	202.5	39.0	23.0	107.9
10	337.5	50.8	22.8	127.2

UMEAN+3.0*RMS/UINF (PERCENT)

LOC	AZ	MEAN	RMS	M13.0RMS
8	45.0	77.1	10.5	132.7
2	247.5	49.0	27.0	130.0
10	292.5	50.3	25.7	127.4
10	337.5	58.8	22.8	127.2
1	90.0	63.7	21.0	126.8
2	90.0	68.2	19.4	126.5
10	315.0	40.1	25.8	125.6
2	270.0	57.0	22.6	124.7
1	292.5	61.8	20.2	122.3
1	225.0	49.3	24.0	121.2

TABLE 2 PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

CONFIGURATION H

LOCATION 1

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	43.9	13.6	84.6
22.50	46.9	17.0	97.8
45.00	50.9	18.7	107.0
67.50	51.7	18.0	102.1
90.00	51.6	19.9	111.4
112.50	63.4	15.7	110.6
135.00	67.5	14.5	110.9
157.50	40.8	23.8	120.2
180.00	23.7	14.4	67.0
202.50	23.1	14.1	65.4
225.00	20.0	17.0	70.9
247.50	28.6	17.6	81.5
270.00	45.3	16.2	93.8
292.50	49.4	16.5	98.8
315.00	40.8	19.5	99.2
337.50	23.1	12.1	59.5

LOCATION 2

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	44.1	12.8	82.5
22.50	24.1	14.0	66.0
45.00	22.4	13.2	61.9
67.50	35.0	14.9	79.8
90.00	54.7	16.6	104.5
112.50	70.7	12.6	108.6
135.00	82.2	12.7	120.1
157.50	46.9	24.4	123.0
180.00	31.9	19.8	91.4
202.50	19.5	11.9	55.3
225.00	46.3	22.2	112.9
247.50	44.1	21.3	108.1
270.00	54.8	18.7	111.0
292.50	63.1	17.4	115.4
315.00	60.6	16.2	109.3
337.50	54.0	17.9	107.6

LOCATION 3

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	20.5	10.6	52.3
22.50	19.8	11.6	54.6
45.00	20.6	10.3	51.6
67.50	31.0	12.1	67.2
90.00	36.0	11.7	71.2
112.50	30.6	14.7	74.8
135.00	24.9	12.5	62.5
157.50	41.4	13.8	82.8
180.00	32.1	13.2	71.6
202.50	28.6	11.7	63.7
225.00	45.3	15.4	91.5
247.50	38.6	11.9	74.2
270.00	39.4	12.9	78.2
292.50	47.6	14.2	90.2
315.00	45.1	13.8	86.5
337.50	43.6	12.5	81.0

LOCATION 4

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	65.3	14.4	108.5
22.50	58.6	16.3	107.5
45.00	41.3	12.8	79.7
67.50	29.7	12.6	67.4
90.00	15.2	8.6	40.9
112.50	14.1	8.4	39.4
135.00	31.8	12.1	68.0
157.50	54.6	12.8	92.9
180.00	57.8	19.3	115.8
202.50	31.4	19.0	88.4
225.00	17.2	12.9	55.8
247.50	10.2	8.0	34.2
270.00	11.4	7.9	35.1
292.50	15.0	10.7	47.2
315.00	27.0	21.9	92.6
337.50	55.4	16.0	103.3

TABLE 2 PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

CONFIGURATION H

LOCATION 5

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	58.5	15.3	104.3
22.50	46.0	17.4	98.2
45.00	29.5	14.0	71.4
67.50	16.5	8.9	43.3
90.00	13.0	7.5	35.5
112.50	11.1	6.6	30.8
135.00	13.2	6.5	32.5
157.50	15.0	7.9	39.5
180.00	12.7	8.4	37.9
202.50	5.3	3.3	15.1
225.00	4.8	2.9	13.5
247.50	4.1	2.4	11.3
270.00	4.8	3.2	14.4
292.50	7.1	5.2	22.6
315.00	14.3	13.0	53.2
337.50	36.0	18.0	89.9

LOCATION 6

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	74.2	15.5	120.6
22.50	51.1	14.7	95.0
45.00	50.3	12.4	95.4
67.50	61.0	11.5	95.5
90.00	48.7	13.4	88.8
112.50	29.9	14.1	72.2
135.00	26.6	14.7	70.7
157.50	59.1	14.1	101.5
180.00	76.6	16.5	126.0
202.50	49.1	25.0	126.4
225.00	15.6	14.2	58.3
247.50	8.3	5.7	25.4
270.00	10.0	6.2	28.7
292.50	16.1	10.4	47.3
315.00	24.0	16.0	72.8
337.50	50.0	20.4	111.3

LOCATION 7

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	50.3	20.8	112.7
22.50	60.1	19.7	119.2
45.00	69.4	16.3	118.3
67.50	78.5	13.8	120.0
90.00	67.5	13.2	109.0
112.50	51.8	14.0	93.9
135.00	29.0	13.1	68.2
157.50	31.4	12.5	67.0
180.00	66.7	16.1	114.9
202.50	70.7	13.9	112.4
225.00	83.1	13.6	124.0
247.50	60.7	13.9	102.4
270.00	40.5	17.1	91.9
292.50	23.0	14.4	66.2
315.00	26.3	14.6	70.2
337.50	30.0	18.3	84.9

LOCATION 8

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	18.4	7.0	39.4
22.50	15.0	4.5	28.6
45.00	17.7	6.8	38.1
67.50	29.0	16.6	78.6
90.00	57.0	19.5	115.6
112.50	65.2	15.8	112.6
135.00	43.4	12.9	82.2
157.50	20.2	10.2	58.8
180.00	39.8	11.4	73.9
202.50	50.6	12.2	87.3
225.00	66.5	11.6	101.2
247.50	50.5	10.2	88.9
270.00	48.5	14.9	93.2
292.50	33.6	15.4	79.7
315.00	27.6	12.3	64.5
337.50	24.6	11.5	59.2

TABLE 2 -- PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

CONFIGURATION H

LOCATION 9

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	11.9	8.9	38.4
22.50	11.1	7.5	33.5
45.00	10.0	6.9	30.7
67.50	11.8	8.9	38.6
90.00	27.6	15.9	77.4
112.50	46.2	17.2	97.6
135.00	44.9	11.3	78.7
157.50	36.0	11.6	70.7
180.00	16.1	8.3	41.0
202.50	18.6	10.2	49.2
225.00	37.6	12.3	74.5
247.50	36.7	14.6	80.5
270.00	42.6	19.2	100.3
292.50	24.9	15.5	71.4
315.00	19.0	13.0	57.9
337.50	11.7	6.8	30.2

LOCATION 10

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	60.3	23.8	131.7
22.50	36.2	19.9	96.7
45.00	20.2	8.0	44.3
67.50	22.6	8.4	47.9
90.00	34.6	16.4	83.9
112.50	61.7	14.4	105.0
135.00	80.3	12.1	116.6
157.50	88.6	13.9	130.3
180.00	68.6	14.5	112.0
202.50	37.7	14.6	81.6
225.00	23.1	8.1	47.4
247.50	25.1	8.7	51.2
270.00	35.3	13.6	75.9
292.50	47.2	21.0	110.1
315.00	47.9	22.8	116.4
337.50	67.0	23.1	136.4

LOCATION 11

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	64.4	15.7	111.5
22.50	56.6	14.8	100.9
45.00	36.7	19.2	94.3
67.50	15.4	11.1	48.8
90.00	17.9	13.0	56.8
112.50	12.4	7.8	35.9
135.00	18.2	12.2	54.7
157.50	25.5	15.3	71.3
180.00	42.8	18.1	97.0
202.50	44.2	15.4	90.3
225.00	46.0	12.9	84.6
247.50	32.9	14.1	75.3
270.00	27.5	13.0	66.6
292.50	29.3	12.8	67.6
315.00	32.3	13.8	73.6
337.50	43.4	13.1	82.7

LOCATION 12

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	11.9	7.8	35.2
22.50	30.8	12.6	68.6
45.00	42.5	14.2	85.1
67.50	32.8	13.1	72.1
90.00	31.7	13.5	72.1
112.50	34.4	14.1	76.8
135.00	34.0	13.5	74.4
157.50	29.7	12.4	63.8
180.00	24.7	10.9	57.3
202.50	25.7	11.6	60.6
225.00	31.6	15.2	77.0
247.50	21.0	11.6	55.6
270.00	18.0	9.7	47.2
292.50	25.9	10.7	58.0
315.00	21.0	10.8	53.3
337.50	19.9	10.8	52.2

TABLE 2 -- PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

CONFIGURATION H

LOCATION 13

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	33.3	9.9	62.9
22.50	19.3	6.2	37.8
45.00	25.7	9.5	54.1
67.50	38.9	10.2	69.5
90.00	46.3	11.8	81.6
112.50	45.7	13.2	85.4
135.00	32.7	11.5	67.1
157.50	16.0	5.1	31.2
180.00	12.9	8.3	37.9
202.50	14.2	4.2	26.9
225.00	13.7	3.7	24.7
247.50	14.4	3.9	26.0
270.00	35.4	12.6	73.3
292.50	42.3	15.2	87.8
315.00	50.6	11.7	85.7
337.50	44.3	9.5	72.7

LOCATION 14

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	42.6	10.0	72.6
22.50	33.5	9.2	61.2
45.00	24.5	7.7	47.7
67.50	16.9	5.5	33.3
90.00	22.9	9.4	51.0
112.50	39.3	10.9	72.1
135.00	56.8	11.2	90.3
157.50	57.6	11.8	92.9
180.00	43.6	13.9	85.4
202.50	20.2	7.4	42.3
225.00	23.1	9.4	51.4
247.50	16.5	6.0	34.5
270.00	13.0	3.1	22.2
292.50	14.1	3.4	24.2
315.00	18.6	5.8	36.1
337.50	29.1	7.3	51.1

LOCATION 15

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	43.6	11.2	77.1
22.50	43.8	9.2	71.5
45.00	37.0	8.1	61.4
67.50	28.6	8.7	54.7
90.00	19.1	6.2	37.8
112.50	27.7	8.1	52.0
135.00	36.4	8.0	60.3
157.50	47.1	8.5	72.5
180.00	52.8	9.1	80.0
202.50	45.8	10.7	77.9
225.00	40.2	16.8	90.4
247.50	23.7	12.0	62.6
270.00	24.1	8.1	48.5
292.50	21.3	7.3	43.2
315.00	26.8	11.2	60.4
337.50	29.6	14.5	73.1

LOCATION 16

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	56.8	12.2	93.4
22.50	63.9	15.0	108.8
45.00	51.8	14.9	96.5
67.50	37.8	11.0	70.9
90.00	30.0	14.2	72.6
112.50	27.9	13.0	66.9
135.00	32.8	9.9	62.5
157.50	53.1	10.9	85.9
180.00	64.0	13.5	104.6
202.50	59.4	15.4	105.7
225.00	35.2	16.8	85.7
247.50	18.7	11.8	52.0
270.00	20.7	7.7	43.9
292.50	25.7	9.9	55.3
315.00	38.8	18.9	95.6
337.50	50.3	16.3	107.2

TABLE 2 PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

CONFIGURATION H

LOCATION 17

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	61.1	16.0	109.2
22.50	63.7	14.4	107.0
45.00	56.6	13.1	95.9
67.50	40.5	11.1	81.9
90.00	35.4	10.6	67.4
112.50	22.9	7.9	46.7
135.00	22.1	8.3	47.0
157.50	35.4	8.0	59.6
180.00	52.8	10.4	83.9
202.50	58.4	12.3	95.2
225.00	64.5	13.5	105.0
247.50	58.7	12.5	96.2
270.00	40.6	16.9	91.4
292.50	27.7	11.6	62.4
315.00	32.0	13.6	72.9
337.50	60.5	19.3	118.6

LOCATION 18

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	45.7	10.4	76.7
22.50	53.9	9.9	83.6
45.00	47.3	9.5	75.9
67.50	38.1	9.1	65.2
90.00	33.7	8.8	60.0
112.50	32.5	9.0	59.6
135.00	32.0	9.7	61.1
157.50	37.0	9.3	64.8
180.00	44.3	10.0	74.3
202.50	46.1	9.8	75.6
225.00	46.6	10.7	78.6
247.50	43.2	10.7	75.4
270.00	41.0	14.9	85.6
292.50	24.3	10.3	55.2
315.00	23.4	11.0	56.5
337.50	38.5	13.0	77.5

LOCATION 19

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	32.3	15.8	79.8
22.50	57.2	18.4	112.3
45.00	70.2	14.1	112.5
67.50	62.0	11.6	93.8
90.00	53.4	9.4	81.7
112.50	46.7	9.3	74.6
135.00	38.3	9.8	67.1
157.50	38.6	10.0	68.7
180.00	37.6	10.5	69.0
202.50	41.3	10.3	72.1
225.00	42.9	8.5	68.3
247.50	47.6	10.3	78.5
270.00	51.3	10.7	83.5
292.50	54.0	14.0	96.1
315.00	52.7	17.2	104.2
337.50	32.3	16.0	80.2

LOCATION 20

WIND AZIMUTH	U/UR (PERCENT)	URMS/UR (PERCENT)	U+3.0*RMS/UR (PERCENT)
0.00	33.2	16.4	82.5
22.50	30.7	12.7	68.7
45.00	34.1	15.5	80.8
67.50	55.4	21.4	119.7
90.00	60.9	13.5	101.3
112.50	55.0	9.6	84.0
135.00	51.8	8.7	78.0
157.50	44.2	8.7	70.4
180.00	32.4	8.8	58.7
202.50	21.6	7.7	44.6
225.00	24.1	7.5	46.6
247.50	31.3	8.9	58.1
270.00	42.8	11.0	75.8
292.50	55.0	12.8	93.3
315.00	53.0	13.3	92.8
337.50	56.1	14.5	99.5

TABLE 2 -- PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

CONFIGURATION H

** GREATEST VALUES **

UMEAN/UINF (PERCENT)

LOC	AZ	MEAN	RMS	M+3.0RMS
10	157.5	88.6	13.9	130.3
7	225.0	83.1	13.6	124.0
2	135.0	82.2	12.7	120.1
10	135.0	80.3	12.1	116.6
7	67.5	78.5	13.8	120.0
6	180.0	76.6	16.5	126.0
6	0.0	74.2	15.5	120.6
2	112.5	70.7	12.6	108.6
7	202.5	70.7	13.9	112.4
19	45.0	70.2	14.1	112.5

URMS/UINF (PERCENT)

LOC	AZ	MEAN	RMS	M+3.0RMS
6	202.5	49.1	25.8	126.4
2	157.5	49.9	24.4	123.0
1	157.5	48.8	23.8	120.2
10	0.0	60.3	23.8	131.7
10	337.5	67.0	23.1	136.4
10	315.0	47.9	22.8	116.4
2	225.0	46.3	22.2	112.9
4	315.0	27.0	21.9	92.6
20	67.5	55.4	21.4	119.7
2	247.5	44.1	21.3	108.1

UMEAN+3.0*RMS/UINF (PERCENT)

LOC	AZ	MEAN	RMS	M+3.0RMS
10	337.5	67.0	23.1	136.4
10	0.0	60.3	23.8	131.7
10	157.5	88.6	13.9	130.3
6	202.5	49.1	25.8	126.4
6	180.0	76.6	16.5	126.0
7	225.0	83.1	13.6	124.0
2	157.5	49.9	24.4	123.0
6	0.0	74.2	15.5	120.6
1	157.5	48.8	23.8	120.2
2	135.0	82.2	12.7	120.1

TABLE 3

PERCENTAGE FREQUENCY OF WIND DIRECTION AND SPEED

DALLAS, TEXAS LOVE FIELD (1951-1960)

SEASON: ANNUAL NO. OF OBS. = 87672 HT. OF MEAS. = 40 ft.

VELOCITY LEVELS IN MPH

DIRECTION	0- 3	4- 7	8-12	13-18	19-24	25-31	32-38	39-46	47 +	TOTAL
N	.59	1.48	1.90	1.45	.52	.10	.03	0.00	0.00	6.07
NNE	.46	1.44	1.52	1.11	.31	.05	0.00	0.00	0.00	4.89
NE	.67	2.23	1.60	.65	.25	.03	0.00	.03	0.00	5.47
ENE	.28	1.09	1.35	.61	.20	.04	0.00	0.00	0.00	3.58
E	.42	1.29	1.52	.53	.22	.01	0.00	0.00	0.00	3.99
ESE	.32	1.28	2.17	.92	.25	.05	0.00	0.00	0.00	4.99
SE	.64	2.90	5.37	3.31	.54	.06	.01	0.00	0.00	12.82
SSE	.31	1.74	5.24	6.44	1.68	.17	.06	.02	0.00	15.67
S	.56	1.87	4.94	6.02	2.13	.25	.05	.02	0.00	15.83
SSW	.30	.90	1.51	2.02	.66	.11	.01	0.00	0.00	5.51
SW	.55	1.08	1.22	.93	.27	.08	.01	.03	0.00	4.16
WSW	.19	.36	.30	.35	.16	.04	.02	.01	0.00	1.42
W	.33	.56	.47	.34	.20	.05	.02	.02	0.00	2.00
WNW	.27	.49	.56	.52	.31	.07	.03	0.00	0.00	2.25
NW	.50	1.14	1.06	1.07	.50	.12	.06	.03	0.00	4.49
NNW	.37	1.08	1.48	1.43	.56	.10	.06	0.00	0.00	5.08
CALM	1.78	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.78
TOT	8.54	20.92	32.21	27.69	8.76	1.34	.36	.16	0.00	100.00

TABLE 4

SUMMARY OF WIND EFFECTS ON PEOPLE

	Beaufort number	Speed (mph)	Effects
Calm, light air	0, 1	0- 3	Calm, no noticeable wind
Light breeze	2	4- 7	Wind felt on face
Gentle breeze	3	8-12	Wind extends light flag Hair is disturbed Clothing flaps
Moderate breeze	4	13-18	Raises dust, dry soil and loose paper Hair disarranged
Fresh breeze	5	19-24	Force of wind felt on body Drifting snow becomes airborne Limit of agreeable wind on land
Strong breeze	6	25-31	Umbrellas used with difficulty Hair blown straight Difficult to walk steadily Wind noise on ears unpleasant Windborne snow above head height (blizzard)
Near gale	7	32-38	Inconvenience felt when walking
Gale	8	39-46	Generally impedes progress Great difficulty with balance in gusts
Strong gale	9	47-54	People blown over by gusts

Note: Table from Reference 4, p. 40.

TABLE 5

SELECTION OF WIND SPEEDS
AND
REFERENCE DYNAMIC PRESSURE

1. Basic wind speeds from fastest mile winds measured at Dallas (1941-1972)*:

   Largest 100-year fastest mile at 30 ft = 69 mph for west winds.

   Mean hourly wind speed at 30 ft = $\frac{69}{1.27}$ = 54.3 mph.

   Mean hourly gradient wind speed = $54.3\ (\frac{960}{30})^{.17}$ = 97.9 mph.

   Reference pressure at site of gradient height of 1250 ft = $(0.00256)(97.9^2)$ = 25 psf.

2. Loads including directional effects for Dallas*:

Wind Direction	100 yr. Fastest Mile, mph 30 ft.	Mean Hourly Gradient Wind Speed (ws) mph	Load Ratio $(ws/max\ ws)^2$
N	65	93	.90
NE	56	81	.68
E	50	73	.55
SE	64	92	.88
S	57	82	.70
SW	61	88	.81
W	69	98	1.00
NW	66	94	.92

3. For 50-year recurrence winds:

   Divide 100-year winds by 1.14 to obtain 50-year winds.

4. Gust load factors to convert hourly mean integrated load to mean load for various gust durations (see Section 4.4):

Duration (sec)	Gust Load Factor
10-15	1.40^2 = 1.96
30	1.32^2 = 1.74**
45	1.28^2 = 1.64

* National Climatic Center, Asheville, North Carolina.
** Thirty second factor was used in Table 7.

TABLE 6A. PEAK LOADS FOR CONFIGURATION A :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)
101	280	-1.29	-32.4	27.6	149	300	2.61	60.1	30.1	197	150	1.09	-24.1	21.0
102	280	-1.42	-35.6	24.3	150	250	2.44	60.9	30.3	198	250	1.62	-40.5	26.7
103	290	-1.38	-34.4	27.0	151	280	1.34	33.6	30.4	199	290	1.08	-27.0	25.5
104	120	-1.55	-34.0	26.0	152	20	1.16	21.9	26.2	200	290	1.97	-49.2	23.5
105	260	-1.31	-32.8	18.8	153	330	1.35	31.1	23.9	201	250	1.20	-30.1	26.3
106	290	-1.40	-35.0	26.5	154	340	1.35	30.3	29.4	202	250	1.32	-33.0	26.4
107	290	-1.59	-39.7	26.9	155	250	1.47	33.7	28.8	203	250	1.21	-30.3	28.4
108	290	-1.48	-37.0	27.6	156	10	1.36	28.4	30.7	204	330	1.20	-27.5	23.3
109	290	-2.06	-51.4	30.0	157	290	1.20	30.1	29.9	205	250	.93	-24.6	21.1
110	10	-1.43	-32.1	27.9	158	290	1.46	36.5	30.0	206	250	1.17	-29.3	22.5
111	290	-1.07	-26.7	24.7	159	300	1.75	40.3	31.9	207	240	1.44	-29.1	22.3
112	10	1.56	-34.4	35.1	160	250	-1.39	-34.8	33.7	208	350	1.30	-29.2	26.1
113	290	-1.32	-33.0	32.5	161	250	1.85	46.3	30.0	209	20	1.00	-22.3	22.4
114	290	-1.53	-38.3	27.7	162	250	1.81	45.2	30.6	210	260	-.92	-22.9	21.4
115	280	-1.70	-42.5	26.4	163	20	1.14	24.5	25.3	211	290	1.23	-30.8	18.8
116	290	-1.43	-35.8	29.3	164	350	1.27	28.7	23.8	212	350	1.40	-31.5	27.3
117	250	1.06	26.5	21.5	165	310	1.40	32.1	24.5	213	120	1.22	-29.8	23.8
118	280	-1.31	-32.7	23.5	166	260	1.45	36.1	27.0	214	250	.93	-23.3	20.2
119	10	1.45	30.1	32.7	167	290	1.13	28.2	25.9	215	20	.98	-21.9	22.0
120	280	-1.20	-30.0	29.7	168	280	-1.37	-34.2	26.6	216	90	1.90	-26.1	22.2
121	290	-1.31	-32.7	28.6	169	290	1.44	35.9	27.5	217	290	-1.90	-47.5	25.6
122	290	-1.31	-32.7	26.0	170	240	-1.45	-29.4	27.7	218	250	1.12	28.0	23.5
123	300	-1.53	-35.3	28.8	171	260	-1.32	-33.0	28.0	219	250	1.20	-30.1	23.2
124	260	-1.12	-27.9	25.1	172	250	1.25	31.2	28.5	220	250	1.93	-48.3	24.1
125	20	.95	21.3	21.4	173	340	1.18	26.6	24.2	221	330	-1.01	-23.2	20.0
126	280	-1.04	-25.9	23.8	174	290	-1.12	-27.9	24.1	222	260	-1.14	-28.4	13.6
127	350	1.20	26.4	26.9	175	310	1.22	28.1	25.7	223	320	1.03	23.7	12.6
128	280	-1.41	-35.2	24.7	176	250	1.39	34.9	32.9	224	0	1.04	-19.7	23.5
129	290	-1.24	-31.1	26.9	177	290	1.10	27.6	27.5	225	0	1.11	10.5	25.1
130	280	-1.66	-41.6	29.9	178	290	-1.50	-37.5	28.8	226	350	1.19	-25.2	26.8
131	340	-1.59	-35.8	24.2	179	290	1.28	32.1	28.6	227	20	-.94	21.2	18.0
132	270	-1.12	-28.0	23.7	180	280	-1.53	-38.1	26.2	228	310	1.21	-19.9	27.8
133	10	1.25	-24.0	28.2	181	250	1.28	32.1	29.6	229	20	-1.10	-24.7	23.3
134	340	1.28	-27.9	28.7	182	250	1.23	30.8	27.9	230	240	-1.27	-25.6	14.0
135	290	-1.30	-32.5	29.7	183	270	1.44	35.9	28.9	231	20	-.95	21.4	20.4
136	280	-1.88	-47.0	29.5	184	330	-1.15	26.5	23.2	232	140	-.82	-18.1	15.4
137	20	-1.67	-37.5	34.8	185	330	-1.29	29.7	22.9	233	330	-.82	18.9	17.0
138	330	-1.36	-31.3	25.3	186	340	-1.42	-31.9	26.1	234	330	-.98	-22.7	15.7
139	250	-1.13	-28.2	26.9	187	250	1.15	28.8	25.4	235	180	-.66	-11.6	10.4
140	10	1.26	27.1	28.4	188	290	1.27	31.7	27.1	236	250	-.51	-12.8	8.8
141	290	-1.27	-31.7	29.4	189	290	1.31	32.7	24.0	237	260	-.50	-12.6	9.5
142	280	-1.79	-44.8	30.6	190	280	-1.47	-36.8	24.3	238	300	-.58	-13.4	8.2
143	330	1.35	27.9	31.1	191	20	-1.44	-32.4	27.0	239	320	.94	-19.2	21.7
144	120	-1.60	-35.3	27.6	192	250	-1.56	39.0	26.4	240	290	.87	-15.4	21.7
145	260	-1.27	-31.8	30.6	193	250	-1.35	33.7	27.1	241	290	.93	-18.5	23.3
146	350	1.26	-27.4	28.2	194	330	-1.17	27.0	21.2	301	290	1.26	-30.4	31.4
147	290	-1.22	-30.4	29.1	195	350	-1.34	30.2	22.6	302	0	1.33	-30.0	26.9
148	290	-1.24	-31.0	30.2	196	340	-1.42	31.9	23.9	303	280	1.19	-28.8	29.8

TABLE 6A. PEAK LOADS FOR CONFIGURATION A :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK
			--- PSF ----					---- PSF ----					---- PSF ----	
304	10	-1.82	-41.0	32.6	352	350	1.41	30.7	31.6	400	210	-1.35	-27.4	23.9
305	350	-1.38	-31.1	27.9	353	250	1.95	48.6	33.7	401	330	-1.60	-36.9	24.4
306	0	-1.51	-34.0	31.7	354	260	-1.38	-34.5	29.9	402	310	-1.86	-42.8	26.6
307	270	1.25	-26.9	31.2	355	270	1.27	30.3	31.8	403	320	-1.34	-30.8	23.6
308	150	-1.29	-28.4	27.4	356	270	1.36	30.0	34.0	404	200	-1.50	-37.5	26.0
309	180	-2.20	-38.6	29.5	357	280	1.23	-26.4	30.8	405	290	1.13	-25.6	28.2
310	270	-1.38	-34.5	30.4	358	270	1.24	-25.4	31.0	406	200	1.09	-21.2	27.2
311	0	-1.76	-39.6	30.0	359	260	1.27	-31.3	31.7	407	260	1.08	-22.0	27.0
312	280	1.30	-32.3	32.6	360	260	1.39	32.3	34.8	408	270	1.10	-27.1	29.6
313	290	1.37	-28.6	34.2	361	260	1.21	29.4	30.3	409	300	-1.41	-32.3	22.5
314	280	1.46	-28.9	36.6	362	250	1.43	30.9	35.0	410	290	1.05	-25.5	26.3
315	210	-1.67	-33.9	32.3	363	240	-1.36	-27.5	27.5	411	280	.94	-22.0	23.5
316	290	-1.22	-30.6	30.6	364	250	-1.24	31.0	30.2	412	290	-.96	-23.9	21.0
317	300	1.43	-29.4	32.8	365	250	1.25	-31.1	28.2	413	20	-1.67	-37.5	28.1
318	290	1.33	-31.5	33.2	366	350	-1.30	-29.3	29.1	414	290	1.00	-24.5	25.1
319	290	1.41	-26.3	35.3	367	290	1.19	-29.5	29.7	415	250	-1.01	-25.2	22.5
320	300	1.41	-24.0	32.4	368	270	1.15	-24.9	28.8	416	0	1.50	-35.4	26.8
321	270	1.44	-23.8	36.1	369	260	1.36	-29.7	33.9	417	210	-1.44	-29.2	25.4
322	260	1.14	-25.9	28.5	370	290	1.26	-31.6	27.7	418	290	-1.15	-28.8	26.1
323	150	-1.51	-33.2	31.2	371	260	1.19	-27.5	29.8	419	320	-1.03	-23.6	23.0
324	0	-1.59	-35.7	28.9	372	260	1.18	-27.4	29.4	420	250	.87	-21.7	21.7
325	300	1.28	-28.1	29.3	373	330	1.21	-27.8	27.9	421	300	1.07	-19.4	24.6
326	280	1.41	-30.1	35.4	374	260	-1.19	-29.7	25.0	422	20	-1.13	-25.5	23.5
327	280	1.41	-25.5	35.2	375	270	-1.39	34.8	30.1	423	290	1.09	-25.4	27.3
328	270	1.32	-25.4	33.1	376	350	-1.40	-31.6	29.3	424	300	1.17	-20.3	26.8
329	290	1.20	-24.9	29.9	377	0	-1.23	27.7	26.8	425	270	1.00	-22.0	24.9
330	250	1.27	-31.4	31.8	378	290	1.17	-27.4	29.2	426	300	1.23	-25.0	28.2
331	20	-1.66	-37.2	32.2	379	280	1.19	-27.5	29.8	427	270	.94	-19.4	23.6
332	0	-1.46	-32.8	28.4	380	210	1.41	28.5	26.1	428	250	1.25	-27.8	31.3
333	350	-1.40	-31.4	30.9	381	310	-1.62	37.2	29.0	429	270	.86	-21.4	21.4
334	260	1.27	-25.3	31.8	382	290	-1.19	29.7	25.4	430	290	1.36	-22.2	34.1
335	260	1.32	-27.5	32.9	383	310	-1.13	-26.0	24.4	431	190	1.20	-21.0	20.7
336	210	-1.58	-32.0	30.8	384	310	1.29	-26.9	29.7	432	330	1.03	-19.6	23.6
337	260	1.30	-29.7	32.5	385	250	-1.28	-32.0	27.4	433	290	.96	-21.2	23.9
338	280	-1.31	-32.6	31.3	386	260	-1.44	-36.1	27.1	434	10	-1.05	-23.7	22.3
339	0	-1.83	-41.3	32.3	387	340	-1.58	-35.5	30.3	435	290	.95	-18.2	23.7
340	290	1.37	-28.0	34.2	388	350	-1.39	-31.4	26.8	436	300	.97	-15.4	22.3
341	270	1.22	-24.5	30.6	389	270	1.10	-26.5	27.5	437	260	.92	-16.1	23.1
342	260	1.24	-30.1	31.1	390	270	1.19	28.2	29.6	438	280	.98	-18.9	24.5
343	250	1.18	-28.7	29.4	391	300	-2.00	-46.0	24.8	439	320	-1.10	-27.0	20.2
344	20	-2.40	-54.0	38.2	392	320	-1.65	-38.0	25.2	440	290	-1.09	-27.2	25.9
345	350	-2.13	-47.9	31.9	393	330	1.18	-27.2	25.6	441	130	-1.36	-30.0	23.3
346	350	-1.39	-31.3	31.2	394	20	1.24	-28.0	23.9	442	240	1.29	-15.8	26.2
347	290	1.32	-26.1	32.9	395	260	-1.34	-33.5	26.2	443	250	-.91	-22.6	21.2
348	270	1.17	-25.3	29.2	396	250	1.84	-45.9	24.4	444	260	1.02	-12.9	25.4
349	210	-2.22	-45.1	30.4	397	0	-1.60	-36.0	28.4	445	290	1.00	-20.3	25.0
350	250	1.26	-24.9	31.4	398	290	1.25	28.5	31.3	501	280	-1.37	-34.2	28.3
351	280	1.24	-24.4	30.9	399	250	1.14	25.5	28.6	502	290	-1.45	-36.3	22.3

TABLE 6A. PEAK LOADS FOR CONFIGURATION A :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)
503	140	-1.47	-32.2	25.4	551	210	1.25	-23.7	25.3	599	320	-1.40	-32.2	22.4
504	280	-1.72	-42.9	24.6	552	300	-1.42	-32.6	26.9	600	320	-1.46	-33.5	13.1
505	280	-1.14	-28.4	22.2	553	290	-1.38	-34.6	33.1	601	260	-1.44	-36.0	6.8
506	150	1.20	-26.4	26.5	554	220	1.34	-25.8	27.1	602	230	-1.42	-28.7	11.5
507	350	-1.37	-30.8	24.8	555	280	-1.15	-28.7	27.9	603	20	-1.39	-31.2	13.9
508	120	-2.46	-54.2	17.6	556	290	-1.22	-30.5	26.5	604	270	1.21	-27.5	30.3
509	120	-1.69	-37.3	24.4	557	290	-1.03	-25.7	25.0	605	320	-1.38	-31.8	19.9
510	290	-1.51	-37.7	24.0	558	150	-1.26	-27.7	25.7	606	320	-1.09	-25.1	21.9
511	270	-1.82	-45.6	33.0	559	290	-1.05	-26.3	14.3	607	320	-1.35	-31.1	22.5
512	280	-1.34	-33.5	25.6	560	250	-1.27	-31.7	10.5	608	270	-1.16	-29.0	21.3
513	290	-1.10	-27.6	26.0	561	250	-1.21	-30.2	15.1	609	200	-1.66	-29.0	21.8
514	350	-1.39	-31.2	23.9	562	130	-1.15	-25.2	12.8	610	320	-1.04	-23.8	19.0
515	120	-2.17	-47.8	14.7	563	290	-1.21	-30.2	30.0	611	320	1.13	-26.1	21.0
516	130	-1.30	-28.5	23.9	564	300	-1.43	-32.8	25.2	612	250	-1.09	-27.2	18.0
517	220	1.48	-26.8	29.9	565	290	-1.16	-29.1	25.2	613	310	-2.16	-49.8	24.1
518	290	-1.27	-31.7	26.0	566	290	-1.48	-37.1	25.7	614	300	-1.36	-31.2	22.5
519	290	-1.03	-25.6	24.7	567	290	-1.26	-31.4	26.4	615	300	-1.32	-30.4	21.8
520	280	-1.02	-25.5	25.2	568	280	-1.07	-26.7	24.2	616	320	-1.33	-30.6	20.0
521	120	-1.28	-28.1	24.3	569	290	.99	-24.7	13.9	617	20	-1.28	-28.8	15.7
522	340	-1.82	-41.1	18.1	570	230	-1.45	-29.3	7.6	618	270	-1.00	-25.0	15.3
523	350	-1.90	-42.8	11.9	571	250	-1.12	-28.1	15.4	619	130	-1.13	-25.0	18.9
524	280	-1.78	-44.5	26.4	572	130	-1.14	-25.0	10.9	620	20	-1.55	-34.9	15.2
525	260	-1.25	-31.4	23.7	573	320	-1.44	-33.1	30.2	621	320	-1.11	-25.6	21.5
526	270	-1.19	-29.7	21.2	574	310	-1.69	-38.8	24.3	622	320	-1.23	-28.3	25.3
527	170	1.57	-26.3	27.5	575	250	1.07	25.7	26.8	623	320	-1.02	-23.6	19.9
528	290	-.97	-24.3	23.7	576	280	-1.26	-31.4	24.0	624	20	-.95	-21.4	19.9
529	120	-1.17	-25.8	16.2	577	280	-1.11	-27.8	23.6	625	320	1.50	-34.5	22.1
530	310	-1.51	-34.7	16.6	578	290	-1.20	30.0	23.7	626	210	1.09	-21.1	22.1
531	310	-1.65	-38.0	26.4	579	290	-1.17	-27.2	23.1	627	330	-1.14	-26.2	12.5
532	280	-1.44	-36.0	27.4	580	320	-1.24	-28.5	13.7	628	130	-1.18	-25.9	12.8
533	140	-1.37	-30.2	23.2	581	250	-1.38	-34.6	23.2	629	130	-.99	-21.8	18.5
534	150	-1.33	-29.3	25.4	582	250	-1.34	-33.6	12.4	630	320	-1.06	-24.4	18.0
535	140	-1.34	-29.4	21.2	583	20	1.16	-26.1	12.2	631	320	-1.06	-24.4	15.1
536	350	-1.45	-32.7	13.5	584	310	-1.33	-30.6	29.2	632	320	-1.03	-23.6	22.5
537	250	-1.20	-30.0	18.7	585	310	-1.99	-45.8	22.8	633	320	-1.07	-24.7	20.4
538	230	1.50	-27.6	30.4	586	250	1.24	-29.6	30.9	634	310	-1.03	-23.7	20.2
539	280	-1.57	-39.3	28.1	587	320	1.53	-35.3	12.1	635	320	1.12	-25.7	18.0
540	280	-1.35	-33.8	23.8	588	310	-1.29	-29.6	22.8	636	320	-1.44	-33.1	23.3
541	290	-1.00	-24.9	21.3	589	270	1.04	26.0	22.7	637	320	-1.06	-24.3	19.4
542	300	-1.12	-25.8	16.0	590	320	-1.18	-27.1	14.0	638	330	-.95	-21.9	21.2
543	250	-1.03	-25.8	16.6	591	260	-1.71	-42.7	13.9	639	320	-1.13	-26.0	23.2
544	300	-2.81	-64.6	27.5	592	250	-1.25	-31.2	14.1	640	330	-2.15	-49.3	17.3
545	290	-1.82	-45.5	23.8	593	250	-1.36	-34.0	11.1	641	320	-1.50	-34.6	26.0
546	300	-1.42	-32.6	27.7	594	320	-1.41	-32.3	26.3	701	140	-1.43	-31.4	28.3
547	220	1.25	-23.6	25.4	595	310	-1.74	-40.1	22.7	702	120	1.52	-30.0	33.5
548	290	-1.14	-28.4	24.8	596	320	-1.24	-28.4	21.8	703	0	-1.33	-30.0	26.3
549	350	-1.11	-25.0	18.1	597	320	-1.50	-34.6	22.1	704	180	-1.77	-31.4	28.4
550	20	-1.66	-37.4	19.3	598	280	-1.33	-33.2	22.8	705	170	-1.94	-33.9	23.1

TABLE 6A. PEAK LOADS FOR CONFIGURATION A :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)
706	300	-1.40	-32.1	31.7	754	250	-1.06	-26.4	6.5	802	330	-1.40	-32.1	20.5
707	120	1.30	-28.0	28.7	755	350	1.16	-26.0	16.2	803	350	-1.49	-33.6	22.6
708	250	-1.33	-33.2	20.4	756	120	1.30	-26.4	28.5	804	150	-.76	-21.1	18.8
709	10	-1.96	-44.1	27.4	757	120	1.29	-23.2	28.5	805	120	1.13	-24.0	24.8
710	120	-1.41	-31.1	24.6	758	120	1.47	-24.3	32.3	806	130	1.17	-23.9	25.7
711	170	-2.35	-41.1	17.9	759	150	-1.35	-29.6	21.1	807	240	-1.20	-24.2	23.5
712	300	-1.65	-38.0	28.3	760	340	-1.20	-28.9	23.6	808	250	-.76	-23.9	21.7
713	300	-1.45	-33.4	30.7	761	350	-1.47	-33.0	25.8	809	40	-1.47	-24.9	11.7
714	120	1.47	-30.0	32.4	762	320	-1.34	-30.8	24.0	810	270	-.93	-23.4	17.8
715	20	-1.73	-38.8	26.0	763	250	-1.14	-28.5	17.2	811	330	-1.43	-32.8	19.6
716	0	-1.77	-39.9	22.9	764	260	-1.06	-26.6	14.4	812	260	-.98	-24.5	21.7
717	150	-1.84	-40.5	15.4	765	130	-1.22	26.8	14.7	813	270	-1.69	-42.3	13.3
718	140	-1.38	-30.4	20.3	766	340	-1.07	-24.0	14.6	814	230	-1.37	-27.7	11.3
719	300	-1.48	-34.1	29.7	767	120	1.24	-23.4	27.3	815	140	-1.29	-28.3	14.0
720	300	-1.29	-29.7	28.9	768	350	-1.19	26.8	23.6	816	250	-1.54	-38.6	20.0
721	120	1.46	-30.0	32.1	769	150	-1.23	27.1	21.6	817	10	-1.37	-30.9	19.5
722	10	-1.31	-29.5	25.2	770	340	-1.13	25.4	20.0	818	330	-.98	-22.6	22.4
723	0	-1.23	-27.7	19.1	771	0	-1.30	-29.3	24.0	819	340	-1.29	-29.1	21.8
724	300	-1.45	-33.3	12.6	772	340	-1.25	28.0	23.1	820	350	-2.16	-48.6	22.3
725	150	-1.36	-30.0	20.8	773	260	-1.17	-29.3	17.1	821	220	-1.04	-21.0	16.9
726	120	1.22	-26.8	26.9	774	250	1.30	32.6	14.0	822	130	-1.18	-26.0	12.7
727	120	1.33	-23.6	29.3	775	120	-1.45	-31.9	18.2	823	230	-1.28	-25.8	13.3
728	10	-1.22	-27.5	26.1	776	260	-.96	-24.0	14.5	824	210	-1.17	-23.6	18.4
729	10	-1.24	-28.0	24.7	777	250	-1.21	-30.3	27.6	825	330	1.17	-26.9	21.1
730	0	-1.92	-43.1	20.6	778	0	-1.13	25.3	24.9	826	320	-1.12	-25.8	19.6
731	250	-1.59	-39.6	17.5	779	320	-1.68	-38.7	27.7	827	330	-1.05	-24.2	14.8
732	300	-1.55	-35.6	15.4	780	10	-1.34	-30.2	21.0	828	330	-.78	-18.0	14.7
733	130	-1.34	-29.6	25.4	781	350	-1.13	-25.4	21.4	829	250	-.94	-23.5	16.3
734	150	-1.24	-27.2	26.4	782	350	-1.31	-27.4	25.7	830	220	-1.60	-32.3	13.2
735	150	-1.49	-32.7	26.2	783	340	-1.32	29.6	25.9	831	320	-1.19	-27.4	17.8
736	150	-1.48	-32.6	21.4	784	250	-1.31	32.7	11.7	832	320	-1.04	-23.9	17.3
737	0	-1.40	-31.4	22.0	785	250	-1.19	29.7	16.9	833	130	-1.18	-26.0	15.2
738	250	-1.18	-29.5	14.1	786	130	-1.57	34.5	10.2	834	130	-1.21	-26.7	17.7
739	300	-1.42	-32.6	15.3	787	250	-.97	-24.3	19.3	835	240	-1.03	-20.9	18.5
740	130	-1.19	-26.1	22.8	788	250	-1.37	34.3	28.6	836	250	-.86	-21.5	18.5
741	0	-1.14	-25.6	24.7	789	0	-1.51	-33.9	23.9	837	130	1.05	-20.5	23.1
742	10	-1.59	-35.8	22.9	790	0	-1.35	30.5	18.8	838	330	-1.03	-23.8	21.8
743	0	-1.15	-25.9	22.3	791	340	-1.23	-27.6	21.9	839	340	-1.35	-30.5	13.7
744	220	-2.69	-54.5	15.5	792	320	-1.38	31.7	24.6	840	320	-.85	-19.7	15.9
745	0	-1.45	-32.5	16.9	793	350	-1.41	-31.6	23.3	841	330	-.99	-22.7	17.8
746	0	-1.32	-29.6	27.0	794	270	-1.31	-32.7	10.5	842	330	-.98	-22.6	18.6
747	130	-1.43	-31.5	30.0	795	270	-1.40	35.0	17.0	843	130	1.20	-19.0	26.3
748	130	1.22	-24.7	26.8	796	30	-1.65	-28.0	11.7	844	330	-.92	-21.1	18.4
749	130	-1.43	-31.4	22.2	797	260	-1.23	-30.8	15.2	845	140	1.06	-16.9	23.3
750	330	-2.42	-55.7	24.2	798	250	-1.48	-36.9	25.9	901	320	1.26	-27.3	29.1
751	130	1.33	-22.6	29.3	799	0	-1.40	-31.4	25.7	902	290	-2.07	-51.8	33.0
752	250	-1.20	-30.1	15.1	800	350	1.53	-34.3	21.5	903	350	1.56	-33.8	35.2
753	250	-1.43	-35.7	13.1	801	340	-1.59	-35.8	19.1	904	250	-1.48	-37.1	33.0

TABLE 6A. PEAK LOADS FOR CONFIGURATION A :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ---- PSF	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ---- PSF	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ---- PSF
905	0	2.22	-39.2	49.9	944	280	-1.25	-31.3	4.8	983	260	-1.70	-42.4	15.5
906	20	1.32	-28.5	29.7	945	300	1.59	-28.9	36.5	984	190	-2.12	-37.1	25.8
907	20	1.14	-25.2	25.7	946	260	1.22	-25.1	30.5	985	120	-1.49	-32.8	23.8
908	290	-2.01	-50.3	27.2	947	280	1.29	-24.2	32.4	986	300	-1.40	-32.3	17.0
909	250	-1.33	-33.2	24.7	948	320	-2.22	-51.0	6.1	987	130	-1.21	-26.5	13.7
910	270	-1.11	-27.8	26.7	949	260	-1.47	-36.8	5.0	988	280	-.97	-24.3	21.7
911	280	-1.13	-28.2	22.5	950	280	-1.21	-30.3	5.9	989	200	-1.03	-25.8	18.1
912	270	-.98	-24.6	17.8	951	340	-1.18	-26.6	6.6	990	300	-1.45	-33.5	21.1
913	290	-1.14	-28.6	27.5	952	20	-1.33	-27.8	6.2	991	290	-1.04	-26.1	23.4
914	300	1.34	-21.0	30.9	953	20	-1.62	-36.5	7.0	992	290	-1.39	-34.6	22.0
915	350	-1.29	-29.1	23.0	954	120	1.17	-24.2	25.7	993	310	-1.36	-31.2	16.0
916	280	-1.81	-45.3	24.9	955	120	1.15	-22.4	25.3	994	250	1.03	-24.8	25.9
917	350	-2.72	-61.2	17.4	956	120	1.74	-29.5	38.4	995	300	-1.67	-38.4	30.0
918	350	-2.29	-51.6	9.1	957	290	-1.17	29.3	6.1	996	140	-1.29	-28.4	24.1
919	20	-1.81	-40.7	6.6	958	270	1.39	-27.8	34.9	997	300	-1.31	-30.2	27.5
920	20	-2.14	-48.0	10.1	959	250	-2.56	-64.1	8.4	998	320	-1.39	-32.1	24.6
921	10	-2.07	-46.5	16.7	960	280	-1.75	-43.7	12.5	999	60	-1.38	-23.4	20.4
922	0	-1.76	-39.6	15.8	961	280	-1.39	-34.7	15.7	1000	170	-1.58	-27.7	10.0
923	10	-1.03	-23.2	15.8	962	120	-1.30	-28.5	15.8	1001	350	1.22	-18.1	27.5
924	20	1.14	-23.5	25.6	963	120	-1.70	-37.5	12.9	1002	20	1.09	-21.7	24.5
925	0	-1.86	-41.7	27.2	964	120	-1.62	-35.6	18.9	1003	300	-1.98	-45.6	19.7
926	20	-1.56	-35.2	17.2	965	320	-1.34	-30.7	30.0	1004	280	-.57	-14.2	10.5
927	0	-1.44	-32.5	29.6	966	250	-1.21	-30.3	5.5	1005	340	-.25	-21.5	8.6
928	290	-2.35	-58.7	15.0	967	320	-1.67	-38.3	32.2	1006	250	-.49	-12.2	10.4
929	270	-1.70	-42.5	13.0	968	250	-2.14	-53.5	20.4	1007	250	-.60	-15.0	10.0
930	350	-1.85	-41.6	10.8	969	250	-2.04	-50.9	9.4	1008	270	-.55	-13.7	10.9
931	20	-1.79	-40.2	16.1	970	300	-1.73	-39.9	12.3	1009	290	1.04	-18.1	26.1
932	20	-1.78	-40.1	13.1	971	250	-1.20	-30.1	12.1	1010	330	-1.05	-24.2	20.1
933	50	-2.10	-35.7	10.7	972	210	-1.64	-33.3	25.8	1011	290	1.06	-16.1	26.6
934	10	-1.63	-36.7	21.6	973	120	-1.58	-34.7	28.2	1012	140	1.02	-20.6	22.5
935	350	-1.61	-36.3	5.6	974	250	-1.75	-43.8	24.7	1013	310	1.05	-22.6	24.2
936	0	-1.49	-33.6	30.8	975	210	-1.65	-33.5	29.9	1014	120	.98	-20.4	21.5
937	300	-2.74	-63.1	8.8	976	300	-1.41	-32.4	16.5	1015	270	.89	-20.8	22.1
938	290	-1.77	-44.3	9.0	977	280	-1.58	-39.4	29.2	1016	230	-1.14	-23.1	18.2
939	280	-1.60	-40.1	9.4	978	0	-1.27	-28.5	27.5	1017	310	-.97	-22.3	17.5
940	20	-1.52	-34.2	19.2	979	290	-1.50	-37.5	22.4	1018	320	-1.06	-24.5	20.4
941	350	-1.58	-35.5	11.2	980	210	-1.78	-36.0	14.3	1019	320	-1.22	-28.1	21.1
942	50	-2.53	-43.0	7.5	981	240	-2.35	-47.5	8.3	1020	330	-1.17	-26.9	20.8
943	140	-1.39	-30.7	24.0	982	260	-2.07	51.9	0.2					

TABLE 6A. PEAK LOADS FOR CONFIGURATION A :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

* * 15 GREATEST PRESSURE MAGNITUDES * *

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK
			--- PSF ---	
544	300	-2.01	-64.6	27.5
957	250	-2.56	-64.1	8.4
937	300	-2.74	-63.1	8.8
917	350	-2.72	-61.2	17.4
150	250	-2.44	-60.9	30.3
147	300	-2.61	-60.1	30.1
928	290	-2.35	-58.7	15.0
750	330	-2.42	-55.7	24.2
744	220	-2.69	-54.5	15.5
508	120	-2.46	54.2	17.6
344	20	-2.40	54.0	38.2
968	250	-2.14	53.5	20.4
982	260	2.07	-51.9	8.2
902	290	-2.07	-51.8	33.0
918	350	-2.29	51.6	9.1

TABLE 6A. PEAK LOADS FOR CONFIGURATION B :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)
101	270	-1.27	-31.8	26.3	149	300	2.50	57.4	30.7	197	130	-1.21	-26.6	20.5
102	290	-1.25	-31.2	25.0	150	250	2.40	62.0	31.8	198	10	1.21	-26.6	27.1
103	290	-1.49	-37.3	28.3	151	290	1.35	33.7	33.3	199	280	1.12	-28.0	27.9
104	330	-1.23	-28.3	26.3	152	120	-1.80	-39.5	24.9	200	290	-1.83	-45.9	25.0
105	280	-1.24	-30.9	19.7	153	340	1.40	33.3	24.8	201	230	-1.28	-25.9	23.2
106	290	-1.42	-35.5	26.3	154	330	1.37	31.5	27.0	202	240	-1.51	-30.6	25.3
107	280	-1.43	-35.8	26.4	155	0	1.33	29.0	29.9	203	320	1.33	-30.0	30.6
108	290	-1.57	-39.3	25.4	156	280	-1.33	-33.3	30.4	204	310	-1.59	-36.5	18.0
109	270	-1.79	-44.9	29.7	157	290	1.29	32.2	31.4	205	270	1.19	-29.0	23.3
110	120	-1.40	-30.8	29.3	158	280	-1.43	-35.7	29.8	206	240	-1.40	-28.4	21.6
111	250	-1.11	-27.8	24.3	159	280	-2.05	-51.3	29.3	207	280	-1.07	-26.6	22.8
112	280	-1.37	-34.2	28.3	160	320	1.25	28.5	28.8	208	10	-1.38	-31.0	27.3
113	280	-1.23	-30.7	30.1	161	340	1.50	33.8	33.8	209	10	1.31	-29.5	16.5
114	280	-1.41	-35.3	29.3	162	250	1.17	29.2	27.6	210	130	-1.20	-26.3	22.5
115	290	-1.95	-48.7	28.5	163	290	1.53	38.3	21.3	211	300	1.61	-37.1	21.2
116	280	-1.67	-41.7	29.9	164	330	-1.38	-31.7	22.8	212	0	1.15	-25.9	25.3
117	280	-1.04	-26.0	21.4	165	310	1.53	35.2	21.8	213	120	1.73	-38.0	20.3
118	270	-1.05	-26.3	24.5	166	280	1.24	31.0	24.2	214	130	-1.06	-23.2	18.0
119	10	1.48	-32.0	33.4	167	120	1.52	33.4	28.0	215	150	1.12	-24.7	22.1
120	20	1.39	-31.1	31.3	168	280	-1.46	-36.5	26.3	216	130	-1.32	-29.0	19.4
121	280	-1.44	-36.0	29.0	169	300	-1.77	-40.7	28.1	217	300	-2.08	-47.9	23.7
122	280	-1.45	-36.2	26.2	170	330	1.26	28.2	28.9	218	330	1.08	-23.5	24.8
123	290	-1.49	-37.4	29.0	171	320	1.29	26.5	29.7	219	250	-1.13	-28.3	27.0
124	280	-1.09	-27.2	22.5	172	310	1.41	27.1	32.4	220	250	-1.65	-41.4	25.8
125	20	1.15	24.8	25.9	173	340	1.10	24.7	19.0	221	330	.96	-22.1	15.3
126	270	-1.05	-26.3	25.7	174	340	1.15	25.8	22.1	222	230	-1.21	-24.5	11.6
127	290	-1.15	-28.8	27.0	175	320	-1.42	-32.6	23.0	223	320	-1.12	-25.8	10.7
128	280	-1.42	-35.4	27.3	176	290	-1.17	29.3	25.5	224	130	-1.21	-26.6	23.1
129	290	-1.29	-32.3	24.3	177	20	1.25	27.5	28.1	225	20	1.02	-21.1	23.0
130	300	-1.83	-42.2	28.5	178	280	-1.43	-35.8	27.5	226	290	-1.06	-26.5	24.7
131	340	-1.42	-31.9	26.0	179	280	1.43	35.6	28.9	227	150	1.03	-22.7	19.5
132	290	-.96	-23.9	23.6	180	290	-1.67	41.7	27.1	228	320	.96	-21.5	22.2
133	20	1.49	-24.5	33.5	181	350	1.30	27.4	29.3	229	300	1.09	-21.3	25.1
134	290	-1.16	-29.1	27.6	182	340	1.40	26.0	33.4	230	330	-1.04	-23.9	10.6
135	290	-1.37	-34.4	29.0	183	320	1.29	27.6	29.8	231	320	1.08	-22.7	24.7
136	290	-1.61	-40.2	28.5	184	310	-1.46	-33.7	19.1	232	230	-.90	-18.3	14.3
137	290	-1.25	-31.2	28.1	185	130	1.24	27.3	22.0	233	280	-.84	-21.1	15.5
138	10	-1.32	-29.7	26.1	186	120	-1.32	-29.0	25.0	234	320	1.13	-25.9	15.7
139	20	1.22	26.3	27.5	187	230	1.31	28.5	22.3	235	150	-.64	-14.0	11.0
140	10	1.30	-29.1	29.3	188	10	1.27	-28.5	28.6	236	120	-.58	-12.7	10.5
141	290	-1.25	-31.3	27.9	189	290	1.46	-36.5	27.8	237	230	-.66	-13.4	9.9
142	290	-1.74	-43.6	31.2	190	290	1.48	37.0	27.9	238	300	-.59	-13.5	10.6
143	310	1.39	-26.5	31.9	191	250	1.27	31.8	25.9	239	140	-.90	-21.6	19.9
144	120	-2.59	-56.9	27.3	192	250	1.16	28.9	25.5	240	150	1.00	-22.0	20.9
145	250	-1.29	-32.1	26.0	193	250	1.12	28.0	26.1	241	290	.89	-17.4	22.2
146	310	-1.40	-32.3	31.9	194	120	1.49	32.8	22.0	301	10	-1.68	-37.8	32.3
147	290	-1.36	-33.9	29.8	195	130	-1.41	-30.9	18.4	302	0	-1.55	-34.9	31.1
148	350	1.46	-30.7	32.9	196	310	-2.30	-52.8	19.2	303	190	-1.70	-29.7	28.9

TABLE 6A. PEAK LOADS FOR CONFIGURATION B :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)
304	340	-1.75	-43.8	37.8	352	20	-1.34	-30.1	29.7	400	150	-1.73	-38.0	23.7
305	0	-1.51	-34.0	29.9	353	250	1.26	31.5	31.2	401	310	-1.96	-45.0	23.0
306	10	-1.62	-36.5	35.2	354	290	1.19	28.0	29.9	402	150	-1.77	-39.0	23.7
307	260	1.31	-29.4	32.7	355	0	1.68	-37.8	29.0	403	150	-1.39	-30.5	21.4
308	10	-1.45	-32.6	30.4	356	290	1.43	33.0	35.7	404	280	-1.30	-32.4	23.1
309	190	-2.22	-38.9	32.8	357	280	1.31	30.0	32.8	405	290	1.13	-27.5	28.4
310	10	-1.64	-36.9	31.2	358	10	1.34	30.2	30.0	406	260	1.07	-25.1	26.8
311	0	-2.19	-49.2	32.5	359	270	1.18	29.2	29.4	407	150	-1.20	-26.4	25.9
312	250	-1.47	-36.8	32.7	360	320	1.58	36.2	35.2	408	270	-1.27	-31.8	24.4
313	300	1.43	-27.7	33.0	361	310	-1.59	-36.7	32.8	409	290	1.21	-30.3	23.5
314	260	1.32	-29.7	33.0	362	230	1.40	27.5	28.5	410	150	-1.35	-29.6	25.2
315	200	-2.05	-35.9	27.8	363	320	1.36	23.6	31.2	411	250	1.01	-24.7	25.3
316	270	-1.26	-31.6	30.2	364	330	1.16	25.9	26.7	412	270	-1.41	-35.4	19.9
317	310	1.46	-32.2	33.6	365	250	-1.16	29.0	28.8	413	40	-2.00	-33.9	26.3
318	0	-1.46	-32.8	28.8	366	0	-1.67	37.6	33.5	414	320	1.08	-22.7	24.8
319	290	1.48	30.8	36.9	367	0	-1.42	32.0	30.7	415	20	-1.13	-25.4	25.2
320	270	1.42	-28.0	35.6	368	280	1.37	31.7	34.3	416	10	-1.56	-35.2	28.9
321	270	1.28	-29.2	32.0	369	10	-1.41	31.8	29.9	417	190	-1.64	-28.7	23.4
322	250	1.26	-27.1	31.5	370	280	-1.15	28.6	28.0	418	290	-1.14	-28.4	22.3
323	210	-1.42	-28.7	27.0	371	290	-1.19	29.7	27.0	419	330	-1.36	-31.3	21.7
324	10	-1.94	-43.6	28.4	372	150	-1.53	33.7	26.8	420	150	-1.51	-33.2	22.9
325	10	-1.70	-38.3	33.4	373	350	1.31	28.1	29.6	421	290	1.11	-19.6	27.7
326	10	-1.48	-33.4	33.3	374	310	1.10	26.7	27.1	422	290	1.00	-19.9	25.1
327	280	1.30	-25.8	32.4	375	260	-1.28	-32.1	29.0	423	0	-1.67	-37.6	24.6
328	270	1.17	-25.3	29.3	376	0	-1.64	37.0	28.4	424	300	1.20	-23.9	27.7
329	350	-1.14	-25.6	25.6	377	0	-1.43	32.2	27.6	425	150	-1.53	-33.7	21.5
330	210	-1.49	-30.1	29.1	378	0	-1.58	35.4	27.7	426	260	1.11	-24.5	27.8
331	260	-1.28	-31.9	31.2	379	0	-1.43	32.2	28.6	427	150	-1.57	-34.5	22.4
332	350	-1.55	-34.9	32.0	380	190	-1.95	34.2	27.2	428	310	-1.54	-35.4	19.7
333	280	1.36	-33.7	33.9	381	310	1.43	32.9	28.7	429	140	-1.16	-25.6	23.8
334	280	1.42	-28.7	35.4	382	310	1.35	31.0	26.9	430	10	1.19	-26.8	25.3
335	280	1.45	-25.2	36.3	383	310	1.29	29.6	23.5	431	260	.89	-21.6	22.3
336	190	-1.91	-33.5	27.8	384	340	1.26	25.5	28.3	432	330	1.06	-20.4	24.4
337	310	-1.67	-38.4	31.1	385	250	-1.41	-35.2	28.6	433	180	-1.31	-22.9	22.1
338	320	1.43	-30.7	32.8	386	250	1.29	32.1	26.2	434	130	-1.28	-28.1	21.4
339	0	-1.93	-43.4	29.7	387	10	-1.68	-37.8	33.2	435	290	.93	-19.9	23.4
340	290	1.30	-28.8	32.5	388	0	-1.47	33.1	30.6	436	280	.92	-19.9	23.1
341	280	1.29	-26.6	32.2	389	190	-1.69	29.5	29.4	437	150	-.99	-21.7	20.6
342	250	1.48	-33.6	36.9	390	200	1.68	29.3	24.4	438	270	1.16	-27.9	28.9
343	250	1.25	-27.0	31.2	391	320	-2.00	-47.8	27.7	439	320	1.12	-25.7	19.6
344	20	-1.97	-44.4	36.6	392	320	-1.63	37.4	23.1	440	10	-1.37	-30.8	20.7
345	0	-2.24	-50.4	33.8	393	310	-1.50	34.4	20.9	441	150	-1.28	-28.1	19.2
346	280	1.70	-32.4	42.5	394	290	1.10	25.2	27.5	442	290	1.06	-15.8	26.6
347	10	-1.49	-33.6	29.7	395	250	-1.23	-30.9	26.9	443	330	1.04	-20.5	24.0
348	280	1.32	-27.3	33.1	396	250	-1.50	37.6	23.3	444	260	.96	-15.6	24.1
349	260	1.36	-33.7	34.0	397	10	-1.58	35.5	25.4	445	320	.94	-20.8	21.7
350	150	-2.42	-53.2	35.2	398	10	-1.51	34.1	30.4	501	270	-1.39	-34.8	23.2
351	300	1.43	-27.3	32.8	399	280	1.08	26.8	27.1	502	280	-1.50	-37.4	19.5

TABLE 6A. PEAK LOADS FOR CONFIGURATION B :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK
			--- PSF	----				---- PSF	----				---- PSF	----
503	280	-1.35	-33.6	25.2	551	280	-1.29	-32.3	23.6	599	320	-1.20	-27.6	20.5
504	290	-1.85	-46.2	23.0	552	300	-1.73	-39.8	28.0	600	330	-1.55	-35.7	22.9
505	280	-1.38	-34.5	24.1	553	320	-1.43	-32.8	27.6	601	220	-1.29	-26.1	24.5
506	280	-1.23	-30.8	21.3	554	150	-1.32	-29.0	24.8	602	230	-1.40	-28.4	25.4
507	310	-1.35	-31.2	21.7	555	280	-1.53	-38.2	26.0	603	20	-1.34	-30.3	23.0
508	320	-1.45	-33.3	25.2	556	260	-1.27	-31.6	24.6	604	150	-1.18	-26.0	25.0
509	120	-1.69	-37.1	24.7	557	270	-1.50	-37.6	23.3	605	280	-1.14	-28.5	19.0
510	270	-1.48	-37.1	23.4	558	290	-1.26	-31.4	23.0	606	270	-1.00	-25.1	18.9
511	260	-2.10	-52.5	25.8	559	300	-1.28	-29.4	26.4	607	320	-1.52	-34.9	20.6
512	280	-1.37	-34.2	25.5	560	220	-1.57	-31.7	27.4	608	320	-1.24	-28.5	22.1
513	270	-1.03	-25.8	25.6	561	170	1.65	-23.4	28.9	609	190	-1.46	-25.5	23.1
514	270	-1.14	-28.4	22.5	562	150	1.33	-26.5	27.2	610	270	-1.31	-32.8	19.4
515	290	-1.25	-31.2	25.8	563	250	1.20	-28.6	30.1	611	320	-1.65	-38.0	18.9
516	210	-1.29	-26.1	21.8	564	150	1.28	-28.1	24.7	612	350	-1.12	-25.3	23.1
517	260	-1.38	-34.5	24.2	565	320	-1.33	-30.7	26.7	613	310	-1.89	-43.5	22.9
518	260	-1.32	-32.9	22.4	566	260	-1.42	-35.5	23.9	614	320	-1.60	-36.9	20.5
519	270	-1.32	-32.9	24.7	567	280	-1.32	-32.9	24.3	615	150	-1.41	-30.9	22.5
520	280	-1.18	-29.4	23.5	568	300	-1.19	-27.3	21.4	616	330	-1.73	-39.8	21.0
521	290	-1.10	-27.6	23.0	569	290	-1.83	-45.9	23.7	617	320	-1.37	-31.4	21.5
522	280	-1.07	-26.8	24.9	570	150	1.25	-26.3	27.5	618	140	1.24	-24.4	27.3
523	290	-1.07	-26.7	24.2	571	140	1.40	28.4	30.8	619	60	-1.41	-23.9	22.8
524	280	-1.78	-44.5	29.3	572	130	1.36	23.1	30.0	620	140	1.13	-22.8	24.8
525	270	-1.27	-31.6	21.7	573	310	1.22	28.2	24.5	621	310	-1.42	-32.6	19.3
526	280	-1.28	-32.0	22.3	574	250	1.24	-30.4	30.9	622	310	-1.53	-35.1	19.6
527	290	-1.05	-26.3	20.6	575	320	1.44	-33.1	25.3	623	320	-1.31	-30.0	19.5
528	280	-1.07	-26.8	22.8	576	270	-1.58	-39.6	20.2	624	320	-1.63	-37.5	16.6
529	290	-1.05	-26.3	23.3	577	270	-1.44	-36.0	21.4	625	20	-1.47	-33.0	17.8
530	120	-1.28	-28.2	28.1	578	270	-1.16	29.1	20.4	626	10	-1.28	-28.8	19.1
531	150	-1.44	-31.6	25.2	579	280	1.20	30.0	21.1	627	320	-1.42	-32.6	18.6
532	260	-1.54	-38.6	27.3	580	320	1.61	37.1	22.0	628	320	-1.11	-25.5	23.5
533	270	-1.24	-30.9	24.8	581	300	1.24	-28.6	25.1	629	150	1.28	-25.7	28.1
534	270	-1.07	-26.8	24.1	582	130	1.25	-24.9	27.6	630	310	1.35	-31.1	21.3
535	290	-1.00	-25.0	23.6	583	150	1.30	-26.3	28.5	631	320	-1.43	-32.9	20.4
536	120	-1.29	-28.3	24.7	584	300	-1.37	-31.5	24.9	632	310	-1.31	-30.1	20.0
537	140	1.23	-24.1	27.0	585	310	1.58	-36.3	24.2	633	320	-1.15	-26.5	18.0
538	250	1.21	-24.5	30.3	586	320	-1.22	28.0	22.4	634	280	-1.18	-29.5	16.9
539	270	-1.82	-45.6	25.1	587	260	-1.44	-35.9	22.5	635	330	-1.70	-39.1	18.8
540	280	-1.50	-37.5	25.7	588	280	-1.37	-34.4	19.9	636	330	-1.15	-26.6	19.3
541	290	-1.06	-26.5	25.0	589	260	-1.18	-29.5	20.7	637	320	-2.03	-46.6	17.9
542	120	-1.43	-31.5	28.5	590	310	-1.45	-33.5	22.0	638	330	-1.19	-27.3	19.5
543	140	1.31	-23.6	28.9	591	210	1.50	-30.4	23.7	639	320	-1.58	-36.3	18.9
544	320	-2.86	-65.8	32.2	592	210	-1.49	-30.1	26.1	640	280	-1.15	-28.7	19.6
545	270	-2.16	-53.9	26.4	593	60	-1.74	-29.5	25.0	641	310	-1.51	-34.7	24.1
546	270	-1.39	-34.7	22.7	594	320	-1.33	-30.5	23.2	701	20	-1.14	-25.6	22.2
547	280	-1.04	-26.1	26.0	595	300	-1.53	-35.1	23.5	702	10	-1.31	-29.5	20.6
548	270	-1.15	-28.8	24.8	596	320	-1.51	-34.7	22.4	703	20	-1.65	-37.1	21.1
549	120	-2.04	-44.8	28.1	597	270	-1.62	-40.6	18.5	704	170	-1.80	-31.4	24.4
550	60	-2.37	-40.3	27.5	598	320	1.47	-33.8	20.3	705	180	-1.56	-27.4	25.5

TABLE 6A. PEAK LOADS FOR CONFIGURATION B :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)
706	10	-1.35	-30.4	22.9	754	140	1.28	-25.3	28.2	802	130	-1.73	-38.0	16.8
707	10	-1.47	-33.1	20.1	755	350	1.52	-34.1	28.1	803	310	-1.66	-38.2	18.2
708	20	-1.71	-38.4	17.2	756	20	-1.30	-29.2	25.5	804	120	-1.31	-28.7	23.2
709	10	-1.89	-42.6	22.0	757	20	-1.36	-30.7	25.8	805	330	-1.27	-29.1	22.7
710	200	-1.82	-31.9	22.5	758	10	-1.55	-34.9	20.0	806	310	-1.22	-28.0	21.4
711	170	-2.02	-35.4	25.5	759	10	-1.61	-36.1	21.6	807	220	-1.70	-34.5	19.5
712	120	1.21	-26.2	26.7	760	130	-1.68	-37.0	20.2	808	120	-1.19	-26.3	22.8
713	120	1.36	-26.0	30.0	761	130	-1.56	-34.3	21.7	809	320	-1.46	-33.7	21.2
714	20	-1.50	-33.8	23.6	762	310	-1.33	-30.5	25.6	810	330	-1.22	-28.1	24.6
715	10	-2.05	-46.1	21.3	763	150	1.33	27.3	29.3	811	300	-1.42	-32.7	19.3
716	10	-1.59	-35.8	19.6	764	130	1.24	25.7	27.4	812	130	-1.43	-31.5	18.6
717	10	-1.26	-28.3	27.1	765	130	1.25	22.8	27.6	813	210	-1.71	-34.6	24.0
718	10	-1.19	-26.8	26.7	766	340	-1.70	-38.2	27.6	814	310	-1.49	-34.2	25.7
719	10	-1.27	-28.5	28.2	767	340	-1.36	-30.5	25.5	815	220	-1.33	-26.9	24.5
720	10	-1.15	-25.9	25.0	768	20	-1.50	-33.7	20.9	816	220	-1.54	-31.3	23.6
721	20	-1.41	-31.8	24.0	769	10	-1.46	-32.9	18.2	817	10	-1.54	-34.7	18.9
722	10	-1.63	-36.7	18.6	770	130	-1.37	-30.1	20.5	818	300	-1.04	-24.0	17.7
723	20	-1.32	-29.8	19.3	771	130	-1.29	-28.5	22.0	819	340	-1.12	-25.2	23.9
724	160	-1.54	-26.9	25.9	772	350	-1.25	-28.2	20.8	820	340	-1.99	-44.9	21.3
725	180	-1.48	-25.9	25.9	773	150	1.27	-27.3	28.0	821	0	-1.16	-26.0	21.3
726	10	-1.21	-27.2	24.2	774	130	1.21	-26.4	26.7	822	270	-1.06	-26.4	22.4
727	190	-1.50	-26.3	24.2	775	130	1.25	-26.9	27.6	823	300	-1.34	-30.8	22.4
728	10	-1.39	-31.4	18.8	776	350	-1.65	-37.2	25.8	824	330	-1.04	-23.9	20.5
729	20	-1.26	-28.3	17.2	777	270	-1.75	-43.8	22.1	825	320	-1.53	-35.3	22.6
730	20	-1.49	-33.5	20.3	778	20	-1.35	-30.5	26.8	826	310	-1.54	-35.3	18.7
731	140	1.51	-31.9	33.2	779	20	-1.37	-30.8	21.8	827	330	-1.41	-32.5	15.8
732	180	-1.56	-27.4	26.6	780	20	-1.57	-35.4	18.7	828	190	-1.34	-23.5	14.8
733	120	1.30	-23.5	28.6	781	130	-1.30	-28.5	21.3	829	330	-.94	-21.7	16.8
734	120	1.16	-24.8	25.6	782	130	-1.34	-29.6	19.7	830	330	-1.10	-25.3	24.4
735	20	-1.45	-32.5	20.8	783	320	-1.15	-26.4	25.9	831	310	-1.21	-27.8	16.1
736	20	-1.61	-36.3	21.0	784	220	-1.33	-26.9	24.1	832	350	-1.42	-32.0	21.5
737	340	-1.40	-31.5	20.7	785	230	2.01	-40.6	26.3	833	300	-1.13	-26.0	21.9
738	130	1.34	-23.4	29.5	786	220	-1.33	-26.9	25.4	834	310	-1.26	-29.0	21.9
739	170	-2.00	-35.0	35.0	787	310	-1.77	-40.7	25.9	835	320	-1.09	-25.0	23.8
740	10	-1.16	-26.1	24.3	788	20	-1.31	-29.6	23.9	836	320	-1.04	-23.9	19.9
741	20	-1.41	-31.7	18.6	789	20	-1.48	-33.2	20.3	837	230	-1.28	-25.9	19.8
742	20	-1.72	-38.8	22.2	790	10	-1.76	-39.5	18.3	838	330	-1.06	-24.3	19.0
743	10	-1.25	-28.1	26.3	791	320	-1.33	-30.5	20.4	839	300	-1.61	-36.9	11.6
744	220	-2.28	-46.1	29.8	792	120	-1.28	-28.1	19.2	840	200	-1.10	-19.3	13.7
745	180	-2.08	-36.4	27.3	793	310	-1.18	-27.2	23.5	841	200	-1.38	-24.2	15.9
746	120	1.31	-24.2	28.7	794	230	-1.67	-33.9	24.9	842	330	-1.07	-24.5	13.5
747	120	1.37	-27.0	30.2	795	230	-1.41	-28.5	24.9	843	150	1.26	-18.3	27.7
748	10	-1.52	-34.2	23.0	796	120	1.26	-27.4	27.8	844	310	-.99	-22.7	21.5
749	20	-2.07	-46.6	21.1	797	230	-1.56	-31.7	24.6	845	140	1.35	-17.7	29.7
750	330	-2.78	-63.9	22.4	798	320	-1.16	-26.7	23.7	901	340	1.45	-22.0	32.7
751	20	-1.24	-27.9	26.6	799	340	-1.54	-34.7	19.8	902	290	-1.62	-40.4	26.2
752	150	1.31	-28.1	28.9	800	10	-1.79	-40.2	16.4	903	130	-1.67	-36.7	30.7
753	220	-1.66	-33.7	28.5	801	130	-1.48	-32.6	16.5	904	10	1.43	-28.8	32.2

TABLE 6A. PEAK LOADS FOR CONFIGURATION B :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF ----	POSITIVE PEAK ---- PSF ----	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF ----	POSITIVE PEAK ---- PSF ----	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF ----	POSITIVE PEAK ---- PSF ----
905	240	-1.65	-33.4	31.1	944	290	-1.18	29.4	3.0	983	150	-2.07	-45.6	5.5
906	140	-1.23	-27.0	26.7	945	280	1.70	-28.6	42.6	984	150	-1.96	-43.0	10.0
907	240	-1.17	-23.7	21.8	946	290	1.28	27.9	32.0	985	210	-1.59	-32.2	19.0
908	290	-1.93	-48.2	26.4	947	290	1.19	-25.2	29.8	986	320	-1.35	-31.0	21.4
909	280	-1.17	-29.1	24.1	948	310	-2.19	-50.3	4.6	987	130	1.30	-23.8	28.5
910	10	1.39	-29.4	31.4	949	270	-1.40	-35.1	4.4	988	270	-1.18	-29.4	21.4
911	290	-1.27	-31.8	23.0	950	150	-1.29	-28.4	3.0	989	270	-1.13	-28.3	17.6
912	280	-.91	-22.8	15.5	951	320	-1.22	-28.0	4.0	990	120	-1.24	-27.3	19.8
913	0	1.27	-27.1	28.6	952	20	-1.27	-28.6	5.3	991	270	-1.15	-28.8	24.2
914	290	1.43	-19.4	35.8	953	150	-1.59	-35.0	5.3	992	270	-1.94	-48.6	24.6
915	310	1.21	-25.4	27.8	954	20	-1.24	-27.9	22.8	993	120	-1.59	-34.9	23.8
916	290	-1.74	-43.5	24.9	955	20	-1.20	-27.0	25.0	994	280	-1.17	-29.2	23.6
917	340	-2.15	-48.3	19.8	956	310	1.57	-36.2	23.7	995	280	-1.50	-37.6	26.0
918	330	-2.07	-47.7	9.4	957	270	-1.19	-29.7	5.0	996	270	-1.45	-36.3	23.7
919	320	-1.90	-43.6	5.8	958	260	1.33	-27.3	33.2	997	310	-1.43	-32.9	31.1
920	20	-1.84	-41.4	7.5	959	250	-2.29	-57.3	9.4	998	210	1.42	-27.8	28.8
921	20	-1.92	-43.3	8.5	960	260	-1.81	-45.3	11.8	999	320	-1.40	-32.3	29.2
922	10	-1.74	-39.0	16.5	961	290	-1.41	-35.2	17.4	1000	310	-1.32	-30.5	26.2
923	0	-1.14	-25.7	14.2	962	150	-1.47	-32.4	16.4	1001	10	1.20	-18.0	26.9
924	310	-1.05	-24.1	20.0	963	0	-1.52	-34.1	11.9	1002	20	1.09	-21.1	24.6
925	0	-1.93	-43.3	31.0	964	130	-2.36	-51.9	8.0	1003	290	-1.82	-45.6	22.2
926	20	-1.90	-42.8	18.4	965	180	-1.64	-28.7	24.5	1004	270	-.52	-13.0	9.4
927	0	-1.65	-37.1	27.9	966	260	-1.29	-32.1	6.8	1005	150	-1.22	-26.8	8.4
928	300	-2.34	-53.8	16.7	967	260	1.40	-33.3	34.9	1006	270	-.50	-12.4	8.6
929	320	-1.93	-44.4	13.8	968	260	-2.27	-56.7	11.6	1007	260	-.53	-13.2	9.1
930	10	-1.64	-36.9	8.0	969	290	-1.63	-40.0	8.7	1008	130	-.58	-12.8	11.1
931	20	-1.89	-42.6	10.6	970	270	-1.47	-36.8	13.4	1009	290	1.04	-19.7	26.0
932	0	-1.81	-40.6	7.7	971	260	-1.51	-37.7	7.6	1010	330	-1.14	-26.3	18.4
933	80	-2.29	-31.4	12.1	972	130	-1.74	-30.4	7.1	1011	260	.92	-17.4	23.1
934	20	-1.87	-42.0	20.4	973	120	-2.04	44.8	11.3	1012	230	-1.20	-24.4	22.8
935	20	-1.56	-35.1	6.8	974	230	-1.52	-30.8	25.6	1013	310	1.10	-24.1	25.2
936	290	1.59	-35.6	39.7	975	260	1.31	32.2	32.8	1014	280	-.89	-22.3	19.4
937	300	-2.56	-58.9	7.6	976	170	-2.09	-36.6	24.0	1015	150	-1.17	-25.6	22.0
938	280	-1.73	-43.2	7.1	977	310	-1.48	-34.0	28.2	1016	330	-.88	-20.4	20.3
939	280	-1.43	-35.7	11.7	978	250	.93	-22.2	23.3	1017	260	-1.20	-30.1	16.4
940	10	-1.61	-36.2	11.1	979	280	-1.72	-42.9	19.6	1018	320	-1.27	-29.3	16.5
941	10	-1.51	-34.0	11.4	980	200	-2.09	36.6	12.4	1019	330	-1.38	-31.8	20.2
942	60	-1.94	-32.9	8.8	981	210	2.37	-48.0	7.4	1020	330	-1.61	-37.0	20.2
943	10	-1.57	-35.3	20.7	982	270	-1.36	-34.1	6.1					

TABLE 6A. PEAK LOADS FOR CONFIGURATION B :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

* * 15 GREATEST PRESSURE MAGNITUDES * *

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK
			PSF ----	
544	320	2.86	65.8	32.2
750	330	-2.70	63.9	22.4
150	250	-2.48	62.0	31.8
937	300	-2.56	58.9	7.6
149	300	2.50	57.4	30.7
959	250	-2.29	57.3	9.4
144	120	2.59	56.9	27.3
960	260	-2.27	56.7	11.6
545	270	2.16	53.9	26.4
928	300	-2.34	53.8	16.7
350	150	2.42	53.2	35.2
196	310	-2.30	52.8	19.2
511	260	2.10	52.5	25.8
964	130	-2.36	51.9	8.0
159	280	-2.05	51.3	29.3

TABLE 6A. PEAK LOADS FOR CONFIGURATION C : LPC MANDALAY LAS COLLINAS,TEXAS
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)
101	190	-1.29	-32.4	27.6	149	180	-2.20	-55.0	28.7	197	320	-1.09	-24.1	21.8
102	190	-1.42	-35.6	24.3	150	210	-2.05	-51.4	34.4	198	220	-1.62	-32.8	26.7
103	180	-1.38	-34.4	27.0	151	190	-1.34	-33.6	30.4	199	180	-1.08	-27.0	25.5
104	350	-1.55	-34.0	26.8	152	90	1.16	-21.9	26.2	200	180	-1.97	-49.2	24.0
105	210	-1.31	-32.8	18.8	153	140	-1.35	-31.1	23.9	201	130	1.16	-26.6	26.8
106	180	-1.40	-35.0	26.5	154	130	-1.35	-31.0	29.4	202	210	-1.27	-31.6	26.4
107	180	-1.59	-39.7	27.0	155	210	-1.40	-35.1	26.8	203	210	-1.16	-29.1	22.4
108	180	-1.48	-37.0	27.6	156	100	1.36	-28.4	30.7	204	140	-1.20	-27.5	23.3
109	180	-2.06	-51.4	30.0	157	180	-1.20	-30.1	29.9	205	230	-1.19	-24.1	21.1
110	100	-1.43	-32.1	27.9	158	180	-1.46	-36.5	30.0	206	230	-1.22	-24.7	22.5
111	180	-1.07	-26.7	24.7	159	170	-1.75	-40.3	32.6	207	230	-1.44	-29.1	22.3
112	100	1.56	-34.4	35.1	160	120	1.50	-30.0	33.7	208	120	-1.30	-29.2	26.1
113	130	1.44	-33.0	33.2	161	220	-1.85	-37.5	30.0	209	130	-.99	-22.8	22.4
114	180	-1.53	-38.3	27.7	162	220	-1.81	-36.6	31.3	210	210	-.92	-22.9	21.4
115	190	-1.70	-42.5	29.4	163	90	1.14	-24.5	25.6	211	180	-1.23	-30.8	18.8
116	180	-1.43	-35.8	29.3	164	120	-1.27	-28.7	23.8	212	120	-1.40	-31.5	27.3
117	190	-1.02	-25.5	21.5	165	160	-1.40	-32.1	24.5	213	350	-1.22	-26.8	24.0
118	190	-1.31	-32.7	23.5	166	210	-1.45	-36.1	27.0	214	350	-.99	-21.7	20.2
119	100	1.45	-30.1	32.7	167	180	-1.13	-28.2	25.9	215	130	-.97	-22.4	22.0
120	190	-1.20	-30.0	29.7	168	190	-1.37	-34.2	26.6	216	20	-1.90	-26.1	22.2
121	180	-1.31	-32.7	28.6	169	180	-1.44	-35.9	27.5	217	180	-1.90	-47.5	25.6
122	180	-1.31	-32.7	26.0	170	230	-1.45	-29.4	27.7	218	200	-.99	-24.8	24.0
123	170	-1.53	-35.3	28.8	171	210	-1.32	-33.0	28.0	219	230	-1.36	-27.6	23.3
124	210	-1.12	-27.9	25.1	172	210	-1.24	-31.1	28.5	220	220	-1.93	-39.1	24.1
125	90	.95	-21.3	21.4	173	130	-1.18	-27.2	24.2	221	140	-1.01	-23.2	20.0
126	190	-1.04	-25.9	23.8	174	100	-1.12	-27.9	24.1	222	210	-1.14	-28.4	13.6
127	120	1.20	-26.4	26.9	175	160	-1.22	-28.1	25.7	223	150	-1.03	-23.7	12.6
128	190	-1.41	-35.2	24.7	176	90	1.46	-31.9	32.9	224	110	1.04	-19.7	23.5
129	180	-1.24	-31.1	26.9	177	180	-1.10	-27.6	27.5	225	110	1.11	-18.5	25.1
130	190	-1.66	-41.6	29.9	178	180	-1.50	-37.5	28.8	226	120	1.19	-25.2	26.8
131	130	-1.59	-36.6	24.2	179	180	-1.28	-32.1	28.6	227	90	-.94	-21.2	18.8
132	200	-1.12	-28.0	23.7	180	190	-1.53	-38.1	26.6	228	160	1.21	-17.7	27.8
133	100	1.25	-24.0	28.2	181	140	1.29	-26.3	29.6	229	90	-1.10	-24.7	23.3
134	130	1.28	-27.9	29.4	182	140	1.21	-27.7	27.9	230	230	-1.27	-25.6	14.0
135	180	-1.30	-32.5	30.3	183	200	-1.44	-35.9	28.9	231	90	-.95	-21.4	20.8
136	190	-1.88	-47.0	29.5	184	140	-1.15	-26.5	23.2	232	330	-.82	-18.1	15.4
137	90	-1.67	-37.5	34.8	185	140	-1.29	-29.7	22.9	233	140	-.82	-18.9	17.8
138	140	-1.36	-31.3	25.3	186	130	-1.42	-32.6	26.1	234	140	-.98	-22.7	15.7
139	100	1.20	-25.6	26.9	187	90	1.13	-24.1	25.4	235	290	-.66	-11.6	10.4
140	100	1.26	-27.1	28.4	188	100	-1.27	-31.7	27.1	236	210	-.50	-12.6	8.8
141	180	-1.27	-31.7	29.4	189	180	-1.31	-32.7	24.0	237	210	-.50	-12.6	9.5
142	190	-1.79	-44.8	30.6	190	190	-1.47	-36.8	24.3	238	170	-.58	-13.4	8.2
143	140	1.35	-27.9	31.1	191	90	-1.44	-32.4	27.8	239	150	.94	-19.9	21.7
144	350	-1.60	-35.3	26.7	192	220	-1.56	-31.6	26.4	240	180	.87	-15.4	21.7
145	40	-2.12	-36.0	30.6	193	220	-1.35	-27.3	27.1	241	180	.93	-18.5	23.3
146	120	1.26	-27.4	28.2	194	130	-1.18	-27.1	21.2	301	180	1.26	-30.4	31.4
147	180	-1.22	-30.4	29.1	195	120	-1.34	-30.2	22.6	302	110	-1.33	-30.0	26.9
148	180	-1.24	-31.0	30.2	196	130	-1.42	-32.6	23.9	303	190	1.19	-28.8	29.8

TABLE 6A. PEAK LOADS FOR CONFIGURATION C : LPC MANDALAY LAS COLLINAS,TEXAS
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----
304	100	-1.82	-41.0	32.6	352	120	1.41	-30.7	31.6	400	260	-1.35	-27.4	23.9
305	120	-1.38	-31.1	27.9	353	220	-1.95	-39.4	33.7	401	140	-1.60	-36.9	24.4
306	110	-1.51	-34.0	31.7	354	210	-1.30	-34.5	29.9	402	160	-1.86	-42.8	26.6
307	200	1.25	-26.9	31.2	355	180	1.27	-30.3	31.8	403	150	-1.34	-30.8	23.6
308	320	-1.29	-28.4	24.7	356	180	1.36	-30.0	34.0	404	190	-1.50	-37.5	26.0
309	290	-2.20	-38.6	29.5	357	190	1.23	-26.4	30.8	405	180	1.13	-25.6	28.2
310	200	-1.38	-34.5	30.4	358	180	1.24	-25.4	31.0	406	190	1.09	-21.2	27.2
311	110	-1.76	-39.6	30.0	359	210	1.27	-31.3	31.7	407	210	1.08	-22.0	27.0
312	190	1.30	-32.3	32.6	360	210	1.39	-32.3	34.8	408	200	1.18	-27.1	29.6
313	180	1.37	-28.6	34.2	361	210	1.21	-27.4	30.3	409	170	-1.41	-32.3	22.5
314	190	1.46	-28.9	36.6	362	150	-1.34	-30.9	29.0	410	180	1.05	-25.5	26.3
315	260	-1.67	-33.9	31.0	363	130	1.22	-27.5	28.1	411	190	.94	-22.0	23.5
316	310	-1.61	-35.5	30.6	364	150	1.31	-26.4	30.2	412	180	-.96	-23.9	21.0
317	170	1.43	-29.4	32.8	365	210	-1.16	-29.1	28.2	413	90	-1.67	-37.5	28.1
318	180	1.33	-31.5	33.2	366	120	-1.30	-29.3	29.1	414	180	1.00	-24.5	25.1
319	180	1.41	-26.3	35.3	367	180	1.19	-27.5	29.7	415	130	.99	-21.9	22.7
320	170	1.41	-24.0	32.4	368	200	1.15	-25.8	28.8	416	110	-1.58	-35.4	26.8
321	200	1.44	-23.8	36.1	369	210	1.36	-29.7	33.9	417	260	-1.44	-29.2	25.4
322	210	1.14	-25.9	28.5	370	180	-1.26	-31.6	27.7	418	180	-1.15	-28.8	26.1
323	320	-1.51	-33.2	26.1	371	210	1.19	-27.5	29.8	419	150	-1.03	-23.6	23.0
324	110	-1.59	-35.7	28.9	372	210	1.18	-27.4	29.4	420	310	-1.00	-21.9	20.4
325	170	1.28	-28.1	29.3	373	140	1.21	-27.8	27.9	421	170	1.07	-19.4	24.6
326	190	1.41	-30.1	35.4	374	210	-1.19	-29.7	25.0	422	90	-1.13	-25.5	23.5
327	190	1.41	-25.5	35.2	375	200	-1.39	-34.8	30.1	423	180	1.09	-25.4	27.3
328	200	1.32	-25.4	33.1	376	120	-1.40	-31.6	29.3	424	170	1.17	-20.3	26.8
329	180	1.20	-24.9	29.9	377	110	-1.23	-27.7	26.8	425	200	1.00	-22.0	24.9
330	260	-1.55	-31.4	26.4	378	180	1.17	-27.4	29.2	426	170	1.23	-25.0	28.2
331	90	-1.66	-37.2	32.2	379	190	1.19	-27.5	29.8	427	200	.94	-19.8	23.6
332	110	-1.46	-32.8	28.4	380	260	-1.41	-28.5	26.1	428	180	-1.11	-27.8	25.3
333	120	-1.40	-31.4	30.9	381	160	-1.62	-37.2	29.0	429	310	-1.00	-21.9	21.4
334	210	1.27	-25.3	31.8	382	180	-1.19	-27.7	25.4	430	180	1.36	-22.2	34.1
335	210	1.32	-27.5	32.9	383	160	-1.13	-26.0	24.4	431	280	-1.20	-21.0	20.7
336	260	-1.58	-32.0	27.7	384	160	1.29	-26.9	29.7	432	140	1.03	-19.6	23.6
337	210	1.30	-29.7	32.5	385	90	-1.34	-30.2	27.4	433	180	.96	-19.2	23.9
338	190	-1.31	-32.6	31.3	386	210	-1.44	-36.1	27.1	434	100	-1.05	-23.7	22.3
339	110	-1.83	-41.3	32.3	387	130	-1.58	-36.3	30.3	435	180	.95	-18.2	23.7
340	180	1.37	-28.0	34.2	388	120	-1.39	-31.4	26.8	436	170	.97	-15.4	22.3
341	200	1.22	-24.5	30.6	389	200	1.10	-26.5	27.5	437	210	.92	-20.2	23.1
342	210	1.24	-30.1	31.1	390	200	1.19	-28.2	29.6	438	190	.98	-19.0	24.5
343	210	1.17	-28.7	29.3	391	170	-2.00	-46.0	24.8	439	150	-1.18	-27.0	20.2
344	90	-2.40	-54.0	38.2	392	150	-1.65	-38.0	25.1	440	180	-1.09	-27.2	23.7
345	120	-2.13	-47.9	31.9	393	140	-1.18	-27.2	25.6	441	340	-1.36	-30.0	23.3
346	120	-1.39	-31.3	31.2	394	90	-1.24	-28.0	23.9	442	230	1.29	-15.8	26.2
347	180	1.32	-26.1	32.9	395	210	-1.34	-33.5	26.2	443	150	.92	-20.6	21.2
348	200	1.17	-25.3	29.2	396	200	-1.54	-38.6	24.4	444	210	1.02	-12.9	25.4
349	260	-2.22	-45.1	30.4	397	110	-1.60	-36.0	28.4	445	180	1.00	-20.3	25.0
350	310	-1.39	-30.6	30.1	398	180	1.25	-28.5	31.3	501	190	-1.37	-34.2	29.4
351	190	1.24	-24.4	30.9	399	190	1.11	-25.5	27.7	502	180	-1.45	-36.3	28.0

TABLE 6A. PEAK LOADS FOR CONFIGURATION C : LPC MANDALAY LAS COLLINAS,TEXAS
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)
503	330	-1.47	-32.2	31.5	551	310	1.41	-23.7	31.0	599	150	-1.40	-32.2	24.8
504	190	-1.72	-42.9	24.6	552	170	-1.42	-32.6	25.0	600	150	-1.46	-33.5	15.8
505	310	-1.29	-28.5	22.2	553	180	-1.38	-34.6	26.8	601	210	-1.44	-36.0	6.8
506	310	1.36	-26.4	30.0	554	250	1.34	-25.8	27.1	602	240	-1.42	-28.7	11.5
507	130	-1.34	-30.9	26.4	555	190	-1.15	-28.7	27.9	603	90	-1.39	-31.2	11.3
508	350	-2.46	-54.2	20.6	556	180	-1.22	-30.5	26.6	604	200	1.21	-27.5	30.3
509	350	-1.69	-37.3	26.0	557	310	1.32	-25.7	29.0	605	150	-1.38	-31.8	20.5
510	180	-1.51	-37.7	24.0	558	310	1.36	-28.8	30.0	606	150	-1.09	-25.1	21.4
511	200	-1.82	-45.6	26.8	559	180	-1.05	-26.3	14.3	607	150	-1.35	-31.1	28.3
512	190	-1.34	-33.5	32.2	560	230	-1.50	-30.4	10.5	608	200	-1.16	-29.0	21.3
513	310	1.49	-27.6	32.7	561	310	-1.26	-27.7	15.1	609	270	-1.66	-29.0	21.8
514	120	-1.39	-31.2	26.8	562	340	-1.15	-25.2	12.8	610	150	-1.04	-23.8	18.7
515	350	-2.17	-47.8	16.8	563	180	-1.21	-30.2	30.0	611	150	-1.13	-26.1	21.0
516	340	-1.30	-28.5	26.3	564	170	-1.43	-32.8	24.3	612	240	-1.21	-24.5	18.0
517	250	1.48	-26.8	29.9	565	180	-1.16	-29.1	25.2	613	160	-2.16	-49.8	24.1
518	180	-1.27	-31.7	26.0	566	180	-1.48	-37.1	25.7	614	170	-1.36	-31.2	22.5
519	310	1.41	-25.6	31.1	567	180	-1.26	-31.4	26.4	615	170	-1.32	-30.4	21.4
520	310	1.32	-25.5	29.0	568	310	1.34	-26.7	29.6	616	150	-1.33	-30.6	20.0
521	310	1.39	-28.1	30.6	569	180	-.99	-24.7	14.6	617	90	-1.28	-28.8	15.7
522	130	-1.82	-42.0	19.2	570	240	-1.45	-29.3	7.6	618	310	-1.42	-31.2	12.4
523	120	-1.90	-42.8	13.2	571	350	-1.25	-27.6	19.4	619	340	-1.13	-25.0	15.3
524	190	-1.78	-44.5	26.3	572	340	-1.14	-25.0	12.2	620	90	-1.55	-34.9	15.2
525	210	-1.25	-31.4	24.4	573	150	-1.44	-33.1	30.2	621	150	-1.11	-25.6	21.5
526	200	-1.19	-29.7	26.7	574	160	-1.69	-38.8	24.3	622	150	-1.23	-28.3	20.5
527	310	1.26	-26.3	27.8	575	150	-1.12	-25.7	23.1	623	150	-1.02	-23.6	18.8
528	180	-.97	-24.3	23.7	576	190	-1.26	-31.4	23.8	624	90	-.95	-21.4	19.9
529	350	-1.17	-25.8	17.9	577	190	-1.11	-27.8	27.5	625	150	-1.50	-34.5	24.5
530	160	-1.51	-34.7	16.6	578	180	-1.20	-30.0	27.2	626	260	1.09	-21.1	22.1
531	160	-1.65	-38.0	26.4	579	180	-1.17	-29.2	23.1	627	140	-1.14	-26.2	12.5
532	190	-1.44	-36.0	27.4	580	150	-1.24	-28.5	13.7	628	340	-1.18	-25.9	12.8
533	310	-1.54	-33.9	29.0	581	200	-1.20	-30.0	23.2	629	340	-.99	-21.8	18.5
534	310	1.45	-29.3	32.0	582	310	-1.38	-30.3	12.4	630	150	-1.06	-24.4	17.0
535	330	-1.34	-29.4	26.5	583	90	-1.16	-26.1	12.2	631	150	-1.06	-24.4	15.3
536	120	-1.45	-32.7	13.5	584	160	-1.33	-30.6	26.4	632	150	-1.03	-23.6	20.1
537	340	-1.36	-29.9	18.7	585	160	-1.99	-45.8	22.1	633	150	-1.07	-24.7	20.4
538	240	1.50	-27.6	30.4	586	140	-1.29	-29.6	26.0	634	160	-1.03	-23.7	19.5
539	190	-1.57	-39.3	28.1	587	150	-1.53	-35.3	19.1	635	150	-1.12	-25.7	20.5
540	190	-1.35	-33.8	28.0	588	160	-1.29	-29.6	22.8	636	150	-1.44	-33.1	23.2
541	310	-1.17	-25.8	21.3	589	200	-1.04	-26.0	24.7	637	150	-1.06	-24.3	21.2
542	170	-1.12	-25.8	16.0	590	150	-1.18	-27.1	17.6	638	140	-.95	-21.9	21.2
543	310	-1.09	-24.0	16.6	591	210	-1.71	-42.7	13.9	639	150	-1.13	-26.0	23.2
544	170	-2.79	-64.1	27.5	592	210	-1.12	-28.0	14.6	640	140	-2.15	-49.3	17.3
545	180	-1.82	-45.5	23.8	593	90	-1.34	-30.1	11.1	641	150	-1.50	-34.6	26.0
546	170	-1.42	-32.6	27.7	594	150	-1.41	-32.3	26.3	701	310	-1.59	-35.0	28.3
547	250	1.25	-23.6	25.4	595	160	-1.74	-40.1	21.1	702	350	1.52	-30.0	33.5
548	310	-1.36	-30.0	25.5	596	150	-1.24	-28.4	21.8	703	110	-1.33	-30.0	26.3
549	120	-1.11	-25.0	18.1	597	150	-1.50	-34.6	19.8	704	310	-1.56	-34.3	28.4
550	90	-1.66	-37.4	19.3	598	190	-1.33	-33.2	22.8	705	310	-1.61	-35.4	23.1

TABLE 6A. PEAK LOADS FOR CONFIGURATION C : LPC MANDALAY LAS COLLINAS,TEXAS
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----
706	170	-1.40	-32.1	31.7	754	60	-1.49	-25.3	6.5	802	140	-1.40	-32.1	20.5
707	350	1.30	-28.0	28.7	755	120	-1.16	-26.0	16.2	803	120	-1.49	-33.6	22.6
708	170	-1.41	-32.3	20.4	756	350	1.30	-26.4	28.5	804	310	-1.11	-24.3	18.8
709	100	-1.96	-44.1	27.4	757	350	1.29	-23.2	28.5	805	350	1.13	-24.0	24.8
710	350	-1.41	-31.1	24.6	758	350	1.47	-24.3	32.3	806	340	1.17	-23.9	25.7
711	300	-2.35	-41.1	17.9	759	320	-1.35	-29.6	22.4	807	130	-1.06	-24.5	23.5
712	170	-1.65	-38.0	28.3	760	130	-1.28	-29.5	23.6	808	210	-.88	-22.1	21.7
713	170	-1.45	-33.4	30.7	761	120	-1.47	-33.0	25.8	809	70	-1.47	-24.9	11.7
714	350	1.47	-30.0	32.4	762	130	-1.34	-30.8	24.0	810	200	-.93	-23.4	17.8
715	90	-1.73	-38.8	26.0	763	240	-1.37	-27.8	17.6	811	140	-1.43	-32.8	19.6
716	110	-1.77	-39.9	22.9	764	310	-1.24	-27.2	14.4	812	210	-.98	-24.5	21.7
717	320	-1.84	-40.5	15.4	765	340	-1.22	-26.8	15.0	813	200	-1.69	-42.3	13.3
718	330	-1.38	-30.4	20.3	766	130	-1.07	-24.5	14.6	814	310	-1.27	-27.9	11.3
719	170	-1.48	-34.1	29.7	767	350	1.24	-23.4	27.3	815	330	-1.29	-28.3	14.0
720	170	-1.29	-29.7	28.9	768	120	-1.19	-26.8	23.6	816	240	-1.65	-33.3	20.0
721	350	1.46	-30.0	32.1	769	320	-1.23	-27.1	21.6	817	100	-1.37	-30.9	19.5
722	100	-1.31	-29.5	25.2	770	130	-1.13	-26.0	21.3	818	130	-.99	-22.7	22.4
723	110	-1.23	-27.7	19.1	771	110	-1.30	-29.3	24.0	819	130	-1.29	-29.7	21.8
724	170	-1.45	-33.3	12.6	772	130	-1.25	-28.6	23.1	820	120	-2.16	-48.6	22.3
725	320	-1.36	-30.0	20.8	773	210	-1.17	-29.3	17.1	821	310	-1.17	-25.6	16.9
726	350	1.22	-26.8	26.9	774	150	-1.34	-30.9	14.3	822	310	-1.32	-29.1	12.7
727	350	1.33	-23.0	29.3	775	350	-1.45	-31.9	18.6	823	240	-1.28	-25.8	13.3
728	100	-1.22	-27.5	26.1	776	210	-.96	-24.0	14.5	824	260	-1.17	-23.6	18.4
729	100	-1.24	-28.0	24.7	777	350	1.26	-25.1	27.6	825	140	-1.17	-26.9	21.1
730	100	-1.58	-35.6	19.6	778	110	-1.13	-25.3	24.9	826	150	-1.12	-25.8	19.6
731	220	-1.59	-32.1	17.9	779	150	-1.68	-38.7	27.7	827	140	-1.05	-24.2	15.7
732	320	-1.58	-34.7	15.4	780	100	-1.34	-30.2	21.0	828	140	-.78	-18.0	14.7
733	340	-1.34	-29.6	25.4	781	130	-1.11	-25.5	21.4	829	150	-.85	-19.6	16.3
734	320	-1.24	-27.2	26.4	782	120	-1.31	-29.4	25.7	830	250	-1.60	-32.3	13.2
735	320	-1.49	-32.7	26.2	783	130	-1.32	-30.3	25.9	831	150	-1.19	-27.4	17.8
736	320	-1.48	-32.6	21.4	784	310	-1.32	-29.1	11.9	832	150	-1.04	-23.9	17.5
737	120	-1.37	-30.8	20.3	785	310	-1.34	-29.5	16.9	833	340	-1.18	-26.0	15.2
738	350	-1.15	-25.2	14.1	786	340	-1.57	-34.5	10.5	834	340	-1.21	-26.7	17.7
739	170	-1.42	-32.6	15.3	787	190	-.93	-23.3	19.3	835	230	-1.03	-20.9	18.5
740	340	-1.19	-26.1	22.8	788	210	-1.16	-28.9	28.6	836	230	-1.00	-20.2	18.5
741	110	-1.14	-25.6	24.7	789	110	-1.51	-33.9	23.9	837	340	1.05	-19.0	23.1
742	100	-1.59	-35.8	22.9	790	110	-1.35	-30.5	19.8	838	140	-1.03	-23.8	21.8
743	110	-1.15	-25.9	22.3	791	130	-1.23	-28.2	21.9	839	130	-1.35	-31.2	13.7
744	250	-2.37	-47.9	13.9	792	150	-1.38	-31.7	24.6	840	150	-.85	-19.7	15.9
745	110	-1.45	-32.5	16.9	793	120	-1.41	-31.6	23.3	841	140	-.99	-22.7	17.8
746	110	-1.32	-29.6	27.0	794	200	-1.31	-32.7	10.5	842	140	-.98	-22.6	18.6
747	340	-1.43	-31.5	30.0	795	200	-1.40	-35.0	17.0	843	340	1.20	-19.4	26.3
748	310	-1.35	-29.7	26.8	796	80	-1.65	-28.0	11.7	844	140	-.92	-21.1	18.4
749	340	-1.43	-31.4	22.2	797	210	-1.23	-30.8	15.2	845	330	1.06	-16.9	23.3
750	130	-2.20	-50.6	24.3	798	220	-1.48	-29.9	25.9	901	150	1.26	-27.3	29.1
751	340	1.33	-22.6	29.3	799	110	-1.40	-31.4	25.7	902	180	-2.07	-51.8	33.0
752	230	-1.36	-27.4	15.1	800	120	-1.53	-34.3	21.5	903	120	1.56	-33.8	35.2
753	220	-1.43	-28.9	13.1	801	130	-1.59	-36.6	19.1	904	100	1.47	-30.1	33.0

TABLE 6A. PEAK LOADS FOR CONFIGURATION C : LPC MANDALAY LAS COLLINAS,TEXAS
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ---- PSF	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ---- PSF	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ---- PSF
905	110	2.22	-31.7	49.9	944	170	-1.25	-31.3	5.9	983	210	-1.70	-42.4	15.5
906	90	1.32	-28.5	29.7	945	170	1.59	-28.9	36.5	984	280	-2.12	-37.1	25.8
907	90	1.14	-25.2	25.7	946	210	1.22	-25.1	30.5	985	350	-1.49	-32.8	23.8
908	180	-2.01	-50.3	27.2	947	190	1.29	-24.2	32.4	986	170	-1.40	-32.3	17.0
909	190	-1.14	-28.5	24.7	948	150	-2.22	-51.0	6.1	987	340	-1.21	-26.5	13.7
910	200	-1.11	-27.8	26.7	949	210	-1.47	-36.8	5.0	988	310	1.12	-24.3	24.7
911	190	-1.13	-28.2	23.0	950	190	-1.21	-30.3	5.9	989	190	-1.03	-25.8	18.1
912	200	-.98	-24.6	17.8	951	130	-1.18	-27.2	6.6	990	170	-1.45	-33.5	21.1
913	180	-1.14	-28.6	27.5	952	90	-1.33	-29.8	6.2	991	310	1.27	-26.1	27.9
914	170	1.34	-21.0	30.9	953	90	-1.62	-36.5	7.0	992	180	-1.39	-34.6	22.0
915	120	-1.29	-29.1	23.0	954	350	1.17	-24.2	25.7	993	160	-1.36	-31.2	16.0
916	190	-1.81	-45.3	24.9	955	350	1.15	-22.4	25.3	994	150	-1.08	-24.8	22.1
917	120	-2.70	-60.7	18.4	956	350	1.74	-29.5	38.4	995	170	-1.67	-38.4	24.3
918	120	-2.29	-51.6	9.1	957	180	-1.17	-29.3	6.1	996	310	-1.47	-32.3	26.6
919	90	-1.81	-40.7	6.6	958	200	1.39	-27.8	34.9	997	170	-1.31	-30.2	28.8
920	170	-2.21	-50.8	10.1	959	210	-2.15	-53.8	8.4	998	150	-1.39	-32.1	26.4
921	100	-2.07	-46.5	16.7	960	190	-1.75	-43.7	12.5	999	50	-1.38	-23.4	20.4
922	110	-1.76	-39.6	15.8	961	190	-1.39	-34.7	15.7	1000	300	-1.58	-27.7	10.0
923	100	-1.03	-23.2	15.8	962	350	-1.30	-28.5	12.8	1001	120	1.22	-17.7	27.5
924	90	1.14	-24.0	25.6	963	350	-1.70	-37.5	13.0	1002	90	1.09	-21.7	24.5
925	110	-1.86	-41.7	27.2	964	350	-1.62	-35.6	18.9	1003	170	-1.98	-45.6	20.2
926	90	-1.56	-35.2	17.2	965	150	-1.34	-30.7	30.0	1004	190	-.57	-14.2	10.5
927	110	-1.44	-32.5	29.6	966	190	-1.20	-30.1	5.5	1005	130	-.95	-22.0	8.6
928	180	-2.35	-58.7	15.0	967	150	-1.67	-38.3	32.2	1006	140	-.50	-11.6	10.4
929	200	-1.70	-42.5	13.0	968	210	-2.14	-53.5	20.4	1007	200	-.50	-12.6	10.0
930	120	-1.85	-41.6	10.8	969	180	-1.71	-42.7	9.4	1008	200	-.55	-13.7	10.9
931	90	-1.79	-40.2	16.1	970	170	-1.73	-39.9	12.3	1009	180	1.04	-18.1	26.1
932	90	-1.78	-40.1	13.4	971	310	-1.54	-33.8	12.1	1010	140	-1.05	-24.2	20.1
933	60	-2.10	-35.7	10.7	972	260	-1.64	-33.3	25.8	1011	180	1.06	-16.1	26.6
934	100	-1.63	-36.7	21.6	973	350	-1.58	-34.7	28.2	1012	330	1.02	-20.6	22.5
935	120	-1.61	-36.3	5.6	974	220	-1.75	-35.5	24.7	1013	160	1.05	-22.6	24.2
936	110	-1.49	-33.6	30.8	975	260	-1.65	-33.5	29.9	1014	350	.98	-20.4	21.5
937	170	-2.76	-63.5	8.2	976	170	-1.41	-32.4	16.5	1015	200	.89	-20.8	22.1
938	180	-1.77	-44.3	11.2	977	190	-1.58	-39.4	24.3	1016	240	-1.14	-23.1	18.2
939	190	-1.60	-40.1	9.4	978	110	-1.27	-28.5	22.3	1017	160	-.97	-22.3	19.9
940	90	-1.52	-34.2	20.3	979	180	-1.50	-37.5	18.5	1018	310	1.17	-24.5	25.6
941	120	-1.58	-35.5	11.2	980	260	-1.78	-36.0	14.3	1019	150	-1.22	-28.1	21.1
942	60	-2.17	-36.9	7.6	981	230	-2.35	-47.5	8.5	1020	140	-1.17	-26.9	20.8
943	310	-1.42	-31.3	24.0	982	210	-2.07	-51.9	8.2					

TABLE 6A. PEAK LOADS FOR CONFIGURATION C : LPC MANDALAY LAS COLLINAS,TEXAS
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 25.0 PSF

* * 15 GREATEST PRESSURE MAGNITUDES * *

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK
			PSF	
544	170	-2.79	-64.1	27.5
937	170	-2.76	-63.5	8.2
917	120	-2.70	-60.7	18.4
928	180	-2.35	-58.7	15.0
149	180	-2.20	-55.0	28.7
508	350	-2.46	-54.2	20.6
344	90	-2.40	-54.0	38.2
959	210	-2.15	-53.8	8.4
968	210	-2.14	-53.5	20.4
982	210	-2.07	-51.9	8.2
902	180	-2.07	-51.8	33.0
918	120	-2.29	-51.6	9.1
109	180	-2.06	-51.4	30.0
150	210	-2.05	-51.4	34.4
948	150	-2.22	-51.0	6.1

TABLE 6A. PEAK LOADS FOR CONFIGURATION D :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK
			PSF					PSF					PSF	
141	356	1.18	-22.3	26.6	730	306	1.34	30.0	23.0	917	350	2.68	-60.2	20.2
149	308	-2.55	-50.6	31.5	732	304	1.57	-36.1	11.1	920	24	-2.85	-64.1	5.6
150	288	-1.60	-40.1	38.5	737	348	1.42	32.0	23.3	937	300	2.78	64.0	10.6
544	300	-2.77	-63.7	26.4	744	218	2.09	42.4	14.3	942	46	2.28	-30.8	9.3
727	358	-1.11	-24.9	16.3	750	342	2.50	53.3	26.2	959	280	1.65	-41.4	4.5

TABLE 6A. PEAK LOADS FOR CONFIGURATION D :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

* * 15 GREATEST PRESSURE MAGNITUDES * *

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK
			PSF	
920	24	-2.85	-64.1	5.6
937	300	-2.78	-64.0	10.6
544	300	2.77	63.7	26.4
717	350	-2.68	-60.2	20.2
149	300	-2.55	-58.6	31.5
750	342	-2.50	-56.3	26.2
744	210	-2.09	-42.4	14.3
959	200	-1.65	-41.4	4.5
150	200	-1.60	-40.1	38.5
942	46	2.28	38.8	9.3
732	304	1.57	36.1	11.1
737	348	-1.42	-32.0	23.3
730	306	-1.34	-30.8	23.0
144	356	1.18	22.3	26.6
727	358	-1.11	-24.9	16.3

TABLE 6A. PEAK LOADS FOR CONFIGURATION E :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK
			---- PSF ----					---- PSF ----					---- PSF ----	
144	120	-2.71	-59.7	7.5	544	320	-2.76	-63.6	20.9	750	330	-2.66	-59.8	15.7
149	312	-2.68	-61.7	32.3	732	124	1.35	22.1	22.8	937	300	-2.85	-65.5	9.3
150	226	-2.02	-41.0	31.6	744	210	2.27	45.9	29.0					

TABLE 6A. PEAK LOADS FOR CONFIGURATION E :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

* * 8 GREATEST PRESSURE MAGNITUDES * *

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK
			PSF	
937	300	-2.05	-65.5	9.3
544	320	-2.76	-63.6	28.9
149	312	-2.68	-61.7	32.3
750	338	-2.66	-59.8	15.7
144	120	-2.71	-59.7	7.5
744	218	-2.27	-45.9	29.0
150	226	-2.02	-41.0	31.6
732	124	1.35	22.1	29.8

TABLE 6A. PEAK LOADS FOR CONFIGURATION W :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----
101	280	-1.29	-32.4	27.6	149	300	-2.53	-50.2	28.7	197	130	-1.21	-26.6	21.8
102	280	-1.42	-35.6	25.0	150	250	-2.48	-62.0	34.4	198	250	-1.62	-40.5	27.1
103	290	-1.49	-37.3	28.3	151	290	-1.35	-33.7	33.3	199	280	-1.12	-28.0	27.9
104	120	-1.55	-34.0	26.8	152	120	-1.80	-39.5	26.2	200	290	-1.97	-49.2	25.0
105	260	-1.31	-32.8	19.7	153	340	-1.48	-33.3	24.8	201	250	-1.20	-30.1	26.3
106	290	-1.42	-35.5	26.5	154	330	-1.37	-31.5	29.4	202	250	-1.32	-33.0	26.4
107	290	-1.59	-39.7	26.9	155	250	-1.47	-36.7	29.9	203	320	-1.33	-30.3	30.6
108	290	-1.57	-39.3	27.6	156	280	-1.33	-33.3	30.7	204	310	-1.59	-36.5	23.3
109	290	-2.06	-51.4	30.0	157	290	-1.29	-32.2	31.4	205	270	-1.19	-29.8	23.3
110	10	-1.43	-32.1	29.3	158	290	-1.46	-36.5	30.0	206	250	-1.17	-29.3	22.5
111	250	-1.11	-27.8	24.7	159	200	-2.05	-51.3	31.9	207	240	-1.44	-29.1	22.8
112	10	1.56	-34.4	35.1	160	250	-1.39	-34.8	33.7	208	10	-1.38	-31.0	27.3
113	290	-1.32	-33.0	32.5	161	250	-1.85	-46.3	33.8	209	10	-1.31	-29.5	22.4
114	290	-1.53	-38.3	29.3	162	250	-1.81	-45.2	30.6	210	130	-1.20	-26.3	22.5
115	290	-1.95	-48.7	29.4	163	290	-1.53	-38.3	25.6	211	300	-1.61	-37.1	21.2
116	280	-1.67	-41.7	29.9	164	330	-1.38	-31.7	23.8	212	350	-1.40	-31.5	27.3
117	250	-1.06	-26.5	21.5	165	310	-1.53	-35.2	24.5	213	120	-1.73	-38.0	23.8
118	280	-1.31	-32.7	24.5	166	260	-1.45	-36.1	27.0	214	250	-.93	-23.3	20.2
119	10	1.48	-32.0	33.4	167	120	-1.52	-33.4	28.0	215	150	1.12	-24.7	22.1
120	20	1.39	-31.1	31.3	168	280	-1.46	-36.5	26.6	216	130	-1.32	-29.0	22.2
121	280	-1.44	-36.0	29.0	169	300	-1.77	-40.7	28.1	217	300	-2.08	-47.9	25.6
122	280	-1.45	-36.2	26.2	170	240	-1.45	-29.4	28.9	218	250	-1.12	-28.0	24.8
123	290	-1.49	-37.4	29.0	171	260	-1.32	-33.0	29.7	219	250	-1.20	-30.1	27.0
124	260	-1.12	-27.9	25.1	172	310	1.41	-31.2	32.4	220	250	-1.93	-48.3	25.8
125	20	1.15	-24.8	25.9	173	340	-1.18	-26.6	24.2	221	330	-1.01	-23.2	20.0
126	270	-1.05	-26.3	25.7	174	290	-1.12	27.9	24.1	222	260	-1.14	-28.4	13.6
127	290	-1.15	-28.8	27.0	175	320	-1.42	-32.6	25.7	223	320	-1.12	-25.8	12.6
128	280	-1.42	-35.4	27.3	176	250	-1.39	-34.9	32.9	224	130	-1.21	-26.6	23.5
129	290	-1.29	-32.3	26.9	177	20	1.25	-27.6	28.1	225	0	1.11	-21.1	25.1
130	300	-1.83	-42.2	29.9	178	290	-1.50	-37.5	28.0	226	350	1.19	-26.5	26.8
131	340	-1.59	-35.8	26.0	179	280	-1.43	-35.6	28.9	227	150	-1.03	-22.7	19.5
132	270	-1.12	-28.0	23.7	180	290	-1.67	-41.7	27.1	228	310	1.21	-21.5	27.8
133	20	1.49	-24.5	33.5	181	250	-1.28	-32.1	29.6	229	300	1.09	-24.7	25.1
134	290	-1.16	-29.1	28.7	182	340	1.48	-30.8	33.4	230	240	-1.27	-25.6	14.0
135	290	-1.37	-34.4	29.7	183	270	1.44	-35.9	29.8	231	320	1.08	-22.7	24.7
136	280	-1.88	-47.0	29.5	184	310	-1.46	-33.7	23.2	232	230	-.90	-18.3	15.4
137	20	-1.67	-37.5	34.8	185	330	-1.29	-29.7	22.9	233	280	-.84	-21.1	17.8
138	330	-1.36	-31.3	26.1	186	340	-1.42	-31.9	26.1	234	320	-1.13	-25.9	15.7
139	250	-1.13	-28.2	27.5	187	250	-1.15	-28.8	25.4	235	150	-.64	-14.0	11.0
140	10	1.30	-29.1	29.3	188	290	-1.27	-31.7	28.6	236	250	-.51	-12.8	10.5
141	290	-1.27	-31.7	29.4	189	290	-1.46	-36.5	27.8	237	230	-.66	-13.4	9.9
142	280	-1.79	-44.8	31.2	190	290	-1.48	-37.0	27.9	238	300	-.59	-13.5	10.6
143	310	1.39	-27.9	31.9	191	20	-1.44	-32.4	27.8	239	320	.94	-21.6	21.7
144	120	-2.65	-58.3	27.3	192	250	-1.56	-39.0	26.4	240	150	-1.00	-22.0	21.7
145	250	-1.29	-32.1	30.6	193	250	-1.35	-33.7	27.1	241	290	.93	-18.5	23.3
146	310	-1.40	-32.3	31.9	194	120	-1.49	-32.8	22.0	301	10	-1.68	-37.8	32.3
147	290	-1.36	-33.9	29.8	195	130	-1.41	-30.9	22.6	302	0	-1.55	-34.9	31.1
148	350	1.46	-31.0	32.9	196	310	-2.30	-52.8	23.9	303	200	1.19	-29.7	29.8

TABLE 6A. PEAK LOADS FOR CONFIGURATION W :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----
304	340	-1.95	-43.8	37.8	352	350	1.41	-30.7	31.6	400	150	-1.73	-38.0	23.9
305	0	-1.51	-34.0	29.9	353	250	-1.95	-48.6	33.7	401	310	-1.96	-45.0	24.4
306	10	-1.62	-36.5	35.2	354	260	-1.38	-34.5	29.9	402	310	-1.86	-42.8	26.6
307	260	1.31	-29.4	32.7	355	0	-1.68	-37.8	31.8	403	320	-1.34	-30.8	23.6
308	10	-1.45	-32.6	30.4	356	290	1.43	-33.0	35.7	404	200	-1.50	-37.5	26.0
309	190	-2.22	-38.9	32.8	357	280	1.31	-30.0	32.8	405	290	1.13	-27.5	28.4
310	10	-1.64	-36.9	31.2	358	290	1.24	-30.2	31.0	406	280	1.02	-25.1	27.2
311	0	-2.19	-49.2	32.5	359	260	1.27	-31.3	31.7	407	260	1.08	-26.4	27.0
312	250	-1.47	-36.8	32.7	360	320	-1.58	-36.2	35.2	408	270	-1.27	-31.8	29.6
313	290	1.37	-28.6	34.2	361	310	-1.59	-36.7	32.8	409	300	-1.41	-32.3	23.5
314	280	1.46	-29.7	36.6	362	250	1.43	30.9	35.8	410	150	-1.35	-29.6	26.3
315	200	-2.05	-35.9	32.3	363	320	1.36	-27.5	31.2	411	250	1.01	-24.7	25.3
316	270	-1.26	-31.6	30.6	364	250	-1.24	-31.0	30.2	412	270	-1.41	-35.4	21.0
317	310	1.46	-32.2	33.6	365	250	1.25	-31.1	28.8	413	20	-1.67	-37.5	28.1
318	290	1.33	-32.8	33.2	366	0	-1.67	-37.6	33.5	414	290	1.00	-24.5	25.1
319	290	1.48	-30.8	36.9	367	0	-1.42	-32.0	30.7	415	20	-1.13	-25.4	25.2
320	270	1.42	-28.0	35.6	368	280	1.37	-31.7	34.3	416	0	-1.58	-35.4	28.9
321	270	1.44	-29.2	36.1	369	260	1.36	-31.8	33.9	417	210	-1.44	-29.2	25.4
322	250	1.26	-27.1	31.5	370	290	-1.26	-31.6	28.0	418	290	-1.15	-28.8	26.1
323	150	-1.51	-33.2	31.2	371	260	1.19	-29.7	29.8	419	330	-1.36	-31.3	23.0
324	10	-1.94	-43.6	28.9	372	150	1.53	-33.7	29.4	420	150	-1.51	-33.2	22.9
325	10	-1.70	-38.3	33.4	373	350	1.31	-28.1	29.6	421	270	1.11	-19.6	27.7
326	280	1.41	-33.4	35.4	374	260	-1.19	-29.7	27.1	422	20	-1.13	-25.5	25.1
327	280	1.41	-25.8	35.2	375	270	-1.39	-34.8	30.1	423	0	-1.67	-37.6	27.3
328	270	1.32	-25.4	33.1	376	0	-1.64	-37.0	29.3	424	300	1.20	-23.9	27.7
329	290	1.20	-25.6	29.9	377	0	-1.43	-32.2	27.6	425	150	-1.53	-33.7	24.9
330	250	1.27	-31.4	31.8	378	0	-1.58	-35.4	29.2	426	300	1.23	-25.0	28.2
331	20	-1.66	-37.2	32.2	379	0	-1.43	-32.2	29.8	427	150	-1.57	-34.5	23.6
332	350	-1.55	-34.9	32.0	380	190	-1.95	-34.2	27.2	428	310	-1.54	-35.4	31.3
333	280	1.36	-33.7	33.9	381	310	-1.62	-37.2	29.0	429	140	-1.16	-25.6	23.8
334	280	1.42	-28.7	35.4	382	310	-1.35	-31.0	26.9	430	290	1.36	-26.8	34.1
335	280	1.45	-27.5	36.3	383	310	-1.29	-29.6	24.4	431	260	.89	-21.6	22.3
336	190	-1.91	-33.5	30.8	384	310	1.29	-26.9	29.7	432	330	1.06	-20.4	24.4
337	310	-1.67	-38.4	32.5	385	250	-1.41	-35.2	28.6	433	290	.96	-22.9	23.9
338	320	1.43	-32.6	32.8	386	260	-1.44	-36.1	27.1	434	130	-1.28	-28.1	22.3
339	0	-1.93	-43.4	32.3	387	10	-1.68	-37.8	33.2	435	290	.95	-19.9	23.7
340	290	1.37	-28.8	34.2	388	0	-1.47	-33.1	30.6	436	200	.92	-19.9	23.1
341	280	1.29	-26.6	32.2	389	190	-1.69	-29.5	29.4	437	260	.92	-21.7	23.1
342	250	1.48	-33.6	36.9	390	270	1.19	-29.3	29.6	438	270	1.16	-27.9	28.9
343	250	1.25	-28.7	31.2	391	320	-2.08	-47.8	27.7	439	320	-1.18	-27.0	20.2
344	20	-2.40	-54.0	38.2	392	320	-1.65	-30.0	25.2	440	10	-1.37	-30.8	25.9
345	0	-2.24	-50.4	33.8	393	310	-1.50	-34.4	25.6	441	130	-1.36	-30.0	23.3
346	280	1.70	-32.4	42.5	394	20	-1.24	-28.0	27.5	442	270	1.06	-15.8	26.6
347	10	-1.49	-33.6	32.9	395	260	-1.34	-33.5	26.9	443	330	1.04	-22.6	24.0
348	280	1.32	-27.3	33.1	396	250	-1.84	-45.9	24.4	444	260	1.02	-15.6	25.4
349	210	-2.22	-45.1	34.0	397	0	-1.60	-36.0	28.4	445	290	1.00	-20.8	25.0
350	150	-2.42	-53.2	35.2	398	10	-1.51	-34.1	31.3	501	270	-1.39	-34.8	28.3
351	300	1.43	-27.3	32.8	399	250	1.14	-26.8	28.6	502	280	-1.50	-37.4	22.3

TABLE 6A. PEAK LOADS FOR CONFIGURATION W :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)
503	280	-1.35	-33.6	25.4	551	280	-1.29	-32.3	25.3	599	320	-1.40	-32.2	22.4
504	290	-1.85	-46.2	24.6	552	300	-1.73	-39.8	20.0	600	330	-1.55	-35.7	22.9
505	280	-1.38	-34.5	24.1	553	270	-1.38	-34.6	33.1	601	260	-1.44	-36.0	24.5
506	280	-1.23	-30.8	26.5	554	150	1.32	-29.0	27.1	602	230	-1.42	-28.7	25.4
507	310	-1.35	-31.2	24.8	555	280	-1.53	-38.2	27.9	603	20	-1.39	-31.2	23.0
508	120	-2.46	-54.2	25.2	556	260	-1.27	-31.6	26.5	604	270	1.21	-27.5	30.3
509	120	-1.69	-37.3	24.7	557	270	-1.50	-37.6	25.0	605	320	-1.38	-31.8	19.9
510	290	-1.51	-37.7	24.0	558	270	-1.26	-31.4	25.7	606	320	-1.09	-25.1	21.9
511	260	-2.10	-52.5	33.0	559	300	-1.28	-29.4	26.4	607	320	-1.52	-34.9	22.5
512	280	-1.37	-34.2	25.6	560	220	-1.57	-31.7	27.4	608	270	-1.16	-29.0	22.1
513	290	-1.10	-27.6	26.0	561	250	-1.21	-30.2	28.9	609	200	-1.66	-29.0	23.1
514	350	-1.39	-31.2	23.9	562	150	1.33	-26.5	27.2	610	270	-1.31	-32.8	19.4
515	120	-2.17	-47.8	25.8	563	290	-1.21	-30.2	30.1	611	320	-1.65	-38.0	21.0
516	130	-1.30	-28.5	23.9	564	300	-1.43	-32.8	25.2	612	250	-1.09	-27.2	23.1
517	260	-1.38	-34.5	29.9	565	320	-1.33	-30.7	26.7	613	310	-2.16	-49.8	24.1
518	260	-1.32	-32.9	26.0	566	290	-1.48	-37.1	25.7	614	320	-1.60	-36.9	22.5
519	270	-1.32	-32.9	24.7	567	280	-1.32	-32.9	26.4	615	150	-1.41	-30.9	22.5
520	280	-1.18	-29.4	25.2	568	300	-1.19	-27.3	24.2	616	330	-1.73	-39.8	21.0
521	120	-1.28	-28.1	24.3	569	290	1.83	-45.9	23.7	617	320	-1.37	-31.4	21.5
522	340	-1.82	-41.1	24.9	570	230	-1.45	-29.3	27.5	618	140	1.24	-25.0	27.3
523	350	-1.90	-42.8	24.2	571	140	1.40	28.4	30.8	619	130	-1.13	-25.0	22.8
524	280	-1.78	-44.5	29.3	572	130	1.36	25.0	30.0	620	20	-1.55	-34.9	24.8
525	270	-1.27	-31.6	23.7	573	320	-1.44	-33.1	30.2	621	310	-1.42	-32.6	21.5
526	280	-1.28	-32.0	22.3	574	310	-1.69	-38.8	30.9	622	310	-1.53	-35.1	25.3
527	170	1.57	-26.3	27.5	575	320	-1.44	-33.1	26.8	623	320	-1.31	-30.0	19.9
528	280	-1.07	-26.8	23.7	576	270	-1.58	-39.6	24.0	624	320	-1.63	-37.5	19.9
529	290	-1.05	-26.3	23.3	577	270	-1.44	-36.0	23.6	625	320	-1.50	-34.5	22.1
530	310	-1.51	-34.7	28.1	578	290	-1.20	-30.0	23.7	626	10	-1.28	-28.8	22.1
531	310	-1.65	-38.0	26.4	579	280	-1.20	30.0	23.1	627	320	-1.42	-32.6	18.6
532	260	-1.54	-38.6	27.4	580	320	-1.61	-37.1	22.0	628	130	-1.18	-25.9	23.5
533	270	-1.24	-30.9	24.8	581	250	1.38	-34.6	25.1	629	150	1.28	-25.7	28.1
534	150	-1.33	-29.3	25.4	582	250	-1.34	-33.6	27.6	630	310	-1.35	-31.1	21.3
535	140	-1.34	-29.4	23.6	583	150	1.30	26.3	28.5	631	320	-1.43	-32.9	20.4
536	350	-1.45	-32.7	24.7	584	300	-1.37	31.5	29.2	632	310	-1.31	-30.1	22.5
537	250	-1.20	-30.0	27.0	585	310	1.99	-45.8	24.2	633	320	-1.15	-26.5	20.4
538	230	1.50	-27.6	30.4	586	250	1.24	-29.6	30.9	634	280	-1.18	-29.5	20.2
539	270	-1.82	-45.6	28.1	587	260	-1.44	-35.9	22.5	635	330	-1.70	-39.1	18.8
540	280	-1.50	-37.5	25.7	588	280	-1.37	-34.4	22.8	636	320	-1.44	-33.1	23.3
541	290	-1.06	-26.5	25.0	589	260	-1.18	-29.5	22.7	637	320	2.03	-46.6	19.4
542	120	-1.43	-31.5	28.5	590	310	-1.45	33.5	22.0	638	330	-1.19	-27.3	21.2
543	140	1.31	-25.8	28.9	591	260	-1.71	-42.7	23.7	639	320	-1.58	-36.3	23.2
544	320	-2.81	-64.7	32.2	592	250	-1.25	31.2	26.1	640	330	-2.15	-49.3	19.6
545	270	-2.16	-53.9	26.4	593	250	-1.36	34.0	25.0	641	310	-1.51	-34.7	26.0
546	270	-1.39	-34.7	27.7	594	320	1.41	-32.3	26.3	701	140	-1.43	-31.4	28.3
547	280	-1.04	-26.1	26.0	595	310	-1.74	-40.1	23.5	702	120	1.52	-30.0	33.5
548	270	-1.15	-28.8	24.8	596	320	-1.51	-34.7	22.4	703	20	-1.65	-37.1	26.3
549	120	-2.04	-44.8	28.1	597	270	-1.62	-40.6	22.1	704	170	-1.80	-31.4	28.4
550	60	-2.37	-40.3	27.5	598	320	-1.47	-33.8	22.8	705	170	-1.94	-33.9	25.5

TABLE 6A. PEAK LOADS FOR CONFIGURATION W :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)
706	300	-1.40	-32.1	31.7
707	10	-1.47	-33.1	28.7
708	20	-1.71	-38.4	20.4
709	10	-1.96	-44.1	27.4
710	200	-1.82	-31.9	24.6
711	170	-2.35	-41.1	25.5
712	300	-1.65	-38.0	28.3
713	300	-1.45	-33.4	30.7
714	20	-1.50	-33.8	32.4
715	10	-2.05	-46.1	26.0
716	0	-1.77	-39.9	22.9
717	150	-1.84	-40.5	27.1
718	140	-1.38	-30.4	26.7
719	300	-1.48	-34.1	29.7
720	300	-1.29	-29.7	28.9
721	120	1.46	-31.8	32.1
722	10	-1.63	-36.7	25.2
723	20	-1.32	-29.8	19.3
724	300	-1.45	-33.3	25.9
725	150	-1.36	-30.0	25.9
726	10	-1.21	-27.2	26.9
727	120	1.33	-26.3	29.3
728	10	-1.39	-31.4	26.1
729	20	-1.26	-28.3	24.7
730	10	-1.58	-35.6	20.3
731	250	-1.59	-39.6	33.2
732	150	-1.58	-34.7	25.3
733	130	-1.34	-29.6	28.6
734	150	-1.24	-27.2	26.4
735	150	-1.49	-32.7	26.2
736	20	-1.61	-36.3	21.4
737	340	-1.40	-31.5	20.7
738	130	1.34	-29.5	29.5
739	170	-2.00	-35.0	35.0
740	10	-1.16	-26.1	24.3
741	20	-1.41	-31.7	24.7
742	20	-1.72	-38.8	22.9
743	10	-1.25	-28.1	26.3
744	220	-2.37	-47.9	29.8
745	180	-2.08	-36.4	27.3
746	0	-1.32	-29.6	28.7
747	130	-1.43	-31.5	30.2
748	10	-1.52	-34.2	26.8
749	20	-2.07	-46.6	22.2
750	330	-2.45	-56.3	24.3
751	130	1.33	-27.9	29.3
752	250	-1.20	-30.1	28.9
753	250	-1.43	-35.7	28.5
754	140	1.28	-26.4	28.2
755	350	1.52	-34.1	28.1
756	20	-1.30	-29.2	28.5
757	20	-1.36	-30.7	28.5
758	10	-1.55	-34.9	32.3
759	10	-1.61	-36.1	21.6
760	130	-1.68	-37.0	23.6
761	130	-1.56	-34.3	25.8
762	320	-1.34	-30.8	25.6
763	150	1.33	-28.5	29.3
764	130	1.24	-26.6	27.4
765	130	1.25	-26.8	27.6
766	340	-1.70	-38.2	27.6
767	340	-1.36	-30.5	27.3
768	20	-1.50	-33.7	23.6
769	10	-1.46	-32.9	21.6
770	130	-1.37	-30.1	20.5
771	0	-1.30	-29.3	24.0
772	350	-1.25	-28.2	23.1
773	260	-1.17	-29.3	28.0
774	250	-1.30	-32.6	26.7
775	120	-1.45	31.9	27.6
776	350	1.65	37.2	25.8
777	270	-1.75	-43.8	27.6
778	20	-1.35	-30.5	26.8
779	320	-1.68	-38.7	27.7
780	20	-1.57	35.4	21.0
781	130	-1.30	-28.5	21.4
782	130	-1.34	-29.6	25.7
783	340	-1.32	-29.6	25.9
784	250	-1.31	-32.7	24.1
785	230	-2.01	-40.6	26.3
786	130	-1.57	34.5	25.4
787	310	-1.77	-40.7	25.9
788	250	1.37	34.3	28.6
789	0	-1.51	-33.9	23.9
790	10	-1.76	39.5	18.8
791	320	-1.33	-30.5	21.9
792	320	-1.38	-31.7	24.6
793	350	-1.41	-31.6	23.5
794	230	-1.67	-33.9	24.9
795	270	-1.40	-35.0	24.9
796	30	-1.65	-28.0	27.8
797	230	-1.56	-31.7	24.6
798	250	-1.48	-36.9	25.9
799	340	-1.54	-34.7	25.7
800	10	-1.79	-40.2	21.5
801	340	-1.59	-35.8	19.1
802	130	-1.73	-38.0	20.5
803	310	-1.66	-38.2	22.6
804	120	-1.31	-28.7	23.2
805	330	-1.27	-29.1	24.8
806	310	-1.22	-28.0	25.7
807	220	-1.70	-34.5	23.5
808	120	-1.19	-26.3	22.8
809	320	-1.46	-33.7	21.2
810	330	-1.22	-28.1	24.6
811	330	-1.43	-32.8	19.6
812	130	-1.43	-31.5	21.7
813	270	-1.69	-42.3	24.0
814	310	-1.49	-34.2	25.7
815	140	-1.29	-28.3	24.5
816	250	-1.54	-38.6	23.6
817	10	-1.54	-34.7	19.5
818	300	-1.04	-24.0	22.4
819	340	-1.29	-29.1	23.9
820	350	-2.16	-48.6	22.3
821	0	-1.16	-26.0	21.3
822	270	-1.06	-26.4	22.4
823	300	-1.34	-30.8	22.4
824	330	-1.04	-23.9	20.5
825	320	-1.53	-35.3	22.6
826	310	-1.54	-35.3	19.6
827	330	-1.41	-32.5	15.8
828	190	-1.34	-23.5	14.8
829	250	-.94	-23.5	16.8
830	220	-1.60	-32.3	24.4
831	310	-1.21	-27.8	17.8
832	350	-1.42	-32.0	21.5
833	300	-1.13	-26.0	21.9
834	310	-1.26	-29.0	21.9
835	320	-1.09	-25.0	23.8
836	320	-1.04	-23.9	19.9
837	230	-1.28	-25.9	23.1
838	330	-1.06	-24.3	21.8
839	300	-1.61	-36.9	13.7
840	320	-.85	-19.7	15.9
841	200	-1.38	-24.2	17.8
842	330	-1.07	-24.5	18.6
843	150	1.26	-19.0	27.7
844	310	-.99	-22.7	21.5
845	140	1.35	-17.7	29.7
901	340	1.45	-27.3	32.7
902	290	-2.07	-51.8	33.0
903	130	-1.67	-36.7	35.2
904	250	-1.48	-37.1	33.0

TABLE 6A. PEAK LOADS FOR CONFIGURATION W :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF ----	POSITIVE PEAK ---- PSF ----	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF ----	POSITIVE PEAK ---- PSF ----	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF ----	POSITIVE PEAK ---- PSF ----
905	0	2.22	-39.2	49.9	944	200	-1.25	-31.3	4.8	983	150	-2.07	-45.6	15.5
906	20	1.32	-28.5	29.7	945	280	1.70	-28.9	42.6	984	150	-1.96	-43.0	25.8
907	20	1.14	-25.2	25.7	946	290	1.28	-27.9	32.0	985	120	-1.49	-32.8	23.8
908	290	-2.01	-50.3	27.2	947	280	1.29	-25.2	32.4	986	300	-1.40	-32.3	21.4
909	250	-1.33	-33.2	24.7	948	320	-2.22	51.0	6.1	987	130	1.30	-26.5	28.5
910	10	1.39	-29.4	31.4	949	260	-1.47	-36.8	5.0	988	270	-1.18	-29.4	21.7
911	290	-1.27	-31.8	23.0	950	280	-1.21	-30.3	5.9	989	270	-1.13	-28.3	18.1
912	270	-.98	-24.6	17.8	951	320	-1.22	-28.0	6.6	990	300	-1.45	-33.5	21.1
913	0	1.27	-28.6	28.6	952	20	-1.33	-29.8	6.2	991	270	-1.15	-28.8	24.2
914	290	1.43	-21.0	35.8	953	20	-1.62	-36.5	7.0	992	270	-1.94	-48.6	24.6
915	350	-1.29	-29.1	27.8	954	20	-1.24	-27.9	25.7	993	120	-1.59	-34.9	23.8
916	280	-1.81	-45.3	24.9	955	20	-1.20	-27.0	25.3	994	280	-1.17	-29.2	25.9
917	350	-2.70	-60.7	19.8	956	120	1.74	-36.2	38.4	995	300	-1.67	-38.4	30.0
918	350	-2.29	-51.6	9.4	957	270	-1.19	-29.7	6.1	996	270	-1.45	-36.3	24.1
919	320	-1.90	-43.6	6.6	958	270	1.39	-27.8	34.9	997	310	-1.43	-32.9	31.1
920	300	-2.21	-50.8	10.1	959	250	-2.56	-64.1	9.4	998	320	-1.39	-32.1	28.8
921	10	-2.07	-46.5	16.7	960	260	-1.81	-45.3	12.5	999	320	-1.40	-32.3	29.2
922	0	-1.76	-39.6	16.5	961	290	-1.41	-35.2	17.4	1000	310	-1.32	-30.5	26.2
923	0	-1.14	-25.7	15.8	962	150	-1.47	-32.4	16.4	1001	350	1.22	-18.1	27.5
924	20	1.14	-24.1	25.6	963	120	-1.70	-37.5	12.9	1002	20	1.09	-21.7	24.6
925	0	-1.93	-43.3	31.0	964	130	-2.36	-51.9	18.9	1003	300	-1.98	-45.6	22.2
926	20	-1.90	-42.8	18.4	965	320	-1.34	30.7	30.0	1004	280	-.57	-14.2	10.5
927	0	-1.65	-37.1	29.6	966	260	-1.29	-32.1	6.8	1005	150	-1.22	-26.8	8.6
928	290	-2.35	-58.7	16.7	967	320	-1.67	-38.3	34.9	1006	270	-.50	-12.4	10.4
929	320	-1.93	-44.4	13.8	968	260	-2.27	-56.7	20.4	1007	250	-.60	-15.0	10.0
930	350	-1.85	-41.6	10.8	969	250	-2.04	50.9	9.4	1008	270	-.55	-13.7	11.1
931	20	-1.89	-42.6	16.1	970	300	-1.73	-39.9	13.4	1009	290	1.04	-19.7	26.1
932	0	-1.81	-40.6	13.1	971	260	-1.51	-37.7	12.1	1010	330	-1.14	-26.3	20.1
933	50	-2.10	-35.7	12.1	972	130	-1.74	-38.4	25.0	1011	290	1.06	-17.4	26.6
934	20	-1.87	-42.0	21.6	973	120	-2.04	-44.8	28.2	1012	230	-1.20	-24.4	22.8
935	350	-1.61	-36.3	6.8	974	250	-1.75	-43.8	25.6	1013	310	1.10	-24.1	25.2
936	290	1.59	-35.6	39.7	975	210	-1.65	-33.5	32.8	1014	280	-.89	-22.3	21.5
937	300	-2.76	-63.5	8.2	976	170	-2.09	-36.6	24.0	1015	150	-1.17	-25.6	22.1
938	290	-1.77	-44.3	9.0	977	280	-1.58	39.4	29.2	1016	230	-1.14	-23.1	20.3
939	280	-1.60	-40.1	11.7	978	0	-1.27	-28.5	27.5	1017	260	-1.20	-30.1	17.5
940	10	-1.61	-36.2	19.2	979	280	-1.72	-42.9	22.4	1018	320	-1.27	-29.3	20.4
941	350	-1.58	-35.5	11.4	980	200	-2.09	-36.6	14.3	1019	330	-1.38	-31.8	21.1
942	50	-2.17	-36.9	8.8	981	210	-2.37	-48.0	8.3	1020	330	-1.61	-37.0	20.8
943	10	-1.57	-35.3	24.0	982	260	-2.07	-51.9	8.2					

TABLE 6A. PEAK LOADS FOR CONFIGURATION W :
LARGEST VALUES OF CLADDING LOAD

REFERENCE PRESSURE = 25.0 PSF

* * 15 GREATEST PRESSURE MAGNITUDES * *

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----
544	320	-2.81	-64.7	32.2
959	250	2.56	-64.1	9.4
937	300	-2.76	-63.5	0.2
150	250	-2.48	-62.0	34.4
917	350	-2.70	-60.7	19.8
928	290	-2.35	-58.7	16.7
144	120	2.65	-58.3	27.3
149	300	-2.53	58.2	28.7
968	260	-2.27	-56.7	20.4
750	330	-2.45	-56.3	24.3
508	120	-2.46	54.2	25.2
344	20	-2.40	-54.0	30.2
545	270	-2.16	-53.9	26.4
350	150	-2.42	-53.2	35.2
196	310	2.30	-52.8	23.9

TABLE 6D. COMPARISON OF CONFIGURATIONS A AND B :
TAPS WHERE NEGATIVE PEAK LOAD FOR CONFIG. B EXCEEDED THAT FOR CONFIG. A BY 2.0 PSF
REF. PRESSURE = 25.0 PSF

TAP	AZIMUTH	A CONFIG. PSF LOAD	AZIMUTH	B CONFIG. PSF LOAD
103	290	-34.4	290	37.3
108	290	-37.0	290	39.3
115	280	-42.5	290	40.7
116	290	-35.0	280	41.7
121	290	-32.7	280	33.0
122	290	-32.7	280	36.2
123	300	-35.3	290	37.9
125	290	-21.3	260	24.8
127	290	-26.4	290	28.0
140	280	-27.1	280	29.1
144	120	-35.3	120	56.9
146	290	-27.4	310	32.3
147	290	-30.4	290	33.9
152	120	-21.9	120	39.5
153	330	-31.1	340	32.3
156	280	-28.4	280	33.3
157	290	-30.1	290	32.2
159	300	-40.3	280	51.3
163	330	-24.5	290	30.3
164	350	-28.7	330	31.7
165	310	-32.1	310	35.2
167	290	-28.2	120	33.4
168	280	-34.2	280	36.5
169	290	-35.9	300	40.7
175	310	-28.1	320	32.6
179	290	-32.1	280	35.6
180	280	-38.1	290	41.7
184	330	-26.5	310	33.7
189	290	-32.7	290	36.5
194	330	-27.0	120	32.8
196	340	-31.9	310	52.0
197	150	-24.1	130	28.3
204	330	-27.5	310	36.5
205	250	-24.6	270	29.8
209	330	-22.3	10	29.5
210	260	-26.9	130	33.3
211	290	-30.8	300	37.1
213	120	-26.8	120	30.0
215	340	-21.9	150	24.7
216	90	-26.1	130	29.0
223	320	-23.7	320	25.8
224	130	-19.7	130	26.3
225	240	-18.5	130	21.1
233	330	-18.9	280	21.1
234	330	-22.7	320	25.9
235	180	-11.6	150	14.0
240	240	-15.4	150	22.0
301	0	-30.4	10	37.0

TABLE 6B. COMPARISON OF CONFIGURATIONS A AND B :
TAPS WHERE NEGATIVE PEAK LOAD FOR CONFIG. B EXCEEDED THAT FOR CONFIG. A BY 2.0 PSF
REF. PRESSURE = 25.0 PSF

TAP	AZIMUTH	A CONFIG. PSF LOAD	AZIMUTH	B CONFIG. PSF LOAD
302	0	-30.0	0	34.9
304	10	-41.0	340	43.8
305	350	-31.1	0	34.0
306	0	-34.0	10	36.5
307	0	-26.9	10	29.4
308	150	-28.4	10	32.3
310	270	-34.5	10	36.9
311	0	-39.3	0	49.2
312	10	-32.3	250	36.8
315	210	-33.9	200	35.9
317	0	-29.4	0	32.2
319	350	-26.3	10	30.8
320	0	-24.0	0	28.0
321	200	-23.8	20	29.2
324	0	-35.7	10	43.6
325	0	-28.1	10	30.3
326	0	-30.1	10	33.4
332	0	-32.8	350	34.9
333	350	-31.4	0	33.7
334	10	-25.3	0	28.7
337	300	-29.7	310	30.4
339	0	-41.3	0	43.4
341	210	-24.5	190	29.6
342	210	-30.1	200	33.6
345	350	-47.9	0	50.4
347	10	-26.1	10	33.6
350	270	-24.9	150	53.8
351	0	-24.4	10	27.3
355	0	-30.3	0	37.8
356	0	-30.0	350	33.0
357	0	-26.4	10	30.0
358	350	-25.4	10	30.8
360	310	-32.3	320	33.8
361	300	-29.4	310	36.7
366	350	-29.3	0	37.3
367	0	-29.5	0	32.0
368	350	-24.9	0	31.7
369	10	-29.7	10	31.0
371	300	-27.5	290	29.7
372	310	-27.4	150	33.7
376	350	-31.3	0	37.0
377	0	-27.7	0	32.2
378	0	-27.4	0	35.3
379	190	-27.5	0	32.2
380	210	-28.5	190	34.2
383	310	-26.0	310	29.3
385	250	-32.0	250	35.2
387	340	-35.5	10	37.8

TABLE 6B. COMPARISON OF CONFIGURATIONS A AND B :
TAPS WHERE NEGATIVE PEAK LOAD FOR CONFIG. B EXCEEDED THAT FOR CONFIG. A BY 2.0 PSF
REF. PRESSURE = 25.0 PSF

TAP	AZIMUTH	A CONFIG. PSF LOAD	AZIMUTH	B CONFIG. PSF LOAD
389	210	-26.5	190	29.5
393	330	-27.2	310	34.4
398	0	-28.5	10	34.1
400	210	-27.4	150	38.0
401	330	-36.9	310	45.0
406	210	-21.2	10	25.1
407	210	-22.0	150	26.4
408	320	-27.1	270	31.0
410	50	-25.5	150	29.6
411	200	-22.0	190	24.7
412	290	-23.9	270	35.4
419	320	-23.6	330	31.3
420	150	-21.7	150	33.2
423	350	-25.4	0	37.6
424	20	-20.3	0	23.9
425	150	-22.0	150	33.7
427	200	-19.4	150	34.5
428	290	-27.8	310	35.4
429	20	-21.4	140	25.6
430	20	-22.2	10	26.8
434	10	-23.7	130	28.1
436	150	-15.4	130	19.9
437	160	-16.1	150	21.7
438	200	-18.9	150	27.9
440	290	-27.2	10	30.8
444	30	-12.9	140	15.6
504	280	-42.9	290	46.2
505	280	-28.4	280	34.5
506	290	-26.4	280	30.8
511	270	-45.6	260	52.5
517	270	-26.8	260	34.5
519	290	-25.6	270	32.9
520	280	-25.5	280	29.4
526	270	-29.7	280	32.0
528	290	-24.3	280	26.8
532	280	-36.0	260	38.6
539	280	-39.3	270	45.6
540	280	-33.8	280	37.5
542	300	-25.8	120	31.5
545	290	-45.5	270	53.9
546	300	-32.6	270	34.7
547	120	-23.6	280	26.1
549	350	-25.0	120	44.8
550	20	-37.4	60	40.3
551	300	-23.7	280	32.3
552	300	-32.6	300	39.8
554	320	-25.8	150	29.0
555	280	-28.7	280	38.2

TABLE 6B. COMPARISON OF CONFIGURATIONS A AND B :
TAPS WHERE NEGATIVE PEAK LOAD FOR CONFIG. B EXCEEDED THAT FOR CONFIG. A BY 2.0 PSF
REF. PRESSURE = 25.0 PSF

TAP	AZIMUTH	A CONFIG. PSF LOAD	AZIMUTH	B CONFIG. PSF LOAD
557	290	-25.7	270	37.6
558	150	-27.7	290	-31.4
559	290	-26.3	300	-29.4
569	290	-24.7	290	-45.9
575	320	-25.7	320	-33.1
576	280	-31.4	270	-39.6
577	280	-27.8	270	36.0
580	320	-28.5	320	-37.1
588	310	-29.6	280	34.4
589	270	-26.0	260	-29.5
590	320	-27.1	310	33.5
596	320	-28.4	320	-34.7
597	320	-34.6	270	-40.6
600	320	-33.5	330	35.7
607	320	-31.1	320	-34.9
610	320	-23.8	270	32.0
611	320	-26.1	320	-38.0
614	300	-31.2	320	-36.9
616	320	-30.6	330	39.0
617	20	-28.8	320	-31.4
621	320	-25.6	310	32.6
622	320	-28.3	310	35.1
623	320	-23.6	320	30.0
624	20	-21.4	320	-37.5
626	50	-21.1	10	28.0
627	330	-26.2	320	-32.6
629	130	-21.0	330	25.7
630	320	-24.4	310	31.1
631	320	-24.4	320	-32.9
632	320	-23.6	310	30.1
634	310	-23.7	200	29.5
635	320	-25.7	330	39.1
637	320	-24.3	320	46.6
638	330	-21.9	330	-27.3
639	320	-26.0	320	-36.3
703	0	-30.0	20	-37.1
707	0	-28.0	10	-33.1
708	250	-33.2	20	-38.4
714	10	-30.0	20	33.0
715	20	-38.8	10	46.1
722	10	-29.5	10	36.7
723	0	-27.7	20	29.8
727	300	-23.6	190	-26.3
728	10	-27.5	10	31.4
736	150	-32.6	20	36.3
739	300	-32.6	170	-35.0
741	0	25.6	20	31.7
742	10	-35.0	20	38.8

TABLE 6B. COMPARISON OF CONFIGURATIONS A AND B :
TAPS WHERE NEGATIVE PEAK LOAD FOR CONFIG. B EXCEEDED THAT FOR CONFIG. A BY 2.0 PSF
REF. PRESSURE = 25.0 PSF

TAP	AZIMUTH	A CONFIG. PSF LOAD	AZIMUTH	B CONFIG. PSF LOAD
743	0	-25.9	10	-28.1
745	0	-32.5	100	-36.4
748	150	-24.7	10	-34.2
749	130	-31.4	20	-46.6
750	330	-55.7	330	-63.9
751	260	-22.6	20	-27.9
755	350	-26.0	350	-34.1
756	170	-26.4	20	-29.8
757	0	-23.2	20	-30.7
758	10	-24.3	10	-34.9
759	150	-29.6	10	-36.1
760	340	-28.9	130	-37.0
766	340	-24.0	340	-38.2
767	0	-23.4	340	-30.5
768	350	-26.8	20	-33.7
769	150	-27.1	10	-32.9
770	340	-25.4	130	-30.1
776	260	-24.0	350	-37.2
777	250	-30.3	270	-43.8
778	0	-25.3	20	-30.5
780	10	-30.2	20	-35.4
781	350	-25.4	130	-28.5
785	250	-29.7	230	-40.6
787	250	-24.3	310	-40.7
790	0	-30.5	10	-39.5
791	340	-27.6	320	-30.5
799	0	-31.4	340	-34.7
800	350	-34.3	10	-40.2
802	330	-32.1	130	-38.0
803	350	-33.6	310	-38.2
804	150	-21.1	120	-28.7
805	320	-24.0	330	-29.1
806	320	-23.9	310	-28.0
807	240	-24.2	220	-34.5
808	250	-23.9	120	-26.3
809	40	-24.9	320	-33.7
810	270	-23.4	330	-28.1
812	260	-24.5	130	-31.5
814	230	-27.7	310	-34.2
817	10	-30.9	10	-34.7
821	220	-21.0	0	-26.0
823	230	-25.8	300	-30.8
825	330	-26.9	320	-35.3
826	320	-25.8	310	-35.3
827	330	-24.2	330	-32.5
828	330	-18.0	190	-23.5
832	320	-23.9	350	-32.0
834	130	-26.7	310	-29.0

TABLE 6B. COMPARISON OF CONFIGURATIONS A AND B :
TAPS WHERE NEGATIVE PEAK LOAD FOR CONFIG. B EXCEEDED THAT FOR CONFIG. A BY 2.0 PSF
REF. PRESSURE = 25.0 PSF

TAP	AZIMUTH	A CONFIG. PSF LOAD	AZIMUTH	B CONFIG. PSF LOAD
835	240	-20.9	320	-25.0
836	250	-21.5	320	-23.9
837	250	-20.5	230	-25.2
839	340	-30.5	300	-33.2
903	280	-33.8	130	-36.7
911	280	-28.2	290	-31.8
919	20	-40.7	320	-43.6
923	10	-23.2	0	-25.7
926	20	-35.2	20	-42.8
927	0	-32.5	0	-37.1
931	20	-40.2	20	-42.6
934	10	-36.7	20	-42.0
940	20	-34.2	10	-36.2
943	140	-30.7	10	-35.3
946	0	-25.1	10	-27.9
954	0	-24.2	20	-27.2
955	10	-22.4	20	-27.0
956	270	-29.5	310	-36.2
962	120	-28.5	150	-32.4
964	120	-35.6	130	-51.2
968	250	-53.5	260	-56.7
971	250	-30.1	260	-37.7
972	210	-33.3	130	-38.4
973	120	-34.7	120	-44.0
976	300	-32.4	170	-36.6
979	290	-37.5	200	-42.9
983	260	-42.4	150	-45.6
984	190	-37.1	150	43.0
988	280	-24.3	270	29.4
989	280	-25.8	270	28.3
991	290	-26.1	270	-28.8
992	290	-34.6	270	-40.6
993	310	-31.2	120	-34.9
994	320	-24.0	280	-29.2
996	140	-28.4	270	-36.3
997	300	-30.2	310	-32.9
999	60	-23.4	320	32.3
1000	170	-27.7	310	-30.5
1005	340	21.5	150	26.0
1010	330	-24.2	330	-26.3
1012	320	-20.6	230	-24.4
1015	150	-20.8	150	25.6
1017	310	-22.3	260	-30.1
1018	320	-24.5	320	-29.3
1019	320	-28.1	330	-31.8
1020	330	-26.9	330	-37.0

TABLE 7. LPC MANDALAY LAS COLINAS,TEXAS

PROJECT 6600 CONFIGURATION A

SCALE = 400 REF. PRESSURE = 25.0

GUST FACTOR = 1.32 STANDARD FLOOR HEIGHT = 12.50

NUMBER OF SIDES = 4 NO. OF FLOORS = 28

SIDE	ANGLE	Z-AXIS	SHFACT
1	0.0	2.330	1.0
2	90.0	2.330	1.0
3	180.0	2.330	1.0
4	270.0	2.330	1.0

FLOOR #	LABEL	HEIGHT-FT	WIND AZIMUTH	LOAD FACTOR
1	GRND	26.00	0	.90
2	2ND	12.50	10	.90
3	3RD	12.50	20	.90
4	4TH	12.50	30	.68
5	5TH	12.50	40	.68
6	6TH	12.50	50	.68
7	7TH	12.50	60	.68
8	8TH	12.50	70	.55
9	9TH	12.50	80	.55
10	10TH	12.50	90	.55
11	11TH	12.50	100	.55
12	12TH	12.50	110	.55
13	13TH	12.50	120	.88
14	14TH	12.50	130	.88
15	15TH	12.50	140	.88
16	16TH	12.50	150	.88
17	17TH	12.50	160	.70
18	18TH	12.50	170	.70
19	19TH	12.50	180	.70
20	20TH	12.50	190	.70
21	21ST	16.00	200	.70
22	22ND	12.50	210	.81
23	23RD	16.00	220	.81
24	24TH	12.50	230	.81
25	25TH	16.00	240	.81
26	26TH	12.50	250	1.00
27	27TH	12.50	260	1.00
28	EAVE	18.00	270	1.00
			280	1.00
			290	1.00
			300	.92
			310	.92
			320	.92
			330	.92
			340	.90
			350	.90

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS

WIND DIRECTION 0 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-928.1	120.9	-9.1	-179.1	.3
		-41.8	33.9	4039	4039	-10.4	8.4	-2	-3					
2ND	26.00									-806.3	87.0	-6.4	-155.5	.5
		-26.2	14.6	1942	1942	-13.5	7.5	-0	-0					
3RD	38.50									-860.1	72.4	-5.5	-144.6	.5
		-30.5	13.9	1942	1942	-15.7	7.1	0	1					
4TH	51.00									-829.6	58.5	-4.6	-134.0	.5
		-30.7	8.0	1942	1942	-15.8	4.1	-1	-5					
5TH	63.50									-799.0	50.5	-4.0	-123.8	.6
		-21.0	10.1	1942	1942	-10.8	5.2	-0	-1					
6TH	76.00									-777.9	40.4	-3.4	-114.0	.6
		-28.2	7.0	1843	1843	-15.3	3.8	-1	-2					
7TH	88.50									-749.7	33.5	-2.9	-104.4	.7
		-30.4	5.1	1817	1817	-16.8	2.8	-0	-2					
8TH	101.00									-719.3	28.4	-2.5	-95.3	.8
		-30.9	3.8	1817	1817	-17.0	2.1	-0	-2					
9TH	113.50									-688.3	24.6	-2.2	-86.5	.8
		-31.5	2.4	1817	1817	-17.3	1.3	-0	-1					
10TH	126.00									-656.9	22.2	-1.9	-78.1	.8
		-32.3	1.9	1817	1817	-17.8	1.1	-0	-1					
11TH	138.50									-624.6	20.2	-1.6	-70.0	.9
		-33.3	1.8	1817	1817	-18.3	1.0	-0	-1					
12TH	151.00									-591.3	18.4	-1.4	-62.4	.9
		-34.2	1.7	1817	1817	-18.8	.9	-0	-0					
13TH	163.50									-557.1	16.7	-1.2	-55.3	.9
		-34.8	1.6	1817	1817	-19.1	.9	-0	-0					
14TH	176.00									-522.3	15.1	-1.0	-48.5	.9
		-35.0	1.5	1817	1817	-19.3	.8	-0	-0					
15TH	188.50									-487.3	13.6	-.8	-42.2	.9
		-35.2	1.4	1817	1817	-19.4	.8	0	0					
16TH	201.00									-452.0	12.2	-.6	-36.3	.9
		-35.5	1.5	1817	1817	-19.5	.8	0	0					
17TH	213.50									-416.5	10.7	-.5	-30.9	.9
		-35.8	1.6	1817	1817	-19.7	.9	0	1					
18TH	226.00									-380.8	9.1	-.4	-25.9	.9
		-36.0	1.8	1817	1817	-19.8	1.0	0	2					
19TH	238.50									-344.8	7.3	-.3	-21.4	.8
		-37.0	1.8	1817	1817	-20.3	1.0	0	2					
20TH	251.00									-307.8	5.6	-.2	-17.3	.7
		-39.4	1.3	1817	1817	-21.7	.7	0	1					
21ST	263.50									-268.4	4.3	-.1	-13.7	.7
		-53.2	1.0	2325	2325	-22.9	.4	0	0					
22ND	279.50									-215.3	3.2	-.1	-9.8	.7
		-30.8	1.5	1570	1570	-19.6	1.0	0	5					
23RD	292.00									-184.5	1.7	-.0	-7.3	.5
		-44.2	.6	2005	2005	-22.0	.3	0	2					
24TH	308.00									-140.3	1.1	-.0	-4.7	.4
		-25.0	.1	1317	1317	-19.0	.1	0	2					
25TH	320.50									-115.3	1.0	-.0	-3.2	.4
		-38.0	1.2	1685	1685	-22.6	.7	0	2					
26TH	336.50									-77.2	-.1	-.0	-1.6	.3
		-23.4	-.3	1276	1276	-18.4	-.2	-0	5					
27TH	349.00									-53.8	.2	.0	-.8	.2
		-23.9	.2	1275	1275	-18.8	.2	0	5					
EAVE	361.50									-29.9	-.1	.0	-.3	.1
		-29.9	-.1	1182	1182	-25.3	-.1	-0	2					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 10 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-1036.8	309.3	-41.9	-200.9	-4.4
		-46.6	45.9	4039	4039	-11.5	11.4	-4	-4					
2ND	26.00									-990.2	263.4	-34.4	-174.6	-4.0
		-28.6	21.1	1942	1942	-14.7	10.9	-2	-2					
3RD	38.50									-961.6	242.3	-31.3	-162.4	-3.9
		-32.8	20.2	1942	1942	-16.9	10.4	-0	-1					
4TH	51.00									-928.7	222.1	-28.4	-150.6	-3.9
		-33.3	17.0	1942	1942	-17.2	8.7	-1	-1					
5TH	63.50									-895.4	205.1	-25.7	-139.2	-3.8
		-24.2	16.4	1942	1942	-12.5	8.4	1	2					
6TH	76.00									-871.2	188.7	-23.2	-128.1	-3.9
		-32.1	14.5	1843	1843	-17.4	7.9	-1	-3					
7TH	88.50									-839.1	174.2	-21.0	-117.4	-3.8
		-34.3	12.9	1817	1817	-18.9	7.1	-2	-4					
8TH	101.00									-804.8	161.3	-18.9	-107.2	-3.6
		-34.9	11.7	1817	1817	-19.2	6.4	-1	-4					
9TH	113.50									-770.0	149.6	-16.9	-97.3	-3.4
		-35.4	10.5	1817	1817	-19.5	5.8	-1	-4					
10TH	126.00									-734.6	139.1	-15.1	-87.9	-3.3
		-35.9	9.7	1817	1817	-19.8	5.4	-1	-4					
11TH	138.50									-698.7	129.4	-13.4	-79.0	-3.1
		-36.4	9.2	1817	1817	-20.0	5.1	-1	-4					
12TH	151.00									-662.3	120.2	-11.9	-70.5	-2.9
		-36.9	8.6	1817	1817	-20.3	4.8	-1	-4					
13TH	163.50									-625.4	111.5	-10.4	-62.4	-2.8
		-37.5	8.1	1817	1817	-20.6	4.5	-1	-4					
14TH	176.00									-587.9	103.4	-9.1	-54.8	-2.6
		-38.1	7.6	1817	1817	-21.0	4.2	-1	-4					
15TH	188.50									-549.7	95.8	-7.8	-47.7	-2.4
		-38.8	7.0	1817	1817	-21.3	3.9	-1	-4					
16TH	201.00									-511.0	88.8	-6.7	-41.1	-2.3
		-39.4	6.8	1817	1817	-21.7	3.8	-1	-4					
17TH	213.50									-471.5	82.0	-5.6	-34.9	-2.1
		-40.1	7.2	1817	1817	-22.1	3.9	-1	-4					
18TH	226.00									-431.5	74.8	-4.6	-29.3	-1.9
		-40.7	7.5	1817	1817	-22.4	4.1	-1	-4					
19TH	238.50									-390.8	67.3	-3.7	-24.2	-1.7
		-41.8	7.9	1817	1817	-23.0	4.3	-1	-5					
20TH	251.00									-349.0	59.5	-3.0	-19.5	-1.5
		-44.4	8.7	1817	1817	-24.4	4.8	-1	-5					
21ST	263.50									-304.6	50.8	-2.3	-15.5	-1.3
		-60.7	12.4	2325	2325	-26.1	5.3	-1	-6					
22ND	279.50									-243.9	38.4	-1.6	-11.1	-.9
		-35.8	7.2	1570	1570	-22.8	4.6	-1	-5					
23RD	292.00									-208.1	31.2	-1.1	-8.2	-.7
		-50.2	10.1	2005	2005	-25.1	5.0	-1	-4					
24TH	308.00									-157.8	21.1	-.7	-5.3	-.6
		-28.7	3.9	1317	1317	-21.8	2.9	-1	-6					
25TH	320.50									-129.2	17.3	-.5	-3.5	-.4
		-42.3	6.2	1685	1685	-25.1	3.7	-1	-4					
26TH	336.50									-86.8	11.1	-.2	-1.8	-.2
		-26.9	4.0	1276	1276	-21.1	3.2	-1	-4					
27TH	349.00									-60.0	7.1	-.1	-.9	-.1
		-27.0	2.3	1275	1275	-21.2	1.8	-0	-2					
EAVE	361.50									-33.0	4.8	-.0	-.3	-.0
		-33.0	4.8	1182	1182	-27.9	4.0	-0	-1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 20 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-1052.3	610.5	-96.3	-204.2	-5.2
		-48.2	61.0	4039	4039	-11.9	15.1	-4	-3					
2ND	26.00									-1004.1	549.4	-81.2	-177.5	-4.8
		-28.4	29.1	1942	1942	-14.6	15.0	-3	-3					
3RD	38.50									-975.7	520.3	-74.5	-165.1	-4.6
		-32.1	28.7	1942	1942	-16.5	14.8	-1	-2					
4TH	51.00									-943.6	491.6	-68.2	-153.1	-4.5
		-34.1	30.0	1942	1942	-17.6	15.4	-0	-0					
5TH	63.50									-909.5	461.6	-62.2	-141.6	-4.5
		-26.4	26.2	1942	1942	-13.6	13.5	2	2					
6TH	76.00									-883.1	435.5	-56.6	-130.4	-4.7
		-32.3	24.9	1843	1843	-17.5	13.5	-2	-2					
7TH	88.50									-850.7	410.6	-51.3	-119.5	-4.5
		-34.0	24.0	1817	1817	-18.7	13.2	-2	-3					
8TH	101.00									-816.8	386.5	-46.3	-109.1	-4.4
		-34.4	23.4	1817	1817	-18.9	12.9	-2	-3					
9TH	113.50									-782.4	363.2	-41.7	-99.1	-4.2
		-34.8	22.7	1817	1817	-19.2	12.5	-2	-3					
10TH	126.00									-747.6	340.5	-37.3	-89.5	-4.0
		-35.6	21.9	1817	1817	-19.6	12.0	-2	-4					
11TH	138.50									-711.9	318.7	-33.1	-80.4	-3.9
		-36.7	21.1	1817	1817	-20.2	11.6	-2	-4					
12TH	151.00									-675.3	297.6	-29.3	-71.8	-3.7
		-37.7	20.2	1817	1817	-20.7	11.1	-2	-4					
13TH	163.50									-637.6	277.4	-25.7	-63.5	-3.4
		-38.3	19.7	1817	1817	-21.1	10.8	-2	-5					
14TH	176.00									-599.3	257.7	-22.3	-55.8	-3.2
		-38.7	19.3	1817	1817	-21.3	10.6	-2	-5					
15TH	188.50									-560.6	238.5	-19.2	-48.6	-3.0
		-39.0	18.9	1817	1817	-21.5	10.4	-2	-5					
16TH	201.00									-521.6	219.6	-16.4	-41.8	-2.8
		-39.6	18.7	1817	1817	-21.8	10.3	-2	-4					
17TH	213.50									-482.0	200.8	-13.8	-35.5	-2.6
		-40.5	19.0	1817	1817	-22.3	10.4	-2	-4					
18TH	226.00									-441.5	181.9	-11.4	-29.8	-2.4
		-41.4	19.2	1817	1817	-22.8	10.6	-2	-4					
19TH	238.50									-400.1	162.6	-9.2	-24.5	-2.2
		-42.8	19.8	1817	1817	-23.6	10.9	-2	-4					
20TH	251.00									-357.3	142.9	-7.3	-19.8	-2.0
		-45.7	21.1	1817	1817	-25.1	11.6	-2	-4					
21ST	263.50									-311.6	121.8	-5.6	-15.6	-1.8
		-62.4	28.7	2325	2325	-26.8	12.4	-2	-4					
22ND	279.50									-249.3	93.1	-3.9	-11.1	-1.5
		-37.8	15.8	1570	1570	-24.1	10.0	-3	-7					
23RD	292.00									-211.4	77.3	-2.9	-8.2	-1.2
		-52.1	21.6	2005	2005	-26.0	10.8	-2	-5					
24TH	308.00									-159.4	55.7	-1.8	-5.3	-.8
		-30.6	11.4	1317	1317	-23.2	8.6	-2	-5					
25TH	320.50									-128.8	44.4	-1.2	-3.5	-.7
		-43.6	14.8	1685	1685	-25.9	8.8	-2	-5					
26TH	336.50									-85.2	29.6	-.6	-1.7	-.4
		-27.4	11.1	1276	1276	-21.5	8.7	-2	-5					
27TH	349.00									-57.8	18.5	-.3	-.8	-.2
		-26.0	7.8	1275	1275	-20.4	6.1	-2	-5					
EAVE	361.50									-31.8	10.7	-.1	-.3	-.1
		-31.8	10.7	1182	1182	-26.9	9.1	-1	-2					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 30 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
BRND	0.00									-750.4	644.0	-108.0	-145.6	-2.7
		-36.6	54.5	4039	4039	-9.1	13.5	-4	-3					
2ND	26.00									-713.8	589.5	-91.9	-126.6	-2.4
		-22.6	26.4	1942	1942	-11.6	13.6	-1	-1					
3RD	38.50									-691.3	563.1	-84.7	-117.8	-2.3
		-23.5	26.0	1942	1942	-12.1	13.4	-1	-1					
4TH	51.00									-667.8	537.0	-77.8	-109.3	-2.3
		-24.5	28.1	1942	1942	-12.6	14.5	-0	-0					
5TH	63.50									-643.3	509.0	-71.3	-101.1	-2.2
		-19.5	25.3	1942	1942	-10.1	13.0	3	2					
6TH	76.00									-623.8	483.7	-65.1	-93.2	-2.4
		-22.8	25.0	1843	1843	-12.4	13.5	-1	-1					
7TH	88.50									-601.0	458.7	-59.2	-85.5	-2.3
		-23.8	24.4	1817	1817	-13.1	13.4	-1	-1					
8TH	101.00									-577.2	434.3	-53.6	-78.2	-2.3
		-24.0	23.9	1817	1817	-13.2	13.1	-1	-1					
9TH	113.50									-553.2	410.4	-48.4	-71.1	-2.2
		-24.3	23.4	1817	1817	-13.4	12.9	-1	-1					
10TH	126.00									-528.9	387.0	-43.4	-64.3	-2.2
		-24.7	23.0	1817	1817	-13.6	12.7	-1	-1					
11TH	138.50									-504.2	364.1	-38.7	-57.9	-2.1
		-25.2	22.6	1817	1817	-13.9	12.4	-2	-2					
12TH	151.00									-479.0	341.5	-34.3	-51.7	-2.0
		-25.8	22.2	1817	1817	-14.2	12.2	-2	-2					
13TH	163.50									-453.2	319.3	-30.1	-45.9	-1.9
		-26.1	21.9	1817	1817	-14.4	12.0	-2	-2					
14TH	176.00									-427.1	297.4	-26.3	-40.4	-1.8
		-26.3	21.7	1817	1817	-14.5	11.9	-2	-2					
15TH	188.50									-400.7	275.7	-22.7	-35.2	-1.7
		-26.6	21.5	1817	1817	-14.6	11.8	-2	-3					
16TH	201.00									-374.1	254.3	-19.4	-30.4	-1.6
		-27.1	21.4	1817	1817	-14.9	11.8	-2	-3					
17TH	213.50									-347.1	232.8	-16.3	-25.9	-1.5
		-28.0	21.7	1817	1817	-15.4	11.9	-2	-2					
18TH	226.00									-319.1	211.2	-13.6	-21.7	-1.4
		-28.9	21.9	1817	1817	-15.9	12.0	-2	-2					
19TH	238.50									-290.2	189.3	-11.1	-17.9	-1.2
		-30.1	22.4	1817	1817	-16.6	12.3	-2	-2					
20TH	251.00									-260.1	166.9	-8.8	-14.5	-1.1
		-32.3	23.5	1817	1817	-17.8	12.9	-2	-3					
21ST	263.50									-227.8	143.4	-6.9	-11.4	-1.0
		-44.3	31.6	2325	2325	-19.0	13.6	-2	-3					
22ND	279.50									-183.5	111.9	-4.9	-8.1	-.8
		-28.0	17.9	1570	1570	-17.9	11.4	-3	-4					
23RD	292.00									-155.5	94.0	-3.6	-6.0	-.6
		-38.4	23.9	2005	2005	-19.1	11.9	-3	-4					
24TH	308.00									-117.1	70.1	-2.3	-3.8	-.4
		-22.8	14.5	1317	1317	-17.3	11.0	-2	-4					
25TH	320.50									-94.3	55.6	-1.5	-2.5	-.3
		-32.1	18.8	1685	1685	-19.1	11.1	-2	-4					
26TH	336.50									-62.2	36.8	-.7	-1.2	-.1
		-20.9	13.1	1276	1276	-16.4	10.3	-1	-1					
27TH	349.00									-41.3	23.6	-.4	-.6	-.1
		-18.7	10.0	1275	1275	-14.7	7.9	-2	-3					
EAVE	361.50									-22.6	13.6	-.1	-.2	-.0
		-22.6	13.6	1182	1182	-19.1	11.5	-1	-1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 40 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-730.2	732.1	-126.5	-142.0	-2.3
		-37.8	59.8	4039	4039	-9.4	14.8	-5	-3					
2ND	26.00									-692.4	672.3	-108.2	-123.5	-1.9
		-21.0	29.7	1942	1942	-10.8	15.3	-4	-3					
3RD	38.50									-671.4	642.6	-100.0	-115.0	-1.7
		-22.5	29.6	1942	1942	-11.6	15.2	-3	-2					
4TH	51.00									-648.8	613.0	-92.2	-106.7	-1.5
		-23.4	30.2	1942	1942	-12.0	15.6	-1	-1					
5TH	63.50									-625.5	582.8	-84.7	-98.7	-1.5
		-18.6	26.7	1942	1942	-9.6	13.8	2	1					
6TH	76.00									-606.9	556.0	-77.6	-91.0	-1.6
		-21.6	26.4	1843	1843	-11.7	14.3	-1	-1					
7TH	88.50									-585.2	529.7	-70.8	-83.6	-1.5
		-22.6	25.8	1817	1817	-12.4	14.2	-1	-1					
8TH	101.00									-562.6	503.8	-64.3	-76.4	-1.5
		-22.9	25.3	1817	1817	-12.6	13.9	-1	-1					
9TH	113.50									-539.7	478.5	-58.2	-69.5	-1.5
		-23.2	24.8	1817	1817	-12.8	13.6	-1	-0					
10TH	126.00									-516.5	453.7	-52.4	-62.9	-1.4
		-23.8	24.6	1817	1817	-13.1	13.5	-1	-1					
11TH	138.50									-492.8	429.2	-46.9	-56.6	-1.4
		-24.4	24.5	1817	1817	-13.4	13.5	-1	-1					
12TH	151.00									-468.4	404.6	-41.6	-50.6	-1.4
		-25.0	24.5	1817	1817	-13.8	13.5	-1	-1					
13TH	163.50									-443.4	380.2	-36.7	-44.9	-1.3
		-25.6	24.6	1817	1817	-14.1	13.5	-1	-1					
14TH	176.00									-417.8	355.6	-32.1	-39.5	-1.3
		-26.0	24.8	1817	1817	-14.3	13.7	-1	-1					
15TH	188.50									-391.8	330.8	-27.9	-34.5	-1.2
		-26.5	25.0	1817	1817	-14.6	13.8	-1	-1					
16TH	201.00									-365.3	305.7	-23.9	-29.7	-1.2
		-27.0	25.2	1817	1817	-14.9	13.9	-1	-1					
17TH	213.50									-338.3	280.5	-20.2	-25.3	-1.1
		-27.7	25.2	1817	1817	-15.2	13.9	-1	-1					
18TH	226.00									-310.6	255.3	-16.9	-21.3	-1.0
		-28.3	25.3	1817	1817	-15.6	13.9	-1	-1					
19TH	238.50									-282.3	230.0	-13.8	-17.6	-1.0
		-29.3	25.6	1817	1817	-16.1	14.1	-1	-1					
20TH	251.00									-253.0	204.4	-11.1	-14.2	-.9
		-31.2	26.7	1817	1817	-17.2	14.7	-2	-3					
21ST	263.50									-221.8	177.8	-8.7	-11.3	-.8
		-42.3	35.6	2325	2325	-18.2	15.3	-3	-4					
22ND	279.50									-179.5	142.2	-6.2	-8.1	-.5
		-26.6	22.5	1570	1570	-17.0	14.3	-2	-2					
23RD	292.00									-152.9	119.7	-4.5	-6.0	-.4
		-37.0	30.5	2005	2005	-18.4	15.2	-2	-2					
24TH	308.00									-115.9	89.2	-2.9	-3.8	-.2
		-22.5	18.4	1317	1317	-17.1	14.0	-1	-2					
25TH	320.50									-93.5	70.8	-1.9	-2.5	-.2
		-30.7	24.4	1685	1685	-18.2	14.5	-2	-2					
26TH	336.50									-62.8	46.4	-.9	-1.3	-.1
		-21.1	16.4	1276	1276	-16.5	12.9	-0	-1					
27TH	349.00									-41.7	29.9	-.4	-.6	-.1
		-18.5	13.1	1275	1275	-14.5	10.3	-1	-2					
EAVE	361.50									-23.2	16.8	-.2	-.2	-.0
		-23.2	16.8	1182	1182	-19.6	14.2	-0	-1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 50 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-632.3	768.7	-134.5	-122.5	-.9
		-35.5	61.8	4039	4039	-8.8	15.3	-4	-2					
2ND	26.00									-596.8	706.9	-115.3	-106.5	-.6
		-18.7	31.3	1942	1942	-9.6	16.1	-5	-3					
3RD	38.50									-578.1	675.6	-106.6	-99.2	-.4
		-19.7	31.6	1942	1942	-10.1	16.3	-4	-2					
4TH	51.00									-558.4	644.0	-98.4	-92.1	-.2
		-19.7	29.9	1942	1942	-10.2	15.4	-5	-3					
5TH	63.50									-538.7	614.1	-90.5	-85.2	.0
		-14.8	27.2	1942	1942	-7.6	14.0	-2	-1					
6TH	76.00									-523.8	586.9	-83.0	-78.6	.1
		-17.9	26.7	1843	1843	-9.7	14.5	-1	-1					
7TH	88.50									-505.9	560.1	-75.9	-72.2	.1
		-19.0	26.2	1817	1817	-10.5	14.4	0	0					
8TH	101.00									-486.9	533.9	-69.0	-66.0	.1
		-19.5	25.9	1817	1817	-10.7	14.2	0	0					
9TH	113.50									-467.4	508.0	-62.5	-60.0	.1
		-19.9	25.5	1817	1817	-11.0	14.0	1	1					
10TH	126.00									-447.5	482.5	-56.3	-54.3	.0
		-20.5	25.4	1817	1817	-11.3	14.0	1	1					
11TH	138.50									-427.0	457.1	-50.4	-48.8	-.0
		-21.1	25.5	1817	1817	-11.6	14.1	1	1					
12TH	151.00									-405.9	431.6	-44.9	-43.6	-.0
		-21.6	25.6	1817	1817	-11.9	14.1	1	1					
13TH	163.50									-384.3	405.9	-39.7	-38.7	-.1
		-22.2	25.8	1817	1817	-12.2	14.2	1	1					
14TH	176.00									-362.1	380.1	-34.7	-34.0	-.1
		-22.8	26.1	1817	1817	-12.5	14.3	1	1					
15TH	188.50									-339.3	354.1	-30.2	-29.6	-.2
		-23.3	26.3	1817	1817	-12.8	14.5	1	0					
16TH	201.00									-316.0	327.8	-25.9	-25.5	-.2
		-23.9	26.5	1817	1817	-13.2	14.6	0	0					
17TH	213.50									-292.1	301.3	-22.0	-21.7	-.2
		-24.5	26.6	1817	1817	-13.5	14.6	0	0					
18TH	226.00									-267.6	274.7	-18.4	-18.2	-.2
		-25.1	26.7	1817	1817	-13.8	14.7	0	0					
19TH	238.50									-242.5	248.1	-15.1	-15.0	-.2
		-26.0	27.0	1817	1817	-14.3	14.9	-0	-0					
20TH	251.00									-216.5	221.1	-12.2	-12.2	-.2
		-27.3	27.9	1817	1817	-15.0	15.3	-1	-1					
21ST	263.50									-189.2	193.2	-9.6	-9.6	-.1
		-36.6	36.7	2325	2325	-15.7	15.8	-2	-2					
22ND	279.50									-152.6	156.5	-6.8	-6.9	.0
		-22.4	24.4	1570	1570	-14.3	15.6	1	0					
23RD	292.00									-130.2	132.1	-5.0	-5.1	.0
		-31.3	33.3	2005	2005	-15.6	16.6	-0	-0					
24TH	308.00									-98.9	98.7	-3.1	-3.3	.0
		-18.8	20.8	1317	1317	-14.3	15.8	-0	-0					
25TH	320.50									-80.1	78.0	-2.0	-2.2	.0
		-25.5	27.7	1685	1685	-15.1	16.4	-0	-0					
26TH	336.50									-54.6	50.3	-1.0	-1.1	.0
		-18.1	17.5	1276	1276	-14.2	13.7	0	0					
27TH	349.00									-36.5	32.8	-.5	-.5	.0
		-16.3	14.9	1275	1275	-12.8	11.7	1	1					
EAVE	361.50									-20.2	17.8	-.2	-.2	.0
		-20.2	17.8	1182	1182	-17.1	15.1	0	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 60 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-368.6	683.9	-120.4	-69.8	2.8
		-26.1	54.5	4039	4039	-6.5	13.5	-0	-0					
2ND	26.00									-342.5	629.4	-103.3	-60.6	2.9
		-12.6	27.8	1942	1942	-6.5	14.3	-2	-1					
3RD	38.50									-330.0	601.6	-95.6	-56.4	2.9
		-12.8	28.2	1942	1942	-6.6	14.5	-2	-1					
4TH	51.00									-317.2	573.4	-88.3	-52.4	3.0
		-10.6	25.6	1942	1942	-5.4	13.2	-1	-1					
5TH	63.50									-306.6	547.8	-81.2	-48.5	3.1
		-7.4	22.6	1942	1942	-3.8	11.7	-0	-0					
6TH	76.00									-299.1	525.2	-74.5	-44.7	3.1
		-10.3	22.9	1843	1843	-5.6	12.4	3	1					
7TH	88.50									-288.9	502.3	-68.1	-41.0	3.0
		-10.8	22.9	1817	1817	-6.0	12.6	4	2					
8TH	101.00									-278.0	479.4	-62.0	-37.4	2.9
		-10.9	22.8	1817	1817	-6.0	12.6	5	2					
9TH	113.50									-267.1	456.5	-56.1	-34.0	2.7
		-11.0	22.7	1817	1817	-6.1	12.5	5	2					
10TH	126.00									-256.1	433.8	-50.6	-30.8	2.6
		-11.5	22.8	1817	1817	-6.3	12.5	5	3					
11TH	138.50									-244.6	411.0	-45.3	-27.6	2.5
		-12.2	23.0	1817	1817	-6.7	12.6	5	3					
12TH	151.00									-232.4	388.1	-40.3	-24.7	2.3
		-12.8	23.1	1817	1817	-7.1	12.7	5	3					
13TH	163.50									-219.6	365.0	-35.6	-21.8	2.2
		-13.1	23.3	1817	1817	-7.2	12.8	5	3					
14TH	176.00									-206.5	341.6	-31.2	-19.2	2.0
		-13.2	23.6	1817	1817	-7.3	13.0	5	3					
15TH	188.50									-193.2	318.1	-27.0	-16.7	1.9
		-13.3	23.8	1817	1817	-7.3	13.1	5	3					
16TH	201.00									-179.9	294.3	-23.2	-14.3	1.7
		-13.6	24.0	1817	1817	-7.5	13.2	5	3					
17TH	213.50									-166.3	270.3	-19.7	-12.2	1.6
		-14.3	24.1	1817	1817	-7.8	13.3	5	3					
18TH	226.00									-152.1	246.2	-16.5	-10.2	1.4
		-14.9	24.2	1817	1817	-8.2	13.3	5	3					
19TH	238.50									-137.2	222.0	-13.5	-8.4	1.2
		-15.6	24.5	1817	1817	-8.6	13.5	5	3					
20TH	251.00									-121.6	197.5	-10.9	-6.8	1.0
		-16.3	25.3	1817	1817	-9.0	13.9	4	2					
21ST	263.50									-105.3	172.2	-8.6	-5.3	.9
		-21.6	33.1	2325	2325	-9.3	14.2	2	2					
22ND	279.50									-83.7	139.1	-6.1	-3.8	.8
		-12.2	21.1	1570	1570	-7.8	13.4	5	3					
23RD	292.00									-71.5	118.1	-4.5	-2.9	.7
		-17.9	29.8	2005	2005	-8.9	14.8	4	3					
24TH	308.00									-53.6	88.3	-2.9	-1.9	.5
		-9.6	17.3	1317	1317	-7.3	13.2	5	3					
25TH	320.50									-44.0	71.0	-1.9	-1.3	.4
		-13.1	24.9	1685	1685	-7.8	14.8	3	2					
26TH	336.50									-30.9	46.0	-.9	-.7	.3
		-9.7	15.8	1276	1276	-7.6	12.4	4	3					
27TH	349.00									-21.2	30.2	-.4	-.3	.2
		-8.5	13.5	1275	1275	-6.6	10.6	8	5					
EAVE	361.50									-12.7	16.7	-.2	-.1	.0
		-12.7	16.7	1182	1182	-10.8	14.2	1	1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 70 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-135.3	553.8	-97.8	-23.2	3.1
		-16.9	43.7	4039	4039	-4.2	10.8	-1	-1					
2ND	26.00									-118.4	510.1	-84.0	-19.9	3.2
		-7.1	22.7	1942	1942	-3.7	11.7	-2	-1					
3RD	38.50									-111.3	487.4	-77.8	-18.4	3.2
		-6.5	23.2	1942	1942	-3.4	11.9	-2	-0					
4TH	51.00									-104.8	464.3	-71.8	-17.1	3.3
		-4.0	20.3	1942	1942	-2.1	10.5	-2	-0					
5TH	63.50									-100.8	444.0	-66.1	-15.8	3.3
		-2.4	17.0	1942	1942	-1.2	8.8	-3	-0					
6TH	76.00									-98.4	427.0	-60.7	-14.6	3.4
		-3.4	18.4	1843	1843	-1.8	10.0	4	1					
7TH	88.50									-95.0	408.6	-55.5	-13.4	3.3
		-3.5	18.6	1817	1817	-1.9	10.2	6	1					
8TH	101.00									-91.5	390.0	-50.5	-12.2	3.2
		-3.6	18.4	1817	1817	-2.0	10.1	6	1					
9TH	113.50									-88.0	371.7	-45.7	-11.1	3.1
		-3.6	18.2	1817	1817	-2.0	10.0	6	1					
10TH	126.00									-84.4	353.5	-41.2	-10.0	3.0
		-3.7	18.4	1817	1817	-2.0	10.1	7	1					
11TH	138.50									-80.7	335.1	-36.9	-9.0	2.8
		-3.7	18.7	1817	1817	-2.0	10.3	8	2					
12TH	151.00									-77.0	316.4	-32.8	-8.0	2.7
		-3.7	19.0	1817	1817	-2.1	10.4	8	2					
13TH	163.50									-73.3	297.5	-29.0	-7.0	2.5
		-3.9	19.2	1817	1817	-2.2	10.6	9	2					
14TH	176.00									-69.3	278.3	-25.4	-6.1	2.3
		-4.3	19.3	1817	1817	-2.3	10.6	8	2					
15TH	188.50									-65.1	259.0	-22.0	-5.3	2.2
		-4.6	19.4	1817	1817	-2.5	10.7	8	2					
16TH	201.00									-60.5	239.6	-18.9	-4.5	2.0
		-4.9	19.6	1817	1817	-2.7	10.8	7	2					
17TH	213.50									-55.6	220.0	-16.0	-3.8	1.9
		-5.3	19.6	1817	1817	-2.9	10.8	8	2					
18TH	226.00									-50.3	200.3	-13.4	-3.1	1.7
		-5.7	19.7	1817	1817	-3.1	10.9	8	2					
19TH	238.50									-44.6	180.6	-11.0	-2.5	1.5
		-6.1	20.0	1817	1817	-3.3	11.0	8	2					
20TH	251.00									-38.5	160.6	-8.9	-2.0	1.4
		-6.3	20.8	1817	1817	-3.5	11.4	7	2					
21ST	263.50									-32.2	139.8	-7.0	-1.6	1.2
		-8.3	27.5	2325	2325	-3.6	11.8	5	2					
22ND	279.50									-23.9	112.3	-5.0	-1.1	1.1
		-3.3	16.7	1570	1570	-2.1	10.6	12	2					
23RD	292.00									-20.6	95.6	-3.7	-.8	.9
		-5.3	23.8	2005	2005	-2.7	11.9	9	2					
24TH	308.00									-15.3	71.8	-2.3	-.6	.6
		-2.4	13.6	1317	1317	-1.8	10.3	10	2					
25TH	320.50									-12.8	58.2	-1.5	-.4	.5
		-3.4	20.6	1685	1685	-2.0	12.2	9	1					
26TH	336.50									-9.4	37.6	-.8	-.2	.3
		-3.1	12.3	1276	1276	-2.4	9.6	8	2					
27TH	349.00									-6.4	25.3	-.4	-.1	.2
		-1.9	11.2	1275	1275	-1.5	8.8	13	2					
EAVE	361.50									-4.5	14.1	-.1	-.0	.1
		-4.5	14.1	1182	1182	-3.8	11.9	4	1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS

WIND DIRECTION 80 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									14.4	553.5	-99.0	7.0	3.8
		-11.1	43.6	4039	4039	-2.8	10.8	1	0					
2ND	26.00									25.5	510.0	-85.2	6.5	3.8
		-3.8	22.4	1942	1942	-2.0	11.5	1	0					
3RD	38.50									29.3	487.6	-79.0	6.2	3.8
		-2.9	22.7	1942	1942	-1.5	11.7	2	0					
4TH	51.00									32.2	464.9	-73.0	5.8	3.7
		.4	19.5	1942	1942	.2	10.0	2	-0					
5TH	63.50									31.8	445.4	-67.3	5.4	3.7
		1.8	15.2	1942	1942	.9	7.8	-5	1					
6TH	76.00									30.1	430.2	-61.8	5.0	3.8
		1.1	18.1	1843	1843	.6	9.8	5	-0					
7TH	88.50									29.0	412.1	-56.6	4.6	3.7
		1.2	18.6	1817	1817	.6	10.2	7	-0					
8TH	101.00									27.8	393.5	-51.5	4.3	3.6
		1.3	18.4	1817	1817	.7	10.1	7	-0					
9TH	113.50									26.5	375.2	-46.7	3.9	3.4
		1.5	18.2	1817	1817	.8	10.0	7	-1					
10TH	126.00									25.0	357.0	-42.2	3.6	3.3
		1.5	18.2	1817	1817	.8	10.0	7	-1					
11TH	138.50									23.5	338.8	-37.8	3.3	3.2
		1.5	18.3	1817	1817	.8	10.1	7	-1					
12TH	151.00									22.0	320.5	-33.7	3.0	3.0
		1.4	18.5	1817	1817	.8	10.2	7	-1					
13TH	163.50									20.6	302.0	-29.8	2.8	2.9
		1.2	18.7	1817	1817	.7	10.3	8	-0					
14TH	176.00									19.4	283.4	-26.1	2.5	2.8
		.9	19.0	1817	1817	.5	10.5	8	-0					
15TH	188.50									18.5	264.4	-22.7	2.3	2.6
		.6	19.3	1817	1817	.3	10.6	8	-0					
16TH	201.00									17.9	245.1	-19.5	2.1	2.4
		.4	19.5	1817	1817	.2	10.8	8	-0					
17TH	213.50									17.5	225.5	-16.6	1.8	2.3
		.4	19.7	1817	1817	.2	10.8	9	-0					
18TH	226.00									17.1	205.8	-13.9	1.6	2.1
		.5	19.8	1817	1817	.3	10.9	9	-0					
19TH	238.50									16.6	186.0	-11.5	1.4	1.9
		.5	20.2	1817	1817	.3	11.1	10	-0					
20TH	251.00									16.1	165.8	-9.3	1.2	1.7
		.4	21.0	1817	1817	.2	11.6	9	-0					
21ST	263.50									15.8	144.8	-7.3	1.0	1.5
		.4	27.7	2325	2325	.2	11.9	9	-0					
22ND	279.50									15.4	117.1	-5.2	.7	1.3
		1.9	17.5	1570	1570	1.2	11.2	14	-2					
23RD	292.00									13.5	99.5	-3.9	.6	1.0
		2.2	24.8	2005	2005	1.1	12.4	11	-1					
24TH	308.00									11.3	74.7	-2.5	.4	.7
		2.1	13.8	1317	1317	1.6	10.5	11	-2					
25TH	320.50									9.2	60.9	-1.6	.2	.6
		3.1	21.5	1685	1685	1.8	12.7	9	-1					
26TH	336.50									6.1	39.5	-.8	.1	.4
		1.9	12.2	1276	1276	1.5	9.6	11	-2					
27TH	349.00									4.2	27.2	-.4	.1	.2
		2.5	12.0	1275	1275	1.9	9.4	14	-3					
EAVE	361.50									1.7	15.3	-.1	.0	.1
		1.7	15.3	1182	1182	1.5	12.9	5	-1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 90 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									64.2	540.6	-98.8	16.7	2.6
		-8.7	39.8	4039	4039	-2.2	9.9	2	0					
2ND	26.00									72.9	500.8	-85.3	14.9	2.5
		-2.5	20.2	1942	1942	-1.3	10.4	1	0					
3RD	38.50									75.4	480.5	-79.1	14.0	2.5
		-1.5	20.4	1942	1942	-.8	10.5	1	0					
4TH	51.00									76.9	460.1	-73.3	13.1	2.5
		2.1	18.0	1942	1942	1.1	9.3	3	-0					
5TH	63.50									74.9	442.1	-67.6	12.1	2.4
		3.9	14.1	1942	1942	2.0	7.3	-2	1					
6TH	76.00									70.9	428.0	-62.2	11.2	2.4
		2.7	17.2	1843	1843	1.5	9.3	5	-1					
7TH	88.50									68.2	410.8	-56.9	10.3	2.4
		2.6	17.9	1817	1817	1.4	9.8	6	-1					
8TH	101.00									65.6	392.9	-51.9	9.5	2.2
		2.8	17.9	1817	1817	1.5	9.9	5	-1					
9TH	113.50									62.8	375.0	-47.1	8.7	2.1
		2.9	18.0	1817	1817	1.6	9.9	5	-1					
10TH	126.00									59.9	356.9	-42.5	7.9	2.1
		2.9	18.1	1817	1817	1.6	10.0	5	-1					
11TH	138.50									56.9	338.8	-38.2	7.2	2.0
		2.9	18.3	1817	1817	1.6	10.1	5	-1					
12TH	151.00									54.0	320.5	-34.1	6.5	1.9
		2.8	18.5	1817	1817	1.6	10.2	5	-1					
13TH	163.50									51.2	302.0	-30.2	5.8	1.8
		2.8	18.6	1817	1817	1.5	10.2	5	-1					
14TH	176.00									48.4	283.4	-26.5	5.2	1.7
		2.8	18.7	1817	1817	1.5	10.3	5	-1					
15TH	188.50									45.7	264.7	-23.1	4.6	1.6
		2.7	18.9	1817	1817	1.5	10.4	5	-1					
16TH	201.00									42.9	245.9	-19.9	4.1	1.5
		2.6	19.0	1817	1817	1.5	10.5	5	-1					
17TH	213.50									40.3	226.9	-17.0	3.6	1.4
		2.5	19.1	1817	1817	1.4	10.5	5	-1					
18TH	226.00									37.7	207.8	-14.2	3.1	1.3
		2.4	19.3	1817	1817	1.3	10.6	6	-1					
19TH	238.50									35.3	188.5	-11.8	2.6	1.2
		2.3	19.7	1817	1817	1.3	10.8	6	-1					
20TH	251.00									33.0	168.8	-9.5	2.2	1.1
		2.2	20.8	1817	1817	1.2	11.4	6	-1					
21ST	263.50									30.7	148.0	-7.5	1.8	1.0
		2.9	28.0	2325	2325	1.3	12.1	5	-1					
22ND	279.50									27.8	120.0	-5.4	1.3	.8
		3.7	17.6	1570	1570	2.4	11.2	10	-2					
23RD	292.00									24.1	102.4	-4.0	1.0	.6
		4.1	25.1	2005	2005	2.1	12.5	7	-1					
24TH	308.00									20.0	77.3	-2.6	.6	.4
		3.9	14.2	1317	1317	3.0	10.8	7	-2					
25TH	320.50									16.1	63.1	-1.7	.4	.3
		5.5	21.7	1685	1685	3.3	12.9	6	-1					
26TH	336.50									10.6	41.4	-.9	.2	.2
		3.8	12.6	1276	1276	2.9	9.9	7	-2					
27TH	349.00									6.8	28.8	-.4	.1	.1
		3.3	12.9	1275	1275	2.6	10.1	6	-2					
EAVE	361.50									3.6	15.9	-.1	.0	.0
		3.6	15.9	1182	1182	3.0	13.5	2	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 100 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									75.4	527.5	-99.3	17.9	.9
		-11.3	35.2	4039	4039	-2.8	8.7	-2	-1					
2ND	26.00									86.7	492.3	-86.0	15.8	1.0
		-3.4	17.5	1942	1942	-1.7	9.0	-3	-1					
3RD	38.50									90.1	474.8	-80.0	14.7	1.1
		-2.2	17.6	1942	1942	-1.2	9.1	-2	-0					
4TH	51.00									92.3	457.2	-74.1	13.5	1.1
		2.2	15.8	1942	1942	1.1	8.2	5	-1					
5TH	63.50									90.1	441.3	-68.5	12.4	1.0
		3.5	11.5	1942	1942	1.8	5.9	-2	1					
6TH	76.00									86.7	429.8	-63.1	11.3	1.1
		3.3	16.5	1843	1843	1.8	9.0	4	-1					
7TH	88.50									83.4	413.3	-57.8	10.2	1.0
		3.8	17.7	1817	1817	2.1	9.7	5	-1					
8TH	101.00									79.5	395.7	-52.7	9.2	.9
		4.5	17.8	1817	1817	2.5	9.8	4	-1					
9TH	113.50									75.1	377.9	-47.9	8.2	.8
		5.1	17.9	1817	1817	2.8	9.9	3	-1					
10TH	126.00									70.0	360.0	-43.3	7.3	.8
		5.2	18.0	1817	1817	2.9	9.9	3	-1					
11TH	138.50									64.7	342.0	-38.9	6.5	.7
		5.2	18.1	1817	1817	2.9	10.0	2	-1					
12TH	151.00									59.5	323.9	-34.7	5.7	.7
		5.2	18.2	1817	1817	2.9	10.0	2	-1					
13TH	163.50									54.3	305.7	-30.8	5.0	.6
		5.0	18.3	1817	1817	2.7	10.1	2	-1					
14TH	176.00									49.4	287.4	-27.1	4.3	.6
		4.6	18.5	1817	1817	2.5	10.2	2	-0					
15TH	188.50									44.7	268.9	-23.6	3.8	.6
		4.3	18.7	1817	1817	2.3	10.3	1	-0					
16TH	201.00									40.5	250.2	-20.4	3.2	.5
		3.9	18.9	1817	1817	2.1	10.4	1	-0					
17TH	213.50									36.6	231.3	-17.4	2.7	.5
		3.5	19.2	1817	1817	1.9	10.6	2	-0					
18TH	226.00									33.1	212.1	-14.6	2.3	.5
		3.2	19.4	1817	1817	1.7	10.7	2	-0					
19TH	238.50									29.9	192.7	-12.1	1.9	.4
		2.9	19.9	1817	1817	1.6	11.0	3	-0					
20TH	251.00									27.0	172.7	-9.8	1.6	.4
		3.3	21.0	1817	1817	1.8	11.6	3	-0					
21ST	263.50									23.7	151.7	-7.8	1.2	.3
		4.7	28.4	2325	2325	2.0	12.2	3	-1					
22ND	279.50									19.0	123.4	-5.6	.9	.2
		2.5	18.1	1570	1570	1.6	11.6	3	-0					
23RD	292.00									16.5	105.2	-4.1	.7	.1
		3.1	25.6	2005	2005	1.5	12.8	2	-0					
24TH	308.00									13.4	79.6	-2.7	.4	.1
		2.4	15.1	1317	1317	1.8	11.5	1	-0					
25TH	320.50									11.0	64.5	-1.8	.3	.1
		3.6	22.0	1685	1685	2.1	13.1	1	-0					
26TH	336.50									7.4	42.5	-.9	.1	.0
		2.7	12.5	1276	1276	2.1	9.8	2	-1					
27TH	349.00									4.7	30.0	-.4	.1	.0
		2.2	13.3	1275	1275	1.8	10.4	0	-0					
EAVE	361.50									2.4	16.8	-.2	.0	.0
		2.4	16.8	1182	1182	2.1	14.2	0	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 110 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									16.8	500.2	-94.8	6.1	-.0
		-13.9	30.7	4039	4039	-3.4	7.6	-4	-2					
2ND	26.00									30.7	469.5	-82.2	5.5	.1
		-5.3	16.6	1942	1942	-2.7	8.6	-6	-2					
3RD	38.50									36.0	452.9	-76.4	5.1	.2
		-4.4	17.6	1942	1942	-2.3	9.0	-5	-1					
4TH	51.00									40.4	435.4	-70.9	4.6	.3
		.6	15.8	1942	1942	.3	8.1	7	-0					
5TH	63.50									39.8	419.6	-65.5	4.1	.2
		1.5	11.0	1942	1942	.8	5.7	5	-1					
6TH	76.00									38.3	408.6	-60.4	3.6	.2
		1.3	15.4	1843	1843	.7	8.4	2	-0					
7TH	88.50									37.0	393.2	-55.3	3.1	.1
		1.7	16.7	1817	1817	1.0	9.2	1	-0					
8TH	101.00									35.3	376.5	-50.5	2.7	.1
		2.3	17.1	1817	1817	1.3	9.4	1	-0					
9TH	113.50									32.9	359.4	-45.9	2.3	.1
		3.0	17.4	1817	1817	1.6	9.6	0	-0					
10TH	126.00									30.0	342.0	-41.6	1.9	.1
		3.2	17.5	1817	1817	1.8	9.6	1	-0					
11TH	138.50									26.8	324.5	-37.4	1.5	.1
		3.3	17.5	1817	1817	1.8	9.6	1	-0					
12TH	151.00									23.5	307.0	-33.4	1.2	.0
		3.3	17.5	1817	1817	1.8	9.6	2	-0					
13TH	163.50									20.2	289.5	-29.7	.9	.0
		3.2	17.5	1817	1817	1.8	9.6	2	-0					
14TH	176.00									17.0	272.0	-26.2	.7	-.0
		2.9	17.3	1817	1817	1.6	9.5	2	-0					
15TH	188.50									14.0	254.7	-22.9	.5	-.0
		2.6	17.2	1817	1817	1.4	9.5	2	-0					
16TH	201.00									11.4	237.5	-19.8	.3	-.1
		2.3	17.2	1817	1817	1.3	9.5	1	-0					
17TH	213.50									9.1	220.3	-17.0	.2	-.1
		2.0	17.4	1817	1817	1.1	9.6	1	-0					
18TH	226.00									7.1	202.9	-14.3	.1	-.1
		1.7	17.6	1817	1817	.9	9.7	1	-0					
19TH	238.50									5.4	185.3	-11.9	.0	-.1
		1.5	18.1	1817	1817	.8	10.0	1	-0					
20TH	251.00									3.8	167.2	-9.7	-.0	-.2
		1.8	19.4	1817	1817	1.0	10.7	1	-0					
21ST	263.50									2.1	147.8	-7.7	-.1	-.2
		2.5	26.7	2325	2325	1.1	11.5	1	-0					
22ND	279.50									-.4	121.2	-5.6	-.1	-.2
		.4	17.1	1570	1570	.3	10.9	-0	0					
23RD	292.00									-.8	104.1	-4.2	-.1	-.2
		.3	24.0	2005	2005	.1	12.0	-1	0					
24TH	308.00									-1.1	80.0	-2.7	-.1	-.2
		-.1	14.9	1317	1317	-.1	11.3	-1	-0					
25TH	320.50									-1.0	65.1	-1.8	-.0	-.2
		.1	21.6	1685	1685	.0	12.8	-2	0					
26TH	336.50									-1.1	43.5	-.9	-.0	-.1
		-.3	12.8	1276	1276	-.3	10.0	-4	-0					
27TH	349.00									-.7	30.7	-.5	-.0	-.1
		-.5	13.5	1275	1275	-.4	10.6	-5	-0					
EAVE	361.50									-.3	17.2	-.2	-.0	-.0
		-.3	17.2	1182	1182	-.2	14.6	-2	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS

WIND DIRECTION 120 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-29.9	630.3	-119.1	-4.3	.1
		-18.3	39.1	4039	4039	-4.5	9.7	-4	-2					
2ND	26.00									-11.5	591.1	-103.2	-3.8	.3
		-7.4	21.1	1942	1942	-3.8	10.9	-5	-2					
3RD	38.50									-4.1	570.0	-96.0	-3.7	.4
		-6.4	22.4	1942	1942	-3.3	11.6	-6	-2					
4TH	51.00									2.3	547.6	-89.0	-3.7	.5
		.1	21.1	1942	1942	.1	10.9	8	-0					
5TH	63.50									2.1	526.5	-82.3	-3.7	.4
		1.9	16.3	1942	1942	1.0	8.4	4	-0					
6TH	76.00									.3	510.2	-75.8	-3.7	.3
		1.6	21.4	1843	1843	.9	11.6	-1	0					
7TH	88.50									-1.4	488.8	-69.5	-3.7	.3
		2.0	22.4	1817	1817	1.1	12.3	-1	0					
8TH	101.00									-3.3	466.4	-63.6	-3.7	.4
		2.6	22.5	1817	1817	1.4	12.4	-1	0					
9TH	113.50									-5.9	443.9	-57.9	-3.6	.4
		3.1	22.6	1817	1817	1.7	12.4	-1	0					
10TH	126.00									-9.0	421.3	-52.5	-3.5	.4
		3.0	22.2	1817	1817	1.6	12.2	-1	0					
11TH	138.50									-12.0	399.1	-47.4	-3.4	.4
		2.5	21.8	1817	1817	1.4	12.0	-0	0					
12TH	151.00									-14.5	377.3	-42.5	-3.2	.4
		2.0	21.3	1817	1817	1.1	11.7	0	-0					
13TH	163.50									-16.5	356.0	-37.9	-3.0	.4
		1.6	20.8	1817	1817	.9	11.5	1	-0					
14TH	176.00									-18.1	335.2	-33.6	-2.8	.4
		1.3	20.4	1817	1817	.7	11.2	1	-0					
15TH	188.50									-19.5	314.8	-29.5	-2.6	.4
		1.0	19.9	1817	1817	.5	11.0	1	-0					
16TH	201.00									-20.5	294.8	-25.7	-2.3	.4
		.6	19.8	1817	1817	.3	10.9	1	-0					
17TH	213.50									-21.1	275.0	-22.2	-2.1	.3
		.1	20.1	1817	1817	.1	11.1	1	-0					
18TH	226.00									-21.2	254.9	-18.8	-1.8	.3
		-.3	20.5	1817	1817	-.2	11.3	2	0					
19TH	238.50									-20.9	234.5	-15.8	-1.5	.3
		-.8	21.2	1817	1817	-.4	11.7	2	0					
20TH	251.00									-20.1	213.2	-13.0	-1.3	.2
		-1.2	23.1	1817	1817	-.6	12.7	3	0					
21ST	263.50									-19.0	190.1	-10.5	-1.0	.2
		-2.1	31.9	2325	2325	-.9	13.7	4	0					
22ND	279.50									-16.8	158.2	-7.7	-.8	.1
		-1.8	18.2	1570	1570	-1.1	11.6	5	0					
23RD	292.00									-15.1	140.0	-5.8	-.6	-.0
		-4.0	29.2	2005	2005	-2.0	14.6	5	1					
24TH	308.00									-11.1	110.8	-3.8	-.4	-.2
		-1.6	19.5	1317	1317	-1.2	14.8	1	0					
25TH	320.50									-9.4	91.3	-2.6	-.2	-.2
		-3.5	29.4	1685	1685	-2.1	17.5	-0	-0					
26TH	336.50									-5.9	61.8	-1.3	-.1	-.2
		-2.2	17.7	1276	1276	-1.7	13.8	-3	-0					
27TH	349.00									-3.8	44.2	-.7	-.0	-.1
		-2.7	18.8	1275	1275	-2.1	14.7	-4	-1					
EAVE	361.50									-1.0	25.4	-.2	-.0	-.1
		-1.0	25.4	1182	1182	-.9	21.5	-3	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 130 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-66.0	285.9	-45.8	-5.5	2.7
		-21.5	26.6	4039	4039	-5.3	6.6	-3	-3					
2ND	26.00									-44.5	259.3	-38.7	-4.1	2.9
		-8.3	14.5	1942	1942	-4.3	7.5	-3	-2					
3RD	38.50									-36.2	244.8	-35.5	-3.6	3.0
		-6.7	15.0	1942	1942	-3.5	7.7	-2	-1					
4TH	51.00									-29.4	229.8	-32.5	-3.2	3.0
		-3.1	13.0	1942	1942	-1.6	6.7	5	1					
5TH	63.50									-26.3	216.8	-29.8	-2.8	2.9
		-2.5	12.2	1942	1942	-1.3	6.3	-3	-1					
6TH	76.00									-23.8	204.6	-27.1	-2.5	3.0
		-1.8	13.5	1843	1843	-1.0	7.3	5	1					
7TH	88.50									-22.0	191.1	-24.7	-2.2	2.9
		-1.0	13.0	1817	1817	-.6	7.2	8	1					
8TH	101.00									-21.0	178.1	-22.3	-2.0	2.8
		-.4	12.3	1817	1817	-.2	6.8	8	0					
9TH	113.50									-20.6	165.8	-20.2	-1.7	2.7
		.2	11.7	1817	1817	.1	6.4	9	-0					
10TH	126.00									-20.7	154.1	-18.2	-1.4	2.6
		-.0	11.0	1817	1817	-.0	6.0	10	0					
11TH	138.50									-20.7	143.1	-16.3	-1.2	2.5
		-.5	10.2	1817	1817	-.3	5.6	12	1					
12TH	151.00									-20.2	132.9	-14.6	-.9	2.4
		-1.0	9.5	1817	1817	-.6	5.2	13	1					
13TH	163.50									-19.2	123.4	-13.0	-.7	2.2
		-1.4	8.9	1817	1817	-.8	4.9	14	2					
14TH	176.00									-17.9	114.5	-11.5	-.5	2.1
		-1.6	8.4	1817	1817	-.9	4.6	15	3					
15TH	188.50									-16.2	106.1	-10.1	-.2	2.0
		-1.9	7.9	1817	1817	-1.0	4.4	16	4					
16TH	201.00									-14.4	98.2	-8.9	-.1	1.8
		-2.1	7.5	1817	1817	-1.2	4.1	17	5					
17TH	213.50									-12.3	90.8	-7.7	.1	1.7
		-2.3	7.0	1817	1817	-1.3	3.9	18	6					
18TH	226.00									-10.0	83.7	-6.6	.3	1.6
		-2.5	6.6	1817	1817	-1.4	3.6	19	7					
19TH	238.50									-7.4	77.1	-5.6	.4	1.4
		-2.6	6.5	1817	1817	-1.4	3.6	21	8					
20TH	251.00									-4.8	70.6	-4.7	.4	1.3
		-2.6	7.2	1817	1817	-1.4	3.9	23	8					
21ST	263.50									-2.3	63.4	-3.8	.5	1.1
		-3.4	10.1	2325	2325	-1.5	4.3	26	9					
22ND	279.50									1.2	53.3	-2.9	.5	.8
		-2.3	3.7	1570	1570	-1.4	2.3	36	22					
23RD	292.00									3.4	49.7	-2.3	.5	.6
		-4.0	8.5	2005	2005	-2.0	4.2	22	10					
24TH	308.00									7.4	41.1	-1.5	.4	.4
		1.5	5.7	1317	1317	1.2	4.3	16	-4					
25TH	320.50									5.9	35.5	-1.0	.3	.3
		-1.3	9.7	1685	1685	-.8	5.7	13	2					
26TH	336.50									7.2	25.8	-.6	.2	.1
		1.4	7.5	1276	1276	1.1	5.9	7	-1					
27TH	349.00									5.9	18.3	-.3	.1	.1
		1.3	7.3	1275	1275	1.0	5.7	12	-2					
EAVE	361.50									4.6	11.0	-.1	.0	.0
		4.6	11.0	1182	1182	3.9	9.3	0	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 140 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-167.3	-37.0	15.8	-22.7	1.6
		-23.9	13.0	4039	4039	-5.9	3.2	-2	-3					
2ND	26.00									-143.5	-50.0	14.6	-18.6	1.7
		-9.3	6.5	1942	1942	-4.8	3.4	-1	-1					
3RD	38.50									-134.2	-56.6	14.0	-16.9	1.7
		-7.9	6.2	1942	1942	-4.1	3.2	2	2					
4TH	51.00									-126.3	-62.7	13.2	-15.3	1.7
		-7.5	3.6	1942	1942	-3.9	1.8	4	9					
5TH	63.50									-118.8	-66.3	12.4	-13.8	1.6
		-9.3	2.9	1942	1942	-4.8	1.5	-2	-6					
6TH	76.00									-109.5	-69.2	11.6	-12.3	1.7
		-6.4	3.1	1843	1843	-3.5	1.7	6	13					
7TH	88.50									-103.1	-72.3	10.7	-11.0	1.6
		-5.4	2.2	1817	1817	-3.0	1.2	10	24					
8TH	101.00									-97.7	-74.5	9.8	-9.7	1.4
		-5.2	1.2	1817	1817	-2.8	.6	7	30					
9TH	113.50									-92.5	-75.6	8.8	-8.6	1.3
		-4.9	.1	1817	1817	-2.7	.1	1	35					
10TH	126.00									-87.6	-75.8	7.9	-7.4	1.1
		-5.1	-1.0	1817	1817	-2.8	-.5	-6	30					
11TH	138.50									-82.5	-74.8	7.0	-6.4	.9
		-5.4	-2.1	1817	1817	-3.0	-1.1	-8	22					
12TH	151.00									-77.0	-72.7	6.0	-5.4	.8
		-5.8	-3.2	1817	1817	-3.2	-1.8	-8	15					
13TH	163.50									-71.2	-69.6	5.1	-4.4	.7
		-6.1	-4.1	1817	1817	-3.4	-2.3	-7	10					
14TH	176.00									-65.1	-65.4	4.3	-3.6	.6
		-6.4	-5.0	1817	1817	-3.5	-2.8	-6	7					
15TH	188.50									-58.7	-60.4	3.5	-2.8	.5
		-6.7	-5.9	1817	1817	-3.7	-3.2	-4	5					
16TH	201.00									-51.9	-54.6	2.8	-2.1	.5
		-6.9	-6.4	1817	1817	-3.8	-3.5	-3	3					
17TH	213.50									-45.1	-48.2	2.2	-1.5	.4
		-6.7	-6.4	1817	1817	-3.7	-3.5	-3	3					
18TH	226.00									-38.4	-41.8	1.6	-1.0	.4
		-6.5	-6.4	1817	1817	-3.6	-3.5	-2	2					
19TH	238.50									-31.8	-35.5	1.1	-.6	.4
		-6.3	-6.3	1817	1817	-3.5	-3.5	-2	2					
20TH	251.00									-25.5	-29.2	.7	-.2	.3
		-6.5	-6.4	1817	1817	-3.6	-3.5	-4	4					
21ST	263.50									-19.0	-22.7	.4	.1	.3
		-9.1	-8.8	2325	2325	-3.9	-3.8	-5	5					
22ND	279.50									-9.9	-14.0	.1	.3	.2
		-5.6	-4.9	1570	1570	-3.6	-3.1	-3	3					
23RD	292.00									-4.3	-9.1	-.1	.4	.2
		-10.0	-9.2	2005	2005	-5.0	-4.6	-3	3					
24TH	308.00									5.7	.1	-.1	.4	.1
		1.0	.4	1317	1317	.8	.3	8	-22					
25TH	320.50									4.7	-.3	-.1	.3	.1
		-3.7	-4.4	1685	1685	-2.2	-2.6	-6	5					
26TH	336.50									8.3	4.1	-.1	.2	.0
		1.4	1.0	1276	1276	1.1	.8	0	-0					
27TH	349.00									6.9	3.1	-.1	.1	.0
		1.8	.7	1275	1275	1.4	.6	7	-16					
EAVE	361.50									5.1	2.4	-.0	.0	.0
		5.1	2.4	1182	1182	4.3	2.0	1	-2					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 150 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-22.8	-117.0	24.9	.7	-2.4
		-8.9	5.8	4039	4039	-2.2	1.4	-15	-23					
2ND	26.00									-13.9	-122.8	21.8	1.2	-2.1
		-1.0	1.8	1942	1942	-.5	.9	-82	-49					
3RD	38.50									-12.8	-124.5	20.3	1.3	-1.9
		.3	.7	1942	1942	.2	.4	-225	92					
4TH	51.00									-13.1	-125.3	18.7	1.5	-1.7
		-.7	-2.5	1942	1942	-.4	-1.3	9	-3					
5TH	63.50									-12.4	-122.8	17.1	1.7	-1.7
		-3.4	-4.9	1942	1942	-1.8	-2.5	-15	10					
6TH	76.00									-9.0	-117.9	15.6	1.8	-1.8
		-1.5	-2.7	1843	1843	-.8	-1.5	2	-1					
7TH	88.50									-7.5	-115.2	14.2	1.9	-1.8
		-1.1	-2.9	1817	1817	-.6	-1.6	9	-3					
8TH	101.00									-6.4	-112.3	12.8	2.0	-1.7
		-1.3	-3.8	1817	1817	-.7	-2.1	6	-2					
9TH	113.50									-5.2	-108.5	11.4	2.1	-1.7
		-1.5	-4.7	1817	1817	-.8	-2.6	5	-1					
10TH	126.00									-3.7	-103.8	10.1	2.1	-1.7
		-1.3	-5.3	1817	1817	-.7	-2.9	7	-2					
11TH	138.50									-2.4	-98.5	8.8	2.2	-1.6
		-1.1	-5.9	1817	1817	-.6	-3.2	10	-2					
12TH	151.00									-1.2	-92.6	7.6	2.2	-1.6
		-.9	-6.4	1817	1817	-.5	-3.5	12	-2					
13TH	163.50									-.3	-86.2	6.5	2.2	-1.5
		-1.0	-6.7	1817	1817	-.5	-3.7	13	-2					
14TH	176.00									.7	-79.6	5.4	2.2	-1.4
		-1.3	-6.8	1817	1817	-.7	-3.7	13	-2					
15TH	188.50									2.0	-72.8	4.5	2.2	-1.3
		-1.6	-6.9	1817	1817	-.9	-3.8	12	-3					
16TH	201.00									3.6	-65.9	3.6	2.1	-1.2
		-1.8	-7.0	1817	1817	-1.0	-3.9	12	-3					
17TH	213.50									5.4	-58.9	2.8	2.1	-1.1
		-1.7	-7.2	1817	1817	-1.0	-3.9	13	-3					
18TH	226.00									7.2	-51.7	2.2	2.0	-1.0
		-1.7	-7.3	1817	1817	-.9	-4.0	15	-3					
19TH	238.50									8.8	-44.4	1.6	1.9	-.9
		-1.6	-7.5	1817	1817	-.9	-4.1	16	-3					
20TH	251.00									10.4	-36.9	1.0	1.8	-.8
		-2.0	-7.8	1817	1817	-1.1	-4.3	17	-4					
21ST	263.50									12.4	-29.1	.6	1.6	-.7
		-3.5	-10.5	2325	2325	-1.5	-4.5	17	-6					
22ND	279.50									15.9	-18.6	.3	1.4	-.5
		-1.9	-6.0	1570	1570	-1.2	-3.8	19	-6					
23RD	292.00									17.8	-12.5	.1	1.2	-.3
		-3.7	-10.6	2005	2005	-1.9	-5.3	15	-5					
24TH	308.00									21.5	-2.0	-.1	.9	-.2
		3.3	.2	1317	1317	2.5	.2	-1	11					
25TH	320.50									18.2	-2.2	-.1	.6	-.1
		1.9	-4.8	1685	1685	1.1	-2.9	12	5					
26TH	336.50									16.3	2.6	-.1	.4	-.1
		4.6	.4	1276	1276	3.6	.3	-1	6					
27TH	349.00									11.8	2.3	-.0	.2	-.0
		4.8	.1	1275	1275	3.8	.0	-0	5					
EAVE	361.50									6.9	2.2	-.0	.1	-.0
		6.9	2.2	1182	1182	5.9	1.9	-0	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 160 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									322.3	-74.1	14.0	65.6	-2.1
		13.2	.6	4039	4039	3.3	.2	-1	14					
2ND	26.00									309.1	-74.7	12.1	57.4	-2.0
		10.3	-.3	1942	1942	5.3	-.1	0	15					
3RD	38.50									298.8	-74.5	11.2	53.6	-1.8
		12.0	-.7	1942	1942	6.2	-.4	1	15					
4TH	51.00									286.8	-73.8	10.2	49.9	-1.6
		10.1	-2.7	1942	1942	5.2	-1.4	0	2					
5TH	63.50									276.6	-71.1	9.3	46.4	-1.6
		10.1	-3.2	1942	1942	5.2	-1.7	-2	-6					
6TH	76.00									266.6	-67.9	8.5	43.0	-1.7
		8.9	-2.8	1843	1843	4.8	-1.5	1	3					
7TH	88.50									257.7	-65.1	7.6	39.7	-1.6
		8.8	-2.7	1817	1817	4.8	-1.5	2	5					
8TH	101.00									248.9	-62.4	6.8	36.6	-1.6
		9.0	-2.8	1817	1817	5.0	-1.5	1	5					
9TH	113.50									239.9	-59.7	6.1	33.5	-1.6
		9.2	-2.8	1817	1817	5.1	-1.6	1	4					
10TH	126.00									230.7	-56.8	5.4	30.6	-1.5
		9.4	-3.1	1817	1817	5.2	-1.7	1	4					
11TH	138.50									221.3	-53.7	4.7	27.8	-1.5
		9.6	-3.4	1817	1817	5.3	-1.9	1	4					
12TH	151.00									211.7	-50.3	4.0	25.1	-1.4
		9.8	-3.8	1817	1817	5.4	-2.1	2	4					
13TH	163.50									202.0	-46.5	3.4	22.5	-1.4
		10.1	-4.0	1817	1817	5.5	-2.2	2	4					
14TH	176.00									191.9	-42.4	2.8	20.0	-1.3
		10.4	-4.2	1817	1817	5.7	-2.3	2	5					
15TH	188.50									181.5	-38.3	2.3	17.7	-1.3
		10.8	-4.3	1817	1817	5.9	-2.4	2	6					
16TH	201.00									170.7	-34.0	1.9	15.5	-1.2
		11.1	-4.3	1817	1817	6.1	-2.4	2	6					
17TH	213.50									159.6	-29.7	1.5	13.4	-1.1
		11.2	-4.1	1817	1817	6.1	-2.2	2	7					
18TH	226.00									148.4	-25.6	1.1	11.5	-1.0
		11.3	-3.8	1817	1817	6.2	-2.1	2	7					
19TH	238.50									137.2	-21.8	.9	9.7	-.9
		11.7	-3.7	1817	1817	6.4	-2.0	2	7					
20TH	251.00									125.5	-18.1	.6	8.1	-.9
		12.8	-4.0	1817	1817	7.0	-2.2	3	8					
21ST	263.50									112.7	-14.1	.4	6.6	-.7
		17.5	-5.8	2325	2325	7.5	-2.5	3	10					
22ND	279.50									95.2	-8.4	.2	4.9	-.5
		8.6	-1.5	1570	1570	5.5	-1.0	3	18					
23RD	292.00									86.6	-6.8	.1	3.8	-.4
		16.4	-4.2	2005	2005	8.2	-2.1	3	12					
24TH	308.00									70.2	-2.6	.0	2.5	-.2
		11.4	.2	1317	1317	8.7	.1	-0	5					
25TH	320.50									58.8	-2.8	.0	1.7	-.1
		17.0	-2.5	1685	1685	10.1	-1.5	1	4					
26TH	336.50									41.8	-.3	-.0	.9	-.0
		11.8	-.2	1276	1276	9.3	-.2	0	3					
27TH	349.00									30.0	-.1	-.0	.5	.0
		12.6	-.8	1275	1275	9.9	-.7	0	2					
EAVE	361.50									17.4	.8	-.0	.2	.0
		17.4	.8	1182	1182	14.8	.7	0	-2					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 170 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									570.8	-153.9	28.1	112.9	.5
		25.6	-10.2	4039	4039	6.3	-2.5	-1	-3					
2ND	26.00									545.2	-143.7	24.2	98.4	.4
		18.0	-4.8	1942	1942	9.3	-2.5	-0	-1					
3RD	38.50									527.2	-138.9	22.5	91.7	.4
		20.6	-4.9	1942	1942	10.6	-2.5	-0	-1					
4TH	51.00									506.6	-134.1	20.8	85.2	.4
		17.1	-5.1	1942	1942	8.8	-2.6	-0	-1					
5TH	63.50									489.5	-128.9	19.1	79.0	.4
		17.8	-3.3	1942	1942	9.1	-1.7	1	3					
6TH	76.00									471.8	-125.6	17.5	73.0	.4
		16.7	-5.4	1843	1843	9.0	-2.9	0	0					
7TH	88.50									455.1	-120.2	16.0	67.2	.4
		16.7	-6.0	1817	1817	9.2	-3.3	-0	-1					
8TH	101.00									438.4	-114.2	14.5	61.6	.4
		17.1	-6.1	1817	1817	9.4	-3.3	-0	-1					
9TH	113.50									421.3	-108.1	13.1	56.2	.4
		17.5	-6.2	1817	1817	9.6	-3.4	-1	-2					
10TH	126.00									403.9	-102.0	11.8	51.1	.3
		17.9	-6.1	1817	1817	9.8	-3.4	-0	-1					
11TH	138.50									386.0	-95.8	10.6	46.2	.3
		18.3	-6.0	1817	1817	10.1	-3.3	-0	-1					
12TH	151.00									367.7	-89.8	9.4	41.4	.3
		18.7	-6.0	1817	1817	10.3	-3.3	-0	-0					
13TH	163.50									349.0	-83.8	8.3	37.0	.3
		19.1	-5.8	1817	1817	10.5	-3.2	-0	-0					
14TH	176.00									329.9	-78.0	7.3	32.7	.3
		19.4	-5.7	1817	1817	10.7	-3.1	-0	-1					
15TH	188.50									310.5	-72.3	6.4	28.7	.3
		19.7	-5.5	1817	1817	10.9	-3.0	-0	-1					
16TH	201.00									290.7	-66.8	5.5	25.0	.3
		20.0	-5.4	1817	1817	11.0	-3.0	-0	-1					
17TH	213.50									270.7	-61.4	4.7	21.5	.2
		20.3	-5.3	1817	1817	11.2	-2.9	-0	-0					
18TH	226.00									250.4	-56.1	4.0	18.2	.2
		20.6	-5.2	1817	1817	11.3	-2.9	0	0					
19TH	238.50									229.8	-50.9	3.3	15.2	.2
		21.2	-5.3	1817	1817	11.7	-2.9	0	0					
20TH	251.00									208.6	-45.6	2.7	12.5	.2
		23.1	-5.7	1817	1817	12.7	-3.2	0	0					
21ST	263.50									185.5	-39.9	2.2	10.0	.2
		32.4	-7.9	2325	2325	13.9	-3.4	0	0					
22ND	279.50									153.1	-31.9	1.6	7.3	.2
		19.2	-3.4	1570	1570	12.2	-2.1	0	2					
23RD	292.00									133.9	-28.5	1.2	5.5	.3
		29.6	-5.3	2005	2005	14.7	-2.6	0	1					
24TH	308.00									104.3	-23.2	.8	3.6	.3
		18.5	-3.4	1317	1317	14.1	-2.6	-0	-1					
25TH	320.50									85.8	-19.8	.5	2.4	.3
		27.9	-5.5	1685	1685	16.5	-3.2	-0	-1					
26TH	336.50									57.9	-14.4	.3	1.2	.3
		16.1	-5.1	1276	1276	12.7	-4.0	-2	-6					
27TH	349.00									41.8	-9.3	.1	.6	.2
		17.9	-5.1	1275	1275	14.0	-4.0	-2	-6					
EAVE	361.50									23.9	-4.2	.0	.2	.1
		23.9	-4.2	1182	1182	20.2	-3.6	-0	-3					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 180 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									658.9	-36.2	5.1	127.4	-.6
		34.8	-3.5	4039	4039	8.6	-.9	0	1					
2ND	26.00									624.1	-32.7	4.2	110.7	-.5
		21.4	-1.7	1942	1942	11.0	-.9	0	1					
3RD	38.50									602.7	-31.0	3.8	103.0	-.5
		23.5	-2.0	1942	1942	12.1	-1.0	0	2					
4TH	51.00									579.3	-29.0	3.4	95.7	-.5
		19.5	-1.6	1942	1942	10.0	-.8	0	0					
5TH	63.50									559.8	-27.4	3.0	88.5	-.5
		18.6	.6	1942	1942	9.6	.3	-0	0					
6TH	76.00									541.2	-28.1	2.7	81.7	-.5
		19.8	-.9	1843	1843	10.7	-.5	0	2					
7TH	88.50									521.4	-27.1	2.3	75.0	-.4
		20.2	-1.5	1817	1817	11.1	-.8	0	2					
8TH	101.00									501.2	-25.7	2.0	68.6	-.4
		20.5	-1.6	1817	1817	11.3	-.9	0	1					
9TH	113.50									480.7	-24.0	1.7	62.5	-.4
		20.8	-1.8	1817	1817	11.5	-1.0	0	1					
10TH	126.00									459.9	-22.2	1.4	56.6	-.4
		21.3	-2.0	1817	1817	11.7	-1.1	0	0					
11TH	138.50									438.6	-20.2	1.2	51.0	-.4
		21.7	-2.2	1817	1817	12.0	-1.2	-0	-0					
12TH	151.00									416.9	-18.0	.9	45.6	-.4
		22.2	-2.4	1817	1817	12.2	-1.3	-0	-0					
13TH	163.50									394.7	-15.6	.7	40.6	-.4
		22.6	-2.4	1817	1817	12.4	-1.3	-0	-0					
14TH	176.00									372.1	-13.2	.5	35.8	-.4
		22.9	-2.1	1817	1817	12.6	-1.2	0	1					
15TH	188.50									349.2	-11.1	.4	31.3	-.3
		23.2	-1.9	1817	1817	12.7	-1.1	0	1					
16TH	201.00									326.1	-9.2	.2	27.0	-.3
		23.5	-1.8	1817	1817	13.0	-1.0	0	2					
17TH	213.50									302.5	-7.4	.1	23.1	-.3
		24.1	-1.7	1817	1817	13.3	-1.0	0	2					
18TH	226.00									278.5	-5.6	.1	19.5	-.2
		24.6	-1.7	1817	1817	13.6	-.9	0	2					
19TH	238.50									253.8	-3.9	.0	16.2	-.2
		25.4	-1.7	1817	1817	14.0	-.9	0	1					
20TH	251.00									228.4	-2.3	-.0	13.1	-.2
		27.0	-1.5	1817	1817	14.9	-.8	0	1					
21ST	263.50									201.4	-.8	-.1	10.5	-.1
		37.1	-1.7	2325	2325	15.9	-.7	0	1					
22ND	279.50									164.4	.9	-.1	7.5	-.1
		22.8	-.7	1570	1570	14.5	-.4	0	2					
23RD	292.00									141.6	1.6	-.0	5.6	-.1
		33.7	-.5	2005	2005	16.8	-.2	0	1					
24TH	308.00									108.0	2.1	-.0	3.6	-.0
		20.2	1.1	1317	1317	15.3	.9	-0	1					
25TH	320.50									87.8	.9	.0	2.4	.0
		29.5	1.2	1685	1685	17.5	.7	-0	1					
26TH	336.50									58.3	-.2	.0	1.2	.0
		17.3	.3	1276	1276	13.5	.2	0	-0					
27TH	349.00									41.0	-.5	.0	.6	.0
		17.9	-.1	1275	1275	14.1	-.1	-0	-2					
EAVE	361.50									23.1	-.4	.0	.2	-.0
		23.1	-.4	1182	1182	19.5	-.4	0	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 190 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									665.1	29.4	-8.8	125.5	-2.6
		36.7	-2.8	4039	4039	9.1	-.7	0	5					
2ND	26.00									628.4	32.1	-8.0	108.6	-2.4
		23.1	.0	1942	1942	11.9	.0	-0	3					
3RD	38.50									605.3	32.1	-7.6	100.9	-2.3
		25.7	.9	1942	1942	13.3	.5	-0	3					
4TH	51.00									579.6	31.2	-7.2	93.5	-2.3
		21.4	-.2	1942	1942	11.0	-.1	0	0					
5TH	63.50									558.2	31.4	-6.9	86.4	-2.3
		19.0	1.7	1942	1942	9.8	.9	-0	0					
6TH	76.00									539.2	29.7	-6.5	79.6	-2.2
		21.2	.5	1843	1843	11.5	.2	-0	4					
7TH	88.50									518.0	29.2	-6.1	72.9	-2.2
		21.8	.2	1817	1817	12.0	.1	-0	5					
8TH	101.00									496.2	29.0	-5.7	66.6	-2.1
		21.9	.2	1817	1817	12.1	.1	-0	4					
9TH	113.50									474.3	28.8	-5.4	60.5	-2.0
		22.1	.3	1817	1817	12.1	.1	-0	4					
10TH	126.00									452.2	28.5	-5.0	54.8	-1.9
		22.2	.4	1817	1817	12.2	.2	-0	4					
11TH	138.50									430.0	28.1	-4.7	49.2	-1.8
		22.3	.6	1817	1817	12.3	.3	-0	3					
12TH	151.00									407.7	27.5	-4.3	44.0	-1.7
		22.4	.8	1817	1817	12.3	.4	-0	3					
13TH	163.50									385.4	26.7	-4.0	39.0	-1.7
		22.6	.8	1817	1817	12.5	.4	-0	3					
14TH	176.00									362.7	25.9	-3.7	34.4	-1.6
		23.0	.5	1817	1817	12.7	.3	-0	4					
15TH	188.50									339.7	25.4	-3.3	30.0	-1.5
		23.4	.3	1817	1817	12.9	.2	-0	4					
16TH	201.00									316.4	25.1	-3.0	25.9	-1.4
		23.7	.2	1817	1817	13.0	.1	-0	5					
17TH	213.50									292.7	24.9	-2.7	22.1	-1.3
		24.0	.2	1817	1817	13.2	.1	-0	5					
18TH	226.00									268.6	24.7	-2.4	18.6	-1.2
		24.4	.2	1817	1817	13.4	.1	-0	4					
19TH	238.50									244.3	24.6	-2.1	15.4	-1.1
		25.0	.1	1817	1817	13.8	.1	-0	4					
20TH	251.00									219.3	24.4	-1.8	12.5	-.9
		26.5	.3	1817	1817	14.6	.1	-0	4					
21ST	263.50									192.8	24.2	-1.5	9.9	-.9
		35.8	.9	2325	2325	15.4	.4	-0	3					
22ND	279.50									157.0	23.3	-1.1	7.1	-.7
		23.1	3.0	1570	1570	14.7	1.9	-1	6					
23RD	292.00									133.9	20.3	-.8	5.3	-.6
		32.6	4.1	2005	2005	16.2	2.0	-1	6					
24TH	308.00									101.3	16.2	-.5	3.4	-.4
		18.7	3.3	1317	1317	14.2	2.5	-1	5					
25TH	320.50									82.6	12.9	-.4	2.2	-.3
		27.9	4.2	1685	1685	16.5	2.5	-1	4					
26TH	336.50									54.7	8.7	-.2	1.1	-.2
		16.5	2.9	1276	1276	13.0	2.2	-1	5					
27TH	349.00									38.2	5.9	-.1	.6	-.1
		16.9	2.4	1275	1275	13.2	1.9	-0	3					
EAVE	361.50									21.3	3.5	-.0	.2	-.0
		21.3	3.5	1182	1182	18.0	3.0	-0	2					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 200 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									679.8	75.3	-19.9	125.9	-4.5
		38.3	-4.0	4039	4039	9.5	-1.0	0	4					
2ND	26.00									641.5	79.3	-17.9	108.7	-4.3
		24.2	-.8	1942	1942	12.5	-.4	0	3					
3RD	38.50									617.3	80.1	-16.9	100.9	-4.2
		27.0	-.2	1942	1942	13.9	-.1	0	3					
4TH	51.00									590.3	80.4	-15.9	93.3	-4.1
		23.1	.2	1942	1942	11.9	.1	0	-1					
5TH	63.50									567.2	80.1	-14.9	86.1	-4.2
		20.0	2.1	1942	1942	10.3	1.1	1	-5					
6TH	76.00									547.2	78.0	-13.9	79.1	-4.3
		22.8	.9	1843	1843	12.4	.5	-0	4					
7TH	88.50									524.4	77.1	-12.9	72.4	-4.2
		23.2	1.0	1817	1817	12.8	.5	-0	6					
8TH	101.00									501.2	76.1	-12.0	66.0	-4.0
		23.0	1.3	1817	1817	12.7	.7	-0	6					
9TH	113.50									478.1	74.8	-11.0	59.9	-3.9
		22.9	1.7	1817	1817	12.6	.9	-0	6					
10TH	126.00									455.3	73.2	-10.1	54.0	-3.8
		23.1	2.1	1817	1817	12.7	1.2	-1	6					
11TH	138.50									432.2	71.0	-9.2	48.5	-3.6
		23.4	2.7	1817	1817	12.9	1.5	-1	7					
12TH	151.00									408.8	68.4	-8.3	43.2	-3.4
		23.8	3.2	1817	1817	13.1	1.8	-1	7					
13TH	163.50									385.0	65.2	-7.5	38.3	-3.3
		24.0	3.5	1817	1817	13.2	1.9	-1	7					
14TH	176.00									360.9	61.8	-6.7	33.6	-3.1
		24.2	3.5	1817	1817	13.3	1.9	-1	7					
15TH	188.50									336.7	58.2	-6.0	29.3	-2.9
		24.4	3.6	1817	1817	13.4	2.0	-1	8					
16TH	201.00									312.3	54.6	-5.2	25.2	-2.7
		24.5	3.5	1817	1817	13.5	1.9	-1	8					
17TH	213.50									287.8	51.1	-4.6	21.5	-2.5
		24.6	3.2	1817	1817	13.5	1.8	-1	8					
18TH	226.00									263.2	47.9	-4.0	18.0	-2.3
		24.6	2.9	1817	1817	13.6	1.6	-1	9					
19TH	238.50									238.6	45.1	-3.4	14.9	-2.1
		25.0	2.6	1817	1817	13.8	1.4	-1	9					
20TH	251.00									213.6	42.5	-2.8	12.0	-1.9
		26.2	2.6	1817	1817	14.4	1.4	-1	9					
21ST	263.50									187.4	39.9	-2.3	9.5	-1.7
		35.0	3.7	2325	2325	15.1	1.6	-1	9					
22ND	279.50									152.4	36.2	-1.7	6.8	-1.3
		22.7	4.6	1570	1570	14.5	2.9	-2	10					
23RD	292.00									129.7	31.6	-1.3	5.1	-1.1
		32.4	5.8	2005	2005	16.2	2.9	-2	9					
24TH	308.00									97.3	25.8	-.8	3.2	-.8
		17.7	5.4	1317	1317	13.4	4.1	-3	9					
25TH	320.50									79.6	20.5	-.5	2.1	-.6
		27.8	6.7	1685	1685	16.5	3.9	-2	8					
26TH	336.50									51.9	13.8	-.3	1.1	-.4
		15.7	4.7	1276	1276	12.3	3.7	-3	8					
27TH	349.00									36.1	9.1	-.1	.5	-.2
		15.7	4.8	1275	1275	12.3	3.8	-3	9					
EAVE	361.50									20.4	4.3	-.0	.2	-.1
		20.4	4.3	1182	1182	17.2	3.6	-1	4					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 210 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									771.4	-112.4	13.2	141.5	-4.5
		46.1	-18.3	4039	4039	11.4	-4.5	1	1					
2ND	26.00									725.3	-94.1	10.5	122.0	-4.4
		27.4	-8.0	1942	1942	14.1	-4.1	0	1					
3RD	38.50									698.0	-86.1	9.4	113.1	-4.4
		29.8	-7.6	1942	1942	15.3	-3.9	0	1					
4TH	51.00									668.2	-78.5	8.4	104.6	-4.3
		26.2	-7.2	1942	1942	13.5	-3.7	-0	-2					
5TH	63.50									642.0	-71.3	7.4	96.4	-4.4
		22.4	-3.9	1942	1942	11.5	-2.0	-0	-1					
6TH	76.00									619.6	-67.4	6.6	88.5	-4.4
		26.5	-5.9	1843	1843	14.4	-3.2	1	3					
7TH	88.50									593.1	-61.5	5.8	80.9	-4.3
		27.2	-5.8	1817	1817	14.9	-3.2	1	4					
8TH	101.00									566.0	-55.8	5.0	73.7	-4.2
		27.1	-5.2	1817	1817	14.9	-2.9	1	4					
9TH	113.50									538.9	-50.6	4.4	66.8	-4.1
		27.0	-4.6	1817	1817	14.8	-2.5	1	5					
10TH	126.00									511.9	-45.9	3.8	60.2	-4.0
		27.0	-4.3	1817	1817	14.9	-2.4	1	5					
11TH	138.50									484.9	-41.6	3.2	54.0	-3.8
		27.1	-4.0	1817	1817	14.9	-2.2	1	4					
12TH	151.00									457.8	-37.6	2.7	48.1	-3.7
		27.2	-3.8	1817	1817	15.0	-2.1	1	4					
13TH	163.50									430.6	-33.8	2.3	42.5	-3.6
		27.2	-3.5	1817	1817	15.0	-1.9	1	5					
14TH	176.00									403.4	-30.4	1.9	37.3	-3.4
		27.1	-3.1	1817	1817	14.9	-1.7	1	6					
15TH	188.50									376.2	-27.3	1.5	32.5	-3.3
		27.1	-2.7	1817	1817	14.9	-1.5	1	8					
16TH	201.00									349.1	-24.6	1.2	27.9	-3.1
		27.2	-2.6	1817	1817	15.0	-1.4	1	8					
17TH	213.50									321.9	-22.0	.9	23.7	-2.8
		27.8	-3.0	1817	1817	15.3	-1.6	1	8					
18TH	226.00									294.1	-19.0	.6	19.9	-2.6
		28.4	-3.4	1817	1817	15.6	-1.9	1	8					
19TH	238.50									265.7	-15.6	.4	16.4	-2.3
		29.0	-3.7	1817	1817	16.0	-2.1	1	8					
20TH	251.00									236.6	-11.9	.3	13.2	-2.1
		29.9	-4.0	1817	1817	16.4	-2.2	1	7					
21ST	263.50									206.7	-7.9	.1	10.5	-1.9
		39.4	-5.5	2325	2325	17.0	-2.4	1	6					
22ND	279.50									167.3	-2.4	.1	7.5	-1.6
		25.0	-.9	1570	1570	15.9	-.6	0	13					
23RD	292.00									142.3	-1.5	.0	5.5	-1.3
		35.1	-2.1	2005	2005	17.5	-1.0	1	9					
24TH	308.00									107.2	.6	.0	3.5	-1.0
		19.9	.3	1317	1317	15.1	.2	-0	11					
25TH	320.50									87.3	.2	.0	2.3	-.8
		30.0	.6	1685	1685	17.8	.3	-0	9					
26TH	336.50									57.3	-.3	.0	1.2	-.5
		18.4	-.1	1276	1276	14.4	-.1	0	9					
27TH	349.00									38.9	-.2	.0	.6	-.3
		17.2	1.3	1275	1275	13.5	1.0	-1	13					
EAVE	361.50									21.6	-1.5	.0	.2	-.1
		21.6	-1.5	1182	1182	18.3	-1.3	0	4					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 220 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									780.6	-473.4	80.3	141.6	-3.1
		49.2	-39.4	4039	4039	12.2	-9.7	-2	-2					
2ND	26.00									731.5	-434.1	68.5	121.9	-3.2
		27.9	-18.9	1942	1942	14.4	-9.7	-0	-1					
3RD	38.50									703.6	-415.2	63.1	113.0	-3.3
		29.7	-19.2	1942	1942	15.3	-9.9	-0	-1					
4TH	51.00									673.9	-396.0	58.1	104.3	-3.3
		27.8	-18.9	1942	1942	14.3	-9.7	-1	-1					
5TH	63.50									646.1	-377.1	53.2	96.1	-3.3
		24.3	-15.0	1942	1942	12.5	-7.7	2	3					
6TH	76.00									621.7	-362.1	48.6	88.2	-3.2
		27.0	-17.7	1843	1843	14.7	-9.6	1	2					
7TH	88.50									594.7	-344.4	44.2	80.6	-3.2
		27.5	-18.1	1817	1817	15.1	-9.9	1	2					
8TH	101.00									567.2	-326.4	40.0	73.3	-3.1
		27.6	-18.0	1817	1817	15.2	-9.9	1	2					
9TH	113.50									539.6	-308.4	36.1	66.4	-3.0
		27.7	-17.9	1817	1817	15.3	-9.8	2	2					
10TH	126.00									511.9	-290.5	32.3	59.8	-2.9
		27.9	-17.6	1817	1817	15.3	-9.7	2	3					
11TH	138.50									484.0	-272.9	28.8	53.6	-2.8
		28.0	-17.2	1817	1817	15.4	-9.5	2	3					
12TH	151.00									456.0	-255.7	25.5	47.7	-2.7
		28.2	-16.9	1817	1817	15.5	-9.3	2	3					
13TH	163.50									427.8	-238.9	22.4	42.2	-2.5
		27.9	-16.6	1817	1817	15.4	-9.1	2	4					
14TH	176.00									399.9	-222.3	19.5	37.0	-2.4
		27.4	-16.4	1817	1817	15.1	-9.0	3	4					
15TH	188.50									372.5	-205.9	16.8	32.2	-2.2
		26.9	-16.2	1817	1817	14.8	-8.9	3	5					
16TH	201.00									345.6	-189.7	14.4	27.7	-2.1
		26.8	-16.3	1817	1817	14.7	-8.9	3	5					
17TH	213.50									318.9	-173.4	12.1	23.6	-1.9
		27.2	-16.6	1817	1817	15.0	-9.2	3	5					
18TH	226.00									291.7	-156.8	10.0	19.7	-1.7
		27.6	-17.0	1817	1817	15.2	-9.4	3	5					
19TH	238.50									264.0	-139.7	8.2	16.3	-1.5
		28.3	-17.6	1817	1817	15.6	-9.7	3	4					
20TH	251.00									235.7	-122.1	6.5	13.1	-1.3
		29.5	-18.2	1817	1817	16.3	-10.0	2	3					
21ST	263.50									206.2	-104.0	5.1	10.4	-1.2
		39.3	-23.7	2325	2325	16.9	-10.2	1	2					
22ND	279.50									166.9	-80.2	3.7	7.4	-1.1
		25.2	-12.0	1570	1570	16.1	-7.6	3	7					
23RD	292.00									141.6	-68.3	2.7	5.5	-.9
		35.2	-16.6	2005	2005	17.6	-8.3	2	5					
24TH	308.00									106.4	-51.7	1.8	3.5	-.7
		20.3	-9.7	1317	1317	15.4	-7.4	3	6					
25TH	320.50									86.1	-41.9	1.2	2.3	-.5
		29.6	-12.6	1685	1685	17.6	-7.5	2	6					
26TH	336.50									56.4	-29.4	.6	1.1	-.3
		18.9	-9.4	1276	1276	14.8	-7.4	2	4					
27TH	349.00									37.5	-20.0	.3	.6	-.2
		16.6	-8.3	1275	1275	13.1	-6.5	4	7					
EAVE	361.50									20.9	-11.6	.1	.2	-.1
		20.9	-11.6	1182	1182	17.7	-9.8	1	2					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 230 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									802.7	-620.3	115.5	145.5	-1.8
		45.9	-38.2	4039	4039	11.4	-9.5	-3	-4					
2ND	26.00									756.8	-582.1	99.8	125.2	-2.1
		26.8	-18.3	1942	1942	13.8	-9.4	-1	-1					
3RD	38.50									730.1	-563.8	92.7	116.0	-2.1
		29.0	-18.8	1942	1942	14.9	-9.7	0	0					
4TH	51.00									701.1	-545.0	85.8	107.0	-2.1
		31.0	-21.7	1942	1942	16.0	-11.2	-1	-2					
5TH	63.50									670.1	-523.3	79.1	98.4	-2.2
		25.8	-16.7	1942	1942	13.3	-8.6	1	2					
6TH	76.00									644.3	-506.6	72.6	90.2	-2.1
		28.3	-21.1	1843	1843	15.3	-11.5	1	1					
7TH	88.50									616.1	-485.5	66.4	82.3	-2.1
		29.0	-22.1	1817	1817	16.0	-12.2	1	1					
8TH	101.00									587.1	-463.4	60.5	74.8	-2.0
		29.3	-22.1	1817	1817	16.1	-12.1	1	2					
9TH	113.50									557.7	-441.3	54.9	67.7	-1.9
		29.7	-22.0	1817	1817	16.3	-12.1	2	2					
10TH	126.00									528.1	-419.3	49.5	60.9	-1.8
		29.8	-21.9	1817	1817	16.4	-12.1	2	3					
11TH	138.50									498.3	-397.4	44.4	54.5	-1.7
		29.8	-21.8	1817	1817	16.4	-12.0	2	3					
12TH	151.00									468.5	-375.6	39.5	48.4	-1.6
		29.8	-21.7	1817	1817	16.4	-11.9	2	3					
13TH	163.50									438.7	-353.9	35.0	42.8	-1.5
		29.5	-21.7	1817	1817	16.2	-12.0	2	3					
14TH	176.00									409.2	-332.2	30.7	37.5	-1.3
		28.8	-22.0	1817	1817	15.9	-12.1	2	3					
15TH	188.50									380.4	-310.2	26.7	32.5	-1.2
		28.2	-22.2	1817	1817	15.5	-12.2	2	3					
16TH	201.00									352.1	-288.1	22.9	27.9	-1.1
		28.0	-22.5	1817	1817	15.4	-12.4	2	3					
17TH	213.50									324.2	-265.6	19.5	23.7	-1.0
		28.2	-23.0	1817	1817	15.5	-12.7	2	3					
18TH	226.00									295.9	-242.6	16.3	19.8	-.8
		28.5	-23.5	1817	1817	15.7	-12.9	2	3					
19TH	238.50									267.5	-219.1	13.4	16.3	-.7
		29.0	-24.2	1817	1817	16.0	-13.3	2	2					
20TH	251.00									238.5	-194.8	10.8	13.2	-.6
		30.3	-25.5	1817	1817	16.7	-14.1	1	1					
21ST	263.50									208.2	-169.3	8.6	10.4	-.5
		40.7	-34.5	2325	2325	17.5	-14.8	-0	-0					
22ND	279.50									167.5	-134.8	6.1	7.4	-.6
		25.6	-20.3	1570	1570	16.3	-13.0	2	2					
23RD	292.00									141.9	-114.5	4.6	5.4	-.5
		35.6	-27.1	2005	2005	17.8	-13.5	2	2					
24TH	308.00									106.3	-87.3	2.9	3.4	-.4
		21.0	-16.5	1317	1317	16.0	-12.5	2	2					
25TH	320.50									85.2	-70.9	2.0	2.2	-.3
		29.4	-22.1	1685	1685	17.4	-13.1	2	2					
26TH	336.50									55.9	-48.8	1.0	1.1	-.2
		19.1	-15.8	1276	1276	14.9	-12.4	1	2					
27TH	349.00									36.8	-33.0	.5	.5	-.1
		16.6	-14.2	1275	1275	13.0	-11.2	3	3					
EAVE	361.50									20.2	-18.7	.2	.2	-.0
		20.2	-18.7	1182	1182	17.1	-15.8	1	1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS

WIND DIRECTION 240 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									851.6	-747.5	141.8	155.1	1.1
		44.3	-47.4	4039	4039	11.0	-11.7	-6	-6					
2ND	26.00									807.3	-700.1	123.0	133.5	.6
		26.4	-23.9	1942	1942	13.6	-12.3	-4	-4					
3RD	38.50									780.9	-676.1	114.4	123.6	.4
		28.7	-24.4	1942	1942	14.8	-12.6	-2	-3					
4TH	51.00									752.2	-651.8	106.1	114.0	.3
		32.7	-25.2	1942	1942	16.8	-13.0	-1	-1					
5TH	63.50									719.6	-626.5	98.1	104.8	.2
		27.6	-20.2	1942	1942	14.2	-10.4	2	3					
6TH	76.00									692.0	-606.3	90.4	96.0	.3
		30.4	-23.0	1843	1843	16.5	-12.5	0	0					
7TH	88.50									661.6	-583.4	83.0	87.6	.4
		31.3	-23.6	1817	1817	17.2	-13.0	0	0					
8TH	101.00									630.3	-559.7	75.8	79.5	.4
		31.8	-23.9	1817	1817	17.5	-13.1	0	0					
9TH	113.50									598.5	-535.9	69.0	71.8	.4
		32.3	-24.1	1817	1817	17.8	-13.3	0	0					
10TH	126.00									566.1	-511.7	62.4	64.5	.4
		32.4	-24.4	1817	1817	17.8	-13.4	0	0					
11TH	138.50									533.8	-487.3	56.2	57.7	.4
		32.2	-24.7	1817	1817	17.7	-13.6	0	0					
12TH	151.00									501.6	-462.6	50.2	51.2	.4
		32.0	-25.1	1817	1817	17.6	-13.8	-0	-0					
13TH	163.50									469.6	-437.5	44.6	45.1	.4
		31.7	-25.2	1817	1817	17.4	-13.9	-0	-0					
14TH	176.00									437.9	-412.3	39.3	39.4	.4
		31.3	-25.2	1817	1817	17.3	-13.9	-0	-0					
15TH	188.50									406.6	-387.1	34.3	34.2	.4
		31.0	-25.2	1817	1817	17.1	-13.9	-0	-0					
16TH	201.00									375.6	-361.8	29.6	29.3	.4
		30.8	-25.7	1817	1817	17.0	-14.1	-0	-0					
17TH	213.50									344.8	-336.1	25.3	24.8	.4
		31.0	-26.8	1817	1817	17.0	-14.7	-0	-0					
18TH	226.00									313.8	-309.4	21.2	20.7	.4
		31.1	-27.9	1817	1817	17.1	-15.3	0	0					
19TH	238.50									282.7	-281.5	17.5	16.9	.4
		31.6	-29.2	1817	1817	17.4	-16.1	-0	-0					
20TH	251.00									251.1	-252.3	14.2	13.6	.4
		33.2	-31.0	1817	1817	18.3	-17.1	-1	-1					
21ST	263.50									217.9	-221.3	11.2	10.7	.3
		44.9	-42.4	2325	2325	19.3	-18.2	-2	-2					
22ND	279.50									173.0	-178.9	8.0	7.5	.2
		27.5	-26.0	1570	1570	17.5	-16.6	-1	-1					
23RD	292.00									145.5	-152.9	6.0	5.5	.1
		36.9	-36.5	2005	2005	18.4	-18.2	-1	-1					
24TH	308.00									108.6	-116.4	3.8	3.5	.1
		22.1	-23.2	1317	1317	16.8	-17.6	-0	-0					
25TH	320.50									86.5	-93.2	2.5	2.3	.0
		29.4	-30.8	1685	1685	17.4	-18.3	-0	-0					
26TH	336.50									57.1	-62.4	1.3	1.1	.0
		19.5	-20.6	1276	1276	15.3	-16.2	-1	-1					
27TH	349.00									37.6	-41.8	.6	.5	.0
		17.3	-18.6	1275	1275	13.6	-14.6	-1	-1					
EAVE	361.50									20.3	-23.2	.2	.2	-.0
		20.3	-23.2	1182	1182	17.1	-19.6	0	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 250 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									906.1	-950.9	184.4	160.5	2.7
		54.7	-56.8	4039	4039	13.5	-14.1	-4	-4					
2ND	26.00									851.4	-894.1	160.4	137.7	2.2
		30.1	-28.7	1942	1942	15.5	-14.8	-1	-2					
3RD	38.50									821.3	-865.4	149.4	127.2	2.2
		32.3	-29.0	1942	1942	16.6	-15.0	0	0					
4TH	51.00									789.0	-836.4	138.8	117.2	2.2
		36.8	-30.9	1942	1942	19.0	-15.9	0	0					
5TH	63.50									752.2	-805.5	128.5	107.5	2.2
		31.2	-23.1	1942	1942	16.1	-11.9	2	2					
6TH	76.00									721.0	-782.4	118.6	98.3	2.3
		33.4	-28.5	1843	1843	18.1	-15.4	0	0					
7TH	88.50									687.5	-753.9	109.0	89.5	2.3
		33.9	-29.4	1817	1817	18.7	-16.2	-0	-0					
8TH	101.00									653.6	-724.5	99.8	81.1	2.3
		34.0	-29.3	1817	1817	18.7	-16.2	-0	-0					
9TH	113.50									619.6	-695.1	90.9	73.2	2.3
		34.0	-29.3	1817	1817	18.7	-16.1	-0	-0					
10TH	126.00									585.7	-665.9	82.4	65.6	2.3
		33.9	-29.8	1817	1817	18.7	-16.4	-1	-1					
11TH	138.50									551.8	-636.1	74.3	58.5	2.2
		33.8	-30.5	1817	1817	18.6	-16.8	-1	-1					
12TH	151.00									517.9	-605.7	66.5	51.8	2.2
		33.8	-31.2	1817	1817	18.6	-17.2	-1	-1					
13TH	163.50									484.1	-574.4	59.1	45.6	2.1
		33.7	-31.8	1817	1817	18.5	-17.5	-1	-2					
14TH	176.00									450.5	-542.6	52.1	39.7	2.0
		33.5	-32.3	1817	1817	18.5	-17.8	-1	-2					
15TH	188.50									416.9	-510.3	45.6	34.3	1.9
		33.4	-32.8	1817	1817	18.4	-18.1	-2	-2					
16TH	201.00									383.5	-477.5	39.4	29.3	1.8
		33.2	-33.5	1817	1817	18.3	-18.4	-2	-2					
17TH	213.50									350.3	-444.0	33.6	24.7	1.7
		32.9	-34.5	1817	1817	18.1	-19.0	-1	-1					
18TH	226.00									317.4	-409.5	28.3	20.6	1.6
		32.7	-35.5	1817	1817	18.0	-19.5	-1	-1					
19TH	238.50									284.7	-374.1	23.4	16.8	1.5
		33.0	-37.0	1817	1817	18.1	-20.4	-1	-1					
20TH	251.00									251.7	-337.0	19.0	13.4	1.4
		34.7	-40.2	1817	1817	19.1	-22.1	-2	-2					
21ST	263.50									217.0	-296.8	15.0	10.5	1.3
		46.6	-56.0	2325	2325	20.0	-24.1	-3	-2					
22ND	279.50									170.4	-240.7	10.7	7.4	1.0
		26.9	-36.1	1570	1570	17.2	-23.0	-4	-3					
23RD	292.00									143.5	-204.6	7.9	5.4	.8
		36.6	-49.3	2005	2005	18.2	-24.6	-3	-3					
24TH	308.00									106.9	-155.3	5.0	3.4	.5
		22.3	-31.6	1317	1317	17.0	-24.0	-3	-2					
25TH	320.50									84.6	-123.7	3.3	2.2	.4
		28.7	-41.9	1685	1685	17.0	-24.9	-2	-2					
26TH	336.50									55.9	-81.8	1.6	1.1	.3
		19.4	-27.3	1276	1276	15.2	-21.4	-3	-2					
27TH	349.00									36.4	-54.5	.8	.5	.1
		15.6	-24.9	1275	1275	12.2	-19.5	-4	-2					
EAVE	361.50									20.8	-29.6	.3	.2	.0
		20.8	-29.6	1182	1182	17.6	-25.0	-0	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 260 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									645.3	-1059.7	200.5	110.0	5.8
		40.5	-66.6	4039	4039	10.0	-16.5	-7	-4					
2ND	26.00									604.8	-993.1	173.8	93.8	5.1
		23.2	-34.4	1942	1942	11.9	-17.7	-3	-2					
3RD	38.50									581.6	-958.7	161.6	86.4	5.0
		25.5	-35.4	1942	1942	13.1	-18.2	-1	-0					
4TH	51.00									556.1	-923.3	149.9	79.2	5.0
		29.4	-33.8	1942	1942	15.1	-17.4	1	1					
5TH	63.50									526.7	-889.5	138.5	72.5	5.0
		26.1	-25.4	1942	1942	13.5	-13.1	2	2					
6TH	76.00									500.6	-864.1	127.6	66.1	5.1
		26.2	-32.8	1843	1843	14.2	-17.8	-1	-1					
7TH	88.50									474.4	-831.3	117.0	60.0	5.1
		25.9	-34.5	1817	1817	14.3	-19.0	-2	-2					
8TH	101.00									448.5	-796.7	106.8	54.2	4.9
		25.7	-34.8	1817	1817	14.1	-19.1	-3	-2					
9TH	113.50									422.8	-762.0	97.1	48.8	4.8
		25.5	-35.0	1817	1817	14.0	-19.2	-3	-2					
10TH	126.00									397.3	-727.0	87.8	43.6	4.6
		24.8	-35.2	1817	1817	13.6	-19.4	-4	-3					
11TH	138.50									372.6	-691.8	78.9	38.8	4.4
		23.9	-35.4	1817	1817	13.2	-19.5	-4	-3					
12TH	151.00									348.6	-656.4	70.5	34.3	4.2
		23.1	-35.7	1817	1817	12.7	-19.6	-5	-3					
13TH	163.50									325.5	-620.7	62.5	30.1	3.9
		22.8	-36.2	1817	1817	12.5	-19.9	-5	-3					
14TH	176.00									302.7	-584.5	54.9	26.2	3.7
		22.8	-36.9	1817	1817	12.6	-20.3	-5	-3					
15TH	188.50									279.9	-547.6	47.9	22.5	3.5
		22.9	-37.6	1817	1817	12.6	-20.7	-5	-3					
16TH	201.00									257.0	-510.0	41.3	19.2	3.2
		22.9	-38.3	1817	1817	12.6	-21.1	-5	-3					
17TH	213.50									234.1	-471.7	35.1	16.1	3.0
		22.8	-39.0	1817	1817	12.5	-21.4	-5	-3					
18TH	226.00									211.3	-432.8	29.5	13.3	2.7
		22.6	-39.6	1817	1817	12.5	-21.8	-5	-3					
19TH	238.50									188.7	-393.1	24.3	10.8	2.5
		22.8	-40.9	1817	1817	12.6	-22.5	-5	-3					
20TH	251.00									165.9	-352.2	19.7	8.6	2.2
		24.2	-43.9	1817	1817	13.3	-24.2	-5	-3					
21ST	263.50									141.6	-308.3	15.5	6.7	2.0
		33.2	-60.5	2325	2325	14.3	-26.0	-5	-3					
22ND	279.50									108.4	-247.8	11.1	4.7	1.6
		17.3	-36.8	1570	1570	11.0	-23.4	-7	-3					
23RD	292.00									91.1	-211.1	8.2	3.4	1.3
		24.5	-50.8	2005	2005	12.2	-25.3	-6	-3					
24TH	308.00									66.6	-160.3	5.2	2.2	.9
		13.3	-31.4	1317	1317	10.1	-23.9	-6	-3					
25TH	320.50									53.3	-128.9	3.4	1.4	.7
		17.6	-44.1	1685	1685	10.4	-26.2	-5	-2					
26TH	336.50									35.7	-84.8	1.7	.7	.4
		12.9	-27.9	1276	1276	10.1	-21.9	-4	-2					
27TH	349.00									22.8	-56.9	.8	.3	.3
		9.5	-25.6	1275	1275	7.5	-20.0	-7	-3					
EAVE	361.50									13.3	-31.3	.3	.1	.1
		13.3	-31.3	1182	1182	11.2	-26.5	-2	-1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 270 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									431.1	-1089.2	204.7	69.6	4.6
		34.2	-69.9	4039	4039	8.5	-17.3	-7	-3					
2ND	26.00									396.9	-1019.3	177.3	58.8	3.9
		18.4	-36.8	1942	1942	9.5	-18.9	-3	-2					
3RD	38.50									378.5	-982.5	164.8	54.0	3.8
		19.7	-38.1	1942	1942	10.2	-19.6	-1	-0					
4TH	51.00									358.8	-944.4	152.8	49.4	3.7
		18.3	-34.6	1942	1942	9.4	-17.8	2	1					
5TH	63.50									340.4	-909.9	141.2	45.0	3.9
		15.9	-26.7	1942	1942	8.2	-13.7	5	3					
6TH	76.00									324.5	-883.2	130.0	40.8	4.1
		17.8	-34.5	1843	1843	9.6	-18.7	0	0					
7TH	88.50									306.7	-848.7	119.2	36.9	4.1
		18.0	-35.9	1817	1817	9.9	-19.8	-2	-1					
8TH	101.00									288.7	-812.8	108.8	33.2	4.0
		18.1	-35.8	1817	1817	10.0	-19.7	-3	-1					
9TH	113.50									270.6	-777.0	98.8	29.7	3.9
		18.3	-35.6	1817	1817	10.0	-19.6	-4	-2					
10TH	126.00									252.3	-741.4	89.4	26.4	3.7
		17.8	-35.8	1817	1817	9.8	-19.7	-4	-2					
11TH	138.50									234.6	-705.7	80.3	23.4	3.5
		17.0	-36.1	1817	1817	9.4	-19.9	-4	-2					
12TH	151.00									217.5	-669.5	71.7	20.5	3.4
		16.3	-36.5	1817	1817	9.0	-20.1	-3	-2					
13TH	163.50									201.2	-633.0	63.6	17.9	3.2
		15.7	-37.1	1817	1817	8.6	-20.4	-3	-1					
14TH	176.00									185.5	-596.0	55.9	15.5	3.1
		15.2	-37.8	1817	1817	8.3	-20.8	-4	-1					
15TH	188.50									170.3	-558.2	48.7	13.3	2.9
		14.6	-38.5	1817	1817	8.1	-21.2	-4	-1					
16TH	201.00									155.7	-519.8	41.9	11.2	2.8
		14.2	-39.2	1817	1817	7.8	-21.6	-4	-1					
17TH	213.50									141.5	-480.5	35.7	9.4	2.6
		13.9	-40.1	1817	1817	7.6	-22.1	-4	-1					
18TH	226.00									127.6	-440.4	29.9	7.7	2.4
		13.6	-41.0	1817	1817	7.5	-22.6	-4	-1					
19TH	238.50									114.0	-399.4	24.7	6.2	2.2
		14.0	-42.3	1817	1817	7.7	-23.3	-4	-1					
20TH	251.00									100.0	-357.0	20.0	4.8	2.0
		16.0	-45.1	1817	1817	8.8	-24.8	-4	-1					
21ST	263.50									84.0	-312.0	15.8	3.7	1.8
		23.2	-61.6	2325	2325	10.0	-26.5	-4	-2					
22ND	279.50									60.8	-250.4	11.3	2.5	1.5
		10.0	-37.4	1570	1570	6.4	-23.8	-8	-2					
23RD	292.00									50.8	-213.0	8.4	1.8	1.2
		16.1	-50.7	2005	2005	8.0	-25.3	-6	-2					
24TH	308.00									34.7	-162.3	5.4	1.2	.9
		6.8	-30.7	1317	1317	5.2	-23.4	-7	-1					
25TH	320.50									27.9	-131.5	3.5	.8	.7
		9.0	-43.8	1685	1685	5.4	-26.0	-6	-1					
26TH	336.50									18.9	-87.8	1.8	.4	.4
		6.5	-28.0	1276	1276	5.1	-22.0	-7	-2					
27TH	349.00									12.3	-59.7	.9	.2	.2
		4.9	-27.3	1275	1275	3.8	-21.4	-5	-1					
EAVE	361.50									7.5	-32.4	.3	.1	.1
		7.5	-32.4	1182	1182	6.3	-27.4	-1	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 280 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									268.1	-1018.4	195.9	42.4	2.4
		19.4	-62.2	4039	4039	4.8	-15.4	-8	-2					
2ND	26.00									248.7	-956.2	170.2	35.7	1.9
		10.2	-33.3	1942	1942	5.3	-17.1	-4	-1					
3RD	38.50									238.5	-922.9	158.5	32.6	1.7
		11.2	-34.7	1942	1942	5.8	-17.9	-2	-1					
4TH	51.00									227.2	-888.2	147.1	29.7	1.7
		14.2	-32.3	1942	1942	7.3	-16.6	1	0					
5TH	63.50									213.0	-855.9	136.2	27.0	1.7
		13.8	-24.4	1942	1942	7.1	-12.6	3	1					
6TH	76.00									199.2	-831.5	125.7	24.4	1.8
		13.2	-30.6	1843	1843	7.2	-16.6	0	0					
7TH	88.50									186.0	-800.9	115.5	22.0	1.8
		12.5	-31.8	1817	1817	6.9	-17.5	-0	-0					
8TH	101.00									173.5	-769.1	105.7	19.7	1.8
		11.7	-31.7	1817	1817	6.4	-17.4	-1	-0					
9TH	113.50									161.8	-737.4	96.3	17.6	1.8
		10.9	-31.5	1817	1817	6.0	-17.3	-1	-0					
10TH	126.00									151.0	-705.9	87.2	15.7	1.8
		10.4	-31.9	1817	1817	5.7	-17.5	-1	-0					
11TH	138.50									140.6	-674.1	78.6	13.9	1.7
		10.1	-32.4	1817	1817	5.6	-17.8	-2	-1					
12TH	151.00									130.5	-641.7	70.4	12.2	1.6
		9.8	-33.0	1817	1817	5.4	-18.1	-2	-1					
13TH	163.50									120.7	-608.7	62.6	10.6	1.5
		9.6	-33.7	1817	1817	5.3	-18.5	-3	-1					
14TH	176.00									111.2	-575.0	55.2	9.1	1.5
		9.4	-34.5	1817	1817	5.2	-19.0	-3	-1					
15TH	188.50									101.7	-540.5	48.2	7.8	1.4
		9.3	-35.4	1817	1817	5.1	-19.5	-3	-1					
16TH	201.00									92.5	-505.1	41.7	6.6	1.2
		9.0	-36.3	1817	1817	5.0	-20.0	-3	-1					
17TH	213.50									83.5	-468.9	35.6	5.5	1.1
		8.5	-37.2	1817	1817	4.7	-20.5	-3	-1					
18TH	226.00									74.9	-431.6	30.0	4.5	1.0
		8.1	-38.2	1817	1817	4.4	-21.0	-3	-1					
19TH	238.50									66.9	-393.5	24.8	3.6	.9
		7.8	-39.7	1817	1817	4.3	-21.9	-3	-1					
20TH	251.00									59.0	-353.8	20.1	2.8	.8
		8.6	-43.1	1817	1817	4.7	-23.7	-3	-1					
21ST	263.50									50.4	-310.7	16.0	2.2	.7
		12.3	-60.1	2325	2325	5.3	-25.8	-3	-1					
22ND	279.50									38.2	-250.6	11.5	1.4	.5
		7.6	-35.6	1570	1570	4.8	-22.7	-3	-1					
23RD	292.00									30.6	-215.0	8.6	1.0	.3
		10.5	-50.6	2005	2005	5.3	-25.2	-1	-0					
24TH	308.00									20.1	-164.4	5.5	.6	.3
		4.9	-30.5	1317	1317	3.7	-23.1	-2	-0					
25TH	320.50									15.2	-134.0	3.7	.4	.2
		5.7	-43.5	1685	1685	3.4	-25.8	-3	-0					
26TH	336.50									9.4	-90.5	1.9	.2	.1
		3.4	-27.3	1276	1276	2.7	-21.4	-2	-0					
27TH	349.00									6.0	-63.2	.9	.1	.0
		2.4	-28.3	1275	1275	1.9	-22.2	-1	-0					
EAVE	361.50									3.6	-34.9	.3	.0	-.0
		3.6	-34.9	1182	1182	3.0	-29.5	0	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 290 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-28.8	-993.1	193.4	-7.9	-2.4
		-.9	-58.8	4039	4039	-.2	-14.6	-9	0					
2ND	26.00									-27.9	-934.4	168.3	-7.1	-2.9
		-1.3	-32.1	1942	1942	-.7	-16.6	-4	0					
3RD	38.50									-26.6	-902.2	156.8	-6.8	-3.0
		-1.1	-33.7	1942	1942	-.6	-17.3	-2	0					
4TH	51.00									-25.5	-868.6	145.8	-6.5	-3.1
		.9	-29.1	1942	1942	.5	-15.0	1	0					
5TH	63.50									-26.4	-839.5	135.1	-6.1	-3.1
		2.3	-23.2	1942	1942	1.2	-12.0	3	0					
6TH	76.00									-28.8	-816.2	124.7	-5.8	-3.0
		1.4	-28.8	1843	1843	.8	-15.6	3	0					
7TH	88.50									-30.2	-787.4	114.7	-5.4	-2.9
		1.0	-30.1	1817	1817	.5	-16.6	4	0					
8TH	101.00									-31.2	-757.3	105.1	-5.0	-2.8
		.5	-30.0	1817	1817	.3	-16.5	4	0					
9TH	113.50									-31.6	-727.4	95.8	-4.7	-2.7
		.0	-29.9	1817	1817	.0	-16.5	4	0					
10TH	126.00									-31.7	-697.5	86.9	-4.3	-2.6
		-.3	-30.4	1817	1817	-.2	-16.7	4	-0					
11TH	138.50									-31.4	-667.0	78.3	-3.9	-2.5
		-.5	-31.2	1817	1817	-.3	-17.2	3	-0					
12TH	151.00									-30.9	-635.9	70.2	-3.5	-2.3
		-.7	-31.9	1817	1817	-.4	-17.6	3	-0					
13TH	163.50									-30.1	-603.9	62.5	-3.1	-2.2
		-1.0	-32.8	1817	1817	-.5	-18.0	3	-0					
14TH	176.00									-29.2	-571.2	55.1	-2.7	-2.1
		-1.3	-33.6	1817	1817	-.7	-18.5	3	-0					
15TH	188.50									-27.8	-537.6	48.2	-2.4	-2.0
		-1.6	-34.4	1817	1817	-.9	-19.0	3	-0					
16TH	201.00									-26.2	-503.1	41.7	-2.0	-1.9
		-1.9	-35.5	1817	1817	-1.1	-19.5	3	-0					
17TH	213.50									-24.3	-467.7	35.6	-1.7	-1.8
		-2.2	-36.9	1817	1817	-1.2	-20.3	3	-0					
18TH	226.00									-22.1	-430.8	30.0	-1.4	-1.7
		-2.4	-38.2	1817	1817	-1.3	-21.0	3	-0					
19TH	238.50									-19.7	-392.6	24.8	-1.2	-1.6
		-2.6	-39.9	1817	1817	-1.4	-22.0	3	-0					
20TH	251.00									-17.1	-352.6	20.2	-.9	-1.4
		-2.7	-42.7	1817	1817	-1.5	-23.5	3	-0					
21ST	263.50									-14.4	-309.9	16.0	-.7	-1.3
		-3.4	-58.8	2325	2325	-1.5	-25.3	2	-0					
22ND	279.50									-11.0	-251.2	11.6	-.5	-1.2
		-1.2	-35.2	1570	1570	-.7	-22.4	6	-0					
23RD	292.00									-9.9	-215.9	8.6	-.4	-1.0
		-2.7	-50.0	2005	2005	-1.4	-25.0	4	-0					
24TH	308.00									-7.1	-165.9	5.6	-.3	-.8
		-1.3	-30.5	1317	1317	-1.0	-23.2	5	-0					
25TH	320.50									-5.8	-135.4	3.7	-.2	-.6
		-1.6	-43.8	1685	1685	-.9	-26.0	4	-0					
26TH	336.50									-4.2	-91.5	1.9	-.1	-.5
		-1.4	-28.7	1276	1276	-1.1	-22.5	5	-0					
27TH	349.00									-2.8	-62.8	.9	-.1	-.3
		-.0	-28.0	1275	1275	-.0	-21.9	7	-0					
EAVE	361.50									-2.8	-34.9	.3	-.0	-.1
		-2.8	-34.9	1182	1182	-2.4	-29.5	3	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 300 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-255.9	-893.2	175.5	-55.0	-2.0
		-4.6	-52.4	4039	4039	-1.1	-13.0	-13	1					
2ND	26.00									-251.3	-840.8	153.0	-48.4	-2.7
		-5.1	-29.7	1942	1942	-2.6	-15.3	-7	1					
3RD	38.50									-246.2	-811.1	142.7	-45.3	-2.9
		-6.4	-31.6	1942	1942	-3.3	-16.3	-4	1					
4TH	51.00									-239.8	-779.5	132.7	-42.3	-3.1
		-5.4	-27.1	1942	1942	-2.8	-13.9	-3	1					
5TH	63.50									-234.4	-752.4	123.1	-39.3	-3.1
		-3.0	-20.7	1942	1942	-1.6	-10.7	-1	0					
6TH	76.00									-231.4	-731.7	113.9	-36.4	-3.2
		-6.1	-25.1	1843	1843	-3.3	-13.6	-0	0					
7TH	88.50									-225.3	-706.6	104.9	-33.6	-3.2
		-6.9	-26.0	1817	1817	-3.8	-14.3	1	-0					
8TH	101.00									-218.5	-680.6	96.2	-30.8	-3.2
		-7.3	-25.8	1817	1817	-4.0	-14.2	1	-0					
9TH	113.50									-211.2	-654.8	87.9	-28.1	-3.1
		-7.7	-25.7	1817	1817	-4.2	-14.1	2	-1					
10TH	126.00									-203.5	-629.1	79.8	-25.5	-3.0
		-8.0	-26.3	1817	1817	-4.4	-14.5	3	-1					
11TH	138.50									-195.6	-602.8	72.1	-23.0	-3.0
		-8.2	-27.1	1817	1817	-4.5	-14.9	3	-1					
12TH	151.00									-187.3	-575.7	64.8	-20.6	-2.9
		-8.5	-28.0	1817	1817	-4.7	-15.4	3	-1					
13TH	163.50									-178.8	-547.8	57.8	-18.3	-2.8
		-8.9	-28.9	1817	1817	-4.9	-15.9	3	-1					
14TH	176.00									-169.9	-518.9	51.1	-16.2	-2.7
		-9.5	-29.9	1817	1817	-5.3	-16.5	4	-1					
15TH	188.50									-160.3	-488.9	44.8	-14.1	-2.6
		-10.1	-30.9	1817	1817	-5.6	-17.0	4	-1					
16TH	201.00									-150.2	-458.0	38.9	-12.1	-2.4
		-10.8	-31.8	1817	1817	-6.0	-17.5	4	-2					
17TH	213.50									-139.4	-426.2	33.3	-10.3	-2.2
		-11.7	-32.4	1817	1817	-6.5	-17.9	4	-2					
18TH	226.00									-127.7	-393.8	28.2	-8.7	-2.1
		-12.6	-33.1	1817	1817	-6.9	-18.2	4	-2					
19TH	238.50									-115.1	-360.7	23.5	-7.2	-1.9
		-13.4	-34.2	1817	1817	-7.4	-18.8	4	-2					
20TH	251.00									-101.6	-326.4	19.2	-5.8	-1.8
		-13.7	-36.5	1817	1817	-7.6	-20.1	4	-2					
21ST	263.50									-87.9	-289.9	15.4	-4.6	-1.6
		-17.7	-49.6	2325	2325	-7.6	-21.3	4	-1					
22ND	279.50									-70.2	-240.3	11.1	-3.3	-1.3
		-10.5	-32.3	1570	1570	-6.7	-20.6	7	-2					
23RD	292.00									-59.8	-208.0	8.3	-2.5	-1.1
		-13.6	-46.0	2005	2005	-6.8	-22.9	4	-1					
24TH	308.00									-46.2	-162.1	5.4	-1.7	-.9
		-7.3	-31.4	1317	1317	-5.5	-23.9	6	-1					
25TH	320.50									-38.9	-130.7	3.5	-1.2	-.7
		-9.8	-43.0	1685	1685	-5.8	-25.5	5	-1					
26TH	336.50									-29.0	-87.6	1.8	-.6	-.5
		-9.6	-28.7	1276	1276	-7.5	-22.5	4	-1					
27TH	349.00									-19.5	-58.9	.9	-.3	-.3
		-7.2	-26.8	1275	1275	-5.7	-21.0	8	-2					
EAVE	361.50									-12.2	-32.1	.3	-.1	-.1
		-12.2	-32.1	1182	1182	-10.4	-27.2	2	-1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 310 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-455.0	-658.7	129.0	-93.5	.1
		-15.1	-37.6	4039	4039	-3.7	-9.3	-11	5					
2ND	26.00									-439.9	-621.0	112.3	-81.8	-.4
		-10.8	-22.8	1942	1942	-5.5	-11.8	-8	4					
3RD	38.50									-429.1	-598.2	104.7	-76.4	-.6
		-12.5	-24.9	1942	1942	-6.4	-12.8	-5	3					
4TH	51.00									-416.6	-573.3	97.4	-71.1	-.8
		-12.1	-22.0	1942	1942	-6.3	-11.3	-3	2					
5TH	63.50									-404.5	-551.3	90.4	-66.0	-.8
		-10.1	-18.1	1942	1942	-5.2	-9.3	1	-1					
6TH	76.00									-394.4	-533.1	83.6	-61.0	-.8
		-12.5	-19.6	1843	1843	-6.8	-10.6	-1	1					
7TH	88.50									-382.0	-513.6	77.1	-56.1	-.8
		-13.1	-19.7	1817	1817	-7.2	-10.8	-1	1					
8TH	101.00									-368.9	-493.9	70.8	-51.4	-.9
		-13.5	-19.3	1817	1817	-7.4	-10.6	-1	0					
9TH	113.50									-355.4	-474.6	64.7	-46.9	-.9
		-13.9	-18.9	1817	1817	-7.6	-10.4	-0	0					
10TH	126.00									-341.5	-455.7	58.9	-42.6	-.9
		-14.4	-19.1	1817	1817	-7.9	-10.5	0	-0					
11TH	138.50									-327.1	-436.6	53.3	-38.4	-.9
		-15.0	-19.5	1817	1817	-8.3	-10.7	0	-0					
12TH	151.00									-312.1	-417.1	48.0	-34.4	-.9
		-15.6	-19.8	1817	1817	-8.6	-10.9	1	-1					
13TH	163.50									-296.5	-397.2	42.9	-30.6	-.9
		-16.1	-20.2	1817	1817	-8.9	-11.1	1	-1					
14TH	176.00									-280.4	-377.0	38.1	-27.0	-.8
		-16.5	-20.6	1817	1817	-9.1	-11.4	1	-1					
15TH	188.50									-264.0	-356.4	33.5	-23.6	-.8
		-16.8	-21.1	1817	1817	-9.3	-11.6	2	-1					
16TH	201.00									-247.1	-335.3	29.1	-20.4	-.7
		-17.5	-21.6	1817	1817	-9.6	-11.9	2	-2					
17TH	213.50									-229.7	-313.8	25.1	-17.4	-.6
		-18.6	-22.2	1817	1817	-10.2	-12.2	2	-2					
18TH	226.00									-211.1	-291.5	21.3	-14.6	-.6
		-19.7	-22.9	1817	1817	-10.8	-12.6	2	-1					
19TH	238.50									-191.4	-268.6	17.8	-12.1	-.5
		-20.6	-23.9	1817	1817	-11.4	-13.1	1	-1					
20TH	251.00									-170.7	-244.7	14.6	-9.9	-.4
		-21.1	-25.4	1817	1817	-11.6	-14.0	0	-0					
21ST	263.50									-149.7	-219.3	11.7	-7.9	-.4
		-27.6	-34.6	2325	2325	-11.9	-14.9	-1	1					
22ND	279.50									-122.1	-184.8	8.5	-5.7	-.5
		-16.8	-25.3	1570	1570	-10.7	-16.1	2	-1					
23RD	292.00									-105.2	-159.5	6.3	-4.3	-.4
		-23.3	-35.9	2005	2005	-11.6	-17.9	1	-1					
24TH	308.00									-81.9	-123.6	4.0	-2.8	-.3
		-15.4	-24.8	1317	1317	-11.7	-18.9	3	-2					
25TH	320.50									-66.5	-98.8	2.7	-1.8	-.2
		-20.4	-32.6	1685	1685	-12.1	-19.3	1	-1					
26TH	336.50									-46.0	-66.2	1.3	-.9	-.2
		-14.7	-21.7	1276	1276	-11.5	-17.0	2	-1					
27TH	349.00									-31.3	-44.5	.6	-.5	-.1
		-14.0	-20.4	1275	1275	-11.0	-16.0	3	-2					
EAVE	361.50									-17.3	-24.1	.2	-.2	-.0
		-17.3	-24.1	1182	1182	-14.6	-20.4	1	-1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 320 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-699.4	-652.8	122.8	-138.0	1.1
		-32.8	-39.6	4039	4039	-8.1	-9.8	-1	1					
2ND	26.00									-666.6	-613.2	106.4	-120.3	1.0
		-18.6	-22.2	1942	1942	-9.6	-11.4	-3	3					
3RD	38.50									-648.0	-591.0	98.9	-112.0	.9
		-20.5	-23.6	1942	1942	-10.6	-12.2	-3	3					
4TH	51.00									-627.5	-567.4	91.6	-104.1	.8
		-20.0	-23.2	1942	1942	-10.3	-12.0	-1	1					
5TH	63.50									-607.4	-544.2	84.7	-96.4	.7
		-18.2	-22.3	1942	1942	-9.4	-11.5	2	-1					
6TH	76.00									-589.3	-521.9	78.0	-88.9	.8
		-20.2	-22.3	1843	1843	-10.9	-12.1	-1	1					
7TH	88.50									-569.1	-499.6	71.6	-81.6	.7
		-21.0	-21.7	1817	1817	-11.5	-11.9	-1	1					
8TH	101.00									-548.1	-477.9	65.5	-74.6	.7
		-21.6	-21.2	1817	1817	-11.9	-11.7	-1	1					
9TH	113.50									-526.5	-456.7	59.7	-67.9	.7
		-22.2	-20.8	1817	1817	-12.2	-11.4	-1	1					
10TH	126.00									-504.3	-435.9	54.1	-61.5	.6
		-22.9	-20.7	1817	1817	-12.6	-11.4	-1	1					
11TH	138.50									-481.4	-415.3	48.8	-55.3	.6
		-23.5	-20.7	1817	1817	-12.9	-11.4	-1	1					
12TH	151.00									-457.9	-394.6	43.7	-49.5	.6
		-24.1	-20.8	1817	1817	-13.3	-11.4	-1	1					
13TH	163.50									-433.8	-373.8	38.9	-43.9	.5
		-24.7	-21.0	1817	1817	-13.6	-11.5	-1	1					
14TH	176.00									-409.1	-352.8	34.4	-38.6	.5
		-25.3	-21.2	1817	1817	-13.9	-11.7	-1	1					
15TH	188.50									-383.8	-331.6	30.1	-33.7	.4
		-25.9	-21.4	1817	1817	-14.2	-11.8	-1	1					
16TH	201.00									-357.9	-310.2	26.1	-29.0	.4
		-26.6	-21.8	1817	1817	-14.7	-12.0	-1	1					
17TH	213.50									-331.3	-288.4	22.3	-24.7	.3
		-27.7	-22.5	1817	1817	-15.2	-12.4	-1	1					
18TH	226.00									-303.6	-265.9	18.9	-20.8	.3
		-28.7	-23.1	1817	1817	-15.8	-12.7	-1	1					
19TH	238.50									-274.9	-242.8	15.7	-17.1	.2
		-29.7	-23.8	1817	1817	-16.3	-13.1	-1	1					
20TH	251.00									-245.2	-218.9	12.8	-13.9	.2
		-30.5	-24.6	1817	1817	-16.8	-13.6	-1	1					
21ST	263.50									-214.8	-194.3	10.2	-11.0	.1
		-40.0	-32.7	2325	2325	-17.2	-14.1	-1	1					
22ND	279.50									-174.8	-161.6	7.4	-7.9	.1
		-25.7	-23.2	1570	1570	-16.4	-14.8	0	-0					
23RD	292.00									-149.2	-138.4	5.5	-5.9	.1
		-35.1	-31.8	2005	2005	-17.5	-15.9	-1	1					
24TH	308.00									-114.1	-106.6	3.5	-3.8	.0
		-22.5	-20.8	1317	1317	-17.1	-15.8	-1	1					
25TH	320.50									-91.6	-85.8	2.3	-2.5	.0
		-29.9	-27.4	1685	1685	-17.8	-16.2	-0	0					
26TH	336.50									-61.6	-58.5	1.2	-1.3	-.0
		-20.0	-18.8	1276	1276	-15.6	-14.7	0	-0					
27TH	349.00									-41.7	-39.7	.6	-.6	-.0
		-19.1	-18.1	1275	1275	-14.9	-14.2	-0	0					
EAVE	361.50									-22.6	-21.6	.2	-.2	-.0
		-22.6	-21.6	1182	1182	-19.1	-18.3	0	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 330 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-731.4	-675.2	123.8	-144.1	2.2
		-38.9	-37.6	4039	4039	-9.6	-9.3	4	-4					
2ND	26.00									-692.5	-637.6	106.7	-125.6	2.6
		-21.0	-22.1	1942	1942	-10.8	-11.4	0	-0					
3RD	38.50									-671.5	-615.5	98.9	-117.1	2.6
		-22.3	-24.0	1942	1942	-11.5	-12.4	-1	1					
4TH	51.00									-649.2	-591.5	91.3	-108.8	2.5
		-21.6	-26.2	1942	1942	-11.1	-13.5	2	-1					
5TH	63.50									-627.7	-565.4	84.1	-100.9	2.6
		-18.6	-24.7	1942	1942	-9.6	-12.7	1	-0					
6TH	76.00									-609.1	-540.7	77.2	-93.1	2.6
		-20.6	-24.4	1843	1843	-11.2	-13.2	-0	0					
7TH	88.50									-588.5	-516.3	70.6	-85.6	2.6
		-21.4	-24.2	1817	1817	-11.8	-13.3	-1	1					
8TH	101.00									-567.1	-492.1	64.3	-78.4	2.6
		-21.8	-24.3	1817	1817	-12.0	-13.3	-1	1					
9TH	113.50									-545.3	-467.8	58.3	-71.5	2.5
		-22.2	-24.3	1817	1817	-12.2	-13.4	-1	1					
10TH	126.00									-523.1	-443.5	52.6	-64.8	2.5
		-22.9	-24.1	1817	1817	-12.6	-13.2	-2	2					
11TH	138.50									-500.2	-419.5	47.2	-58.4	2.4
		-23.8	-23.8	1817	1817	-13.1	-13.1	-2	2					
12TH	151.00									-476.4	-395.7	42.1	-52.3	2.3
		-24.6	-23.5	1817	1817	-13.5	-12.9	-3	3					
13TH	163.50									-451.8	-372.3	37.3	-46.5	2.2
		-25.3	-23.2	1817	1817	-13.9	-12.7	-3	3					
14TH	176.00									-426.6	-349.1	32.8	-41.0	2.0
		-25.8	-22.9	1817	1817	-14.2	-12.6	-3	3					
15TH	188.50									-400.7	-326.3	28.6	-35.8	1.9
		-26.4	-22.6	1817	1817	-14.5	-12.4	-3	4					
16TH	201.00									-374.3	-303.7	24.6	-31.0	1.7
		-27.0	-22.7	1817	1817	-14.9	-12.5	-3	4					
17TH	213.50									-347.3	-281.0	21.0	-26.5	1.5
		-27.7	-23.6	1817	1817	-15.2	-13.0	-3	3					
18TH	226.00									-319.6	-257.4	17.6	-22.3	1.4
		-28.4	-24.4	1817	1817	-15.6	-13.5	-2	3					
19TH	238.50									-291.2	-233.0	14.6	-18.5	1.2
		-29.2	-25.3	1817	1817	-16.1	-13.9	-2	2					
20TH	251.00									-262.0	-207.7	11.8	-15.0	1.1
		-30.4	-26.0	1817	1817	-16.8	-14.3	-2	2					
21ST	263.50									-231.6	-181.7	9.4	-11.9	1.0
		-40.6	-34.2	2325	2325	-17.5	-14.7	-2	2					
22ND	279.50									-191.0	-147.6	6.7	-8.6	.8
		-27.7	-21.6	1570	1570	-17.6	-13.8	-3	3					
23RD	292.00									-163.3	-125.9	5.0	-6.3	.7
		-39.2	-29.8	2005	2005	-19.5	-14.8	-3	3					
24TH	308.00									-124.1	-96.2	3.2	-4.0	.5
		-25.3	-18.4	1317	1317	-19.2	-13.9	-2	3					
25TH	320.50									-98.9	-77.8	2.2	-2.6	.4
		-33.5	-23.7	1685	1685	-19.9	-14.1	-2	3					
26TH	336.50									-65.4	-54.1	1.1	-1.3	.2
		-21.2	-17.6	1276	1276	-16.6	-13.8	-2	2					
27TH	349.00									-44.2	-36.5	.5	-.6	.1
		-19.8	-16.2	1275	1275	-15.5	-12.7	-3	4					
EAVE	361.50									-24.4	-20.3	.2	-.2	.0
		-24.4	-20.3	1182	1182	-20.7	-17.1	-0	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 340 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-749.8	-498.8	95.0	-146.9	3.6
		-37.0	-16.0	4039	4039	-9.2	-4.0	3	-6					
2ND	26.00									-712.8	-482.8	82.3	-127.9	3.8
		-21.3	-9.9	1942	1942	-11.0	-5.1	-1	1					
3RD	38.50									-691.5	-472.9	76.3	-119.1	3.8
		-23.7	-10.9	1942	1942	-12.2	-5.6	-1	3					
4TH	51.00									-667.9	-462.1	70.5	-110.6	3.7
		-24.9	-18.3	1942	1942	-12.8	-9.4	4	-6					
5TH	63.50									-643.0	-443.8	64.8	-102.4	3.9
		-19.1	-15.7	1942	1942	-9.8	-8.1	1	-1					
6TH	76.00									-623.9	-428.1	59.3	-94.5	4.0
		-21.7	-19.2	1843	1843	-11.8	-10.4	-1	1					
7TH	88.50									-602.2	-408.9	54.1	-86.8	3.9
		-22.6	-19.8	1817	1817	-12.5	-10.9	-1	1					
8TH	101.00									-579.6	-389.1	49.1	-79.5	3.9
		-22.9	-19.8	1817	1817	-12.6	-10.9	-2	2					
9TH	113.50									-556.7	-369.4	44.4	-72.4	3.8
		-23.2	-19.7	1817	1817	-12.8	-10.9	-2	2					
10TH	126.00									-533.5	-349.7	39.9	-65.5	3.7
		-23.9	-19.4	1817	1817	-13.2	-10.7	-3	3					
11TH	138.50									-509.6	-330.2	35.6	-59.0	3.6
		-24.8	-19.0	1817	1817	-13.7	-10.5	-3	4					
12TH	151.00									-484.8	-311.2	31.6	-52.8	3.4
		-25.8	-18.6	1817	1817	-14.2	-10.3	-4	5					
13TH	163.50									-459.0	-292.6	27.9	-46.9	3.3
		-26.4	-18.6	1817	1817	-14.5	-10.3	-4	5					
14TH	176.00									-432.6	-273.9	24.3	-41.3	3.0
		-26.8	-19.0	1817	1817	-14.7	-10.4	-4	5					
15TH	188.50									-405.8	-254.9	21.0	-36.1	2.8
		-27.2	-19.3	1817	1817	-15.0	-10.6	-4	5					
16TH	201.00									-378.6	-235.6	17.9	-31.2	2.6
		-27.7	-19.8	1817	1817	-15.2	-10.9	-4	5					
17TH	213.50									-350.9	-215.8	15.1	-26.6	2.4
		-28.3	-20.7	1817	1817	-15.6	-11.4	-4	5					
18TH	226.00									-322.6	-195.1	12.6	-22.4	2.2
		-29.0	-21.6	1817	1817	-15.9	-11.9	-4	5					
19TH	238.50									-293.6	-173.5	10.3	-18.6	1.9
		-29.8	-22.4	1817	1817	-16.4	-12.3	-3	4					
20TH	251.00									-263.8	-151.2	8.2	-15.1	1.7
		-31.0	-22.9	1817	1817	-17.1	-12.6	-2	3					
21ST	263.50									-232.8	-128.2	6.5	-12.0	1.6
		-41.0	-30.0	2325	2325	-17.6	-12.9	-1	2					
22ND	279.50									-191.8	-98.2	4.7	-8.6	1.5
		-27.4	-13.5	1570	1570	-17.5	-8.6	-5	9					
23RD	292.00									-164.4	-84.7	3.5	-6.4	1.1
		-39.4	-19.8	2005	2005	-19.7	-9.9	-3	7					
24TH	308.00									-124.9	-64.9	2.3	-4.1	.8
		-24.8	-10.8	1317	1317	-18.8	-8.2	-3	6					
25TH	320.50									-100.2	-54.2	1.6	-2.6	.6
		-34.7	-14.1	1685	1685	-20.6	-8.4	-2	5					
26TH	336.50									-65.5	-40.1	.8	-1.3	.4
		-21.9	-13.1	1276	1276	-17.2	-10.3	-3	5					
27TH	349.00									-43.6	-26.9	.4	-.6	.3
		-19.7	-11.1	1275	1275	-15.5	-8.7	-5	9					
EAVE	361.50									-23.8	-15.8	.1	-.2	.0
		-23.8	-15.8	1182	1182	-20.2	-13.4	-1	1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 350 CONFIGURATION A REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-894.3	-204.4	48.7	-174.1	3.1
		-42.8	13.7	4039	4039	-10.6	3.4	-2	-5					
2ND	26.00									-851.4	-218.1	43.2	-151.4	3.3
		-25.7	4.6	1942	1942	-13.2	2.4	-0	-0					
3RD	38.50									-825.7	-222.8	40.4	-141.0	3.4
		-29.1	3.8	1942	1942	-15.0	2.0	0	1					
4TH	51.00									-796.6	-226.6	37.6	-130.8	3.3
		-29.9	-4.8	1942	1942	-15.4	-2.4	2	-10					
5TH	63.50									-766.7	-221.8	34.8	-121.1	3.6
		-20.9	-1.5	1942	1942	-10.8	-.8	0	-2					
6TH	76.00									-745.8	-220.3	32.0	-111.6	3.7
		-27.5	-5.5	1843	1843	-14.9	-3.0	0	-1					
7TH	88.50									-718.4	-214.8	29.3	-102.4	3.7
		-29.1	-7.2	1817	1817	-16.0	-4.0	0	-0					
8TH	101.00									-689.3	-207.6	26.7	-93.6	3.7
		-29.1	-8.3	1817	1817	-16.0	-4.6	-0	1					
9TH	113.50									-660.2	-199.3	24.1	-85.2	3.7
		-29.1	-9.4	1817	1817	-16.0	-5.2	-0	1					
10TH	126.00									-631.1	-189.9	21.7	-77.1	3.7
		-29.5	-9.9	1817	1817	-16.2	-5.4	-1	2					
11TH	138.50									-601.6	-180.0	19.4	-69.4	3.6
		-30.0	-10.0	1817	1817	-16.5	-5.5	-1	4					
12TH	151.00									-571.6	-170.0	17.2	-62.1	3.5
		-30.5	-10.2	1817	1817	-16.8	-5.6	-2	5					
13TH	163.50									-541.1	-159.9	15.1	-55.2	3.3
		-31.0	-10.3	1817	1817	-17.1	-5.7	-2	5					
14TH	176.00									-510.0	-149.6	13.2	-48.6	3.1
		-31.6	-10.4	1817	1817	-17.4	-5.7	-2	5					
15TH	188.50									-478.4	-139.2	11.4	-42.4	3.0
		-32.1	-10.5	1817	1817	-17.7	-5.8	-2	5					
16TH	201.00									-446.3	-128.6	9.7	-36.6	2.8
		-32.8	-10.8	1817	1817	-18.0	-5.9	-2	5					
17TH	213.50									-413.5	-117.8	8.2	-31.3	2.6
		-33.6	-11.1	1817	1817	-18.5	-6.1	-2	5					
18TH	226.00									-379.9	-106.8	6.8	-26.3	2.4
		-34.5	-11.4	1817	1817	-19.0	-6.3	-2	6					
19TH	238.50									-345.5	-95.3	5.5	-21.8	2.2
		-35.6	-11.9	1817	1817	-19.6	-6.6	-2	5					
20TH	251.00									-309.9	-83.4	4.4	-17.7	2.0
		-37.6	-12.9	1817	1817	-20.7	-7.1	-1	4					
21ST	263.50									-272.2	-70.5	3.4	-14.0	1.8
		-51.2	-17.6	2325	2325	-22.0	-7.6	-1	3					
22ND	279.50									-221.1	-52.9	2.5	-10.1	1.7
		-31.6	-8.1	1570	1570	-20.1	-5.1	-3	10					
23RD	292.00									-189.4	-44.9	1.8	-7.5	1.4
		-43.8	-12.0	2005	2005	-21.8	-6.0	-2	6					
24TH	308.00									-145.6	-32.9	1.2	-4.8	1.0
		-26.7	-4.8	1317	1317	-20.3	-3.7	-1	8					
25TH	320.50									-118.9	-28.0	.8	-3.2	.8
		-40.1	-6.7	1685	1685	-23.8	-4.0	-1	7					
26TH	336.50									-78.8	-21.3	.4	-1.6	.6
		-25.3	-7.2	1276	1276	-19.8	-5.6	-2	7					
27TH	349.00									-53.5	-14.2	.2	-.8	.4
		-24.9	-5.2	1275	1275	-19.5	-4.1	-2	10					
EAVE	361.50									-28.6	-8.9	.1	-.3	.1
		-28.6	-8.9	1182	1182	-24.2	-7.5	-1	4					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. BASE SHEAR AND MOMENT SUMMARY : LPC MANDALAY LAS COLINAS,TEXAS
CONFIGURATION A REFERENCE PRESSURE 25.0 GUST FACTOR 1.32

AZIMUTH	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z	ECCEN (FT) X	ECCEN (FT) Y
0	-928.1	120.9	-9.1	-179.1	.3	0	0
10	-1036.8	309.3	-41.9	-200.9	-4.4	-1	-4
20	-1052.3	610.5	-96.3	-204.2	-5.2	-2	-4
30	-750.4	644.0	-108.0	-145.6	-2.7	-2	-2
40	-730.2	732.1	-126.5	-142.0	-2.3	-2	-2
50	-632.3	768.7	-134.5	-122.5	-.9	-1	-1
60	-368.6	683.9	-120.4	-69.8	2.8	3	2
70	-135.3	553.8	-97.8	-23.2	3.1	5	1
80	14.4	553.5	-99.0	7.0	3.8	7	-0
90	64.2	540.6	-98.8	16.7	2.6	5	-1
100	75.4	527.5	-99.3	17.9	.9	2	-0
110	16.8	500.2	-94.8	6.1	-.0	-0	0
120	-29.9	630.3	-119.1	-4.3	.1	0	0
130	-66.0	285.9	-45.8	-5.5	2.7	9	2
140	-167.3	-37.0	15.8	-22.7	1.6	-2	9
150	-22.8	-117.0	24.9	.7	-2.4	19	-4
160	322.3	-74.1	14.0	65.6	-2.1	1	6
170	570.8	-153.9	28.1	112.9	.5	-0	-1
180	658.9	-36.2	5.1	127.4	-.6	0	1
190	665.1	29.4	-8.8	125.5	-2.6	-0	4
200	679.8	75.3	-19.9	125.9	-4.5	-1	6
210	771.4	-112.4	13.2	141.5	-4.5	1	6
220	780.6	-473.4	80.3	141.6	-3.1	2	3
230	802.7	-620.3	115.5	145.5	-1.8	1	1
240	851.6	-747.5	141.8	155.1	1.1	-1	-1
250	906.1	-950.9	184.4	160.5	2.7	-1	-1
260	645.3	-1059.7	200.5	110.0	5.8	-4	-2
270	431.1	-1089.2	204.7	69.6	4.6	-4	-1
280	268.1	-1018.4	195.9	42.4	2.4	-2	-1
290	-28.8	-993.1	193.4	-7.9	-2.4	2	-0
300	-255.9	-893.2	175.5	-55.0	-2.0	2	-1
310	-455.0	-658.7	129.0	-93.5	.1	-0	0
320	-699.4	-652.8	122.8	-138.0	1.1	-1	1
330	-731.4	-675.2	123.8	-144.1	2.2	-2	2
340	-749.8	-498.8	95.0	-146.9	3.6	-2	3
350	-894.3	-204.4	48.7	-174.1	3.1	-1	3

TABLE 7. LPC MANDALAY LAS COLINAS,TEXAS

PROJECT 6600 CONFIGURATION B

SCALE = 400 REF. PRESSURE = 25.0

GUST FACTOR = 1.32 STANDARD FLOOR HEIGHT = 12.50

NUMBER OF SIDES = 4 NO. OF FLOORS = 28

SIDE	ANGLE	Z-AXIS	SHFACT
1	0.0	2.330	1.0
2	90.0	2.330	1.0
3	180.0	2.330	1.0
4	270.0	2.330	1.0

FLOOR #	LABEL	HEIGHT-FT	WIND AZIMUTH	LOAD FACTOR
1	GRND	26.00	0	.90
2	2ND	12.50	10	.90
3	3RD	12.50	20	.90
4	4TH	12.50	30	.68
5	5TH	12.50	40	.68
6	6TH	12.50	50	.68
7	7TH	12.50	60	.68
8	8TH	12.50	70	.55
9	9TH	12.50	80	.55
10	10TH	12.50	90	.55
11	11TH	12.50	100	.55
12	12TH	12.50	110	.55
13	13TH	12.50	120	.88
14	14TH	12.50	130	.88
15	15TH	12.50	140	.88
16	16TH	12.50	150	.88
17	17TH	12.50	160	.70
18	18TH	12.50	170	.70
19	19TH	12.50	180	.70
20	20TH	12.50	190	.70
21	21ST	16.00	200	.70
22	22ND	12.50	210	.81
23	23RD	16.00	220	.81
24	24TH	12.50	230	.81
25	25TH	16.00	240	.81
26	26TH	12.50	250	1.00
27	27TH	12.50	260	1.00
28	EAVE	18.00	270	1.00
			280	1.00
			290	1.00
			300	.92
			310	.92
			320	.92
			330	.92
			340	.90
			350	.90

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 0 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-962.5	82.0	-19.6	-187.2	5.0
		-42.6	-3.2	4039	4039	-10.6	-.8	-0	3					
2ND	26.00									-919.9	85.2	-17.5	-162.7	4.9
		-27.5	-.2	1942	1942	-14.2	-.1	-0	4					
3RD	38.50									-892.4	85.4	-16.4	-151.4	4.8
		-32.2	.5	1942	1942	-16.6	.2	0	3					
4TH	51.00									-860.1	84.9	-15.3	-140.4	4.7
		-30.4	.3	1942	1942	-15.6	.1	-0	-1					
5TH	63.50									-829.8	84.7	-14.3	-129.9	4.7
		-22.4	1.0	1942	1942	-11.5	.5	-0	-4					
6TH	76.00									-807.4	83.7	-13.2	-119.6	4.8
		-29.0	1.2	1843	1843	-15.7	.6	0	4					
7TH	88.50									-778.4	82.5	-12.2	-109.7	4.7
		-31.0	1.9	1817	1817	-17.1	1.0	0	5					
8TH	101.00									-747.4	80.6	-11.2	-100.2	4.5
		-31.6	2.6	1817	1817	-17.4	1.4	0	5					
9TH	113.50									-715.8	78.0	-10.2	-91.0	4.3
		-32.1	3.3	1817	1817	-17.7	1.8	1	5					
10TH	126.00									-683.7	74.8	-9.2	-82.3	4.2
		-32.7	3.6	1817	1817	-18.0	2.0	1	6					
11TH	138.50									-651.0	71.2	-8.3	-74.0	4.0
		-33.4	3.7	1817	1817	-18.4	2.0	1	6					
12TH	151.00									-617.6	67.5	-7.4	-66.0	3.8
		-34.1	3.8	1817	1817	-18.8	2.1	1	6					
13TH	163.50									-583.5	63.7	-6.6	-58.5	3.5
		-34.7	4.0	1817	1817	-19.1	2.2	1	6					
14TH	176.00									-548.8	59.8	-5.8	-51.4	3.3
		-35.2	4.2	1817	1817	-19.4	2.3	1	6					
15TH	188.50									-513.7	55.6	-5.1	-44.8	3.1
		-35.7	4.4	1817	1817	-19.6	2.4	1	5					
16TH	201.00									-478.0	51.1	-4.5	-38.6	2.9
		-36.2	4.4	1817	1817	-19.9	2.4	1	5					
17TH	213.50									-441.8	46.7	-3.8	-32.9	2.7
		-36.9	4.0	1817	1817	-20.3	2.2	1	6					
18TH	226.00									-404.9	42.8	-3.3	-27.6	2.5
		-37.6	3.6	1817	1817	-20.7	2.0	1	6					
19TH	238.50									-367.3	39.2	-2.8	-22.7	2.3
		-38.7	3.3	1817	1817	-21.3	1.8	1	6					
20TH	251.00									-328.6	35.9	-2.3	-18.4	2.0
		-40.9	3.2	1817	1817	-22.5	1.8	0	6					
21ST	263.50									-287.7	32.7	-1.9	-14.5	1.8
		-55.5	3.8	2325	2325	-23.9	1.6	0	6					
22ND	279.50									-232.2	28.9	-1.4	-10.4	1.5
		-35.2	4.0	1570	1570	-22.4	2.6	1	9					
23RD	292.00									-196.9	24.9	-1.0	-7.7	1.2
		-48.2	4.4	2005	2005	-24.0	2.2	1	7					
24TH	308.00									-148.7	20.5	-.7	-4.9	.8
		-28.9	4.0	1317	1317	-21.9	3.0	1	5					
25TH	320.50									-119.9	16.6	-.4	-3.3	.7
		-40.6	5.1	1685	1685	-24.1	3.0	1	5					
26TH	336.50									-79.3	11.5	-.2	-1.7	.5
		-24.0	3.7	1276	1276	-18.8	2.9	1	8					
27TH	349.00									-55.3	7.8	-.1	-.8	.3
		-24.4	4.4	1275	1275	-19.1	3.5	1	7					
EAVE	361.50									-30.9	3.4	-.0	-.3	.1
		-30.9	3.4	1182	1182	-26.2	2.9	0	3					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 10 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-984.8	15.6	-1.0	-192.3	-1.1
		-41.3	1.8	4039	4039	-10.2	.4	-0	-2					
2ND	26.00									-943.5	13.8	-.6	-167.3	-1.0
		-26.6	1.2	1942	1942	-13.7	.6	0	1					
3RD	38.50									-916.8	12.6	-.5	-155.6	-1.1
		-31.4	1.5	1942	1942	-16.2	.8	0	2					
4TH	51.00									-885.4	11.1	-.3	-144.4	-1.1
		-30.4	1.9	1942	1942	-15.6	1.0	0	1					
5TH	63.50									-855.0	9.3	-.2	-133.5	-1.1
		-22.0	1.5	1942	1942	-11.3	.7	-0	-1					
6TH	76.00									-833.0	7.8	-.1	-123.0	-1.1
		-29.4	1.1	1843	1843	-16.0	.6	-0	-1					
7TH	88.50									-803.6	6.7	-.0	-112.7	-1.1
		-31.8	1.1	1817	1817	-17.5	.6	-0	-1					
8TH	101.00									-771.7	5.6	.1	-102.9	-1.1
		-32.5	1.0	1817	1817	-17.9	.6	-0	-1					
9TH	113.50									-739.2	4.6	.1	-93.4	-1.0
		-33.2	1.0	1817	1817	-18.3	.6	-0	-1					
10TH	126.00									-706.0	3.5	.2	-84.4	-1.0
		-33.9	.9	1817	1817	-18.6	.5	-0	-1					
11TH	138.50									-672.1	2.6	.2	-75.8	-1.0
		-34.5	.8	1817	1817	-19.0	.4	-0	-1					
12TH	151.00									-637.6	1.9	.3	-67.6	-1.0
		-35.1	.6	1817	1817	-19.3	.3	-0	-1					
13TH	163.50									-602.5	1.2	.3	-59.9	-1.0
		-35.9	.6	1817	1817	-19.7	.3	-0	-1					
14TH	176.00									-566.6	.6	.3	-52.5	-.9
		-36.7	.7	1817	1817	-20.2	.4	-0	-1					
15TH	188.50									-529.9	-.0	.3	-45.7	-.9
		-37.6	.7	1817	1817	-20.7	.4	-0	-1					
16TH	201.00									-492.2	-.7	.3	-39.3	-.8
		-38.4	.7	1817	1817	-21.1	.4	-0	-2					
17TH	213.50									-453.9	-1.4	.3	-33.4	-.8
		-39.0	.4	1817	1817	-21.5	.2	-0	-2					
18TH	226.00									-414.9	-1.8	.3	-28.0	-.7
		-39.6	.1	1817	1817	-21.8	.1	-0	-2					
19TH	238.50									-375.3	-1.9	.2	-23.0	-.6
		-40.5	-.1	1817	1817	-22.3	-.0	0	-2					
20TH	251.00									-334.9	-1.8	.2	-18.6	-.6
		-42.6	.1	1817	1817	-23.4	.1	-0	-2					
21ST	263.50									-292.3	-1.9	.2	-14.7	-.5
		-57.8	.6	2325	2325	-24.9	.2	-0	-2					
22ND	279.50									-234.5	-2.5	.1	-10.4	-.4
		-35.4	-.0	1570	1570	-22.5	-.0	0	-1					
23RD	292.00									-199.1	-2.5	.1	-7.7	-.3
		-49.5	-.4	2005	2005	-24.7	-.2	0	-2					
24TH	308.00									-149.7	-2.0	.1	-4.9	-.2
		-29.1	-.3	1317	1317	-22.1	-.2	0	-2					
25TH	320.50									-120.6	-1.7	.1	-3.3	-.2
		-40.7	-1.0	1685	1685	-24.2	-.6	0	-2					
26TH	336.50									-79.8	-.8	.0	-1.7	-.1
		-24.5	.4	1276	1276	-19.2	.3	-0	-1					
27TH	349.00									-55.3	-1.2	.0	-.8	-.1
		-24.8	-.1	1275	1275	-19.4	-.1	0	-1					
EAVE	361.50									-30.6	-1.1	.0	-.3	-.0
		-30.6	-1.1	1182	1182	-25.8	-.9	0	-1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 20 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-953.8	.4	5.4	-185.9	-6.3
		-41.3	7.0	4039	4039	-10.2	1.7	-1	-4					
2ND	26.00									-912.5	-6.7	5.4	-161.6	-6.1
		-26.6	2.6	1942	1942	-13.7	1.4	-0	-3					
3RD	38.50									-885.9	-9.3	5.3	-150.4	-6.0
		-31.4	2.2	1942	1942	-16.2	1.1	-0	-1					
4TH	51.00									-854.6	11.5	5.1	-139.5	-6.0
		-30.7	4.0	1942	1942	-15.8	2.1	0	2					
5TH	63.50									-823.9	-15.4	5.0	-129.0	-6.0
		-23.0	2.1	1942	1942	-11.8	1.1	0	4					
6TH	76.00									-800.9	17.6	4.8	-118.9	-6.1
		-28.3	1.9	1843	1843	-15.4	1.0	-0	-5					
7TH	88.50									-772.6	-19.5	4.5	-109.0	-6.0
		-30.2	1.4	1817	1817	-16.6	.8	-0	-7					
8TH	101.00									-742.4	-20.8	4.3	-99.6	-5.8
		-30.9	.9	1817	1817	-17.0	.5	-0	-7					
9TH	113.50									-711.5	-21.8	4.0	-90.5	-5.5
		-31.6	.5	1817	1817	-17.4	.2	-0	-7					
10TH	126.00									-679.9	-22.2	3.7	-81.8	-5.3
		-32.3	.1	1817	1817	-17.8	.1	-0	-7					
11TH	138.50									-647.6	-22.3	3.5	-73.5	-5.1
		-33.0	-.2	1817	1817	-18.2	-.1	0	-7					
12TH	151.00									-614.6	-22.1	3.2	-65.6	-4.8
		-33.8	-.5	1817	1817	-18.6	-.3	0	-8					
13TH	163.50									-580.8	-21.6	2.9	-58.1	-4.6
		-34.5	-.7	1817	1817	-19.0	-.4	0	-8					
14TH	176.00									-546.3	-20.9	2.6	-51.1	-4.3
		-35.2	-.8	1817	1817	-19.3	-.4	0	-8					
15TH	188.50									-511.2	-20.1	2.4	-44.5	-4.0
		-35.8	-.9	1817	1817	-19.7	-.5	0	-8					
16TH	201.00									-475.4	-19.1	2.1	-38.3	-3.8
		-36.4	-.9	1817	1817	-20.1	-.5	0	-8					
17TH	213.50									-438.9	-18.2	1.9	-32.6	-3.5
		-36.9	-.9	1817	1817	-20.3	-.5	0	-8					
18TH	226.00									-402.0	-17.3	1.7	-27.3	-3.2
		-37.4	-.8	1817	1817	-20.6	-.5	0	-8					
19TH	238.50									-364.6	-16.5	1.5	-22.5	-2.9
		-38.4	-.7	1817	1817	-21.2	-.4	0	-8					
20TH	251.00									-326.1	-15.8	1.3	-18.2	-2.6
		-40.8	-.3	1817	1817	-22.5	-.2	0	-8					
21ST	263.50									-285.3	-15.5	1.1	-14.4	-2.3
		-55.4	.2	2325	2325	-23.8	.1	-0	-7					
22ND	279.50									-229.9	-15.7	.8	-10.3	-1.9
		-34.6	-1.4	1570	1570	-22.0	-.9	0	-11					
23RD	292.00									-195.3	-14.3	.6	-7.6	-1.5
		-47.8	-1.0	2005	2005	-23.8	-.5	0	-9					
24TH	308.00									-147.5	-13.3	.4	-4.9	-1.1
		-28.7	-2.9	1317	1317	-21.8	-2.2	1	-9					
25TH	320.50									-118.9	-10.4	.3	-3.2	-.8
		-40.6	-3.8	1685	1685	-24.1	-2.2	1	-8					
26TH	336.50									-78.3	-6.7	.1	-1.6	-.5
		-24.3	-2.0	1276	1276	-19.1	-1.5	1	-8					
27TH	349.00									-54.0	-4.7	.1	-.8	-.3
		-23.7	-2.9	1275	1275	-18.6	-2.2	1	-8					
EAVE	361.50									-30.3	-1.9	.0	-.3	-.1
		-30.3	-1.9	1182	1182	-25.6	-1.6	0	-4					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 30 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-653.8	234.5	-41.2	-127.2	-5.2
		-29.4	17.4	4039	4039	-7.3	4.3	-2	-4					
2ND	26.00									-624.3	217.1	-35.3	-110.5	-5.0
		-17.9	7.1	1942	1942	-9.2	3.7	-2	-6					
3RD	38.50									-606.4	210.0	-32.7	-102.9	-4.9
		-20.8	6.2	1942	1942	-10.7	3.2	-2	-6					
4TH	51.00									-585.7	203.8	-30.1	-95.4	-4.7
		-21.7	10.4	1942	1942	-11.2	5.3	2	4					
5TH	63.50									-564.0	193.4	-27.6	-88.2	-4.9
		-18.0	8.2	1942	1942	-9.2	4.2	2	4					
6TH	76.00									-546.0	185.2	-25.2	-81.3	-5.0
		-20.1	8.8	1843	1843	-10.9	4.8	-2	-5					
7TH	88.50									-525.8	176.4	-23.0	-74.6	-4.8
		-20.9	8.7	1817	1817	-11.5	4.8	-3	-7					
8TH	101.00									-505.0	167.7	-20.8	-68.1	-4.7
		-21.2	8.5	1817	1817	-11.7	4.7	-3	-7					
9TH	113.50									-483.8	159.1	-18.8	-62.0	-4.5
		-21.6	8.3	1817	1817	-11.9	4.6	-3	-8					
10TH	126.00									-462.1	150.8	-16.8	-56.0	-4.3
		-21.9	8.3	1817	1817	-12.1	4.6	-3	-8					
11TH	138.50									-440.2	142.5	-15.0	-50.4	-4.1
		-22.2	8.4	1817	1817	-12.2	4.6	-3	-8					
12TH	151.00									-418.0	134.2	-13.3	-45.0	-3.9
		-22.5	8.4	1817	1817	-12.4	4.6	-3	-9					
13TH	163.50									-395.6	125.8	-11.6	-40.0	-3.7
		-22.9	8.4	1817	1817	-12.6	4.6	-3	-9					
14TH	176.00									-372.7	117.4	-10.1	-35.2	-3.4
		-23.5	8.4	1817	1817	-12.9	4.6	-3	-9					
15TH	188.50									-349.2	108.9	-8.7	-30.6	-3.2
		-24.0	8.4	1817	1817	-13.2	4.6	-3	-10					
16TH	201.00									-325.2	100.5	-7.4	-26.4	-2.9
		-24.5	8.6	1817	1817	-13.5	4.7	-3	-10					
17TH	213.50									-300.7	92.0	-6.2	-22.5	-2.7
		-24.8	9.0	1817	1817	-13.6	5.0	-3	-9					
18TH	226.00									-276.0	83.0	-5.1	-18.9	-2.4
		-25.0	9.4	1817	1817	-13.8	5.2	-3	-9					
19TH	238.50									-250.9	73.5	-4.1	-15.6	-2.2
		-25.6	10.0	1817	1817	-14.1	5.5	-3	-8					
20TH	251.00									-225.3	63.5	-3.3	-12.6	-1.9
		-27.3	10.5	1817	1817	-15.0	5.8	-2	-6					
21ST	263.50									-198.0	53.1	-2.5	-10.0	-1.7
		-37.4	13.7	2325	2325	-16.1	5.9	-2	-5					
22ND	279.50									-160.6	39.4	-1.8	-7.1	-1.5
		-24.0	5.7	1570	1570	-15.3	3.6	-3	-12					
23RD	292.00									-136.6	33.7	-1.3	-5.3	-1.2
		-33.1	9.2	2005	2005	-16.5	4.6	-2	-9					
24TH	308.00									-103.5	24.6	-.9	-3.4	-.9
		-21.0	4.2	1317	1317	-15.9	3.2	-2	-9					
25TH	320.50									-82.5	20.3	-.6	-2.2	-.7
		-28.9	5.6	1605	1685	-17.1	3.3	-2	-9					
26TH	336.50									-53.6	14.8	-.3	-1.1	-.4
		-17.2	4.9	1276	1276	-13.5	3.9	-2	-7					
27TH	349.00									-36.4	9.8	-.2	-.5	-.3
		-16.2	3.2	1275	1275	-12.7	2.5	-2	-11					
EAVE	361.50									-20.3	6.6	-.1	-.2	-.1
		-20.3	6.6	1182	1182	-17.1	5.6	-1	-3					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 40 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-603.9	449.3	-81.8	-116.3	-4.3
		-29.4	30.2	4039	4039	-7.3	7.5	-2	-2					
2ND	26.00									-574.5	419.1	-70.5	-101.0	-4.2
		-17.1	13.5	1942	1942	-8.8	7.0	-4	-5					
3RD	38.50									-557.4	405.6	-65.3	-93.9	-4.1
		-19.0	12.7	1942	1942	-9.8	6.5	-3	-5					
4TH	51.00									-538.4	392.9	-60.3	-87.1	-3.9
		-19.9	16.9	1942	1942	-10.2	8.7	1	2					
5TH	63.50									-518.5	376.0	-55.5	-80.5	-4.0
		-18.4	15.1	1942	1942	-9.5	7.8	2	2					
6TH	76.00									-500.1	360.9	-50.9	-74.1	-4.0
		-19.0	15.7	1843	1843	-10.3	8.5	-3	-3					
7TH	88.50									-481.0	345.2	-46.5	-68.0	-3.9
		-19.3	15.8	1817	1817	-10.6	8.7	-4	-5					
8TH	101.00									-461.7	329.4	-42.3	-62.1	-3.8
		-19.6	15.7	1817	1817	-10.8	8.7	-4	-5					
9TH	113.50									-442.1	313.6	-38.3	-56.4	-3.6
		-19.8	15.7	1817	1817	-10.9	8.6	-4	-5					
10TH	126.00									-422.3	298.0	-34.5	-51.0	-3.4
		-20.1	15.8	1817	1817	-11.1	8.7	-5	-6					
11TH	138.50									-402.2	282.2	-30.8	-45.9	-3.2
		-20.4	16.0	1817	1817	-11.2	8.8	-5	-6					
12TH	151.00									-381.8	266.2	-27.4	-41.0	-3.0
		-20.8	16.1	1817	1817	-11.4	8.9	-5	-7					
13TH	163.50									-361.0	250.1	-24.2	-36.3	-2.8
		-21.2	16.2	1817	1817	-11.7	8.9	-5	-7					
14TH	176.00									-339.8	233.9	-21.1	-32.0	-2.6
		-21.8	16.3	1817	1817	-12.0	9.0	-5	-6					
15TH	188.50									-318.0	217.6	-18.3	-27.8	-2.4
		-22.4	16.4	1817	1817	-12.3	9.0	-4	-6					
16TH	201.00									-295.6	201.2	-15.7	-24.0	-2.2
		-22.8	16.6	1817	1817	-12.6	9.1	-4	-6					
17TH	213.50									-272.8	184.6	-13.3	-20.5	-2.0
		-23.0	16.9	1817	1817	-12.7	9.3	-4	-6					
18TH	226.00									-249.8	167.7	-11.1	-17.2	-1.8
		-23.2	17.3	1817	1817	-12.8	9.5	-4	-5					
19TH	238.50									-226.6	150.5	-9.1	-14.2	-1.6
		-23.6	17.7	1817	1817	-13.0	9.7	-4	-5					
20TH	251.00									-203.0	132.8	-7.3	-11.5	-1.4
		-24.5	18.1	1817	1817	-13.5	10.0	-3	-4					
21ST	263.50									-178.4	114.7	-5.8	-9.1	-1.2
		-32.7	23.5	2325	2325	-14.0	10.1	-2	-3					
22ND	279.50									-145.8	91.2	-4.1	-6.6	-1.0
		-21.2	13.7	1570	1570	-13.5	8.7	-4	-7					
23RD	292.00									-124.6	77.6	-3.1	-4.9	-.8
		-29.4	18.9	2005	2005	-14.7	9.4	-4	-6					
24TH	308.00									-95.2	58.6	-2.0	-3.1	-.6
		-19.1	11.1	1317	1317	-14.5	8.4	-4	-6					
25TH	320.50									-76.1	47.6	-1.3	-2.0	-.4
		-26.1	14.3	1685	1685	-15.5	8.5	-3	-6					
26TH	336.50									-50.0	33.3	-.7	-1.0	-.2
		-16.2	10.9	1276	1276	-12.7	8.6	-2	-3					
27TH	349.00									-33.8	22.4	-.3	-.5	-.2
		-14.7	9.5	1275	1275	-11.5	7.5	-4	-6					
EAVE	361.50									-19.0	12.9	-.1	-.2	-.0
		-19.0	12.9	1182	1182	-16.1	10.9	-1	-2					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 50 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-569.1	568.6	-103.7	-108.1	-1.3
		-29.0	38.9	4039	4039	-7.2	9.6	0	0					
2ND	26.00									-540.1	529.7	-89.4	-93.7	-1.3
		-16.3	18.7	1942	1942	-8.4	9.6	-1	-1					
3RD	38.50									-523.8	511.0	-82.9	-87.1	-1.2
		-18.0	18.0	1942	1942	-9.3	9.3	-1	-1					
4TH	51.00									-505.8	493.0	-76.6	-80.6	-1.2
		-19.4	20.3	1942	1942	-10.0	10.5	1	1					
5TH	63.50									-486.3	472.7	-70.6	-74.4	-1.2
		-18.6	19.5	1942	1942	-9.6	10.0	1	1					
6TH	76.00									-467.7	453.2	-64.8	-68.5	-1.3
		-18.6	19.4	1843	1843	-10.1	10.5	-2	-2					
7TH	88.50									-449.1	433.8	-59.3	-62.7	-1.2
		-18.7	19.4	1817	1817	-10.3	10.7	-2	-2					
8TH	101.00									-430.4	414.4	-54.0	-57.2	-1.1
		-18.8	19.4	1817	1817	-10.3	10.7	-2	-2					
9TH	113.50									-411.6	395.0	-48.9	-52.0	-1.1
		-18.9	19.4	1817	1817	-10.4	10.7	-2	-2					
10TH	126.00									-392.7	375.6	-44.1	-47.0	-1.0
		-19.3	19.7	1817	1817	-10.6	10.8	-2	-2					
11TH	138.50									-373.5	355.9	-39.5	-42.2	-.9
		-19.7	20.0	1817	1817	-10.9	11.0	-2	-1					
12TH	151.00									-353.8	335.8	-35.2	-37.6	-.9
		-20.2	20.4	1817	1817	-11.1	11.2	-1	-1					
13TH	163.50									-333.5	315.5	-31.1	-33.3	-.8
		-20.4	20.4	1817	1817	-11.2	11.2	-1	-1					
14TH	176.00									-313.1	295.1	-27.3	-29.3	-.8
		-20.5	20.2	1817	1817	-11.3	11.1	-1	-1					
15TH	188.50									-292.6	274.9	-23.7	-25.5	-.7
		-20.5	20.1	1817	1817	-11.3	11.0	-1	-1					
16TH	201.00									-272.1	254.8	-20.4	-22.0	-.7
		-20.8	20.1	1817	1817	-11.4	11.1	-1	-1					
17TH	213.50									-251.3	234.7	-17.4	-18.7	-.6
		-21.4	20.5	1817	1817	-11.8	11.3	-1	-1					
18TH	226.00									-229.9	214.2	-14.6	-15.7	-.6
		-22.1	20.9	1817	1817	-12.1	11.5	-2	-2					
19TH	238.50									-207.8	193.2	-12.0	-12.9	-.5
		-22.7	21.3	1817	1817	-12.5	11.7	-2	-2					
20TH	251.00									-185.1	171.9	-9.7	-10.5	-.4
		-23.1	21.5	1817	1817	-12.7	11.8	-2	-2					
21ST	263.50									-162.1	150.4	-7.7	-8.3	-.3
		-29.8	27.8	2325	2325	-12.8	12.0	-1	-1					
22ND	279.50									-132.2	122.6	-5.5	-6.0	-.2
		-19.4	18.0	1570	1570	-12.4	11.5	-2	-2					
23RD	292.00									-112.8	104.6	-4.1	-4.4	-.2
		-27.1	25.2	2005	2005	-13.5	12.5	-1	-1					
24TH	308.00									-85.7	79.4	-2.6	-2.8	-.1
		-16.7	15.4	1317	1317	-12.6	11.7	-1	-1					
25TH	320.50									-69.0	64.1	-1.7	-1.9	-.1
		-22.2	20.7	1685	1685	-13.2	12.3	-1	-1					
26TH	336.50									-46.8	43.4	-.9	-1.0	-.1
		-15.3	14.2	1276	1276	-12.0	11.1	-1	-1					
27TH	349.00									-31.5	29.2	-.4	-.5	-.0
		-14.0	13.0	1275	1275	-11.0	10.2	-1	-1					
EAVE	361.50									-17.5	16.2	-.1	-.2	-.0
		-17.5	16.2	1182	1182	-14.8	13.7	-0	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 60 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-496.6	623.9	-114.4	-93.2	2.0
		-28.8	42.8	4039	4039	-7.1	10.6	2	1					
2ND	26.00									-467.8	581.1	-98.7	-80.7	1.9
		-15.5	21.6	1942	1942	-8.0	11.1	1	1					
3RD	38.50									-452.3	559.5	-91.6	-74.9	1.8
		-16.6	21.6	1942	1942	-8.6	11.1	2	1					
4TH	51.00									-435.7	537.9	-84.8	-69.4	1.8
		-16.8	21.3	1942	1942	-8.7	11.0	-0	-0					
5TH	63.50									-418.8	516.6	-78.2	-64.1	1.8
		-15.5	20.2	1942	1942	-8.0	10.4	-1	-1					
6TH	76.00									-403.4	496.4	-71.8	-58.9	1.9
		-15.7	21.0	1843	1843	-8.5	11.4	2	1					
7TH	88.50									-387.7	475.4	-65.8	-54.0	1.8
		-15.9	21.1	1817	1817	-8.7	11.6	2	2					
8TH	101.00									-371.9	454.3	-59.9	-49.2	1.7
		-16.2	21.1	1817	1817	-8.9	11.6	2	2					
9TH	113.50									-355.7	433.1	-54.4	-44.7	1.6
		-16.4	21.1	1817	1817	-9.1	11.6	2	2					
10TH	126.00									-339.3	412.0	-49.1	-40.3	1.6
		-16.8	21.3	1817	1817	-9.2	11.7	2	2					
11TH	138.50									-322.5	390.7	-44.1	-36.2	1.5
		-17.2	21.5	1817	1817	-9.4	11.8	3	2					
12TH	151.00									-305.3	369.2	-39.4	-32.3	1.4
		-17.5	21.7	1817	1817	-9.7	11.9	3	2					
13TH	163.50									-287.8	347.6	-34.9	-28.6	1.3
		-17.8	21.6	1817	1817	-9.8	11.9	3	2					
14TH	176.00									-269.9	325.9	-30.7	-25.1	1.2
		-18.0	21.4	1817	1817	-9.9	11.8	2	2					
15TH	188.50									-251.9	304.5	-26.7	-21.8	1.1
		-18.2	21.2	1817	1817	-10.0	11.7	2	2					
16TH	201.00									-233.7	283.3	-23.0	-18.8	1.0
		-18.5	21.3	1817	1817	-10.2	11.7	2	2					
17TH	213.50									-215.2	262.0	-19.6	-16.0	.9
		-18.7	22.0	1817	1817	-10.3	12.1	2	2					
18TH	226.00									-196.5	240.0	-16.5	-13.4	.9
		-19.0	22.7	1817	1817	-10.5	12.5	2	2					
19TH	238.50									-177.4	217.4	-13.6	-11.1	.8
		-19.3	23.3	1817	1817	-10.6	12.8	2	2					
20TH	251.00									-158.2	194.1	-11.1	-9.0	.7
		-19.7	23.6	1817	1817	-10.8	13.0	2	2					
21ST	263.50									-138.5	170.5	-8.8	-7.1	.6
		-25.9	30.6	2325	2325	-11.1	13.2	2	1					
22ND	279.50									-112.6	139.9	-6.3	-5.1	.5
		-16.8	20.6	1570	1570	-10.7	13.1	3	2					
23RD	292.00									-95.8	119.4	-4.7	-3.8	.4
		-22.9	28.4	2005	2005	-11.4	14.2	2	2					
24TH	308.00									-72.9	91.0	-3.0	-2.5	.3
		-13.9	17.4	1317	1317	-10.6	13.3	2	2					
25TH	320.50									-59.0	73.5	-2.0	-1.6	.2
		-18.4	24.3	1685	1685	-10.9	14.4	1	1					
26TH	336.50									-40.6	49.2	-1.0	-.8	.2
		-12.8	16.2	1276	1276	-10.1	12.7	2	2					
27TH	349.00									-27.7	33.0	-.5	-.4	.1
		-12.0	14.7	1275	1275	-9.4	11.5	4	3					
EAVE	361.50									-15.7	18.3	-.2	-.1	.0
		-15.7	18.3	1182	1182	-13.3	15.5	0	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 70 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-290.9	535.5	-98.2	-52.7	3.8
		-21.8	37.5	4039	4039	-5.4	9.3	4	2					
2ND	26.00									-269.2	498.0	-84.7	-45.4	3.6
		-10.7	19.1	1942	1942	-5.5	9.8	3	2					
3RD	38.50									-258.5	478.9	-78.6	-42.1	3.6
		-11.0	19.4	1942	1942	-5.7	10.0	3	2					
4TH	51.00									-247.5	459.5	-72.7	-38.9	3.5
		-9.7	18.4	1942	1942	-5.0	9.5	0	0					
5TH	63.50									-237.9	441.1	-67.1	-35.9	3.5
		-8.2	16.7	1942	1942	-4.2	8.6	-4	-2					
6TH	76.00									-229.7	424.4	-61.7	-33.0	3.6
		-8.8	17.4	1843	1843	-4.8	9.4	5	3					
7TH	88.50									-220.8	407.0	-56.5	-30.2	3.5
		-9.0	17.6	1817	1817	-4.9	9.7	7	4					
8TH	101.00									-211.8	389.4	-51.5	-27.5	3.3
		-9.2	17.8	1817	1817	-5.0	9.8	7	4					
9TH	113.50									-202.7	371.6	-46.8	-24.9	3.1
		-9.3	17.9	1817	1817	-5.1	9.9	7	4					
10TH	126.00									-193.3	353.7	-42.2	-22.4	3.0
		-9.6	18.0	1817	1817	-5.3	9.9	7	4					
11TH	138.50									-183.7	335.7	-37.9	-20.0	2.8
		-9.9	18.1	1817	1817	-5.5	10.0	7	4					
12TH	151.00									-173.8	317.6	-33.9	-17.8	2.6
		-10.3	18.2	1817	1817	-5.7	10.0	7	4					
13TH	163.50									-163.5	299.4	-30.0	-15.7	2.5
		-10.5	18.2	1817	1817	-5.8	10.0	7	4					
14TH	176.00									-153.0	281.2	-26.4	-13.7	2.3
		-10.6	18.3	1817	1817	-5.8	10.1	7	4					
15TH	188.50									-142.4	262.8	-23.0	-11.9	2.1
		-10.7	18.4	1817	1817	-5.9	10.1	7	4					
16TH	201.00									-131.7	244.4	-19.8	-10.2	1.9
		-10.9	18.6	1817	1817	-6.0	10.2	7	4					
17TH	213.50									-120.8	225.8	-16.9	-8.6	1.8
		-11.2	18.9	1817	1817	-6.1	10.4	7	4					
18TH	226.00									-109.6	206.9	-14.2	-7.1	1.6
		-11.4	19.2	1817	1817	-6.3	10.6	7	4					
19TH	238.50									-98.2	187.7	-11.7	-5.8	1.4
		-11.8	19.7	1817	1817	-6.5	10.9	7	4					
20TH	251.00									-86.4	168.0	-9.5	-4.7	1.2
		-12.4	20.6	1817	1817	-6.8	11.3	5	3					
21ST	263.50									-74.0	147.4	-7.5	-3.7	1.1
		-16.4	27.3	2325	2325	-7.1	11.7	4	2					
22ND	279.50									-57.6	120.1	-5.4	-2.6	.9
		-8.7	17.6	1570	1570	-5.5	11.2	9	4					
23RD	292.00									-48.9	102.5	-4.0	-2.0	.7
		-12.3	24.8	2005	2005	-6.1	12.4	6	3					
24TH	308.00									-36.6	77.7	-2.5	-1.3	.5
		-6.7	15.4	1317	1317	-5.1	11.7	7	3					
25TH	320.50									-29.9	62.3	-1.6	-.9	.4
		-8.4	21.8	1685	1685	-5.0	12.9	6	2					
26TH	336.50									-21.5	40.5	-.8	-.4	.3
		-7.0	13.2	1276	1276	-5.5	10.3	5	3					
27TH	349.00									-14.5	27.3	-.4	-.2	.2
		-5.7	12.3	1275	1275	-4.5	9.6	10	4					
EAVE	361.50									-8.8	15.0	-.1	-.1	.0
		-8.8	15.0	1182	1182	-7.4	12.7	2	1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 80 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-98.2	550.5	-101.3	-14.4	4.5
		-15.2	39.4	4039	4039	-3.8	9.8	4	1					
2ND	26.00									-83.0	511.0	-87.5	-12.0	4.3
		-6.7	20.0	1942	1942	-3.5	10.3	3	1					
3RD	38.50									-76.3	491.0	-81.3	-11.0	4.2
		-6.4	20.3	1942	1942	-3.3	10.5	4	1					
4TH	51.00									-69.9	470.6	-75.3	-10.1	4.2
		-3.6	17.7	1942	1942	-1.9	9.1	2	0					
5TH	63.50									-66.3	452.9	-69.5	-9.3	4.1
		-2.2	14.7	1942	1942	-1.1	7.6	-4	-1					
6TH	76.00									-64.2	438.3	-63.9	-8.5	4.2
		-2.7	17.9	1843	1843	-1.5	9.7	7	1					
7TH	88.50									-61.4	420.3	-58.5	-7.7	4.1
		-2.7	18.4	1817	1817	-1.5	10.1	10	1					
8TH	101.00									-58.8	402.0	-53.4	-6.9	3.9
		-2.6	18.2	1817	1817	-1.4	10.0	10	1					
9TH	113.50									-56.2	383.7	-48.5	-6.2	3.7
		-2.5	18.1	1817	1817	-1.4	10.0	10	1					
10TH	126.00									-53.7	365.6	-43.8	-5.5	3.5
		-2.6	18.1	1817	1817	-1.4	10.0	10	1					
11TH	138.50									-51.1	347.5	-39.4	-4.9	3.3
		-2.8	18.2	1817	1817	-1.5	10.0	10	2					
12TH	151.00									-48.3	329.3	-35.1	-4.2	3.1
		-2.9	18.3	1817	1817	-1.6	10.1	10	2					
13TH	163.50									-45.4	311.0	-31.1	-3.7	2.9
		-3.1	18.5	1817	1817	-1.7	10.2	10	2					
14TH	176.00									-42.3	292.5	-27.3	-3.1	2.7
		-3.3	18.7	1817	1817	-1.8	10.3	10	2					
15TH	188.50									-38.9	273.8	-23.8	-2.6	2.5
		-3.5	19.0	1817	1817	-1.9	10.5	10	2					
16TH	201.00									-35.4	254.8	-20.5	-2.1	2.4
		-3.7	19.3	1817	1817	-2.0	10.6	9	2					
17TH	213.50									-31.7	235.5	-17.4	-1.7	2.2
		-3.9	19.8	1817	1817	-2.1	10.9	9	2					
18TH	226.00									-27.8	215.7	-14.6	-1.4	2.0
		-4.0	20.3	1817	1817	-2.2	11.2	9	2					
19TH	238.50									-23.8	195.4	-12.0	-1.0	1.8
		-4.2	21.0	1817	1817	-2.3	11.5	9	2					
20TH	251.00									-19.6	174.4	-9.7	-.8	1.6
		-4.5	21.9	1817	1817	-2.5	12.1	8	2					
21ST	263.50									-15.1	152.5	-7.7	-.5	1.4
		-6.0	29.3	2325	2325	-2.6	12.6	6	1					
22ND	279.50									-9.1	123.2	-5.5	-.3	1.2
		-1.9	18.4	1570	1570	-1.2	11.7	13	1					
23RD	292.00									-7.2	104.8	-4.1	-.2	1.0
		-3.4	25.6	2005	2005	-1.7	12.8	9	1					
24TH	308.00									-3.7	79.3	-2.6	-.2	.7
		-.4	15.3	1317	1317	-.3	11.6	10	0					
25TH	320.50									-3.3	64.0	-1.7	-.1	.6
		-.6	22.4	1685	1685	-.4	13.3	9	0					
26TH	336.50									-2.7	41.6	-.9	-.1	.4
		-1.0	13.4	1276	1276	-.8	10.5	10	1					
27TH	349.00									-1.7	28.2	-.4	-.0	.2
		.3	12.6	1275	1275	.2	9.9	14	-0					
EAVE	361.50									-1.9	15.6	-.1	-.0	.1
		-1.9	15.6	1182	1182	-1.6	13.2	4	1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 90 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									48.9	588.8	-108.3	13.8	2.8
		-11.3	43.5	4039	4039	-2.8	10.8	-1	-0					
2ND	26.00									60.2	545.4	-93.6	12.4	2.8
		-3.9	21.2	1942	1942	-2.0	10.9	0	0					
3RD	38.50									64.1	524.2	-86.9	11.6	2.8
		-3.0	21.1	1942	1942	-1.6	10.9	1	0					
4TH	51.00									67.1	503.1	-80.4	10.8	2.8
		1.6	18.1	1942	1942	.8	9.3	4	-0					
5TH	63.50									65.5	485.0	-74.3	10.0	2.7
		2.2	13.2	1942	1942	1.1	6.8	-7	1					
6TH	76.00									63.3	471.8	-68.3	9.2	2.8
		2.3	19.0	1843	1843	1.2	10.3	6	-1					
7TH	88.50									61.0	452.8	-62.5	8.4	2.7
		2.7	19.9	1817	1817	1.5	11.0	7	-1					
8TH	101.00									58.4	432.9	-57.0	7.7	2.5
		2.9	19.6	1817	1817	1.6	10.8	7	-1					
9TH	113.50									55.5	413.3	-51.7	7.0	2.4
		3.1	19.3	1817	1817	1.7	10.6	7	-1					
10TH	126.00									52.4	394.0	-46.6	6.3	2.3
		3.1	19.6	1817	1817	1.7	10.8	6	-1					
11TH	138.50									49.3	374.4	-41.8	5.6	2.1
		3.0	20.1	1817	1817	1.7	11.1	6	-1					
12TH	151.00									46.3	354.3	-37.3	5.1	2.0
		2.9	20.6	1817	1817	1.6	11.3	6	-1					
13TH	163.50									43.4	333.7	-33.0	4.5	1.9
		2.8	20.9	1817	1817	1.6	11.5	5	-1					
14TH	176.00									40.5	312.8	-28.9	4.0	1.8
		2.7	20.9	1817	1817	1.5	11.5	5	-1					
15TH	188.50									37.8	291.9	-25.2	3.5	1.7
		2.7	21.0	1817	1817	1.5	11.6	5	-1					
16TH	201.00									35.1	270.8	-21.7	3.0	1.6
		2.6	21.2	1817	1817	1.5	11.7	5	-1					
17TH	213.50									32.5	249.6	-18.4	2.6	1.5
		2.7	21.6	1817	1817	1.5	11.9	5	-1					
18TH	226.00									29.8	228.0	-15.4	2.2	1.4
		2.8	21.9	1817	1817	1.6	12.1	5	-1					
19TH	238.50									26.9	206.1	-12.7	1.9	1.2
		2.7	22.4	1817	1817	1.5	12.3	5	-1					
20TH	251.00									24.2	183.7	-10.3	1.5	1.1
		2.2	23.2	1817	1817	1.2	12.8	5	-0					
21ST	263.50									22.0	160.5	-8.1	1.2	1.0
		2.6	31.0	2325	2325	1.1	13.3	5	-0					
22ND	279.50									19.3	129.5	-5.8	.9	.8
		2.7	19.3	1570	1570	1.7	12.3	10	-1					
23RD	292.00									16.6	110.2	-4.3	.7	.7
		2.6	27.2	2005	2005	1.3	13.6	7	-1					
24TH	308.00									14.0	83.0	-2.7	.4	.5
		2.8	15.9	1317	1317	2.1	12.1	7	-1					
25TH	320.50									11.2	67.1	-1.8	.3	.4
		3.8	22.8	1685	1685	2.3	13.5	5	-1					
26TH	336.50									7.4	44.3	-.9	.1	.2
		2.6	13.8	1276	1276	2.0	10.8	7	-1					
27TH	349.00									4.8	30.5	-.4	.1	.1
		2.7	13.6	1275	1275	2.1	10.7	7	-1					
EAVE	361.50									2.2	16.9	-.2	.0	.1
		2.2	16.9	1182	1182	1.8	14.3	3	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 100 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									52.3	601.8	-111.2	11.4	-.5
		-11.7	42.4	4039	4039	-2.9	10.5	-5	-1					
2ND	26.00									64.0	559.4	-96.1	9.9	-.2
		-3.5	20.8	1942	1942	-1.8	10.7	-6	-1					
3RD	38.50									67.6	538.6	-89.3	9.1	-.1
		-2.1	20.9	1942	1942	-1.1	10.7	-5	-1					
4TH	51.00									69.7	517.8	-82.7	8.2	-.0
		3.2	17.9	1942	1942	1.7	9.2	4	-1					
5TH	63.50									66.5	499.8	-76.3	7.4	-.1
		2.6	12.6	1942	1942	1.4	6.5	1	-0					
6TH	76.00									63.9	487.2	-70.1	6.6	-.1
		3.5	18.8	1843	1843	1.9	10.2	2	-0					
7TH	88.50									60.3	468.4	-64.2	5.8	-.1
		4.0	20.2	1817	1817	2.2	11.1	2	-0					
8TH	101.00									56.4	448.2	-58.4	5.1	-.2
		4.2	20.3	1817	1817	2.3	11.2	2	-0					
9TH	113.50									52.1	427.9	-53.0	4.4	-.2
		4.5	20.5	1817	1817	2.5	11.3	2	-0					
10TH	126.00									47.7	407.4	-47.7	3.8	-.3
		4.5	20.8	1817	1817	2.5	11.4	1	-0					
11TH	138.50									43.2	386.6	-42.8	3.2	-.3
		4.4	21.1	1817	1817	2.4	11.6	1	-0					
12TH	151.00									38.8	365.5	-38.1	2.7	-.3
		4.2	21.5	1817	1817	2.3	11.8	1	-0					
13TH	163.50									34.6	344.0	-33.6	2.2	-.3
		4.1	21.8	1817	1817	2.2	12.0	0	-0					
14TH	176.00									30.5	322.2	-29.5	1.8	-.3
		3.8	22.0	1817	1817	2.1	12.1	0	-0					
15TH	188.50									26.7	300.2	-25.6	1.5	-.3
		3.6	22.3	1817	1817	2.0	12.3	-0	0					
16TH	201.00									23.1	278.0	-22.0	1.2	-.3
		3.4	22.5	1817	1817	1.9	12.4	-0	0					
17TH	213.50									19.7	255.5	-18.6	.9	-.3
		3.3	22.6	1817	1817	1.8	12.5	-1	0					
18TH	226.00									16.5	232.9	-15.6	.7	-.3
		3.2	22.8	1817	1817	1.7	12.5	-1	0					
19TH	238.50									13.3	210.1	-12.8	.5	-.3
		3.0	23.2	1817	1817	1.7	12.8	-0	0					
20TH	251.00									10.3	186.9	-10.3	.3	-.3
		2.9	24.3	1817	1817	1.6	13.4	0	-0					
21ST	263.50									7.3	162.6	-8.2	.2	-.3
		3.8	32.4	2325	2325	1.6	13.9	1	-0					
22ND	279.50									3.5	130.2	-5.8	.1	-.3
		1.0	19.7	1570	1570	.6	12.6	-3	0					
23RD	292.00									2.5	110.5	-4.3	.1	-.3
		1.3	27.2	2005	2005	.6	13.6	-2	0					
24TH	308.00									1.3	83.3	-2.8	.1	-.2
		-.3	16.0	1317	1317	-.2	12.2	-3	-0					
25TH	320.50									1.6	67.3	-1.8	.0	-.1
		.3	23.0	1685	1685	.2	13.7	-3	0					
26TH	336.50									1.2	44.2	-.9	.0	-.1
		.7	13.4	1276	1276	.5	10.5	-2	0					
27TH	349.00									.6	30.8	-.5	.0	-.1
		.1	13.7	1275	1275	.0	10.8	-2	0					
EAVE	361.50									.5	17.1	-.2	.0	-.0
		.5	17.1	1182	1182	.4	14.4	-2	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 110 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									48.7	585.7	-107.7	7.8	-3.6
		-8.8	42.5	4039	4039	-2.2	10.5	-9	-2					
2ND	26.00									57.5	543.1	-93.0	6.4	-3.2
		-2.2	21.1	1942	1942	-1.1	10.9	-10	-1					
3RD	38.50									59.7	522.0	-86.3	5.7	-3.0
		-.4	21.4	1942	1942	-.2	11.0	-8	-0					
4TH	51.00									60.1	500.6	-79.9	4.9	-2.8
		4.8	18.1	1942	1942	2.5	9.3	7	-2					
5TH	63.50									55.3	482.5	-73.8	4.2	-2.9
		3.7	12.2	1942	1942	1.9	6.3	8	-2					
6TH	76.00									51.6	470.3	-67.8	3.5	-3.1
		4.1	18.4	1843	1843	2.2	10.0	-1	0					
7TH	88.50									47.5	452.0	-62.1	2.9	-3.0
		4.3	19.5	1817	1817	2.3	10.7	-3	1					
8TH	101.00									43.2	432.4	-56.6	2.3	-3.0
		4.3	19.4	1817	1817	2.4	10.7	-3	1					
9TH	113.50									38.9	413.0	-51.3	1.8	-2.9
		4.4	19.3	1817	1817	2.4	10.6	-4	1					
10TH	126.00									34.6	393.8	-46.2	1.4	-2.8
		4.5	19.6	1817	1817	2.5	10.8	-4	1					
11TH	138.50									30.0	374.2	-41.4	.9	-2.8
		4.7	20.0	1817	1817	2.6	11.0	-5	1					
12TH	151.00									25.4	354.2	-36.9	.6	-2.7
		4.8	20.5	1817	1817	2.6	11.3	-5	1					
13TH	163.50									20.6	333.7	-32.6	.3	-2.5
		4.5	20.9	1817	1817	2.5	11.5	-6	1					
14TH	176.00									16.0	312.8	-28.5	.1	-2.4
		3.9	21.2	1817	1817	2.2	11.7	-6	1					
15TH	188.50									12.1	291.6	-24.8	-.1	-2.3
		3.4	21.6	1817	1817	1.8	11.9	-7	1					
16TH	201.00									8.8	270.0	-21.3	-.2	-2.1
		2.9	21.8	1817	1817	1.6	12.0	-7	1					
17TH	213.50									5.9	248.2	-18.0	-.3	-2.0
		2.5	22.1	1817	1817	1.4	12.2	-7	1					
18TH	226.00									3.3	226.1	-15.0	-.4	-1.8
		2.2	22.3	1817	1817	1.2	12.3	-7	1					
19TH	238.50									1.1	203.8	-12.4	-.4	-1.7
		2.0	22.7	1817	1817	1.1	12.5	-6	1					
20TH	251.00									-.9	181.0	-10.0	-.4	-1.5
		2.2	23.4	1817	1817	1.2	12.9	-6	1					
21ST	263.50									-3.2	157.6	-7.8	-.4	-1.4
		3.1	30.9	2325	2325	1.3	13.3	-6	1					
22ND	279.50									-6.3	126.7	-5.6	-.3	-1.2
		-.7	20.0	1570	1570	-.5	12.7	-12	-0					
23RD	292.00									-5.5	106.7	-4.1	-.2	-.9
		-.3	27.0	2005	2005	-.1	13.4	-10	-0					
24TH	308.00									-5.2	79.7	-2.6	-.1	-.7
		-1.6	15.5	1317	1317	-1.2	11.8	-10	-1					
25TH	320.50									-3.6	64.2	-1.7	-.1	-.5
		-1.4	22.4	1685	1685	-.8	13.3	-9	-1					
26TH	336.50									-2.2	41.8	-.9	-.0	-.3
		-.8	13.1	1276	1276	-.6	10.3	-9	-1					
27TH	349.00									-1.4	28.7	-.4	-.0	-.2
		-1.0	12.5	1275	1275	-.8	9.8	-10	-1					
EAVE	361.50									-.3	16.2	-.1	-.0	-.1
		-.3	16.2	1182	1182	-.3	13.7	-5	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 120 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									387.3	872.8	-158.4	71.9	-6.1
2ND	26.00	4.4	68.0	4039	4039	1.1	16.8	-9	1	382.9	804.9	-136.5	61.9	-5.5
3RD	38.50	5.6	33.2	1942	1942	2.9	17.1	-9	2	377.3	771.7	-126.7	57.1	-5.2
4TH	51.00	8.7	33.2	1942	1942	4.5	17.1	-7	2	368.6	738.5	-117.3	52.5	-5.0
5TH	63.50	16.0	28.7	1942	1942	8.2	14.8	7	-4	352.6	709.9	-108.2	48.0	-5.2
6TH	76.00	12.9	20.8	1942	1942	6.6	10.7	8	-5	339.7	689.1	-99.5	43.6	-5.5
7TH	88.50	15.8	28.3	1843	1843	8.6	15.3	-1	1	323.9	660.8	-91.0	39.5	-5.4
8TH	101.00	16.5	29.4	1817	1817	9.1	16.2	-4	2	307.5	631.4	-82.9	35.5	-5.3
9TH	113.50	16.8	29.1	1817	1817	9.2	16.0	-5	3	290.7	602.3	-75.2	31.8	-5.1
10TH	126.00	17.1	28.8	1817	1817	9.4	15.8	-5	3	273.6	573.5	-67.9	28.3	-4.9
11TH	138.50	17.4	29.0	1817	1817	9.6	16.0	-6	3	256.2	544.5	-60.9	25.0	-4.7
12TH	151.00	17.8	29.4	1817	1817	9.8	16.2	-6	4	238.3	515.1	-54.3	21.9	-4.4
13TH	163.50	18.2	29.8	1817	1817	10.0	16.4	-6	4	220.1	485.3	-48.0	19.0	-4.2
14TH	176.00	18.1	30.1	1817	1817	10.0	16.6	-7	4	202.0	455.2	-42.1	16.4	-3.9
15TH	188.50	17.7	30.2	1817	1817	9.7	16.6	-7	4	184.3	425.0	-36.6	14.0	-3.6
16TH	201.00	17.3	30.4	1817	1817	9.5	16.7	-7	4	167.1	394.6	-31.5	11.8	-3.3
17TH	213.50	17.0	30.7	1817	1817	9.4	16.9	-8	4	150.1	363.8	-26.8	9.8	-3.0
18TH	226.00	17.0	31.3	1817	1817	9.4	17.2	-7	4	133.0	332.6	-22.4	8.0	-2.7
19TH	238.50	17.1	31.8	1817	1817	9.4	17.5	-7	4	115.9	300.8	-18.5	6.4	-2.4
20TH	251.00	17.2	32.5	1817	1817	9.4	17.9	-6	3	98.8	268.3	-14.9	5.1	-2.2
21ST	263.50	17.2	33.7	1817	1817	9.5	18.6	-5	3	81.6	234.5	-11.8	4.0	-2.0
22ND	279.50	21.9	44.7	2325	2325	9.4	19.2	-4	2	59.6	189.9	-8.4	2.9	-1.8
23RD	292.00	7.9	28.9	1570	1570	5.0	18.4	-11	3	51.7	161.0	-6.2	2.2	-1.4
24TH	308.00	12.5	40.2	2005	2005	6.2	20.1	-8	3	39.3	120.8	-3.9	1.4	-1.1
25TH	320.50	6.2	23.9	1317	1317	4.7	18.2	-10	2	33.1	96.8	-2.6	1.0	-.8
26TH	336.50	8.6	33.9	1685	1685	5.1	20.1	-9	2	24.5	62.9	-1.3	.5	-.5
27TH	349.00	8.2	20.6	1276	1276	6.5	16.2	-7	3	16.3	42.3	-.6	.3	-.3
EAVE	361.50	6.0	18.4	1275	1275	4.7	14.5	-11	4	10.3	23.9	-.2	.1	-.1
TOP	379.50	10.3	23.9	1182	1182	8.7	20.2	-3	1	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 130 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									657.8	831.7	-149.2	121.5	-5.3
		22.1	69.1	4039	4039	5.5	17.1	-8	3					
2ND	26.00									635.7	762.6	-128.5	104.7	-4.7
		15.6	33.3	1942	1942	8.1	17.2	-7	3					
3RD	38.50									620.1	729.3	-119.2	96.9	-4.5
		19.3	32.8	1942	1942	9.9	16.9	-5	3					
4TH	51.00									600.7	696.4	-110.3	89.2	-4.2
		25.9	29.6	1942	1942	13.3	15.2	5	-5					
5TH	63.50									574.9	666.9	-101.8	81.9	-4.5
		21.6	25.8	1942	1942	11.1	13.3	4	-4					
6TH	76.00									553.3	641.1	-93.6	74.8	-4.7
		24.4	27.8	1843	1843	13.2	15.1	-2	1					
7TH	88.50									528.9	613.2	-85.7	68.1	-4.6
		25.7	27.4	1817	1817	14.1	15.1	-3	3					
8TH	101.00									503.2	585.8	-78.2	61.6	-4.5
		26.6	26.8	1817	1817	14.6	14.7	-4	4					
9TH	113.50									476.6	559.1	-71.1	55.5	-4.3
		27.5	26.1	1817	1817	15.1	14.4	-4	4					
10TH	126.00									449.1	532.9	-64.3	49.7	-4.0
		27.5	26.2	1817	1817	15.2	14.4	-4	5					
11TH	138.50									421.6	506.8	-57.8	44.3	-3.8
		27.2	26.5	1817	1817	15.0	14.6	-5	5					
12TH	151.00									394.4	480.3	-51.6	39.2	-3.5
		26.8	26.8	1817	1817	14.8	14.8	-5	5					
13TH	163.50									367.6	453.5	-45.8	34.4	-3.3
		26.5	27.1	1817	1817	14.6	14.9	-5	5					
14TH	176.00									341.1	426.4	-40.3	30.0	-3.0
		26.2	27.3	1817	1817	14.4	15.0	-5	5					
15TH	188.50									314.9	399.1	-35.1	25.9	-2.7
		25.9	27.5	1817	1817	14.3	15.2	-5	5					
16TH	201.00									289.0	371.6	-30.3	22.1	-2.5
		25.7	27.9	1817	1817	14.2	15.4	-5	5					
17TH	213.50									263.3	343.6	-25.8	18.7	-2.2
		25.7	28.6	1817	1817	14.2	15.7	-5	4					
18TH	226.00									237.6	315.1	-21.7	15.5	-2.0
		25.7	29.2	1817	1817	14.1	16.1	-5	4					
19TH	238.50									211.9	285.9	-17.9	12.7	-1.7
		25.9	29.9	1817	1817	14.3	16.5	-4	4					
20TH	251.00									186.0	255.9	-14.6	10.2	-1.5
		26.4	30.7	1817	1817	14.5	16.9	-3	3					
21ST	263.50									159.6	225.2	-11.6	8.1	-1.4
		34.0	40.1	2325	2325	14.6	17.2	-2	2					
22ND	279.50									125.6	185.1	-8.3	5.8	-1.2
		18.0	27.1	1570	1570	11.4	17.2	-7	5					
23RD	292.00									107.6	158.0	-6.1	4.3	-1.0
		25.0	38.1	2005	2005	12.5	19.0	-6	4					
24TH	308.00									82.6	119.9	-3.9	2.8	-.7
		15.1	23.9	1317	1317	11.5	18.2	-5	3					
25TH	320.50									67.5	96.0	-2.6	1.9	-.5
		20.5	33.0	1685	1685	12.2	19.6	-4	3					
26TH	336.50									47.0	63.0	-1.3	1.0	-.3
		15.1	20.8	1276	1276	11.8	16.3	-3	2					
27TH	349.00									31.9	42.3	-.6	.5	-.2
		13.9	18.6	1275	1275	10.9	14.6	-6	4					
EAVE	361.50									18.0	23.7	-.2	.2	-.0
		18.0	23.7	1182	1182	15.2	20.0	-1	1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 140 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									799.7	750.6	-134.5	147.4	-1.2
		36.5	61.7	4039	4039	9.0	15.3	-3	2					
2ND	26.00									763.2	688.9	-115.8	127.1	-1.0
		23.0	29.3	1942	1942	11.8	15.1	-2	2					
3RD	38.50									740.2	659.6	-107.4	117.7	-.8
		26.8	29.0	1942	1942	13.8	14.9	-1	1					
4TH	51.00									713.4	630.6	-99.3	108.6	-.8
		30.5	26.6	1942	1942	15.7	13.7	3	-3					
5TH	63.50									682.9	604.1	-91.6	99.9	-1.0
		27.3	25.3	1942	1942	14.1	13.0	3	-3					
6TH	76.00									655.5	578.8	-84.2	91.5	-1.1
		29.1	25.1	1843	1843	15.8	13.6	-1	1					
7TH	88.50									626.4	553.6	-77.1	83.5	-1.1
		29.9	24.7	1817	1817	16.5	13.6	-1	1					
8TH	101.00									596.5	529.0	-70.4	75.9	-1.0
		30.4	24.4	1817	1817	16.8	13.4	-1	2					
9TH	113.50									566.1	504.6	-63.9	68.6	-.9
		31.0	24.1	1817	1817	17.1	13.2	-1	2					
10TH	126.00									535.1	480.5	-57.7	61.7	-.9
		30.8	23.9	1817	1817	17.0	13.2	-1	2					
11TH	138.50									504.2	456.6	-51.9	55.2	-.8
		30.4	23.9	1817	1817	16.7	13.1	-1	1					
12TH	151.00									473.8	432.7	-46.3	49.1	-.7
		30.0	23.8	1817	1817	16.5	13.1	-1	1					
13TH	163.50									443.8	408.9	-41.1	43.4	-.7
		29.7	24.1	1817	1817	16.3	13.3	-1	1					
14TH	176.00									414.1	384.7	-36.1	38.0	-.6
		29.4	24.7	1817	1817	16.2	13.6	-1	1					
15TH	188.50									384.7	360.0	-31.4	33.0	-.6
		29.2	25.3	1817	1817	16.1	13.9	-1	1					
16TH	201.00									355.5	334.8	-27.1	28.4	-.5
		29.0	25.8	1817	1817	16.0	14.2	-1	1					
17TH	213.50									326.5	308.9	-23.1	24.1	-.5
		29.1	26.4	1817	1817	16.0	14.5	-1	1					
18TH	226.00									297.4	282.6	-19.4	20.2	-.4
		29.2	26.9	1817	1817	16.1	14.8	-1	2					
19TH	238.50									268.2	255.7	-16.0	16.7	-.3
		29.4	27.5	1817	1817	16.2	15.1	-1	2					
20TH	251.00									238.8	228.2	-13.0	13.5	-.2
		29.9	28.1	1817	1817	16.5	15.4	-1	1					
21ST	263.50									208.9	200.2	-10.3	10.7	-.2
		39.0	36.4	2325	2325	16.8	15.7	-0	0					
22ND	279.50									169.8	163.7	-7.4	7.7	-.2
		25.4	24.3	1570	1570	16.2	15.5	-1	1					
23RD	292.00									144.4	139.4	-5.5	5.7	-.1
		34.2	32.7	2005	2005	17.1	16.3	-1	1					
24TH	308.00									110.2	106.7	-3.5	3.7	-.1
		20.9	20.7	1317	1317	15.9	15.7	0	-0					
25TH	320.50									89.2	85.9	-2.3	2.4	-.1
		28.6	28.1	1685	1685	17.0	16.7	-1	1					
26TH	336.50									60.6	57.8	-1.2	1.2	-.0
		19.5	18.5	1276	1276	15.3	14.5	-0	0					
27TH	349.00									41.2	39.3	-.6	.6	-.0
		18.1	17.0	1275	1275	14.2	13.3	-1	1					
EAVE	361.50									23.1	22.3	-.2	.2	-.0
		23.1	22.3	1182	1182	19.5	18.9	-0	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 150 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									821.6	692.1	-122.9	155.0	2.7
		40.1	55.8	4039	4039	9.9	13.8	1	-0					
2ND	26.00									781.5	636.3	-105.6	134.1	2.6
		24.6	26.3	1942	1942	12.7	13.5	1	-1					
3RD	38.50									756.9	610.0	-97.8	124.5	2.6
		27.7	26.3	1942	1942	14.3	13.5	1	-1					
4TH	51.00									729.2	583.7	-90.3	115.2	2.5
		28.9	24.9	1942	1942	14.9	12.8	1	-1					
5TH	63.50									700.3	558.9	-83.2	106.3	2.5
		26.5	23.0	1942	1942	13.6	11.8	1	-1					
6TH	76.00									673.8	535.9	-76.4	97.7	2.5
		28.0	23.9	1843	1843	15.2	13.0	1	-2					
7TH	88.50									645.8	512.0	-69.8	89.4	2.4
		28.5	23.5	1817	1817	15.7	13.0	2	-2					
8TH	101.00									617.3	488.5	-63.6	81.5	2.3
		28.8	23.2	1817	1817	15.8	12.8	1	-2					
9TH	113.50									588.5	465.3	-57.6	74.0	2.2
		29.0	22.9	1817	1817	16.0	12.6	1	-2					
10TH	126.00									559.5	442.4	-51.9	66.8	2.1
		29.0	22.9	1817	1817	16.0	12.6	2	-2					
11TH	138.50									530.5	419.5	-46.5	60.0	2.0
		28.9	23.0	1817	1817	15.9	12.7	2	-2					
12TH	151.00									501.6	396.5	-41.4	53.6	1.9
		28.8	23.1	1817	1817	15.8	12.7	2	-2					
13TH	163.50									472.8	373.4	-36.6	47.5	1.8
		28.7	23.3	1817	1817	15.8	12.8	2	-2					
14TH	176.00									444.1	350.2	-32.1	41.8	1.7
		28.7	23.5	1817	1817	15.8	12.9	2	-3					
15TH	188.50									415.4	326.6	-27.9	36.4	1.6
		28.7	23.8	1817	1817	15.8	13.1	2	-3					
16TH	201.00									386.6	302.9	-23.9	31.4	1.4
		29.1	24.1	1817	1817	16.0	13.3	2	-3					
17TH	213.50									357.5	278.7	-20.3	26.7	1.3
		30.0	24.7	1817	1817	16.5	13.6	2	-3					
18TH	226.00									327.5	254.0	-17.0	22.4	1.2
		30.9	25.4	1817	1817	17.0	14.0	2	-3					
19TH	238.50									296.6	228.6	-14.0	18.5	1.0
		31.9	26.0	1817	1817	17.5	14.3	2	-3					
20TH	251.00									264.7	202.6	-11.3	15.0	.9
		32.6	26.6	1817	1817	18.0	14.7	2	-2					
21ST	263.50									232.1	176.0	-8.9	11.9	.7
		42.6	34.7	2325	2325	18.3	14.9	1	-2					
22ND	279.50									189.5	141.3	-6.4	8.5	.6
		27.5	21.4	1570	1570	17.5	13.7	2	-3					
23RD	292.00									162.1	119.8	-4.7	6.3	.5
		38.9	29.3	2005	2005	19.4	14.6	2	-2					
24TH	308.00									123.1	90.5	-3.0	4.1	.4
		23.6	17.5	1317	1317	18.0	13.3	2	-3					
25TH	320.50									99.5	73.0	-2.0	2.7	.3
		33.1	22.4	1685	1685	19.6	13.3	1	-2					
26TH	336.50									66.4	50.6	-1.0	1.3	.2
		21.8	16.6	1276	1276	17.1	13.0	2	-2					
27TH	349.00									44.6	34.0	-.5	.7	.1
		19.9	14.6	1275	1275	15.6	11.4	3	-4					
EAVE	361.50									24.7	19.4	-.2	.2	.0
		24.7	19.4	1182	1182	20.9	16.4	0	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 160 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									693.7	412.0	-70.3	132.5	4.9
2ND	26.00	34.2	34.7	4039	4039	8.5	8.6	3	-3	659.6	377.3	-60.1	114.9	4.6
3RD	38.50	20.9	16.3	1942	1942	10.8	8.4	2	-2	638.7	361.0	-55.4	106.8	4.6
4TH	51.00	23.3	16.5	1942	1942	12.0	8.5	2	-2	615.4	344.5	-51.0	99.0	4.5
5TH	63.50	21.7	16.6	1942	1942	11.2	8.6	-0	0	593.7	327.8	-46.8	91.4	4.5
6TH	76.00	19.6	14.7	1942	1942	10.1	7.6	0	-0	574.1	313.1	-42.8	84.1	4.5
7TH	88.50	21.6	15.3	1843	1843	11.7	8.3	3	-4	552.5	297.8	-39.0	77.1	4.4
8TH	101.00	22.0	14.9	1817	1817	12.1	8.2	4	-6	530.5	282.9	-35.4	70.3	4.2
9TH	113.50	22.1	14.7	1817	1817	12.2	8.1	4	-6	508.4	268.2	-31.9	63.8	4.0
10TH	126.00	22.3	14.4	1817	1817	12.3	7.9	4	-7	486.1	253.9	-28.7	57.6	3.8
11TH	138.50	23.3	14.3	1817	1817	12.8	7.9	4	-7	462.8	239.6	-25.6	51.7	3.6
12TH	151.00	24.7	14.3	1817	1817	13.6	7.9	4	-7	438.1	225.3	-22.7	46.0	3.3
13TH	163.50	26.1	14.3	1817	1817	14.4	7.9	4	-7	412.0	211.0	-20.0	40.7	3.1
14TH	176.00	26.6	14.2	1817	1817	14.6	7.8	4	-7	385.3	196.7	-17.4	35.7	2.9
15TH	188.50	26.4	14.1	1817	1817	14.5	7.8	4	-7	358.9	182.6	-15.0	31.1	2.6
16TH	201.00	26.2	13.9	1817	1817	14.4	7.7	4	-7	332.7	168.7	-12.8	26.8	2.4
17TH	213.50	26.2	14.0	1817	1817	14.4	7.7	4	-7	306.5	154.7	-10.8	22.8	2.2
18TH	226.00	26.4	14.5	1817	1817	14.5	8.0	3	-6	280.1	140.2	-9.0	19.1	2.0
19TH	238.50	26.6	15.0	1817	1817	14.7	8.3	3	-6	253.5	125.2	-7.3	15.8	1.8
20TH	251.00	27.0	15.5	1817	1817	14.9	8.5	3	-5	226.5	109.6	-5.9	12.8	1.6
21ST	263.50	27.6	15.9	1817	1817	15.2	8.8	3	-5	198.8	93.7	-4.6	10.1	1.4
22ND	279.50	36.2	20.8	2325	2325	15.6	8.9	2	-4	162.6	72.9	-3.2	7.2	1.2
23RD	292.00	24.5	11.2	1570	1570	15.6	7.2	4	-9	138.1	61.7	-2.4	5.3	1.0
24TH	308.00	33.8	16.7	2005	2005	16.9	8.3	3	-6	104.3	45.0	-1.6	3.4	.7
25TH	320.50	20.5	8.4	1317	1317	15.6	6.4	3	-6	83.8	36.6	-1.0	2.2	.5
26TH	336.50	29.6	10.7	1685	1685	17.6	6.4	2	-5	54.2	25.9	-.5	1.1	.4
27TH	349.00	17.7	8.4	1276	1276	13.9	6.6	3	-6	36.5	17.4	-.3	.5	.2
EAVE	361.50	15.7	6.6	1275	1275	12.3	5.2	4	-10	20.8	10.8	-.1	.2	.0
TOP	379.50	20.8	10.8	1182	1182	17.6	9.2	1	-2	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 170 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									714.9	184.0	-27.4	136.1	5.2
2ND	26.00	36.8	20.5	4039	4039	9.1	5.1	3	-6	678.1	163.5	-22.9	118.0	4.9
3RD	38.50	22.9	9.7	1942	1942	11.8	5.0	2	-4	655.2	153.7	-20.9	109.6	4.8
4TH	51.00	25.5	10.0	1942	1942	13.1	5.1	2	-4	629.7	143.7	-19.1	101.6	4.7
5TH	63.50	23.0	9.4	1942	1942	11.8	4.8	-0	1	606.7	134.3	-17.3	93.9	4.7
6TH	76.00	18.2	8.0	1942	1942	9.4	4.1	-2	6	588.5	126.4	-15.7	86.4	4.8
7TH	88.50	23.1	7.9	1843	1843	12.5	4.3	1	-4	565.5	118.5	-14.2	79.2	4.7
8TH	101.00	24.2	7.4	1817	1817	13.3	4.1	2	-6	541.3	111.1	-12.7	72.3	4.6
9TH	113.50	24.3	7.2	1817	1817	13.4	3.9	2	-7	516.9	103.9	-11.4	65.7	4.4
10TH	126.00	24.5	6.9	1817	1817	13.5	3.8	2	-8	492.5	97.0	-10.1	59.4	4.2
11TH	138.50	24.4	6.6	1817	1817	13.5	3.6	2	-8	468.0	90.5	-8.9	53.4	4.0
12TH	151.00	24.4	6.2	1817	1817	13.4	3.4	2	-8	443.7	84.2	-7.9	47.7	3.8
13TH	163.50	24.3	5.9	1817	1817	13.4	3.3	2	-8	419.4	78.3	-6.8	42.3	3.5
14TH	176.00	24.5	5.8	1817	1817	13.5	3.2	2	-8	394.9	72.5	-5.9	37.2	3.3
15TH	188.50	24.9	5.8	1817	1817	13.7	3.2	2	-8	370.0	66.8	-5.0	32.4	3.1
16TH	201.00	25.3	5.8	1817	1817	13.9	3.2	2	-8	344.7	61.0	-4.2	27.9	2.9
17TH	213.50	25.8	5.8	1817	1817	14.2	3.2	2	-8	319.0	55.2	-3.5	23.8	2.7
18TH	226.00	26.3	5.8	1817	1817	14.5	3.2	2	-8	292.6	49.5	-2.8	20.0	2.4
19TH	238.50	26.9	5.8	1817	1817	14.8	3.2	2	-8	265.7	43.7	-2.3	16.5	2.2
20TH	251.00	27.8	6.0	1817	1817	15.3	3.3	2	-8	237.8	37.6	-1.8	13.3	2.0
21ST	263.50	29.5	6.7	1817	1817	16.2	3.7	2	-7	208.3	30.9	-1.3	10.5	1.8
22ND	279.50	39.8	9.4	2325	2325	17.1	4.1	1	-6	168.5	21.5	-.9	7.5	1.5
23RD	292.00	25.2	3.9	1570	1570	16.1	2.5	2	-12	143.3	17.6	-.7	5.6	1.2
24TH	308.00	34.9	5.9	2005	2005	17.4	3.0	1	-8	108.4	11.6	-.4	3.6	.9
25TH	320.50	21.1	2.0	1317	1317	16.0	1.5	1	-9	87.3	9.6	-.3	2.3	.7
26TH	336.50	30.0	2.3	1685	1685	17.8	1.4	1	-8	57.3	7.3	-.2	1.2	.5
27TH	349.00	18.0	2.5	1276	1276	14.1	1.9	1	-10	39.3	4.8	-.1	.6	.3
EAVE	361.50	17.7	1.0	1275	1275	13.9	.8	1	-12	21.6	3.8	-.0	.2	.1
TOP	379.50	21.6	3.8	1182	1182	18.3	3.2	1	-3	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 180 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									744.6	-16.5	8.0	141.7	2.6
		37.1	3.6	4039	4039	9.2	.9	0	-2					
2ND	26.00									707.5	-20.1	7.6	122.8	2.5
		23.3	2.1	1942	1942	12.0	1.1	0	-1					
3RD	38.50									684.3	-22.2	7.3	114.1	2.5
		26.8	2.4	1942	1942	13.8	1.3	0	-1					
4TH	51.00									657.5	-24.6	7.0	105.8	2.5
		22.9	1.7	1942	1942	11.8	.9	-0	3					
5TH	63.50									634.6	-26.4	6.7	97.7	2.5
		16.6	1.5	1942	1942	8.5	.7	-0	5					
6TH	76.00									618.0	-27.8	6.4	89.9	2.6
		23.7	1.1	1843	1843	12.9	.6	0	-2					
7TH	88.50									594.3	-28.9	6.0	82.3	2.6
		25.3	.7	1817	1817	14.0	.4	0	-3					
8TH	101.00									569.0	-29.6	5.6	75.0	2.5
		25.6	.6	1817	1817	14.1	.3	0	-3					
9TH	113.50									543.4	-30.2	5.3	68.1	2.5
		25.8	.5	1817	1817	14.2	.3	0	-3					
10TH	126.00									517.7	-30.7	4.9	61.4	2.4
		26.1	.2	1817	1817	14.4	.1	0	-3					
11TH	138.50									491.5	-30.9	4.5	55.1	2.3
		26.5	-.1	1817	1817	14.6	-.0	-0	-3					
12TH	151.00									465.0	-30.8	4.1	49.1	2.2
		26.9	-.3	1817	1817	14.8	-.2	-0	-4					
13TH	163.50									438.1	-30.5	3.7	43.5	2.1
		27.2	-.6	1817	1817	15.0	-.3	-0	-4					
14TH	176.00									411.0	-29.9	3.3	38.2	2.0
		27.3	-.9	1817	1817	15.0	-.5	-0	-4					
15TH	188.50									383.7	-29.0	3.0	33.2	1.9
		27.5	-1.2	1817	1817	15.1	-.7	-0	-4					
16TH	201.00									356.2	-27.8	2.6	28.6	1.8
		27.7	-1.5	1817	1817	15.2	-.8	-0	-4					
17TH	213.50									328.5	-26.3	2.3	24.3	1.7
		28.0	-1.6	1817	1817	15.4	-.9	-0	-4					
18TH	226.00									300.5	-24.7	2.0	20.4	1.6
		28.4	-1.8	1817	1817	15.6	-1.0	-0	-4					
19TH	238.50									272.1	-22.9	1.7	16.8	1.4
		29.0	-1.8	1817	1817	16.0	-1.0	-0	-4					
20TH	251.00									243.1	-21.1	1.4	13.6	1.3
		30.6	-1.5	1817	1817	16.9	-.8	-0	-4					
21ST	263.50									212.5	-19.6	1.1	10.7	1.2
		41.5	-1.6	2325	2325	17.8	-.7	-0	-4					
22ND	279.50									171.0	-18.0	.8	7.7	1.0
		25.4	-2.5	1570	1570	16.2	-1.6	-1	-9					
23RD	292.00									145.6	-15.5	.6	5.7	.8
		35.6	-2.7	2005	2005	17.8	-1.3	-0	-6					
24TH	308.00									110.0	-12.8	.4	3.6	.6
		21.1	-2.6	1317	1317	16.0	-2.0	-1	-5					
25TH	320.50									88.9	-10.2	.3	2.4	.5
		30.2	-3.5	1685	1685	17.9	-2.0	-1	-5					
26TH	336.50									58.7	-6.7	.1	1.2	.3
		17.7	-2.3	1276	1276	13.9	-1.8	-1	-7					
27TH	349.00									40.9	-4.4	.1	.6	.2
		18.2	-2.5	1275	1275	14.3	-2.0	-1	-7					
EAVE	361.50									22.7	-1.9	.0	.2	.1
		22.7	-1.9	1182	1182	19.2	-1.6	-0	-3					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 190 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									746.2	74.4	-17.0	142.3	-2.5
		36.5	-2.1	4039	4039	9.0	-.5	0	4					
2ND	26.00									709.7	76.5	-15.0	123.3	-2.3
		23.5	-.7	1942	1942	12.1	-.3	0	4					
3RD	38.50									686.2	77.2	-14.1	114.6	-2.2
		27.0	-.5	1942	1942	13.9	-.2	0	3					
4TH	51.00									659.3	77.6	-13.1	106.2	-2.1
		22.7	1.2	1942	1942	11.7	.6	-0	3					
5TH	63.50									636.6	76.4	-12.1	98.1	-2.1
		17.0	1.5	1942	1942	8.8	.8	0	-5					
6TH	76.00									619.5	74.9	-11.2	90.2	-2.1
		23.8	2.2	1843	1843	12.9	1.2	-0	4					
7TH	88.50									595.7	72.7	-10.3	82.7	-2.0
		25.3	2.4	1817	1817	14.0	1.3	-0	5					
8TH	101.00									570.4	70.3	-9.4	75.4	-1.9
		25.6	2.5	1817	1817	14.1	1.4	-0	5					
9TH	113.50									544.8	67.9	-8.5	68.4	-1.8
		25.8	2.5	1817	1817	14.2	1.4	-0	4					
10TH	126.00									519.0	65.3	-7.7	61.7	-1.7
		26.0	2.8	1817	1817	14.3	1.5	-0	4					
11TH	138.50									492.9	62.5	-6.9	55.4	-1.6
		26.2	3.1	1817	1817	14.4	1.7	-0	3					
12TH	151.00									466.7	59.4	-6.1	49.4	-1.5
		26.4	3.5	1817	1817	14.5	1.9	-0	3					
13TH	163.50									440.4	55.9	-5.4	43.8	-1.4
		26.7	3.6	1817	1817	14.7	2.0	-0	3					
14TH	176.00									413.6	52.2	-4.7	38.4	-1.3
		27.2	3.7	1817	1817	15.0	2.0	-0	3					
15TH	188.50									386.4	48.6	-4.1	33.4	-1.2
		27.7	3.7	1817	1817	15.2	2.0	-0	3					
16TH	201.00									358.7	44.9	-3.5	28.8	-1.2
		28.1	3.8	1817	1817	15.5	2.1	-0	3					
17TH	213.50									330.6	41.1	-3.0	24.5	-1.1
		28.4	3.9	1817	1817	15.6	2.2	-0	3					
18TH	226.00									302.2	37.2	-2.5	20.5	-1.0
		28.7	4.1	1817	1817	15.8	2.2	-0	3					
19TH	238.50									273.5	33.1	-2.0	16.9	-.9
		29.3	4.1	1817	1817	16.1	2.3	-0	3					
20TH	251.00									244.2	29.0	-1.7	13.7	-.8
		30.7	3.8	1817	1817	16.9	2.1	-0	4					
21ST	263.50									213.5	25.2	-1.3	10.8	-.7
		41.3	4.5	2325	2325	17.8	1.9	-1	5					
22ND	279.50									172.2	20.7	-.9	7.7	-.5
		25.7	3.2	1570	1570	16.3	2.0	-0	4					
23RD	292.00									146.5	17.6	-.7	5.7	-.4
		36.1	3.5	2005	2005	18.0	1.8	-0	3					
24TH	308.00									110.4	14.0	-.5	3.7	-.3
		20.8	2.6	1317	1317	15.8	2.0	-0	3					
25TH	320.50									89.6	11.4	-.3	2.4	-.2
		30.3	3.6	1685	1685	18.0	2.2	-0	2					
26TH	336.50									59.3	7.8	-.1	1.2	-.1
		18.2	2.8	1276	1276	14.3	2.2	-0	2					
27TH	349.00									41.1	4.9	-.1	.6	-.1
		18.5	2.9	1275	1275	14.5	2.3	-0	3					
EAVE	361.50									22.7	2.1	-.0	.2	-.0
		22.7	2.1	1182	1182	19.2	1.7	-0	1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 200 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									733.1	-87.2	6.3	140.0	-4.9
		37.9	-20.7	4039	4039	9.4	-5.1	2	4					
2ND	26.00									695.3	-66.5	4.3	121.4	-4.7
		23.1	-9.7	1942	1942	11.9	-5.0	2	5					
3RD	38.50									672.2	-56.8	3.6	112.9	-4.6
		25.9	-9.3	1942	1942	13.3	-4.8	1	4					
4TH	51.00									646.3	-47.5	2.9	104.6	-4.5
		22.9	-7.1	1942	1942	11.8	-3.6	0	0					
5TH	63.50									623.4	-40.5	2.3	96.7	-4.5
		18.9	-6.1	1942	1942	9.7	-3.2	-1	-3					
6TH	76.00									604.5	-34.3	1.9	89.0	-4.5
		23.0	-5.7	1843	1843	12.5	-3.1	1	6					
7TH	88.50									581.5	-28.6	1.5	81.6	-4.4
		24.1	-4.8	1817	1817	13.2	-2.7	1	7					
8TH	101.00									557.4	-23.8	1.2	74.5	-4.2
		24.4	-4.1	1817	1817	13.4	-2.3	1	7					
9TH	113.50									533.1	-19.6	.9	67.7	-4.0
		24.7	-3.4	1817	1817	13.6	-1.9	1	7					
10TH	126.00									508.4	-16.2	.7	61.2	-3.9
		25.0	-2.9	1817	1817	13.7	-1.6	1	7					
11TH	138.50									483.4	-13.3	.5	55.0	-3.7
		25.3	-2.4	1817	1817	13.9	-1.3	1	7					
12TH	151.00									458.2	-10.9	.3	49.1	-3.5
		25.5	-1.9	1817	1817	14.1	-1.0	0	7					
13TH	163.50									432.7	-9.0	.2	43.5	-3.3
		25.8	-1.5	1817	1817	14.2	-.8	0	7					
14TH	176.00									406.8	-7.6	.1	38.3	-3.2
		26.1	-1.1	1817	1817	14.4	-.6	0	7					
15TH	188.50									380.8	-6.4	.0	33.4	-3.0
		26.3	-.8	1817	1817	14.5	-.4	0	8					
16TH	201.00									354.4	-5.7	-.1	28.8	-2.8
		26.7	-.7	1817	1817	14.7	-.4	0	8					
17TH	213.50									327.7	-5.0	-.1	24.5	-2.6
		27.1	-.9	1817	1817	14.9	-.5	0	8					
18TH	226.00									300.6	-4.0	-.2	20.6	-2.3
		27.6	-1.2	1817	1817	15.2	-.7	0	8					
19TH	238.50									273.0	-2.8	-.2	17.0	-2.1
		28.4	-1.5	1817	1817	15.6	-.8	0	8					
20TH	251.00									244.6	-1.4	-.3	13.8	-1.9
		30.2	-1.8	1817	1817	16.6	-1.0	0	7					
21ST	263.50									214.4	.4	-.3	10.9	-1.7
		41.0	-2.9	2325	2325	17.6	-1.2	0	6					
22ND	279.50									173.4	3.3	-.2	7.8	-1.4
		26.1	.2	1570	1570	16.6	.1	-0	11					
23RD	292.00									147.3	3.1	-.2	5.8	-1.2
		35.5	-1.5	2005	2005	17.7	-.8	0	8					
24TH	308.00									111.8	4.6	-.1	3.7	-.9
		21.5	1.0	1317	1317	16.3	.8	-0	9					
25TH	320.50									90.4	3.6	-.1	2.4	-.7
		30.4	1.4	1685	1685	18.0	.9	-0	8					
26TH	336.50									60.0	2.1	-.0	1.2	-.4
		18.7	.7	1276	1276	14.6	.5	-0	9					
27TH	349.00									41.3	1.5	-.0	.6	-.3
		18.5	1.5	1275	1275	14.5	1.2	-1	9					
EAVE	361.50									22.9	.0	-.0	.2	-.1
		22.9	.0	1182	1182	19.3	.0	-0	4					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 210 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									740.2	-383.8	61.2	142.7	-4.4
		36.7	-36.5	4039	4039	9.1	-9.0	0	0					
2ND	26.00									703.6	-347.3	51.7	124.0	-4.4
		22.3	-18.6	1942	1942	11.5	-9.6	1	1					
3RD	38.50									681.3	-328.7	47.5	115.3	-4.4
		25.2	-18.8	1942	1942	13.0	-9.7	1	1					
4TH	51.00									656.1	-309.9	43.5	107.0	-4.3
		24.0	-17.2	1942	1942	12.4	-8.9	-1	-1					
5TH	63.50									632.1	-292.8	39.7	98.9	-4.4
		21.4	-15.3	1942	1942	11.0	-7.9	1	1					
6TH	76.00									610.7	-277.5	36.2	91.1	-4.4
		23.6	-15.3	1843	1843	12.8	-8.3	2	3					
7TH	88.50									587.0	-262.1	32.8	83.7	-4.3
		24.1	-14.9	1817	1817	13.3	-8.2	2	4					
8TH	101.00									562.9	-247.3	29.6	76.5	-4.1
		24.2	-14.5	1817	1817	13.3	-8.0	2	4					
9TH	113.50									538.7	-232.8	26.6	69.6	-4.0
		24.3	-14.1	1817	1817	13.4	-7.8	2	4					
10TH	126.00									514.4	-218.6	23.8	63.0	-3.9
		24.5	-13.8	1817	1817	13.5	-7.6	3	5					
11TH	138.50									489.9	-204.8	21.2	56.7	-3.7
		24.7	-13.5	1817	1817	13.6	-7.4	3	5					
12TH	151.00									465.2	-191.3	18.7	50.7	-3.6
		24.9	-13.2	1817	1817	13.7	-7.3	3	5					
13TH	163.50									440.3	-178.1	16.4	45.1	-3.4
		25.2	-12.9	1817	1817	13.9	-7.1	3	6					
14TH	176.00									415.1	-165.2	14.2	39.7	-3.2
		25.4	-12.6	1817	1817	14.0	-7.0	3	6					
15TH	188.50									389.7	-152.6	12.2	34.7	-3.0
		25.7	-12.3	1817	1817	14.1	-6.8	3	7					
16TH	201.00									364.0	-140.2	10.4	30.0	-2.8
		26.2	-12.3	1817	1817	14.4	-6.8	3	7					
17TH	213.50									337.8	-128.0	8.7	25.6	-2.6
		27.0	-12.6	1817	1817	14.8	-6.9	3	7					
18TH	226.00									310.9	-115.4	7.2	21.6	-2.3
		27.8	-12.9	1817	1817	15.3	-7.1	3	7					
19TH	238.50									283.1	-102.5	5.9	17.8	-2.1
		28.9	-13.2	1817	1817	15.9	-7.3	3	6					
20TH	251.00									254.2	-89.3	4.7	14.5	-1.9
		30.4	-13.8	1817	1817	16.7	-7.6	2	6					
21ST	263.50									223.8	-75.5	3.6	11.5	-1.7
		40.8	-18.2	2325	2325	17.6	-7.8	2	5					
22ND	279.50									183.0	-57.3	2.6	8.2	-1.5
		26.4	-8.4	1570	1570	16.8	-5.4	3	10					
23RD	292.00									156.6	-48.9	1.9	6.1	-1.2
		37.6	-13.5	2005	2005	18.8	-6.8	2	6					
24TH	308.00									119.0	-35.3	1.2	3.9	-.9
		23.2	-6.6	1317	1317	17.6	-5.0	2	8					
25TH	320.50									95.8	-28.8	.8	2.6	-.7
		32.6	-8.4	1685	1685	19.3	-5.0	2	8					
26TH	336.50									63.2	-20.3	.4	1.3	-.4
		20.1	-6.7	1276	1276	15.7	-5.3	2	6					
27TH	349.00									43.1	-13.6	.2	.6	-.3
		18.4	-4.9	1275	1275	14.4	-3.9	3	12					
EAVE	361.50									24.7	-8.7	.1	.2	-.1
		24.7	-8.7	1182	1182	20.9	-7.3	1	2					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 220 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									724.9	-641.7	112.8	138.7	-2.5
		36.8	-47.8	4039	4039	9.1	-11.8	-1	-0					
2ND	26.00									688.1	-593.9	96.8	120.3	-2.5
		21.6	-24.0	1942	1942	11.1	-12.4	1	1					
3RD	38.50									666.5	-569.9	89.5	111.9	-2.5
		23.9	-24.2	1942	1942	12.3	-12.5	1	1					
4TH	51.00									642.6	-545.7	82.5	103.7	-2.4
		25.2	-23.9	1942	1942	13.0	-12.3	-0	-0					
5TH	63.50									617.4	-521.8	75.9	95.8	-2.4
		22.4	-21.4	1942	1942	11.5	-11.0	1	1					
6TH	76.00									595.1	-500.4	69.5	88.2	-2.4
		23.4	-23.0	1843	1843	12.7	-12.5	1	1					
7TH	88.50									571.7	-477.4	63.4	80.9	-2.3
		23.8	-23.1	1817	1817	13.1	-12.7	1	1					
8TH	101.00									547.9	-454.3	57.5	73.9	-2.3
		24.1	-23.0	1817	1817	13.3	-12.6	1	1					
9TH	113.50									523.8	-431.4	52.0	67.2	-2.2
		24.3	-22.8	1817	1817	13.4	-12.6	1	2					
10TH	126.00									499.5	-408.5	46.8	60.8	-2.2
		24.5	-22.8	1817	1817	13.5	-12.5	2	2					
11TH	138.50									475.0	-385.7	41.8	54.8	-2.1
		24.6	-22.8	1817	1817	13.6	-12.5	1	2					
12TH	151.00									450.3	-363.0	37.1	49.0	-2.0
		24.8	-22.7	1817	1817	13.6	-12.5	1	2					
13TH	163.50									425.6	-340.2	32.7	43.5	-1.9
		24.8	-22.6	1817	1817	13.7	-12.4	2	2					
14TH	176.00									400.7	-317.6	28.6	38.3	-1.9
		24.9	-22.4	1817	1817	13.7	-12.4	2	2					
15TH	188.50									375.8	-295.2	24.8	33.5	-1.8
		25.0	-22.3	1817	1817	13.7	-12.3	2	2					
16TH	201.00									350.9	-272.9	21.2	28.9	-1.7
		25.3	-22.4	1817	1817	13.9	-12.3	2	3					
17TH	213.50									325.6	-250.5	18.0	24.7	-1.5
		26.1	-22.9	1817	1817	14.4	-12.6	2	3					
18TH	226.00									299.5	-227.6	15.0	20.8	-1.4
		26.9	-23.5	1817	1817	14.8	-12.9	3	3					
19TH	238.50									272.6	-204.1	12.3	17.2	-1.3
		27.8	-24.1	1817	1817	15.3	-13.3	2	3					
20TH	251.00									244.8	-180.0	9.9	14.0	-1.1
		29.2	-24.7	1817	1817	16.0	-13.6	2	2					
21ST	263.50									215.6	-155.3	7.8	11.1	-1.0
		39.0	-32.1	2325	2325	16.8	-13.8	2	2					
22ND	279.50									176.6	-123.2	5.5	8.0	-.9
		25.7	-18.7	1570	1570	16.4	-11.9	4	5					
23RD	292.00									150.9	-104.5	4.1	5.9	-.7
		35.7	-25.9	2005	2005	17.8	-12.9	3	4					
24TH	308.00									115.2	-78.6	2.7	3.8	-.5
		22.6	-14.9	1317	1317	17.2	-11.3	2	4					
25TH	320.50									92.7	-63.7	1.8	2.5	-.4
		30.9	-19.4	1685	1685	18.3	-11.5	2	4					
26TH	336.50									61.8	-44.3	.9	1.3	-.2
		19.9	-14.6	1276	1276	15.6	-11.4	1	2					
27TH	349.00									41.9	-29.8	.4	.6	-.1
		18.3	-13.0	1275	1275	14.4	-10.2	3	4					
EAVE	361.50									23.6	-16.7	.2	.2	-.0
		23.6	-16.7	1182	1182	20.0	-14.1	1	1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 230 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									731.3	-692.7	125.9	139.4	-.6
		33.8	-50.3	4039	4039	8.4	-12.5	-1	-1					
2ND	26.00									697.5	-642.4	108.5	120.8	-.6
		20.0	-25.2	1942	1942	10.3	-13.0	0	0					
3RD	38.50									677.5	-617.2	100.7	112.2	-.6
		22.1	-25.2	1942	1942	11.4	-13.0	1	1					
4TH	51.00									655.4	-592.0	93.1	103.9	-.6
		25.7	-24.6	1942	1942	13.2	-12.7	2	3					
5TH	63.50									629.8	-567.4	85.9	95.9	-.4
		22.3	-21.8	1942	1942	11.5	-11.2	2	2					
6TH	76.00									607.4	-545.6	78.9	88.1	-.4
		24.0	-23.4	1843	1843	13.0	-12.7	0	0					
7TH	88.50									583.4	-522.2	72.2	80.7	-.3
		24.7	-23.5	1817	1817	13.6	-12.9	-0	-0					
8TH	101.00									558.7	-498.8	65.9	73.5	-.3
		25.1	-23.4	1817	1817	13.8	-12.9	-0	-0					
9TH	113.50									533.5	-475.4	59.8	66.7	-.3
		25.6	-23.4	1817	1817	14.1	-12.9	-0	-1					
10TH	126.00									508.0	-452.0	54.0	60.2	-.4
		26.1	-23.4	1817	1817	14.3	-12.9	-0	-0					
11TH	138.50									481.9	-428.6	48.5	54.0	-.4
		26.6	-23.4	1817	1817	14.7	-12.9	-0	-0					
12TH	151.00									455.3	-405.2	43.3	48.2	-.4
		27.2	-23.4	1817	1817	15.0	-12.9	0	0					
13TH	163.50									428.1	-381.9	38.3	42.6	-.4
		27.3	-23.3	1817	1817	15.0	-12.8	0	0					
14TH	176.00									400.8	-358.5	33.7	37.5	-.4
		27.2	-23.3	1817	1817	15.0	-12.8	1	1					
15TH	188.50									373.6	-335.2	29.4	32.6	-.3
		27.1	-23.3	1817	1817	14.9	-12.8	1	1					
16TH	201.00									346.5	-312.0	25.3	28.1	-.3
		27.1	-23.5	1817	1817	14.9	-12.9	1	1					
17TH	213.50									319.4	-288.4	21.6	24.0	-.2
		27.4	-24.2	1817	1817	15.1	-13.3	1	1					
18TH	226.00									292.0	-264.2	18.1	20.1	-.2
		27.7	-24.9	1817	1817	15.2	-13.7	1	1					
19TH	238.50									264.3	-239.3	15.0	16.7	-.2
		28.0	-25.6	1817	1817	15.4	-14.1	0	1					
20TH	251.00									236.3	-213.7	12.1	13.5	-.1
		28.6	-26.1	1817	1817	15.8	-14.4	1	1					
21ST	263.50									207.7	-187.6	9.6	10.8	-.1
		37.4	-34.4	2325	2325	16.1	-14.8	1	1					
22ND	279.50									170.3	-153.2	6.9	7.7	-.1
		24.5	-22.4	1570	1570	15.6	-14.2	0	0					
23RD	292.00									145.7	-130.8	5.1	5.8	-.0
		34.4	-31.7	2005	2005	17.2	-15.8	0	0					
24TH	308.00									111.3	-99.2	3.3	3.7	-.0
		21.6	-19.3	1317	1317	16.4	-14.7	1	1					
25TH	320.50									89.7	-79.8	2.2	2.5	-.0
		28.7	-25.6	1685	1685	17.0	-15.2	0	0					
26TH	336.50									61.0	-54.2	1.1	1.2	.0
		19.7	-17.6	1276	1276	15.5	-13.8	-0	-1					
27TH	349.00									41.3	-36.6	.5	.6	-.0
		18.6	-16.5	1275	1275	14.6	-12.9	0	0					
EAVE	361.50									22.7	-20.1	.2	.2	-.0
		22.7	-20.1	1182	1182	19.2	-17.0	0	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 240 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									662.2	-656.4	122.8	123.2	1.6
		30.2	-45.4	4039	4039	7.5	-11.2	-2	-2					
2ND	26.00									632.1	-611.0	106.3	106.4	1.4
		18.0	-23.1	1942	1942	9.3	-11.9	-0	-0					
3RD	38.50									614.1	-587.9	98.8	98.6	1.4
		20.2	-23.6	1942	1942	10.4	-12.2	1	1					
4TH	51.00									593.9	-564.3	91.6	91.1	1.4
		24.4	-22.9	1942	1942	12.6	-11.8	4	4					
5TH	63.50									569.5	-541.4	84.7	83.8	1.6
		20.9	-20.0	1942	1942	10.8	-10.3	1	1					
6TH	76.00									548.6	-521.4	78.1	76.8	1.7
		22.9	-20.9	1843	1843	12.4	-11.3	0	0					
7TH	88.50									525.7	-500.4	71.7	70.1	1.7
		23.8	-20.8	1817	1817	13.1	-11.5	-0	-0					
8TH	101.00									501.9	-479.6	65.6	63.7	1.7
		24.4	-20.7	1817	1817	13.4	-11.4	-1	-1					
9TH	113.50									477.5	-458.9	59.7	57.6	1.6
		25.0	-20.5	1817	1817	13.7	-11.3	-1	-1					
10TH	126.00									452.6	-438.4	54.1	51.7	1.6
		25.2	-20.7	1817	1817	13.9	-11.4	-1	-2					
11TH	138.50									427.4	-417.7	48.7	46.2	1.5
		25.2	-21.1	1817	1817	13.9	-11.6	-1	-2					
12TH	151.00									402.1	-396.6	43.7	41.1	1.4
		25.3	-21.5	1817	1817	13.9	-11.8	-2	-2					
13TH	163.50									376.8	-375.1	38.8	36.2	1.4
		25.3	-21.6	1817	1817	13.9	-11.9	-2	-2					
14TH	176.00									351.5	-353.5	34.3	31.6	1.3
		25.2	-21.5	1817	1817	13.9	-11.8	-2	-2					
15TH	188.50									326.3	-332.0	30.0	27.4	1.2
		25.2	-21.4	1817	1817	13.9	-11.8	-2	-2					
16TH	201.00									301.1	-310.6	26.0	23.5	1.1
		25.3	-21.6	1817	1817	13.9	-11.9	-2	-2					
17TH	213.50									275.8	-289.0	22.2	19.9	1.0
		25.6	-22.3	1817	1817	14.1	-12.3	-2	-2					
18TH	226.00									250.3	-266.8	18.8	16.6	.9
		25.9	-22.9	1817	1817	14.2	-12.6	-2	-2					
19TH	238.50									224.4	-243.8	15.6	13.6	.8
		26.2	-23.8	1817	1817	14.4	-13.1	-1	-1					
20TH	251.00									198.2	-220.0	12.7	11.0	.8
		26.7	-25.2	1817	1817	14.7	-13.9	-1	-1					
21ST	263.50									171.5	-194.8	10.1	8.7	.7
		35.0	-34.1	2325	2325	15.1	-14.7	-0	-0					
22ND	279.50									136.5	-160.7	7.2	6.2	.7
		20.4	-23.2	1570	1570	13.0	-14.7	-4	-3					
23RD	292.00									116.1	-137.5	5.4	4.6	.6
		27.8	-32.6	2005	2005	13.8	-16.3	-3	-2					
24TH	308.00									88.4	-104.9	3.4	3.0	.4
		16.9	-21.0	1317	1317	12.8	-16.0	-2	-2					
25TH	320.50									71.5	-83.9	2.2	2.0	.3
		22.0	-28.3	1685	1685	13.1	-16.8	-2	-2					
26TH	336.50									49.5	-55.5	1.1	1.0	.2
		15.8	-18.3	1276	1276	12.4	-14.3	-3	-2					
27TH	349.00									33.7	-37.2	.5	.5	.1
		14.9	-16.6	1275	1275	11.7	-13.0	-4	-3					
EAVE	361.50									18.8	-20.6	.2	.2	.0
		18.8	-20.6	1182	1182	15.9	-17.4	-0	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 250 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									488.6	-854.0	160.7	87.9	4.9
		21.3	-55.3	4039	4039	5.3	-13.7	-5	-2					
2ND	26.00									467.3	-798.7	139.2	75.5	4.6
		14.2	-29.4	1942	1942	7.3	-15.1	-1	-0					
3RD	38.50									453.1	-769.3	129.4	69.7	4.6
		16.9	-30.5	1942	1942	8.7	-15.7	1	0					
4TH	51.00									436.2	-738.8	120.0	64.1	4.6
		21.5	-29.3	1942	1942	11.1	-15.1	5	4					
5TH	63.50									414.8	-709.6	110.9	58.8	4.8
		17.7	-23.8	1942	1942	9.1	-12.3	2	1					
6TH	76.00									397.1	-685.8	102.2	53.8	4.9
		18.1	-26.9	1843	1843	9.8	-14.6	-1	-1					
7TH	88.50									379.0	-658.9	93.8	48.9	4.8
		18.6	-27.5	1817	1817	10.2	-15.1	-2	-1					
8TH	101.00									360.4	-631.4	85.7	44.3	4.7
		19.1	-27.4	1817	1817	10.5	-15.1	-3	-2					
9TH	113.50									341.3	-603.9	78.0	39.9	4.6
		19.6	-27.4	1817	1817	10.8	-15.1	-3	-2					
10TH	126.00									321.7	-576.5	70.6	35.8	4.5
		19.6	-27.6	1817	1817	10.8	-15.2	-4	-3					
11TH	138.50									302.1	-548.9	63.6	31.9	4.4
		19.4	-27.9	1817	1817	10.7	-15.3	-4	-3					
12TH	151.00									282.7	-521.1	56.9	28.2	4.2
		19.2	-28.2	1817	1817	10.6	-15.5	-5	-4					
13TH	163.50									263.5	-492.9	50.6	24.8	4.0
		18.9	-28.4	1817	1817	10.4	-15.6	-6	-4					
14TH	176.00									244.6	-464.5	44.6	21.6	3.7
		18.5	-28.6	1817	1817	10.2	-15.7	-6	-4					
15TH	188.50									226.2	-435.9	39.0	18.7	3.5
		18.0	-28.7	1817	1817	9.9	-15.8	-6	-4					
16TH	201.00									208.2	-407.2	33.7	16.0	3.3
		17.9	-29.1	1817	1817	9.8	-16.0	-6	-4					
17TH	213.50									190.3	-378.0	28.8	13.5	3.0
		18.2	-29.8	1817	1817	10.0	-16.4	-6	-4					
18TH	226.00									172.1	-348.2	24.2	11.2	2.8
		18.4	-30.6	1817	1817	10.2	-16.8	-6	-4					
19TH	238.50									153.7	-317.7	20.1	9.2	2.5
		18.9	-31.6	1817	1817	10.4	-17.4	-6	-3					
20TH	251.00									134.9	-286.1	16.3	7.4	2.3
		19.4	-33.4	1817	1817	10.7	-18.4	-5	-3					
21ST	263.50									115.4	-252.6	12.9	5.8	2.1
		25.5	-45.2	2325	2325	11.0	-19.5	-5	-3					
22ND	279.50									89.9	-207.4	9.3	4.1	1.8
		13.0	-30.8	1570	1570	8.3	-19.6	-10	-4					
23RD	292.00									76.9	-176.6	6.9	3.1	1.4
		19.1	-42.3	2005	2005	9.5	-21.1	-7	-3					
24TH	308.00									57.8	-134.3	4.4	2.0	1.0
		10.4	-26.9	1317	1317	7.9	-20.4	-8	-3					
25TH	320.50									47.4	-107.4	2.9	1.4	.8
		13.4	-37.1	1685	1685	7.9	-22.0	-7	-3					
26TH	336.50									34.0	-70.3	1.4	.7	.5
		10.7	-22.5	1276	1276	8.4	-17.6	-7	-3					
27TH	349.00									23.3	-47.8	.7	.4	.3
		9.1	-21.1	1275	1275	7.2	-16.5	-11	-5					
EAVE	361.50									14.2	-26.7	.2	.1	.1
		14.2	-26.7	1182	1182	12.0	-22.6	-2	-1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 260 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									153.2	-923.6	173.6	22.8	6.9
		1.6	-61.9	4039	4039	.4	-15.3	-9	-0					
2ND	26.00									151.6	-861.7	150.4	18.9	6.4
		4.0	-32.9	1942	1942	2.1	-16.9	-5	-1					
3RD	38.50									147.6	-828.8	139.8	17.0	6.2
		6.8	-34.2	1942	1942	3.5	-17.6	-3	-1					
4TH	51.00									140.8	-794.6	129.7	15.2	6.1
		11.3	-29.4	1942	1942	5.8	-15.1	6	2					
5TH	63.50									129.5	-765.3	119.9	13.5	6.3
		9.7	-22.9	1942	1942	5.0	-11.8	6	2					
6TH	76.00									119.8	-742.4	110.5	11.9	6.5
		9.2	-28.0	1843	1843	5.0	-15.2	-2	-1					
7TH	88.50									110.7	-714.4	101.4	10.5	6.4
		8.9	-29.1	1817	1817	4.9	-16.0	-4	-1					
8TH	101.00									101.8	-685.3	92.6	9.2	6.3
		8.9	-29.2	1817	1817	4.9	-16.0	-5	-1					
9TH	113.50									92.9	-656.1	84.2	7.9	6.1
		8.9	-29.2	1817	1817	4.9	-16.1	-6	-2					
10TH	126.00									84.0	-626.9	76.2	6.8	5.9
		8.5	-29.7	1817	1817	4.7	-16.3	-6	-2					
11TH	138.50									75.4	-597.3	68.6	5.8	5.7
		8.0	-30.3	1817	1817	4.4	-16.7	-7	-2					
12TH	151.00									67.4	-567.0	61.3	5.0	5.5
		7.5	-30.9	1817	1817	4.1	-17.0	-8	-2					
13TH	163.50									59.9	-536.1	54.4	4.2	5.2
		6.9	-31.3	1817	1817	3.8	-17.2	-9	-2					
14TH	176.00									53.0	-504.8	47.9	3.5	4.9
		6.2	-31.6	1817	1817	3.4	-17.4	-10	-2					
15TH	188.50									46.9	-473.2	41.8	2.8	4.6
		5.4	-32.0	1817	1817	3.0	-17.6	-10	-2					
16TH	201.00									41.4	-441.2	36.1	2.3	4.3
		5.0	-32.5	1817	1817	2.8	-17.9	-11	-2					
17TH	213.50									36.4	-408.8	30.8	1.8	3.9
		5.0	-33.2	1817	1817	2.7	-18.3	-10	-2					
18TH	226.00									31.5	-375.5	25.9	1.4	3.6
		4.9	-34.0	1817	1817	2.7	-18.7	-10	-1					
19TH	238.50									26.6	-341.5	21.4	1.0	3.2
		5.1	-35.1	1817	1817	2.8	-19.3	-9	-1					
20TH	251.00									21.5	-306.5	17.3	.7	2.9
		5.8	-37.1	1817	1817	3.2	-20.4	-8	-1					
21ST	263.50									15.7	-269.3	13.7	.5	2.6
		8.7	-50.4	2325	2325	3.7	-21.7	-6	-1					
22ND	279.50									7.0	-219.0	9.8	.3	2.2
		2.0	-32.7	1570	1570	1.3	-20.8	-14	-1					
23RD	292.00									5.0	-186.3	7.3	.2	1.8
		3.2	-44.7	2005	2005	1.6	-22.3	-10	-1					
24TH	308.00									1.8	-141.6	4.7	.2	1.3
		-.7	-27.4	1317	1317	-.5	-20.8	-11	0					
25TH	320.50									2.5	-114.2	3.1	.1	1.0
		-.7	-39.5	1685	1685	-.4	-23.4	-10	0					
26TH	336.50									3.2	-74.7	1.6	.1	.6
		1.0	-23.3	1276	1276	.8	-18.2	-10	-0					
27TH	349.00									2.1	-51.5	.8	.1	.4
		-.5	-22.5	1275	1275	-.4	-17.7	-13	0					
EAVE	361.50									2.6	-28.9	.3	.0	.1
		2.6	-28.9	1182	1182	2.2	-24.5	-4	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 270 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-15.0	-930.2	177.6	-6.7	5.1
		-11.1	-57.8	4039	4039	-2.8	-14.3	-8	1					
2ND	26.00									-3.9	-872.4	154.1	-6.5	4.6
		-3.1	-31.8	1942	1942	-1.6	-16.4	-6	1					
3RD	38.50									-.9	-840.5	143.4	-6.5	4.4
		-.9	-33.6	1942	1942	-.5	-17.3	-4	0					
4TH	51.00									.0	-806.9	133.1	-6.5	4.3
		4.3	-27.8	1942	1942	2.2	-14.3	6	1					
5TH	63.50									-4.3	-779.1	123.2	-6.4	4.4
		4.3	-20.8	1942	1942	2.2	-10.7	10	2					
6TH	76.00									-8.6	-758.3	113.6	-6.4	4.6
		4.3	-27.1	1843	1843	2.3	-14.7	-2	-0					
7TH	88.50									-12.9	-731.2	104.3	-6.2	4.6
		3.6	-28.6	1817	1817	2.0	-15.7	-4	-0					
8TH	101.00									-16.4	-702.6	95.3	-6.0	4.5
		3.0	-28.8	1817	1817	1.6	-15.9	-4	-0					
9TH	113.50									-19.4	-673.7	86.7	-5.8	4.4
		2.4	-29.1	1817	1817	1.3	-16.0	-5	-0					
10TH	126.00									-21.8	-644.7	78.5	-5.6	4.2
		2.1	-29.6	1817	1817	1.2	-16.3	-5	-0					
11TH	138.50									-23.9	-615.1	70.6	-5.3	4.1
		2.0	-30.4	1817	1817	1.1	-16.7	-6	-0					
12TH	151.00									-25.9	-584.7	63.1	-5.0	3.9
		1.9	-31.1	1817	1817	1.0	-17.1	-6	-0					
13TH	163.50									-27.7	-553.6	56.0	-4.6	3.7
		1.5	-31.9	1817	1817	.8	-17.6	-6	-0					
14TH	176.00									-29.2	-521.7	49.3	-4.3	3.5
		1.0	-32.7	1817	1817	.5	-18.0	-6	-0					
15TH	188.50									-30.2	-489.0	43.0	-3.9	3.3
		.4	-33.6	1817	1817	.2	-18.5	-6	-0					
16TH	201.00									-30.6	-455.4	37.1	-3.5	3.1
		-.0	-34.2	1817	1817	-.0	-18.8	-6	0					
17TH	213.50									-30.6	-421.2	31.6	-3.1	2.9
		-.3	-34.7	1817	1817	-.2	-19.1	-6	0					
18TH	226.00									-30.3	-386.4	26.6	-2.8	2.7
		-.6	-35.2	1817	1817	-.3	-19.4	-7	0					
19TH	238.50									-29.7	-351.2	21.9	-2.4	2.5
		-1.0	-36.1	1817	1817	-.5	-19.9	-7	0					
20TH	251.00									-28.7	-315.1	17.8	-2.0	2.2
		-1.5	-38.1	1817	1817	-.8	-21.0	-7	0					
21ST	263.50									-27.3	-277.0	14.1	-1.7	1.9
		-2.4	-51.5	2325	2325	-1.0	-22.2	-6	0					
22ND	279.50									-24.8	-225.5	10.1	-1.3	1.6
		-2.8	-34.2	1570	1570	-1.8	-21.8	-10	1					
23RD	292.00									-22.0	-191.3	7.5	-1.0	1.3
		-2.7	-46.6	2005	2005	-1.3	-23.2	-8	0					
24TH	308.00									-19.3	-144.7	4.8	-.6	.9
		-4.0	-28.9	1317	1317	-3.0	-22.0	-7	1					
25TH	320.50									-15.3	-115.8	3.1	-.4	.7
		-5.1	-39.6	1685	1685	-3.0	-23.5	-6	1					
26TH	336.50									-10.2	-76.1	1.6	-.2	.5
		-2.8	-22.7	1276	1276	-2.2	-17.8	-7	1					
27TH	349.00									-7.4	-53.4	.8	-.1	.3
		-4.0	-23.2	1275	1275	-3.1	-18.2	-8	1					
EAVE	361.50									-3.4	-30.2	.3	-.0	.1
		-3.4	-30.2	1182	1182	-2.9	-25.5	-4	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 280 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
BRND	0.00									7.1	-898.7	177.1	8.8	-1.2
		-23.1	-49.0	4039	4039	-5.7	-12.1	-3	2					
2ND	26.00									30.2	-849.7	154.4	8.3	-1.4
		-8.4	-27.7	1942	1942	-4.3	-14.3	-3	1					
3RD	38.50									38.6	-822.0	144.0	7.9	-1.5
		-6.3	-29.4	1942	1942	-3.2	-15.1	-1	0					
4TH	51.00									44.8	-792.6	133.9	7.4	-1.5
		-.3	-25.7	1942	1942	-.2	-13.2	5	-0					
5TH	63.50									45.2	-766.9	124.1	6.8	-1.4
		.0	-18.9	1942	1942	.0	-9.7	7	0					
6TH	76.00									45.2	-748.0	114.7	6.2	-1.2
		1.2	-25.2	1843	1843	.7	-13.6	5	0					
7TH	88.50									44.0	-722.8	105.5	5.7	-1.1
		1.7	-26.5	1817	1817	1.0	-14.6	4	0					
8TH	101.00									42.2	-696.3	96.6	5.1	-1.0
		2.0	-26.4	1817	1817	1.1	-14.5	4	0					
9TH	113.50									40.3	-669.9	88.1	4.6	-.9
		2.2	-26.2	1817	1817	1.2	-14.4	3	0					
10TH	126.00									38.1	-643.7	79.9	4.1	-.8
		2.3	-27.1	1817	1817	1.2	-14.9	2	0					
11TH	138.50									35.8	-616.6	72.0	3.7	-.8
		2.3	-28.4	1817	1817	1.3	-15.6	2	0					
12TH	151.00									33.5	-588.2	64.4	3.2	-.7
		2.4	-29.7	1817	1817	1.3	-16.4	2	0					
13TH	163.50									31.1	-558.5	57.3	2.8	-.6
		2.4	-30.9	1817	1817	1.3	-17.0	2	0					
14TH	176.00									28.7	-527.6	50.5	2.5	-.6
		2.4	-31.9	1817	1817	1.3	-17.5	2	0					
15TH	188.50									26.3	-495.7	44.1	2.1	-.5
		2.4	-32.9	1817	1817	1.3	-18.1	2	0					
16TH	201.00									23.8	-462.9	38.1	1.8	-.5
		2.4	-33.7	1817	1817	1.3	-18.6	1	0					
17TH	213.50									21.5	-429.2	32.5	1.5	-.4
		2.2	-34.3	1817	1817	1.2	-18.9	1	0					
18TH	226.00									19.3	-394.8	27.4	1.3	-.4
		2.0	-35.0	1817	1817	1.1	-19.3	1	0					
19TH	238.50									17.2	-359.8	22.7	1.0	-.3
		1.9	-36.1	1817	1817	1.0	-19.9	1	0					
20TH	251.00									15.4	-323.7	18.4	.8	-.3
		2.0	-38.5	1817	1817	1.1	-21.2	1	0					
21ST	263.50									13.4	-285.2	14.6	.6	-.2
		3.0	-52.6	2325	2325	1.3	-22.6	2	0					
22ND	279.50									10.3	-232.6	10.4	.5	-.2
		1.9	-34.2	1570	1570	1.2	-21.8	1	0					
23RD	292.00									8.5	-198.4	7.8	.3	-.1
		1.6	-47.9	2005	2005	.8	-23.9	0	0					
24TH	308.00									6.9	-150.6	5.0	.2	-.1
		1.3	-29.9	1317	1317	1.0	-22.7	1	0					
25TH	320.50									5.6	-120.7	3.3	.1	-.1
		1.8	-40.6	1685	1685	1.1	-24.1	1	0					
26TH	336.50									3.8	-80.1	1.7	.1	-.1
		1.4	-24.8	1276	1276	1.1	-19.4	1	0					
27TH	349.00									2.4	-55.3	.8	.0	-.0
		1.7	-24.9	1275	1275	1.4	-19.5	1	0					
EAVE	361.50									.7	-30.5	.3	.0	-.0
		.7	-30.5	1182	1182	.6	-25.8	1	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 290 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-70.6	-997.3	193.2	.3	-6.4
		-32.2	-57.5	4039	4039	-8.0	-14.2	1	-1					
2ND	26.00									-38.4	-939.8	168.0	1.7	-6.3
		-12.9	-32.0	1942	1942	-6.6	-16.5	0	-0					
3RD	38.50									-25.5	-907.8	156.5	2.1	-6.3
		-11.2	-33.7	1942	1942	-5.7	-17.4	1	-0					
4TH	51.00									-14.4	-874.1	145.3	2.4	-6.3
		-4.8	-30.4	1942	1942	-2.5	-15.7	5	-1					
5TH	63.50									-9.5	-843.7	134.6	2.5	-6.1
		-2.9	-25.5	1942	1942	-1.5	-13.1	0	-0					
6TH	76.00									-6.6	-818.2	124.2	2.6	-6.1
		-3.2	-29.7	1843	1843	-1.7	-16.1	8	-1					
7TH	88.50									-3.4	-788.5	114.2	2.7	-5.9
		-2.9	-30.5	1817	1817	-1.6	-16.8	9	-1					
8TH	101.00									-.6	-758.1	104.5	2.7	-5.6
		-2.6	-30.3	1817	1817	-1.4	-16.7	9	-1					
9TH	113.50									2.0	-727.7	95.2	2.7	-5.3
		-2.3	-30.1	1817	1817	-1.3	-16.6	8	-1					
10TH	126.00									4.4	-697.6	86.3	2.7	-5.1
		-1.9	-30.5	1817	1817	-1.1	-16.8	8	-1					
11TH	138.50									6.3	-667.1	77.8	2.6	-4.8
		-1.5	-31.2	1817	1817	-.8	-17.2	8	-0					
12TH	151.00									7.7	-635.9	69.6	2.5	-4.6
		-1.0	-31.8	1817	1817	-.6	-17.5	7	-0					
13TH	163.50									8.7	-604.1	61.9	2.4	-4.4
		-.7	-32.8	1817	1817	-.4	-18.0	7	-0					
14TH	176.00									9.5	-571.3	54.5	2.3	-4.1
		-.6	-34.0	1817	1817	-.3	-18.7	7	-0					
15TH	188.50									10.1	-537.3	47.6	2.2	-3.9
		-.5	-35.1	1817	1817	-.3	-19.3	7	-0					
16TH	201.00									10.5	-502.2	41.1	2.0	-3.7
		-.5	-36.3	1817	1817	-.3	-20.0	7	-0					
17TH	213.50									11.0	-465.9	35.1	1.9	-3.4
		-.8	-37.4	1817	1817	-.5	-20.6	7	-0					
18TH	226.00									11.9	-428.4	29.5	1.8	-3.2
		-1.1	-38.5	1817	1817	-.6	-21.2	7	-0					
19TH	238.50									13.0	-389.9	24.4	1.6	-2.9
		-1.6	-40.1	1817	1817	-.9	-22.1	7	-0					
20TH	251.00									14.6	-349.9	19.7	1.4	-2.6
		-2.1	-42.7	1817	1817	-1.1	-23.5	6	-0					
21ST	263.50									16.6	-307.2	15.6	1.2	-2.4
		-3.1	-58.3	2325	2325	-1.3	-25.1	5	-0					
22ND	279.50									19.7	-248.9	11.2	.9	-2.1
		2.4	-36.9	1570	1570	1.5	-23.5	10	1					
23RD	292.00									17.3	-212.0	8.3	.7	-1.7
		2.3	-50.5	2005	2005	1.2	-25.2	9	0					
24TH	308.00									15.0	-161.5	5.3	.5	-1.3
		3.2	-31.7	1317	1317	2.4	-24.1	9	1					
25TH	320.50									11.8	-129.8	3.5	.3	-1.0
		4.6	-43.7	1685	1685	2.7	-25.9	8	1					
26TH	336.50									7.2	-86.1	1.8	.1	-.6
		2.3	-27.3	1276	1276	1.8	-21.4	8	1					
27TH	349.00									4.9	-58.9	.9	.1	-.4
		3.1	-26.3	1275	1275	2.4	-20.6	9	1					
EAVE	361.50									1.9	-32.6	.3	.0	-.2
		1.9	-32.6	1182	1182	1.6	-27.6	5	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 300 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-270.2	-917.3	172.6	-46.6	-5.5
		-32.9	-58.1	4039	4039	-8.1	-14.4	1	-1					
2ND	26.00									-237.3	-859.2	149.6	-40.0	-5.4
		-14.8	-33.4	1942	1942	-7.6	-17.2	-0	0					
3RD	38.50									-222.6	-825.7	139.0	-37.1	-5.4
		-13.8	-35.8	1942	1942	-7.1	-18.4	0	-0					
4TH	51.00									-208.7	-790.0	128.9	-34.4	-5.4
		-9.7	-30.3	1942	1942	-5.0	-15.6	1	-0					
5TH	63.50									-199.0	-759.7	119.2	-31.9	-5.4
		-7.3	-25.6	1942	1942	-3.8	-13.2	-3	1					
6TH	76.00									-191.7	-734.1	109.9	-29.4	-5.5
		-7.6	-28.5	1843	1843	-4.1	-15.5	4	-1					
7TH	88.50									-184.1	-705.6	100.9	-27.1	-5.4
		-7.2	-29.1	1817	1817	-4.0	-16.0	6	-2					
8TH	101.00									-176.9	-676.5	92.3	-24.8	-5.2
		-6.9	-29.0	1817	1817	-3.8	-16.0	6	-2					
9TH	113.50									-170.0	-647.4	84.0	-22.6	-5.0
		-6.6	-29.0	1817	1817	-3.6	-16.0	7	-1					
10TH	126.00									-163.4	-618.4	76.1	-20.6	-4.8
		-6.5	-29.2	1817	1817	-3.6	-16.1	7	-1					
11TH	138.50									-156.9	-589.2	68.5	-18.6	-4.6
		-6.6	-29.5	1817	1817	-3.6	-16.2	7	-2					
12TH	151.00									-150.3	-559.8	61.4	-16.6	-4.4
		-6.6	-29.7	1817	1817	-3.6	-16.4	7	-2					
13TH	163.50									-143.6	-530.0	54.5	-14.8	-4.2
		-6.8	-30.0	1817	1817	-3.8	-16.5	7	-2					
14TH	176.00									-136.8	-500.0	48.1	-13.1	-3.9
		-7.2	-30.3	1817	1817	-4.0	-16.7	8	-2					
15TH	188.50									-129.6	-469.8	42.0	-11.4	-3.7
		-7.5	-30.5	1817	1817	-4.1	-16.8	9	-2					
16TH	201.00									-122.1	-439.3	36.4	-9.8	-3.4
		-8.1	-31.0	1817	1817	-4.5	-17.1	9	-2					
17TH	213.50									-114.0	-408.2	31.1	-8.3	-3.1
		-9.1	-31.9	1817	1817	-5.0	-17.6	8	-2					
18TH	226.00									-104.9	-376.3	26.2	-7.0	-2.8
		-10.1	-32.9	1817	1817	-5.6	-18.1	7	-2					
19TH	238.50									-94.8	-343.4	21.7	-5.7	-2.6
		-11.0	-34.2	1817	1817	-6.1	-18.8	7	-2					
20TH	251.00									-83.8	-309.2	17.6	-4.6	-2.3
		-11.4	-36.5	1817	1817	-6.3	-20.1	6	-2					
21ST	263.50									-72.4	-272.8	13.9	-3.6	-2.1
		-14.7	-49.8	2325	2325	-6.3	-21.4	6	-2					
22ND	279.50									-57.7	-223.0	10.0	-2.6	-1.8
		-8.9	-33.1	1570	1570	-5.7	-21.1	9	-3					
23RD	292.00									-48.8	-189.9	7.4	-1.9	-1.4
		-12.7	-45.1	2005	2005	-6.4	-22.5	8	-2					
24TH	308.00									-36.0	-144.8	4.7	-1.2	-1.1
		-6.9	-29.5	1317	1317	-5.2	-22.4	8	-2					
25TH	320.50									-29.1	-115.3	3.1	-.8	-.8
		-8.1	-39.3	1685	1685	-4.8	-23.3	8	-2					
26TH	336.50									-21.0	-76.0	1.6	-.4	-.5
		-7.2	-24.3	1276	1276	-5.7	-19.0	6	-2					
27TH	349.00									-13.8	-51.8	.8	-.2	-.3
		-5.3	-22.8	1275	1275	-4.1	-17.9	9	-2					
EAVE	361.50									-8.6	-28.9	.3	-.1	-.1
		-8.6	-28.9	1182	1182	-7.2	-24.5	3	-1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS

WIND DIRECTION 310 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-510.4	-729.0	136.1	-98.0	-2.5
		-34.7	-46.3	4039	4039	-8.6	-11.5	1	-0					
2ND	26.00									-475.7	-682.7	117.7	-85.1	-2.5
		-17.4	-27.5	1942	1942	-9.0	-14.2	-2	1					
3RD	38.50									-458.4	-655.2	109.4	-79.3	-2.5
		-17.8	-29.5	1942	1942	-9.2	-15.2	-2	1					
4TH	51.00									-440.6	-625.7	101.3	-73.7	-2.6
		-15.4	-26.4	1942	1942	-7.9	-13.6	-0	0					
5TH	63.50									-425.2	-599.3	93.7	-68.3	-2.6
		-12.7	-24.0	1942	1942	-6.6	-12.4	1	-0					
6TH	76.00									-412.5	-575.3	86.4	-63.0	-2.6
		-14.8	-24.2	1843	1843	-8.0	-13.1	2	-1					
7TH	88.50									-397.7	-551.1	79.3	-58.0	-2.5
		-15.0	-24.0	1817	1817	-8.3	-13.2	3	-2					
8TH	101.00									-382.7	-527.1	72.6	-53.1	-2.4
		-14.9	-23.8	1817	1817	-8.2	-13.1	3	-2					
9TH	113.50									-367.9	-503.3	66.1	-48.4	-2.3
		-14.7	-23.6	1817	1817	-8.1	-13.0	3	-2					
10TH	126.00									-353.2	-479.8	60.0	-43.9	-2.3
		-15.0	-23.4	1817	1817	-8.3	-12.9	3	-2					
11TH	138.50									-338.2	-456.4	54.1	-39.6	-2.2
		-15.5	-23.1	1817	1817	-8.5	-12.7	3	-2					
12TH	151.00									-322.7	-433.3	48.6	-35.4	-2.0
		-15.9	-22.9	1817	1817	-8.8	-12.6	4	-2					
13TH	163.50									-306.8	-410.4	43.3	-31.5	-1.9
		-16.4	-22.8	1817	1817	-9.0	-12.6	3	-2					
14TH	176.00									-290.3	-387.5	38.3	-27.8	-1.8
		-17.0	-22.8	1817	1817	-9.3	-12.6	3	-2					
15TH	188.50									-273.4	-364.7	33.6	-24.3	-1.7
		-17.5	-22.8	1817	1817	-9.6	-12.5	3	-2					
16TH	201.00									-255.9	-341.9	29.2	-21.0	-1.6
		-18.2	-23.0	1817	1817	-10.0	-12.7	3	-2					
17TH	213.50									-237.6	-318.9	25.1	-17.9	-1.5
		-19.2	-23.6	1817	1817	-10.6	-13.0	3	-2					
18TH	226.00									-218.4	-295.3	21.2	-15.0	-1.4
		-20.2	-24.2	1817	1817	-11.1	-13.3	3	-3					
19TH	238.50									-198.2	-271.1	17.7	-12.4	-1.2
		-21.2	-25.2	1817	1817	-11.6	-13.9	3	-3					
20TH	251.00									-177.0	-245.9	14.5	-10.1	-1.1
		-21.9	-27.1	1817	1817	-12.1	-14.9	2	-2					
21ST	263.50									-155.1	-218.8	11.6	-8.0	-1.0
		-29.2	-36.7	2325	2325	-12.6	-15.8	1	-1					
22ND	279.50									-125.9	-182.1	8.3	-5.7	-.9
		-18.6	-25.1	1570	1570	-11.9	-16.0	4	-3					
23RD	292.00									-107.2	-157.0	6.2	-4.3	-.8
		-24.8	-35.1	2005	2005	-12.4	-17.5	4	-3					
24TH	308.00									-82.4	-121.9	4.0	-2.8	-.6
		-15.8	-24.6	1317	1317	-12.0	-18.7	4	-3					
25TH	320.50									-66.7	-97.3	2.6	-1.8	-.5
		-20.5	-32.5	1685	1685	-12.2	-19.3	4	-3					
26TH	336.50									-46.1	-64.8	1.3	-.9	-.3
		-15.2	-20.6	1276	1276	-11.9	-16.2	3	-2					
27TH	349.00									-30.9	-44.2	.6	-.5	-.2
		-13.7	-19.8	1275	1275	-10.7	-15.5	4	-3					
EAVE	361.50									-17.2	-24.4	.2	-.2	-.1
		-17.2	-24.4	1182	1182	-14.5	-20.6	1	-1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 320 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-757.5	-672.9	124.9	-143.7	1.5
		-45.8	-44.3	4039	4039	-11.3	-11.0	-1	1					
2ND	26.00									-711.7	-628.6	107.9	-124.6	1.4
		-23.7	-24.3	1942	1942	-12.2	-12.5	-4	4					
3RD	38.50									-687.9	-604.4	100.2	-115.8	1.2
		-24.8	-25.3	1942	1942	-12.8	-13.1	-4	4					
4TH	51.00									-663.1	-579.1	92.8	-107.4	1.0
		-24.0	-24.2	1942	1942	-12.4	-12.5	-1	1					
5TH	63.50									-639.1	-554.9	85.8	-99.2	1.0
		-21.2	-22.8	1942	1942	-10.9	-11.8	1	-1					
6TH	76.00									-617.9	-532.0	79.0	-91.4	1.0
		-23.6	-22.3	1843	1843	-12.8	-12.1	-1	1					
7TH	88.50									-594.3	-509.8	72.5	-83.8	1.0
		-24.2	-21.9	1817	1817	-13.3	-12.1	-1	2					
8TH	101.00									-570.1	-487.8	66.2	-76.5	.9
		-24.3	-21.7	1817	1817	-13.4	-11.9	-1	2					
9TH	113.50									-545.8	-466.2	60.3	-69.5	.8
		-24.3	-21.4	1817	1817	-13.4	-11.8	-1	1					
10TH	126.00									-521.5	-444.8	54.6	-62.9	.8
		-24.7	-21.5	1817	1817	-13.6	-11.8	-1	1					
11TH	138.50									-496.8	-423.2	49.1	-56.5	.7
		-25.2	-21.7	1817	1817	-13.9	-12.0	-1	1					
12TH	151.00									-471.5	-401.5	44.0	-50.5	.7
		-25.8	-22.0	1817	1817	-14.2	-12.1	-1	1					
13TH	163.50									-445.7	-379.5	39.1	-44.7	.6
		-26.2	-22.2	1817	1817	-14.4	-12.2	-1	1					
14TH	176.00									-419.5	-357.3	34.5	-39.3	.6
		-26.7	-22.3	1817	1817	-14.7	-12.3	-1	1					
15TH	188.50									-392.9	-335.1	30.2	-34.2	.6
		-27.1	-22.4	1817	1817	-14.9	-12.3	-1	1					
16TH	201.00									-365.8	-312.7	26.1	-29.5	.5
		-27.7	-22.6	1817	1817	-15.3	-12.5	-1	1					
17TH	213.50									-338.1	-290.1	22.3	-25.1	.5
		-28.7	-23.1	1817	1817	-15.8	-12.7	-1	1					
18TH	226.00									-309.4	-267.0	18.9	-21.1	.4
		-29.6	-23.6	1817	1817	-16.3	-13.0	-1	1					
19TH	238.50									-279.7	-243.4	15.7	-17.4	.4
		-30.6	-24.2	1817	1817	-16.9	-13.3	-1	1					
20TH	251.00									-249.1	-219.2	12.8	-14.1	.3
		-31.4	-24.9	1817	1817	-17.3	-13.7	-1	1					
21ST	263.50									-217.7	-194.3	10.2	-11.1	.3
		-41.1	-32.6	2325	2325	-17.7	-14.0	-2	2					
22ND	279.50									-176.6	-161.8	7.4	-8.0	.1
		-25.6	-23.5	1570	1570	-16.3	-15.0	-1	1					
23RD	292.00									-151.0	-138.3	5.5	-5.9	.1
		-35.4	-32.0	2005	2005	-17.7	-15.9	-1	1					
24TH	308.00									-115.6	-106.3	3.5	-3.8	.1
		-22.7	-21.2	1317	1317	-17.2	-16.1	-0	0					
25TH	320.50									-92.9	-85.1	2.3	-2.5	.0
		-30.1	-27.1	1685	1685	-17.8	-16.1	-0	0					
26TH	336.50									-62.8	-58.0	1.2	-1.3	.0
		-20.9	-18.8	1276	1276	-16.4	-14.7	-1	1					
27TH	349.00									-41.9	-39.2	.6	-.6	.0
		-19.3	-17.7	1275	1275	-15.1	-13.9	-0	0					
EAVE	361.50									-22.7	-21.5	.2	-.2	-.0
		-22.7	-21.5	1182	1182	-19.2	-18.2	0	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 330 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-782.9	-672.4	121.6	-148.9	2.7
		-46.7	-47.3	4039	4039	-11.6	-11.7	1	-1					
2ND	26.00									-736.2	-625.2	104.7	-129.1	2.8
		-25.1	-23.9	1942	1942	-12.9	-12.3	-2	2					
3RD	38.50									-711.1	-601.3	97.1	-120.1	2.7
		-26.9	-24.1	1942	1942	-13.9	-12.4	-2	2					
4TH	51.00									-684.2	-577.2	89.7	-111.4	2.6
		-25.3	-25.0	1942	1942	-13.0	-12.9	1	-1					
5TH	63.50									-658.9	-552.2	82.6	-103.0	2.6
		-23.2	-23.2	1942	1942	-11.9	-11.9	2	-2					
6TH	76.00									-635.7	-529.1	75.9	-94.9	2.7
		-24.2	-23.4	1843	1843	-13.1	-12.7	-1	1					
7TH	88.50									-611.5	-505.6	69.4	-87.1	2.7
		-24.4	-23.2	1817	1817	-13.4	-12.8	-1	2					
8TH	101.00									-587.1	-482.4	63.2	-79.6	2.6
		-24.4	-22.9	1817	1817	-13.4	-12.6	-2	2					
9TH	113.50									-562.7	-459.5	57.4	-72.4	2.5
		-24.4	-22.6	1817	1817	-13.5	-12.4	-2	2					
10TH	126.00									-538.3	-436.9	51.8	-65.5	2.5
		-25.0	-22.5	1817	1817	-13.8	-12.4	-2	2					
11TH	138.50									-513.3	-414.3	46.4	-59.0	2.4
		-25.8	-22.6	1817	1817	-14.2	-12.4	-2	3					
12TH	151.00									-487.5	-391.8	41.4	-52.7	2.2
		-26.6	-22.6	1817	1817	-14.6	-12.4	-3	3					
13TH	163.50									-460.9	-369.2	36.6	-46.8	2.1
		-27.1	-22.7	1817	1817	-14.9	-12.5	-3	3					
14TH	176.00									-433.7	-346.5	32.2	-41.2	2.0
		-27.4	-22.8	1817	1817	-15.1	-12.5	-3	3					
15TH	188.50									-406.3	-323.7	28.0	-35.9	1.8
		-27.7	-22.9	1817	1817	-15.3	-12.6	-3	3					
16TH	201.00									-378.6	-300.8	24.1	-31.0	1.6
		-28.1	-23.3	1817	1817	-15.5	-12.8	-3	3					
17TH	213.50									-350.5	-277.5	20.5	-26.5	1.5
		-28.7	-24.1	1817	1817	-15.8	-13.3	-3	3					
18TH	226.00									-321.7	-253.4	17.1	-22.3	1.3
		-29.4	-24.9	1817	1817	-16.2	-13.7	-3	3					
19TH	238.50									-292.4	-228.6	14.1	-18.4	1.2
		-30.1	-25.6	1817	1817	-16.6	-14.1	-2	3					
20TH	251.00									-262.3	-203.0	11.4	-15.0	1.0
		-31.1	-26.1	1817	1817	-17.1	-14.4	-2	2					
21ST	263.50									-231.2	-176.8	9.1	-11.9	.9
		-41.2	-34.1	2325	2325	-17.7	-14.7	-1	1					
22ND	279.50									-190.0	-142.7	6.5	-8.5	.8
		-28.2	-21.0	1570	1570	-18.0	-13.4	-3	4					
23RD	292.00									-161.9	-121.8	4.9	-6.3	.7
		-38.7	-28.8	2005	2005	-19.3	-14.4	-3	4					
24TH	308.00									-123.2	-93.0	3.1	-4.0	.4
		-24.4	-18.0	1317	1317	-18.5	-13.7	-2	3					
25TH	320.50									-98.8	-75.0	2.1	-2.7	.3
		-33.3	-23.0	1685	1685	-19.8	-13.7	-2	2					
26TH	336.50									-65.5	-51.9	1.1	-1.3	.2
		-21.4	-16.5	1276	1276	-16.8	-12.9	-2	3					
27TH	349.00									-44.2	-35.5	.5	-.7	.1
		-19.6	-15.6	1275	1275	-15.4	-12.2	-3	4					
EAVE	361.50									-24.6	-19.9	.2	-.2	.0
		-24.6	-19.9	1182	1182	-20.8	-16.8	-0	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS

WIND DIRECTION 340 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-833.6	-550.4	97.1	-159.4	5.7
		-44.9	-40.0	4039	4039	-11.1	-9.9	-0	0					
2ND	26.00									-788.8	-510.4	83.3	-138.3	5.7
		-25.6	-18.9	1942	1942	-13.2	-9.7	-2	3					
3RD	38.50									-763.2	-491.5	77.1	-128.6	5.5
		-28.4	-18.5	1942	1942	-14.6	-9.5	-2	4					
4TH	51.00									-734.7	-473.0	71.0	-119.3	5.4
		-27.8	-21.6	1942	1942	-14.3	-11.1	2	-2					
5TH	63.50									-706.9	-451.4	65.3	-110.3	5.5
		-24.8	-19.5	1942	1942	-12.8	-10.0	2	-3					
6TH	76.00									-682.2	-431.9	59.7	-101.6	5.6
		-26.0	-20.1	1843	1843	-14.1	-10.9	-2	3					
7TH	88.50									-656.2	-411.8	54.5	-93.2	5.5
		-26.3	-19.9	1817	1817	-14.5	-11.0	-3	4					
8TH	101.00									-629.9	-391.8	49.5	-85.2	5.3
		-26.4	-19.6	1817	1817	-14.5	-10.8	-4	5					
9TH	113.50									-603.5	-372.2	44.7	-77.5	5.1
		-26.4	-19.4	1817	1817	-14.5	-10.7	-4	5					
10TH	126.00									-577.1	-352.9	40.1	-70.1	4.9
		-27.0	-19.3	1817	1817	-14.9	-10.6	-4	6					
11TH	138.50									-550.0	-333.5	35.9	-63.0	4.7
		-27.9	-19.4	1817	1817	-15.4	-10.7	-4	6					
12TH	151.00									-522.1	-314.1	31.8	-56.3	4.4
		-28.8	-19.5	1817	1817	-15.8	-10.7	-4	7					
13TH	163.50									-493.4	-294.6	28.0	-50.0	4.1
		-29.3	-19.6	1817	1817	-16.1	-10.8	-5	7					
14TH	176.00									-464.1	-275.0	24.4	-44.0	3.8
		-29.4	-19.6	1817	1817	-16.2	-10.8	-5	7					
15TH	188.50									-434.6	-255.4	21.1	-38.4	3.5
		-29.6	-19.6	1817	1817	-16.3	-10.8	-5	7					
16TH	201.00									-405.0	-235.9	18.1	-33.2	3.2
		-30.0	-19.9	1817	1817	-16.5	-10.9	-5	7					
17TH	213.50									-375.0	-216.0	15.2	-28.3	2.9
		-30.7	-20.6	1817	1817	-16.9	-11.3	-4	6					
18TH	226.00									-344.3	-195.4	12.7	-23.8	2.6
		-31.3	-21.3	1817	1817	-17.2	-11.8	-4	6					
19TH	238.50									-313.0	-174.1	10.4	-19.7	2.4
		-32.0	-21.9	1817	1817	-17.6	-12.0	-4	5					
20TH	251.00									-281.0	-152.2	8.3	-16.0	2.1
		-33.0	-21.9	1817	1817	-18.2	-12.1	-3	4					
21ST	263.50									-248.0	-130.3	6.6	-12.7	1.9
		-43.8	-28.2	2325	2325	-18.9	-12.1	-2	3					
22ND	279.50									-204.1	-102.1	4.7	-9.0	1.7
		-30.7	-14.8	1570	1570	-19.5	-9.4	-4	9					
23RD	292.00									-173.5	-87.3	3.5	-6.7	1.4
		-42.1	-21.3	2005	2005	-21.0	-10.6	-4	7					
24TH	308.00									-131.4	-66.0	2.3	-4.2	1.0
		-26.9	-11.9	1317	1317	-20.5	-9.0	-3	7					
25TH	320.50									-104.4	-54.1	1.5	-2.8	.8
		-36.6	-15.9	1685	1685	-21.7	-9.4	-3	6					
26TH	336.50									-67.8	-38.2	.8	-1.4	.5
		-22.3	-12.4	1276	1276	-17.5	-9.8	-3	6					
27TH	349.00									-45.5	-25.7	.4	-.7	.3
		-19.8	-10.3	1275	1275	-15.5	-8.1	-5	10					
EAVE	361.50									-25.7	-15.4	.1	-.2	.1
		-25.7	-15.4	1182	1182	-21.8	-13.1	-1	2					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 350 CONFIGURATION B REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-891.1	-212.8	33.9	-171.6	6.9
		-42.9	-20.8	4039	4039	-10.6	-5.2	-1	3					
2ND	26.00									-848.2	-192.0	28.7	-149.0	6.7
		-26.3	-8.4	1942	1942	-13.6	-4.3	-1	4					
3RD	38.50									-821.9	-183.6	26.3	-138.5	6.6
		-30.5	-7.1	1942	1942	-15.7	-3.7	-1	4					
4TH	51.00									-791.4	-176.4	24.1	-128.4	6.5
		-30.5	-10.9	1942	1942	-15.7	-5.6	2	-4					
5TH	63.50									-760.9	-165.6	21.9	-118.7	6.6
		-24.2	-8.7	1942	1942	-12.4	-4.5	1	-3					
6TH	76.00									-736.8	-156.9	19.9	-109.4	6.7
		-28.0	-8.8	1843	1843	-15.2	-4.8	-2	6					
7TH	88.50									-708.8	-148.1	18.0	-100.3	6.5
		-28.9	-8.4	1817	1817	-15.9	-4.6	-2	7					
8TH	101.00									-679.8	-139.7	16.2	-91.7	6.3
		-28.9	-8.0	1817	1817	-15.9	-4.4	-2	8					
9TH	113.50									-650.9	-131.7	14.5	-83.4	6.1
		-28.9	-7.6	1817	1817	-15.9	-4.2	-2	8					
10TH	126.00									-622.0	-124.1	12.9	-75.4	5.8
		-29.4	-7.4	1817	1817	-16.2	-4.1	-2	9					
11TH	138.50									-592.6	-116.6	11.4	-67.8	5.6
		-30.1	-7.4	1817	1817	-16.6	-4.1	-2	9					
12TH	151.00									-562.5	-109.3	10.0	-60.6	5.3
		-30.8	-7.3	1817	1817	-17.0	-4.0	-2	9					
13TH	163.50									-531.7	-102.0	8.7	-53.7	5.0
		-31.2	-7.3	1817	1817	-17.2	-4.0	-2	10					
14TH	176.00									-500.5	-94.7	7.5	-47.3	4.6
		-31.3	-7.4	1817	1817	-17.2	-4.1	-2	10					
15TH	188.50									-469.2	-87.2	6.3	-41.2	4.3
		-31.4	-7.5	1817	1817	-17.3	-4.1	-2	10					
16TH	201.00									-437.8	-79.7	5.3	-35.6	4.0
		-31.9	-7.7	1817	1817	-17.6	-4.2	-2	10					
17TH	213.50									-405.8	-72.0	4.3	-30.3	3.7
		-33.0	-8.0	1817	1817	-18.2	-4.4	-2	10					
18TH	226.00									-372.8	-64.0	3.5	-25.4	3.3
		-34.1	-8.2	1817	1817	-18.8	-4.5	-2	9					
19TH	238.50									-338.7	-55.8	2.7	-21.0	3.0
		-35.4	-8.6	1817	1817	-19.5	-4.7	-2	9					
20TH	251.00									-303.3	-47.2	2.1	-17.0	2.7
		-37.2	-9.2	1817	1817	-20.5	-5.0	-2	7					
21ST	263.50									-266.1	-38.1	1.6	-13.4	2.4
		-50.0	-12.8	2325	2325	-21.5	-5.5	-1	6					
22ND	279.50									-216.1	-25.3	1.1	-9.6	2.1
		-33.0	-4.3	1570	1570	-21.0	-2.7	-2	12					
23RD	292.00									-183.1	-21.0	.8	-7.1	1.7
		-45.0	-7.1	2005	2005	-22.5	-3.5	-1	9					
24TH	308.00									-138.1	-13.9	.5	-4.5	1.3
		-27.5	-2.6	1317	1317	-20.8	-2.0	-1	9					
25TH	320.50									-110.6	-11.3	.3	-2.9	1.0
		-38.8	-3.1	1685	1685	-23.0	-1.8	-1	9					
26TH	336.50									-71.8	-8.3	.2	-1.5	.7
		-22.8	-3.1	1276	1276	-17.9	-2.5	-1	10					
27TH	349.00									-49.0	-5.1	.1	-.7	.4
		-22.0	-1.5	1275	1275	-17.3	-1.2	-1	13					
EAVE	361.50									-27.0	-3.6	.0	-.2	.1
		-27.0	-3.6	1182	1182	-22.9	-3.1	-1	5					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. BASE SHEAR AND MOMENT SUMMARY : LPC MANDALAY LAS COLINAS,TEXAS
CONFIGURATION B REFERENCE PRESSURE 25.0 GUST FACTOR 1.32

AZIMUTH	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z	ECCEN (FT) X	ECCEN (FT) Y
0	-962.5	82.0	-19.6	-187.2	5.0	0	5
10	-984.8	15.6	-1.0	-192.3	-1.1	-0	-1
20	-953.8	.4	5.4	-185.9	-6.3	-0	-7
30	-653.8	234.5	-41.2	-127.2	-5.2	-3	-7
40	-603.9	449.3	-81.8	-116.3	-4.3	-3	-5
50	-569.1	568.6	-103.7	-108.1	-1.3	-1	-1
60	-496.6	623.9	-114.4	-93.2	2.0	2	2
70	-290.9	535.5	-98.2	-52.7	3.8	6	3
80	-98.2	550.5	-101.3	-14.4	4.5	8	1
90	48.9	588.8	-108.3	13.8	2.8	5	-0
100	52.3	601.8	-111.2	11.4	-.5	-1	0
110	48.7	585.7	-107.7	7.8	-3.6	-6	1
120	387.3	872.8	-158.4	71.9	-6.1	-6	3
130	657.8	831.7	-149.2	121.5	-5.3	-4	3
140	799.7	750.6	-134.5	147.4	-1.2	-1	1
150	821.6	692.1	-122.9	155.0	2.7	2	-2
160	693.7	412.0	-70.3	132.5	4.9	3	-5
170	714.9	184.0	-27.4	136.1	5.2	2	-7
180	744.6	-16.5	8.0	141.7	2.6	-0	-4
190	746.2	74.4	-17.0	142.3	-2.5	-0	3
200	733.1	-87.2	6.3	140.0	-4.9	1	7
210	740.2	-383.8	61.2	142.7	-4.4	2	5
220	724.9	-641.7	112.8	138.7	-2.5	2	2
230	731.3	-692.7	125.9	139.4	-.6	0	0
240	662.2	-656.4	122.8	123.2	1.6	-1	-1
250	488.6	-854.0	160.7	87.9	4.9	-4	-2
260	153.2	-923.6	173.6	22.8	6.9	-7	-1
270	-15.0	-930.2	177.6	-6.7	5.1	-5	0
280	7.1	-898.7	177.1	8.8	-1.2	1	0
290	-70.6	-997.3	193.2	.3	-6.4	6	-0
300	-270.2	-917.3	172.6	-46.6	-5.5	6	-2
310	-510.4	-729.0	136.1	-98.0	-2.5	2	-2
320	-757.5	-672.9	124.9	-143.7	1.5	-1	1
330	-782.9	-672.4	121.6	-148.9	2.7	-2	2
340	-833.6	-550.4	97.1	-159.4	5.7	-3	5
350	-891.1	-212.8	33.9	-171.6	6.9	-2	7

TABLE 7. LPC MANDALAY LAS COLINAS,TEXAS

PROJECT 6600 CONFIGURATION C

SCALE = 400 REF. PRESSURE = 25.0

GUST FACTOR = 1.32 STANDARD FLOOR HEIGHT = 12.50

NUMBER OF SIDES = 4 NO. OF FLOORS = 28

SIDE	ANGLE	Z-AXIS	SHFACT
1	0.0	2.330	1.0
2	90.0	2.330	1.0
3	180.0	2.330	1.0
4	270.0	2.330	1.0

FLOOR #	LABEL	HEIGHT-FT	WIND AZIMUTH	LOAD FACTOR
1	GRND	26.00	0	.55
2	2ND	12.50	10	.55
3	3RD	12.50	20	.55
4	4TH	12.50	30	.55
5	5TH	12.50	40	.68
6	6TH	12.50	50	.68
7	7TH	12.50	60	.68
8	8TH	12.50	70	.68
9	9TH	12.50	80	.68
10	10TH	12.50	90	.90
11	11TH	12.50	100	.90
12	12TH	12.50	110	.90
13	13TH	12.50	120	.90
14	14TH	12.50	130	.92
15	15TH	12.50	140	.92
16	16TH	12.50	150	.92
17	17TH	12.50	160	.92
18	18TH	12.50	170	.92
19	19TH	12.50	180	1.00
20	20TH	12.50	190	1.00
21	21ST	16.00	200	1.00
22	22ND	12.50	210	1.00
23	23RD	16.00	220	.81
24	24TH	12.50	230	.81
25	25TH	16.00	240	.81
26	26TH	12.50	250	.81
27	27TH	12.50	260	.81
28	EAVE	18.00	270	.70
			280	.70
			290	.70
			300	.70
			310	.88
			320	.88
			330	.88
			340	.88
			350	.88

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 0 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									16.8	500.2	-94.8	6.1	-.0
		-13.9	30.7	4039	4039	-3.4	7.6	-4	-2					
2ND	26.00									30.7	469.5	-82.2	5.5	.1
		-5.3	16.6	1942	1942	-2.7	8.6	-6	-2					
3RD	38.50									36.0	452.9	-76.4	5.1	.2
		-4.4	17.6	1942	1942	-2.3	9.0	-5	-1					
4TH	51.00									40.4	435.4	-70.9	4.6	.3
		.6	15.8	1942	1942	.3	8.1	7	-0					
5TH	63.50									39.8	419.6	-65.5	4.1	.2
		1.5	11.0	1942	1942	.8	5.7	5	-1					
6TH	76.00									38.3	408.6	-60.4	3.6	.2
		1.3	15.4	1843	1843	.7	8.4	2	-0					
7TH	88.50									37.0	393.2	-55.3	3.1	.1
		1.7	16.7	1817	1817	1.0	9.2	1	-0					
8TH	101.00									35.3	376.5	-50.5	2.7	.1
		2.3	17.1	1817	1817	1.3	9.4	1	-0					
9TH	113.50									32.9	359.4	-45.9	2.3	.1
		3.0	17.4	1817	1817	1.6	9.6	0	-0					
10TH	126.00									30.0	342.0	-41.6	1.9	.1
		3.2	17.5	1817	1817	1.8	9.6	1	-0					
11TH	138.50									26.8	324.5	-37.4	1.5	.1
		3.3	17.5	1817	1817	1.8	9.6	1	-0					
12TH	151.00									23.5	307.0	-33.4	1.2	.0
		3.3	17.5	1817	1817	1.8	9.6	2	-0					
13TH	163.50									20.2	289.5	-29.7	.9	.0
		3.2	17.5	1817	1817	1.8	9.6	2	-0					
14TH	176.00									17.0	272.0	-26.2	.7	-.0
		2.9	17.3	1817	1817	1.6	9.5	2	-0					
15TH	188.50									14.0	254.7	-22.9	.5	-.0
		2.6	17.2	1817	1817	1.4	9.5	2	-0					
16TH	201.00									11.4	237.5	-19.8	.3	-.1
		2.3	17.2	1817	1817	1.3	9.5	1	-0					
17TH	213.50									9.1	220.3	-17.0	.2	-.1
		2.0	17.4	1817	1817	1.1	9.6	1	-0					
18TH	226.00									7.1	202.9	-14.3	.1	-.1
		1.7	17.6	1817	1817	.9	9.7	1	-0					
19TH	238.50									5.4	185.3	-11.9	.0	-.1
		1.5	18.1	1817	1817	.8	10.0	1	-0					
20TH	251.00									3.8	167.2	-9.7	-.0	-.2
		1.8	19.4	1817	1817	1.0	10.7	1	-0					
21ST	263.50									2.1	147.8	-7.7	-.1	-.2
		2.5	26.7	2325	2325	1.1	11.5	1	-0					
22ND	279.50									-.4	121.2	-5.6	-.1	-.2
		.4	17.1	1570	1570	.3	10.9	-0	0					
23RD	292.00									-.8	104.1	-4.2	-.1	-.2
		.3	24.0	2005	2005	.1	12.0	-1	0					
24TH	308.00									-1.1	80.0	-2.7	-.1	-.2
		-.1	14.9	1317	1317	-.1	11.3	-1	-0					
25TH	320.50									-1.0	65.1	-1.8	-.0	-.2
		.1	21.6	1685	1685	.0	12.8	-2	0					
26TH	336.50									-1.1	43.5	-.9	-.0	-.1
		-.3	12.8	1276	1276	-.3	10.0	-4	-0					
27TH	349.00									-.7	30.7	-.5	-.0	-.1
		-.5	13.5	1275	1275	-.4	10.6	-5	-0					
EAVE	361.50									-.3	17.2	-.2	-.0	-.0
		-.3	17.2	1182	1182	-.2	14.6	-2	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 10 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									75.4	527.5	-99.3	17.9	.9
		-11.3	35.2	4039	4039	-2.8	8.7	-2	-1					
2ND	26.00									86.7	492.3	-86.0	15.8	1.0
		-3.4	17.5	1942	1942	-1.7	9.0	-3	-1					
3RD	38.50									90.1	474.8	-80.0	14.7	1.1
		-2.2	17.6	1942	1942	-1.2	9.1	-2	-0					
4TH	51.00									92.3	457.2	-74.1	13.5	1.1
		2.2	15.8	1942	1942	1.1	8.2	5	-1					
5TH	63.50									90.1	441.3	-68.5	12.4	1.0
		3.5	11.5	1942	1942	1.8	5.9	-2	1					
6TH	76.00									86.7	429.8	-63.1	11.3	1.1
		3.3	16.5	1843	1843	1.8	9.0	4	-1					
7TH	88.50									83.4	413.3	-57.8	10.2	1.0
		3.8	17.7	1817	1817	2.1	9.7	5	-1					
8TH	101.00									79.5	395.7	-52.7	9.2	.9
		4.5	17.8	1817	1817	2.5	9.8	4	-1					
9TH	113.50									75.1	377.9	-47.9	8.2	.8
		5.1	17.9	1817	1817	2.8	9.9	3	-1					
10TH	126.00									70.0	360.0	-43.3	7.3	.8
		5.2	18.0	1817	1817	2.9	9.9	3	-1					
11TH	138.50									64.7	342.0	-38.9	6.5	.7
		5.2	18.1	1817	1817	2.9	10.0	2	-1					
12TH	151.00									59.5	323.9	-34.7	5.7	.7
		5.2	18.2	1817	1817	2.9	10.0	2	-1					
13TH	163.50									54.3	305.7	-30.8	5.0	.6
		5.0	18.3	1817	1817	2.7	10.1	2	-1					
14TH	176.00									49.4	287.4	-27.1	4.3	.6
		4.6	18.5	1817	1817	2.5	10.2	2	-0					
15TH	188.50									44.7	268.9	-23.6	3.8	.6
		4.3	18.7	1817	1817	2.3	10.3	1	-0					
16TH	201.00									40.5	250.2	-20.4	3.2	.5
		3.9	18.9	1817	1817	2.1	10.4	1	-0					
17TH	213.50									36.6	231.3	-17.4	2.7	.5
		3.5	19.2	1817	1817	1.9	10.6	2	-0					
18TH	226.00									33.1	212.1	-14.6	2.3	.5
		3.2	19.4	1817	1817	1.7	10.7	2	-0					
19TH	238.50									29.9	192.7	-12.1	1.9	.4
		2.9	19.9	1817	1817	1.6	11.0	3	-0					
20TH	251.00									27.0	172.7	-9.8	1.6	.4
		3.3	21.0	1817	1817	1.8	11.6	3	-0					
21ST	263.50									23.7	151.7	-7.8	1.2	.3
		4.7	28.4	2325	2325	2.0	12.2	3	-1					
22ND	279.50									19.0	123.4	-5.6	.9	.2
		2.5	18.1	1570	1570	1.6	11.6	3	-0					
23RD	292.00									16.5	105.2	-4.1	.7	.1
		3.1	25.6	2005	2005	1.5	12.8	2	-0					
24TH	308.00									13.4	79.6	-2.7	.4	.1
		2.4	15.1	1317	1317	1.8	11.5	1	-0					
25TH	320.50									11.0	64.5	-1.8	.3	.1
		3.6	22.0	1685	1685	2.1	13.1	1	-0					
26TH	336.50									7.4	42.5	-.9	.1	.0
		2.7	12.5	1276	1276	2.1	9.8	2	-1					
27TH	349.00									4.7	30.0	-.4	.1	.0
		2.2	13.3	1275	1275	1.8	10.4	0	-0					
EAVE	361.50									2.4	16.8	-.2	.0	.0
		2.4	16.8	1182	1182	2.1	14.2	0	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 20 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
BRND	0.00									64.2	540.6	-98.8	16.7	2.6
		-8.7	39.8	4039	4039	-2.2	9.9	2	0					
2ND	26.00									72.9	500.8	-85.3	14.9	2.5
		-2.5	20.2	1942	1942	-1.3	10.4	1	0					
3RD	38.50									75.4	480.5	-79.1	14.0	2.5
		-1.5	20.4	1942	1942	-.8	10.5	1	0					
4TH	51.00									76.9	460.1	-73.3	13.1	2.5
		2.1	18.0	1942	1942	1.1	9.3	3	-0					
5TH	63.50									74.9	442.1	-67.6	12.1	2.4
		3.9	14.1	1942	1942	2.0	7.3	-2	1					
6TH	76.00									70.9	428.0	-62.2	11.2	2.4
		2.7	17.2	1843	1843	1.5	9.3	5	-1					
7TH	88.50									68.2	410.8	-56.9	10.3	2.4
		2.6	17.9	1817	1817	1.4	9.8	6	-1					
8TH	101.00									65.6	392.9	-51.9	9.5	2.2
		2.8	17.9	1817	1817	1.5	9.9	5	-1					
9TH	113.50									62.8	375.0	-47.1	8.7	2.1
		2.9	18.0	1817	1817	1.6	9.9	5	-1					
10TH	126.00									59.9	356.9	-42.5	7.9	2.1
		2.9	18.1	1817	1817	1.6	10.0	5	-1					
11TH	138.50									56.9	338.8	-38.2	7.2	2.0
		2.9	18.3	1817	1817	1.6	10.1	5	-1					
12TH	151.00									54.0	320.5	-34.1	6.5	1.9
		2.8	18.5	1817	1817	1.6	10.2	5	-1					
13TH	163.50									51.2	302.0	-30.2	5.8	1.8
		2.8	18.6	1817	1817	1.5	10.2	5	-1					
14TH	176.00									48.4	283.4	-26.5	5.2	1.7
		2.8	18.7	1817	1817	1.5	10.3	5	-1					
15TH	188.50									45.7	264.7	-23.1	4.6	1.6
		2.7	18.9	1817	1817	1.5	10.4	5	-1					
16TH	201.00									42.9	245.9	-19.9	4.1	1.5
		2.6	19.0	1817	1817	1.5	10.5	5	-1					
17TH	213.50									40.3	226.9	-17.0	3.6	1.4
		2.5	19.1	1817	1817	1.4	10.5	5	-1					
18TH	226.00									37.7	207.8	-14.2	3.1	1.3
		2.4	19.3	1817	1817	1.3	10.6	6	-1					
19TH	238.50									35.3	188.5	-11.8	2.6	1.2
		2.3	19.7	1817	1817	1.3	10.8	6	-1					
20TH	251.00									33.0	168.8	-9.5	2.2	1.1
		2.2	20.8	1817	1817	1.2	11.4	6	-1					
21ST	263.50									30.7	148.0	-7.5	1.8	1.0
		2.9	28.0	2325	2325	1.3	12.1	5	-1					
22ND	279.50									27.8	120.0	-5.4	1.3	.8
		3.7	17.6	1570	1570	2.4	11.2	10	-2					
23RD	292.00									24.1	102.4	-4.0	1.0	.6
		4.1	25.1	2005	2005	2.1	12.5	7	-1					
24TH	308.00									20.0	77.3	-2.6	.6	.4
		3.9	14.2	1317	1317	3.0	10.8	7	-2					
25TH	320.50									16.1	63.1	-1.7	.4	.3
		5.5	21.7	1685	1685	3.3	12.9	6	-1					
26TH	336.50									10.6	41.4	-.9	.2	.2
		3.8	12.6	1276	1276	2.9	9.9	7	-2					
27TH	349.00									6.8	28.8	-.4	.1	.1
		3.3	12.9	1275	1275	2.6	10.1	6	-2					
EAVE	361.50									3.6	15.9	-.1	.0	.0
		3.6	15.9	1182	1182	3.0	13.5	2	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 30 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									14.4	553.5	-99.0	7.0	3.8
		-11.1	43.6	4039	4039	-2.8	10.8	1	0					
2ND	26.00									25.5	510.0	-85.2	6.5	3.8
		-3.8	22.4	1942	1942	-2.0	11.5	1	0					
3RD	38.50									29.3	487.6	-79.0	6.2	3.8
		-2.9	22.7	1942	1942	-1.5	11.7	2	0					
4TH	51.00									32.2	464.9	-73.0	5.8	3.7
		.4	19.5	1942	1942	.2	10.0	2	-0					
5TH	63.50									31.8	445.4	-67.3	5.4	3.7
		1.8	15.2	1942	1942	.9	7.8	-5	1					
6TH	76.00									30.1	430.2	-61.8	5.0	3.8
		1.1	18.1	1843	1843	.6	9.8	5	-0					
7TH	88.50									29.0	412.1	-56.6	4.6	3.7
		1.2	18.6	1817	1817	.6	10.2	7	-0					
8TH	101.00									27.8	393.5	-51.5	4.3	3.6
		1.3	18.4	1817	1817	.7	10.1	7	-0					
9TH	113.50									26.5	375.2	-46.7	3.9	3.4
		1.5	18.2	1817	1817	.8	10.0	7	-1					
10TH	126.00									25.0	357.0	-42.2	3.6	3.3
		1.5	18.2	1817	1817	.8	10.0	7	-1					
11TH	138.50									23.5	338.8	-37.8	3.3	3.2
		1.5	18.3	1817	1817	.8	10.1	7	-1					
12TH	151.00									22.0	320.5	-33.7	3.0	3.0
		1.4	18.5	1817	1817	.8	10.2	7	-1					
13TH	163.50									20.6	302.0	-29.8	2.8	2.9
		1.2	18.7	1817	1817	.7	10.3	8	-0					
14TH	176.00									19.4	283.4	-26.1	2.5	2.8
		.9	19.0	1817	1817	.5	10.5	8	-0					
15TH	188.50									18.5	264.4	-22.7	2.3	2.6
		.6	19.3	1817	1817	.3	10.6	8	-0					
16TH	201.00									17.9	245.1	-19.5	2.1	2.4
		.4	19.5	1817	1817	.2	10.8	8	-0					
17TH	213.50									17.5	225.5	-16.6	1.8	2.3
		.4	19.7	1817	1817	.2	10.8	9	-0					
18TH	226.00									17.1	205.8	-13.9	1.6	2.1
		.5	19.8	1817	1817	.3	10.9	9	-0					
19TH	238.50									16.6	186.0	-11.5	1.4	1.9
		.5	20.2	1817	1817	.3	11.1	10	-0					
20TH	251.00									16.1	165.8	-9.3	1.2	1.7
		.4	21.0	1817	1817	.2	11.6	9	-0					
21ST	263.50									15.8	144.8	-7.3	1.0	1.5
		.4	27.7	2325	2325	.2	11.9	9	-0					
22ND	279.50									15.4	117.1	-5.2	.7	1.3
		1.9	17.5	1570	1570	1.2	11.2	14	-2					
23RD	292.00									13.5	99.5	-3.9	.6	1.0
		2.2	24.8	2005	2005	1.1	12.4	11	-1					
24TH	308.00									11.3	74.7	-2.5	.4	.7
		2.1	13.8	1317	1317	1.6	10.5	11	-2					
25TH	320.50									9.2	60.9	-1.6	.2	.6
		3.1	21.5	1685	1685	1.8	12.7	9	-1					
26TH	336.50									6.1	39.5	-.8	.1	.4
		1.9	12.2	1276	1276	1.5	9.6	11	-2					
27TH	349.00									4.2	27.2	-.4	.1	.2
		2.5	12.0	1275	1275	1.9	9.4	14	-3					
EAVE	361.50									1.7	15.3	-.1	.0	.1
		1.7	15.3	1182	1182	1.5	12.9	5	-1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS, TEXAS
WIND DIRECTION 40 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-167.3	684.7	-120.9	-28.7	3.8
		-20.9	54.0	4039	4039	-5.2	13.4	-1	-1					
2ND	26.00									-146.4	630.7	-103.8	-24.6	3.9
		-8.8	28.0	1942	1942	-4.5	14.4	-2	-1					
3RD	38.50									-137.6	602.6	-96.1	-22.8	4.0
		-8.0	28.6	1942	1942	-4.1	14.7	-2	-0					
4TH	51.00									-129.6	574.0	-88.8	-21.1	4.1
		-5.0	25.1	1942	1942	-2.6	12.9	-2	-0					
5TH	63.50									-124.6	548.9	-81.8	-19.5	4.1
		-2.9	21.0	1942	1942	-1.5	10.8	-3	-0					
6TH	76.00									-121.7	527.9	-75.0	-18.0	4.2
		-4.2	22.7	1843	1843	-2.3	12.3	4	1					
7TH	88.50									-117.5	505.2	-68.6	-16.5	4.1
		-4.3	22.9	1817	1817	-2.4	12.6	6	1					
8TH	101.00									-113.2	482.2	-62.4	-15.1	3.9
		-4.4	22.7	1817	1817	-2.4	12.5	6	1					
9TH	113.50									-108.8	459.5	-56.5	-13.7	3.8
		-4.5	22.5	1817	1817	-2.5	12.4	6	1					
10TH	126.00									-104.3	437.0	-50.9	-12.3	3.7
		-4.5	22.7	1817	1817	-2.5	12.5	7	1					
11TH	138.50									-99.8	414.3	-45.6	-11.1	3.5
		-4.6	23.1	1817	1817	-2.5	12.7	8	2					
12TH	151.00									-95.2	391.2	-40.6	-9.9	3.3
		-4.6	23.4	1817	1817	-2.5	12.9	8	2					
13TH	163.50									-90.6	367.8	-35.8	-8.7	3.1
		-4.9	23.7	1817	1817	-2.7	13.0	9	2					
14TH	176.00									-85.7	344.1	-31.4	-7.6	2.9
		-5.3	23.9	1817	1817	-2.9	13.1	8	2					
15TH	188.50									-80.4	320.2	-27.2	-6.6	2.7
		-5.7	24.0	1817	1817	-3.1	13.2	8	2					
16TH	201.00									-74.8	296.2	-23.4	-5.6	2.5
		-6.1	24.2	1817	1817	-3.4	13.3	7	2					
17TH	213.50									-68.7	272.0	-19.8	-4.7	2.3
		-6.6	24.3	1817	1817	-3.6	13.4	8	2					
18TH	226.00									-62.1	247.7	-16.6	-3.9	2.1
		-7.0	24.4	1817	1817	-3.9	13.4	8	2					
19TH	238.50									-55.1	223.3	-13.6	-3.1	1.9
		-7.5	24.8	1817	1817	-4.1	13.6	8	2					
20TH	251.00									-47.6	198.5	-11.0	-2.5	1.7
		-7.8	25.7	1817	1817	-4.3	14.1	7	2					
21ST	263.50									-39.8	172.8	-8.7	-1.9	1.5
		-10.3	34.0	2325	2325	-4.4	14.6	5	2					
22ND	279.50									-29.5	138.9	-6.2	-1.4	1.3
		-4.0	20.6	1570	1570	-2.6	13.1	12	2					
23RD	292.00									-25.4	118.2	-4.6	-1.0	1.1
		-6.6	29.5	2005	2005	-3.3	14.7	9	2					
24TH	308.00									-18.9	88.8	-2.9	-.7	.8
		-3.0	16.8	1317	1317	-2.3	12.8	10	2					
25TH	320.50									-15.9	71.9	-1.9	-.5	.6
		-4.2	25.5	1685	1685	-2.5	15.1	9	1					
26TH	336.50									-11.6	46.5	-.9	-.3	.4
		-3.8	15.1	1276	1276	-3.0	11.9	8	2					
27TH	349.00									-7.9	31.3	-.5	-.1	.3
		-2.3	13.9	1275	1275	-1.8	10.9	13	2					
EAVE	361.50									-5.5	17.5	-.2	-.0	.1
		-5.5	17.5	1182	1182	-4.7	14.8	4	1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 50 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-368.6	683.9	-120.4	-69.8	2.8
		-26.1	54.5	4039	4039	-6.5	13.5	-0	-0					
2ND	26.00									-342.5	629.4	-103.3	-60.6	2.9
		-12.6	27.8	1942	1942	-6.5	14.3	-2	-1					
3RD	38.50									-330.0	601.6	-95.6	-56.4	2.9
		-12.8	28.2	1942	1942	-6.6	14.5	-2	-1					
4TH	51.00									-317.2	573.4	-88.3	-52.4	3.0
		-10.6	25.6	1942	1942	-5.4	13.2	-1	-1					
5TH	63.50									-306.6	547.8	-81.2	-48.5	3.1
		-7.4	22.6	1942	1942	-3.8	11.7	-0	-0					
6TH	76.00									-299.1	525.2	-74.5	-44.7	3.1
		-10.3	22.9	1843	1843	-5.6	12.4	3	1					
7TH	88.50									-288.9	502.3	-68.1	-41.0	3.0
		-10.8	22.9	1817	1817	-6.0	12.6	4	2					
8TH	101.00									-278.0	479.4	-62.0	-37.4	2.9
		-10.9	22.8	1817	1817	-6.0	12.6	5	2					
9TH	113.50									-267.1	456.5	-56.1	-34.0	2.7
		-11.0	22.7	1817	1817	-6.1	12.5	5	2					
10TH	126.00									-256.1	433.8	-50.6	-30.8	2.6
		-11.5	22.8	1817	1817	-6.3	12.5	5	3					
11TH	138.50									-244.6	411.0	-45.3	-27.6	2.5
		-12.2	23.0	1817	1817	-6.7	12.6	5	3					
12TH	151.00									-232.4	388.1	-40.3	-24.7	2.3
		-12.8	23.1	1817	1817	-7.1	12.7	5	3					
13TH	163.50									-219.6	365.0	-35.6	-21.8	2.2
		-13.1	23.3	1817	1817	-7.2	12.8	5	3					
14TH	176.00									-206.5	341.6	-31.2	-19.2	2.0
		-13.2	23.6	1817	1817	-7.3	13.0	5	3					
15TH	188.50									-193.2	318.1	-27.0	-16.7	1.9
		-13.3	23.8	1817	1817	-7.3	13.1	5	3					
16TH	201.00									-179.9	294.3	-23.2	-14.3	1.7
		-13.6	24.0	1817	1817	-7.5	13.2	5	3					
17TH	213.50									-166.3	270.3	-19.7	-12.2	1.6
		-14.3	24.1	1817	1817	-7.8	13.3	5	3					
18TH	226.00									-152.1	246.2	-16.5	-10.2	1.4
		-14.9	24.2	1817	1817	-8.2	13.3	5	3					
19TH	238.50									-137.2	222.0	-13.5	-8.4	1.2
		-15.6	24.5	1817	1817	-8.6	13.5	5	3					
20TH	251.00									-121.6	197.5	-10.9	-6.8	1.0
		-16.3	25.3	1817	1817	-9.0	13.9	4	2					
21ST	263.50									-105.3	172.2	-8.6	-5.3	.9
		-21.6	33.1	2325	2325	-9.3	14.2	2	2					
22ND	279.50									-83.7	139.1	-6.1	-3.8	.8
		-12.2	21.1	1570	1570	-7.8	13.4	5	3					
23RD	292.00									-71.5	118.1	-4.5	-2.9	.7
		-17.9	29.8	2005	2005	-8.9	14.8	4	3					
24TH	308.00									-53.6	88.3	-2.9	-1.9	.5
		-9.6	17.3	1317	1317	-7.3	13.2	5	3					
25TH	320.50									-44.0	71.0	-1.9	-1.3	.4
		-13.1	24.9	1685	1685	-7.8	14.8	3	2					
26TH	336.50									-30.9	46.0	-.9	-.7	.3
		-9.7	15.8	1276	1276	-7.6	12.4	4	3					
27TH	349.00									-21.2	30.2	-.4	-.3	.2
		-8.5	13.5	1275	1275	-6.6	10.6	8	5					
EAVE	361.50									-12.7	16.7	-.2	-.1	.0
		-12.7	16.7	1182	1182	-10.8	14.2	1	1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 60 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-632.3	768.7	-134.5	-122.5	-.9
		-35.5	61.8	4039	4039	-8.8	15.3	-4	-2					
2ND	26.00									-596.8	706.9	-115.3	-106.5	-.6
		-18.7	31.3	1942	1942	-9.6	16.1	-5	-3					
3RD	38.50									-578.1	675.6	-106.6	-99.2	-.4
		-19.7	31.6	1942	1942	-10.1	16.3	-4	-2					
4TH	51.00									-558.4	644.0	-98.4	-92.1	-.2
		-19.7	29.9	1942	1942	-10.2	15.4	-5	-3					
5TH	63.50									-538.7	614.1	-90.5	-85.2	.0
		-14.8	27.2	1942	1942	-7.6	14.0	-2	-1					
6TH	76.00									-523.8	586.9	-83.0	-78.6	.1
		-17.9	26.7	1843	1843	-9.7	14.5	-1	-1					
7TH	88.50									-505.9	560.1	-75.9	-72.2	.1
		-19.0	26.2	1817	1817	-10.5	14.4	0	0					
8TH	101.00									-486.9	533.9	-69.0	-66.0	.1
		-19.5	25.9	1817	1817	-10.7	14.2	0	0					
9TH	113.50									-467.4	508.0	-62.5	-60.0	.1
		-19.9	25.5	1817	1817	-11.0	14.0	1	1					
10TH	126.00									-447.5	482.5	-56.3	-54.3	.0
		-20.5	25.4	1817	1817	-11.3	14.0	1	1					
11TH	138.50									-427.0	457.1	-50.4	-48.8	-.0
		-21.1	25.5	1817	1817	-11.6	14.1	1	1					
12TH	151.00									-405.9	431.6	-44.9	-43.6	-.0
		-21.6	25.6	1817	1817	-11.9	14.1	1	1					
13TH	163.50									-384.3	405.9	-39.7	-38.7	-.1
		-22.2	25.8	1817	1817	-12.2	14.2	1	1					
14TH	176.00									-362.1	380.1	-34.7	-34.0	-.1
		-22.8	26.1	1817	1817	-12.5	14.3	1	1					
15TH	188.50									-339.3	354.1	-30.2	-29.6	-.2
		-23.3	26.3	1817	1817	-12.8	14.5	1	0					
16TH	201.00									-316.0	327.8	-25.9	-25.5	-.2
		-23.9	26.5	1817	1817	-13.2	14.6	0	0					
17TH	213.50									-292.1	301.3	-22.0	-21.7	-.2
		-24.5	26.6	1817	1817	-13.5	14.6	0	0					
18TH	226.00									-267.6	274.7	-18.4	-18.2	-.2
		-25.1	26.7	1817	1817	-13.8	14.7	0	0					
19TH	238.50									-242.5	248.1	-15.1	-15.0	-.2
		-26.0	27.0	1817	1817	-14.3	14.9	-0	-0					
20TH	251.00									-216.5	221.1	-12.2	-12.2	-.2
		-27.3	27.9	1817	1817	-15.0	15.3	-1	-1					
21ST	263.50									-189.2	193.2	-9.6	-9.6	-.1
		-36.6	36.7	2325	2325	-15.7	15.8	-2	-2					
22ND	279.50									-152.6	156.5	-6.8	-6.9	.0
		-22.4	24.4	1570	1570	-14.3	15.6	1	0					
23RD	292.00									-130.2	132.1	-5.0	-5.1	.0
		-31.3	33.3	2005	2005	-15.6	16.6	-0	-0					
24TH	308.00									-98.9	98.7	-3.1	-3.3	.0
		-18.8	20.8	1317	1317	-14.3	15.8	-0	-0					
25TH	320.50									-80.1	78.0	-2.0	-2.2	.0
		-25.5	27.7	1685	1685	-15.1	16.4	-0	-0					
26TH	336.50									-54.6	50.3	-1.0	-1.1	.0
		-18.1	17.5	1276	1276	-14.2	13.7	0	0					
27TH	349.00									-36.5	32.8	-.5	-.5	.0
		-16.3	14.9	1275	1275	-12.8	11.7	1	1					
EAVE	361.50									-20.2	17.8	-.2	-.2	.0
		-20.2	17.8	1182	1182	-17.1	15.1	0	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 70 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-730.2	732.1	-126.5	-142.0	-2.3
		-37.8	59.8	4039	4039	-9.4	14.8	-5	-3					
2ND	26.00									-692.4	672.3	-108.2	-123.5	-1.9
		-21.0	29.7	1942	1942	-10.8	15.3	-4	-3					
3RD	38.50									-671.4	642.6	-100.0	-115.0	-1.7
		-22.5	29.6	1942	1942	-11.6	15.2	-3	-2					
4TH	51.00									-648.8	613.0	-92.2	-106.7	-1.5
		-23.4	30.2	1942	1942	-12.0	15.6	-1	-1					
5TH	63.50									-625.5	582.8	-84.7	-98.7	-1.5
		-18.6	26.7	1942	1942	-9.6	13.8	2	1					
6TH	76.00									-606.9	556.0	-77.6	-91.0	-1.6
		-21.6	26.4	1843	1843	-11.7	14.3	-1	-1					
7TH	88.50									-585.2	529.7	-70.8	-83.6	-1.5
		-22.6	25.8	1817	1817	-12.4	14.2	-1	-1					
8TH	101.00									-562.6	503.8	-64.3	-76.4	-1.5
		-22.9	25.3	1817	1817	-12.6	13.9	-1	-1					
9TH	113.50									-539.7	478.5	-58.2	-69.5	-1.5
		-23.2	24.8	1817	1817	-12.8	13.6	-1	-0					
10TH	126.00									-516.5	453.7	-52.4	-62.9	-1.4
		-23.8	24.6	1817	1817	-13.1	13.5	-1	-1					
11TH	138.50									-492.8	429.2	-46.9	-56.6	-1.4
		-24.4	24.5	1817	1817	-13.4	13.5	-1	-1					
12TH	151.00									-468.4	404.6	-41.6	-50.6	-1.4
		-25.0	24.5	1817	1817	-13.8	13.5	-1	-1					
13TH	163.50									-443.4	380.2	-36.7	-44.9	-1.3
		-25.6	24.6	1817	1817	-14.1	13.5	-1	-1					
14TH	176.00									-417.8	355.6	-32.1	-39.5	-1.3
		-26.0	24.8	1817	1817	-14.3	13.7	-1	-1					
15TH	188.50									-391.8	330.8	-27.9	-34.5	-1.2
		-26.5	25.0	1817	1817	-14.6	13.8	-1	-1					
16TH	201.00									-365.3	305.7	-23.9	-29.7	-1.2
		-27.0	25.2	1817	1817	-14.9	13.9	-1	-1					
17TH	213.50									-338.3	280.5	-20.2	-25.3	-1.1
		-27.7	25.2	1817	1817	-15.2	13.9	-1	-1					
18TH	226.00									-310.6	255.3	-16.9	-21.3	-1.0
		-28.3	25.3	1817	1817	-15.6	13.9	-1	-1					
19TH	238.50									-282.3	230.0	-13.8	-17.6	-1.0
		-29.3	25.6	1817	1817	-16.1	14.1	-1	-1					
20TH	251.00									-253.0	204.4	-11.1	-14.2	-.9
		-31.2	26.7	1817	1817	-17.2	14.7	-2	-3					
21ST	263.50									-221.8	177.8	-8.7	-11.3	-.8
		-42.3	35.6	2325	2325	-18.2	15.3	-3	-4					
22ND	279.50									-179.5	142.2	-6.2	-8.1	-.5
		-26.6	22.5	1570	1570	-17.0	14.3	-2	-2					
23RD	292.00									-152.9	119.7	-4.5	-6.0	-.4
		-37.0	30.5	2005	2005	-18.4	15.2	-2	-2					
24TH	308.00									-115.9	89.2	-2.9	-3.8	-.2
		-22.5	18.4	1317	1317	-17.1	14.0	-1	-2					
25TH	320.50									-93.5	70.8	-1.9	-2.5	-.2
		-30.7	24.4	1685	1685	-18.2	14.5	-2	-2					
26TH	336.50									-62.8	46.4	-.9	-1.3	-.1
		-21.1	16.4	1276	1276	-16.5	12.9	-0	-1					
27TH	349.00									-41.7	29.9	-.4	-.6	-.1
		-18.5	13.1	1275	1275	-14.5	10.3	-1	-2					
EAVE	361.50									-23.2	16.8	-.2	-.2	-.0
		-23.2	16.8	1182	1182	-19.6	14.2	-0	-1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 80 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-750.4	644.0	-108.0	-145.6	-2.7
		-36.6	54.5	4039	4039	-9.1	13.5	-4	-3					
2ND	26.00									-713.8	589.5	-91.9	-126.6	-2.4
		-22.6	26.4	1942	1942	-11.6	13.6	-1	-1					
3RD	38.50									-691.3	563.1	-84.7	-117.8	-2.3
		-23.5	26.0	1942	1942	-12.1	13.4	-1	-1					
4TH	51.00									-667.8	537.0	-77.8	-109.3	-2.3
		-24.5	28.1	1942	1942	-12.6	14.5	-0	-0					
5TH	63.50									-643.3	509.0	-71.3	-101.1	-2.2
		-19.5	25.3	1942	1942	-10.1	13.0	3	2					
6TH	76.00									-623.8	483.7	-65.1	-93.2	-2.4
		-22.8	25.0	1843	1843	-12.4	13.5	-1	-1					
7TH	88.50									-601.0	458.7	-59.2	-85.5	-2.3
		-23.8	24.4	1817	1817	-13.1	13.4	-1	-1					
8TH	101.00									-577.2	434.3	-53.6	-78.2	-2.3
		-24.0	23.9	1817	1817	-13.2	13.1	-1	-1					
9TH	113.50									-553.2	410.4	-48.4	-71.1	-2.2
		-24.3	23.4	1817	1817	-13.4	12.9	-1	-1					
10TH	126.00									-528.9	387.0	-43.4	-64.3	-2.2
		-24.7	23.0	1817	1817	-13.6	12.7	-1	-1					
11TH	138.50									-504.2	364.1	-38.7	-57.9	-2.1
		-25.2	22.6	1817	1817	-13.9	12.4	-2	-2					
12TH	151.00									-479.0	341.5	-34.3	-51.7	-2.0
		-25.8	22.2	1817	1817	-14.2	12.2	-2	-2					
13TH	163.50									-453.2	319.3	-30.1	-45.9	-1.9
		-26.1	21.9	1817	1817	-14.4	12.0	-2	-2					
14TH	176.00									-427.1	297.4	-26.3	-40.4	-1.8
		-26.3	21.7	1817	1817	-14.5	11.9	-2	-2					
15TH	188.50									-400.7	275.7	-22.7	-35.2	-1.7
		-26.6	21.5	1817	1817	-14.6	11.8	-2	-3					
16TH	201.00									-374.1	254.3	-19.4	-30.4	-1.6
		-27.1	21.4	1817	1817	-14.9	11.8	-2	-3					
17TH	213.50									-347.1	232.8	-16.3	-25.9	-1.5
		-28.0	21.7	1817	1817	-15.4	11.9	-2	-2					
18TH	226.00									-319.1	211.2	-13.6	-21.7	-1.4
		-28.9	21.9	1817	1817	-15.9	12.0	-2	-2					
19TH	238.50									-290.2	189.3	-11.1	-17.9	-1.2
		-30.1	22.4	1817	1817	-16.6	12.3	-2	-2					
20TH	251.00									-260.1	166.9	-8.8	-14.5	-1.1
		-32.3	23.5	1817	1817	-17.8	12.9	-2	-3					
21ST	263.50									-227.8	143.4	-6.9	-11.4	-1.0
		-44.3	31.6	2325	2325	-19.0	13.6	-2	-3					
22ND	279.50									-183.5	111.9	-4.9	-8.1	-.8
		-28.0	17.9	1570	1570	-17.9	11.4	-3	-4					
23RD	292.00									-155.5	94.0	-3.6	-6.0	-.6
		-38.4	23.9	2005	2005	-19.1	11.9	-3	-4					
24TH	308.00									-117.1	70.1	-2.3	-3.8	-.4
		-22.8	14.5	1317	1317	-17.3	11.0	-2	-4					
25TH	320.50									-94.3	55.6	-1.5	-2.5	-.3
		-32.1	18.8	1685	1685	-19.1	11.1	-2	-4					
26TH	336.50									-62.2	36.8	-.7	-1.2	-.1
		-20.9	13.1	1276	1276	-16.4	10.3	-1	-1					
27TH	349.00									-41.3	23.6	-.4	-.6	-.1
		-18.7	10.0	1275	1275	-14.7	7.9	-2	-3					
EAVE	361.50									-22.6	13.6	-.1	-.2	-.0
		-22.6	13.6	1182	1182	-19.1	11.5	-1	-1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 90 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-1052.3	610.5	-96.3	-204.2	-5.2
		-48.2	61.0	4039	4039	-11.9	15.1	-4	-3					
2ND	26.00									-1004.1	549.4	-81.2	-177.5	-4.8
		-28.4	29.1	1942	1942	-14.6	15.0	-3	-3					
3RD	38.50									-975.7	520.3	-74.5	-165.1	-4.6
		-32.1	28.7	1942	1942	-16.5	14.8	-1	-2					
4TH	51.00									-943.6	491.6	-68.2	-153.1	-4.5
		-34.1	30.0	1942	1942	-17.6	15.4	-0	-0					
5TH	63.50									-909.5	461.6	-62.2	-141.6	-4.5
		-26.4	26.2	1942	1942	-13.6	13.5	2	2					
6TH	76.00									-883.1	435.5	-56.6	-130.4	-4.7
		-32.3	24.9	1843	1843	-17.5	13.5	-2	-2					
7TH	88.50									-850.7	410.6	-51.3	-119.5	-4.5
		-34.0	24.0	1817	1817	-18.7	13.2	-2	-3					
8TH	101.00									-816.8	386.5	-46.3	-109.1	-4.4
		-34.4	23.4	1817	1817	-18.9	12.9	-2	-3					
9TH	113.50									-782.4	363.2	-41.7	-99.1	-4.2
		-34.8	22.7	1817	1817	-19.2	12.5	-2	-3					
10TH	126.00									-747.6	340.5	-37.3	-89.5	-4.0
		-35.6	21.9	1817	1817	-19.6	12.0	-2	-4					
11TH	138.50									-711.9	318.7	-33.1	-80.4	-3.9
		-36.7	21.1	1817	1817	-20.2	11.6	-2	-4					
12TH	151.00									-675.3	297.6	-29.3	-71.8	-3.7
		-37.7	20.2	1817	1817	-20.7	11.1	-2	-4					
13TH	163.50									-637.6	277.4	-25.7	-63.5	-3.4
		-38.3	19.7	1817	1817	-21.1	10.8	-2	-5					
14TH	176.00									-599.3	257.7	-22.3	-55.8	-3.2
		-38.7	19.3	1817	1817	-21.3	10.6	-2	-5					
15TH	188.50									-560.6	238.5	-19.2	-48.6	-3.0
		-39.0	18.9	1817	1817	-21.5	10.4	-2	-5					
16TH	201.00									-521.6	219.6	-16.4	-41.8	-2.8
		-39.6	18.7	1817	1817	-21.8	10.3	-2	-4					
17TH	213.50									-482.0	200.8	-13.8	-35.5	-2.6
		-40.5	19.0	1817	1817	-22.3	10.4	-2	-4					
18TH	226.00									-441.5	181.9	-11.4	-29.8	-2.4
		-41.4	19.2	1817	1817	-22.8	10.6	-2	-4					
19TH	238.50									-400.1	162.6	-9.2	-24.5	-2.2
		-42.8	19.8	1817	1817	-23.6	10.9	-2	-4					
20TH	251.00									-357.3	142.9	-7.3	-19.8	-2.0
		-45.7	21.1	1817	1817	-25.1	11.6	-2	-4					
21ST	263.50									-311.6	121.8	-5.6	-15.6	-1.8
		-62.4	28.7	2325	2325	-26.8	12.4	-2	-4					
22ND	279.50									-249.3	93.1	-3.9	-11.1	-1.5
		-37.8	15.8	1570	1570	-24.1	10.0	-3	-7					
23RD	292.00									-211.4	77.3	-2.9	-8.2	-1.2
		-52.1	21.6	2005	2005	-26.0	10.8	-2	-5					
24TH	308.00									-159.4	55.7	-1.8	-5.3	-.8
		-30.6	11.4	1317	1317	-23.2	8.6	-2	-5					
25TH	320.50									-128.8	44.4	-1.2	-3.5	-.7
		-43.6	14.8	1685	1685	-25.9	8.8	-2	-5					
26TH	336.50									-85.2	29.6	-.6	-1.7	-.4
		-27.4	11.1	1276	1276	-21.5	8.7	-2	-5					
27TH	349.00									-57.8	18.5	-.3	-.8	-.2
		-26.0	7.8	1275	1275	-20.4	6.1	-2	-5					
EAVE	361.50									-31.8	10.7	-.1	-.3	-.1
		-31.8	10.7	1182	1182	-26.9	9.1	-1	-2					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 100 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-1036.8	309.3	-41.9	-200.9	-4.4
		-46.6	45.9	4039	4039	-11.5	11.4	-4	-4					
2ND	26.00									-990.2	263.4	-34.4	-174.6	-4.0
		-28.6	21.1	1942	1942	-14.7	10.9	-2	-2					
3RD	38.50									-961.6	242.3	-31.3	-162.4	-3.9
		-32.8	20.2	1942	1942	-16.9	10.4	-0	-1					
4TH	51.00									-928.7	222.1	-28.4	-150.6	-3.9
		-33.3	17.0	1942	1942	-17.2	8.7	-1	-1					
5TH	63.50									-895.4	205.1	-25.7	-139.2	-3.8
		-24.2	16.4	1942	1942	-12.5	8.4	1	2					
6TH	76.00									-871.2	188.7	-23.2	-128.1	-3.9
		-32.1	14.5	1843	1843	-17.4	7.9	-1	-3					
7TH	88.50									-839.1	174.2	-21.0	-117.4	-3.8
		-34.3	12.9	1817	1817	-18.9	7.1	-2	-4					
8TH	101.00									-804.8	161.3	-18.9	-107.2	-3.6
		-34.9	11.7	1817	1817	-19.2	6.4	-1	-4					
9TH	113.50									-770.0	149.6	-16.9	-97.3	-3.4
		-35.4	10.5	1817	1817	-19.5	5.8	-1	-4					
10TH	126.00									-734.6	139.1	-15.1	-87.9	-3.3
		-35.9	9.7	1817	1817	-19.8	5.4	-1	-4					
11TH	138.50									-698.7	129.4	-13.4	-79.0	-3.1
		-36.4	9.2	1817	1817	-20.0	5.1	-1	-4					
12TH	151.00									-662.3	120.2	-11.9	-70.5	-2.9
		-36.9	8.6	1817	1817	-20.3	4.8	-1	-4					
13TH	163.50									-625.4	111.5	-10.4	-62.4	-2.8
		-37.5	8.1	1817	1817	-20.6	4.5	-1	-4					
14TH	176.00									-587.9	103.4	-9.1	-54.8	-2.6
		-38.1	7.6	1817	1817	-21.0	4.2	-1	-4					
15TH	188.50									-549.7	95.8	-7.8	-47.7	-2.4
		-38.8	7.0	1817	1817	-21.3	3.9	-1	-4					
16TH	201.00									-511.0	88.8	-6.7	-41.1	-2.3
		-39.4	6.8	1817	1817	-21.7	3.8	-1	-4					
17TH	213.50									-471.5	82.0	-5.6	-34.9	-2.1
		-40.1	7.2	1817	1817	-22.1	3.9	-1	-4					
18TH	226.00									-431.5	74.8	-4.6	-29.3	-1.9
		-40.7	7.5	1817	1817	-22.4	4.1	-1	-4					
19TH	238.50									-390.8	67.3	-3.7	-24.2	-1.7
		-41.8	7.9	1817	1817	-23.0	4.3	-1	-5					
20TH	251.00									-349.0	59.5	-3.0	-19.5	-1.5
		-44.4	8.7	1817	1817	-24.4	4.8	-1	-5					
21ST	263.50									-304.6	50.8	-2.3	-15.5	-1.3
		-60.7	12.4	2325	2325	-26.1	5.3	-1	-6					
22ND	279.50									-243.9	38.4	-1.6	-11.1	-.9
		-35.8	7.2	1570	1570	-22.8	4.6	-1	-5					
23RD	292.00									-208.1	31.2	-1.1	-8.2	-.7
		-50.2	10.1	2005	2005	-25.1	5.0	-1	-4					
24TH	308.00									-157.8	21.1	-.7	-5.3	-.6
		-28.7	3.9	1317	1317	-21.8	2.9	-1	-6					
25TH	320.50									-129.2	17.3	-.5	-3.5	-.4
		-42.3	6.2	1685	1685	-25.1	3.7	-1	-4					
26TH	336.50									-86.8	11.1	-.2	-1.8	-.2
		-26.9	4.0	1276	1276	-21.1	3.2	-1	-4					
27TH	349.00									-60.0	7.1	-.1	-.9	-.1
		-27.0	2.3	1275	1275	-21.2	1.8	-0	-2					
EAVE	361.50									-33.0	4.8	-.0	-.3	-.0
		-33.0	4.8	1182	1182	-27.9	4.0	-0	-1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 110 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-928.1	120.9	-9.1	-179.1	.3
		-41.8	33.9	4039	4039	-10.4	8.4	-2	-3					
2ND	26.00									-886.3	87.0	-6.4	-155.5	.5
		-26.2	14.6	1942	1942	-13.5	7.5	-0	-0					
3RD	38.50									-860.1	72.4	-5.5	-144.6	.5
		-30.5	13.9	1942	1942	-15.7	7.1	0	1					
4TH	51.00									-829.6	58.5	-4.6	-134.0	.5
		-30.7	8.0	1942	1942	-15.8	4.1	-1	-5					
5TH	63.50									-799.0	50.5	-4.0	-123.8	.6
		-21.0	10.1	1942	1942	-10.8	5.2	-0	-1					
6TH	76.00									-777.9	40.4	-3.4	-114.0	.6
		-28.2	7.0	1843	1843	-15.3	3.8	-1	-2					
7TH	88.50									-749.7	33.5	-2.9	-104.4	.7
		-30.4	5.1	1817	1817	-16.8	2.8	-0	-2					
8TH	101.00									-719.3	28.4	-2.5	-95.3	.8
		-30.9	3.8	1817	1817	-17.0	2.1	-0	-2					
9TH	113.50									-688.3	24.6	-2.2	-86.5	.8
		-31.5	2.4	1817	1817	-17.3	1.3	-0	-1					
10TH	126.00									-656.9	22.2	-1.9	-78.1	.8
		-32.3	1.9	1817	1817	-17.8	1.1	-0	-1					
11TH	138.50									-624.6	20.2	-1.6	-70.0	.9
		-33.3	1.8	1817	1817	-18.3	1.0	-0	-1					
12TH	151.00									-591.3	18.4	-1.4	-62.4	.9
		-34.2	1.7	1817	1817	-18.8	.9	-0	-0					
13TH	163.50									-557.1	16.7	-1.2	-55.3	.9
		-34.8	1.6	1817	1817	-19.1	.9	-0	-0					
14TH	176.00									-522.3	15.1	-1.0	-48.5	.9
		-35.0	1.5	1817	1817	-19.3	.8	-0	-0					
15TH	188.50									-487.3	13.6	-.8	-42.2	.9
		-35.2	1.4	1817	1817	-19.4	.8	0	0					
16TH	201.00									-452.0	12.2	-.6	-36.3	.9
		-35.5	1.5	1817	1817	-19.5	.8	0	0					
17TH	213.50									-416.5	10.7	-.5	-30.9	.9
		-35.8	1.6	1817	1817	-19.7	.9	0	1					
18TH	226.00									-380.8	9.1	-.4	-25.9	.9
		-36.0	1.8	1817	1817	-19.8	1.0	0	2					
19TH	238.50									-344.8	7.3	-.3	-21.4	.8
		-37.0	1.8	1817	1817	-20.3	1.0	0	2					
20TH	251.00									-307.8	5.6	-.2	-17.3	.7
		-39.4	1.3	1817	1817	-21.7	.7	0	1					
21ST	263.50									-268.4	4.3	-.1	-13.7	.7
		-53.2	1.0	2325	2325	-22.9	.4	0	0					
22ND	279.50									-215.3	3.2	-.1	-9.8	.7
		-30.8	1.5	1570	1570	-19.6	1.0	0	5					
23RD	292.00									-184.5	1.7	-.0	-7.3	.5
		-44.2	.6	2005	2005	-22.0	.3	0	2					
24TH	308.00									-140.3	1.1	-.0	-4.7	.4
		-25.0	.1	1317	1317	-19.0	.1	0	2					
25TH	320.50									-115.3	1.0	-.0	-3.2	.4
		-38.0	1.2	1685	1685	-22.6	.7	0	2					
26TH	336.50									-77.2	-.1	-.0	-1.6	.3
		-23.4	-.3	1276	1276	-18.4	-.2	-0	5					
27TH	349.00									-53.8	.2	.0	-.8	.2
		-23.9	.2	1275	1275	-18.8	.2	0	5					
EAVE	361.50									-29.9	-.1	.0	-.3	.1
		-29.9	-.1	1182	1182	-25.3	-.1	-0	2					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 120 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-894.3	-204.4	48.7	-174.1	3.1
		-42.8	13.7	4039	4039	-10.6	3.4	-2	-5					
2ND	26.00									-851.4	-218.1	43.2	-151.4	3.3
		-25.7	4.6	1942	1942	-13.2	2.4	-0	-0					
3RD	38.50									-825.7	-222.8	40.4	-141.0	3.4
		-29.1	3.8	1942	1942	-15.0	2.0	0	1					
4TH	51.00									-796.6	-226.6	37.6	-130.8	3.3
		-29.9	-4.8	1942	1942	-15.4	-2.4	2	-10					
5TH	63.50									-766.7	-221.8	34.8	-121.1	3.6
		-20.9	-1.5	1942	1942	-10.8	-.8	0	-2					
6TH	76.00									-745.8	-220.3	32.0	-111.6	3.7
		-27.5	-5.5	1843	1843	-14.9	-3.0	0	-1					
7TH	88.50									-718.4	-214.8	29.3	-102.4	3.7
		-29.1	-7.2	1817	1817	-16.0	-4.0	0	-0					
8TH	101.00									-689.3	-207.6	26.7	-93.6	3.7
		-29.1	-8.3	1817	1817	-16.0	-4.6	-0	1					
9TH	113.50									-660.2	-199.3	24.1	-85.2	3.7
		-29.1	-9.4	1817	1817	-16.0	-5.2	-0	1					
10TH	126.00									-631.1	-189.9	21.7	-77.1	3.7
		-29.5	-9.9	1817	1817	-16.2	-5.4	-1	2					
11TH	138.50									-601.6	-180.0	19.4	-69.4	3.6
		-30.0	-10.0	1817	1817	-16.5	-5.5	-1	4					
12TH	151.00									-571.6	-170.0	17.2	-62.1	3.5
		-30.5	-10.2	1817	1817	-16.8	-5.6	-2	5					
13TH	163.50									-541.1	-159.9	15.1	-55.2	3.3
		-31.0	-10.3	1817	1817	-17.1	-5.7	-2	5					
14TH	176.00									-510.0	-149.6	13.2	-48.6	3.1
		-31.6	-10.4	1817	1817	-17.4	-5.7	-2	5					
15TH	188.50									-478.4	-139.2	11.4	-42.4	3.0
		-32.1	-10.5	1817	1817	-17.7	-5.8	-2	5					
16TH	201.00									-446.3	-128.6	9.7	-36.6	2.8
		-32.8	-10.8	1817	1817	-18.0	-5.9	-2	5					
17TH	213.50									-413.5	-117.8	8.2	-31.3	2.6
		-33.6	-11.1	1817	1817	-18.5	-6.1	-2	5					
18TH	226.00									-379.9	-106.8	6.8	-26.3	2.4
		-34.5	-11.4	1817	1817	-19.0	-6.3	-2	6					
19TH	238.50									-345.5	-95.3	5.5	-21.8	2.2
		-35.6	-11.9	1817	1817	-19.6	-6.6	-2	5					
20TH	251.00									-309.9	-83.4	4.4	-17.7	2.0
		-37.6	-12.9	1817	1817	-20.7	-7.1	-1	4					
21ST	263.50									-272.2	-70.5	3.4	-14.0	1.8
		-51.2	-17.6	2325	2325	-22.0	-7.6	-1	3					
22ND	279.50									-221.1	-52.9	2.5	-10.1	1.7
		-31.6	-8.1	1570	1570	-20.1	-5.1	-3	10					
23RD	292.00									-189.4	-44.9	1.8	-7.5	1.4
		-43.8	-12.0	2005	2005	-21.8	-6.0	-2	6					
24TH	308.00									-145.6	-32.9	1.2	-4.8	1.0
		-26.7	-4.8	1317	1317	-20.3	-3.7	-1	8					
25TH	320.50									-118.9	-28.0	.8	-3.2	.8
		-40.1	-6.7	1685	1685	-23.8	-4.0	-1	7					
26TH	336.50									-78.8	-21.3	.4	-1.6	.6
		-25.3	-7.2	1276	1276	-19.8	-5.6	-2	7					
27TH	349.00									-53.5	-14.2	.2	-.8	.4
		-24.9	-5.2	1275	1275	-19.5	-4.1	-2	10					
EAVE	361.50									-28.6	-8.9	.1	-.3	.1
		-28.6	-8.9	1182	1182	-24.2	-7.5	-1	4					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS

WIND DIRECTION 130 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-766.5	-509.9	97.1	-150.2	3.6
		-37.8	-16.4	4039	4039	-9.4	-4.1	3	-6					
2ND	26.00									-728.6	-493.5	84.1	-130.7	3.9
		-21.7	-10.1	1942	1942	-11.2	-5.2	-1	1					
3RD	38.50									-706.9	-483.4	78.0	-121.8	3.9
		-24.2	-11.1	1942	1942	-12.5	-5.7	-1	3					
4TH	51.00									-682.7	-472.3	72.0	-113.1	3.8
		-25.4	-18.7	1942	1942	-13.1	-9.6	4	-6					
5TH	63.50									-657.3	-453.6	66.2	-104.7	4.0
		-19.5	-16.0	1942	1942	-10.1	-8.3	1	-1					
6TH	76.00									-637.7	-437.6	60.7	-96.6	4.1
		-22.2	-19.6	1843	1843	-12.0	-10.6	-1	1					
7TH	88.50									-615.6	-418.0	55.3	-88.8	4.0
		-23.1	-20.2	1817	1817	-12.7	-11.1	-1	1					
8TH	101.00									-592.4	-397.8	50.2	-81.2	4.0
		-23.4	-20.2	1817	1817	-12.9	-11.1	-2	2					
9TH	113.50									-569.0	-377.6	45.4	-74.0	3.9
		-23.7	-20.2	1817	1817	-13.0	-11.1	-2	2					
10TH	126.00									-545.4	-357.4	40.8	-67.0	3.8
		-24.4	-19.9	1817	1817	-13.5	-10.9	-3	3					
11TH	138.50									-520.9	-337.6	36.4	-60.3	3.7
		-25.4	-19.5	1817	1817	-14.0	-10.7	-3	4					
12TH	151.00									-495.5	-318.1	32.3	-54.0	3.5
		-26.3	-19.0	1817	1817	-14.5	-10.5	-4	5					
13TH	163.50									-469.2	-299.1	28.5	-48.0	3.3
		-27.0	-19.1	1817	1817	-14.9	-10.5	-4	5					
14TH	176.00									-442.2	-280.0	24.9	-42.3	3.1
		-27.4	-19.4	1817	1817	-15.1	-10.7	-4	5					
15TH	188.50									-414.8	-260.6	21.5	-36.9	2.9
		-27.8	-19.7	1817	1817	-15.3	-10.9	-4	5					
16TH	201.00									-387.0	-240.9	18.3	-31.9	2.7
		-28.3	-20.3	1817	1817	-15.6	-11.2	-4	5					
17TH	213.50									-358.7	-220.6	15.5	-27.2	2.4
		-29.0	-21.2	1817	1817	-15.9	-11.6	-4	5					
18TH	226.00									-329.8	-199.4	12.8	-22.9	2.2
		-29.6	-22.0	1817	1817	-16.3	-12.1	-4	5					
19TH	238.50									-300.2	-177.4	10.5	-19.0	2.0
		-30.5	-22.9	1817	1817	-16.8	-12.6	-3	4					
20TH	251.00									-269.7	-154.5	8.4	-15.4	1.8
		-31.7	-23.4	1817	1817	-17.5	-12.9	-2	3					
21ST	263.50									-238.0	-131.1	6.6	-12.3	1.6
		-41.9	-30.7	2325	2325	-18.0	-13.2	-1	2					
22ND	279.50									-196.1	-100.4	4.8	-8.8	1.5
		-28.0	-13.8	1570	1570	-17.9	-8.8	-5	9					
23RD	292.00									-168.0	-86.6	3.6	-6.5	1.2
		-40.3	-20.2	2005	2005	-20.1	-10.1	-3	7					
24TH	308.00									-127.7	-66.4	2.4	-4.1	.8
		-25.3	-11.0	1317	1317	-19.2	-8.4	-3	6					
25TH	320.50									-102.4	-55.4	1.6	-2.7	.6
		-35.5	-14.4	1685	1685	-21.0	-8.6	-2	5					
26TH	336.50									-67.0	-40.9	.8	-1.3	.4
		-22.4	-13.4	1276	1276	-17.6	-10.5	-3	5					
27TH	349.00									-44.5	-27.5	.4	-.6	.3
		-20.2	-11.4	1275	1275	-15.8	-8.9	-5	9					
EAVE	361.50									-24.4	-16.2	.1	-.2	.0
		-24.4	-16.2	1182	1182	-20.6	-13.7	-1	1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 140 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-731.4	-675.2	123.8	-144.1	2.2
		-38.9	-37.6	4039	4039	-9.6	-9.3	4	-4					
2ND	26.00									-692.5	-637.6	106.7	-125.6	2.6
		-21.0	-22.1	1942	1942	-10.8	-11.4	0	-0					
3RD	38.50									-671.5	-615.5	98.9	-117.1	2.6
		-22.3	-24.0	1942	1942	-11.5	-12.4	-1	1					
4TH	51.00									-649.2	-591.5	91.3	-108.8	2.5
		-21.6	-26.2	1942	1942	-11.1	-13.5	2	-1					
5TH	63.50									-627.7	-565.4	84.1	-100.9	2.6
		-18.6	-24.7	1942	1942	-9.6	-12.7	1	-0					
6TH	76.00									-609.1	-540.7	77.2	-93.1	2.6
		-20.6	-24.4	1843	1843	-11.2	-13.2	-0	0					
7TH	88.50									-588.5	-516.3	70.6	-85.6	2.6
		-21.4	-24.2	1817	1817	-11.8	-13.3	-1	1					
8TH	101.00									-567.1	-492.1	64.3	-78.4	2.6
		-21.8	-24.3	1817	1817	-12.0	-13.3	-1	1					
9TH	113.50									-545.3	-467.8	58.3	-71.5	2.5
		-22.2	-24.3	1817	1817	-12.2	-13.4	-1	1					
10TH	126.00									-523.1	-443.5	52.6	-64.8	2.5
		-22.9	-24.1	1817	1817	-12.6	-13.2	-2	2					
11TH	138.50									-500.2	-419.5	47.2	-58.4	2.4
		-23.8	-23.8	1817	1817	-13.1	-13.1	-2	2					
12TH	151.00									-476.4	-395.7	42.1	-52.3	2.3
		-24.6	-23.5	1817	1817	-13.5	-12.9	-3	3					
13TH	163.50									-451.8	-372.3	37.3	-46.5	2.2
		-25.3	-23.2	1817	1817	-13.9	-12.7	-3	3					
14TH	176.00									-426.6	-349.1	32.8	-41.0	2.0
		-25.8	-22.9	1817	1817	-14.2	-12.6	-3	3					
15TH	188.50									-400.7	-326.3	28.6	-35.8	1.9
		-26.4	-22.6	1817	1817	-14.5	-12.4	-3	4					
16TH	201.00									-374.3	-303.7	24.6	-31.0	1.7
		-27.0	-22.7	1817	1817	-14.9	-12.5	-3	4					
17TH	213.50									-347.3	-281.0	21.0	-26.5	1.5
		-27.7	-23.6	1817	1817	-15.2	-13.0	-3	3					
18TH	226.00									-319.6	-257.4	17.6	-22.3	1.4
		-28.4	-24.4	1817	1817	-15.6	-13.5	-2	3					
19TH	238.50									-291.2	-233.0	14.6	-18.5	1.2
		-29.2	-25.3	1817	1817	-16.1	-13.9	-2	2					
20TH	251.00									-262.0	-207.7	11.8	-15.0	1.1
		-30.4	-26.0	1817	1817	-16.8	-14.3	-2	2					
21ST	263.50									-231.6	-181.7	9.4	-11.9	1.0
		-40.6	-34.2	2325	2325	-17.5	-14.7	-2	2					
22ND	279.50									-191.0	-147.6	6.7	-8.6	.8
		-27.7	-21.6	1570	1570	-17.6	-13.8	-3	3					
23RD	292.00									-163.3	-125.9	5.0	-6.3	.7
		-39.2	-29.8	2005	2005	-19.5	-14.8	-3	3					
24TH	308.00									-124.1	-96.2	3.2	-4.0	.5
		-25.3	-18.4	1317	1317	-19.2	-13.9	-2	3					
25TH	320.50									-98.9	-77.8	2.2	-2.6	.4
		-33.5	-23.7	1685	1685	-19.9	-14.1	-2	3					
26TH	336.50									-65.4	-54.1	1.1	-1.3	.2
		-21.2	-17.6	1276	1276	-16.6	-13.8	-2	2					
27TH	349.00									-44.2	-36.5	.5	-.6	.1
		-19.8	-16.2	1275	1275	-15.5	-12.7	-3	4					
EAVE	361.50									-24.4	-20.3	.2	-.2	.0
		-24.4	-20.3	1182	1182	-20.7	-17.1	-0	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 150 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-699.4	-652.8	122.8	-138.0	1.1
		-32.8	-39.6	4039	4039	-8.1	-9.8	-1	1					
2ND	26.00									-666.6	-613.2	106.4	-120.3	1.0
		-18.6	-22.2	1942	1942	-9.6	-11.4	-3	3					
3RD	38.50									-648.0	-591.0	98.9	-112.0	.9
		-20.5	-23.6	1942	1942	-10.6	-12.2	-3	3					
4TH	51.00									-627.5	-567.4	91.6	-104.1	.8
		-20.0	-23.2	1942	1942	-10.3	-12.0	-1	1					
5TH	63.50									-607.4	-544.2	84.7	-96.4	.7
		-18.2	-22.3	1942	1942	-9.4	-11.5	2	-1					
6TH	76.00									-589.3	-521.9	78.0	-88.9	.8
		-20.2	-22.3	1843	1843	-10.9	-12.1	-1	1					
7TH	88.50									-569.1	-499.6	71.6	-81.6	.7
		-21.0	-21.7	1817	1817	-11.5	-11.9	-1	1					
8TH	101.00									-548.1	-477.9	65.5	-74.6	.7
		-21.6	-21.2	1817	1817	-11.9	-11.7	-1	1					
9TH	113.50									-526.5	-456.7	59.7	-67.9	.7
		-22.2	-20.8	1817	1817	-12.2	-11.4	-1	1					
10TH	126.00									-504.3	-435.9	54.1	-61.5	.6
		-22.9	-20.7	1817	1817	-12.6	-11.4	-1	1					
11TH	138.50									-481.4	-415.3	48.8	-55.3	.6
		-23.5	-20.7	1817	1817	-12.9	-11.4	-1	1					
12TH	151.00									-457.9	-394.6	43.7	-49.5	.6
		-24.1	-20.8	1817	1817	-13.3	-11.4	-1	1					
13TH	163.50									-433.8	-373.8	38.9	-43.9	.5
		-24.7	-21.0	1817	1817	-13.6	-11.5	-1	1					
14TH	176.00									-409.1	-352.8	34.4	-38.6	.5
		-25.3	-21.2	1817	1817	-13.9	-11.7	-1	1					
15TH	188.50									-383.8	-331.6	30.1	-33.7	.4
		-25.9	-21.4	1817	1817	-14.2	-11.8	-1	1					
16TH	201.00									-357.9	-310.2	26.1	-29.0	.4
		-26.6	-21.8	1817	1817	-14.7	-12.0	-1	1					
17TH	213.50									-331.3	-288.4	22.3	-24.7	.3
		-27.7	-22.5	1817	1817	-15.2	-12.4	-1	1					
18TH	226.00									-303.6	-265.9	18.9	-20.8	.3
		-28.7	-23.1	1817	1817	-15.8	-12.7	-1	1					
19TH	238.50									-274.9	-242.8	15.7	-17.1	.2
		-29.7	-23.8	1817	1817	-16.3	-13.1	-1	1					
20TH	251.00									-245.2	-218.9	12.8	-13.9	.2
		-30.5	-24.6	1817	1817	-16.8	-13.6	-1	1					
21ST	263.50									-214.8	-194.3	10.2	-11.0	.1
		-40.0	-32.7	2325	2325	-17.2	-14.1	-1	1					
22ND	279.50									-174.8	-161.6	7.4	-7.9	.1
		-25.7	-23.2	1570	1570	-16.4	-14.8	0	-0					
23RD	292.00									-149.2	-138.4	5.5	-5.9	.1
		-35.1	-31.8	2005	2005	-17.5	-15.9	-1	1					
24TH	308.00									-114.1	-106.6	3.5	-3.8	.0
		-22.5	-20.8	1317	1317	-17.1	-15.8	-1	1					
25TH	320.50									-91.6	-85.8	2.3	-2.5	.0
		-29.9	-27.4	1685	1685	-17.8	-16.2	-0	0					
26TH	336.50									-61.6	-58.5	1.2	-1.3	-.0
		-20.0	-18.8	1276	1276	-15.6	-14.7	0	-0					
27TH	349.00									-41.7	-39.7	.6	-.6	-.0
		-19.1	-18.1	1275	1275	-14.9	-14.2	-0	0					
EAVE	361.50									-22.6	-21.6	.2	-.2	-.0
		-22.6	-21.6	1182	1182	-19.1	-18.3	0	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 160 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-455.0	-658.7	129.0	-93.5	.1
		-15.1	-37.6	4039	4039	-3.7	-9.3	-11	5					
2ND	26.00									-439.9	-621.0	112.3	-81.8	-.4
		-10.8	-22.8	1942	1942	-5.5	-11.8	-8	4					
3RD	38.50									-429.1	-598.2	104.7	-76.4	-.6
		-12.5	-24.9	1942	1942	-6.4	-12.8	-5	3					
4TH	51.00									-416.6	-573.3	97.4	-71.1	-.8
		-12.1	-22.0	1942	1942	-6.3	-11.3	-3	2					
5TH	63.50									-404.5	-551.3	90.4	-66.0	-.8
		-10.1	-18.1	1942	1942	-5.2	-9.3	1	-1					
6TH	76.00									-394.4	-533.1	83.6	-61.0	-.8
		-12.5	-19.6	1843	1843	-6.8	-10.6	-1	1					
7TH	88.50									-382.0	-513.6	77.1	-56.1	-.8
		-13.1	-19.7	1817	1817	-7.2	-10.8	-1	1					
8TH	101.00									-368.9	-493.9	70.8	-51.4	-.9
		-13.5	-19.3	1817	1817	-7.4	-10.6	-1	0					
9TH	113.50									-355.4	-474.6	64.7	-46.9	-.9
		-13.9	-18.9	1817	1817	-7.6	-10.4	-0	0					
10TH	126.00									-341.5	-455.7	58.9	-42.6	-.9
		-14.4	-19.1	1817	1817	-7.9	-10.5	0	-0					
11TH	138.50									-327.1	-436.6	53.3	-38.4	-.9
		-15.0	-19.5	1817	1817	-8.3	-10.7	0	-0					
12TH	151.00									-312.1	-417.1	48.0	-34.4	-.9
		-15.6	-19.8	1817	1817	-8.6	-10.9	1	-1					
13TH	163.50									-296.5	-397.2	42.9	-30.6	-.9
		-16.1	-20.2	1817	1817	-8.9	-11.1	1	-1					
14TH	176.00									-280.4	-377.0	38.1	-27.0	-.8
		-16.5	-20.6	1817	1817	-9.1	-11.4	1	-1					
15TH	188.50									-264.0	-356.4	33.5	-23.6	-.8
		-16.8	-21.1	1817	1817	-9.3	-11.6	2	-1					
16TH	201.00									-247.1	-335.3	29.1	-20.4	-.7
		-17.5	-21.6	1817	1817	-9.6	-11.9	2	-2					
17TH	213.50									-229.7	-313.8	25.1	-17.4	-.6
		-18.6	-22.2	1817	1817	-10.2	-12.2	2	-2					
18TH	226.00									-211.1	-291.5	21.3	-14.6	-.6
		-19.7	-22.9	1817	1817	-10.8	-12.6	2	-1					
19TH	238.50									-191.4	-268.6	17.8	-12.1	-.5
		-20.6	-23.9	1817	1817	-11.4	-13.1	1	-1					
20TH	251.00									-170.7	-244.7	14.6	-9.9	-.4
		-21.1	-25.4	1817	1817	-11.6	-14.0	0	-0					
21ST	263.50									-149.7	-219.3	11.7	-7.9	-.4
		-27.6	-34.6	2325	2325	-11.9	-14.9	-1	1					
22ND	279.50									-122.1	-184.8	8.5	-5.7	-.5
		-16.8	-25.3	1570	1570	-10.7	-16.1	2	-1					
23RD	292.00									-105.2	-159.5	6.3	-4.3	-.4
		-23.3	-35.9	2005	2005	-11.6	-17.9	1	-1					
24TH	308.00									-81.9	-123.6	4.0	-2.8	-.3
		-15.4	-24.8	1317	1317	-11.7	-18.9	3	-2					
25TH	320.50									-66.5	-98.8	2.7	-1.8	-.2
		-20.4	-32.6	1685	1685	-12.1	-19.3	1	-1					
26TH	336.50									-46.0	-66.2	1.3	-.9	-.2
		-14.7	-21.7	1276	1276	-11.5	-17.0	2	-1					
27TH	349.00									-31.3	-44.5	.6	-.5	-.1
		-14.0	-20.4	1275	1275	-11.0	-16.0	3	-2					
EAVE	361.50									-17.3	-24.1	.2	-.2	-.0
		-17.3	-24.1	1182	1182	-14.6	-20.4	1	-1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 170 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-255.9	-893.2	175.5	-55.0	-2.0
		-4.6	-52.4	4039	4039	-1.1	-13.0	-13	1					
2ND	26.00									-251.3	-840.8	153.0	-48.4	-2.7
		-5.1	-29.7	1942	1942	-2.6	-15.3	-7	1					
3RD	38.50									-246.2	-811.1	142.7	-45.3	-2.9
		-6.4	-31.6	1942	1942	-3.3	-16.3	-4	1					
4TH	51.00									-239.8	-779.5	132.7	-42.3	-3.1
		-5.4	-27.1	1942	1942	-2.8	-13.9	-3	1					
5TH	63.50									-234.4	-752.4	123.1	-39.3	-3.1
		-3.0	-20.7	1942	1942	-1.6	-10.7	-1	0					
6TH	76.00									-231.4	-731.7	113.9	-36.4	-3.2
		-6.1	-25.1	1843	1843	-3.3	-13.6	-0	0					
7TH	88.50									-225.3	-706.6	104.9	-33.6	-3.2
		-6.9	-26.0	1817	1817	-3.8	-14.3	1	-0					
8TH	101.00									-218.5	-680.6	96.2	-30.8	-3.2
		-7.3	-25.8	1817	1817	-4.0	-14.2	1	-0					
9TH	113.50									-211.2	-654.8	87.9	-28.1	-3.1
		-7.7	-25.7	1817	1817	-4.2	-14.1	2	-1					
10TH	126.00									-203.5	-629.1	79.8	-25.5	-3.0
		-8.0	-26.3	1817	1817	-4.4	-14.5	3	-1					
11TH	138.50									-195.6	-602.8	72.1	-23.0	-3.0
		-8.2	-27.1	1817	1817	-4.5	-14.9	3	-1					
12TH	151.00									-187.3	-575.7	64.8	-20.6	-2.9
		-8.5	-28.0	1817	1817	-4.7	-15.4	3	-1					
13TH	163.50									-178.8	-547.8	57.8	-18.3	-2.8
		-8.9	-28.9	1817	1817	-4.9	-15.9	3	-1					
14TH	176.00									-169.9	-518.9	51.1	-16.2	-2.7
		-9.5	-29.9	1817	1817	-5.3	-16.5	4	-1					
15TH	188.50									-160.3	-488.9	44.8	-14.1	-2.6
		-10.1	-30.9	1817	1817	-5.6	-17.0	4	-1					
16TH	201.00									-150.2	-458.0	38.9	-12.1	-2.4
		-10.8	-31.8	1817	1817	-6.0	-17.5	4	-2					
17TH	213.50									-139.4	-426.2	33.3	-10.3	-2.2
		-11.7	-32.4	1817	1817	-6.5	-17.9	4	-2					
18TH	226.00									-127.7	-393.8	28.2	-8.7	-2.1
		-12.6	-33.1	1817	1817	-6.9	-18.2	4	-2					
19TH	238.50									-115.1	-360.7	23.5	-7.2	-1.9
		-13.4	-34.2	1817	1817	-7.4	-18.8	4	-2					
20TH	251.00									-101.6	-326.4	19.2	-5.8	-1.8
		-13.7	-36.5	1817	1817	-7.6	-20.1	4	-2					
21ST	263.50									-87.9	-289.9	15.4	-4.6	-1.6
		-17.7	-49.6	2325	2325	-7.6	-21.3	4	-1					
22ND	279.50									-70.2	-240.3	11.1	-3.3	-1.3
		-10.5	-32.3	1570	1570	-6.7	-20.6	7	-2					
23RD	292.00									-59.8	-208.0	8.3	-2.5	-1.1
		-13.6	-46.0	2005	2005	-6.8	-22.9	4	-1					
24TH	308.00									-46.2	-162.1	5.4	-1.7	-.9
		-7.3	-31.4	1317	1317	-5.5	-23.9	6	-1					
25TH	320.50									-38.9	-130.7	3.5	-1.2	-.7
		-9.8	-43.0	1685	1685	-5.8	-25.5	5	-1					
26TH	336.50									-29.0	-87.6	1.8	-.6	-.5
		-9.6	-28.7	1276	1276	-7.5	-22.5	4	-1					
27TH	349.00									-19.5	-58.9	.9	-.3	-.3
		-7.2	-26.8	1275	1275	-5.7	-21.0	8	-2					
EAVE	361.50									-12.2	-32.1	.3	-.1	-.1
		-12.2	-32.1	1182	1182	-10.4	-27.2	2	-1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 180 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
BRND	0.00									-28.8	-993.1	193.4	-7.9	-2.4
		-.9	-58.8	4039	4039	-.2	-14.6	-9	0					
2ND	26.00									-27.9	-934.4	168.3	-7.1	-2.9
		-1.3	-32.1	1942	1942	-.7	-16.6	-4	0					
3RD	38.50									-26.6	-902.2	156.8	-6.8	-3.0
		-1.1	-33.7	1942	1942	-.6	-17.3	-2	0					
4TH	51.00									-25.5	-868.6	145.8	-6.5	-3.1
		.9	-29.1	1942	1942	.5	-15.0	1	0					
5TH	63.50									-26.4	-839.5	135.1	-6.1	-3.1
		2.3	-23.2	1942	1942	1.2	-12.0	3	0					
6TH	76.00									-28.8	-816.2	124.7	-5.8	-3.0
		1.4	-28.8	1843	1843	.8	-15.6	3	0					
7TH	88.50									-30.2	-787.4	114.7	-5.4	-2.9
		1.0	-30.1	1817	1817	.5	-16.6	4	0					
8TH	101.00									-31.2	-757.3	105.1	-5.0	-2.8
		.5	-30.0	1817	1817	.3	-16.5	4	0					
9TH	113.50									-31.6	-727.4	95.8	-4.7	-2.7
		.0	-29.9	1817	1817	.0	-16.5	4	0					
10TH	126.00									-31.7	-697.5	86.9	-4.3	-2.6
		-.3	-30.4	1817	1817	-.2	-16.7	4	-0					
11TH	138.50									-31.4	-667.0	78.3	-3.9	-2.5
		-.5	-31.2	1817	1817	-.3	-17.2	3	-0					
12TH	151.00									-30.9	-635.9	70.2	-3.5	-2.3
		-.7	-31.9	1817	1817	-.4	-17.6	3	-0					
13TH	163.50									-30.1	-603.9	62.5	-3.1	-2.2
		-1.0	-32.8	1817	1817	-.5	-18.0	3	-0					
14TH	176.00									-29.2	-571.2	55.1	-2.7	-2.1
		-1.3	-33.6	1817	1817	-.7	-18.5	3	-0					
15TH	188.50									-27.8	-537.6	48.2	-2.4	-2.0
		-1.6	-34.4	1817	1817	-.9	-19.0	3	-0					
16TH	201.00									-26.2	-503.1	41.7	-2.0	-1.9
		-1.9	-35.5	1817	1817	-1.1	-19.5	3	-0					
17TH	213.50									-24.3	-467.7	35.6	-1.7	-1.8
		-2.2	-36.9	1817	1817	-1.2	-20.3	3	-0					
18TH	226.00									-22.1	-430.8	30.0	-1.4	-1.7
		-2.4	-38.2	1817	1817	-1.3	-21.0	3	-0					
19TH	238.50									-19.7	-392.6	24.8	-1.2	-1.6
		-2.6	-39.9	1817	1817	-1.4	-22.0	3	-0					
20TH	251.00									-17.1	-352.6	20.2	-.9	-1.4
		-2.7	-42.7	1817	1817	-1.5	-23.5	3	-0					
21ST	263.50									-14.4	-309.9	16.0	-.7	-1.3
		-3.4	-58.8	2325	2325	-1.5	-25.3	2	-0					
22ND	279.50									-11.0	-251.2	11.6	-.5	-1.2
		-1.2	-35.2	1570	1570	-.7	-22.4	6	-0					
23RD	292.00									-9.9	-215.9	8.6	-.4	-1.0
		-2.7	-50.0	2005	2005	-1.4	-25.0	4	-0					
24TH	308.00									-7.1	-165.9	5.6	-.3	-.8
		-1.3	-30.5	1317	1317	-1.0	-23.2	5	-0					
25TH	320.50									-5.8	-135.4	3.7	-.2	-.6
		-1.6	-43.8	1685	1685	-.9	-26.0	4	-0					
26TH	336.50									-4.2	-91.5	1.9	-.1	-.5
		-1.4	-28.7	1276	1276	-1.1	-22.5	5	-0					
27TH	349.00									-2.8	-62.8	.9	-.1	-.3
		-.0	-28.0	1275	1275	-.0	-21.9	7	-0					
EAVE	361.50									-2.8	-34.9	.3	-.0	-.1
		-2.8	-34.9	1182	1182	-2.4	-29.5	3	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 190 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									268.1	-1018.4	195.9	42.4	2.4
		19.4	-62.2	4039	4039	4.8	-15.4	-8	-2					
2ND	26.00									248.7	-956.2	170.2	35.7	1.9
		10.2	-33.3	1942	1942	5.3	-17.1	-4	-1					
3RD	38.50									238.5	-922.9	158.5	32.6	1.7
		11.2	-34.7	1942	1942	5.8	-17.9	-2	-1					
4TH	51.00									227.2	-888.2	147.1	29.7	1.7
		14.2	-32.3	1942	1942	7.3	-16.6	1	0					
5TH	63.50									213.0	-855.9	136.2	27.0	1.7
		13.8	-24.4	1942	1942	7.1	-12.6	3	1					
6TH	76.00									199.2	-831.5	125.7	24.4	1.8
		13.2	-30.6	1843	1843	7.2	-16.6	0	0					
7TH	88.50									186.0	-800.9	115.5	22.0	1.8
		12.5	-31.8	1817	1817	6.9	-17.5	-0	-0					
8TH	101.00									173.5	-769.1	105.7	19.7	1.8
		11.7	-31.7	1817	1817	6.4	-17.4	-1	-0					
9TH	113.50									161.8	-737.4	96.3	17.6	1.8
		10.9	-31.5	1817	1817	6.0	-17.3	-1	-0					
10TH	126.00									151.0	-705.9	87.2	15.7	1.8
		10.4	-31.9	1817	1817	5.7	-17.5	-1	-0					
11TH	138.50									140.6	-674.1	78.6	13.9	1.7
		10.1	-32.4	1817	1817	5.6	-17.8	-2	-1					
12TH	151.00									130.5	-641.7	70.4	12.2	1.6
		9.8	-33.0	1817	1817	5.4	-18.1	-2	-1					
13TH	163.50									120.7	-608.7	62.6	10.6	1.5
		9.6	-33.7	1817	1817	5.3	-18.5	-3	-1					
14TH	176.00									111.2	-575.0	55.2	9.1	1.5
		9.4	-34.5	1817	1817	5.2	-19.0	-3	-1					
15TH	188.50									101.7	-540.5	48.2	7.8	1.4
		9.3	-35.4	1817	1817	5.1	-19.5	-3	-1					
16TH	201.00									92.5	-505.1	41.7	6.6	1.2
		9.0	-36.3	1817	1817	5.0	-20.0	-3	-1					
17TH	213.50									83.5	-468.9	35.6	5.5	1.1
		8.5	-37.2	1817	1817	4.7	-20.5	-3	-1					
18TH	226.00									74.9	-431.6	30.0	4.5	1.0
		8.1	-38.2	1817	1817	4.4	-21.0	-3	-1					
19TH	238.50									66.9	-393.5	24.8	3.6	.9
		7.8	-39.7	1817	1817	4.3	-21.9	-3	-1					
20TH	251.00									59.0	-353.8	20.1	2.8	.8
		8.6	-43.1	1817	1817	4.7	-23.7	-3	-1					
21ST	263.50									50.4	-310.7	16.0	2.2	.7
		12.3	-60.1	2325	2325	5.3	-25.8	-3	-1					
22ND	279.50									38.2	-250.6	11.5	1.4	.5
		7.6	-35.6	1570	1570	4.8	-22.7	-3	-1					
23RD	292.00									30.6	-215.0	8.6	1.0	.3
		10.5	-50.6	2005	2005	5.3	-25.2	-1	-0					
24TH	308.00									20.1	-164.4	5.5	.6	.3
		4.9	-30.5	1317	1317	3.7	-23.1	-2	-0					
25TH	320.50									15.2	-134.0	3.7	.4	.2
		5.7	-43.5	1685	1685	3.4	-25.8	-3	-0					
26TH	336.50									9.4	-90.5	1.9	.2	.1
		3.4	-27.3	1276	1276	2.7	-21.4	-2	-0					
27TH	349.00									6.0	-63.2	.9	.1	.0
		2.4	-28.3	1275	1275	1.9	-22.2	-1	-0					
EAVE	361.50									3.6	-34.9	.3	.0	-.0
		3.6	-34.9	1182	1182	3.0	-29.5	0	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 200 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									431.1	-1089.2	204.7	69.6	4.6
		34.2	-69.9	4039	4039	8.5	-17.3	-7	-3					
2ND	26.00									396.9	-1019.3	177.3	58.8	3.9
		18.4	-36.8	1942	1942	9.5	-18.9	-3	-2					
3RD	38.50									378.5	-982.5	164.8	54.0	3.8
		19.7	-38.1	1942	1942	10.2	-19.6	-1	-0					
4TH	51.00									358.8	-944.4	152.8	49.4	3.7
		18.3	-34.6	1942	1942	9.4	-17.8	2	1					
5TH	63.50									340.4	-909.9	141.2	45.0	3.9
		15.9	-26.7	1942	1942	8.2	-13.7	5	3					
6TH	76.00									324.5	-883.2	130.0	40.8	4.1
		17.8	-34.5	1843	1843	9.6	-18.7	0	0					
7TH	88.50									306.7	-848.7	119.2	36.9	4.1
		18.0	-35.9	1817	1817	9.9	-19.8	-2	-1					
8TH	101.00									288.7	-812.8	108.8	33.2	4.0
		18.1	-35.8	1817	1817	10.0	-19.7	-3	-1					
9TH	113.50									270.6	-777.0	98.8	29.7	3.9
		18.3	-35.6	1817	1817	10.0	-19.6	-4	-2					
10TH	126.00									252.3	-741.4	89.4	26.4	3.7
		17.8	-35.8	1817	1817	9.8	-19.7	-4	-2					
11TH	138.50									234.6	-705.7	80.3	23.4	3.5
		17.0	-36.1	1817	1817	9.4	-19.9	-4	-2					
12TH	151.00									217.5	-669.5	71.7	20.5	3.4
		16.3	-36.5	1817	1817	9.0	-20.1	-3	-2					
13TH	163.50									201.2	-633.0	63.6	17.9	3.2
		15.7	-37.1	1817	1817	8.6	-20.4	-3	-1					
14TH	176.00									185.5	-596.0	55.9	15.5	3.1
		15.2	-37.8	1817	1817	8.3	-20.8	-4	-1					
15TH	188.50									170.3	-558.2	48.7	13.3	2.9
		14.6	-38.5	1817	1817	8.1	-21.2	-4	-1					
16TH	201.00									155.7	-519.8	41.9	11.2	2.8
		14.2	-39.2	1817	1817	7.8	-21.6	-4	-1					
17TH	213.50									141.5	-480.5	35.7	9.4	2.6
		13.9	-40.1	1817	1817	7.6	-22.1	-4	-1					
18TH	226.00									127.6	-440.4	29.9	7.7	2.4
		13.6	-41.0	1817	1817	7.5	-22.6	-4	-1					
19TH	238.50									114.0	-399.4	24.7	6.2	2.2
		14.0	-42.3	1817	1817	7.7	-23.3	-4	-1					
20TH	251.00									100.0	-357.0	20.0	4.8	2.0
		16.0	-45.1	1817	1817	8.8	-24.8	-4	-1					
21ST	263.50									84.0	-312.0	15.8	3.7	1.8
		23.2	-61.6	2325	2325	10.0	-26.5	-4	-2					
22ND	279.50									60.8	-250.4	11.3	2.5	1.5
		10.0	-37.4	1570	1570	6.4	-23.8	-8	-2					
23RD	292.00									50.8	-213.0	8.4	1.8	1.2
		16.1	-50.7	2005	2005	8.0	-25.3	-6	-2					
24TH	308.00									34.7	-162.3	5.4	1.2	.9
		6.8	-30.7	1317	1317	5.2	-23.4	-7	-1					
25TH	320.50									27.9	-131.5	3.5	.8	.7
		9.0	-43.8	1685	1685	5.4	-26.0	-6	-1					
26TH	336.50									18.9	-87.8	1.8	.4	.4
		6.5	-28.0	1276	1276	5.1	-22.0	-7	-2					
27TH	349.00									12.3	-59.7	.9	.2	.2
		4.9	-27.3	1275	1275	3.8	-21.4	-5	-1					
EAVE	361.50									7.5	-32.4	.3	.1	.1
		7.5	-32.4	1182	1182	6.3	-27.4	-1	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 210 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									645.3	-1059.7	200.5	110.0	5.8
		40.5	-66.6	4039	4039	10.0	-16.5	-7	-4					
2ND	26.00									604.8	-993.1	173.8	93.8	5.1
		23.2	-34.4	1942	1942	11.9	-17.7	-3	-2					
3RD	38.50									581.6	-958.7	161.6	86.4	5.0
		25.5	-35.4	1942	1942	13.1	-18.2	-1	-0					
4TH	51.00									556.1	-923.3	149.9	79.2	5.0
		29.4	-33.8	1942	1942	15.1	-17.4	1	1					
5TH	63.50									526.7	-889.5	138.5	72.5	5.0
		26.1	-25.4	1942	1942	13.5	-13.1	2	2					
6TH	76.00									500.6	-864.1	127.6	66.1	5.1
		26.2	-32.8	1843	1843	14.2	-17.8	-1	-1					
7TH	88.50									474.4	-831.3	117.0	60.0	5.1
		25.9	-34.5	1817	1817	14.3	-19.0	-2	-2					
8TH	101.00									448.5	-796.7	106.8	54.2	4.9
		25.7	-34.8	1817	1817	14.1	-19.1	-3	-2					
9TH	113.50									422.8	-762.0	97.1	48.8	4.8
		25.5	-35.0	1817	1817	14.0	-19.2	-3	-2					
10TH	126.00									397.3	-727.0	87.8	43.6	4.6
		24.8	-35.2	1817	1817	13.6	-19.4	-4	-3					
11TH	138.50									372.6	-691.8	78.9	38.8	4.4
		23.9	-35.4	1817	1817	13.2	-19.5	-4	-3					
12TH	151.00									348.6	-656.4	70.5	34.3	4.2
		23.1	-35.7	1817	1817	12.7	-19.6	-5	-3					
13TH	163.50									325.5	-620.7	62.5	30.1	3.9
		22.8	-36.2	1817	1817	12.5	-19.9	-5	-3					
14TH	176.00									302.7	-584.5	54.9	26.2	3.7
		22.8	-36.9	1817	1817	12.6	-20.3	-5	-3					
15TH	188.50									279.9	-547.6	47.9	22.5	3.5
		22.9	-37.6	1817	1817	12.6	-20.7	-5	-3					
16TH	201.00									257.0	-510.0	41.3	19.2	3.2
		22.9	-38.3	1817	1817	12.6	-21.1	-5	-3					
17TH	213.50									234.1	-471.7	35.1	16.1	3.0
		22.8	-39.0	1817	1817	12.5	-21.4	-5	-3					
18TH	226.00									211.3	-432.8	29.5	13.3	2.7
		22.6	-39.6	1817	1817	12.5	-21.8	-5	-3					
19TH	238.50									188.7	-393.1	24.3	10.8	2.5
		22.8	-40.9	1817	1817	12.6	-22.5	-5	-3					
20TH	251.00									165.9	-352.2	19.7	8.6	2.2
		24.2	-43.9	1817	1817	13.3	-24.2	-5	-3					
21ST	263.50									141.6	-308.3	15.5	6.7	2.0
		33.2	-60.5	2325	2325	14.3	-26.0	-5	-3					
22ND	279.50									108.4	-247.8	11.1	4.7	1.6
		17.3	-36.8	1570	1570	11.0	-23.4	-7	-3					
23RD	292.00									91.1	-211.1	8.2	3.4	1.3
		24.5	-50.8	2005	2005	12.2	-25.3	-6	-3					
24TH	308.00									66.6	-160.3	5.2	2.2	.9
		13.3	-31.4	1317	1317	10.1	-23.9	-6	-3					
25TH	320.50									53.3	-128.9	3.4	1.4	.7
		17.6	-44.1	1685	1685	10.4	-26.2	-5	-2					
26TH	336.50									35.7	-84.8	1.7	.7	.4
		12.9	-27.9	1276	1276	10.1	-21.9	-4	-2					
27TH	349.00									22.8	-56.9	.8	.3	.3
		9.5	-25.6	1275	1275	7.5	-20.0	-7	-3					
EAVE	361.50									13.3	-31.3	.3	.1	.1
		13.3	-31.3	1182	1182	11.2	-26.5	-2	-1					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 220 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									733.9	-770.2	149.4	130.0	2.2
		44.3	-46.0	4039	4039	11.0	-11.4	-4	-4					
2ND	26.00									689.6	-724.2	130.0	111.5	1.8
		24.4	-23.2	1942	1942	12.6	-12.0	-1	-2					
3RD	38.50									665.2	-701.0	121.1	103.0	1.8
		26.2	-23.5	1942	1942	13.5	-12.1	0	0					
4TH	51.00									639.1	-677.5	112.4	94.9	1.8
		29.8	-25.0	1942	1942	15.4	-12.9	0	0					
5TH	63.50									609.3	-652.5	104.1	87.1	1.8
		25.3	-18.7	1942	1942	13.0	-9.6	2	2					
6TH	76.00									584.0	-633.7	96.1	79.6	1.9
		27.1	-23.0	1843	1843	14.7	-12.5	0	0					
7TH	88.50									556.9	-610.7	88.3	72.5	1.9
		27.5	-23.8	1817	1817	15.1	-13.1	-0	-0					
8TH	101.00									529.4	-586.8	80.8	65.7	1.9
		27.5	-23.8	1817	1817	15.1	-13.1	-0	-0					
9TH	113.50									501.9	-563.1	73.6	59.3	1.9
		27.5	-23.7	1817	1817	15.1	-13.0	-0	-0					
10TH	126.00									474.4	-539.4	66.7	53.2	1.9
		27.5	-24.1	1817	1817	15.1	-13.3	-1	-1					
11TH	138.50									446.9	-515.3	60.2	47.4	1.8
		27.4	-24.7	1817	1817	15.1	-13.6	-1	-1					
12TH	151.00									419.5	-490.6	53.9	42.0	1.8
		27.4	-25.3	1817	1817	15.1	-13.9	-1	-1					
13TH	163.50									392.1	-465.3	47.9	36.9	1.7
		27.3	-25.8	1817	1817	15.0	-14.2	-1	-2					
14TH	176.00									364.9	-439.5	42.2	32.2	1.6
		27.2	-26.2	1817	1817	15.0	-14.4	-1	-2					
15TH	188.50									337.7	-413.4	36.9	27.8	1.5
		27.1	-26.6	1817	1817	14.9	-14.6	-2	-2					
16TH	201.00									310.6	-386.8	31.9	23.7	1.5
		26.9	-27.1	1817	1817	14.8	-14.9	-2	-2					
17TH	213.50									283.7	-359.7	27.2	20.0	1.4
		26.7	-27.9	1817	1817	14.7	-15.4	-1	-1					
18TH	226.00									257.1	-331.7	22.9	16.6	1.3
		26.4	-28.7	1817	1817	14.6	-15.8	-1	-1					
19TH	238.50									230.6	-303.0	19.0	13.6	1.2
		26.7	-30.0	1817	1817	14.7	-16.5	-1	-1					
20TH	251.00									203.9	-273.0	15.4	10.9	1.1
		28.1	-32.6	1817	1817	15.5	-17.9	-2	-2					
21ST	263.50									175.8	-240.4	12.1	8.5	1.0
		37.8	-45.4	2325	2325	16.2	-19.5	-3	-2					
22ND	279.50									138.0	-195.0	8.7	6.0	.8
		21.8	-29.3	1570	1570	13.9	-18.6	-4	-3					
23RD	292.00									116.2	-165.7	6.4	4.4	.6
		29.6	-40.0	2005	2005	14.8	-19.9	-3	-3					
24TH	308.00									86.6	-125.8	4.1	2.8	.4
		18.1	-25.6	1317	1317	13.7	-19.4	-3	-2					
25TH	320.50									68.5	-100.2	2.7	1.8	.3
		23.3	-34.0	1685	1685	13.8	-20.2	-2	-2					
26TH	336.50									45.3	-66.3	1.3	.9	.2
		15.7	-22.1	1276	1276	12.3	-17.3	-3	-2					
27TH	349.00									29.5	-44.1	.6	.4	.1
		12.6	-20.2	1275	1275	9.9	-15.8	-4	-2					
EAVE	361.50									16.9	-24.0	.2	.2	.0
		16.9	-24.0	1182	1182	14.3	-20.3	-0	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 230 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									851.6	-747.5	141.8	155.1	1.1
		44.3	-47.4	4039	4039	11.0	-11.7	-6	-6					
2ND	26.00									807.3	-700.1	123.0	133.5	.6
		26.4	-23.9	1942	1942	13.6	-12.3	-4	-4					
3RD	38.50									780.9	-676.1	114.4	123.6	.4
		28.7	-24.4	1942	1942	14.8	-12.6	-2	-3					
4TH	51.00									752.2	-651.8	106.1	114.0	.3
		32.7	-25.2	1942	1942	16.8	-13.0	-1	-1					
5TH	63.50									719.6	-626.5	98.1	104.8	.2
		27.6	-20.2	1942	1942	14.2	-10.4	2	3					
6TH	76.00									692.0	-606.3	90.4	96.0	.3
		30.4	-23.0	1843	1843	16.5	-12.5	0	0					
7TH	88.50									661.6	-583.4	83.0	87.6	.4
		31.3	-23.6	1817	1817	17.2	-13.0	0	0					
8TH	101.00									630.3	-559.7	75.8	79.5	.4
		31.8	-23.9	1817	1817	17.5	-13.1	0	0					
9TH	113.50									598.5	-535.9	69.0	71.8	.4
		32.3	-24.1	1817	1817	17.8	-13.3	0	0					
10TH	126.00									566.1	-511.7	62.4	64.5	.4
		32.4	-24.4	1817	1817	17.8	-13.4	0	0					
11TH	138.50									533.8	-487.3	56.2	57.7	.4
		32.2	-24.7	1817	1817	17.7	-13.6	0	0					
12TH	151.00									501.6	-462.6	50.2	51.2	.4
		32.0	-25.1	1817	1817	17.6	-13.8	-0	-0					
13TH	163.50									469.6	-437.5	44.6	45.1	.4
		31.7	-25.2	1817	1817	17.4	-13.9	-0	-0					
14TH	176.00									437.9	-412.3	39.3	39.4	.4
		31.3	-25.2	1817	1817	17.3	-13.9	-0	-0					
15TH	188.50									406.6	-387.1	34.3	34.2	.4
		31.0	-25.2	1817	1817	17.1	-13.9	-0	-0					
16TH	201.00									375.6	-361.8	29.6	29.3	.4
		30.8	-25.7	1817	1817	17.0	-14.1	-0	-0					
17TH	213.50									344.8	-336.1	25.3	24.8	.4
		31.0	-26.8	1817	1817	17.0	-14.7	-0	-0					
18TH	226.00									313.8	-309.4	21.2	20.7	.4
		31.1	-27.9	1817	1817	17.1	-15.3	0	0					
19TH	238.50									282.7	-281.5	17.5	16.9	.4
		31.6	-29.2	1817	1817	17.4	-16.1	-0	-0					
20TH	251.00									251.1	-252.3	14.2	13.6	.4
		33.2	-31.0	1817	1817	18.3	-17.1	-1	-1					
21ST	263.50									217.9	-221.3	11.2	10.7	.3
		44.9	-42.4	2325	2325	19.3	-18.2	-2	-2					
22ND	279.50									173.0	-178.9	8.0	7.5	.2
		27.5	-26.0	1570	1570	17.5	-16.6	-1	-1					
23RD	292.00									145.5	-152.9	6.0	5.5	.1
		36.9	-36.5	2005	2005	18.4	-18.2	-1	-1					
24TH	308.00									108.6	-116.4	3.8	3.5	.1
		22.1	-23.2	1317	1317	16.8	-17.6	-0	-0					
25TH	320.50									86.5	-93.2	2.5	2.3	.0
		29.4	-30.8	1685	1685	17.4	-18.3	-0	-0					
26TH	336.50									57.1	-62.4	1.3	1.1	.0
		19.5	-20.6	1276	1276	15.3	-16.2	-1	-1					
27TH	349.00									37.6	-41.8	.6	.5	.0
		17.3	-18.6	1275	1275	13.6	-14.6	-1	-1					
EAVE	361.50									20.3	-23.2	.2	.2	-.0
		20.3	-23.2	1182	1182	17.1	-19.6	0	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 240 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									802.7	-620.3	115.5	145.5	-1.8
2ND	26.00	45.9	-38.2	4039	4039	11.4	-9.5	-3	-4	756.8	-582.1	99.8	125.2	-2.1
3RD	38.50	26.8	-18.3	1942	1942	13.8	-9.4	-1	-1	730.1	-563.8	92.7	116.0	-2.1
4TH	51.00	29.0	-18.8	1942	1942	14.9	-9.7	0	0	701.1	-545.0	85.8	107.0	-2.1
5TH	63.50	31.0	-21.7	1942	1942	16.0	-11.2	-1	-2	670.1	-523.3	79.1	98.4	-2.2
6TH	76.00	25.8	-16.7	1942	1942	13.3	-8.6	1	2	644.3	-506.6	72.6	90.2	-2.1
7TH	88.50	28.3	-21.1	1843	1843	15.3	-11.5	1	1	616.1	-485.5	66.4	82.3	-2.1
8TH	101.00	29.0	-22.1	1817	1817	16.0	-12.2	1	1	587.1	-463.4	60.5	74.8	-2.0
9TH	113.50	29.3	-22.1	1817	1817	16.1	-12.1	1	2	557.7	-441.3	54.9	67.7	-1.9
10TH	126.00	29.7	-22.0	1817	1817	16.3	-12.1	2	2	528.1	-419.3	49.5	60.9	-1.8
11TH	138.50	29.8	-21.9	1817	1817	16.4	-12.1	2	3	498.3	-397.4	44.4	54.5	-1.7
12TH	151.00	29.8	-21.8	1817	1817	16.4	-12.0	2	3	468.5	-375.6	39.5	48.4	-1.6
13TH	163.50	29.8	-21.7	1817	1817	16.4	-11.9	2	3	438.7	-353.9	35.0	42.8	-1.5
14TH	176.00	29.5	-21.7	1817	1817	16.2	-12.0	2	3	409.2	-332.2	30.7	37.5	-1.3
15TH	188.50	28.8	-22.0	1817	1817	15.9	-12.1	2	3	380.4	-310.2	26.7	32.5	-1.2
16TH	201.00	28.2	-22.2	1817	1817	15.5	-12.2	2	3	352.1	-288.1	22.9	27.9	-1.1
17TH	213.50	28.0	-22.5	1817	1817	15.4	-12.4	2	3	324.2	-265.6	19.5	23.7	-1.0
18TH	226.00	28.2	-23.0	1817	1817	15.5	-12.7	2	3	295.9	-242.6	16.3	19.8	-.8
19TH	238.50	28.5	-23.5	1817	1817	15.7	-12.9	2	3	267.5	-219.1	13.4	16.3	-.7
20TH	251.00	29.0	-24.2	1817	1817	16.0	-13.3	2	2	238.5	-194.8	10.8	13.2	-.6
21ST	263.50	30.3	-25.5	1817	1817	16.7	-14.1	1	1	208.2	-169.3	8.6	10.4	-.5
22ND	279.50	40.7	-34.5	2325	2325	17.5	-14.8	-0	-0	167.5	-134.8	6.1	7.4	-.6
23RD	292.00	25.6	-20.3	1570	1570	16.3	-13.0	2	2	141.9	-114.5	4.6	5.4	-.5
24TH	308.00	35.6	-27.1	2005	2005	17.8	-13.5	2	2	106.3	-87.3	2.9	3.4	-.4
25TH	320.50	21.0	-16.5	1317	1317	16.0	-12.5	2	2	85.2	-70.9	2.0	2.2	-.3
26TH	336.50	29.4	-22.1	1685	1685	17.4	-13.1	2	2	55.9	-48.8	1.0	1.1	-.2
27TH	349.00	19.1	-15.8	1276	1276	14.9	-12.4	1	2	36.8	-33.0	.5	.5	-.1
EAVE	361.50	16.6	-14.2	1275	1275	13.0	-11.2	3	3	20.2	-18.7	.2	.2	-.0
TOP	379.50	20.2	-18.7	1182	1182	17.1	-15.8	1	1	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 250 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									780.6	-473.4	80.3	141.6	-3.1
		49.2	-39.4	4039	4039	12.2	-9.7	-2	-2					
2ND	26.00									731.5	-434.1	68.5	121.9	-3.2
		27.9	-18.9	1942	1942	14.4	-9.7	-0	-1					
3RD	38.50									703.6	-415.2	63.1	113.0	-3.3
		29.7	-19.2	1942	1942	15.3	-9.9	-0	-1					
4TH	51.00									673.9	-396.0	58.1	104.3	-3.3
		27.8	-18.9	1942	1942	14.3	-9.7	-1	-1					
5TH	63.50									646.1	-377.1	53.2	96.1	-3.3
		24.3	-15.0	1942	1942	12.5	-7.7	2	3					
6TH	76.00									621.7	-362.1	48.6	88.2	-3.2
		27.0	-17.7	1843	1843	14.7	-9.6	1	2					
7TH	88.50									594.7	-344.4	44.2	80.6	-3.2
		27.5	-18.1	1817	1817	15.1	-9.9	1	2					
8TH	101.00									567.2	-326.4	40.0	73.3	-3.1
		27.6	-18.0	1817	1817	15.2	-9.9	1	2					
9TH	113.50									539.6	-308.4	36.1	66.4	-3.0
		27.7	-17.9	1817	1817	15.3	-9.8	2	2					
10TH	126.00									511.9	-290.5	32.3	59.8	-2.9
		27.9	-17.6	1817	1817	15.3	-9.7	2	3					
11TH	138.50									484.0	-272.9	28.8	53.6	-2.8
		28.0	-17.2	1817	1817	15.4	-9.5	2	3					
12TH	151.00									456.0	-255.7	25.5	47.7	-2.7
		28.2	-16.9	1817	1817	15.5	-9.3	2	3					
13TH	163.50									427.8	-238.9	22.4	42.2	-2.5
		27.9	-16.6	1817	1817	15.4	-9.1	2	4					
14TH	176.00									399.9	-222.3	19.5	37.0	-2.4
		27.4	-16.4	1817	1817	15.1	-9.0	3	4					
15TH	188.50									372.5	-205.9	16.8	32.2	-2.2
		26.9	-16.2	1817	1817	14.8	-8.9	3	5					
16TH	201.00									345.6	-189.7	14.4	27.7	-2.1
		26.8	-16.3	1817	1817	14.7	-8.9	3	5					
17TH	213.50									318.9	-173.4	12.1	23.6	-1.9
		27.2	-16.6	1817	1817	15.0	-9.2	3	5					
18TH	226.00									291.7	-156.8	10.0	19.7	-1.7
		27.6	-17.0	1817	1817	15.2	-9.4	3	5					
19TH	238.50									264.0	-139.7	8.2	16.3	-1.5
		28.3	-17.6	1817	1817	15.6	-9.7	3	4					
20TH	251.00									235.7	-122.1	6.5	13.1	-1.3
		29.5	-18.2	1817	1817	16.3	-10.0	2	3					
21ST	263.50									206.2	-104.0	5.1	10.4	-1.2
		39.3	-23.7	2325	2325	16.9	-10.2	1	2					
22ND	279.50									166.9	-80.2	3.7	7.4	-1.1
		25.2	-12.0	1570	1570	16.1	-7.6	3	7					
23RD	292.00									141.6	-68.3	2.7	5.5	-.9
		35.2	-16.6	2005	2005	17.6	-8.3	2	5					
24TH	308.00									106.4	-51.7	1.8	3.5	-.7
		20.3	-9.7	1317	1317	15.4	-7.4	3	6					
25TH	320.50									86.1	-41.9	1.2	2.3	-.5
		29.6	-12.6	1685	1685	17.6	-7.5	2	6					
26TH	336.50									56.4	-29.4	.6	1.1	-.3
		18.9	-9.4	1276	1276	14.8	-7.4	2	4					
27TH	349.00									37.5	-20.0	.3	.6	-.2
		16.6	-8.3	1275	1275	13.1	-6.5	4	7					
EAVE	361.50									20.9	-11.6	.1	.2	-.1
		20.9	-11.6	1182	1182	17.7	-9.8	1	2					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 260 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									771.4	-112.4	13.2	141.5	-4.5
		46.1	-18.3	4039	4039	11.4	-4.5	1	1					
2ND	26.00									725.3	-94.1	10.5	122.0	-4.4
		27.4	-8.0	1942	1942	14.1	-4.1	0	1					
3RD	38.50									698.0	-86.1	9.4	113.1	-4.4
		29.8	-7.6	1942	1942	15.3	-3.9	0	1					
4TH	51.00									668.2	-78.5	8.4	104.6	-4.3
		26.2	-7.2	1942	1942	13.5	-3.7	-0	-2					
5TH	63.50									642.0	-71.3	7.4	96.4	-4.4
		22.4	-3.9	1942	1942	11.5	-2.0	-0	-1					
6TH	76.00									619.6	-67.4	6.6	88.5	-4.4
		26.5	-5.9	1843	1843	14.4	-3.2	1	3					
7TH	88.50									593.1	-61.5	5.8	80.9	-4.3
		27.2	-5.8	1817	1817	14.9	-3.2	1	4					
8TH	101.00									566.0	-55.8	5.0	73.7	-4.2
		27.1	-5.2	1817	1817	14.9	-2.9	1	4					
9TH	113.50									538.9	-50.6	4.4	66.8	-4.1
		27.0	-4.6	1817	1817	14.8	-2.5	1	5					
10TH	126.00									511.9	-45.9	3.8	60.2	-4.0
		27.0	-4.3	1817	1817	14.9	-2.4	1	5					
11TH	138.50									484.9	-41.6	3.2	54.0	-3.8
		27.1	-4.0	1817	1817	14.9	-2.2	1	4					
12TH	151.00									457.8	-37.6	2.7	48.1	-3.7
		27.2	-3.8	1817	1817	15.0	-2.1	1	4					
13TH	163.50									430.6	-33.8	2.3	42.5	-3.6
		27.2	-3.5	1817	1817	15.0	-1.9	1	5					
14TH	176.00									403.4	-30.4	1.9	37.3	-3.4
		27.1	-3.1	1817	1817	14.9	-1.7	1	6					
15TH	188.50									376.2	-27.3	1.5	32.5	-3.3
		27.1	-2.7	1817	1817	14.9	-1.5	1	8					
16TH	201.00									349.1	-24.6	1.2	27.9	-3.1
		27.2	-2.6	1817	1817	15.0	-1.4	1	8					
17TH	213.50									321.9	-22.0	.9	23.7	-2.8
		27.8	-3.0	1817	1817	15.3	-1.6	1	8					
18TH	226.00									294.1	-19.0	.6	19.9	-2.6
		28.4	-3.4	1817	1817	15.6	-1.9	1	8					
19TH	238.50									265.7	-15.6	.4	16.4	-2.3
		29.0	-3.7	1817	1817	16.0	-2.1	1	8					
20TH	251.00									236.6	-11.9	.3	13.2	-2.1
		29.9	-4.0	1817	1817	16.4	-2.2	1	7					
21ST	263.50									206.7	-7.9	.1	10.5	-1.9
		39.4	-5.5	2325	2325	17.0	-2.4	1	6					
22ND	279.50									167.3	-2.4	.1	7.5	-1.6
		25.0	-.9	1570	1570	15.9	-.6	0	13					
23RD	292.00									142.3	-1.5	.0	5.5	-1.3
		35.1	-2.1	2005	2005	17.5	-1.0	1	9					
24TH	308.00									107.2	.6	.0	3.5	-1.0
		19.9	.3	1317	1317	15.1	.2	-0	11					
25TH	320.50									87.3	.2	.0	2.3	-.8
		30.0	.6	1685	1685	17.8	.3	-0	9					
26TH	336.50									57.3	-.3	.0	1.2	-.5
		18.4	-.1	1276	1276	14.4	-.1	0	9					
27TH	349.00									38.9	-.2	.0	.6	-.3
		17.2	1.3	1275	1275	13.5	1.0	-1	13					
EAVE	361.50									21.6	-1.5	.0	.2	-.1
		21.6	-1.5	1182	1182	18.3	-1.3	0	4					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 270 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									679.8	75.3	-19.9	125.9	-4.5
		38.3	-4.0	4039	4039	9.5	-1.0	0	4					
2ND	26.00									641.5	79.3	-17.9	108.7	-4.3
		24.2	-.8	1942	1942	12.5	-.4	0	3					
3RD	38.50									617.3	80.1	-16.9	100.9	-4.2
		27.0	-.2	1942	1942	13.9	-.1	0	3					
4TH	51.00									590.3	80.4	-15.9	93.3	-4.1
		23.1	.2	1942	1942	11.9	.1	0	-1					
5TH	63.50									567.2	80.1	-14.9	86.1	-4.2
		20.0	2.1	1942	1942	10.3	1.1	1	-5					
6TH	76.00									547.2	78.0	-13.9	79.1	-4.3
		22.8	.9	1843	1843	12.4	.5	-0	4					
7TH	88.50									524.4	77.1	-12.9	72.4	-4.2
		23.2	1.0	1817	1817	12.8	.5	-0	6					
8TH	101.00									501.2	76.1	-12.0	66.0	-4.0
		23.0	1.3	1817	1817	12.7	.7	-0	6					
9TH	113.50									478.1	74.8	-11.0	59.9	-3.9
		22.9	1.7	1817	1817	12.6	.9	-0	6					
10TH	126.00									455.3	73.2	-10.1	54.0	-3.8
		23.1	2.1	1817	1817	12.7	1.2	-1	6					
11TH	138.50									432.2	71.0	-9.2	48.5	-3.6
		23.4	2.7	1817	1817	12.9	1.5	-1	7					
12TH	151.00									408.8	68.4	-8.3	43.2	-3.4
		23.8	3.2	1817	1817	13.1	1.8	-1	7					
13TH	163.50									385.0	65.2	-7.5	38.3	-3.3
		24.0	3.5	1817	1817	13.2	1.9	-1	7					
14TH	176.00									360.9	61.8	-6.7	33.6	-3.1
		24.2	3.5	1817	1817	13.3	1.9	-1	7					
15TH	188.50									336.7	58.2	-6.0	29.3	-2.9
		24.4	3.6	1817	1817	13.4	2.0	-1	8					
16TH	201.00									312.3	54.6	-5.2	25.2	-2.7
		24.5	3.5	1817	1817	13.5	1.9	-1	8					
17TH	213.50									287.8	51.1	-4.6	21.5	-2.5
		24.6	3.2	1817	1817	13.5	1.8	-1	8					
18TH	226.00									263.2	47.9	-4.0	18.0	-2.3
		24.6	2.9	1817	1817	13.6	1.6	-1	9					
19TH	238.50									238.6	45.1	-3.4	14.9	-2.1
		25.0	2.6	1817	1817	13.8	1.4	-1	9					
20TH	251.00									213.6	42.5	-2.8	12.0	-1.9
		26.2	2.6	1817	1817	14.4	1.4	-1	9					
21ST	263.50									187.4	39.9	-2.3	9.5	-1.7
		35.0	3.7	2325	2325	15.1	1.6	-1	9					
22ND	279.50									152.4	36.2	-1.7	6.8	-1.3
		22.7	4.6	1570	1570	14.5	2.9	-2	10					
23RD	292.00									129.7	31.6	-1.3	5.1	-1.1
		32.4	5.8	2005	2005	16.2	2.9	-2	9					
24TH	308.00									97.3	25.8	-.8	3.2	-.8
		17.7	5.4	1317	1317	13.4	4.1	-3	9					
25TH	320.50									79.6	20.5	-.5	2.1	-.6
		27.8	6.7	1685	1685	16.5	3.9	-2	8					
26TH	336.50									51.9	13.8	-.3	1.1	-.4
		15.7	4.7	1276	1276	12.3	3.7	-3	8					
27TH	349.00									36.1	9.1	-.1	.5	-.2
		15.7	4.8	1275	1275	12.3	3.8	-3	9					
EAVE	361.50									20.4	4.3	-.0	.2	-.1
		20.4	4.3	1182	1182	17.2	3.6	-1	4					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 280 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									665.1	29.4	-8.8	125.5	-2.6
		36.7	-2.8	4039	4039	9.1	-.7	0	5					
2ND	26.00									628.4	32.1	-8.0	108.6	-2.4
		23.1	.0	1942	1942	11.9	.0	-0	3					
3RD	38.50									605.3	32.1	-7.6	100.9	-2.3
		25.7	.9	1942	1942	13.3	.5	-0	3					
4TH	51.00									579.6	31.2	-7.2	93.5	-2.3
		21.4	-.2	1942	1942	11.0	-.1	0	0					
5TH	63.50									558.2	31.4	-6.9	86.4	-2.3
		19.0	1.7	1942	1942	9.8	.9	-0	0					
6TH	76.00									539.2	29.7	-6.5	79.6	-2.2
		21.2	.5	1843	1843	11.5	.2	-0	4					
7TH	88.50									518.0	29.2	-6.1	72.9	-2.2
		21.8	.2	1817	1817	12.0	.1	-0	5					
8TH	101.00									496.2	29.0	-5.7	66.6	-2.1
		21.9	.2	1817	1817	12.1	.1	-0	4					
9TH	113.50									474.3	28.8	-5.4	60.5	-2.0
		22.1	.3	1817	1817	12.1	.1	-0	4					
10TH	126.00									452.2	28.5	-5.0	54.8	-1.9
		22.2	.4	1817	1817	12.2	.2	-0	4					
11TH	138.50									430.0	28.1	-4.7	49.2	-1.8
		22.3	.6	1817	1817	12.3	.3	-0	3					
12TH	151.00									407.7	27.5	-4.3	44.0	-1.7
		22.4	.8	1817	1817	12.3	.4	-0	3					
13TH	163.50									385.4	26.7	-4.0	39.0	-1.7
		22.6	.8	1817	1817	12.5	.4	-0	3					
14TH	176.00									362.7	25.9	-3.7	34.4	-1.6
		23.0	.5	1817	1817	12.7	.3	-0	4					
15TH	188.50									339.7	25.4	-3.3	30.0	-1.5
		23.4	.3	1817	1817	12.9	.2	-0	4					
16TH	201.00									316.4	25.1	-3.0	25.9	-1.4
		23.7	.2	1817	1817	13.0	.1	-0	5					
17TH	213.50									292.7	24.9	-2.7	22.1	-1.3
		24.0	.2	1817	1817	13.2	.1	-0	5					
18TH	226.00									268.6	24.7	-2.4	18.6	-1.2
		24.4	.2	1817	1817	13.4	.1	-0	4					
19TH	238.50									244.3	24.6	-2.1	15.4	-1.1
		25.0	.1	1817	1817	13.8	.1	-0	4					
20TH	251.00									219.3	24.4	-1.8	12.5	-.9
		26.5	.3	1817	1817	14.6	.1	-0	4					
21ST	263.50									192.8	24.2	-1.5	9.9	-.9
		35.8	.9	2325	2325	15.4	.4	-0	3					
22ND	279.50									157.0	23.3	-1.1	7.1	-.7
		23.1	3.0	1570	1570	14.7	1.9	-1	6					
23RD	292.00									133.9	20.3	-.8	5.3	-.6
		32.6	4.1	2005	2005	16.2	2.0	-1	6					
24TH	308.00									101.3	16.2	-.5	3.4	-.4
		18.7	3.3	1317	1317	14.2	2.5	-1	5					
25TH	320.50									82.6	12.9	-.4	2.2	-.3
		27.9	4.2	1685	1685	16.5	2.5	-1	4					
26TH	336.50									54.7	8.7	-.2	1.1	-.2
		16.5	2.9	1276	1276	13.0	2.2	-1	5					
27TH	349.00									38.2	5.9	-.1	.6	-.1
		16.9	2.4	1275	1275	13.2	1.9	-0	3					
EAVE	361.50									21.3	3.5	-.0	.2	-.0
		21.3	3.5	1182	1182	18.0	3.0	-0	2					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 290 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									658.9	-36.2	5.1	127.4	-.6
		34.8	-3.5	4039	4039	8.6	-.9	0	1					
2ND	26.00									624.1	-32.7	4.2	110.7	-.5
		21.4	-1.7	1942	1942	11.0	-.9	0	1					
3RD	38.50									602.7	-31.0	3.8	103.0	-.5
		23.5	-2.0	1942	1942	12.1	-1.0	0	2					
4TH	51.00									579.3	-29.0	3.4	95.7	-.5
		19.5	-1.6	1942	1942	10.0	-.8	0	0					
5TH	63.50									559.8	-27.4	3.0	88.5	-.5
		18.6	.6	1942	1942	9.6	.3	-0	0					
6TH	76.00									541.2	-28.1	2.7	81.7	-.5
		19.8	-.9	1843	1843	10.7	-.5	0	2					
7TH	88.50									521.4	-27.1	2.3	75.0	-.4
		20.2	-1.5	1817	1817	11.1	-.8	0	2					
8TH	101.00									501.2	-25.7	2.0	68.6	-.4
		20.5	-1.6	1817	1817	11.3	-.9	0	1					
9TH	113.50									480.7	-24.0	1.7	62.5	-.4
		20.8	-1.8	1817	1817	11.5	-1.0	0	1					
10TH	126.00									459.9	-22.2	1.4	56.6	-.4
		21.3	-2.0	1817	1817	11.7	-1.1	0	0					
11TH	138.50									438.6	-20.2	1.2	51.0	-.4
		21.7	-2.2	1817	1817	12.0	-1.2	-0	-0					
12TH	151.00									416.9	-18.0	.9	45.6	-.4
		22.2	-2.4	1817	1817	12.2	-1.3	-0	-0					
13TH	163.50									394.7	-15.6	.7	40.6	-.4
		22.6	-2.4	1817	1817	12.4	-1.3	-0	-0					
14TH	176.00									372.1	-13.2	.5	35.8	-.4
		22.9	-2.1	1817	1817	12.6	-1.2	0	1					
15TH	188.50									349.2	-11.1	.4	31.3	-.3
		23.2	-1.9	1817	1817	12.7	-1.1	0	1					
16TH	201.00									326.1	-9.2	.2	27.0	-.3
		23.5	-1.8	1817	1817	13.0	-1.0	0	2					
17TH	213.50									302.5	-7.4	.1	23.1	-.3
		24.1	-1.7	1817	1817	13.3	-1.0	0	2					
18TH	226.00									278.5	-5.6	.1	19.5	-.2
		24.6	-1.7	1817	1817	13.6	-.9	0	2					
19TH	238.50									253.8	-3.9	.0	16.2	-.2
		25.4	-1.7	1817	1817	14.0	-.9	0	1					
20TH	251.00									228.4	-2.3	-.0	13.1	-.2
		27.0	-1.5	1817	1817	14.9	-.8	0	1					
21ST	263.50									201.4	-.8	-.1	10.5	-.1
		37.1	-1.7	2325	2325	15.9	-.7	0	1					
22ND	279.50									164.4	.9	-.1	7.5	-.1
		22.8	-.7	1570	1570	14.5	-.4	0	2					
23RD	292.00									141.6	1.6	-.0	5.6	-.1
		33.7	-.5	2005	2005	16.8	-.2	0	1					
24TH	308.00									108.0	2.1	-.0	3.6	-.0
		20.2	1.1	1317	1317	15.3	.9	-0	1					
25TH	320.50									87.8	.9	.0	2.4	.0
		29.5	1.2	1685	1685	17.5	.7	-0	1					
26TH	336.50									58.3	-.2	.0	1.2	.0
		17.3	.3	1276	1276	13.5	.2	0	-0					
27TH	349.00									41.0	-.5	.0	.6	.0
		17.9	-.1	1275	1275	14.1	-.1	-0	-2					
EAVE	361.50									23.1	-.4	.0	.2	-.0
		23.1	-.4	1182	1182	19.5	-.4	0	0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 300 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									570.8	-153.9	28.1	112.9	.5
		25.6	-10.2	4039	4039	6.3	-2.5	-1	-3					
2ND	26.00									545.2	-143.7	24.2	98.4	.4
		18.0	-4.8	1942	1942	9.3	-2.5	-0	-1					
3RD	38.50									527.2	-138.9	22.5	91.7	.4
		20.6	-4.9	1942	1942	10.6	-2.5	-0	-1					
4TH	51.00									506.6	-134.1	20.8	85.2	.4
		17.1	-5.1	1942	1942	8.8	-2.6	-0	-1					
5TH	63.50									489.5	-128.9	19.1	79.0	.4
		17.8	-3.3	1942	1942	9.1	-1.7	1	3					
6TH	76.00									471.8	-125.6	17.5	73.0	.4
		16.7	-5.4	1843	1843	9.0	-2.9	0	0					
7TH	88.50									455.1	-120.2	16.0	67.2	.4
		16.7	-6.0	1817	1817	9.2	-3.3	-0	-1					
8TH	101.00									438.4	-114.2	14.5	61.6	.4
		17.1	-6.1	1817	1817	9.4	-3.3	-0	-1					
9TH	113.50									421.3	-108.1	13.1	56.2	.4
		17.5	-6.2	1817	1817	9.6	-3.4	-1	-2					
10TH	126.00									403.9	-102.0	11.8	51.1	.3
		17.9	-6.1	1817	1817	9.8	-3.4	-0	-1					
11TH	138.50									386.0	-95.8	10.6	46.2	.3
		18.3	-6.0	1817	1817	10.1	-3.3	-0	-1					
12TH	151.00									367.7	-89.8	9.4	41.4	.3
		18.7	-6.0	1817	1817	10.3	-3.3	-0	-0					
13TH	163.50									349.0	-83.8	8.3	37.0	.3
		19.1	-5.8	1817	1817	10.5	-3.2	-0	-0					
14TH	176.00									329.9	-78.0	7.3	32.7	.3
		19.4	-5.7	1817	1817	10.7	-3.1	-0	-1					
15TH	188.50									310.5	-72.3	6.4	28.7	.3
		19.7	-5.5	1817	1817	10.9	-3.0	-0	-1					
16TH	201.00									290.7	-66.8	5.5	25.0	.3
		20.0	-5.4	1817	1817	11.0	-3.0	-0	-1					
17TH	213.50									270.7	-61.4	4.7	21.5	.2
		20.3	-5.3	1817	1817	11.2	-2.9	-0	-0					
18TH	226.00									250.4	-56.1	4.0	18.2	.2
		20.6	-5.2	1817	1817	11.3	-2.9	0	0					
19TH	238.50									229.8	-50.9	3.3	15.2	.2
		21.2	-5.3	1817	1817	11.7	-2.9	0	0					
20TH	251.00									208.6	-45.6	2.7	12.5	.2
		23.1	-5.7	1817	1817	12.7	-3.2	0	0					
21ST	263.50									185.5	-39.9	2.2	10.0	.2
		32.4	-7.9	2325	2325	13.9	-3.4	0	0					
22ND	279.50									153.1	-31.9	1.6	7.3	.2
		19.2	-3.4	1570	1570	12.2	-2.1	0	2					
23RD	292.00									133.9	-28.5	1.2	5.5	.3
		29.6	-5.3	2005	2005	14.7	-2.6	0	1					
24TH	308.00									104.3	-23.2	.8	3.6	.3
		18.5	-3.4	1317	1317	14.1	-2.6	-0	-1					
25TH	320.50									85.8	-19.8	.5	2.4	.3
		27.9	-5.5	1685	1685	16.5	-3.2	-0	-1					
26TH	336.50									57.9	-14.4	.3	1.2	.3
		16.1	-5.1	1276	1276	12.7	-4.0	-2	-6					
27TH	349.00									41.8	-9.3	.1	.6	.2
		17.9	-5.1	1275	1275	14.0	-4.0	-2	-6					
EAVE	361.50									23.9	-4.2	.0	.2	.1
		23.9	-4.2	1182	1182	20.2	-3.6	-0	-3					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 310 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									405.1	-93.2	17.6	82.5	-2.7
		16.6	.8	4039	4039	4.1	.2	-1	14					
2ND	26.00									388.6	-93.9	15.2	72.2	-2.5
		13.0	-.3	1942	1942	6.7	-.2	0	15					
3RD	38.50									375.6	-93.6	14.0	67.4	-2.3
		15.1	-.9	1942	1942	7.8	-.5	1	15					
4TH	51.00									360.5	-92.7	12.9	62.8	-2.0
		12.7	-3.3	1942	1942	6.6	-1.7	0	2					
5TH	63.50									347.8	-89.4	11.7	58.4	-2.0
		12.6	-4.0	1942	1942	6.5	-2.1	-2	-6					
6TH	76.00									335.1	-85.3	10.6	54.1	-2.1
		11.2	-3.5	1843	1843	6.1	-1.9	1	3					
7TH	88.50									324.0	-81.9	9.6	50.0	-2.1
		11.1	-3.4	1817	1817	6.1	-1.9	2	5					
8TH	101.00									312.9	-78.5	8.6	46.0	-2.0
		11.3	-3.5	1817	1817	6.2	-1.9	1	5					
9TH	113.50									301.6	-75.0	7.6	42.1	-2.0
		11.6	-3.5	1817	1817	6.4	-2.0	1	4					
10TH	126.00									290.0	-71.4	6.7	38.5	-1.9
		11.8	-3.9	1817	1817	6.5	-2.1	1	4					
11TH	138.50									278.2	-67.6	5.9	34.9	-1.8
		12.0	-4.3	1817	1817	6.6	-2.4	1	4					
12TH	151.00									266.2	-63.2	5.0	31.5	-1.8
		12.3	-4.8	1817	1817	6.8	-2.6	2	4					
13TH	163.50									253.9	-58.4	4.3	28.2	-1.7
		12.6	-5.1	1817	1817	7.0	-2.8	2	4					
14TH	176.00									241.2	-53.4	3.6	25.2	-1.7
		13.1	-5.2	1817	1817	7.2	-2.9	2	5					
15TH	188.50									228.1	-48.1	2.9	22.2	-1.6
		13.6	-5.4	1817	1817	7.5	-3.0	2	6					
16TH	201.00									214.5	-42.7	2.4	19.5	-1.5
		13.9	-5.4	1817	1817	7.7	-3.0	2	6					
17TH	213.50									200.6	-37.3	1.9	16.9	-1.4
		14.0	-5.1	1817	1817	7.7	-2.8	2	7					
18TH	226.00									186.6	-32.2	1.4	14.4	-1.3
		14.2	-4.8	1817	1817	7.8	-2.6	2	7					
19TH	238.50									172.4	-27.4	1.1	12.2	-1.2
		14.7	-4.6	1817	1817	8.1	-2.6	2	7					
20TH	251.00									157.7	-22.8	.8	10.1	-1.1
		16.1	-5.0	1817	1817	8.8	-2.8	3	8					
21ST	263.50									141.7	-17.8	.5	8.3	-.9
		22.0	-7.3	2325	2325	9.4	-3.1	3	10					
22ND	279.50									119.7	-10.5	.3	6.2	-.7
		10.9	-1.9	1570	1570	6.9	-1.2	3	18					
23RD	292.00									108.9	-8.6	.2	4.7	-.5
		20.6	-5.3	2005	2005	10.3	-2.6	3	12					
24TH	308.00									88.3	-3.3	.1	3.2	-.2
		14.4	.2	1317	1317	10.9	.2	-0	5					
25TH	320.50									73.9	-3.6	.0	2.1	-.1
		21.3	-3.2	1685	1685	12.6	-1.9	1	4					
26TH	336.50									52.6	-.4	-.0	1.1	-.0
		14.8	-.3	1276	1276	11.6	-.2	0	3					
27TH	349.00									37.7	-.1	-.0	.6	.0
		15.8	-1.1	1275	1275	12.4	-.8	0	2					
EAVE	361.50									21.9	1.0	-.0	.2	.0
		21.9	1.0	1182	1182	18.6	.8	0	-2					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 320 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-22.8	-117.0	24.9	.7	-2.4
2ND	26.00	-8.9	5.8	4039	4039	-2.2	1.4	-15	-23	-13.9	-122.8	21.8	1.2	-2.1
3RD	38.50	-1.0	1.8	1942	1942	-.5	.9	-82	-49	-12.8	-124.5	20.3	1.3	-1.9
4TH	51.00	.3	.7	1942	1942	.2	.4	-225	92	-13.1	-125.3	18.7	1.5	-1.7
5TH	63.50	-.7	-2.5	1942	1942	-.4	-1.3	9	-3	-12.4	-122.8	17.1	1.7	-1.7
6TH	76.00	-3.4	-4.9	1942	1942	-1.8	-2.5	-15	10	-9.0	-117.9	15.6	1.8	-1.8
7TH	88.50	-1.5	-2.7	1843	1843	-.8	-1.5	2	-1	-7.5	-115.2	14.2	1.9	-1.8
8TH	101.00	-1.1	-2.9	1817	1817	-.6	-1.6	9	-3	-6.4	-112.3	12.8	2.0	-1.7
9TH	113.50	-1.3	-3.8	1817	1817	-.7	-2.1	6	-2	-5.2	-108.5	11.4	2.1	-1.7
10TH	126.00	-1.5	-4.7	1817	1817	-.8	-2.6	5	-1	-3.7	-103.8	10.1	2.1	-1.7
11TH	138.50	-1.3	-5.3	1817	1817	-.7	-2.9	7	-2	-2.4	-98.5	8.8	2.2	-1.6
12TH	151.00	-1.1	-5.9	1817	1817	-.6	-3.2	10	-2	-1.2	-92.6	7.6	2.2	-1.6
13TH	163.50	-.9	-6.4	1817	1817	-.5	-3.5	12	-2	-.3	-86.2	6.5	2.2	-1.5
14TH	176.00	-1.0	-6.7	1817	1817	-.5	-3.7	13	-2	.7	-79.6	5.4	2.2	-1.4
15TH	188.50	-1.3	-6.8	1817	1817	-.7	-3.7	13	-2	2.0	-72.8	4.5	2.2	-1.3
16TH	201.00	-1.6	-6.9	1817	1817	-.9	-3.8	12	-3	3.6	-65.9	3.6	2.1	-1.2
17TH	213.50	-1.8	-7.0	1817	1817	-1.0	-3.9	12	-3	5.4	-58.9	2.8	2.1	-1.1
18TH	226.00	-1.7	-7.2	1817	1817	-1.0	-3.9	13	-3	7.2	-51.7	2.2	2.0	-1.0
19TH	238.50	-1.7	-7.3	1817	1817	-.9	-4.0	15	-3	8.8	-44.4	1.6	1.9	-.9
20TH	251.00	-1.6	-7.5	1817	1817	-.9	-4.1	16	-3	10.4	-36.9	1.0	1.8	-.8
21ST	263.50	-2.0	-7.8	1817	1817	-1.1	-4.3	17	-4	12.4	-29.1	.6	1.6	-.7
22ND	279.50	-3.5	-10.5	2325	2325	-1.5	-4.5	17	-6	15.9	-18.6	.3	1.4	-.5
23RD	292.00	-1.9	-6.0	1570	1570	-1.2	-3.8	19	-6	17.8	-12.5	.1	1.2	-.3
24TH	308.00	-3.7	-10.6	2005	2005	-1.9	-5.3	15	-5	21.5	-2.0	-.1	.9	-.2
25TH	320.50	3.3	.2	1317	1317	2.5	.2	-1	11	18.2	-2.2	-.1	.6	-.1
26TH	336.50	1.9	-4.8	1685	1685	1.1	-2.9	12	5	16.3	2.6	-.1	.4	-.1
27TH	349.00	4.6	.4	1276	1276	3.6	.3	-1	6	11.8	2.3	-.0	.2	-.0
EAVE	361.50	4.8	.1	1275	1275	3.8	.0	-0	5	6.9	2.2	-.0	.1	-.0
TOP	379.50	6.9	2.2	1182	1182	5.9	1.9	-0	0	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 330 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-167.3	-37.0	15.8	-22.7	1.6
		-23.9	13.0	4039	4039	-5.9	3.2	-2	-3					
2ND	26.00									-143.5	-50.0	14.6	-18.6	1.7
		-9.3	6.5	1942	1942	-4.8	3.4	-1	-1					
3RD	38.50									-134.2	-56.6	14.0	-16.9	1.7
		-7.9	6.2	1942	1942	-4.1	3.2	2	2					
4TH	51.00									-126.3	-62.7	13.2	-15.3	1.7
		-7.5	3.6	1942	1942	-3.9	1.8	4	9					
5TH	63.50									-118.8	-66.3	12.4	-13.8	1.6
		-9.3	2.9	1942	1942	-4.8	1.5	-2	-6					
6TH	76.00									-109.5	-69.2	11.6	-12.3	1.7
		-6.4	3.1	1843	1843	-3.5	1.7	6	13					
7TH	88.50									-103.1	-72.3	10.7	-11.0	1.6
		-5.4	2.2	1817	1817	-3.0	1.2	10	24					
8TH	101.00									-97.7	-74.5	9.8	-9.7	1.4
		-5.2	1.2	1817	1817	-2.8	.6	7	30					
9TH	113.50									-92.5	-75.6	8.8	-8.6	1.3
		-4.9	.1	1817	1817	-2.7	.1	1	35					
10TH	126.00									-87.6	-75.8	7.9	-7.4	1.1
		-5.1	-1.0	1817	1817	-2.8	-.5	-6	30					
11TH	138.50									-82.5	-74.8	7.0	-6.4	.9
		-5.4	-2.1	1817	1817	-3.0	-1.1	-8	22					
12TH	151.00									-77.0	-72.7	6.0	-5.4	.8
		-5.8	-3.2	1817	1817	-3.2	-1.8	-8	15					
13TH	163.50									-71.2	-69.6	5.1	-4.4	.7
		-6.1	-4.1	1817	1817	-3.4	-2.3	-7	10					
14TH	176.00									-65.1	-65.4	4.3	-3.6	.6
		-6.4	-5.0	1817	1817	-3.5	-2.8	-6	7					
15TH	188.50									-58.7	-60.4	3.5	-2.8	.5
		-6.7	-5.9	1817	1817	-3.7	-3.2	-4	5					
16TH	201.00									-51.9	-54.6	2.8	-2.1	.5
		-6.9	-6.4	1817	1817	-3.8	-3.5	-3	3					
17TH	213.50									-45.1	-48.2	2.2	-1.5	.4
		-6.7	-6.4	1817	1817	-3.7	-3.5	-3	3					
18TH	226.00									-38.4	-41.8	1.6	-1.0	.4
		-6.5	-6.4	1817	1817	-3.6	-3.5	-2	2					
19TH	238.50									-31.8	-35.5	1.1	-.6	.4
		-6.3	-6.3	1817	1817	-3.5	-3.5	-2	2					
20TH	251.00									-25.5	-29.2	.7	-.2	.3
		-6.5	-6.4	1817	1817	-3.6	-3.5	-4	4					
21ST	263.50									-19.0	-22.7	.4	.1	.3
		-9.1	-8.8	2325	2325	-3.9	-3.8	-5	5					
22ND	279.50									-9.9	-14.0	.1	.3	.2
		-5.6	-4.9	1570	1570	-3.6	-3.1	-3	3					
23RD	292.00									-4.3	-9.1	-.1	.4	.2
		-10.0	-9.2	2005	2005	-5.0	-4.6	-3	3					
24TH	308.00									5.7	.1	-.1	.4	.1
		1.0	.4	1317	1317	.8	.3	8	-22					
25TH	320.50									4.7	-.3	-.1	.3	.1
		-3.7	-4.4	1685	1685	-2.2	-2.6	-6	5					
26TH	336.50									8.3	4.1	-.1	.2	.0
		1.4	1.0	1276	1276	1.1	.8	0	-0					
27TH	349.00									6.9	3.1	-.1	.1	.0
		1.8	.7	1275	1275	1.4	.6	7	-16					
EAVE	361.50									5.1	2.4	-.0	.0	.0
		5.1	2.4	1182	1182	4.3	2.0	1	-2					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 340 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-66.0	285.9	-45.8	-5.5	2.7
		-21.5	26.6	4039	4039	-5.3	6.6	-3	-3					
2ND	26.00									-44.5	259.3	-38.7	-4.1	2.9
		-8.3	14.5	1942	1942	-4.3	7.5	-3	-2					
3RD	38.50									-36.2	244.8	-35.5	-3.6	3.0
		-6.7	15.0	1942	1942	-3.5	7.7	-2	-1					
4TH	51.00									-29.4	229.8	-32.5	-3.2	3.0
		-3.1	13.0	1942	1942	-1.6	6.7	5	1					
5TH	63.50									-26.3	216.8	-29.8	-2.8	2.9
		-2.5	12.2	1942	1942	-1.3	6.3	-3	-1					
6TH	76.00									-23.8	204.6	-27.1	-2.5	3.0
		-1.8	13.5	1843	1843	-1.0	7.3	5	1					
7TH	88.50									-22.0	191.1	-24.7	-2.2	2.9
		-1.0	13.0	1817	1817	-.6	7.2	8	1					
8TH	101.00									-21.0	178.1	-22.3	-2.0	2.8
		-.4	12.3	1817	1817	-.2	6.8	8	0					
9TH	113.50									-20.6	165.8	-20.2	-1.7	2.7
		.2	11.7	1817	1817	.1	6.4	9	-0					
10TH	126.00									-20.7	154.1	-18.2	-1.4	2.6
		-.0	11.0	1817	1817	-.0	6.0	10	0					
11TH	138.50									-20.7	143.1	-16.3	-1.2	2.5
		-.5	10.2	1817	1817	-.3	5.6	12	1					
12TH	151.00									-20.2	132.9	-14.6	-.9	2.4
		-1.0	9.5	1817	1817	-.6	5.2	13	1					
13TH	163.50									-19.2	123.4	-13.0	-.7	2.2
		-1.4	8.9	1817	1817	-.8	4.9	14	2					
14TH	176.00									-17.9	114.5	-11.5	-.5	2.1
		-1.6	8.4	1817	1817	-.9	4.6	15	3					
15TH	188.50									-16.2	106.1	-10.1	-.2	2.0
		-1.9	7.9	1817	1817	-1.0	4.4	16	4					
16TH	201.00									-14.4	98.2	-8.9	-.1	1.8
		-2.1	7.5	1817	1817	-1.2	4.1	17	5					
17TH	213.50									-12.3	90.8	-7.7	.1	1.7
		-2.3	7.0	1817	1817	-1.3	3.9	18	6					
18TH	226.00									-10.0	83.7	-6.6	.3	1.6
		-2.5	6.6	1817	1817	-1.4	3.6	19	7					
19TH	238.50									-7.4	77.1	-5.6	.4	1.4
		-2.6	6.5	1817	1817	-1.4	3.6	21	8					
20TH	251.00									-4.8	70.6	-4.7	.4	1.3
		-2.6	7.2	1817	1817	-1.4	3.9	23	8					
21ST	263.50									-2.3	63.4	-3.8	.5	1.1
		-3.4	10.1	2325	2325	-1.5	4.3	26	9					
22ND	279.50									1.2	53.3	-2.9	.5	.8
		-2.3	3.7	1570	1570	-1.4	2.3	36	22					
23RD	292.00									3.4	49.7	-2.3	.5	.6
		-4.0	8.5	2005	2005	-2.0	4.2	22	10					
24TH	308.00									7.4	41.1	-1.5	.4	.4
		1.5	5.7	1317	1317	1.2	4.3	16	-4					
25TH	320.50									5.9	35.5	-1.0	.3	.3
		-1.3	9.7	1685	1685	-.8	5.7	13	2					
26TH	336.50									7.2	25.8	-.6	.2	.1
		1.4	7.5	1276	1276	1.1	5.9	7	-1					
27TH	349.00									5.9	18.3	-.3	.1	.1
		1.3	7.3	1275	1275	1.0	5.7	12	-2					
EAVE	361.50									4.6	11.0	-.1	.0	.0
		4.6	11.0	1182	1182	3.9	9.3	0	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : LPC MANDALAY LAS COLINAS,TEXAS
WIND DIRECTION 350 CONFIGURATION C REFERENCE PRESSURE 25.0 PSF GUST FACTOR 1.32

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (FT) X	ECCEN (FT) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-29.9	630.3	-119.1	-4.3	.1
		-18.3	39.1	4039	4039	-4.5	9.7	-4	-2					
2ND	26.00									-11.5	591.1	-103.2	-3.8	.3
		-7.4	21.1	1942	1942	-3.8	10.9	-5	-2					
3RD	38.50									-4.1	570.0	-96.0	-3.7	.4
		-6.4	22.4	1942	1942	-3.3	11.6	-6	-2					
4TH	51.00									2.3	547.6	-89.0	-3.7	.5
		.1	21.1	1942	1942	.1	10.9	8	-0					
5TH	63.50									2.1	526.5	-82.3	-3.7	.4
		1.9	16.3	1942	1942	1.0	8.4	4	-0					
6TH	76.00									.3	510.2	-75.8	-3.7	.3
		1.6	21.4	1843	1843	.9	11.6	-1	0					
7TH	88.50									-1.4	488.8	-69.5	-3.7	.3
		2.0	22.4	1817	1817	1.1	12.3	-1	0					
8TH	101.00									-3.3	466.4	-63.6	-3.7	.4
		2.6	22.5	1817	1817	1.4	12.4	-1	0					
9TH	113.50									-5.9	443.9	-57.9	-3.6	.4
		3.1	22.6	1817	1817	1.7	12.4	-1	0					
10TH	126.00									-9.0	421.3	-52.5	-3.5	.4
		3.0	22.2	1817	1817	1.6	12.2	-1	0					
11TH	138.50									-12.0	399.1	-47.4	-3.4	.4
		2.5	21.8	1817	1817	1.4	12.0	-0	0					
12TH	151.00									-14.5	377.3	-42.5	-3.2	.4
		2.0	21.3	1817	1817	1.1	11.7	0	-0					
13TH	163.50									-16.5	356.0	-37.9	-3.0	.4
		1.6	20.8	1817	1817	.9	11.5	1	-0					
14TH	176.00									-18.1	335.2	-33.6	-2.8	.4
		1.3	20.4	1817	1817	.7	11.2	1	-0					
15TH	188.50									-19.5	314.8	-29.5	-2.6	.4
		1.0	19.9	1817	1817	.5	11.0	1	-0					
16TH	201.00									-20.5	294.8	-25.7	-2.3	.4
		.6	19.8	1817	1817	.3	10.9	1	-0					
17TH	213.50									-21.1	275.0	-22.2	-2.1	.3
		.1	20.1	1817	1817	.1	11.1	1	-0					
18TH	226.00									-21.2	254.9	-18.8	-1.8	.3
		-.3	20.5	1817	1817	-.2	11.3	2	0					
19TH	238.50									-20.9	234.5	-15.8	-1.5	.3
		-.8	21.2	1817	1817	-.4	11.7	2	0					
20TH	251.00									-20.1	213.2	-13.0	-1.3	.2
		-1.2	23.1	1817	1817	-.6	12.7	3	0					
21ST	263.50									-19.0	190.1	-10.5	-1.0	.2
		-2.1	31.9	2325	2325	-.9	13.7	4	0					
22ND	279.50									-16.8	158.2	-7.7	-.8	.1
		-1.8	18.2	1570	1570	-1.1	11.6	5	0					
23RD	292.00									-15.1	140.0	-5.8	-.6	-.0
		-4.0	29.2	2005	2005	-2.0	14.6	5	1					
24TH	308.00									-11.1	110.8	-3.8	-.4	-.2
		-1.6	19.5	1317	1317	-1.2	14.8	1	0					
25TH	320.50									-9.4	91.3	-2.6	-.2	-.2
		-3.5	29.4	1685	1685	-2.1	17.5	-0	-0					
26TH	336.50									-5.9	61.8	-1.3	-.1	-.2
		-2.2	17.7	1276	1276	-1.7	13.8	-3	-0					
27TH	349.00									-3.8	44.2	-.7	-.0	-.1
		-2.7	18.8	1275	1275	-2.1	14.7	-4	-1					
EAVE	361.50									-1.0	25.4	-.2	-.0	-.1
		-1.0	25.4	1182	1182	-.9	21.5	-3	-0					
TOP	379.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. BASE SHEAR AND MOMENT SUMMARY : LPC MANDALAY LAS COLINAS,TEXAS
CONFIGURATION C REFERENCE PRESSURE 25.0 GUST FACTOR 1.32

AZIMUTH	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z	ECCEN (FT) X	ECCEN (FT) Y
0	16.8	500.2	-94.8	6.1	-.0	-0	0
10	73.4	527.5	-99.3	17.9	.9	2	-0
20	64.2	540.6	-98.8	16.7	2.6	5	-1
30	14.4	553.5	-99.0	7.0	3.8	7	-0
40	-167.3	684.7	-120.9	-28.7	3.8	5	1
50	-368.6	683.9	-120.4	-69.8	2.8	3	2
60	-632.3	768.7	-134.5	-122.5	-.9	-1	-1
70	-730.2	732.1	-126.5	-142.0	-2.3	-2	-2
80	-750.4	644.0	-108.0	-145.6	-2.7	-2	-2
90	-1052.3	610.5	-96.3	-204.2	-5.2	-2	-4
100	-1036.8	309.3	-41.9	-200.9	-4.4	-1	-4
110	-928.1	120.9	-9.1	-179.1	.3	0	0
120	-894.3	-204.4	48.7	-174.1	3.1	-1	3
130	-766.5	-509.9	97.1	-150.2	3.6	-2	3
140	-731.4	-675.2	123.8	-144.1	2.2	-2	2
150	-699.4	-652.8	122.8	-138.0	1.1	-1	1
160	-455.0	-658.7	129.0	-93.5	.1	-0	0
170	-255.9	-893.2	175.5	-55.0	-2.0	2	-1
180	-28.8	-993.1	193.4	-7.9	-2.4	2	-0
190	268.1	-1018.4	195.9	42.4	2.4	-2	-1
200	431.1	-1089.2	204.7	69.6	4.6	-4	-1
210	645.3	-1059.7	200.5	110.0	5.8	-4	-2
220	733.9	-770.2	149.4	130.0	2.2	-1	-1
230	851.6	-747.5	141.8	155.1	1.1	-1	-1
240	802.7	-620.3	115.5	145.5	-1.8	1	1
250	780.6	-473.4	80.3	141.6	-3.1	2	3
260	771.4	-112.4	13.2	141.5	-4.5	1	6
270	679.8	75.3	-19.9	125.9	-4.5	-1	6
280	665.1	29.4	-8.8	125.5	-2.6	-0	4
290	658.9	-36.2	5.1	127.4	-.6	0	1
300	570.8	-153.9	28.1	112.9	.5	-0	-1
310	405.1	-93.2	17.6	82.5	-2.7	1	6
320	-22.8	-117.0	24.9	.7	-2.4	19	-4
330	-167.3	-37.0	15.8	-22.7	1.6	-2	9
340	-66.0	285.9	-45.8	-5.5	2.7	9	2
350	-29.9	630.3	-119.1	-4.3	.1	0	0