THESIS

DEVELOPMENT OF FRAMEWORK FOR PREDICTING WATER PRODUCTION FROM OIL AND GAS WELLS IN WATTENBERG FIELD, COLORADO

Submitted by

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ABSTRACT

DEVELOPMENT OF FRAMEWORK FOR PREDICTING WATER PRODUCTION FROM OIL AND GAS WELLS IN WATTENBERG FIELD, COLORADO

Water issues in the oil and gas industry have drawn attention from various stakeholders including the public, industry and environmental groups. With the increasing demand for energy, the number of oil and gas wells has increased greatly providing 60% of the energy in the United States. Besides the large volume of fresh water required for drilling and hydraulic fracturing, wastewater from the well can also lead to serious problems. The current approach for managing wastewater from oil and gas fields is deep well injection or evaporation both of which can potentially cause environmental issues. One of the best strategies to solve water issues from oil and gas operations is to reuse wastewater as drilling and fracturing water so the volume of fresh water required and wastewater disposed can be reduced. Information on both water quantity and quality are required when designing wastewater reuse treatment facilities. This study provides a framework for understanding water production trends from oil and gas wells in the Wattenberg field in Northern Colorado by analyzing historical data from Noble Energy Inc. The Arps equations were chosen for modeling water production from oil and gas wells. After studying 1,677 vertical and 32 horizontal wells in Wattenberg field, an exponential decline function was applied to model the produced water production of all the wells and the frac flowback water of horizontal wells. An Excel based 30-year water production prediction tool was developed based on the two protocols developed for vertical and horizontal wells in the Wattenberg field. Three case studies of different subsets of oil and gas wells were examined to illustrate the function of

the tool. In addition, a comparison of exponential and harmonic functions was made in the third case study, and a significant difference was observed. The harmonic decline function predicts a less aggressive decline resulting in higher production volumes. It was concluded that in the absence of long term production data, the harmonic decline function should be used since the exponential decline function may underestimate the volume of produced water.

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Chapter 1. Introduction

1.1. Origins of the problem

"Courage, determination, and hard work are all very nice, but not so nice as an oil well in the back yard."

-Mason Cooley

With the rapid growth of economies throughout the world over the past several decades, the availability of energy has become critically important. As major forms of fuel, oil and gas provide about 60 percent of the world's 6.9 billion people with their daily energy needs, while other forms of energy like coal, nuclear and hydroelectric power, wind and solar provide the other 40 percent [1]. With the economic recovery of the United States and the rest of the world, total energy demand will rise by 1.2% per annum in the next five years in the US [2], driving the need for additional oil and gas supplies. More oil and gas wells will be drilled to meet the energy demand increase; therefore, more hydraulic fracturing will be performed in the future. With heightened public knowledge and awareness of hydraulic fracturing, many people believe that the fracturing process can cause severe environmental problems, such as water shortages and pollution of both surface and ground water [3].

In order to drill a new oil and gas well, water mixed with other chemical components and sand is used for hydraulic fracturing to release oil and gas from shale formations deep beneath the ground [4]. Water usage varies depending on the type of well. Typically for vertical wells, 65,000 to 600,000 gallons of water is needed, but horizontal deep shale gas and oil wells require an average of 4.5 million gallons of water per well [4]. Fresh water is

often the major water source for hydraulic fracturing. As one of the states that have large oil and gas reserves, Colorado has over 95,000 oil and gas wells in total as of February, 2012 [5]. The biggest oil and gas field in Colorado is the Wattenberg field lying northeast of Denver, and average water usage for the wells in the Wattenberg field is around 3 million gallons per well [6]. Due to the rapid growth of population and industry in Colorado, the water scarcity problem has drawn more attention than ever before [7]. Besides the large amount of water needed for hydraulic fracturing, the water pollution problem is also becoming critical with the exploration and production of oil and gas wells. Though there is no evidence that hydraulic fracturing pollutes ground and surface water, people have begun to discuss this because of the additives in the fracturing water [8]. At the same time, since water also comes out with gas and oil from a well, it is important and necessary to have a good understanding of water as well as oil and gas production.

1.2. Structure of thesis

To better understand the impact of water from oil and gas wells, an in-depth study was performed to analyze the overall water balance during the entire oil and gas production process. Protocols and models were designed to predict total water production from oil and gas wells from a given field. The thesis is divided into 4 sections: (1) review of existing literature about water production in oil and gas wells, (2) analysis of production data from sample wells in Wattenberg field and modeling of the water production trend for both vertical and horizontal wells, (3) discussion of protocols and tools designed to predict total water production for the life of the well and (4) case studies on wells in different selected regions of Wattenberg field with uncertainty analysis.

Chapter 2. Literature review

2.1. Introduction

By the end of 2009, according to the U.S. Energy Information Administration, the proven reserves of crude oil in the U.S. were 22.3 billion barrels, and natural gas reserves were 283.9 trillion cubic feet [9]. The latest report released by the U.S. EIA showed that by the end of 2010, the proved reserves of crude oil in the U.S. were 25.2 billion barrels and the natural gas reserves were 317.6 trillion cubic feet [9]. Oil and gas make up to 60% of the energy source in the U.S. and the number of oil and gas wells will increase as a result of the increased energy demand. [10]. Water problems associated with oil and gas wells have caused concern [11] including water demand for drilling and fracturing [12,13,14], water contamination [15,16] and collection and handling of frac flowback and produced water during the oil and gas production process[17,18,19].

When oil or gas is extracted from underground formations, water also comes to the surface, and it is usually called produced water [20]. Also, as the largest waste stream generated by the oil and gas industry [20], produced water is difficult to manage and treat. In the United States, approximately 21 billion barrels of produced water has been generated from nearly one million oil and gas wells in 1985 and 18 billion bbls in 1995 [21,22] and 14 billion bbls in 2002 [20,23]. In Colorado, there are roughly 49,800 active wells and with an additional 46,300 wells which have been plugged and abandoned [5]. As one of the largest natural gas deposits in the United States, Wattenberg oil and gas field is located in the Denver-Julesburg Basin. In 2009, with an estimated 195.3 billion cubic feet of natural gas

production, Wattenberg field was ranked as the 10th largest source of natural gas in the United States [24]. Figure 2.1 shows the location of Wattenberg field in Colorado.



Figure 2.1. Wattenberg field in Colorado [25]

The 100 square mile geological formation located north of Denver, Colorado in Weld, Adams, Boulder, Broomfield and Larimer counties, Wattenberg field produces both crude oil and natural gas [25]. Currently there are over 18,000 wells in the Wattenberg field [26] and over 7,700 wells are operated by the Noble Energy Inc. New wells are still being drilled every year in the Wattenberg field [5], which demands a large volume of water for drilling and fracturing and results in significant frac flowback and produced water. In Colorado, most of the drilling water, known as hydraulic fracturing water, comes from fresh water.

Today, water shortages are not only a regional problem but a global consideration. The rapidly increasing population and industrial activity have led to increased water demand and

use. That, together with climate change, has contributed to a world-wide water crisis. In the United States, the government projects that by 2013 at least 36 states will face water shortages due to the combined results of rising temperatures, drought, population growth, urban sprawl, waste and excess [27]. As the principal river of the southwestern United States and northwestern Mexico, the Colorado River supplies water for agricultural and urban areas as well as hydroelectric power in the southwestern desert lands of North America [28]. A study in Water Resources Research in 2007 showed Colorado River reservoirs would risk running dry by 2057, leaving many downstream cities like Las Vegas, Los Angeles and San Diego short of water [29]. The Colorado Water Conservation Board has identified potential solutions to mitigate the water shortage in Colorado. One of the key outcomes to reach the water conservation goal is to recycle and reuse waste water [30], which also applies to the oil and gas industry.

2.2. Water use in energy production

Water is very important in energy resource development. Table 2.1 shows the water use for generating 1 million British thermal unit (MMBTU) of energy by different types of energy resources. On average coal requires 2-8 gallons of water without slurry transport and 13-32 gallons of water with slurry transport. On the other hand, only 0.82-3.7 gallons of water is needed by deep shale natural gas [31] to produce the same amount of energy, and groundwater is the major source of water used in shale gas exploration. It is clearly shown that water use for natural gas extraction can be less than the water used by other energy sources, therefore natural gas would be the best choice for saving water in energy production.

Table 2.1: Water use for energy production from various energy resources [32]

Energy Resource ¹	Range of Gallons of Water Used per MMBTU of Energy Produced	
Deep Shale Natural Gas	0.84 - 3.70 ²	
Coal (no slurry transport) Coal (with slurry transport)	2 – 8 13 – 32	
Nuclear (uranium ready to use in a power plant)	8 – 14	
Conventional Oil	8 – 20	
Synfuel - Coal Gasification	11 – 26	
Oil Shale	22 – 56	
Tar Sands	27 – 68	
Synfuel - Fisher Tropsch (from coal)	41 – 60	
Enhanced Oil Recovery (EOR)	21 – 2,500	
Biofuels (Irrigated Corn Ethanol, Irrigated Soy Biodiesel)	> 2,500	

Source: "Deep Shale Natural Gas: Abundant, Affordable, and Still Water Efficient", GWPC, 2010.

On average 1 to 5 million gallons of water is used to drill and fracture a shale gas well, and sometimes a well can be fractured up to 18 times. According to "The Marcellus Effect," a typical gas well uses about 4 million gallons of fresh water over its lifetime [33]. A study of Noble oil and gas wells in Wattenberg field [6, 34] found that an average of 3 million gallons of fresh water is used for the hydraulic fracturing of one well. Besides the impact this might have on regional water availability, water transportation and storage must also be considered because the cost can be significant [35].

²The transport of natural gas can add between zero and two gallons per MMBTU.

2.3. Water production from oil and gas wells

Water production, one of the major environmental, economic, and technical problems in the oil and gas industry, can limit the productive life of wells and cause severe operational problems such as corrosion, fines migration and hydrostatic loading. It is estimated that on average 8 barrels of water are generated while producing one barrel of oil, and the money spent in the United States to handle and dispose of the produced water is around 5 to 10 billion dollars every year [20].

2.3.1. Water production source and mechanism

The sources of produced water include injected water (frac water), formation water and aquifers. The injected hydraulic fracturing water could be the major source of water from oil and gas wells. After a large amount of water is injected into the formation where the well is drilled, only 15-40% of that water comes out as frac flowback [36]. The rest of the water stays in the formation and may come out at some point as produced water with oil and gas production through the life-cycle of the well. Formation water is another source of produced water. This is water which was originally trapped within the formation like oil and gas, but it can have limited contribution to water production. Aquifers could be another potential source of produced water.

Water can follow two types of paths to the wellbore. In the first one, water usually flows to the wellbore through a separate path from that of the hydrocarbons. Usually this type of water production will compete with oil and gas production, so in order to increase oil and gas production rates with higher recovery efficiency, this type of water production must be reduced. The second type of water production is water that is co-produced with oil, usually in

the later life time of a well. In this case, the reduced water production may result in a corresponding reduction in oil production [20].

2.3.2. Causes of water production problems

The causes of water contamination and production problems can be divided into three main categories: mechanical problems, completion related problems and reservoir related problems.

Mechanical problems refer to poor mechanical integrity of the casing, such as holes, wear and splits, and other leaks. Casing leaks lead to unwanted water entry and a rise in water production. Completion related problems include channels behind the casing, completion into or close to a water zone and fracturing out of the zone. The reservoir related problems are mainly channeling, coning and depletion [20].

2.4. Characteristics of water production

Based on the quantity and quality of the water coming out of the well, the water can be classified as two types: frac flowback water and conventional produced water.

2.4.1. Frac flowback water

Frac flowback water is the water produced from the fracturing of oil and gas wells, and it usually consists of fracturing fluid which returns to the surface. This water always contains chemicals, metals, and other components that are used for hydraulic fracturing. The frac load recovery can be from 15-40% of the fracturing fluid [36], and it flows back over a period of 3 to 4 weeks after fracturing, most of it within 7-10 days. Flowback water usually has high salinity and total dissolved solids (TDS) as well as organics and metals [37]. Table 2.2 shows the comparison of water quality between feed water and frac flowback. From the table, water

quality changes significantly from feed water to flowback. High salinity and TDS is seen in flowback water as well as organic materials like methanol and total organic carbon (TOC).

Table 2.2: Flowback water quality (mg/L) [35]

Parameter	Feed Water	Flowback	
рН	8.5	4.5 to 6.5	
Calcium	22	22,200	
Magnesium	6	1,940	
Sodium	57	32,300	
Iron	4	539	
Barium	0.22	228	
Strontium	0.45	4,030	
Manganese	1	4	
Sulfate	5	32	
Chloride	20	121,000	
Methanol	Neglible	2,280	
TOC	Neglible	5,690	

2.4.2. Produced water

Produced water is the water that naturally occurs in the shale beds that are traversed by the wellbore. Usually, produced water flows throughout the whole lifecycle of the well along with oil and gas production, and there is currently no clear understanding of the volume and production rate of produced water over time. This water is also very saline with a high TDS. The water quality of produced water can vary a lot depending on the formation and the type of well [37]. The comparison of flowback water with conventional produced water is shown in Table 2.3. High TDS and TSS can be seen in produced water, and the oil and grease can vary a lot from a dry natural gas well to crude oil well.

Table 2.3: Comparison of flowback water quality with produced water quality [38]

Comparison of FB Water with Conventional Produced Water							
Parameter	14-d FB	Location B	Conv. PW				
Parameter	14-u FB	14-u FD	Ranges ^F				
pH	5.5	6.5	5 - 8				
Alkalinity *	52	93	NA				
TDS **	112,000	105,000	20,000 - 100,000				
Tot Susp Solids **	17	197	0-250				
Tot Org Carbon **	34	39	NA				
Biochemical Oxygen Demand *	149	2.8	NA				
Oil & Grease **	31	< 5 mg/l	3 – 100				
* mg/l as CaCO3 ** mg/l	¥ mg/l as O ₂ ‡ ND = Nondete	1	Not Available 2004; GRI, '94				

2.5. Produced water management

Due to the potentially hazardous components in the flowback and produced water, U.S. Environmental Protection Agency (EPA) has regulated the disposal of produced water [39]. There are five ways currently in use for the management and disposal of flowback and produced water.

2.5.1. Evaporation in pits/ponds

Though natural evaporation would be the easiest and cheapest way to handle produced water, it is not practical due to a number of restrictions. Usually natural evaporation can only happen in dry areas where the precipitation rate is lower than the evaporation rate, and evaporation will be limited because of the extremely high salinity and TDS of the water. Also

the grease and organics in the water may form a crust over the pond and lead to the failure of evaporation [35].

2.5.2. Disposal wells

As the most commonly used method for produced water disposal, the disposal well is a contentious topic. The injection of produced water into deep underground injection wells allows saltwater (frac flowback and produced water) to be managed [40]. According to the Energy Tomorrow Blog, the number of class II injection wells in each state is shown in Figure 2.2.

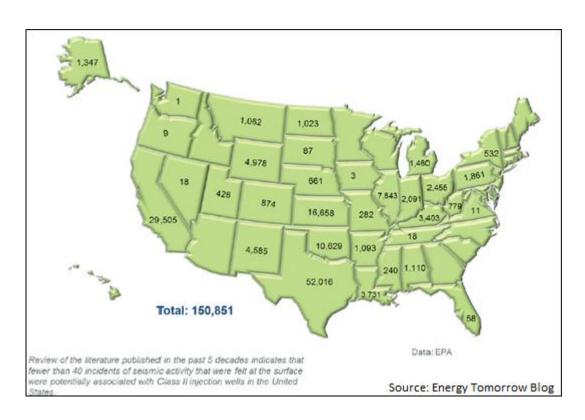


Figure 2.2. Class II injection wells across the country

EPA has delegated underground injection control to each state, following the federal Safe Drinking Water Act for surface ground water protection. Operators are therefore required to follow the disposal regulations of each state [40].

Figure 2.3 shows the typical construction of a class II injection well. The construction standards for a disposal well require three layers of casing to protect groundwater. The first layer is surface casing, with a steel pipe encased in cement from ground surface to the deepest groundwater level. This casing provides protection during the drilling of the well. The second layer is the production casing, with a pipe placed in the wellbore and cemented permanently in place. The third protection layer is the injection tubing string and packer through which the injected water can travel to the underground formation. Because of the three protection layers in a class II injection well, impact on groundwater can only be seen when all three layers fail at the same time [40].

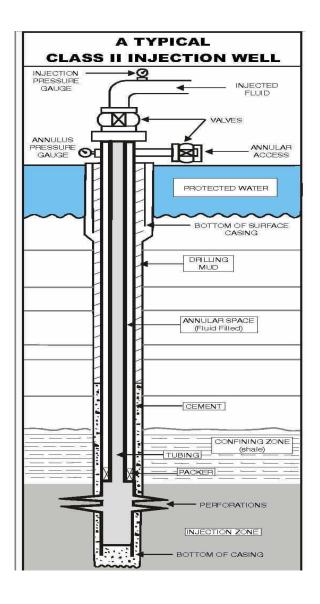


Figure 2.3. Wellbore of typical class II injection well [40]

Though disposal wells have been adopted widely for produced water management, it is considered unsafe to inject produced water directly into disposal wells because of the potential impacts to water supply aquifers and the possibility that the produced water may migrate to streams. So in many states, disposal wells are inspected at least once a year to make sure that no contamination has occurred. Another concern of injection wells was the potential of causing induced seismicity. Earthquakes related to injection wells have been reported in Texas and Ohio. In October 20, 2011 a 4.8 magnitude earthquake struck the area

of South Texas where many oil and gas wells are located. Seismologists explained that it was not caused by hydraulic fracturing but the injection of disposed fracing wastewater [41]. Besides earthquakes, induced seismicity is more likely to happen as a result of the injection of fracing wastewater [42]. At the same time, due to the limited capacities of the disposal well (1200 to 3000 bpd) and the substantial capital investment with uncertain life span (1 to 2 million dollars), as well as other factors like transportation, few new injection wells have been permitted. As a result, disposal wells will probably play less of a future role in the management of produced water [35].

2.5.3. Disposal to publicly owned treatment works (POTWs)

Another alternative for handling produced water is to dispose of the water into publicly owned treatment works (POTWs). However, because of the high salinity of produced water and the biological processes commonly adapted in POTWs which do not remove TDS, it's currently impractical and perhaps not possible to treat the produced water in POTWs. In addition regulatory limitations prohibit this option [35].

2.5.4. Direct reuse for fracturing

Since the hydraulic fracturing fluid has high viscosity and various additives, many companies have considered reusing produced water directly for fracturing. Chemical additives can be recycled by recycling produced water for hydraulic fracturing, and because of the high salinity requirement of fracturing fluid, TDS does not need to be decreased, so that energy and cost for treatment can be kept at a lower level. However some other chemical components such as chlorides should be removed or reduced because they can cause

corrosion and impact fracturing. Also safety problems such as chlorides and bacteria should be considered when reusing produced water for fracturing [35]. To treat produced water for fracturing use, typical treatment processes include: separation of oil and grease, organic material adsorption and removal, hardness removal and raw TSS removal. Figure 2.4 shows an example of the treatment process for treating produced water for reuse as fracturing fluid.

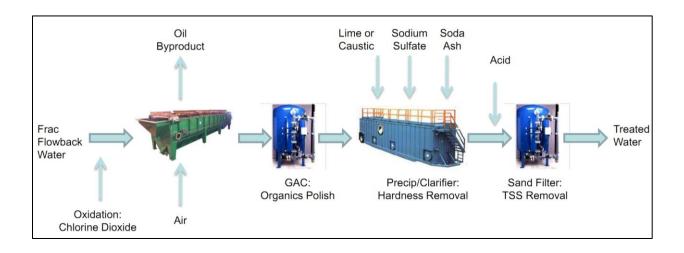


Figure 2.4. Example treatment process of produced water for reuse as fracturing fluid [43]

2.5.5. Treatment for reuse or surface discharge

In order to reuse produced water for purposes other than use in hydraulic fracturing, additional treatment processes are needed. TDS reduction is the most critical process in this type of treatment of produced water. For example, the TDS standard for agricultural irrigation is less than 2,000 mg/L and for surface discharge, the TDS should be less than 500 mg/L. Hence different treatment processes should be used for different TDS removal targets. For this type of reuse, membrane filtration is usually used after the treatment processes

illustrated in Figure 2.4, and reverse osmosis (RO) membrane is the best choice. Figure 2.5 shows the treatment process for reusing produced water for agriculture or surface discharge.

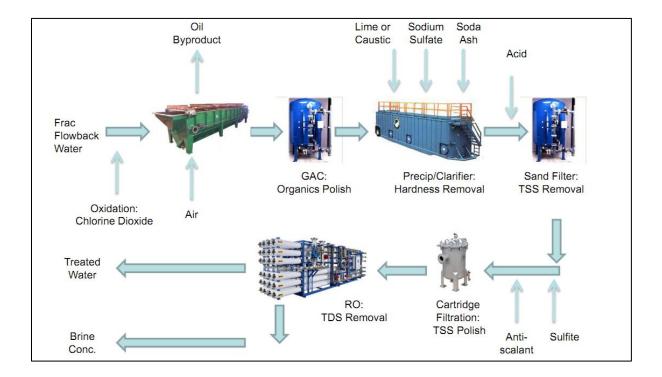


Figure 2.5. Example treatment process of produced water for agricultural use or surface discharge [43]

Though membrane filtration is the most efficient way for TDS removal, the cost is always high and varies depending on the influent water quality and outflow water quality target [35]. Figure 2.6 shows the relative cost vs. the range of applicability.

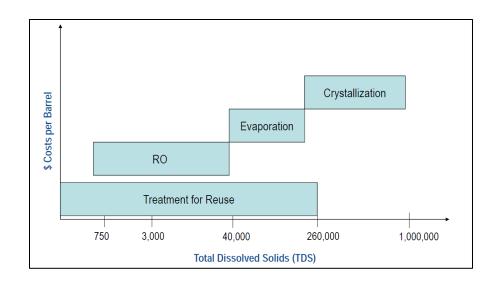


Figure 2.6. Range of applicability vs. cost for treating produced water [43]

2.6. Environmental impacts in the oil and gas industry

In addition to the amount of water use in hydraulic fracturing, there are other environmental and community concerns related to shale oil and gas development. The potential impacts are summarized in Figure 2.7: air issues, community impacts, water issues and land issues.

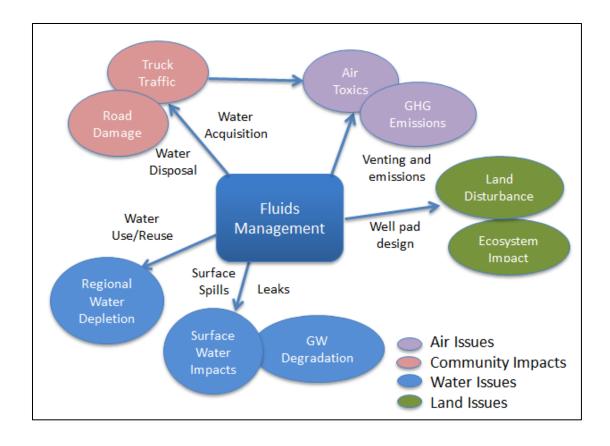


Figure 2.7. Major issues from shale oil and gas well development

2.6.1. Air issues

Leakage of gases from the well and engine emissions from trucks and pumps are two sources of air issues. The major type of leakage from a gas well is the gas itself, composed of methane, ethane, liquid condensate and VOCs. Some of these are potent greenhouse gases (GHGs) that can contribute to global warming and others (e.g. benzene) can cause public health problems. Studies conducted in Denver in 2011 and 2012 show that 4% (more than the 1-2% estimated previously) of the methane produced by gas wells was being released [28, 44, 45]. Research in 2012 shows that air pollution caused by fracturing may lead to acute and chronic health problems for people living near drilling sites [46]. Also, diesel trucks that

transport water and other materials for fracturing and the engines for the high pressure pumping are important sources of emissions.

2.6.2. Community impacts

Because nearly all oil and gas wells are in rural areas, a dramatic increase in traffic is required. Gas Field Specialists, one of the well services companies in Shinglehouse, Pennsylvania, uses tanker trucks to carry fracturing fluids and wastewater from the well. According to their estimates, if 2 million gallons of water is used for one well, 366 tanker trucks are required for hauling fresh water and another 183 trucks for hauling waste water, so a total of 549 tanker truck trips are needed for the hydraulic fracturing of one well [47]. However in Pennsylvania, in order to drill one horizontal Marcellus well, total water use is 3.5 million gallons on average and it requires about 960 truck trips to carry all the fresh and waste water [47]. According to the study on Noble wells in Wattenberg field, Colorado, 3 million gallons of water is needed for hydraulic fracturing [6, 34] and 824 truck trips are needed.

2.6.3. Water issues

Water used for drilling and hydraulic fracturing usually comes from existing sources and therefore competes with other users. Due to the amount of water that is used for hydraulic fracturing, well drilling may lead to regional water depletion, especially in dry areas.

Additionally, water contamination is another concern in oil and gas operations. Surface spills and leakages of fracturing fluid from the wellbore are two potential mechanisms for water contamination. Both fracturing liquids and produced water can spill out from the well and cause environmental contamination. Meanwhile, the wastewater disposed of either in disposal wells or evaporation ponds can pollute surface and ground water with both the

chemicals used in the fracturing fluids, contaminants from the formation water and naturally occurring radioactive materials (NORM) from the deep shale formation. The typical gases that can escape during fracturing and drilling operations are methane, ethane, and other VOCs that may be hazardous (e.g. benzene).

2.6.4. Land issues

Another issue is the land and space used by the well. For a Marcellus well, only 16 wells can be spaced per square mile, and on average a town can contain up to 1500 wells [47]. Horizontal wells, on the other hand, require a large space, so more land is needed. Usually a pad can range from 5 to 15 acres. The development of natural gas could also potentially have an impact on the terrestrial ecosystem. Trees, shrubs and other understory plants respond to the fracturing fluid with leaves turning brown, wilting, and subsequent leaf and bud mortality [48]. Also it may have impact on wild animals by destroying their living habitats and ranges and exposing them with chemical additives. In Pennsylvania, September 2009, Dunkard Creek suffered from a massive fish kill and EPA scientists pointed out it may have been the result of the wastewater from hydraulic fracturing of shale gas [49]. At the same time, road damage as well as erosion and sediment can be seen as a result of drilling new natural gas well.

2.7. Ways to minimize environmental impacts from hydraulic fracturing

Since water is the most important part in hydraulic fracturing, the best way to minimize environmental impacts is better fluid management. This includes both water management and air emission control.

2.7.1. Water management

Oil and gas wells are usually widely dispersed and wastewater from the wells is generated in small volumes compared to domestic wastewater. In addition, there is a difference in water quality between frac flowback and produced water, and different purposes for the end use of the treated water exist. For these reasons, it is difficult to set up a centralized wastewater treatment facility in rural areas for these wells. Therefore, a Geographic Information System (GIS) based approach is required to optimize water management. Among all water management practices, water reuse and recycling is the most efficient and effective approach for minimizing impacts.

By recycling and reusing wastewater for hydraulic fracturing, fresh water demand will decrease and hence the required truck trips will also be decreased. Also, with less wastewater being injected into disposal wells or evaporation ponds, the possibility of surface and groundwater contamination will be lowered as well as the impact of the contamination on ecosystems.

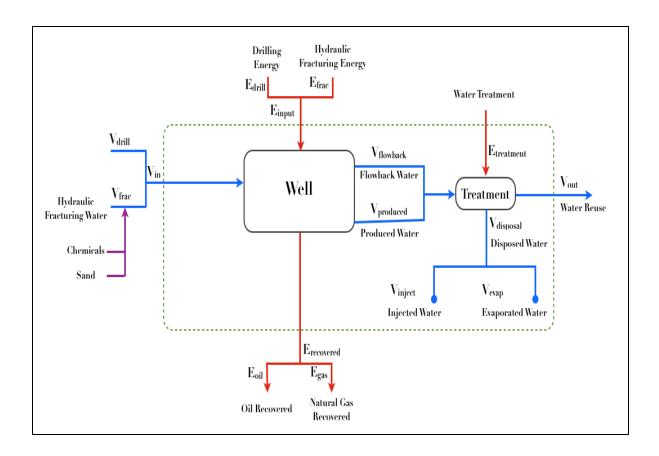


Figure 2.8. Oil and gas well energy and water balance

Figure 2.8 shows energy and water balance for a typical shale oil and gas well. Best water management can be achieved by treating wastewater from the well. According to Figure 2.8, by reusing treated water from the wastewater treatment facility, there will be less disposal water and the related issues will be reduced. Also the reused water will help decrease the amount of fresh water demand which provides higher efficiency of water use. In order to design the capacity of the treatment facility, both water quantity and quality of frac flowback and produced water is required. Water quality can be easily tested; however, there is no method for calculating and predicting water quantity from a dynamic well field that is being actively developed. Therefore, it is important to develop a protocol for water production calculation and prediction.

2.7.2. Green completions

Recycling wastewater can reduce air emissions from trucks since new water does not need to be transported to the site. In addition, other potential spills and leakages of gas can be lowered, such as the storage tank of wastewater from which gas (methane for example) can emit into the air. EPA issued new regulations on air pollution from hydraulically fractured gas wells on Apr. 17, 2012 [50]. The new regulation requires all operations to practice "reduced emissions" or "green completions" to capture gas and other volatile organic compounds (VOCs) that are released with hydraulic fracturing flowback water. Much of the gas released during fracturing is off-gassing from the flowback water and measures need to be taken to assure it is not vented to the atmosphere.

Green completion techniques are the methods designed to minimize the released natural gas and oil vapors into the environment during the completion period of a well. The benefits of green completions include minimizing the release of greenhouse gases (such as methane) and VOCs, and maximizing the recovery of natural resources by selling the gas instead of letting it go into the atmosphere [5].

Under the new rule, estimation was made that between 190,000 and 290,000 tons of VOCs emissions and from 12,000 to 20,000 tons of benzene emissions from hydraulic fracturing equipment would be eliminated per year. In addition, between 1 million and 1.7 million tons of unrecovered methane emissions would be eliminated by this rule. The EPA announced it would delay requiring the use of green completion technology until 2015 to provide time for producers to finish the transition. Before 2015 operators will have the option of using either green completion technology or flaring gas [51].

2.8. Current research on produced water quantity

In order to treat and reuse produced water, it is important to understand how much water is produced as well as its quality. Current research has focused on the quality of produced water, since the production pattern of produced water is complicated and changes from well to well. There are many factors impacting the volume of produced water: type of well drilled, location of well within the reservoir structure, type of completion, type of water separation and treatment facilities, water flooding for enhanced oil recovery, insufficient produced water volume for water flooding, loss of mechanical integrity and subsurface communication problems [20]. Typically horizontal wells have higher water production rates than vertical wells. On average, 7 bbls of water is produced with production of one bbl of crude oil in the U.S. [52], the same result American Petroleum Institute's (API) produced water surveys found in 1985 and 1995. API had calculated the water-to-oil ratio of about 7.5 bbls of water for each bbl of oil produced, and the number increased to approximately 9.5 according to the produced water survey in 2002 conducted by API [20].

There has been very limited research on produced water decline trends. In 2011, the USGS (United States Geological Survey) conducted a study on oil, gas and water production from Wattenberg Field in Colorado. Produced water volume of one sample well decreases from 1.2 to 0.65 bbl/day over 5 years from 1990 to 1995; however the pattern of water production is not analyzed [53].

The Arps equation (Equation 2.1) [54] is generally used for calculating the production rate of oil and gas and therefore can be used as a first approximation for modeling decline rates. In the Arps equation, $q_{(t)}$ is production rate at t, q_i is initial production rate, D_i is the decline rate constant, t is time and b is the degree of curvature.

$$q_{(t)} = \frac{q_i}{(1 + D_i t)^{1/b}}$$
 2.1

In the Arps equation (Equation 2.1), b value changes from 0 to 1. When b=0, the Arps equation changes to the form of Q=Ae^{-kt} which is exponential decline, and when b=1, the equation changes to harmonic decline.

Figure 2.9 shows the different decline curves with different b values in Arps equation.

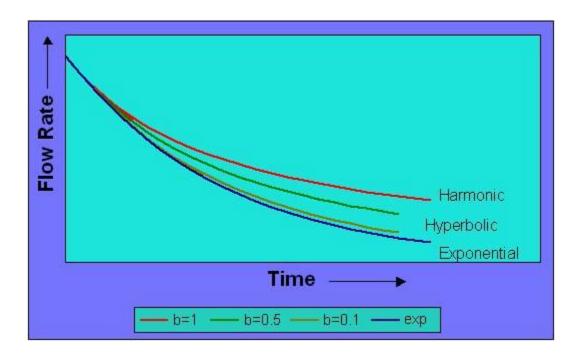


Figure 2.9. Decline curves from different b values in Arps equation [55]

2.9. Objectives and hypothesis

Previous research has focused on produced water quality and methods for treatment.

When considering reusing frac flowback and produced water, the quantity of water is also important for designing the capacity of the treatment facility. Therefore, it is necessary to study the water production trends from these wells as well as the relationships between water production and spatial location. GIS will be the best tool for understanding how water

quantity varies in different locations. At the same time, since disposal wells are still the most commonly used way to handle wastewater from oil and gas wells, it is important to be aware of how much water to expect so that truck trips to carry the water to disposal wells can be estimated.

This research focuses on fitting historical water production data from Noble Energy Inc. wells in Wattenberg field with the Arps equation, by studying the historical decline trends of water produced, and modeling prediction of water production. The research has four research objectives:

- 1. Develop protocol for predicting produced water production from vertical wells
- Develop protocol for predicting frac flowback and produced water production from horizontal wells
- 3. Create Excel tool for predicting total water production for Wattenberg field
- 4. Complete case studies of tool application in three different well fields.

Chapter 3. Development of protocols and tools for predicting frac flowback and produced water volume from Wattenberg oil and gas field

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Abstract

The objective of this study was to develop protocols and interactive tools that could be used to predict frac flowback and produced water volumes considering the unique decline rates that exist for different types of oil and gas wells. Specifically, water production data from the Colorado Oil and Gas Conservation Commission (COGCC) and Noble Energy Inc. were used to develop protocols for modeling water production for vertical and horizontal wells, a distinction made largely due to the different amounts of water used for each. If centralized water treatment and handling facilities are going to be designed and constructed, it is important to have a reliable estimate of the water that will be produced in the future as wells are completed and brought on line. An Excel-based tool was developed utilizing the horizontal and vertical well protocols for predicting total volume of water production by current and future wells in Wattenberg Field.

Two case studies have been conducted including one with all of the Noble wells in Wattenberg Field and one with a subset assuming a regional treatment center might be established.

Uncertainty of the predictions was determined using standard error calculations on the two

modeling parameters for water flow decline rates. An interactive Excel-based spreadsheet has been developed to allow predictions of water production based on the number of horizontal and

vertical wells drilled in the future.

Research highlights:

Two protocols were developed for predicting water production from vertical and

horizontal oil and gas wells.

An Excel-based tool was created that utilizes the two protocols to predict total water

production in Wattenberg field.

• Uncertainty of predictions was estimated by determining the 95% confidence limits of

two parameters used for decline rate modeling.

• Two cases studies were conducted using the Excel-based tool to predict flowback and

produced water.

Keywords: Oil and Gas Wells, Frac Flowback, Produced Water, Wattenberg Field

Introduction 3.1.

By the end of 2010, the proven reserves of crude oil in the U.S. were 19.1 billion barrels

[56], and the natural gas reserves were estimated to be greater than 300 trillion cubic feet

[57]. Since more than 60% of US energy is supplied by oil and gas, it is likely that the

number of wells drilled over the next few decades will continue to increase as a result of

increased energy demand [2]. In the oil and gas industry, water is a major concern, not only

because of its demand in drilling and hydraulic fracturing, but also because of the water

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produced from oil and gas wells. Drilling and hydraulically fracturing a horizontal shale well requires an average of 3 to 6 million gallons of water [31] and in the Wattenberg field in northern Colorado, each vertical and horizontal well uses an average of 0.39 million and 2.8 million gallons of water respectively [6, 34]. Increased water demand for the oil and gas industry may stress already scarce water supplies in Colorado. However, after the completion of a well, a large amount of water, known as frac flowback and produced water returns with the extracted oil and gas. This water has higher total dissolved solids (TDS) and lower water quality than fresh water [35, 58] and can be difficult to handle and treat. Water pollution from frac flowback and produced water has drawn attention recently and will likely continue to be a controversial topic in the future. One of the best strategies to mitigate the water related risks in the oil and gas industry is to recycle and reuse water. Therefore it is important to understand how much water is being produced and what the quality of that water is so that the appropriate treatment processes can be chosen for reusing and recycling the water [59, 60].

Nomenclature

- Q Water flow rate (bbl/year)
- t Well age (year)
- *k* Vertical well water production decay rate (year⁻¹)
- *k*₁ Horizontal well frac flowback production decay rate (year⁻¹)
- *a* Horizontal well produced water production decay rate (year⁻¹)
- A Vertical well initial water flow rate (bbl/year)
- A₁ Horizontal well initial frac flowback flow rate (bbl/year)
- C Horizontal well initial produced water flow rate (bbl/year)

3.2. Methods and materials

3.2.1. Site location and description

The Wattenberg field is an unconventional shale play located northeast of Denver, Colorado. With an estimated 195.3 billion cubic feet reserve of wet natural gas in 2009, the Wattenberg field is ranked as the 10th largest natural gas field in the United States [24]. Additionally, some estimates have predicted that Wattenberg field could yield as much as 1 to 2 billion barrels of oil equivalent, comprised of 70% oil and 30% natural gas [61]. Lying in the Denver-Julesburg Basin, the Wattenberg field has five formations: J Sandstone, Codell Sandstone, Niobrara Formation, Hygiene Sandstone and Terry Sandstone [62]. By August 2011, there were over 18,000 active wells in Wattenberg field with approximately 7,700 operated by Noble Energy [63]. Figure 3.1 shows the locations of Noble wells in Wattenberg field in Colorado.

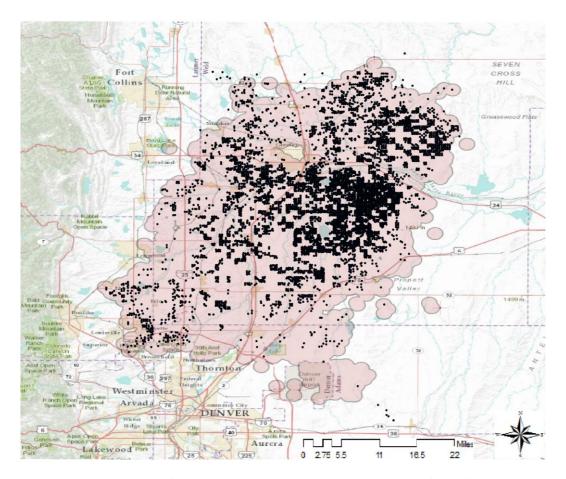


Figure 3.1. Location of Noble oil and gas wells in the Wattenberg field of Colorado

3.2.2. Methods and data collection

Based on the different types of oil and gas wells, separate methods of analysis were performed to study life-cycle water production trends of vertical and horizontal wells.

a. Methods and data collection for vertical oil and gas wells

For vertical wells, annual water production data for a sample of 1,677 Noble Energy wells from 1999 to 2011 was obtained from the Colorado Oil and Gas Conservation Commission (COGCC) database. According to the dates of completion and first production, new wells in each year were selected for this study as shown in Table 3.1.

The selected wells were then classified according to well age to study the water production trend for 13 years. This subset of Noble Energy wells was used to make water production predictions for the 30 year life-cycle of vertical wells in the Wattenberg field, a timeframe that was chosen to represent the maximum well life.

Table 3.1. New wells from 1999 to 2011 and number of wells in each operating year

Year	New wells	Years in Operation	Number of wells	
1999	6 1		1677	
2000	10	2	1494	
2001	29	3	1324	
2002	28	4	1140	
2003	65	5	807	
2004	105	6	535	
2005	131	7	374	
2006	161	8	243	
2007	227	9	138	
2008	333	10	73	
2009	184	11	45	
2010	170	12	16	
2011	183	13	6	

b. Methods and data collection for horizontal oil and gas wells

Since the drilling of horizontal wells is relatively new (first started in 2010 in Wattenberg) and since there are currently only approximately 200 horizontal wells for Noble Energy in the Wattenberg field, a sample of 32 Noble Energy horizontal wells were studied. Daily frac flowback and produced water data were acquired from Noble Energy. Based on the existing frac flowback and produced water data, predictions of water production for the 30 year lifecycle of horizontal wells in the Wattenberg field were made.

3.3. Data analysis and protocol

3.3.1. Protocol for vertical well predictions of produced water

The protocol for vertical wells is based on both frac flowback and produced water data. Total water production in each operating year was summed for the chosen subset of vertical wells and the average number of producing days in each operating year was calculated based on the distribution of existing Noble Energy data (Table 3.2). Average daily water production per well was computed from operating years 1 to 13 and annual water production was calculated by multiplying average daily water production with the average number of producing days. High water flow rates were observed in the first year of operation because of the intrinsic frac flowback period (typically 1 to 2 days of high volume water production) included in that year. Based on the results of these calculations, predictions of water production for future years were made to an assumed well life-cycle of 30 years.

Table 3.2. Distribution of producing days for each operating year

Operating Year	Average Producing Days		
1	162		
2	337		
3	339		
4	342		
5	342		
6	348		
7	354		
8	346		
9	350		
10	339		
11	322		
12	339		
13	333		

For the first operating year, all wells were not started at the beginning of the year; hence the average production period is 162 days (less than half of the production days in the following years). Based on the existing 13 years of water production data, an exponential decline curve was applied to the water production trend for predicting future water generation ($Q=Ae^{-kt}$). An exponential decline curve was chosen for this subset of wells because it best fits the behavior of vertical water production in the Wattenberg field. However, some fields with more connate water will have a different best-fit curve. The type of curve chosen as a foundation may change, but the protocol should yield a consistent outcome. Based on the average value of A and k (rate constant) from all 1,677 vertical wells (Appendix A, Table A.1), and the days of production from Table 3.2, the equation of water production rate is:

$$Q=1.981e^{-0.1614t} (R^2=0.5336) (1)$$

Equation 1 shows the average water production rate from vertical wells in Wattenberg Field. However, from the water production data, it is known that the water production varies throughout the Wattenberg field. In order to understand the relationship between the spatial location of wells and the decay rate constant, an ArcGIS map was interpolated based on the decay rate constant (k value) of each vertical well as shown in Figure 3.2. Based on the interpolated GIS map of k values shown in Figure 3.2, the average k value for a selected subset of the Wattenberg field can be calculated in ArcGIS. An example of using ArcGIS to calculate average k value for a particular case study is described later in the paper.

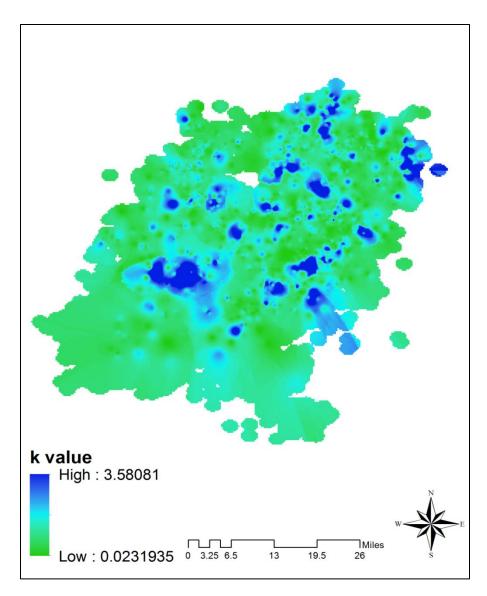


Figure 3.2. Interpolated *k* values of Noble Energy vertical oil and gas wells in Wattenberg field In Figure 3.2, the *k* (decay rate) of water production from vertical wells varies from 0.023 (half-life of 30.14 years) in the southwest to 3.58 (half-life of 0.19 years) in the northeast of the Wattenberg field. The reason for the large variation in *k* or half-life may be due to geologic formation differences that can be studied in the future. Additionally, the newer a well is, the less water production data are available. This may lead to a higher *k* and shorter half-life prediction. It is also observed that the *k* value is not homogeneous, as shown by the dark blue pockets in light green areas. Therefore, to adequately determine the proper *k* value,

a spatial area must be defined. In Equation 1, the k value was defined as the average k across the 1,677 vertical wells.

3.3.2. Protocol for horizontal well predictions of frac flowback and produced water

Unlike vertical wells, horizontal wells use more water for drilling and fracturing, while having longer frac flowback periods that last up to two months. The protocol for horizontal wells is based on both frac flowback and produced water data. However, since there are only about 200 horizontal wells in the Wattenberg field, all of which were completed after 2010, a sample of 32 horizontal wells from Noble Energy was chosen for the estimation of water production rates.

When production data are plotted by years in operation, it is seen that the water production decline rate is different for frac flowback and produced water. Therefore distinct rate models need to be developed. To distinguish flowback from produced water, two methods of analysis were performed on the data of the 32 horizontal wells. Raw data analysis uses the flowback report from Noble Energy as the flowback period and the day after the period as the first day of produced water generation. Another approach, the modified data analysis, uses the intersection point of first order decay trend lines of flowback and produced water curves as the first day of produced water generation. Both methods can be seen in Figure 3.3.

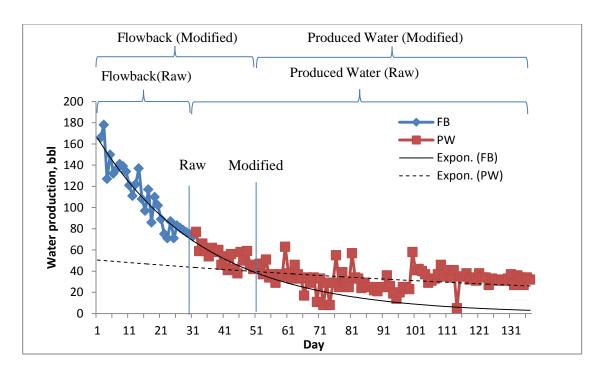


Figure 3.3. Comparison of two methods (raw and modified data analysis) of example horizontal well 70 Ranch BB21-65HN

Using the raw data analysis, it was found that the average flowback time for a horizontal well was 27 days. However, it was also found that the average horizontal well did not produce until the 74th day. This can be due to waiting for production equipment, waiting for midstream infrastructure, or waiting for other wells on the pad to be completed. Hence, a total flowback time is defined as the time after a well is completed till just before a well produces and the flowback period for the average horizontal well in Wattenberg is assumed to be 74 days from the raw data analysis. And from the modified analysis the average frac flowback period for horizontal wells in Wattenberg field is assumed to be 61 days. After analyzing the frac flowback and produced water production curves for the 32 wells based on the modified analysis method, the average curve was plotted and a prediction of future water production was made. For frac flowback water, exponential decay function was used to calculate the water production rate. Based on the average A_1 and A_1 for all 32 horizontal wells, the equation of frac flowback water production for horizontal wells in the first 61 days is:

$$Q=264.4e^{-0.043t} (R^2=0.7869) (2)$$

However for produced water, production rate was modeled with harmonic function for peak flow condition. The equation of harmonic decay is: $Q = \frac{C}{1+at}$, in which C is the initial water production rate and a is the initial decay rate. After applying harmonic function to each horizontal well, the average C and a value of 32 wells was calculated and the equation of produced water production for horizontal wells is:

$$Q = \frac{88.8638}{1 + 0.04469t} \qquad (R^2 = 0.7379) \tag{3}$$

The average number of production days in each operating year used in the analysis is the same as the vertical wells, and for the 162 days in the first operating year, there are assumed to be 61 days of frac flowback and 101 days of produced water production.

Again, ArcGIS interpolated maps are used to estimate the spatially-defined k_1 value (frac flowback decay rate constant) in Equation 2 and a value (produced water decay rate constant) in Equation 3. Figure 3.4 shows how k_1 and a for horizontal wells differ spatially throughout the Wattenberg field. Like the decay rate of vertical wells (k), the distribution of k_1 and a are not homogeneous. Therefore, in the analysis of all horizontal wells in the Wattenberg field, an average k_1 value of 0.043 (half-life of 16.12 days) and average a value of 0.04469 (half-life of 15.51 years) was used. The average is depicted in Equations 2 and 3.

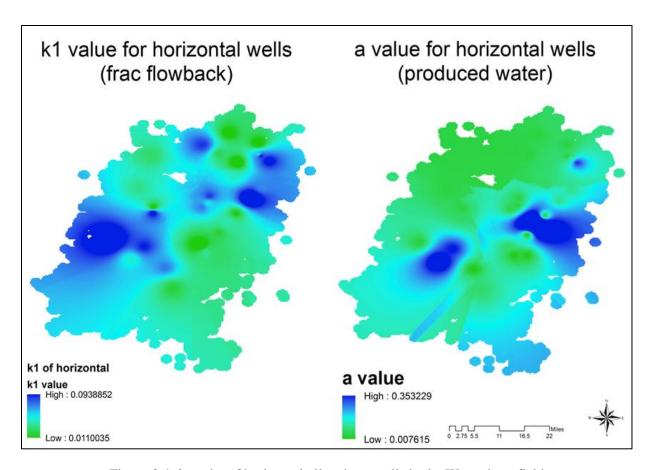


Figure 3.4. k_1 and a of horizontal oil and gas wells in the Wattenberg field

Based on Equation 1, 2 and 3, averaged water production curves of horizontal and vertical wells in the Wattenberg field are shown in Figure 3.5. With more fracturing water use and longer frac flowback time, horizontal wells have higher water production rate than vertical wells. Also shown in Figure 3.5, horizontal wells have faster decay in the first year of operation because of the large volume of frac flowback generated in the first year.

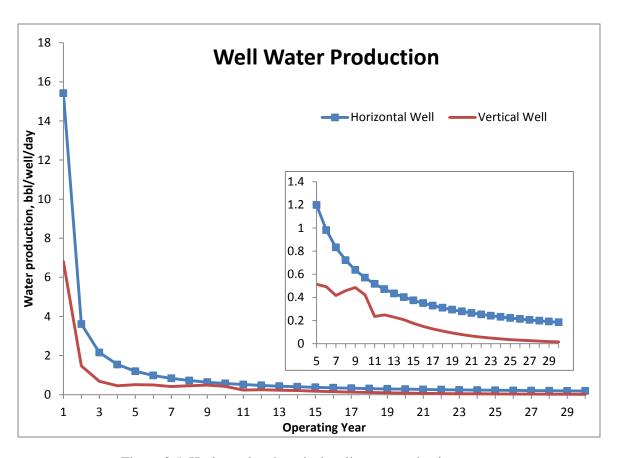


Figure 3.5. Horizontal and vertical well water production curves

3.4. Development of Excel-based tool for predicting frac flowback and produced water volumes from the Wattenberg oil and gas field

3.4.1. Introduction of the tool

After combining the protocols of vertical and horizontal wells, an Excel-based tool was developed to predict frac flowback and produced water volumes for existing wells in the Wattenberg field. This was achieved through the development of the water production curves, based on current well counts and historical production data. As seen from the Wattenberg vertical and horizontal well models, water production prediction models can be fitted with a single curve or with multiple curves

The developed Excel-based tool can also be used to predict water production for future proposed development from given oil and gas field (or other spatially defined area) based on the historical data. In order to perform the calculation, the required historical data includes the number of existing wells, the type of these wells, and the associated production dates and volumes in the given area so that the years of operation of each well can be determined. Once curves are developed from existing wells in the area, the models can be applied to future annual drilling and fracturing in terms of yearly wells planned.

Prediction of total water production in future years is calculated after inputting the planned new wells and their types for each year, and by summing water produced from both existing wells and proposed wells.

Inputs and outputs of the tool

The tool, based on the model developed with spatially-relevant historical data, has two major inputs: the number of new vertical wells and the number of new horizontal wells for each future year. Because the water production rate changes with the length of wellbore, and all historical Noble wells were relatively homogeneous with the length of 4,500 feet, new wells are all considered as or equivalent to 4,500 feet long. The output of the tool is the predicted water production in each future year for the defined area. Figure 3.6 shows the screen shot of the Excel tool (Available on the CEWC (Colorado Energy Water Consortium) website).

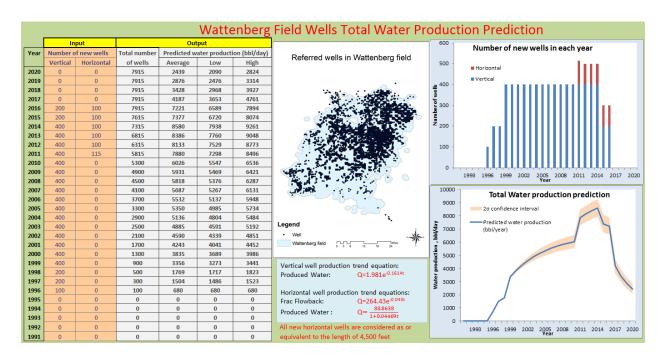


Figure 3.6. Screen shot of the Excel tool with inputs and outputs

Method of prediction

From the described protocols, using historical water production data, area-specific water production equations can be determined. These equations can be used to model the future water production of existing wells. Additionally, the equations can be used to forecast water production for future, proposed wells within the defined boundaries. By default, a prediction of water produced from existing wells is made based on no new wells in future years. However, the effect of future wells on water production can be determined by inputting the planned number of each type of new wells into the developed tool.

In Figure 3.6, the tool depicts a Wattenberg-wide water prediction analysis where historical well counts for each year and associated water production were obtained from COGCC (pre 2009) and Noble Energy (after 2010). Example future well development was input for years of 2012 through 2014 to include 200 new vertical wells and 100 new horizontal wells annually in the defined area. These future development plans do not reflect Noble Energy's true well development forecasts for the Wattenberg field. Figure 3.7 shows how future water production is affected by existing wells and proposed wells. It is seen that water production will continue to increase along with well development but after drilling stops, water production starts to drop. Additionally, Figure 3.7 depicts the default prediction of the tool where no new wells are drilled and completed. In this example, water production drops off drastically in the first few years and then settles into a gentler decay.

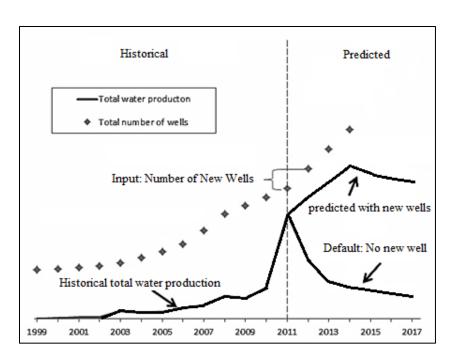


Figure 3.7. Description of method for predicting future total water production Assumptions

Due to the complexity of the historical data, several assumptions were made during the development of the tool:

- a. Though there are more than 7,000 Noble Energy vertical wells in Wattenberg field, only 1,677 vertical wells have available timeline information such as drilling dates and first production dates. Therefore, these 1,677 wells were chosen as a subset to develop the water production curves. This subset will affect assumptions drawn about field-wide production curves.
- b. Water production changes with the length of wellbore, since all historical wells from Noble have been relatively homogeneous with the wellbore length of 4,500 feet, all new wells are considered equivalent to 4,500 feet long.

- c. When a well is plugged and abandoned, it is assumed to have been operated for greater than 10 years so that it produced very little water. Additionally, only around 10 to 20 wells are plugged and abandoned in each year. Hence, the impact from plugged and abandoned wells on total water production in that year was assumed negligible.
- d. Refractured wells are considered to behave similar to newly completed wells.
 This assumption will be verified in future work.
- e. Future wells are assumed to behave the same as historical wells.

3.4.2. Uncertainty analysis

Water production trends of vertical wells, as well as frac flowback water production trends of horizontal wells in the Wattenberg field, were all fitted with an exponential decay function of the form $Q=A \cdot e^{-kt}$ and produced water production trends of horizontal wells were fitted with a harmonic decay function of the form $Q=\frac{C}{1+at}$. For the developed tool, average values of A, k, C and a for all Wattenberg field wells studied were used. However, Figures 3.2 and 3.5 both show significant variability in k, k_I , and a. Another variables, A and C, also will have variability from well to well. Therefore, uncertainty analyses were performed for all parameters.

For all 1,677 vertical wells, the water production decline trend for each well was analyzed and fitted to an exponential decay function. Since 438 of the vertical wells had limited water production data and another 113 wells did not fit the decay function, only 1,126 k values were used in the uncertainty analysis. A smaller subset of 153 wells was chosen randomly for evaluation of k variability. The normal distribution of k and k is shown in Figure 3.8.

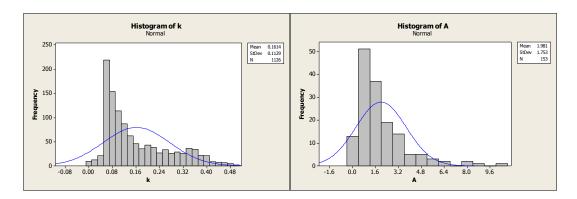


Figure 3.8. Distribution of *k* and *A* for vertical wells

Since horizontal wells in the Wattenberg field are modeled by two separate functions for flowback and produced water, four variables (A_1 and k_1 for flowback and C and a for produced water) were analyzed for uncertainty using the same statistical method. Figure 3.9 shows the distribution of k_1 , A_I , C and a values of horizontal wells.

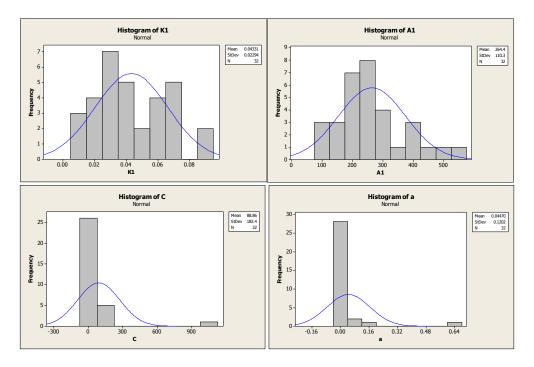


Figure 3.9. Distribution of k_1 , A_1 , C and a for horizontal wells

Assuming the parameter values for both vertical and horizontal wells are normally distributed, the z score for 95% confidence interval is 1.645 and the calculated statistical values are shown in Table 3.3.

Table 3.3. Uncertainty analysis and acceptable range of variables

	k	\boldsymbol{A}	k_1	A_1	С	a
μ	0.1613	1.981	0.0434	264.4	88.8638	0.0447
σ	0.0033	0.141	0.0040	19.4	32.4282	0.0212
μ-1.645σ	0.1558	1.748	0.0366	232.3	35.5194	0.0098
μ +1.645 σ	0.1669	2.214	0.0499	296.5	142.208	0.0796

3.5. Case study of Noble wells in Wattenberg field

A case study to estimate total water production for all Noble Energy wells from 2012 to 2017 in Wattenberg field was conducted using the developed Excel-based tool. Historical total water production and well count data was acquired for all Noble wells in Wattenberg Field each year from 1999 to 2011. Data from 1999 to 2009 were extracted from the COGCC website database, and the data for 2010 and 2011 was taken directly from the Noble Energy Carte® database.

By the end of 2011, a total of 7,486 wells from Noble Energy were producing in the Wattenberg field. Overall, there were 7,371 vertical wells and 115 horizontal wells. Each of these wells was modeled with the appropriate Wattenberg-average decay functions (Equations 1, 2, and 3) and their specific well age. All water production from existing wells in the Wattenberg field was projected out to 2017.

After applying the tool to all existing wells in the Wattenberg field, a development assumption was made where 100 new horizontal wells and 200 new vertical wells would be drilled and completed each year from 2012 to 2017. For each of these proposed wells, the appropriate water production model was also applied using the tool. This assumption of well development is used to demonstrate the planning capabilities of the tool if a company would like to know how their new well plans will affect future water production.

The additive predicted volume of water production from both existing and proposed wells from 2012 to 2017 is shown in Figure 3.10. Additionally, the case where no new wells are drilled is shown in Figure 3.10. Finally, the 95% confidence interval for both cases is also shown in Figure 3.10. The 95% or 2σ confidence interval is calculated using values from Table 3.3. For the high limit of the 95% confidence interval, the biggest A and smallest k value was used in the calculation. This means the water production curve has the biggest initial flow rate and slowest decay rate. For the lower limit of the 95% confidence interval, the smallest A and biggest k value was used in the model.

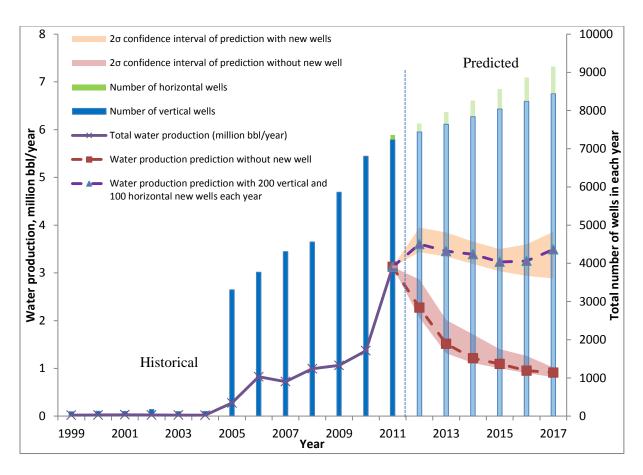


Figure 3.10. Total water production prediction of all Noble wells in the Wattenberg field from 2012 to 2017

From Figure 3.10, a few observations can be drawn. A large jump in water production is seen in 2010. This is due to the introduction of horizontal wells. From the prediction made by the tool, it is also clear that water production will decrease from 2012 to 2015. From 2016 to 2017 the total water production increases again to around 3.5 million bbls. Though there are new wells being drilled each year from 2012 to 2015, total water production in Wattenberg field actually decreased due to the large number of new wells from 2009 to 2011. This shows that from 2012 to 2015, total water production in the Wattenberg field is strongly affected by the wells drilled in 2010 and 2011 (total of 1,415 vertical and 115 horizontal) rather than the new wells from 2012 to 2015 (200 vertical and 100 horizontal each year). Total water production increases again in 2016 and 2017 when new wells in each year provide greater

influence than the existing wells. If no new wells are drilled, water production is seen to drop from approximately 3 million bbls in 2011 to about 1 million bbls in 2017. This is expected since without new wells, the water production trend would revert to the produced water rate after 2011, as seen in Figure 3.5.

3.6. Case study of selected Noble wells in northeast Wattenberg field

In the previous case study estimating water production for all 7,486 Noble wells in the Wattenberg field, the k values for both vertical and horizontal wells were average values for the whole field. However, according to Figures 3.2 and 3.5, k values vary spatially throughout the Wattenberg field. To make a more precise water production prediction, a smaller area can be chosen where the k value is more tailored. Therefore in order to understand the water produced in a smaller geographic area, a case study of selected wells in the northeast Wattenberg field was conducted using both the predictive k value tool in ArcGIS and the estimated water production tool in Excel. The selection of wells is shown in Figure 3.11.

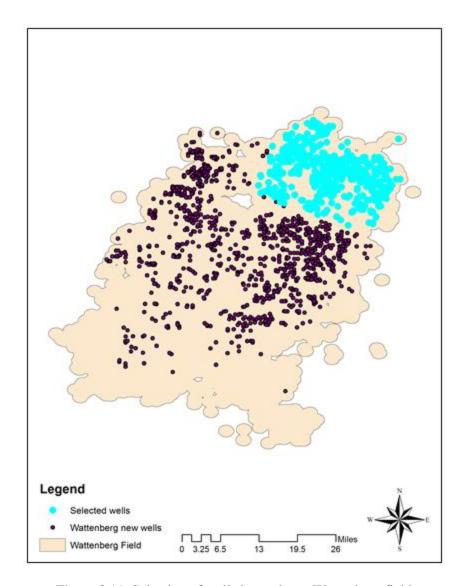


Figure 3.11. Selection of wells in northeast Wattenberg field

From the GIS attribute table of the selected region, 568 vertical and 12 horizontal wells were analyzed, and the average k values for both types of wells were computed in ArcGIS, as shown in Figure 3.12 and Figure 3.13.

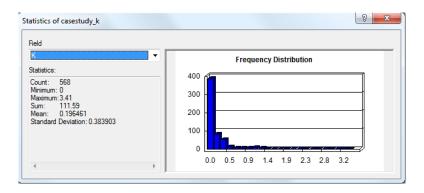


Figure 3.12. Distribution of k value of selected vertical wells in ArcGIS

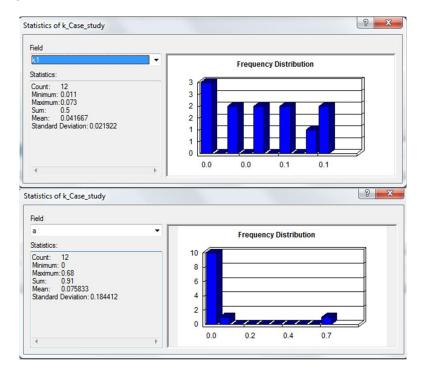


Figure 3.13. Distribution of k_1 and a values of selected horizontal wells in ArcGIS

After applying the computed, spatially relevant k, k_1 and a into Equations 1, 2, and 3, the water production functions for wells in the selected area of the Wattenberg field were modified from the averaged equations. And for the selected wells, the average value of A, A_1 and C was 2.003, 259.9 and 142.995 respectively. As a result, the equation for predicting vertical well water production for the selected area is:

$$Q=2.003e^{-0.197t}$$
 (R²=0.8073) (4)

The equation for predicting horizontal well frac flowback water production for the selected area is:

$$Q=259.9e^{-0.042t}$$
 (R²=0.7849) (5)

The equation for horizontal well produced water production for the selected area is:

$$Q = \frac{142.995}{1 + 0.07583t} \qquad (R^2 = 0.8022) \tag{6}$$

Water production for selected vertical and horizontal wells was calculated using the Excel-based tool. Figure 3.14 and Figure 3.15 show the comparison of water production trends for both vertical and horizontal wells between Wattenberg field-average k value and area-specific k values from selected wells in northeast Wattenberg Field.

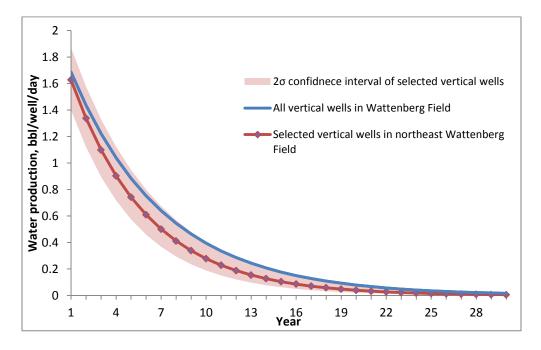


Figure 3.14. Comparison of water production trends between all vertical wells and selected vertical wells in northeast Wattenberg Field

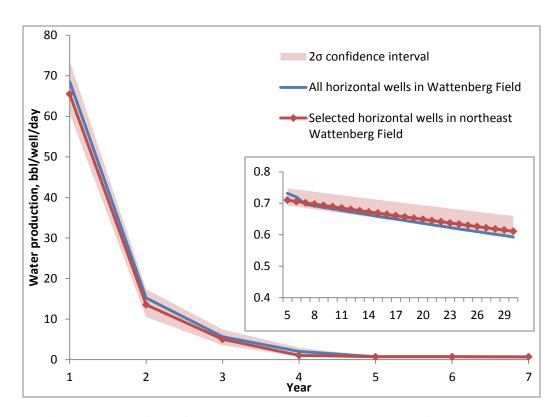


Fig. 3.15. Comparison of water production trends between all horizontal wells and selected horizontal wells in northeast Wattenberg field

In this case study, the difference in k, k_1 , and a values for a chosen subset area (northeast part) of the Wattenberg field is compared to the entire field model. Different k, k_1 , and a values result in different equations for both vertical and horizontal wells when predicting the water production. As shown in Figures 3.14 and 3.15, the model used for predictions of the well subset is different from the one of the whole Wattenberg field. It may be more accurate at predicting subset water production than applying the field-wide model. This case study shows the value of applying ArcGIS with the Excel tool to predict water production based on spatial locations.

3.7. Conclusion

Water usage in oil and gas development has been discussed at great length. However, it is known that oil and gas wells have the potential to produce and return water to the hydrologic cycle. Understanding these return flows is essential to understanding the complete water cycle associated with oil and gas development. Additionally, understanding these return flows can aid in treatment efforts that bring produced water back to beneficial uses.

This paper describes a simple tool for predicting total water production from existing and future oil and gas wells. While the tool is developed for the Wattenberg field in this paper, the case study of northeast Wattenberg demonstrates the tool's ability to be tailored to other areas by altering the functions. In the case of the Wattenberg field, the curves chosen are a first order decay function. It was determined that a single first order decay function was sufficient at modeling vertical well water production and two separate decay functions were required for predicting flowback and produced water from horizontal wells. Additionally, it was observed that decay rates vary drastically over a given area. Hence, to accurately forecast water production, a keen knowledge of historical decay rates and a defined project boundary are required.

From the first case study of all Noble wells in the Wattenberg field, it is clear that an increased total volume of produced water should be expected in the future with the expanded reliance on horizontal wells. Additionally, it is seen how proposed future development affects water production. As industry moves toward greater reliance on horizontal wells, water production will increase. From the second case study of the northeast Wattenberg field, it is seen that a tighter boundary can positively affect the accuracy of the decay rate. Therefore, choosing smaller project areas will increase the accuracy of the water production forecast.

While work can be done to minimize the effects of assumptions and historical data can be improved, ArcGIS and Excel tools can be built with models based on historical data to predict future water production for existing and proposed oil and gas wells. This knowledge of how current and future oil and gas development will affect water production in a field can be used to aid in decision making surrounding water treatment, disposal, transportation, and the efficacy of pursuing development in a given field.

Chapter 4. Case study on wells in Wells Ranch region, Wattenberg

4.1. Water production prediction of wells in Wells Ranch region

Another case study was performed in the Wells Ranch Region in northeast Wattenberg Field. Figure 4.1 shows the location and the studied wells in the Wells Ranch play in Wattenberg Field. A centralized water supply and wastewater treatment facility was considered to be built, and according to the database of Noble Energy, there are 283 vertical wells and 28 horizontal wells in this area. These wells were classified according to the year of the flowback report and Table 4.1 shows the number of new wells in each year.

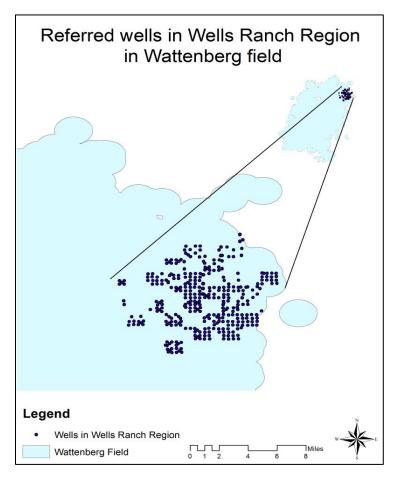


Figure 4.1: Location of wells ranch region and referred wells in Wattenberg Field

Table 4.1: Number of new wells in each year in Wells Ranch Region

Year	New vertical well	New horizontal well
2007	14	0
2008	83	0
2009	60	0
2010	37	5
2011	26	6
2012	63	17

Daily water production for each of these 311 wells was obtained from Noble Energy and due to the limited data for horizontal wells, only 15 flowback reports for horizontal wells were available from Noble Energy. Water production trends for vertical and horizontal wells were modeled all with exponential decay function.

In order to calculate the water production rate for these wells, production curves were made for each of these wells. Because among the 283 vertical wells, 61 wells have only one year of production data, data from 222 vertical wells were fitted to an exponential decline curve in water production and their *A* and *k* values were used to determine the vertical wells production rate. For the 15 horizontal wells with sufficient data sets, both frac flowback and produced water production curves were plotted.

Based on the average *A* and *k* values from 222 vertical wells, the water production rate for vertical wells in the Wells Ranch region is:

$$Q=5.189e^{-0.2747t} (R^2=0.8356) (7)$$

And based on the average A_1 , A_2 , k_1 and k_2 values from 15 horizontal wells, frac flowback water production rate for horizontal wells in this region is:

$$Q=1773.45e^{-0.1946t}$$
 (R²=0.7236) (8)

And the produced water flow rate for horizontal wells in this region is:

$$Q=0.6731e^{-0.0082t}$$
 (R²=0.8418) (9)

In Eq. (7), (8) and (9), the average value of A, k, A_1 , k_1 , A_2 and k_2 were used for the prediction of water production. In order to understand the reliability of these equations, an uncertainty analysis for these wells was performed. Figure 4.2 and 4.3 show the normal distribution of these variables.

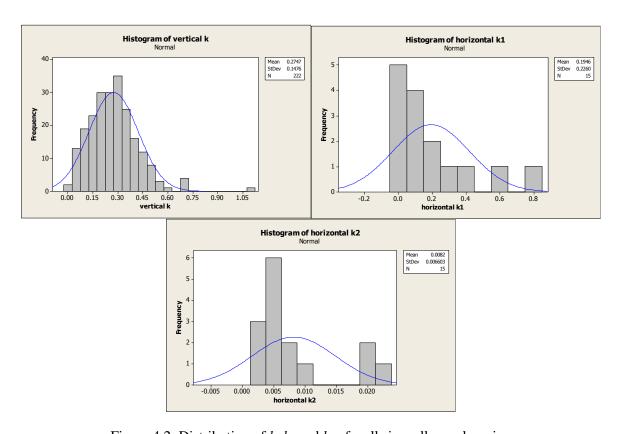


Figure 4.2: Distribution of k, k_1 and k_2 of wells in wells ranch region

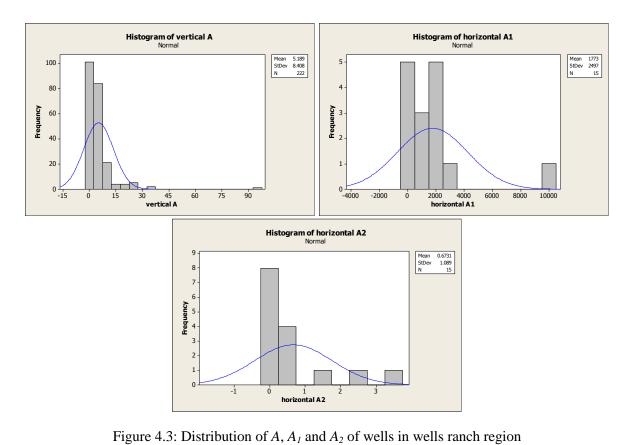


Figure 4.4 shows a comparison of k values from all vertical wells (A) and 222 Wells Ranch vertical wells (B). Better resolution of k values is seen in the map B because more k values were used in map B compared to map A with only 66 k values.

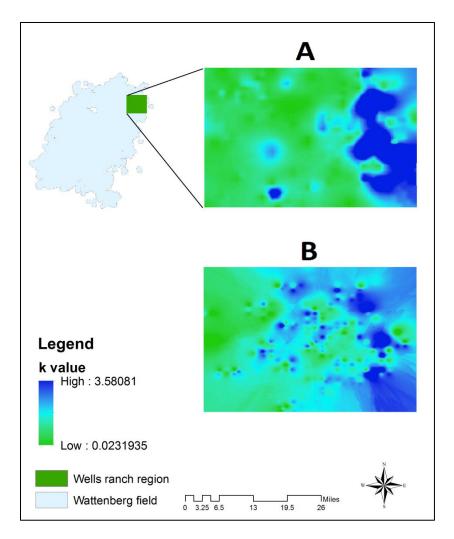


Figure 4.4: (A) Map of *k* values interpolated from 1,667 vertical wells in Wattenberg field (B) Map of *k* values interpolated from 222 wells ranch vertical wells

Table 4.2: Uncertainty analysis and acceptable range of variables

	k	\boldsymbol{A}	k_1	A_{I}	k_2	A_2
μ	0.2747	5.189	0.1946	1773.45	0.0082	0.6731
σ	0.0099	0.564	0.0584	644.65	0.0017	0.2811
μ-1.645σ	0.258	4.261	0.099	713.001	0.005	0.211
μ+1.645σ	0.291	6.117	0.291	2833.9	0.011	1.136

Figure 4.5 and 4.6 show the production trends of vertical and horizontal well with 95% confidence intervals.

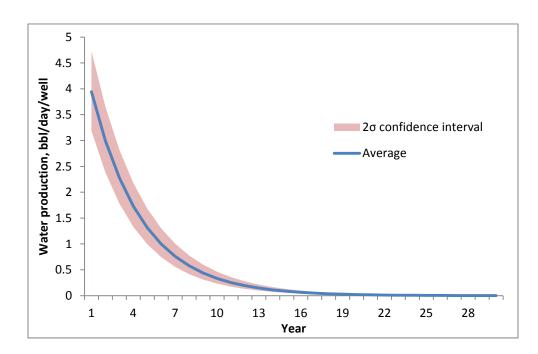


Figure 4.5. Water production trend of vertical well in wells ranch region

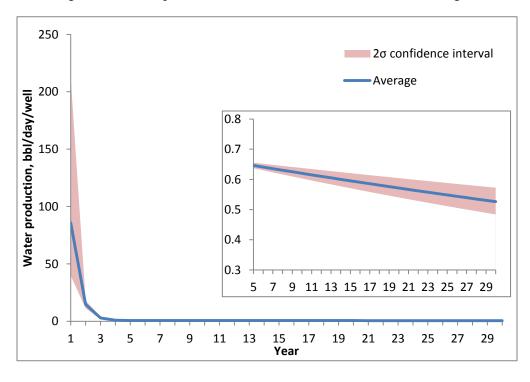


Figure 4.6. Water production trend of horizontal well in wells ranch region

Compared to the case study conducted in chapter 3 with selected wells in northeast Wattenberg field, this case study is more specific and focused on the Wells Ranch area, where Noble Energy is planning future development. This specific case study provides more precise water production trends of wells in Wells Ranch region compared to the results from average values of Wattenberg field. When predicting future water production in this region, more accurate computation will be available by using the Equations (7), (8) and (9).

Figure 4.7 shows the predicted water production from all wells in the Wells Ranch area with 50 vertical and 30 horizontal new wells drilled each year from 2012 to 2017. The assumption of well development is used to demonstrate the planning capabilities of the tool if a user would like to know how their new well plans will affect future water production.

Because it is assumed that 30 new horizontal wells are drilled in 2012 compared to 6 in 2011, the water production increases rapidly. And since the number of new wells after 2012 stays constant, the predicted water production increases more consistently. On the other hand, if there are no new wells drilled after 2011, water production drops quickly from 400,000 to 70,000 bbl/year.

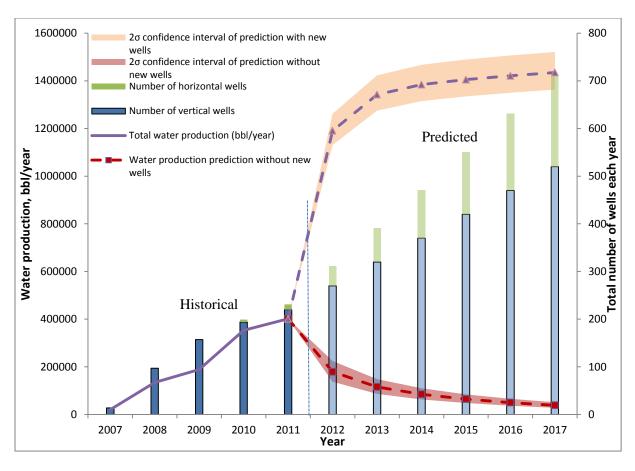


Figure 4.7. Total water production prediction of all wells in Wells Ranch Region from 2012 to 2017

4.2. Comparison of exponential and harmonic functions

In chapter 3 and 4, production of horizontal wells was fitted with exponential decline curves, however it may underestimate the volume of produced water since the exponential function is a form of Arps equation when b=0. When designing wastewater treatment facilities, it is essential to know the peak flow rate and in this case, exponential decline may not be the best function for predicting water production. Therefore, a comparison of exponential and harmonic functions was conducted on production predictions in the Wells Ranch area.

When b=1, the Arps equation is referred to as a harmonic decline with the equation of $=\frac{c}{1+at}$. After fitting the produced water data of 15 Wells Ranch wells with harmonic decline, the produced water production trend is:

$$Q = \frac{97.307}{1 + 0.022t} \qquad (R^2 = 0.7273) \tag{10}$$

The comparison of exponential and harmonic functions is shown in Figure 4.8. When using an exponential function, the water production rate decays quickly from 85 bbl/day/well in the first year to 2.9 bbl/day/well in the third year. For the same decline rate constant (Di), the production rate decreases from 69 to 52 in the first three years assuming a harmonic function. Therefore the exponential function is considered as the aggressive decline and the harmonic function is considered as the conservative decline.

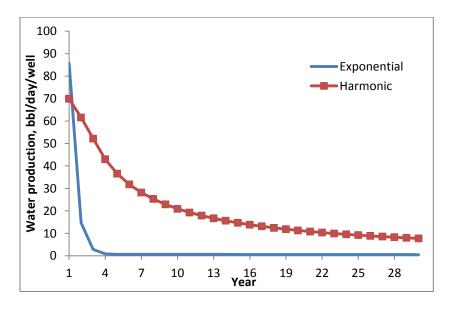


Figure 4.8. Comparison of exponential and harmonic decline of produced water production from 15 horizontal wells in Wells Ranch region in Wattenberg field, Colorado

Figure 4.8 shows a huge difference in water production between two different functions, and because the initial flow rates were different from two functions, the two water production curves in Figure 4.8 don't start from the same point. As a result, produced water flow rate

varies a lot with different fitting functions. Because there is only one year of data available for these 15 horizontal wells, it is not possible to determine the true long term decline trend and therefore an assumption needs to be made. In this case, it is recommended that wastewater treatment facilities be designed based on conservative decline assumptions and therefore it is recommended that a harmonic function be used.

Chapter 5. Conclusions

A study of water production from oil and gas wells in Wattenberg field was performed and Arps equation can be used for modeling produced water flow rate for both vertical and horizontal well. In this study, the water production rate was modeled with exponential decline which has the most aggressive decay when b=0 in the Arps equation. Limitations of the approach occurred because of the limited production data of horizontal wells and the use of average k values, even though there is considerable spatial variability as shown in Figure 3.2 and 3.4. The case study on Wells Ranch wells showed significant difference in the water production rate between exponential (b=0) and harmonic (b=1) functions, indicating that the exponential function may not be the best approach for predicting produced water production because it may underestimate the volume of produced water.

This study described a framework which can be used when trying to understand water production trends from oil and gas wells. In the future, more data will be collected and Arps equations with various b values will be studied to find out the best fitting function for water production. At the same time, in order to better understand the relationship between k values and spatial locations, a web based, user friendly GIS application will be developed using ArcGIS so that the prediction can be made based on the chosen area rather than the average value from the entire field. Finally water quality data will also be integrated into the application so it can provide a reference for users to design treatment facilities for water recycling.

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Appendix A. Method details

A.1. Vertical well water production data collection and analysis

There are two major sources for historical water production data of oil and gas wells in Wattenberg field. COGCC has yearly reports of all producing wells in each year in Colorado State, including oil, gas and water production data. Due to the limited access to all information of these wells, a sample of 1,677 vertical and 32 horizontal wells is chosen. Several filtration methods were applied to the COGCC reports to select the sample: All sample wells should be in Wattenberg field, and have all information including completion date, first production date, operation status and well type. The completion dates and first production dates are used in this study to determine well ages, and only wells that are producing were selected in this sample. There are totally 13 yearly reports of all wells in Colorado, after applying the filtration methods to all of these reports, 1,677 vertical wells with needed information were chosen for analysis.

Another source of data collection is the Carte[®] system of Noble Energy Incorporation. However there is not any information about completion and first production date in the system, only frac flowback data report of vertical wells were acquired from Noble Energy. After comparing flowback water with produced water of vertical wells in Wattenberg, it is necessary to neglect water produced during flowback period since it is so short (usually less than 1 to 2 days). Therefore, only produced water data from COGCC database was used for the analysis of water production trend of vertical wells in Wattenberg field.

The analysis is based on the average value of water production and producing days. From the COGCC data, average producing days were calculated (see Table 3.2) and depending on the well age, all these wells were classified from well age 1 to 13 (see Table 3.1). By summing up

total water produced from all wells of the same well age and divided by total number of wells of the same well age, the average water production rate (bbl/well/year) was computed. And the daily water production rate is calculated from the yearly rate divided by average producing days in each year.

After plotting the daily water production in each operating year with time, the water production trend curve of vertical well is made. As shown in Eq. (1), the curve was fitted into exponential decay. The average decay rate for the entire Wattenberg field is 0.112 year⁻¹ and in order to study the relationship between decay rate k and spatial location of wells, k value for each vertical well of 1,677 well samples was computed. And there are only 1,230 k values calculated from the sample, for the other 447 wells k value was not able to compute either because of the curve was not exponential decay or there was only one value (wells in 2011). All data and calculation results of vertical wells are shown in Table A.1 and A.2.

A.2. Horizontal well water production data collection and analysis

Unlike vertical wells, there was no horizontal well before 2010 so yearly water production data from COGCC cannot be used for analyzing water production trend for horizontal wells.

Also because of long frac flowback period of horizontal wells, it is essential to study both frac flowback and produced water production trend.

All the analysis of horizontal wells in this research was based on water production data from Noble Energy Carte[®] system, including both hourly frac flowback report and daily produced water data. Only 32 wells' production data was acquired so only a sample of 32 horizontal wells was studied in this research. New report for each well was made by converting frac flowback data into daily data and combining them with produced water data. Frac flowback

water curves were fitted into exponential decay and produced water curves were fitted into harmonic decay and k_I and a values were calculated and these calculations were all made from the modified data analysis method for horizontal wells (Figure 3.3). All calculation results of horizontal wells are shown in Table A.3. After Calculating k_I and a value for each well, curves were plotted for each k value of every well, and based on the 64 curves (32 for k_I and 32 for a) the average curve (Eq.(2) and (3)) was made to represent the water production trend of all horizontal wells.

A.3. 30-year water production rate for vertical and horizontal wells

For both vertical and horizontal well, a life time (30 year) of water production rate was predicted for use by the developed Excel based tool. According to Eq. (1), (2) and (3), daily water production for both types of wells and predicted yearly volume of water production is shown in Table A.4 and A.5.

Table A.1. Water production data and k value calculation of 1677 sample vertical wells

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Zv.	A ON	AW OW	21	ZV	W SW	SNV SNV	SW	ΔVO	AN AN	W.	AN9	NS SW	OW	W W	AV9	AND AND	OW	W	AV6	W GW	A AND	4W	8W	ΦV	3W	8W	× ×	W.	W.	8W	W.	34V	AW6	8W	8W	W.	SWV SWV	W.	4W	34V	2W	NG.	AV6	OW	4W	N.	W.	AV6	WV ANV	AV9	N/S	IW.	ANG OW	W.	8W	SWV SWV	8W	4W	1	ZW	6W	NS N	4v	N/S	2 24	2	W.	W.	W.	4W	NA SW	AV6	ZW	WV WW	8W	WW.	AVD.	ΦV	347	W SW	W.	SW	340	ZV AV	W.	NV NV	¥ 24	W.	OW
10 ng	043337	043828	04.7558	D4.3824 D4.5338	04.4283	D48475	D4.6421	044572	D4.4533	D4.6164	D48394	04.8491	04.5471	104,644	048433	045664	04.5149	046060	045895	D48043	046375	049679	044773	045030	04.6516	D45244	05.0201	104.4211	04.4935	044958	046407	046405	047397	04.5104	04.5103	044249	04.8531	04500	044202	D4.8414	045621	045946	D4A292	D4807sm	044248	04.7398	046635	044250	050478	045029	046037	04.6038	048390	04.6158	04.5 120	045903	044965	04.7081	104,6112	045223	104.6161	04.4931	046548	046564	04.7814	04.5702	04.8139	04.6531	04.4067	043783	04.3918	046682	04.6165	045884	044348	044398	044488	044347	04.4351	D46544	04.9458	D47664	D47678	D44624	04.6588	D45904 P45506	043533	046499	047680
at 9020N	6553N 9623N	3056N	4377N	2062N	9446N	8245N	4809N	N2980	3568N 51740N	35 t24N	6762N	8522N	N1.2965	6890N 51205N	3923N	3534N	N9969	22581N	4996N	1808tN	33.25N	5373N	NOOD	8 104N	4405N	6282N	2234N	2868N	6385N	51723N	8 195N	V8.8N	5628N	8492N	8036N	0495N	Z28ZN	MACHIN	9387N	3240N	SECEN STREET	3080N	9729N	37.4 BN	9372N	5634N	35 168N	9783N	NOON	16 104N	54581N	33851N	3078N	N2659	5987N	8780N	18 t24N	8370N	83.70N 6985N	11024N	34677N	8964N	9251N	19482N	KO92N	8694N	6326N	2294N	1603N	2289N	3358N	32 VN	2454N	NOODS	NB 02t	72 BON	7723N	77.46N	7363N	N828N	0242N	9048N	9235N	0240N	N11311N	97 f78N	9/ ap	N0.44	13803N
166 40.3	87 40.5	D1 40.4	129 40.3	26 157 40.5	176 40.3	35 40.4	67 40.5	82 403	30 405	129 40.3	33 40.5	34 40.4	42 40.5	361 40.5	371 40.5	A05 A05	196 40.4	194 40.5	417 40.5	120 407	29 404	431 402	32 407	36 40.4	137 40.4	139 40.5	44 403	40.4	165 40.4	168 40.5	180 40	481 40.	182 40.3	198 40.4	199 40.4	02 404	05 404	512 404	24 40.3	25 40.3	K31 40.5	32 40.5	34 40.3	37 40.1	561 40.3	53 40.3	57 40.3	160 40.3	72 402	96 40	591 40.5	92 40.5	819 40.4	621 40.3	36 40.3	42 40.4	145 40.4	52 40.1	54 402	157 40.4	160 40.3	162 40.4	164 40.	166 40.1	72 403	74 402	75 40.4	178 40.3	58 40.4	70 40.4	73 40.4	82 402	87 40.4	791 403	109 404	811 40.4	814 40.4	815 40.4	816 40.4	125 40.1	145 40.3	146 40.4	147 40.4	168 40.5	172 40	174 402	92 404	96 40	30 40.1
api_se	8 8	260	88	8 8	8 8	8 8	38.28	382	8 8	88	88	8 8	283	8 8	88	8 8	88	383	8	387	8 8	28	8 8	38	287	8 8	38.	8	384	88	387	98	38	387	88	386	8 8	38	286	286	8	386	286	386	38	286	386	286	8 8	38	58	38	38	26	386	88	286	38,6	38.8	386	286	8	38	286	386	38	386	286	8 8	287	8 8	287	287	8 8	388	8 8	8 8	38	8 8	38.	38	288	38.8	388	386	395	388	388	392
pi_county t23	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123
Year a	8008	2008	2008	2008	2008	8008	2008	2008	2008	2008	2008	2008	2008	8008	2008	2008	3008	2008	2008	2008	2008	2008	2008	2008	2008	2008	2008	8008	2008	8008	2008	2008	8008	2008	8008	2008	2008	2008	2008	2008	2008	8008	2008	2008	2008	2008	2008	2008	2008	8008	2008	2008	2008	2008	2008	2008	2008	2008	8008	2008	2008	8008	3008	2008	2008	2008	2008	2008	8008	2008	2008	2008	2008	2008	2008	3008	2008	2008	2008	2008	2008	2008	2008	2008	2008	3008	2008	2008	2008
1,459	2.884	1.548	0.84	174	0.097	1641	0.944		0.359	0.063	1307	0.60	0.644	0.496	0.586	0.827	1267	0.717	0.818	0.347	137	0.493	0.926	0.409	1.589	1726			0.85			0.478	0.94	1261	1009	0.465	0.997	0.216	0.486	0.503	0.86	0.595	0.586		0.491	0.111	0.858		0.945	0.252	0.207	0.00	1.79	0.689	1363	0.05	0.532	0.12	1.61	0.47	2.336	000	0.487	1916	0.887	039	0.955	0.00	280	1032		1.02	0.506	0 68	0.844	1346	0.577	0.016	0.442	1.81	0.715	1625	0.507	0.455	0.951	2.039	6.500	0.555	3.414
0.046	2.088	0.858	0.395	0.786	1233	0.984	1017	1264	0.983	0.461	0.058	0.553	0.365	0.130	0.029	0.300	0.031	0.300	0.153	0.053	1086	0.026	0.129	0.462	0.616	0.300	0.054	1.152		0.979	0.494	0.095	0.433	0.822	0515	0.636	0.852	0.651	0.296	0.609	0.286		0.682	0.200	0.608	0071	0971	0.055	0.183	0.029		0007	0.120	0.664	7000	0.050	0.045	0.572	0.815		0.763	00041	0.328	0.490	1056	0211	0.671	0.183	0371	0.162	0.716	0.144	0.226	0.308	0.705	0.280	0.568	0.722	0.086	0.272	1.052	0.132	0.423	0.818	0.195	0.689	0.142	0.277	0.849
0.650	3203	0.997	0.527	1097	1.129	0.322	0.538	0.342	0.425	0.852	0.540	0.916	0.278	0.207	0.011	0.263	0.017	0.458	0.387	0.00	0.448	0.030	0000	0.087	0.670	0.488	0.048	1289	0.261	1.142	3	0.345	0.519	0.953	0.529	1,014	141	1367	0.245	0.589	0.245		0.858	0.685	0.740	0.605	0.811	0.214	0.196	0.150	1045	0.696	1235	0.867	2000	0.042	0.042	0.625	0.723		0.958	00000	0.723	0.825	1001	0395	0.338	0.143	0260	0.526	1096	0.115	0.504	0.133	0.879	0322	0.709	1392	0.826	0.476	1.449	0.490	0.142	1078	0.269	0.153	0.130	0.413	1,409
1200 1200	4.16	0.958	0336	1744	1301	1187	0230	1183	1939	1730	9020	1795	0774	0.351	0.0 14	0340	0022	0340	0.521	0.513	0.410	0.061	0384		10 19	1462	0.197	0.341	0335	0554	0,403	2620	1285	0.789	1321	1926	1163	1877	0.348	0723	0348	2	1253	0.922	0.293	0208	2.190	0.409	1606	0.450	0.522	2745	2.914	17.17	0.480	0.048	0.049	221	1025	0.794	2879	0.422	0994	0.893	2.132	0347	0287	1132	0.694	0525	1091	9020	0.863	1844	0350	1488	1069	1452	2 480	0.716	4549	1017	1071	0.901	0.714	1043	0.194	0.475	1144
1508	7.151	90700	1409	1952	0330	11093	4.631	7962	29556	2054	0.631	3,608	2.061	3037	0.014	1646		1503	0.91	11307	1722	1175	0.244	9860	1166	10.450	0384	0830	10.013	0.000	9763	2.170	2987		2353	13.583	1441	4.154	4457	2559	851	3	1889	4926	1432	8341	4242	5.060	6848	0978	66.154	9000	11681	14.811	8582	0.092	2900	16790	0.7.0	4097	12.281	0349	1670	4075		1552	2.196	6282	200	2482	2281	7556	1067	4049	2720	33559	0.918	3506	1436	6854	3384	2880	1724	0.949	2,465	12.14	6335	2625	1685
R 07																																																																																									
9 8	378	94	96	. fg	291	0	0 0	292	234	21 12	, A	131	88	0 0	-	73		73	32	Ŧ,	229	9	26	110	133	73	2 2	220	0	238	4	23	87	66	24	5 64	202	200	7.5	118	N C	0	161	35	46	2	236	Ð	43	-	0	0 10	25	120	0 9	G =	Ŧ	139	88	0	183	9 9	78	110	267	200	50	40	46	38	44	35	48	4 4	0.4	68	121	63	4 5	99	425	32	0 0	246	47	21	35	99	203
97 J	10 G	204	243	243	236	23 22	243	231	238	243	243	237	241	243	243	243	227	243	229	208	243	235	201	238	216	243	241	10	10	243	241	243	80	242	241	242	243	243	243	243	243	239	236	236	240	239	243	236	235	243	241	242	208	226	189	219	243	243	243	243	240	243	238	243	241	237	82	218	24	234	243	243	212	243	241	243	213	212	212	243	404	242	243	398	241	238	225	235	239
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363	237	382	334	382	385	329	216	298	322	385	365	329	334	362	386	098	328	382	364	306	384	382	294	334	312	334	354	332	329	332	334	365	339	382	385	365	350	364	364	350	334	382	385	365	385	344	382	332	332	334	332	332	332	330	334	326	380	333	382	342	333	385	385	361	350	362	344	322	385	310	388	331	385	386	382	329	387	365	363	334	546	385	365	74	334	328	323	334	303
00 AM	928	320	05	438	475	432	88	394	988	628	231	27.1	281	121	40	50	0	24	148	44	200	6	62	0	372	341	72	30	104	82	0	28	84	288	481	703	472	686	127	264	2 6	0	455	332	100	73	795	146	242	03	187	936	1052	929	118	490	\$	743	37.4	270	1045	4 6	380	326	107	5 2	87	394	75	191	396	257	242	27.1	310	543	387	630	38.1	244	1342	361	380	219	287	243	202	443	412
900	232	334	304	362	382	364	303	333	343	363	327	23.6	363	345	369	8 88	380	365	284	345	332	147	336	362	382	356	385	88	310	334	384	385	6	385	364	365	352	385	385	385	36.0	384	363	363	345	327	363	357	198	229	358	341	361	332	246	387	365	336	365	340	363	385	362	365	367	363	303	348	000	364	363	364	385	390	337	382	362	365	380	341	292	355	365	243	380	351	380	364	380
WP08	980	0	434	574	88	252	2083	2118	1330	532	142	1021	474	826	4	45	0	463	246	1289	2490	309	91	2110	302	1787	91	85	1572	0	1650	220	693	0	640	978	200	20 00	624	348	2017	0	495	410	335	1910	140	1093	1534	136	2.60	0	1390	785	1991	200	23	2401	000	885	200	99	308	925	0 0	256	112	735	0	474	438	136	180	246	408	2282	101	610	234	1036	382	311	250 10	204	663	329	1438	441	278
900 366	6 6	9	308	284	300	94	244	266	88	259	225	283	230	272	296	27.4	279	308	270	178	237	263	96	214	259	230	237	223	12	34	89	235	232	182	272	72	22	63	140	136	237	158	282	236	234	229	33	216	224	139	13	3	119	23	232	217	64	143	225	218	29	202	85	227	62	92	15	417	32	191	95	8	84	g g	120	68	110	44	633	2 5	294	108	162	245	589	t 27.1	227	68	85
2007 WP07																																																																																									_
10 ng P	D4.55669W D4.50942W	D4.62389W	D4.69357W	04.78930W 104.66122W	104.71140W	104.510 BW	D4.65575W	104.7 D93W	D457924V	104.67132W	104.41129W	104.7 B55W	104.809 fftV	D4.58293W D4.58994W	D454963W	D4.68026W	D4.54045W	104.598.BW	104.585 ffV	D450543W	104.50063W	D4.48044W	D450073W	D4.79920W	D4.66283W	D4.59868W	104.71135W	D4.48085W	104.572.41V	104.517.41V	D5.02292W	D454098N	D4.72582W	D4.56036W	104.5 E99NV	D4.627.75W	D4.62620W	D462623V	D4.62622W	D4.62622W	104.6262TV	D4.72976W	104.630 fftV	D46826 AV	D454853W	104.5348ftV	104.53091W	104.8 E82W	104.8 N 75W	D4.76669N	D4.86227W	D4.85343N	D4.47677W	D4.60696W	104.487.BW	104.499 BW	D450409W	104.6 1499W	D4.57857W	104.625 P.W	104.6 E69NV	104.41t22W	D439225W	D4.60993W	D457434W	D436858W	D4.36843W	104.467.21W	D4.34955W	D4.76903W	D4.60697W	D4.92964W	104.41f76W	04.8375.AV	104.657.2W	104.81551W	D4.60704W	104.41151W	D439688W	D4.535554V	D4.65027W	D4.66632W	D4.74757W	105.00157W	D480830W	104.429.71V 104.825.47V	D4.82786W	104.8 B82W	04.38245W
1a t 19606N	7875N	2288N	2738 fN	6385N	12392N	49 5 1N	3662N	13702N	2335N	1496N	N9669	2602N	18550N	9635N	N9980	N9288	13794N	19992N	B644N	N8208t	8240N	N0698	18430N	8622N	3304 IN	3450 th	5772N	7993N	3084N	29384N	8000N	9837N	B475N	NE9EE	3274 fN	34038N	34911N	M877N	M870N	M884N	7584N	7230N	10472N	8677N 8645N	31782N	6803N	12243N	49 t20 N	2460M	19406N	10848N	N96806	9237N	29413N	18465N	6522N	96843N	3377 fN	7687N	54583N	294t2N	47019N	6272N	N09696	3602N	3759N	14463N	W233N	6242N	N2980	25749N	18278N	17765N	3435N	7.115 IN	45 185N	42.45 TN	W827N	14462N	8027N	19618N	E977N	N62008	01653N	19864N	51039N	5244 fN	N39657	40 t23N
181 40.3	V4 40.5	287 40.4	293 40.	294 40.3	300 402	106 40.	308 40.5	323 40.5	346 40X	348 40.	380 40.4	385 40.	388 40.4	394 40.7	398 40.3	400 40	419 40.3	420 40.	126 40:	429 404	132 402	133 402	439 404	150 40.4	453 40.	457 40.2	W65 40.2	772 402	175 40.5	489 402	192 40.2	198 402	705 40.	508 40.5	517 40.	518 402	520 40	22 40.3	523 40.5	526 402	239 404	744 402	547 402	554 40.3 355 40.3	356 40.2	557 40.4	581 40.5	582 40.	220 402	340 40.4	347 40.5	848 402	651 40.4	352 40.	855 40.4	775 402	681 402	No 40.	714 40.3	715 40.3	723 40.	724 40.	750 40.4	757 402	759 402	764 40.4	767 40.4	770 40.	785 40.4	786 40.5	900 402	307 40.3	909 404	20 402	322 40	837 40.	775 40.4	980 40.4	883 40A	194 40.3	304 40.	916 40.	775 402	776 40.K	377 40.4	MO 40.5	081 403	762 40.4	365 40.
api_s	25 25	252	252	32 S	385	8 P	25.	255	8 8	55.5	28. 8	100	285	8 8	285	Ř	8	254	264	\$	9 19	254	38.	254	254	28.4	254	8	254	Š	254	254	38	255	8 8	16	26.	26.5	255	284	ğ (S	38	28¢	255	255	255	88	255	202	256	256	286	25,00	256	254	326	32	25.2	8 8	8	257	8	8 9	257	8 28	257	257	285	8 8	257	250	255	325	25.	255	32	258	255	252	8	255	28	35.05	255	255	380	38	280	380
county t23	2 2	23 23	123	2 2	123	123	123	123	23 23	123	2 2	123	123	22 23	123	23 23	123	123	123	123	2 2	123	123	123	123	123	23 23	123	123	123	23 22	123	23	123	123	123	123	23 23	123	123	23 23	123	123	22 22	23 22	123	123	123	23 23	23	123	123	23 23	123	123	23 23	123	123	23 23	123	123	2 2	2 22	123	123	123	123	123	123	123	123	123	123	23 62	123	2 2	123	123	123	23 23	123	123	2 23	123	123	2 2	123	123	3
a bi	m -																	_		e-																								_						15					_		5							5				-		_			e-																_
2000	2000	2005	2000	2000	2000	2006	2000	2006	2006	2000	2000	200	2006	200	2000	2000	2006	2000	2006	2000	2006	2006	200	2000	2006	200	2006	2005	2005	200	2006	2006	2005	2006	200	200	200	2000	2006	2000	2006	2005	2000	2006	2006	2006	2006	2000	2000	2005	2006	200	2006	2006	2000	2006	2000	200	2006	2006	2000	2000	2006	2006	200	2008	2006	2000	2006	2006	200	2006	2000	2000	2006	200	200	2008	200	2006	2005	2006	2008	2005	200	200.	2006	2000	20G

×	0.94	0.342	0.761	1.161	1275	0222	0.074	0	0.866	0.74	0.55		0.598		0.427	0.101	0.716	1272	0877	0.656	0.597	0.06.0	0746	2699	9600	0.959	0574	2900				1391	0.76	0034	1844	0869		0.916	0.653	1615	132	0.489	0.89	0599	2.67		0.828	1791	0.17			1.12	1205	0398	243	0.51	0.388	0000	0.415	0.605	026		0292	0.563	0.106	1489	1299	1306	5	0929	0738	1253
-R 11	0.333	2.472	0.523	0.554	0.486	0.330	9.359	0.272	0.612	0.066	0.782	0.432	0.830		0.058	1715	1.52	0.527	2.000	0.358	0.450	0.202	0.709	0.349	0.853	2.280	0.634	0.930	0.250	0.638	0.85	0.374	0.428	0.445	1391	0.988	6.329	0.790	0.095	0.461	0.186	0.941	1074	0.650	0.864	47.088	0.613	0.765	2.502	3.11	1284	0.509	0.868		1,614	2.85	0.918	1.737	0.617	1.481	7.904	0.433	0.234	0.272	0.453	0.527	0.480	0.006	0.971	4.89	1.684	1.88
R 10	0.734	2.967	0.737	0.734	1340	2.691	0.564	0.559	1065	0.252	0.921	0.515	0.15	0.030	0.088	4.041	1041	0.625	0.073	0.241	0.468	0.666	1715	0.093	0.992	1.146	0.932	1728	0.342	0.085	0.701	0.830	0.921	0.970	2.298	2.044	5.290	1274	90.0	0.603	1405	0.751	1841	1,809	1.404	6.092	1321	0.969	3.84	3.636	3.803	0.818	1,759		1598	4.049	1.87	1912	0.953	2.675	1267	1.87	0.649	0.761	0.942	1203	0.810	0.994	1532	1338	1036	2.431
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lon	104.585	104.386	104.829	104.837	104.415	104.401	104.893	104.555	104.64762	104.556	104.782	104.607	104.381	104.616	104.610	104.416	104.565	104.392	104.381	104.377	104.792	104.662	104.598	104.516	104.518	104.780	104.518	104.648	104.440	104.837	104.504	104.516	104.602	104.45	104.834	104.503	104.937	104.913	104.473	104.462	104.452841	105.018	104.752	104.742	105.00	104.406	104.832	104.57928	104.444	104.786	104.626	104.626	104.626	104.634	104.636	104.636	104.63-	0451	104.781	104.521	104.704	104.592	104.523	105.019	104.5TC	104.592	104.80	104.415	0467	104.532		-
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WW OW OW	ZW	AN A	W SW	A A A	W.	AV AV	ONV SNV	N AV	ZV.	W SW	W.	ANA BAV	NS SW	A A	W SW	NO.	ZW	A A	A 54	NA SWA	3VV	OW	W.	ZW	NV NS	OW	AV SW	ANS SNV	W SW	2NV	WAV AVV	SAV SAV	NI.	OW	ONV SAV	3VV SVV	M1 V	AV.	OW SW	W SW	ANV ANV	A A	347	SNV GNV	WV AVV	ZVA	ANA SAV	1 1	AN.	3W	W ZW	AV OV	WW 8W	SW SW	AN OW	NV OW	SNV	ANA MA	3W	OW
104.78759NV 104.78759NV 104.78750NV	104.4563.	104.4584	104.5969	104.7803	043737	104.6445	104.8566	104.8469	104.6093	104.77.86	045196	104.5283. 104.6283.	104.6445	046465	104.3692	104.5804	104.8028	D4.4348	044195	104.5824	104.8006	046120	104.5448	045912	04585	104.7896:	104.7895	104.0630	104.5569	104.6493	104.8005	104.7422	04854	104.7343	104.6633	104.5027	104.5293	104.5837	104.5262	104.6200	104.5265	045755	104.6083	104.6083 104.8103	104.58552	104.6463	045281	104.37.28	04.587	104.3542	104.3572		D4.5568	104.87.46	104.87.45	0 0	\$ \$	2 2 5		ě
40.32928N 40.32928N 40.32930N	N 28	Z Z	Z Z	4 K 8	K 18	4 4	N N	88	Z 26	88	4 8	60026N	43183N	3298N	4095N	2643N	N9201	754N	2072N	854N	7546N 7546N	N600	51114N	NB 200	3531N	7563N 6008N	7376N 6000N	3796N 9045N	2449N 3576N	7505N	9202N	6785N	74N	N N	2 Z	2 AN	40.35183N 40.33227N	N 88	Z Z.	N N	20 20	N N N	157121N	56759N 17782N	59670N	32246N	59307N			44863N 44844N	47750N 44492N					40.23664N 40.32047N				
30544 40.3 30545 40.3 30546 40.3	320 40.	1323 40 1445 40.	729 40	736 40,	765 40,4	864 404	877 40.	5106 40.	3328 40 460 40	65 B 40	3947 40		1990 40		7124 40.4			8146 40.5													9721 40.		783 40.										3166 40		265 40.5		1293 40.	1333 40.	1426 40.			4997 40.	0550 40.5	5552 40. 5553 40	1554 40	1595 40.	837 40	1872 40.	683 40. 688 40.	690 40
8 8 8 8																																																												
m m =			3 8	2 2 2	2 2	23	23	23 23	22	23	53 6	1 1 1 E	1 22 0	1 2 5	1 23 5	1 22 6	100	i i i	12 K	123	23	100	100	100	23	23 23	23	223	223	100	50 0	51 6	51 6	123	23 62	23	123	223	23	20.00	50 0	100	153 E	23 23	23	23	101	1 52 c	1 62 kg	23 23	23	23	23	23	23	23 23	223	4 CH C	23 23	ŝ
23 23 23	4 64 6	51 51																																																										

Table A.1 (Cont.)

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FR 11	0.000	3.888	2.665	3.000	5.240	7.466	0.805	0.373	43.285	30.600	6.348	19.500	4.667	6.994	10.682	2.283	0.963	6.525	25.048	12.421	4.127	5.912	0.000	0.000	6.430	21.169	24.632	6.208	2.673	1.723	6.514	16.690	9.185	7.593	9.342	6.375	7.100	8.824	0.000
WP11 FR 11	0	416	24	630	524	1202	124	09	5930	612	419	468	644	1238	1880	105	52	398	1578	944	260	141	0	0	508	1630	1872	447	139	162	241	484	248	205	355	153	142	150	0
PD11	109	107	194	210	100	191	45	191	137	8	99	54	138	177	176	46	54	61	83	9/	83	193	2	9	79	14	26	72	25	96	37	53	27	27	88	24	20	4	54
long	104.46553W	104.65065W	104.65048W	104.65056W	104.53223W	104.43455W	104.43722W	104.43718W	104.63728W	104.54831W	104.59673W	104.54322W	104.58823W	104.67288W	104.67288W	104.54148W	104.54301W	104.53261W	104.83548W	104.83547W	104.61701W	104.38767W	104.55053W	104.59179W	104.53702W	104.50658W	104.50664W	104.33895W	104.37715W	104.36086W	104.58368W	104.66534W	104.66541W	104.66520W	104.66549W	104.66527W	104.51798W	104.51806W	104.45839W
lat	32575 40.50457N	4020668N	4020664N	4020666N	40.42504N	40.50293N	40.50099N	40.49811N	40.47515N	40.39297N	40.48209N	40.54602N	40.48277N	40.33014N	40.33007N	40.54114N	40.53899N	40.21842N	40.35972N	40.35965N	40.33018N	40.47760N	40.52607N	40.17691N	40.41215N	4026605N	40.26617N	40.46683N	40.49958N	40.49063N	40.19598N	40.52416N	40.52416N	40.52416N	40.52416N	40.52416N	4024763N	4024763N	33351 40.55764N 104.45839W
api_seq	32575	32579	32580	32584	32630	32642	32643	32644	32648	32652	32655	32656	32666	32700	32701	32722	32724	32788	32822	32823	32827	32830	32865	32907	32964	33116	33117	33187	33206	33224	33242	33282	33283	33284	33286	33289	33327	33329	33351
api_county	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123
k Year	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011
FR 11	4.359	7.557	11.594	24.396	14.275	0.599	1331	5.321	3.679	0.062	0.000	4.615	0.000	4.396	8.762	9.712	1.661	3.880	5.159	3.894	0.838	6.449	4.765	5.038	3.642	9.714	11.404	0.807	0.000	0.000	6.353	2.940	0.000	4.000	12.585	9.339	0.176	0.308	0.195
WP11	728	922	1658	3757	2127	127	205	894	721	\$2	0	300	0	1121	1507	1418	309	322	423	627	429	445	405	403	295	2409	2030	130	0	0	540	488	0	089	299	1653	6	9	22
PD11 \	167	122	143	124	149	212	154	168	196	292	29	92	2	255	17.5	146	186	83	82	191	154	69	82	80	8	248	178	161	158	156	85	166	106	170	53	177	51	25	13
long	104.62272W	104.59404W	104.59395W	104.59422W	104.59413W	104,45633W	104.46035W	104.46031W	104.62674W	104.62864W	104.63317W	104.63326W	104.63307W	104.93427W	104.77414W	104.77414W	104.60678W	104.61363W	104.61381W	104.44431W	104.44248W	104.61336W	104.61354W	104.61371W	104.61344W	104.65870W	104.66115W	104.63350W	104.63340W	104.63332W	104.61327W	104.61787W	104.46251W	104.61852W	104.54196W	104.66272W	104.46553W	104.46553W	104.46553W
lat	32300 40.24839N	40.25397N	40.25397N	40.25397N	40.25397N	40.49009N	40.49024N	40.49029N	40.35212N	4024117N	40.24207N	40.24207N	40.24207N	40.22.101N	40.31834N	40.31827N	40.34102N	40.34597N	40.34597N	40.49576N	40.49772N	40.34597N	40.34597N	40.34597N	40.34596N	40.20732N	40.32098N	40.24488N	40.24487N	40.24487N	40.34597N	40.35413N	40.50252N	40.35756N	40.25425N	40.32306N	40.50451N	40.50464N	32573 40.50444N 104.46553W
api_seq	32300	32301	32302	32304	32322	32357	32358	32359	32375	32394	32410	32412	32418	32431	32464	32466	32478	32506	32507	32508	32509	32510	32512	32513	32516	32517	32531	32534	32535	32536	32538	32545	32546	32547	32555	32563	32568	32571	32573
api_county a	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123
k Year	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011
FR 11	2.578	1387	1.578	1.935	2.071	1.688	0.810	3.185	19.158	7.563	0.527	1.094	23.519	7.429	4.187	0.000	574.333	2.484	21291	4.280	13.625	0.957	9.866	0.500	3.474	0.956	1.548	1308	5.131	22.089	0.463	12.612	0.327	3.156	1.536	2.542	4.667	3.912	3.543
WP11	116	43	7	09	381	216	8	586	728	658	29	28	1270	260	1721	0	1723	380	1171	779	436	154	1401	80	809	197	209	187	431	1237	25	618	\$2	999	258	450	630	999	457
PD11	45	31	45	31	184	128	100	184	88	87	SS	23	25	35	44	88	8	53	83	182	32	191	442	160	175	206	135	£4	8	26	25	64	55	211	168	14	135	170	129
long	31665 40.29664N 104.74494W	31667 40.29669N 104.74499W	31671 40.29660N 104.74489W	40.23194N 104.94880W	104.56235W	40.2151N 104.93104W	104.93096W	104.82533W	31850 40.25426N 104.54188W	104.53657W	40.47710N 104.42565W	31895 40.47710N 104.42565W	104.43008W	31910 40.24923N 104.54906W	31914 40.17275N 104.61043W	40.51409N 104.45339W	40.16926N 104.60952W	40.16868N 104.61393W	31950 40.47390N 104.42487W	104.60696W	104.58769W	32072 40.30468N 104.53196W	104.54220W	104.53462W	32108 40.48287N 104.46537W	104.61995W	104.53723W	104.53722W	40.36766N 104.47491W	40.47398N 104.41548W	32250 40.47750N 104.42058W	104.42111W	104.41585W	32260 40.48645N 104.45643W	40.51617N 104.44648W	104.46527W	104.77177W	104.46070W	32299 40.32453N 104.77178W
lat	40.29664N	40.29669N	40.29660N	40.23194N	40.55252N 104.562	4021151N	40.21149N 104.9309	31843 40.52581N 104.825	40.25426N	40.26155N 104.536	40.47710N	40.47710N	31896 40.47385N 104.430	40.24923N	40.17275N	40.51409N	40.16926N	40.16868N	40.47390N	31965 40.25477N 104.606	32011 40.26099N 104.587	40.30468N	40.61128N 104.542	40.30341N 104.534	40.48287N	32113 40.45627N 104.619	32134 40.29466N 104.537	32/40 40.29460N 104.537;	40.36766N	40.47398N	40.47750N	32252 40.47413N 104.42	32253 40.47750N 104.4158	40.48645N	40.51617N	32266 40.48607N 104.465	40.32446N 104.77	40.48621N 104.460	40.32453N
api_seq	31665	31667	31671	31697	31715	31737	31778	31843	31850	31880	31894	31895	31896	31910	31914	31918	31920	31947	31950	31965	32011	32072	32075	32077	32108	32113	32134	32140	32152	32239	32250	32252	32253	32260	32263	32266	32269	32282	32299
Year api_county api_seq	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123	123
Year a	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011	2011

Table A.2: Results of produced water analysis of 1,677 vertical wells in Wattenberg field

Operating year	Number of wells	Total WP	WP/well	Production days	WP/well/day
		(bbl)	(bbl)	-	(bbl)
1	1,677	1,847,953	1,101.940	162	6.802
2	1,494	736,296	492.835	336	1.467
3	1,324	306,487	231.486	339	0.683
4	1,140	175,038	153.542	341	0.450
5	807	141,775	175.682	342	0.514
6	535	91,548	171.118	348	0.492
7	374	55,024	147.123	354	0.416
8	243	38,351	157.823	345	0.457
9	138	23,375	169.384	349	0.485
10	73	10,410	142.603	338	0.422
11	45	3,395	75.444	322	0.234
12	16	1,351	84.438	339	0.249
13	6	957	159.5	333	0.479

Table A.3. Results of frac flowback and produced water analysis for 32 horizontal wells in Wattenberg field

								Raw Data			Protocol Data	
API	Well Name	Well Number	Well Type	Total Water (gal) Flowback Trend	Flowback Trend	Produced Water Trend	Flowback Days	Flowback Days Total Flowback (gal) FB/Total Water	FB/Total Water	Flowback Days To	Flowback Days Total Flowback (gal) FB/Total Water	/Total Water
05-123-33576	70 RANCH BB	21-65HN	HORIZONTAL	3258822 y	3258822 y = 165.57e ^{-0.029x}	y=72.05784/(1+0.013901x)	30	132477.1814	0.041	52	181734.80	0.056
05-123-33577	70 RANCH BB	21-63HN	HORIZONTAL	2666958 y	2666958 y = 251,47e ^{-0.056x}	y=39.52193/(1+0.004337x)	25	151704	0.057	26	153363.00	0.058
05-123-33579	70 RANCH BB	21-67HN	HORIZONTAL	2581530 y	2581530 y = 201.09e ^{-0.053x}	y=93.3955/(1+0.036711x)	20	96264	0.037	25	119679.00	0.046
05-123-33556	70 RANCH USX	BB09-63HN	HORIZONTAL	2741928 y	2741928 y = 243,54e ^{-0.034x}	y=176.9398/(1+0.102339x)	39	236594.4738	0.086	43	246282.03	0.090
05-123-33546	Degenhart State	AE16-63HN	HORIZONTAL	2777418 y	2777418 y = 227,18e ^{-0.044x}	y=56.20368/(1+0.015408x)	51	187383	0.067	38	165816.00	090'0
05-123-33545	Degenhart USX	AE17-63HN	HORIZONTAL	2826432 y	2826432 y = 260.5e ^{-0.052x}	y=156.3435/(1+0.11475x)	51	193389	0.068	35	169176.00	090'0
05-123-32595	Feit	E23-97HZ	HORIZONTAL	2894136 y	2894136 y = 244,16e ^{-0.065x}	y=8.53998/(1+0.006637x)	175	242526.1298	0.084	48	148998.93	0.051
05-123-32648	FEITE	23-99HZ	HORIZONTAL	2968938 y	2968938 y = 223.52e ^{-0.072x}	y=16.00014/(1+0.007997x)	168	275972.5047	0.093	32	110844.10	0.037
05-123-32649	FEITE	23-98HZ	HORIZONTAL	3315984 y	3315984 y = 364.7e-0.062x	y=17.19166/(1+0.009755x)	179	402624.0295	0.121	49	237325.13	0.072
05-123-33277	Guttersen	D29-65HN	HORIZONTAL	2987838 y	2987838 y = 258,59e ^{-0.018x}	y=43.53527/(1+0.023925x)	69	423217.428	0.142	92	486373.06	0.163
05-123-33326	GUTTERSEN	D02-75HN	HORIZONTAL	2774436 y	2774436 y = 313,58e ^{-0.094} x	y=68.45044/(1+0.015931x)	14	90220.73921	0.033	24	119758.81	0.043
05-123-32709	GUTTERSEN D	29-99HZ	HORIZONTAL	3207708 y	3207708 y = 389.68e ^{-0.055x}	y=14.64023/(1+0.019218x)	147	400945.8772	0.125	49	279001.46	0.087
05-123-33223	Guttersen State	D28-79HN	HORIZONTAL	3096072 y	3096072 y = 310,36e ^{-0.026x}	y=19.62883/(1+0.010333x)	91	441607.2448	0.143	114	462904.27	0.150
05-123-32650	KLEIN	B16-99HZ	HORIZONTAL	3924900 y	3924900 y = 235,22e ^{-0.011x}	y=46.31031/(1+0.004432x)	110	625734.6464	0.159	144	697897.28	0.178
05-123-32651	KLEIN	B16-98HZ	HORIZONTAL	4593414 y	4593414 y = 251,78e ^{-0.011x}	y=50.62407/(1+0.005129x)	131	728625.6548	0.159	178	806661.65	0.176
05-123-33320	SCHOLFIELD STATE A 36-69HN	36-69HN	HORIZONTAL	3238830 y	3238830 y = 384.88e ^{-0.04x}	y=70.23207/(1+0.014761x)	54	342594	0.106	47	329175.00	0.102
05-123-33325	SCHOLFIELD STATE A 36-79HN	36-79HN	HORIZONTAL	3200022 y	3200022 y = 389,29e ^{-0.04x}	y=67.42931/(1+0.010178x)	54	344799	0.108	39	308385.00	0.096
05-123-34231	SOONER STATE B	36-63HN	HORIZONTAL	2789934 y	2789934 y = 194,58e ^{-0.036x}	y=22.12595/(1+002263x)	26	195195	0.070	54	193053.00	0.069
05-123-32821	SPIKE STATE D	16-99HZ	HORIZONTAL	3377556 y	3377556 y = 583,52e ^{-0.055x}	y=9.206827/(1+0.004122x)	140	655660.1738	0.194	57	479955.59	0.142
05-123-33114	STATEC	36-99HZ	HORIZONTAL	3182676 y	3182676 y = 221.52e ^{-0.019x}	y=43.56955/(1+0.015602x)	75	362313.5943	0.114	108	419439.05	0.132
05-123-33415	STOCKLEY	C22-79HN	HORIZONTAL	2391984 y	2391984 y = 173.02e ^{-0.072x}	y=69.26069/(1+0.021961x)	21	72093	0:030	30	84084.00	0.035
05-123-33416	STOCKLEY	C15-79HN	HORIZONTAL	3460170 y	$3460170 \text{ y} = 455.64e^{-0.073 \times}$	y=24.36715/(1+0.003722x)	72	211113	0.061	28	215964.00	0.062
05-123-33698	STREAR V	06-63HN	HORIZONTAL	2504292 y	2504292 y = 69.649e ^{-0.04x}	y=28.62867/(1+0.031515x)	29	49527.7692	0.020	34	53572.88	0.021
05-123-33702	TANNER K	33-65HN	HORIZONTAL	3144960 y	3144960 y = 286.78e ^{-0.071x}	y=1057.131/(1+0.676856x)	19	116088	0.037	25	133507.61	0.042
05-123-32747	UPRC	H17-99HZ	HORIZONTAL	3444546 y	3444546 y = 210.88e ^{-0.017x}	y=26.88737/(1+0.009147x)	128	457164.1289	0.133	133	462864.47	0.134
05-123-33869	Wacker	B01-79HN	HORIZONTAL	3001236 y	3001236 y = 178.09e-0.031x	y=31.962/(1+0.011489x)	53	206703	0.069	51	202293.00	0.067
05-123-33870	Wacker	B11-69HN	HORIZONTAL	2488458 y	2488458 y = 178.21e ^{-0.031x}	y=31.48131/(1+0.011091x)	53	206661	0.083	52	204960.00	0.082
05-123-33874	Wacker	B12-69HN	HORIZONTAL	712614 y	712614 y = 109.36e ^{-0.026x}	y=60.28455/(1+0.028376x)	38	119553	0.168	34	113253.00	0.159
05-123-33100	Wells Ranch USX	BB15-65HN	HORIZONTAL	3363654 y	3363654 y = 110.94e-0.011x	y=195.5892/(1+0.150384x)	95	269140.1773	0.080	137	323608.77	0.096
05-123-33101	Wells Ranch USX	BB15-67HN	HORIZONTAL	3019296 y	3019296 y = 163.31e-0.022x	y=162.7571/(1+0.023175x)	84	264085.8987	0.087	96	278429.17	0.092
05-123-33708	WELLS RANCH USX	AA11-65HN	HORIZONTAL	4350822 y	4350822 y = 1701,4e ^{-0.089x}	y=40.7521/(1+0.012849x)	29	746692.2559	0.172	37	764269.26	0.176
05-123-33324	Wells Ranch USX AE	29-68HN	HORIZONTAL	924840 y	924840 y = 569,79e ^{-0.031x}	y=22.59393/(1+0.012061x)	99	673887.3773	0.729	35	512677.76	0.554

Table A.4. Vertical well 30-year water production trend prediction

Operating Year	Н	7	က	4	2	9		∞				12		14	15
Water Type	ΡW	PW	PW	ΡM	PW	PW		PW				ΡW		ΡW	PW
Production rate (bbl/well/day)	6.802097	1.466772	0.682849	0.45027	0.513689	0.491718	_	0.457458	_			0.249078	_	0.2335	0.212551
Producdion days	162	336	339	341	342	348		345				339		341	341
Predicted WP (bbl/well/year)	1101.94	492.9428	231.2637	153.6113	175.6135	171.0472	٠.,	157.8433				84.42089	٠.,	79.62354	72.47994
Operating Year	16	17	18	19	20	21	22	23	24	22	56	27	78	53	30
Water Type	ΡW	PW	PW	ΡW	PW	PW		PW				ΡW		ΡW	PW
Production rate (bbl/well/day)	0.193482	0.176123	0.160322	0.145938	0.132845	0.120926	_	0.100201	_			0.068799	_	0.057007	0.051893
Producdion days	341	341	341	341	341	341		341				341		341	341
Predicted WP (bbl/well/year) 65.97724 60.05794 54.66971 49	65.97724	60.05794	54.66971	49.7649	45.30013	41.23592	٠.,	34.16869				23.4603	٠,٠	19.43955	17.69549

Table A.5. Horizontal well 30-year water production trend prediction

Operating Year	Н	7	3	4	2	9	7	∞	6	9	11	12	13	14	12
Water Type	FF+PW	ΡW	ΡW	PW	PW	ΡW	ΡW	ΡW	ΡW	PW		ΡW	PW	PW	
Production rate (bbl/well/day)	68.56049	68.56049 15.20399	5.64254	2.016466	0.731484	0.719873	_				_		_	0.675245	
Producdion days	162	336	339	341	342	348								341	
Predicted WP (bbl/well/year)	11106.8	11106.8 5109.655	1910.987	687.9247		250.4127								230.2585	
Operating Year	16	16 17	18	19	20	21	22	23	24	22	56	27	28	53	30
Water Type	PW	ΡW	PW	PW		PW								PW	
Production rate (bbl/well/day)	0.664527	0.664527 0.659232	0.653979	_	0.643599	0.63847	0.633383				_		_	0.598888	
Producdion days	341	341	341	341	341	341	341						341	341	
Predicted WP (bbl/well/year)	226.6037	226.6037 224.7981	223.0069	221.2299	219.4671	217.7184	215.9836		212.5554	210.8617			205.8613	204.221	202.5937

FF-Frac Flowback PW-Produced Water

Appendix B. Uncertainty analysis

B.1. Uncertainty analysis of 1,677 vertical and 32 horizontal wells in Wattenberg field

In order to model the decline functions of both vertical and horizontal wells in the whole Wattenberg field, average A and k values of 1,677 vertical wells and average k_I , a, A_I and C values of 32 horizontal wells were used. However from Figure 3.2 and 3.4, all decay rate value (k for vertical well and k_I , a for horizontal well) varies spatially in the Wattenberg field, it is necessary to study the reliability of the water production trends from Equation (1), (2) and (3).

For all 1,677 vertical wells, water production trend for each well was analyzed and fitted to an exponential decay function. Because there are 438 wells having only one year water production data (one data point) due to limited data got from COGCC database and another 113 wells have increased water production trends (which did not fit exponential decay function used in this study), only 1,126 k values of vertical wells were used in this uncertainty analysis. Unlike the k value, only 153 wells' k values were selected by random from these vertical wells. Assuming the distributions of k and k were normal, and for k0 confidence interval, the k2 score was 1.645.

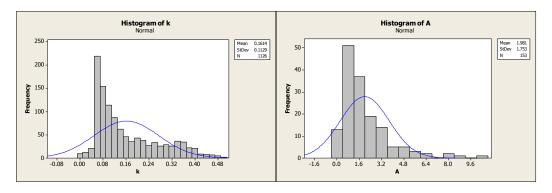


Figure B.1. Distribution of *k* and *A* of vertical wells

For 32 horizontal wells, flowback and produced water curves were all fitted and the distributions of A_1 , k_1 , C and a were analyzed.

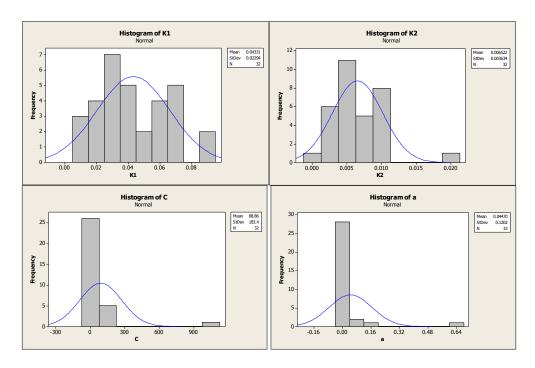


Figure B.2. Distribution of k_1 , A_1 , C and a for horizontal wells

Assuming all distributions were normal, and the z score for 2σ (95%) confidence interval was 1.645. Table B.1 shows the 2σ (95%) confidence interval for all variables of vertical and horizontal wells.

Table B.1. Uncertainty analysis and acceptable range of variables of all wells

	k	A	k_1	A_1	С	а
μ	0.1613	1.981	0.0434	264.4	88.8638	0.0447
σ	0.0033	0.141	0.0040	19.4	32.4282	0.0212
μ-1.645σ	0.1558	1.748	0.0366	232.3	35.5194	0.0098
μ +1.645 σ	0.1669	2.214	0.0499	296.5	142.208	0.0796

For horizontal wells, because frac flowback only lasts for 61 days, the water production rate for the first year is the average of 61 days of frac flowback and 101 days of produced water. Figure B.3 and B.4 show the water production trends with 2σ confidence interval of vertical and horizontal wells in the Wattenberg field.

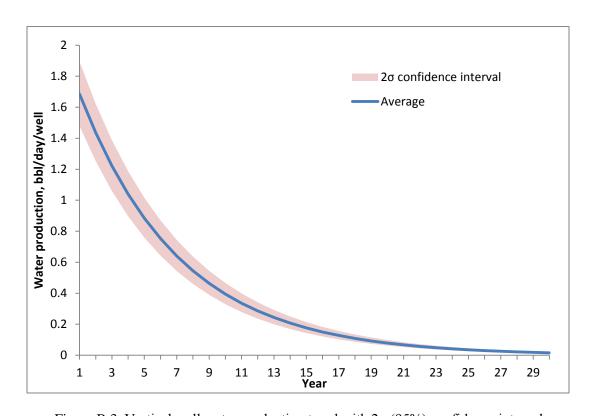


Figure B.3. Vertical well water production trend with 2σ (95%) confidence interval

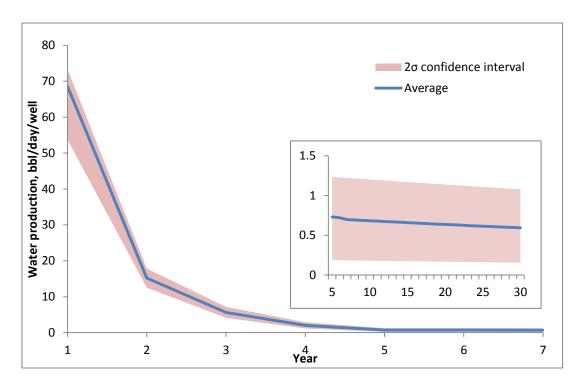


Figure B.4. Horizontal well water production trend with 2σ (95%) confidence interval

B.2. Uncertainty analysis of case study of selected wells in northeast Wattenberg field

In the case study of selected wells in northeast Wattenberg Field, 568 vertical and 12 horizontal wells were included and the same methods of uncertainty analysis were conducted to these wells. Figure B.5 shows the distribution of k, k_1 , A, A_1 , C and a values of all selected wells.

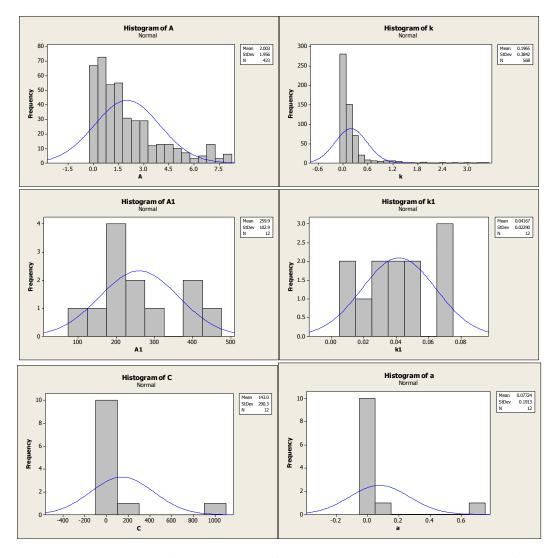


Figure B.5. Distribution of all parameters of selected wells in northeast Wattenberg field

Also the results of uncertainty analysis and acceptable ranges of variables of selected wells were shown in Table B.2.

Table B.2. Uncertainty analysis and acceptable range of variables of selected wells

	\boldsymbol{k}	\boldsymbol{A}	k_1	A_1	\boldsymbol{C}	а
μ	0.197	2.003	0.042	259.9	142.994	0.0772
σ	0.016	0.095	0.006	29.70	83.8	0.0452
μ-1.645σ	0.171	1.847	0.032	343.6	5.143	0.0029
μ +1.645 σ	0.223	2.159	0.052	441.4	280.847	0.1516

Water production trends of these selected wells were shown in Figure B.6 (vertical) and Figure B.7 (horizontal), with 2σ (95%) confidence interval.

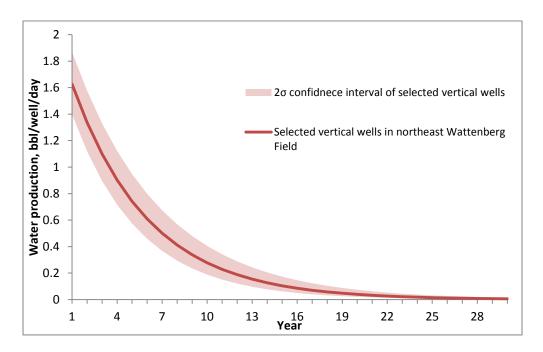


Figure B.6. Water production trend of selected vertical wells in northeast Wattenberg field with 2σ (95%) confidence interval

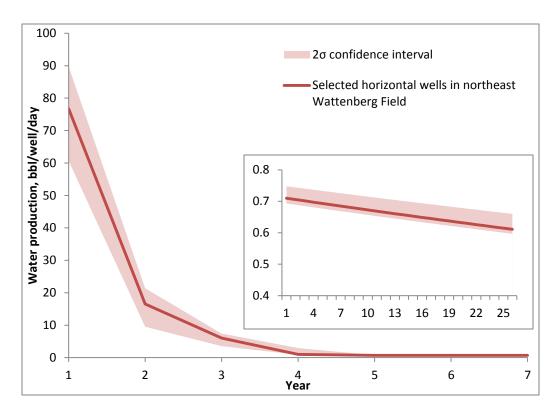


Figure B.7. Water production trend of selected horizontal wells in northeast Wattenberg field with 2σ (95%) confidence interval

Appendix C. 7,486 Noble wells case study data and results

From COGCC database, number of all Noble wells in Wattenberg field and total water production from 1999 to 2009 was collected. Data for 2010 and 2011 was collected from Noble Energy Carte[®] system. The case study was based on the existing data and the prediction was based on 200 new vertical and 100 new horizontal wells increase each following year. The summary of data is shown in Table C.1.

Table C.1: Historical and Prediction Data of 7,486 Noble Wells Case Study

Year	Number of vertical wells	Number of horizontal wells	Total WP	Predicted WP without new well	Predicted total WP with new wells
			(million	/ '!!' 111\	('11' 111)
			bbl)	(million bbl)	(million bbl)
1999	113	0	0.020		
2000	127	0	0.024		
2001	122	0	0.029		
2002	174	0	0.024		
2003	118	0	0.022		
2004	123	0	0.021		
2005	3,306	0	0.275		
2006	3,768	0	0.824		
2007	4,309	0	0.722		
2008	4,558	0	0.992		
2009	5,862	0	1.063		
2010	6,803	0	1.369		
2011	7,371	115	3.125	3.125	3.125
2012	7,571*	215*		2.273*	4.238*
2013	7,771*	315*		1.516*	5.352*
2014	7,971*	415*		1.214*	6.466*
2015	8,171*	515*		0.954*	7.580*
2016	8,371*	615*		0.914*	8.694*
2017	8,571*	715*		1.097*	9.808*

^{*} Predicted Value from 2012 to 2017, with 200 new vertical and 100 new horizontal wells each year