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WIND-TUNNEL STUDY OF
RESORTS HOTEL CASINO, ATLANTIC CITY

by

J. A. Peterka,¹ D. W. Boggs,²
and J. E. Cermak³



Engineering Sciences

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**FLUID MECHANICS AND
WIND ENGINEERING PROGRAM**

COLLEGE OF ENGINEERING

**COLORADO STATE UNIVERSITY
FORT COLLINS, COLORADO**

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WIND-TUNNEL STUDY OF
RESORTS HOTEL CASINO, ATLANTIC CITY

by

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and J. E. Cermak³

for

Resorts International

through

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<u>Symbol</u>	<u>Definition</u>
P_{∞}	Static pressure in wind tunnel above model
P^*	Generalized load
P_i	Resultant force of applied wind load acting at floor i
\bar{P}_i	Response (static equivalent) force acting at floor i
$\bar{P}_i, P_i', \hat{P}_i$	Mean, fluctuating, and expected peak values of P_i
q	Reference dynamic pressure, $\rho U_{\infty}^2/2$
$S_{()}(f)$	Power spectral density of ()
T_u	Turbulence intensity $\frac{U_{rms}}{U_{\infty}}$ or $\frac{U_{rms}}{U}$
U	Local mean velocity
U_{pk}	Effective peak velocity = $U + 3(U_{rms})$
U_{∞}	Reference mean velocity outside the boundary layer
U_{rms}	Root-mean-square of fluctuating velocity
x, y	Horizontal coordinates
z	Height above surface
z_i	Height of floor i
α	Approach wind azimuth
δ	Height of boundary layer
Δ_i	Lateral displacement of floor i
$\bar{\Delta}_i, \Delta_i', \hat{\Delta}_i$	Mean, fluctuating, and expected peak values of Δ
ν	Kinematic viscosity of approach flow
ρ	Density of approach flow
σ_M	Standard deviation of $M, = M'_{rms}$
σ_{P_i}	Standard deviation of $P_i, = (P_i')_{rms}$
σ_{Δ_i}	Standard deviation of $\Delta_i, = (\Delta_i')_{rms}$

<u>Symbol</u>	<u>Definition</u>
θ	Rotation of a straight line approximating the building displacement
θ'	Fluctuating rotation, approximates the generalized coordinate ξ
ϕ	Modal deflection
ζ	Critical damping ratio
ξ	Generalized response

1. INTRODUCTION

1.1 General

A significant characteristic of modern building design is lighter cladding and more flexible frames. These features produce an increased vulnerability of glass and cladding to wind damage and result in larger deflections of the building frame. In addition, increased use of pedestrian plazas at the base of the buildings has brought about a need to consider the effects of wind and gustiness in the design of these areas.

The building geometry itself may substantially influence the wind loading on the structure. Wind forces may be modified by nearby structures which can produce beneficial shielding or adverse increases in loading. Overestimating loads results in uneconomical design; underestimating may result in cladding or glazing failures. Tall structures have historically produced unpleasant wind and turbulence conditions at their bases. The intensity and frequency of objectionable winds in pedestrian areas is influenced both by the structure shape and by the shape and position of adjacent structures. In flexible structures, wind-induced motion may cause occupant discomfort if not anticipated during the design phase.

Techniques have been developed for wind-tunnel modeling of proposed structures which allow the prediction of wind pressures on cladding and windows, overall structural loading, and also wind velocities and gusts in pedestrian areas adjacent to the building. Information on sidewalk-level gustiness allows plaza areas to be protected by design changes before the structure is constructed. Accurate knowledge of the intensity and distribution of the pressures on the structure permits adequate but economical selection of cladding strength to meet selected

maximum design winds and overall wind loads for the design of the frame for flexural control.

Modeling of the aerodynamic loading on a structure requires special consideration of flow conditions in order to guarantee similitude between model and prototype. A detailed discussion of the similarity requirements and their wind-tunnel implementation can be found in references [1], [2], and [3]. In general, the requirements are that the model and prototype be geometrically similar, that the approach mean velocity at the building site have a vertical profile shape similar to the full-scale flow, that the turbulence characteristics of the flows be similar, and that the Reynolds number for the model and prototype be equal.

These criteria are satisfied by constructing a scale model of the structure and its surroundings and performing the wind tests in a wind tunnel specifically designed to model atmospheric boundary-layer flows. Reynolds number similarity requires that the quantity UD/ν be similar for model and prototype. Since ν , the kinematic viscosity of air, is identical for both, Reynolds numbers cannot be made equal with reasonable wind velocities. To accomplish this the air velocity in the wind tunnel would have to be as large as the model scale factor times the prototype wind velocity, a velocity which would introduce unacceptable compressibility effects. However, for sufficiently high Reynolds numbers ($>2 \times 10^4$) the pressure coefficient at any location on the structure will be essentially constant for a large range of Reynolds numbers. Typical values encountered are 10^7 - 10^8 for the full-scale and 10^5 - 10^6 for the wind-tunnel model. In this range acceptable flow similarity is achieved without precise Reynolds number equality.

Modeling of the building's dynamic response required that dynamic tests of the structure be performed. A three degrees-of-freedom model was assumed and scaled for the wind-tunnel conditions. Requirements for similarity between model and full-scale building for the dynamic model are discussed in references [3], [4], and [5]. For the dynamic tests, a rigid model was elastically supported by springs at its base. The springs permitted rotation of the model around two orthogonal axes located in the horizontal plane, and about a vertical axis. The natural frequencies of the three degrees of freedom of the model were significantly higher than the frequencies in the aerodynamic loading spectrum of the wind-induced forces. This enabled direct measurement of the fluctuating wind loads on the building. Mathematical computation using dynamic properties of the full-scale building in combination with wind-tunnel measurements of loading spectra allowed the building response to be determined.

1.2 The Wind-Tunnel Test

The wind engineering study was performed on the Resorts Hotel Casino building group modeled at a scale of 1:300. The rigid building models for pressure data acquisition were constructed of clear plastic fastened together with screws. The structure was modeled in detail to provide accurate flow patterns in the wind passing over the building surfaces. To achieve similarity in wind effects, the area surrounding the test building was also modeled. A flow visualization study was made (using smoke to make the air currents visible) to define overall flow patterns and identify regions where local flow features might cause difficulties in building curtain-wall design or produce pedestrian discomfort.

The pressure test models, equipped with pressure or "piezometer" taps, were exposed to an appropriately modeled atmospheric wind in the wind tunnel and the fluctuating pressure at each tap measured electronically. The model, and the modeled area, were rotated 10 degrees and another set of data recorded for each pressure tap. The entire 360-degree range was covered at 10-degree intervals.

Data were recorded, analyzed and processed by an on-line computerized data-acquisition system. Pressure coefficients of several types were calculated by the computer for each reading on each piezometer tap and were printed in tabular form as computer readout. Using wind data applicable to the building site, representative wind velocities were selected for combination with measured pressures on the building model. Integration of test data with wind data resulted in prediction of peak local wind pressures for design of glass or cladding. Overall mean forces and moments on the structure were obtained by integrating the mean pressures over the building's surface. Pressure contours were drawn on the developed building surfaces showing the intensity and distribution of peak wind loads on the building. These results may be used to divide the building into zones where lighter or heavier cladding or glass may be desirable.

Based on the visualization (smoke) tests and on a knowledge of heavy pedestrian use areas, locations were chosen at the base of the building where wind velocities were measured to determine the relative comfort or discomfort of pedestrians in plaza areas, near building entrances, near building corners, or on sidewalks. A reference pedestrian position was also tested to determine whether the wind environment in the building area is better or worse than the environment a block or so away in an undisturbed area.

The dynamic response of the building was evaluated using the dynamic model, which was instrumented to sense fluctuating base moments. These measurements were made for each of 36 wind directions to determine building response sensitivity to different wind directions. Several wind directions were selected to remeasure the fluctuating base moments in the presence of possible future buildings. The dynamic load information obtained by the dynamic model was combined with structural characteristics of the tower provided by the sponsor to predict building dynamic response, including response base moments, top floor deflections, and top floor accelerations.

The following pages discuss in greater detail the procedures followed and the equipment and data collecting and processing methods used. In addition, the data presentation format is explained and the implications of the data are discussed.

2. EXPERIMENTAL CONFIGURATION

2.1 Wind Tunnel

Wind engineering studies are performed in the Fluid Dynamics and Diffusion Laboratory at Colorado State University (Figure 1). Three large wind tunnels are available for wind loading studies depending on the detailed requirements of the study. The wind tunnel used for this investigation is shown in Figure 2. The tunnel has a flexible roof adjustable in height to maintain a zero pressure gradient along the test section. The mean velocity can be adjusted continuously in the tunnel to the maximum velocity available.

2.2 Pressure Model

In order to obtain an accurate assessment of local pressures using piezometer taps, models are constructed to the largest scale that does

not produce significant blockage in the wind-tunnel test section. The models were constructed of 1/2-in. (1.3 cm) thick acrylic plastic and fastened together with metal screws. Significant variations in the building surface were machined into the plastic. Piezometer taps (1/16 in. (1.6 mm) diameter) were drilled normal to the exterior vertical surfaces in rows at a number of elevations between the bottom and top of the building. Similarly, taps were placed in the roof and on sloping, protruding, or otherwise distinctive features of the building that might need investigation.

Pressure tap locations were chosen so that the entire surface of the building could be investigated for pressure loading and at the same time permit critical examination of areas where experience has shown that maximum wind effects may be expected to occur. Locations of the pressure taps for this study are shown in Figure 3. Dimensions are given both for full-scale building (in ft) and for model (in in.). The pressure tap numbers are shown adjacent to the taps.

The pressure tests are sometimes made in two stages. In the first stage, measurements are made on the initial distribution of pressure taps. If it becomes apparent from the data that the loading on the building is being influenced by some unsuspected geometry of the building or adjacent structures, additional pressure taps are installed in the critical areas. The locations of the taps are selected so that the maximum loading can be detected and the area over which this loading is acting can be defined. Any added taps are also shown in Figure 3.

Photographs of the pressure model installed in the wind tunnel are shown in Figure 4.

2.3 Dynamic Model

The dynamic model was designed to study the dynamic response of the fundamental mode of vibration of the tower in three independent components: translation in two orthogonal directions, and rotation about a vertical axis. To accomplish this, in each component the structure is reduced to an equivalent single-degree-of-freedom (SDOF) system using the modal analysis technique of generalized coordinates. This procedure is described in Appendix C. The equivalent SDOF system is characterized by a generalized mass m^* , generalized stiffness k^* , generalized load P^* , and generalized response ξ . A linear mode shape is assumed, for which the test models used represent an exact analogy. For this case, it is shown in Appendix C that the corresponding model properties to the above generalized values are mass moment of inertia I , rotational stiffness k_θ , externally-applied base moment M , and axis rotation θ .

The dynamic properties of generalized mass, generalized stiffness, and natural frequency assumed in this study are given in Table 8. (The coordinate system is defined in Figure 5.) The natural frequency f_0 and mass matrix $[m]$ were specified by Paulus, Sokolowski and Sartor personnel. The generalized mass m^* , or moment of inertia I , was calculated using Equation (C.4). The generalized stiffness k^* , or rotational stiffness k_θ was then calculated using Equation (C.3).

The construction of the dynamic model and balance system is shown in Figure 6. The model was built up of aluminum and magnesium and mounted on a 1 1/2-in. diameter steel tube. The tube was bolted to the balance plate as shown, and provided the high rigidity required to respond as an SDOF system at a high natural frequency. The balance

plate was connected to a heavy steel reaction ring via necked-down sections of steel crossbeams. These "springs" deform in both the horizontal and vertical planes, and thus provide three components of motion-rotation about the x, y, and z axes shown.

The dynamic balance was instrumented with strain gages to measure the base moment M, or generalized load P*, about these three axes. Scaling was accomplished by expressing this load as a moment coefficient, defined as

$$C_M = \frac{M}{q A L}$$

where q is the dynamic reference pressure $\rho U_\infty^2/2$, A is a reference area, and L is a characteristic reference length such as the height of the building. Measured coefficients are applicable to both the model and prototype.

Once the generalized load is determined, its power spectral density $S_M(f)$ is computed (Appendix C). The fluctuating mean square of the response base moment can then be computed by combining equations (C.7) and (C.9):

$$\sigma_M^2 = \int_0^\infty S_M(f) df = \int_0^\infty |H(f)|^2 S_M(f) df$$

All of the essential dynamic properties of the building are incorporated in $|H(f)|^2$, the mechanical admittance:

$$|H(f)|^2 = \frac{1}{[1-(f/f_0)^2]^2 + (2\zeta f/f_0)^2}$$

where f_0 is the natural frequency, and ζ is the critical damping ratio.

An accepted procedure in the present context is to use the so-called white noise approximation; then

$$\sigma_M^2 = S_M(f_o) \int_0^{\infty} |H(f)|^2 df$$

This integration can be performed analytically, with the result

$$\sigma_M^2 = \frac{\pi}{4\xi} f_o S_M(f_o) \quad (5)$$

The square root of this is the desired rms dynamic response σ_M . Note that any value of natural frequency f_o and damping ratio ξ may be incorporated after the test results, $S_M(f)$, are obtained.

2.4 Model Environment

A circular area of 1300 ft (400 m) in radius surrounding the building was modeled in detail. Structures within the modeled region were made from styrofoam and cut to the individual building geometries. The model and its surroundings were mounted on a turntable (Figure 2) near the downwind end of the test section. Any significant buildings or terrain features which did not fit on the turntable were placed on removable pieces and placed upwind of the turntable for appropriate wind directions. A plan view of the building and its surroundings is shown in Figure 7. This environment was used for the pressure model and the dynamic model.

The region upstream from the modeled area was covered with a randomized roughness constructed using various sized cubes placed on the floor of the wind tunnel. Spires were installed at the test-section entrance to provide a thicker boundary layer than would otherwise be available. The thicker boundary layer permitted a somewhat larger scale model than would otherwise be possible. The spires were approximately triangularly-shaped pieces of 1/2-in. (1.3 cm) thick plywood 6 in.

(15 cm) wide at the base and 1 in. (2.5 cm) wide at the top, extending from the floor to the top of the test section. They were placed so that the broad side intercepted the flow. A barrier approximately 8 in. (20 cm) high was placed on the test-section floor downstream of the spires to aid in development of the boundary-layer flow.

The distribution of the roughness cubes and the spires in the roughened area was designed to provide a boundary-layer thickness of approximately 4 ft (1.2 m), and a velocity profile power-law exponent similar to that expected to occur in the region approaching the modeled area for each wind direction. Photographs of the completed pressure model in the wind tunnel are shown in Figure 4. The wind-tunnel ceiling was adjusted after placement of the model to obtain a zero pressure gradient along the test section.

3. INSTRUMENTATION AND DATA ACQUISITION

3.1 Flow Visualization

Making the air flow visible in the vicinity of the model is helpful (a) in understanding and interpreting mean and fluctuating pressures, (b) in defining zones of separated flow and reattachment and zones of vortex formation where pressure coefficients may be expected to be high, (c) in interpretation of building dynamic response, and (d) in indicating areas where pedestrian discomfort may be a problem. Titanium tetrachloride smoke was released from sources on and near the model to make the flow lines visible to the eye and to make it possible to obtain motion picture records of the tests. Conclusions obtained from these smoke studies are discussed in Sections 4.1 and 5.1.

3.2 Pressures

Mean and fluctuating pressures were measured at each of the pressure taps on the model structure. Data were obtained for 36 wind

directions, rotating the entire model assembly in a complete circle. Up to 184 pieces of 1/16 in. (1.6 mm) I.D. plastic tubing were used to connect 184 pressure ports at a time to four 48-tap pressure switches mounted underneath the model. The switches were designed to minimize the attenuation of pressure fluctuation across the switch. Each of the 184 measurement ports was directed in turn by the switch to one of four pressure transducers mounted close to the switch. Four pressure input ports not used for transmitting building surface pressures were connected to a common tube leading to a pitot tube mounted inside the wind tunnel which provided a means of automatically monitoring the tunnel speed. The switch was operated under control of the data acquisition system. The other four input ports were used for monitoring of the transducer zero.

The pressure transducers used were Setra differential transducers (Model 237) with a 0.10 psid (690 Pad) range. Reference pressures were obtained by connecting the reference sides of the four transducers, using plastic tubing, to the static side of a pitot-static tube mounted in the wind-tunnel free stream above the model building. In this way the transducer measured the instantaneous difference between the local pressures on the surface of the building and the static pressure in the free stream above the model.

Output from the pressure transducers was fed to an on-line data acquisition system consisting of a Hewlett-Packard 21 MX computer, disc unit, card reader, printer, Digi-Data digital tape drive and a Preston Scientific analog-to-digital converter. The data were processed immediately into pressure coefficient form as described in Section 4.3 and stored for printout or further analysis.

All four transducers were recorded simultaneously for 16 seconds at a 250 sample-per-second rate. The results of an experiment to determine the length of record required to obtain stable mean and rms (root-mean-square) pressures and to determine the overall accuracy of the pressure data acquisition system is shown in Figure 8. A typical pressure port record was integrated for a number of different time periods to obtain the data shown. Examination of a large number of pressure taps showed that the overall accuracy for a 16-second period is, in pressure coefficient form, 0.03 for mean pressures, 0.1 for peak pressures, and 0.01 for rms pressures. Pressure coefficients are defined in Section 4.3.

3.3 Wind Velocity

Mean velocity and turbulence intensity profiles were measured upstream of the model, using a hot-film anemometer, to confirm that an approach boundary-layer flow appropriate to the site had been established. Tests were made at one wind velocity in the tunnel. This velocity was well above that required to satisfy Reynolds number similarity between the model and the prototype as discussed in Section 1.1.

In addition, mean velocity and turbulence intensity measurements were made 5 to 7 ft (1.5 to 2.1 m) (prototype) above the surface at 20 or more locations near the building for 16 wind directions. The measurement locations are shown on Figure 7. The surface measurements are indicative of the wind environment to which a pedestrian at the measurement location should be subjected. The locations were chosen to determine the degree of pedestrian comfort or discomfort at the building corners where relatively severe conditions frequently are found, near building entrances and on adjacent sidewalks where pedestrian traffic is

heavy, and in open plaza areas. A reference pedestrian position, located away from the building, was also tested. This data is helpful in evaluating the degree of pedestrian comfort or discomfort in the proposed plaza area in terms of the undisturbed environment in the immediate vicinity.

The pedestrian-level measurements were made with a single hot-film anemometer mounted with its axis vertical. The instrumentation used is a TSI constant temperature anemometer (Model 1050) with a 0.001 in. (0.025 mm) diameter platinum film sensing element 0.020 in. (0.508 mm) long. Output is directed to the on-line data acquisition system for analysis.

Calibration of the hot-film anemometer was performed by comparing output with the pitot-static tube in the wind tunnel. The calibration data were fit to a variable exponent King's Law relationship of the form

$$E^2 = A + BU^n$$

where E is the hot-film output voltage, U the velocity and A , B , and n are coefficients selected to fit the data. The above relationship was used to determine the mean velocity at measurement points using the measured mean voltage. The fluctuating velocity in the form U_{rms} (root-mean-square velocity) was obtained from

$$U_{\text{rms}} = \frac{2 E E_{\text{rms}}}{B n U^{n-1}}$$

where E_{rms} is the root-mean-square voltage output from the anemometer. For interpretation all turbulence measurements for pedestrian winds were divided by the mean velocity outside the boundary-layer U_{∞} . Turbulence intensity in velocity profile measurements, however, used the local mean velocity as a reference.

3.4 Base Moments

The spring elements in the balance fixtures for the dynamic model (see Figure 6) were instrumented with strain gages to sense the rotation of the model. The spring deformations are very small, so semiconductor gages (BLH-type SPB3-07-35), which have a much higher sensitivity than standard foil gages, were used.

The strain gages were formed into three bridge networks--one for each of the three degrees-of-freedom of the building motion. These bridges were conditioned and monitored by Honeywell Accudata 218 Gage Control/Amplifier units which provided excitation to the bridge and amplification of the bridge output. These signals were processed through the on-line data-acquisition system described earlier. The output signal was converted to a moment value using the results of a static calibration of the balance.

During test runs data were taken at a sample rate of 125 samples per second on each channel. The sample duration time was selected on the basis of repeatability of sampling runs made early in the testing phase, and corresponds to about 1 hour at full scale. The data were processed immediately to determine mean, rms, and peak loads. The data were also stored on digital tape for further analysis.

4. RESULTS

4.1 Flow Visualization

A film is included as part of this report showing the characteristics of flow about the structure using smoke to make the flow visible. A listing of the contents of the film is shown in Table 1. Several features can be noted from the visualization. As with all large structures, wind approaching the building is deflected down to the plaza

level, up over the structure and around the sides. A description of the smoke test results emphasizing flow patterns of concern relative to possible high-wind load areas and pedestrian comfort is given in Section 5.1.

4.2 Velocity

Velocity and turbulence profiles are shown in Figure 9. Profiles were taken upstream from the model which are characteristic of the boundary layer approaching the model. The boundary-layer thickness, δ , is shown in Figure 9. The corresponding prototype value of δ for this study is also shown in the figure. This value was established as a reasonable height for this study. The mean velocity profile approaching the modeled area has the form

$$\frac{U}{U_{\infty}} = \left(\frac{Z}{\delta}\right)^n .$$

The exponent n for the approach flow established for this study is shown in Figure 9.

Profiles of longitudinal turbulence intensity in the flow approaching the modeled area are also shown in Figure 9. The turbulence intensities are appropriate for the approach mean velocity profile selected. For the velocity profiles, turbulence intensity is defined as the root-mean-square about the mean of the longitudinal velocity fluctuations divided by the local mean velocity U ,

$$T_u = \frac{U_{rms}}{U}$$

Velocity data obtained at each of the pedestrian measurement locations shown in Figure 7 are listed in Table 2 as mean velocity U/U_{∞} , turbulence intensity U_{rms}/U_{∞} , and largest effective gust

$$\frac{U_{pk}}{U_{\infty}} = \frac{U + 3U_{rms}}{U_{\infty}} .$$

These data are plotted in polar form in Figure 10. Measurements were taken 5 to 7 ft (1.5 to 2.1 m) above the ground surface. A site map is superimposed on the polar plots to aid in visualization of the effects of the nearby structures on the velocity and turbulence magnitudes. An analysis of these wind data is given in Section 5.2.

To enable a quantitative assessment of the wind environment, the wind-tunnel data were combined with wind frequency and direction information obtained at the local airport. Table 3 shows local wind frequency by direction and magnitude. These data, usually obtained at an elevation of about 30-40 ft (9 to 12 m), were converted to velocities at the reference velocity height for the wind-tunnel measurements and combined with the wind-tunnel data to obtain cumulative probability distributions (percent time a given velocity is exceeded) for wind velocity at each measuring location. The percentage times were summed by wind direction to obtain a percent time exceeded at each measuring position independent of wind direction (but accounting for the fact that the wind blows from different directions with varying frequency). These results are plotted in Figure 11.

Interpretation of Figure 11 is aided by a description of the effects of wind of various magnitudes on people. The earliest quantitative description of wind effects was established by Sir Francis Beaufort in 1806 for use at sea and is still in use today. Several recent investigators have added to the knowledge of wind effects on pedestrians. These investigations along with suggested criteria for acceptance have been summarized by Penwarden and Wise [6] and Melbourne [7]. The Beaufort scale (from reference 6), based on mean velocity only, is reproduced as Table 4 including qualitative descriptions of

wind effects. Table 4 suggests that mean wind speeds below 12 mph (5.4 m/s) are of minor concern and that mean speeds above 24 mph (10.8 m/s) are definitely inconvenient. Quantitative criteria for acceptance from reference [7] are superimposed as dashed lines on Figure 11. The peak gust curves shown in Figure 11 are the percent of time during which a short gust of the stated magnitude could occur (say about one of these gusts per hour). Implications of the data plotted in Figure 11 are presented in Section 5.2.

Because some pedestrian wind measuring positions are purposely chosen at sites where the smoke test showed large velocities of small spatial extent, the general wind environment about the structure may be less severe than one might infer from a strict analysis of Table 2 and Figure 11.

4.3 Pressures

For each of the pressure taps examined at each wind direction, the data record was analyzed to obtain four separate pressure coefficients. The first is the mean pressure coefficient

$$C_{p_{\text{mean}}} = \frac{(p-p_{\infty})_{\text{mean}}}{q}$$

It represents the mean of the instantaneous pressure difference between the building pressure tap and the static pressure in the wind tunnel above the building model, nondimensionalized by the dynamic pressure

$$q = \rho U_{\infty}^2 / 2$$

at the reference velocity position. This relationship produces a dimensionless coefficient which indicates that the mean pressure difference between building and ambient wind at a given point on the structure is some fraction less or some fraction greater than the undisturbed

wind dynamic pressure near the upper edge of the boundary layer. Using the measured coefficient, prototype mean pressure values for any wind velocity may be calculated.

The magnitude of the fluctuating pressure is obtained by the rms pressure coefficient

$$C_{p_{rms}} = \frac{\left((p-p_{\infty}) - (p-p_{\infty})_{\text{mean}} \right)_{rms}}{q}$$

in which the numerator is the root-mean-square of the instantaneous pressure difference about the mean.

If the pressure fluctuations followed a Gaussian probability distribution, no additional data would be required to predict the frequency with which any given pressure level would be observed. However, the pressure fluctuations do not, in general, follow a Gaussian probability distribution so that additional information is required to show the extreme values of pressure expected. The peak maximum and peak minimum pressure coefficients are used to determine these values:

$$C_{p_{max}} = \frac{(p-p_{\infty})_{max}}{q}$$

$$C_{p_{min}} = \frac{(p-p_{\infty})_{min}}{q}$$

The values of $p-p_{\infty}$ which were digitized at 250 samples per second for 16 seconds, representing about one hour of time in the full-scale, are examined individually by the computer to obtain the most positive and most negative values during the 16-second period. These are converted to $C_{p_{max}}$ and $C_{p_{min}}$ by nondimensionalizing with the free stream dynamic pressure.

The four pressure coefficients are calculated by the on-line data acquisition system computer and tabulated along with the approach wind

azimuth in degrees from true north. The list of coefficients is included as Appendix A. The pressure tap code numbers used in the appendix are explained in Figure 3.

To determine the largest peak loads acting at any point on the structure for cladding design purposes, the pressure coefficients for all wind directions were searched to obtain, at each a pressure tap, the largest value of peak pressure coefficient. Table 6 provides these pressure coefficients and associated wind directions. Included in Section 5.3 is an analysis of the coefficients of Table 6 including the maximum values obtained and where they occurred on the building.

The pressure coefficients of Table 6 can be converted to full-scale loads by multiplication by a suitable reference pressure, q , selected for the field site. This value is the dynamic pressure associated with an hourly mean wind at the reference velocity measurement position at the edge of the boundary layer. In general, the method of arriving at a design reference pressure for a particular site involves selection of a design wind velocity, translation of the velocity to an hourly mean wind at the reference velocity location and conversion to a reference pressure. Selection of the design velocity can be made from statistical analysis of extreme wind data. The calculation of reference pressure for this study is shown in Table 5. The factor used in Table 5 to reduce gust winds to hourly mean winds is given in reference [9].

The reference pressure associated with the design hourly mean velocity at the reference velocity location can be used directly with the peak-pressure coefficients to obtain peak local design wind loads for cladding design. Local, instantaneous peak loads on the full-scale building suitable for cladding design were computed by multiplying the

reference pressure of Table 5 by the peak coefficients of Table 6 and are listed as peak pressure in that table. The maximum psf load given at each tap location is the absolute value of the maximum value found in the tests, irrespective of its algebraic sign. For ease in visualizing the loads on the structure, contours of equal peak pressures for cladding loads shown in Table 6 have been plotted on developed elevation views of the structure, Figure 12. For control of water infiltration from outside to inside, the largest positive (inward-acting) pressure of each tap location is tabulated in Table 6.

For glass design pressures, a glass load factor is used to account for the different duration between measured peak pressures and the one-minute loading commonly used in glass design charts. The design pressure used for glass is normally less than the peak pressures used for cladding design because of the static fatigue property of glass which can withstand higher pressures for short duration loads than for long duration loads. Recent research [10] indicates that the period of application of the peak pressures reported herein is about 5-10 seconds or less. If a glass design is based on these peak-pressure values, then a glass strength associated with this duration load should be used. Because glass design charts are normally based on some alternate load duration--usually one minute--then some reduction in peak loads should be made. An estimate of a load reduction factor can be obtained from an empirical relation of glass strength as a function of load duration. Current glass selection charts showing glass strength as a function of load duration [11] and older references [12] indicate the following load reduction factors:

	ref. 9	ref. 10
annealed float	0.80	0.81
heat strengthened	0.94	
tempered	0.97	0.98

Loadings appropriate for glass design can be computed by multiplying the peak-pressure loads of Table 6 by these load factors.

4.4 Mean Forces and Moments

Since the mean load on a structure is independent of its dynamic response, and therefore of any time scale in the model, measured mean values may be scaled to the prototype in the same manner as pressures. Thus if the mean pressure distribution is determined as described in the preceding section, the associated force acting on any part of the structure may be determined by integration. This has been done in a manner which results in the mean force acting at each floor level in the x and y directions, and the resultant torque about the z axis. The coordinate system is shown in Figure 5.

The mean forces and torques obtained at each floor were used to obtain load, shear, and moment diagrams for the building for each wind direction, Table 7. The shear distribution, in kips, was obtained by algebraic sum of all forces in each coordinate direction acting above the floor of interest. The load distribution, in psf, was obtained by dividing the forces by their contributing areas (listed in Table 7). Eccentricities were computed such that the product of the y force and x eccentricity minus the product of the x force and y eccentricity equaled the torque at that floor. The moment diagram, in 1000 kip-ft, was obtained by integration of the shear values so that the moment due to forces acting above the floor level of interest was

calculated. The sign of the moment was established by the right-hand rule about an x' , y' axis through the floor of interest. Moments about the z axis were calculated by summing the torques acting on all floors above the floor level of interest. Mean load, shear, and moment diagrams are shown in Figure 13 for several wind directions.

Mean base moments are also available from the dynamic model test results, as described in Section 2.3. A comparison is made of mean base moments from both methods in Figure 14, which shows the x , y , and z base moments plotted as a function of wind direction.

4.5 Total Base Moments

This section presents the results of the dynamic model tests. As described in Section 2.3, the moment at the base of the structure is treated as the fundamental response parameter. The "total" base moment is the sum of the mean and fluctuating parts. In particular, the test results will be analyzed in terms of the maximum (or minimum) expected peak response. Section 4.6 will describe how these results may be used to estimate the distribution of equivalent static loads at each floor level.

The peak response base moment for a given wind direction α can be expressed as (see Equation (C.10))

$$\hat{M}(\alpha) = \bar{M}(\alpha) + g\sigma_M(\alpha)$$

where \hat{M} , \bar{M} , and σ_M are observed peak, mean, and fluctuating rms values, respectively, of the base moment determined by procedures described above. The "peak factor" g was determined from Equation (C.11), and σ_M was computed according to equation (5).

Peak base moments \hat{M} were calculated for each degree of freedom at each wind direction. The results are given in Figure 15. The wind

velocity for these results corresponds to the 100-year mean recurrence interval conditions described in Table 5. The damping ratio in the structure, ζ , is assumed to be .01 (1 percent of critical). The peak factors g are indicated as "PF." The peak values shown may be interpreted as "the expected value of the largest peak excursion in (static equivalent) response base moment occurring in a 1-hour period during the wind storm which occurs, on the average, every 100 years."

4.6 Force Distribution with Height

If the total response (or static equivalent) force acting at the i th floor is expressed as the sum of a mean and a fluctuating component, i.e.,

$$P_i = \bar{P}_i + P'_i$$

then, in a manner analogous to that used for the base moment in the previous section, the peak expected force may be written

$$\hat{P}_i = \bar{P}_i + g \sigma_{P_i} \quad (4.1)$$

where g is the same peak factor which was determined for the base moment. The distribution of the mean forces \bar{P}_i (which are the same as P_i) was discussed in Section 4.4, and the results appear in Table 7. In this section a means of estimating the rms fluctuating forces σ_{P_i} will be described. Reference is made to Appendix C concerning modal analysis concepts.

Since the structure's motion is essentially in a normal mode, the fluctuating equivalent static load at floor i is proportional to the mass and the modal deflection at that floor. If the modal deflection ϕ_i is approximated by the straight line z_i , then this force may be written

$$P'_i = \alpha m_i z_i$$

These forces can be related to the base moment M , since

$$M' = \sum P'_i z_i .$$

Substituting for P'_i leads to

$$M' = \alpha \sum m_i z_i^2 = \alpha m^* .$$

where m^* is the generalized mass (see Table 8). This allows the proportionality constant α to be evaluated, and the equation above for P'_i becomes

$$P'_i = \frac{M'}{m^*} m_i z_i .$$

This equation shows that the individual fluctuating floor loads, P'_i , may be determined from the fluctuating base moment, M' . The rms forces can now be expressed as

$$\sigma_{P'_i} = \frac{m_i z_i}{m^*} \sigma_M . \quad (4.2)$$

A simpler approximation may be obtained by assuming that the mode shape ϕ_i approximates the static deflected shape. In this case the above analysis applies to the total response, not just the fluctuating part, so that P_i and M can be substituted for P'_i and M' . The expected peak forces then become

$$\hat{P}_i \cong \frac{m_i z_i}{m^*} \hat{M} . \quad (4.3)$$

The expected peak base moment \hat{M} may be read directly from Figure 15.

This approximation may not be good for wind directions where the mean response is a large fraction of the peak response, depending on how much the static deflected shape deviates from a straight line. Note, however, that in many cases the largest response occurs in the

cross-wind direction, where the mean response is very small; in these cases the approximation is excellent.

4.7 Displacement and Acceleration

Displacements of the tower may be treated in a manner analogous to the analysis of forces in the preceding section. Thus the peak expected lateral deflection at floor i is

$$\hat{\Delta}_i = \bar{\Delta}_i + g\sigma_{\Delta} \quad (4.4)$$

where $\bar{\Delta}$ is the mean static deflection, σ_{Δ} is the fluctuating rms deflection, and g is the peak factor introduced above. The mean displacements can be obtained from a static analysis of the structural frame under the applied loads P_i (see Section 4.4). The dynamic displacements are obtained from Equation (C.2),

$$\Delta'_i = \theta' \phi_i$$

where θ' is the fluctuating rotation of the approximate straight-line mode shape of the structure (thus θ' approximates the generalized coordinate ξ). By Appendix C,

$$\theta' = \frac{M'}{k_{\theta}}$$

Combining these equations and taking the rms value results in

$$g\sigma_{\Delta_i} = \frac{1}{k_{\theta}} g\sigma_M z_i \quad (4.5)$$

where z_i is taken as an approximation to the actual shape ϕ_i . The rotational stiffness k_{θ} is given in Table 8, and the value $g\sigma_M$ may be read from Figure 16 or 17.

In the preceding section regarding force distributions, a simplifying assumption was made that the static deflected shape can be approximated by a straight line. This lead to the simple equation (4.3)

for the peak expected force. Parallel treatment of the displacements leads to

$$\hat{\Delta}_i = \frac{z_i}{k_\theta} \hat{M} \quad (4.6)$$

and
$$\theta = \frac{M}{k_\theta}$$

The value \hat{M} may be read directly from Figure 15. Note again that the accuracy of this approximation depends on how well the deflected shape can be fit by a straight line, and on the relative contributions of mean and fluctuating response to the total response. The equation is quite accurate for the cross-wind response, for example, where the mean response is zero.

Note also that the rotation θ is essentially the so-called "drift ratio." The expected peak value of this is

$$\hat{\theta} = \frac{\hat{M}}{k_\theta}$$

Using the proportionality constant $1/k_\theta$ from Table 8, an accessory scale for θ could be drawn directly on Figure 15.

Due to the high degree of resonance in the dynamic response of the towers, the displacement can be written in the general functional form

$$x(t) = X \sin \omega_0 t$$

where $\omega_0 = 2\pi f_0$ is the natural circular frequency. Differentiating this equation twice yields the following expression for acceleration:

$$\ddot{x}(t) = -\omega_0^2 \sin \omega_0 t = -\omega_0^2 x(t)$$

The root-mean-square acceleration may therefore be calculated as

$$\sigma_{\ddot{x}} = \omega_0^2 \sigma_x$$

In a similar manner, $\sigma_{\ddot{y}}$ and $\sigma_{\ddot{\theta}}$ can be calculated. The rotational acceleration $\ddot{\theta}$ is converted to a tangential acceleration at a representative point located at the corner of the top floor, at distance r from the z-axis:

$$\sigma_{r\ddot{\theta}} = r\sigma_{\ddot{\theta}}$$

The values $\sigma_{\ddot{x}}$, $\sigma_{\ddot{y}}$, and $\sigma_{r\ddot{\theta}}$ can then be combined using Equation (B.3) to obtain a characteristic total rms acceleration of the top floor.

Using this technique, the dynamic balance data have been converted to rms accelerations for two damping ratios. These are presented in Figure 17, along with some criteria describing human response to motion in tall buildings. This issue is discussed further in Section 5.5.

5. DISCUSSION

5.1 Flow Visualization

Flow patterns identified with smoke showed that the largest pressures would probably be found near corners of the tower due to flow separation phenomena. The wind flow tended to separate from the upwind corner of the balcony diagonals, an indication that high suction pressures might occur on the diagonal facing or on the inset walls of the balconies. Wind flow over the skylights projecting above the low-rise roof appeared to be strong enough to produce elevated suction pressures near corners of the skylights where flow might separate from the surface. Wind flow about the low rise did not appear to be particularly strong. Thus wind pressures on the low rise would be expected to be typical of buildings of that height set on the oceanfront. The presence of the tower did not appear to be a significant factor in increasing wind pressures on the low-rise structure.

Winds in pedestrian areas at ground level did not appear to be stronger than in adjacent areas. The boardwalk appeared to be about as windy in front of the Resorts project as on adjacent blocks. The overhead structure connecting the Resorts low rise to the Steel Pier did not appear to concentrate winds on the boardwalk underneath. Winds on the low-rise roof appeared to be stronger than at beach or boardwalk level and were quite strong and gusty near the tower base. Where high velocity winds were brought down to the low-rise roof by the tower, approaching winds tended to sweep the high-velocity winds across the roof so that, for some wind directions, much of the roof area appeared to be enveloped in strong, gusty winds.

The pedestrian area in the courtyard at the main entrance on the northwest side appeared to be moderate to low, although for a few wind directions, stronger winds appeared to penetrate down into that area.

5.2 Pedestrian Winds

Figure 7 shows the 21 locations selected for investigation of pedestrian wind comfort. Location 1 was selected as a reference location on the beach where wind conditions are well known locally and where influence of the Resorts Hotel Casino would be minor. Locations 2, 4-7, 10-14 and 21 were positioned on the roof of the low rise. Location 3 was in the pedestrian walkway at about ground level. Locations 9 and 18-20 were located at ground (or boardwalk) elevation under overhangs. Location 16 was on a connecting bridge over Pennsylvania Avenue.

Table 2 and Figure 10 show that the largest mean velocities were measured at locations 6, 7, 11 and 21 with values between 90 and 96 percent of U_{∞} , the velocity near the edge of the boundary layer at 700 ft. These values are quite high and are caused by the tower concentrating winds on the low-rise roof near the tower base. By

comparison, the largest mean velocity at reference location 1 was 53 percent of U_{∞} , while an open-country environment might expect 40-45 percent of U_{∞} .

The largest values of fluctuating velocity, U_{rms} , were measured at locations 2, 7 and 11 with values of 34, 28 and 28 percent of U_{∞} respectively. Values above 25 percent usually indicate a very gusty environment. The largest peak gusts, represented by the mean plus three rms as discussed in Section 4.2, were measured at locations 2, 6, 7, 11 and 21, all of which had values of 150 percent or more of U_{∞} . These peak gusts are quite high measured against typical city environments. Reference location 1 experienced peak gusts up to 106 percent of U_{∞} while an open-country environment might expect values of 80-90 percent of U_{∞} .

Velocity data of Table 2 integrated with local wind data listed in Table 3 are shown in Figure 11. Based on the data of this figure, the windiest locations should be 2, 7 and 21 which are predicted to exceed the acceptable limit by a wide margin. This area on the low-rise roof at the east end of the tower will not be suitable for any pedestrian activity for a large proportion of the time. Locations 6 and 10 on the low-rise roof are predicted to be slightly windier than reference location 1 on the beach. All other measured locations are predicted to be at or below the beach area in windiness. Several areas including locations 3, 8, 9, 15, 16 and 17 are predicted to be comfortable for long-duration activities a high percentage of time.

5.3 Pressures

Table 6 shows the largest peak pressure coefficients and corresponding loads measured on the building for each pressure tap

location. Data identified as Configuration A in Table 6 and Appendix A represent data obtained at all pressure tap locations on the tower and low rise for 36 wind directions without possible future towers in place. Configuration B data is the same except that several possible nearby future towers were included in the model (see Figure 7--buildings marked CONF B were added). Configurations C and D represent data obtained at selected taps at 2-degree azimuthal increments near azimuths where large pressure peaks were observed in Configurations A and B, respectively, to ensure that the largest peaks were obtained. Configuration W in Table 6 represents the highest peak pressures at each tap location from either Configuration A or B.

The largest peak pressures for combined Configurations A and B (Configuration W) were measured at tap locations 540 and 248 with values of -96 and -95 psf. Tap 540 was located on a corner diagonal where flow visualization showed the possibility of high suction pressures. Tap 248 was located where a small vortex could form for winds approaching the building face at an angle. This would be expected to be a small flow feature with a relatively small area of high pressure. Figure 12 shows the distribution of peak cladding pressures on the tower. Most of the area of the tower had negative peak pressures in the -40 to -60 psf range and positive pressures less than +40 psf. The low-rise portion of the project experienced significantly lower wind pressures except on the roof and skylights where local pressures up to -67 psf (skylights) and -85 psf (penthouse roof) were measured. The cladding pressures measured are consistent with the flow visualization studies.

Where doors open onto balconies, a possible increase in cladding load can exist. If a door is left open on high-wind days, the positive

or negative pressure which would otherwise act on the door is transmitted into the interior space to which the door is connected. This interior pressure can act to increase or decrease loading on cladding elements subjected to the interior pressure and to an exterior wind pressure. Where an increase in loading occurs, design load on cladding which is selected to withstand external wind loads only can be developed at wind speeds well below the design wind speed. This fact should be taken into account in the design of the cladding or in operation of the building (for example, insuring that the doors are closed on high-wind days).

5.4 Forces and Moments

Mean base moments in the tower referred to street level have been measured by two separate methods: spatial integration of mean pressure measurements, and dynamic balance measurements. A comparison of the two methods is shown in Figure 14 and the results are in excellent agreement. The distribution with height of load, shear and moment for two wind directions has been plotted in Figure 13 from Table 7 which lists mean load, shear and moment distributions in the tower for 36 wind directions.

Fluctuating base moments were obtained using the dynamic balance. Peak base moments were computed from

$$\hat{M} = \bar{M} + g\sigma_M$$

as described in Section 3.2 and Appendix C.

The peak base moments, along with the mean, are shown in Figure 15. These are response base moments which include both the applied wind load and the inertial response of the structure at its natural frequency. Dynamic measurements were made for 36 wind directions for

Configuration A without the possible future buildings in place and for a few selected wind directions for Configuration B with possible future buildings in place (see Figure 7) where it appeared that peak base moments might be larger. The building frequencies assumed to produce these peak base moments are shown in Table 8. A damping ratio of one percent of critical was assumed.

The results of Figure 15 show a consistent pattern. The x moment tends to follow a sinusoidal variation of moment with wind direction with a decrease in loading at an azimuth of 240 degrees where an existing building partially blocked the wind. The largest base moments occurred for wind perpendicular to the broad face in a buffeting mode. However, peak moments remained large for winds parallel to the long axis indicating a significant crosswind response. Peak base moments about the y axis peaked with the wind perpendicular to the broad face, where mean moment was near zero, indicating a strong crosswind response. The peak y moments occurred at the same wind directions as the peak x moments. Torsional moments showed characteristics typical of an airfoil with peak moments occurring for wind angles slightly away from an axial flow direction. Torsional moments were large, but not at their maximum level when x and y moments reached their largest values.

Mean and peak base shears were calculated and are presented in Figure 16. The distribution of peak loads with height in the tower can be calculated, if desired, using procedures outlined in Section 4.6.

5.5 Accelerations

It is generally agreed that acceleration provides the best measure of possible human discomfort due to motion in tall buildings; however, there is very little data available by which this issue can be judged

quantitatively. The best guidelines currently available are due to two research studies. Reed et al. [13] measured the acceleration response of two buildings in two separate storms, and evaluated the corresponding human response through questionnaires and interviews with the building's occupants. Conclusions were drawn as to how often the measured levels of acceleration could occur with a given level of objection. In the second study, Chen and Robertson [14] simulated an office environment with a cubicle which could be moved horizontally. The intent of this program was to determine the minimum level of acceleration which could be sensed by humans. This "threshold of perception" was found to vary with many factors, including inherent variation from person to person, whether the person had been previously conditioned to the type of motion, and the frequency of motion. A procedure was presented by which any desired threshold level--in terms of percentage of an average cross section of people representing--could be estimated, as a function of frequency.

Figure 17 shows how these research results compare to the predicted acceleration in the Resorts Hotel Casino. These graphs show various levels of total rms acceleration in the end rooms on the top floor plotted against the number of times per year that such a level is expected to occur, for two different damping ratios--the most likely value of 0.01 and a probable low value of 0.005.

The horizontal dashed lines in the lower right-hand corner represent acceleration levels, computed for the torsional natural frequency of the building (torsion produced the largest component to the acceleration), representing the lower limit of perception by 2 percent and 10 percent of the average population. The figures indicate that,

even at the lowest value of damping, 2 percent of the top floor occupants will be able to perceive the motion no more than one or two times per year in the top floor corner rooms for the most likely damping ratio. At no time should as many as 10 percent of the top floor occupants be able to perceive motion for a damping ratio of 0.01. If the damping ratio should be as low as 0.005, then 10 percent of room occupants might perceive motion as often as four times per year.

The solid data points so indicated represent suggested design criteria based on reference [13]. They represent top-floor acceleration levels at which 2 or 10 percent of the occupants in the top one-third of the building would find "objectionable" (as opposed to perceivable) if they occurred at the frequency indicated. According to this criteria, the motion may be objectionable to up to 10 percent of the occupants in the top one-third of the tower, if the damping ratio is as low as 0.5 percent. For a damping ratio of 1.0 percent, the motion may be objectionable to 2 to 3 percent of the occupants in the top one-third of the tower.

At very low frequencies of occurrence (i.e., high acceleration levels) no data are available by which to judge the human response issue. It is generally agreed, however, that performance-type criteria such as occupant comfort should be based on events which occur relatively frequently, say at least once per year.

In conclusion, therefore, the building motions are expected to be generally acceptable, even at a very low value of damping. At a more probable value of damping, the motion levels should be acceptable to more than 98 percent of the buildings' occupants. The motion should be perceivable, if at all, no more than twice per year for 2 percent of the

top floor corner occupants of the tower. Finally, it is cautioned that these conclusions are based on a very limited amount of research and field data, which nevertheless represent the best criteria available. It is expected that no problems should be experienced due to wind-induced motion.

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FIGURES

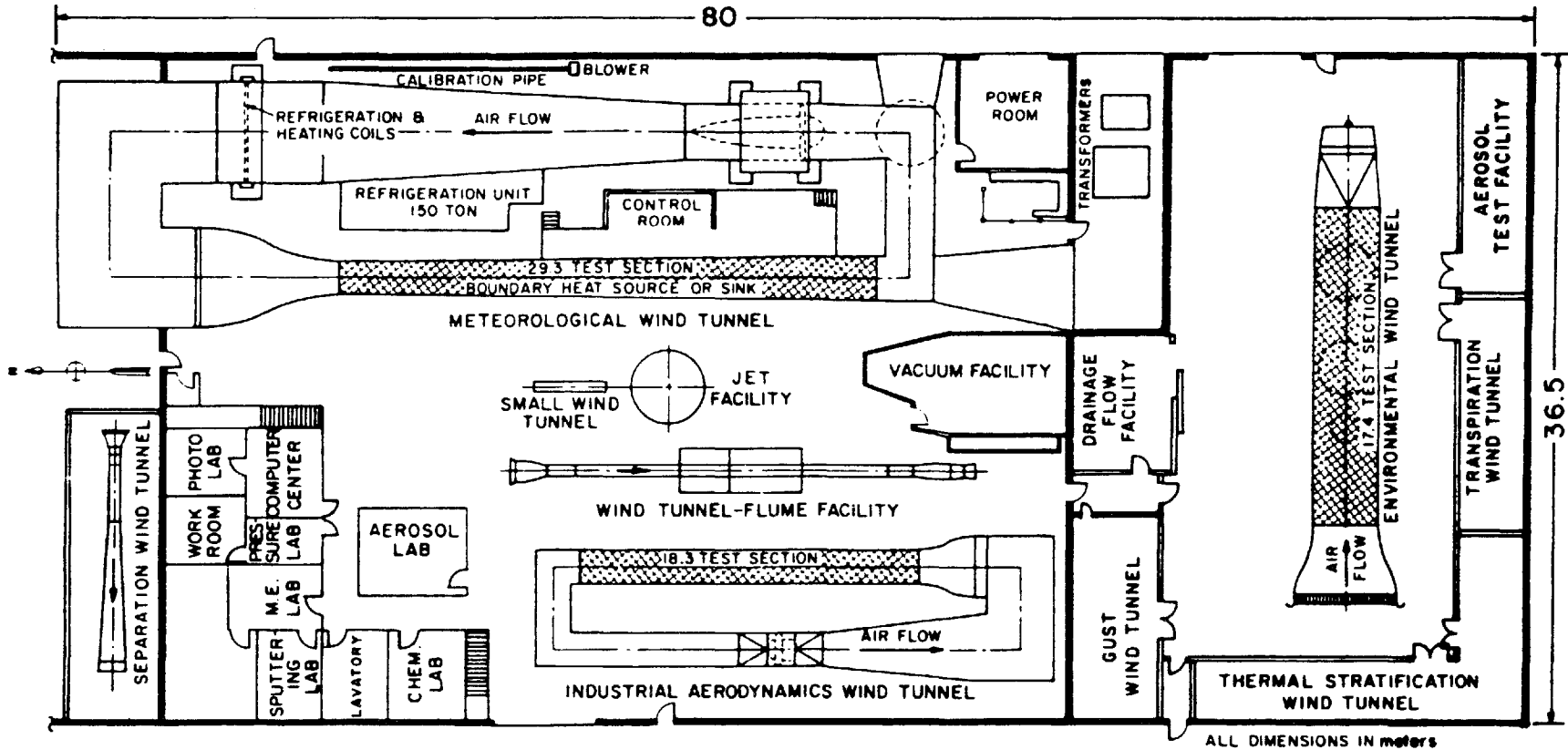
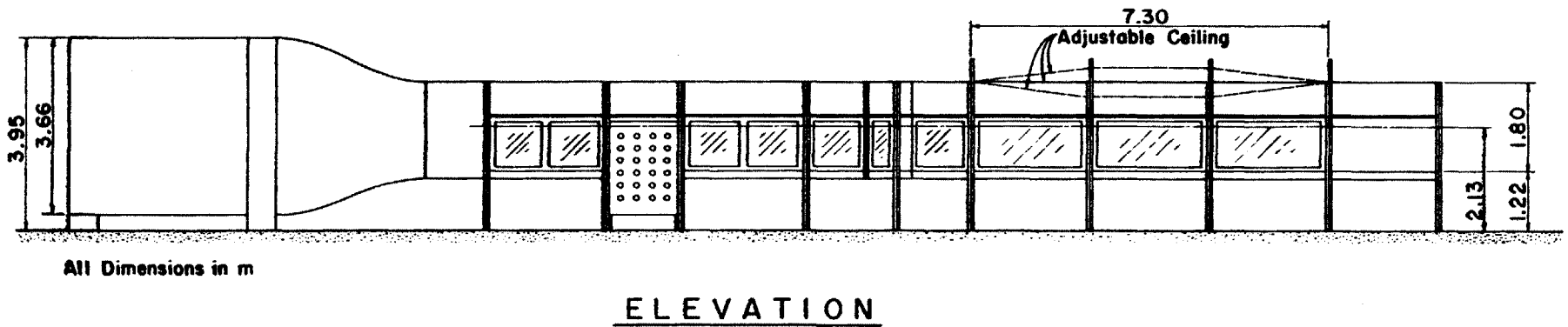
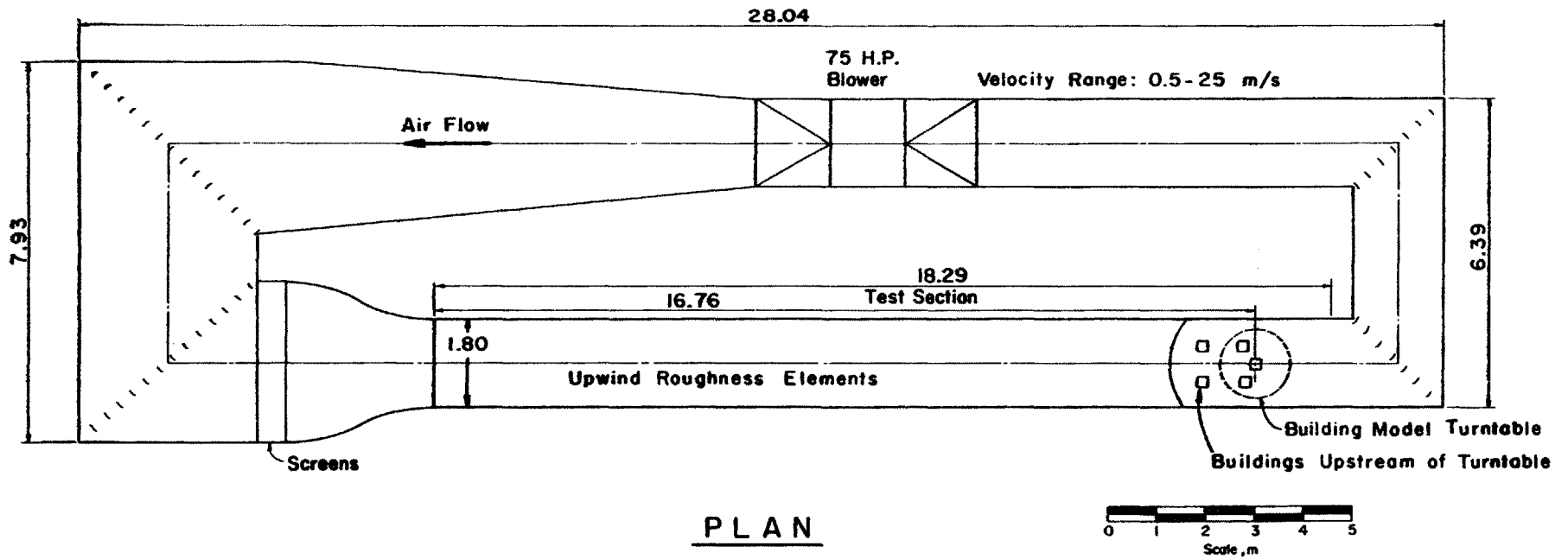
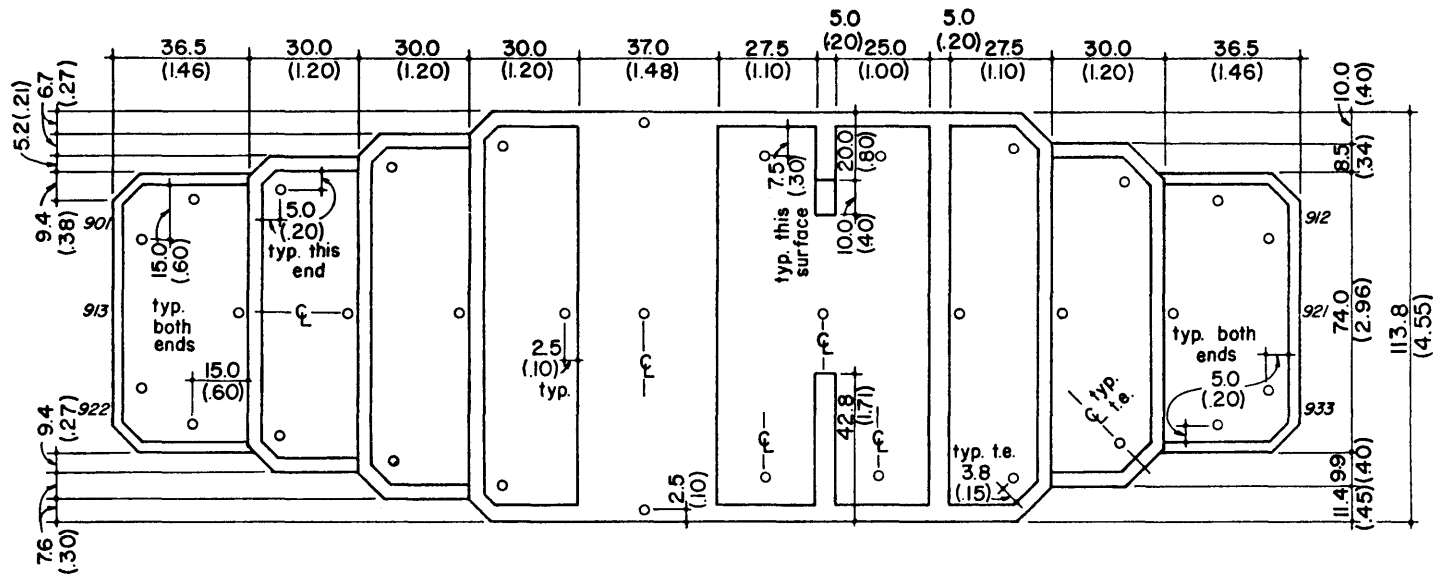


Figure 1. FLUID DYNAMICS AND DIFFUSION LABORATORY
COLORADO STATE UNIVERSITY

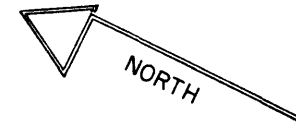


INDUSTRIAL AERODYNAMICS WIND TUNNEL

Figure 2. Wind-Tunnel Configuration



TOWER ROOF



Total taps = 435
 Model scale is 1/300
 Dimensions in model inches and full scale feet

Note:
 Angles are 45°

Figure 3a. Pressure Tap Locations

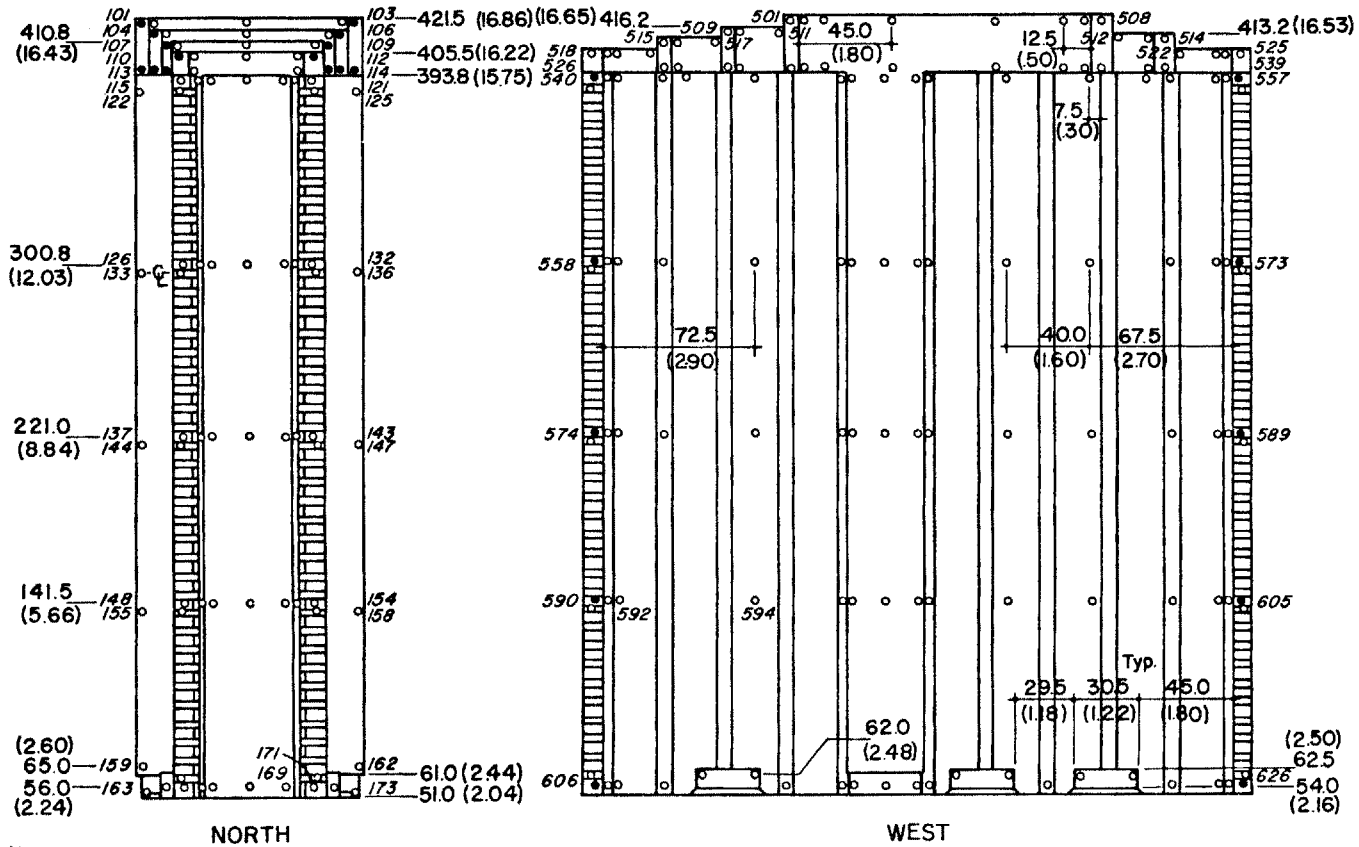
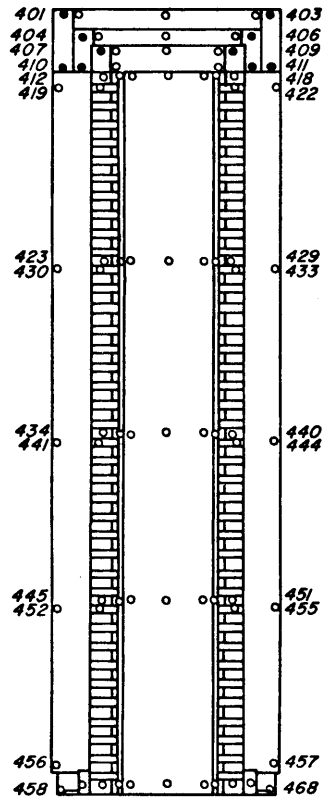
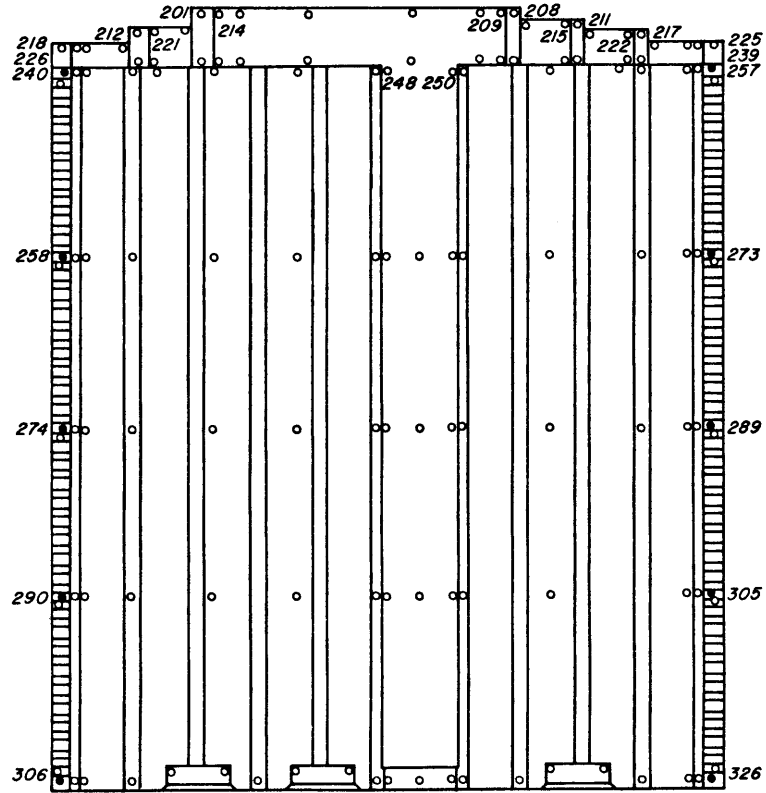


Figure 3b. Pressure Tap Locations



SOUTH



EAST

Figure 3c. Pressure Tap Locations

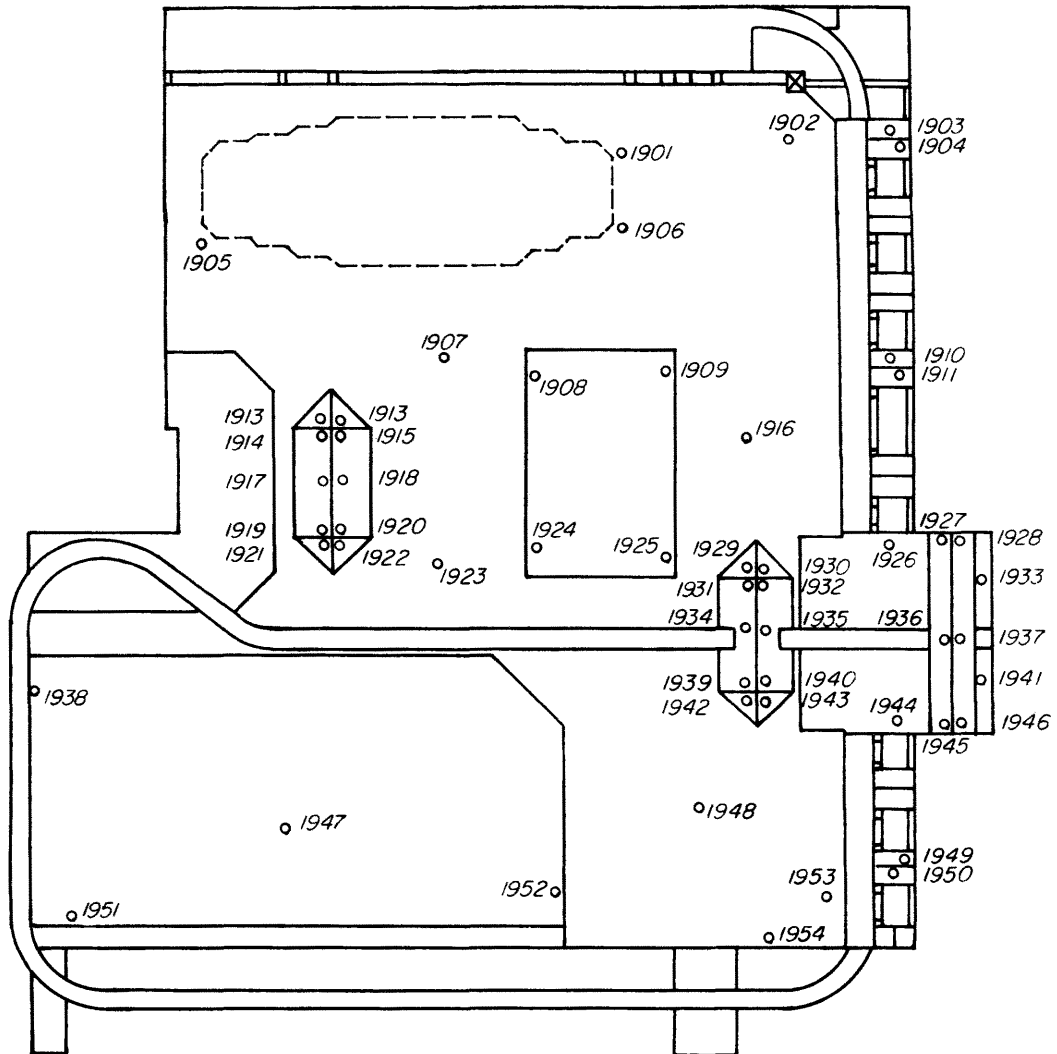
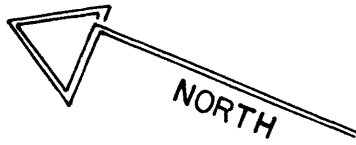


Figure 3d. Pressure Tap Locations

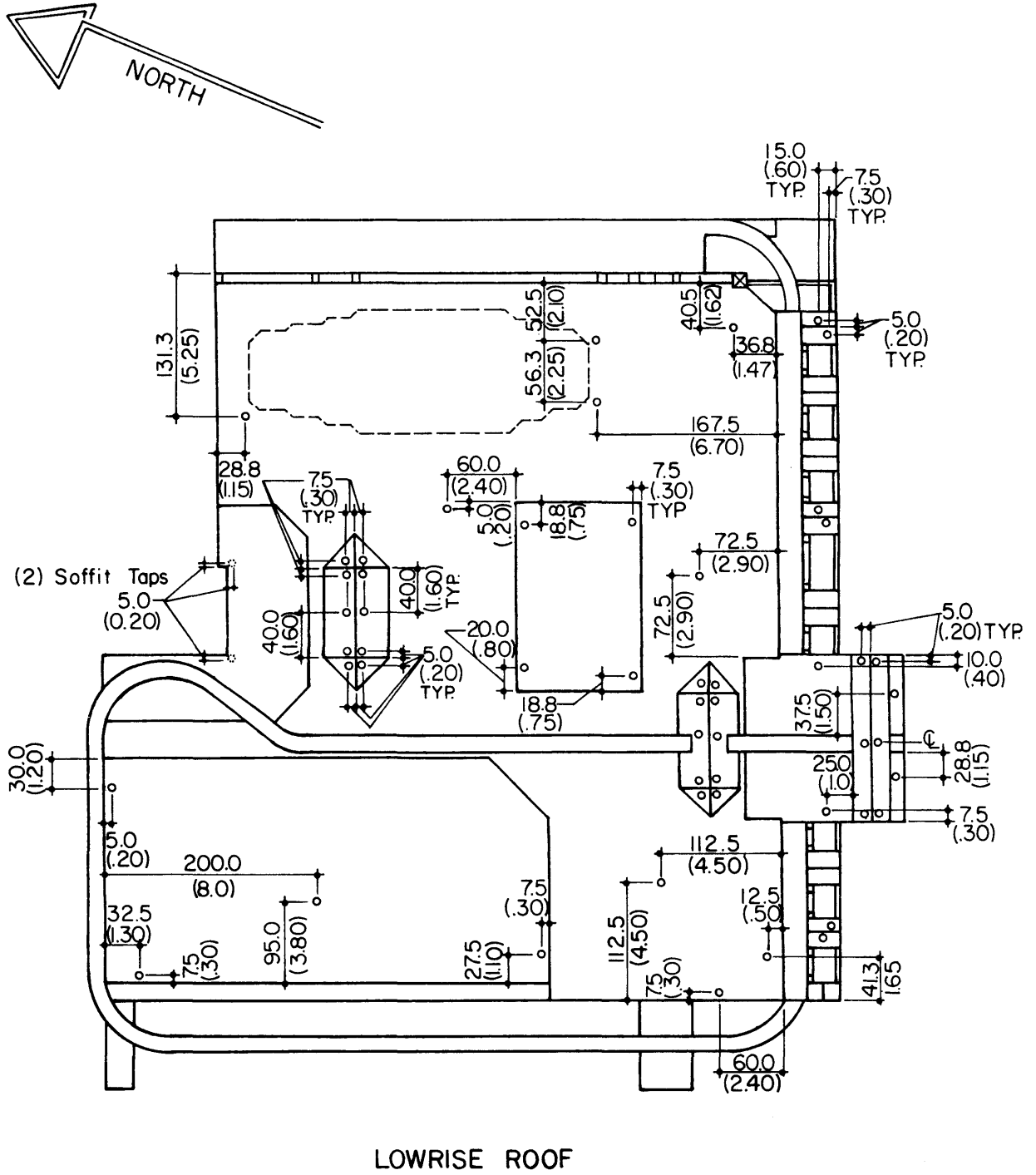
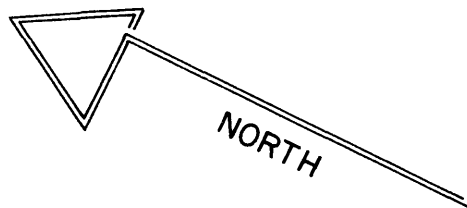
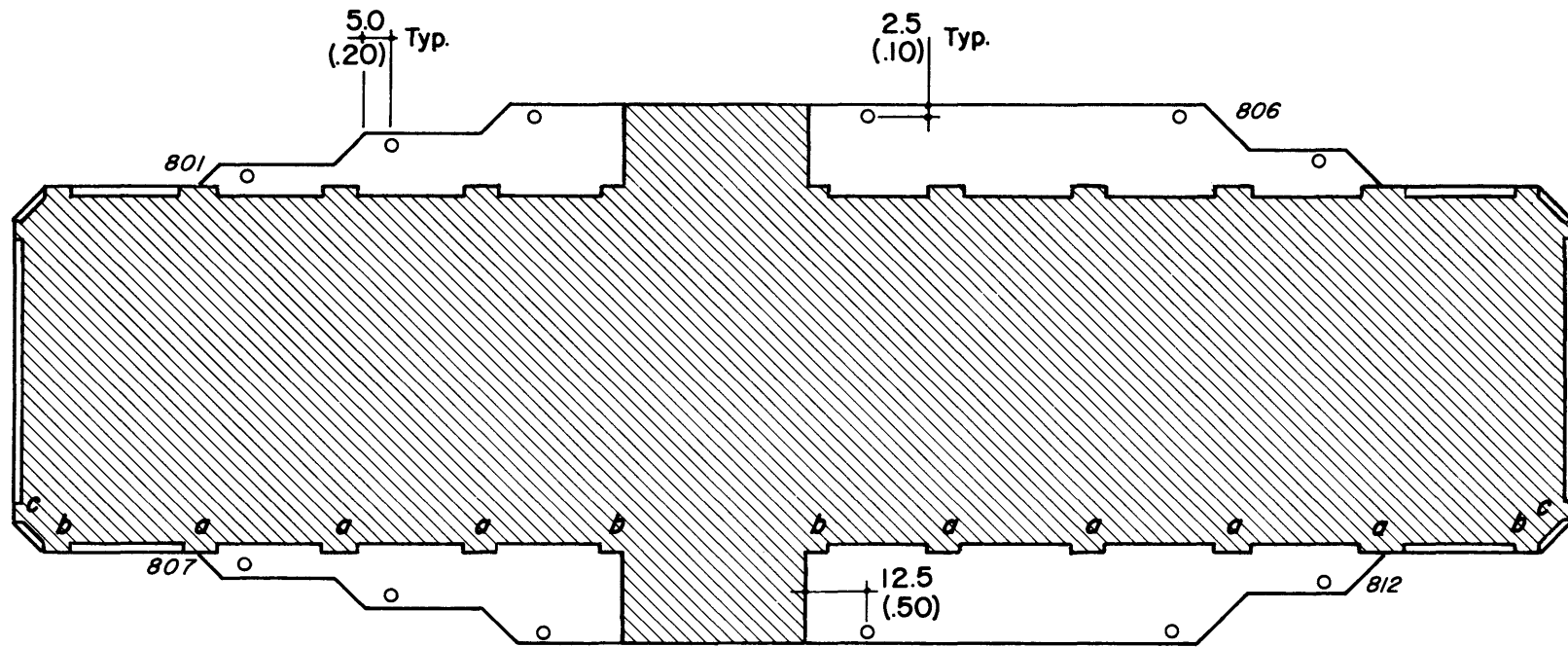


Figure 3e. Pressure Tap Locations



SOFFIT

Note:
 Facade strips are 1.5 (.06) X :
 (a) 7.5 (.30), equally spaced
 (b) 4.5 (.18)
 (c) 3.0 (.12)

Figure 3f. Pressure Tap Locations

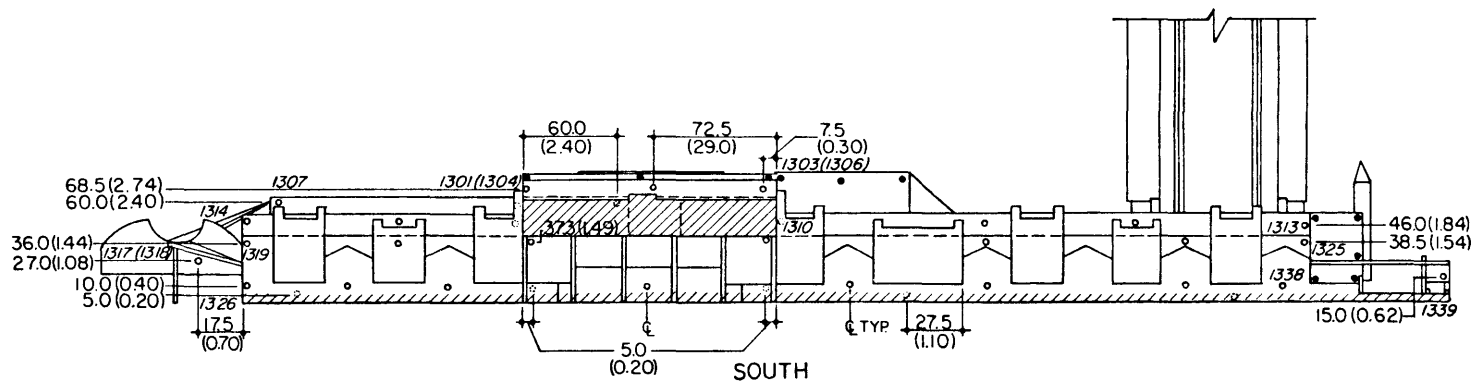
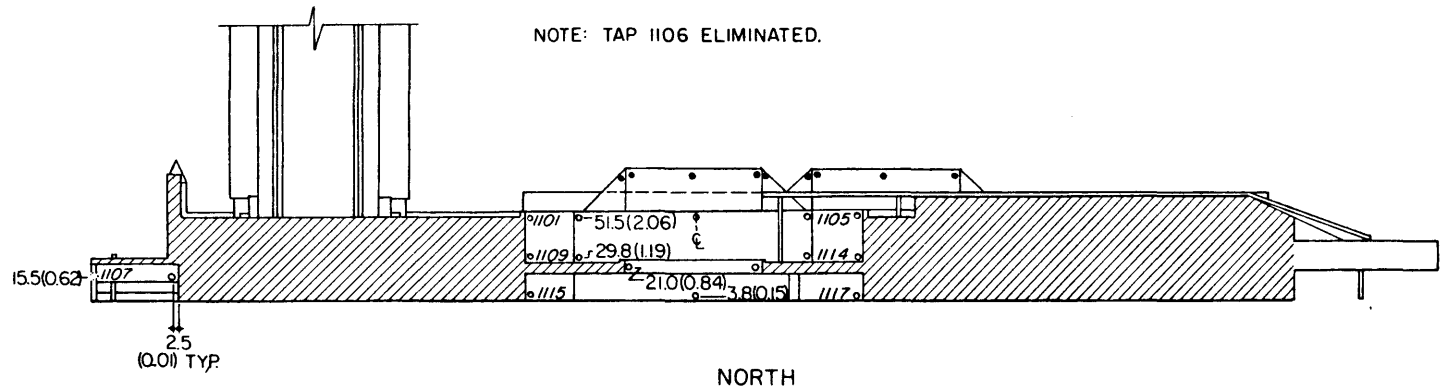


Figure 3g. Pressure Tap Locations

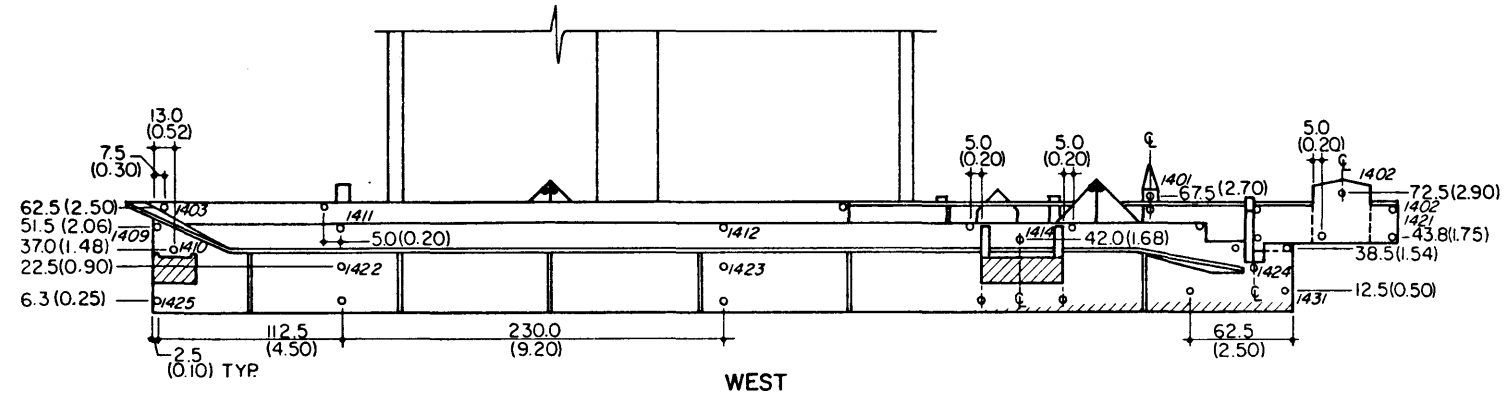
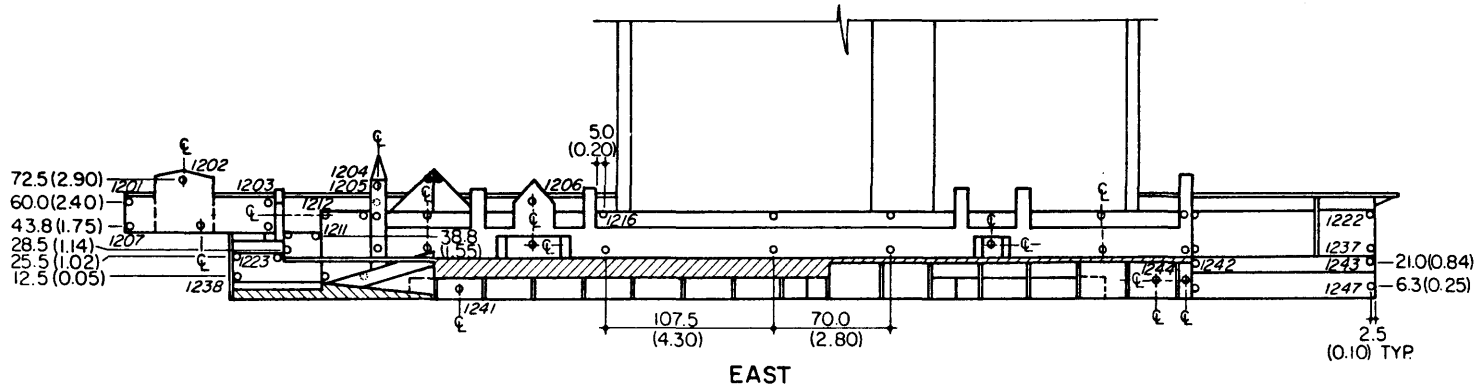
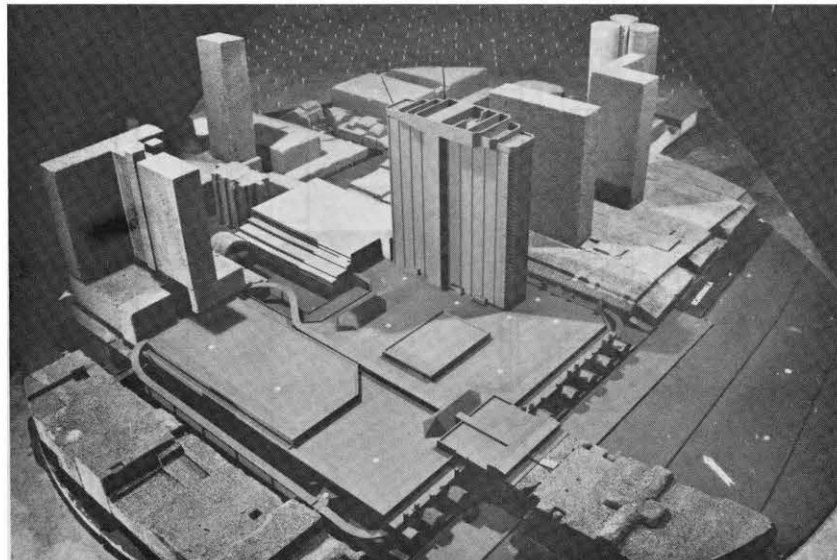
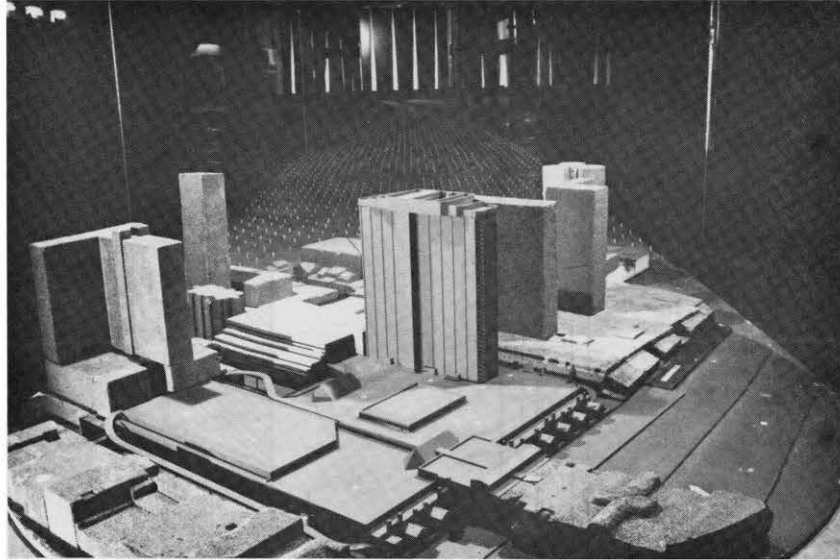
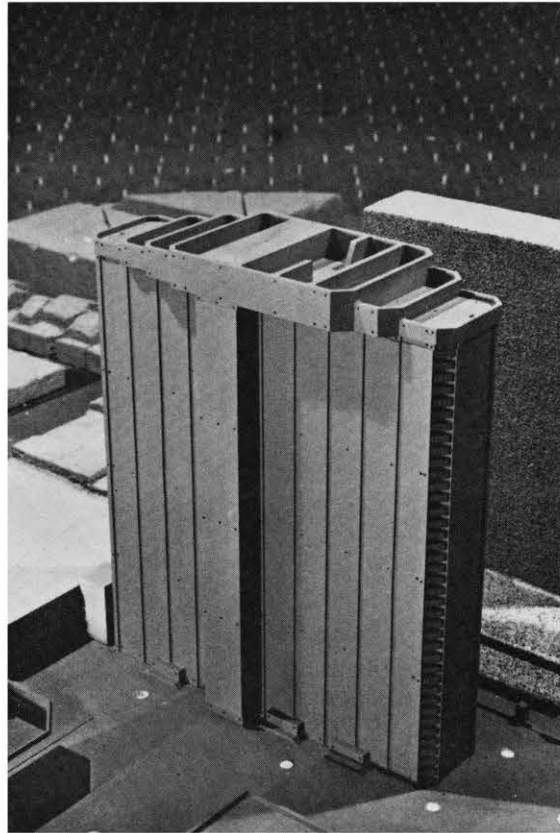


Figure 3h. Pressure Tap Locations



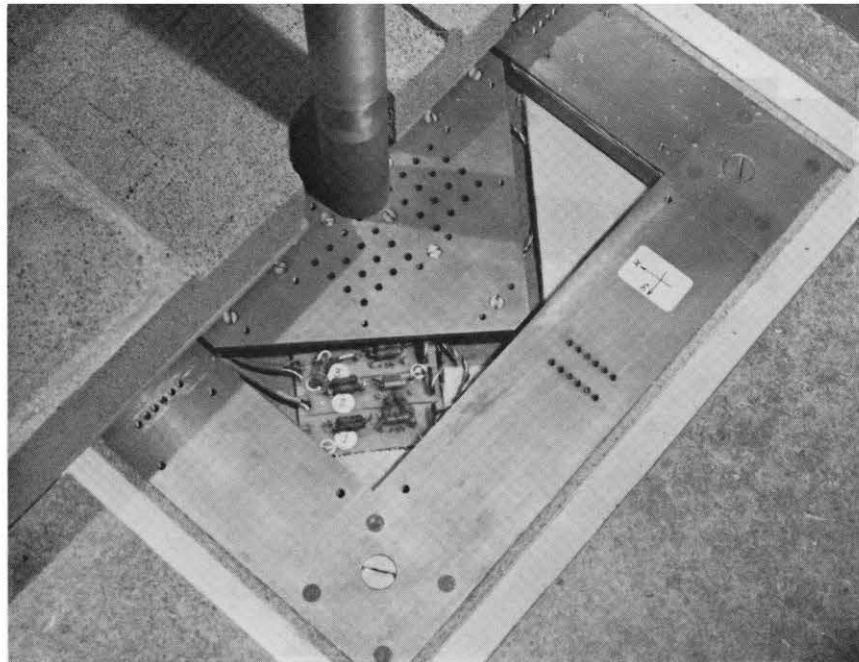
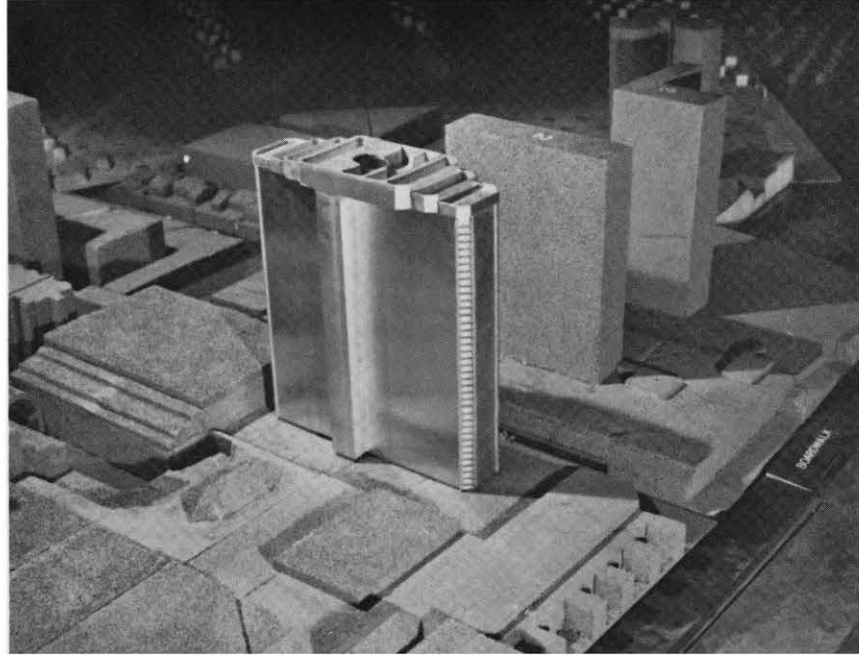
PRESSURE MODEL

Figure 4a. Completed Model in Wind Tunnel



PRESSURE MODEL

Figure 4b. Completed Model in Wind Tunnel



DYNAMIC MODEL AND BALANCE

Figure 4c. Completed Model in Wind Tunnel

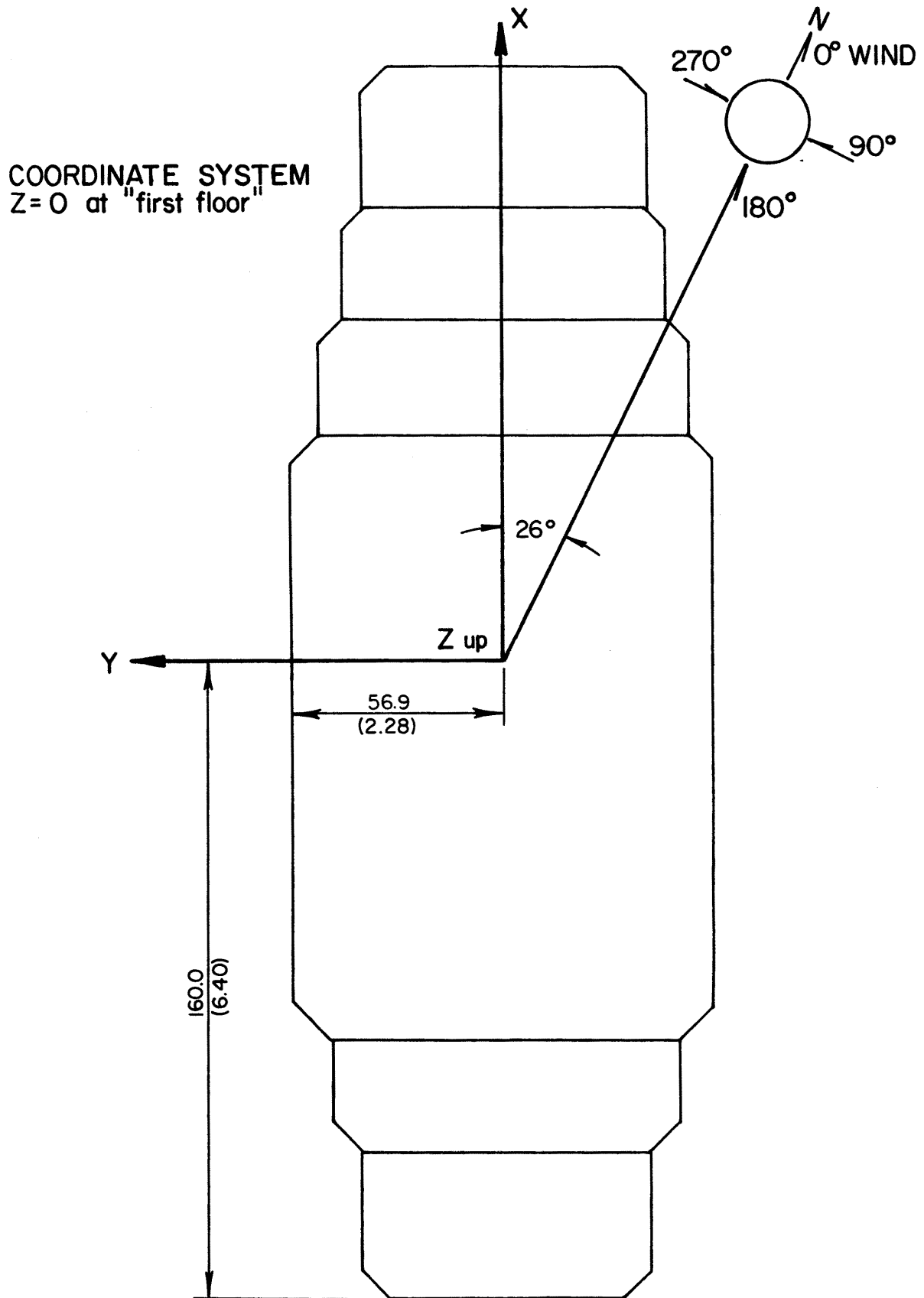


Figure 5. Tower Coordinate System

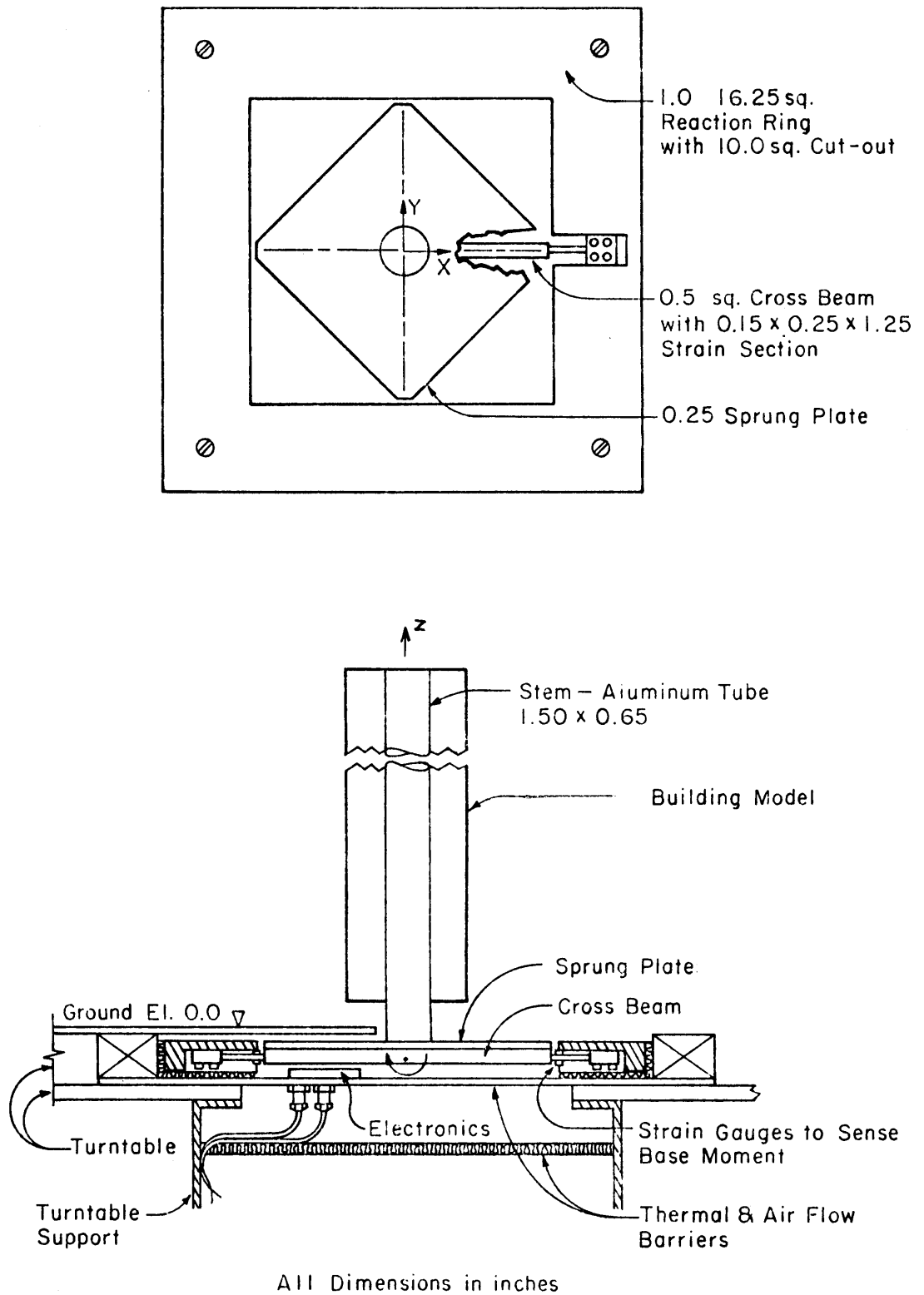


Figure 6. Dynamic Model and Balance System

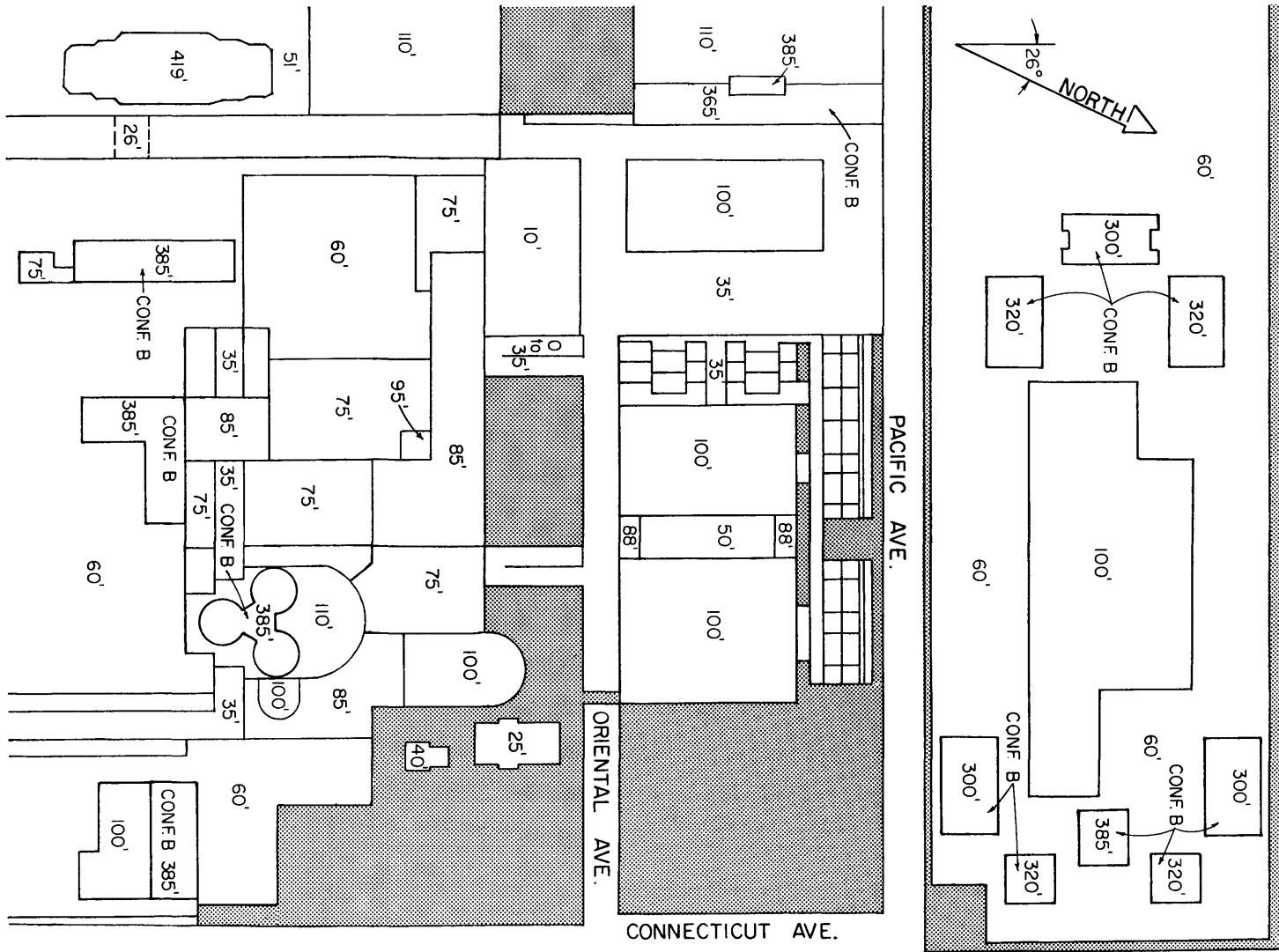


Figure 7a. Building Location and Pedestrian Wind Velocity Measuring Positions

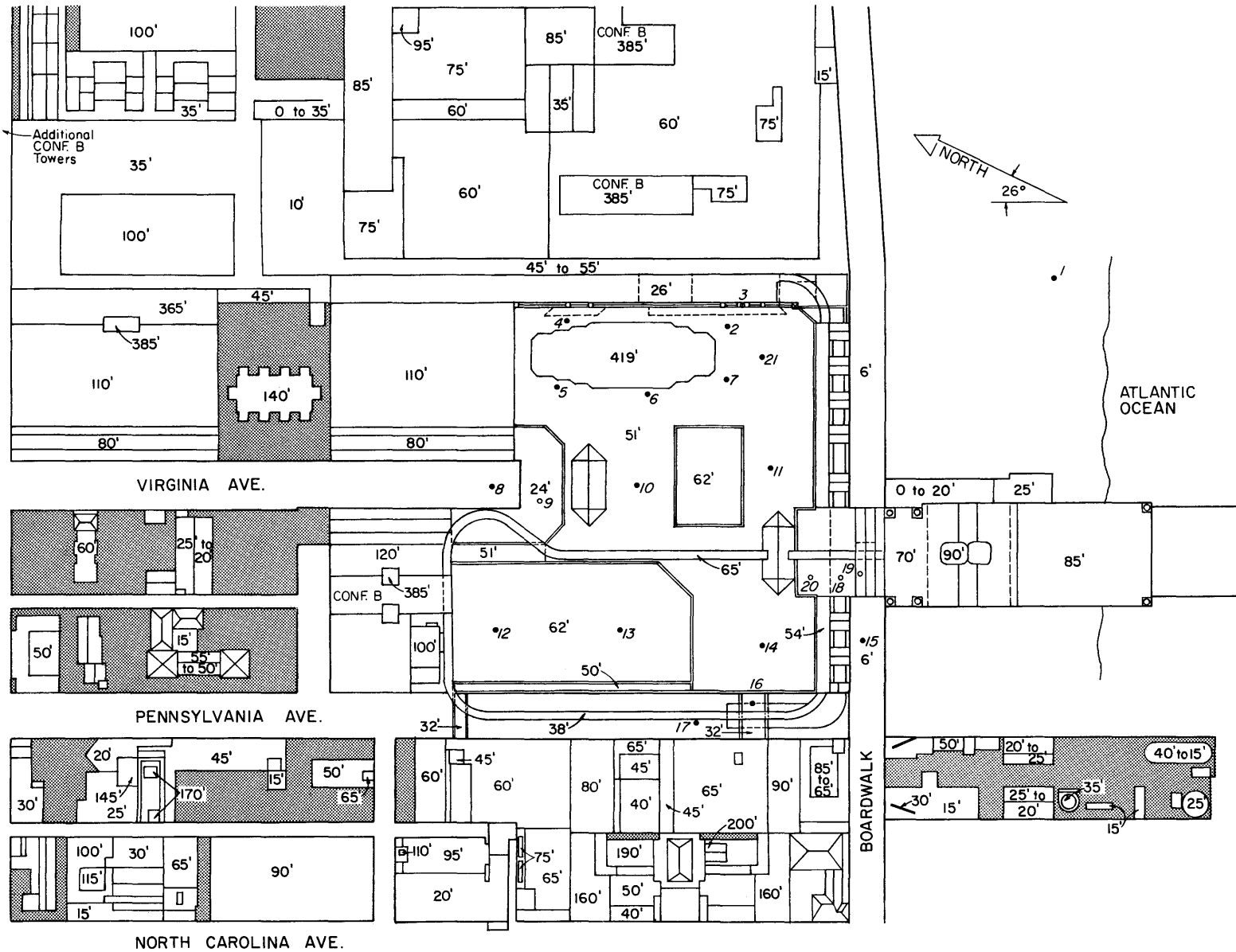


Figure 7b. Building Location and Pedestrian Wind Velocity Measuring Positions

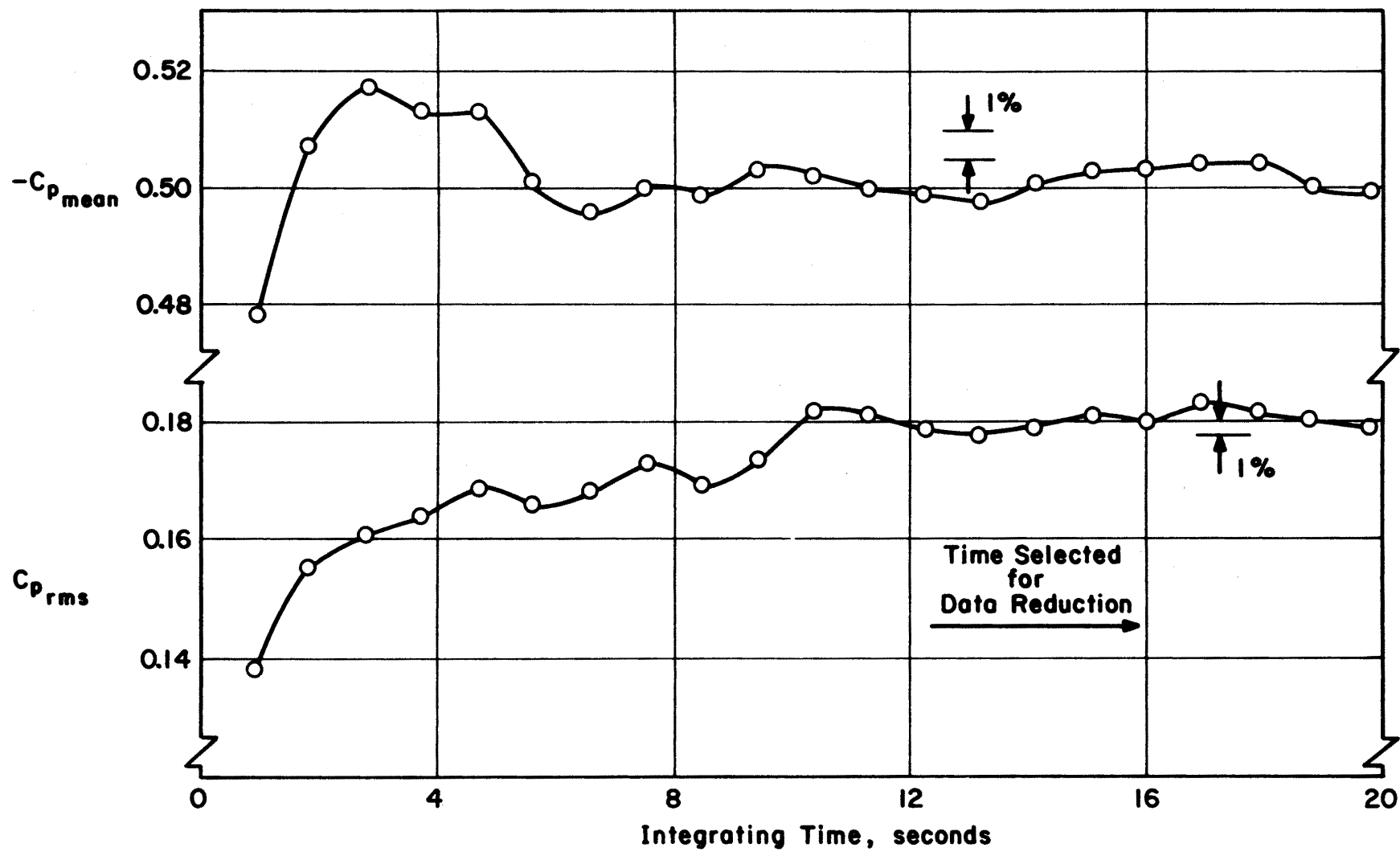


Figure 8. Data Sampling Time Verification

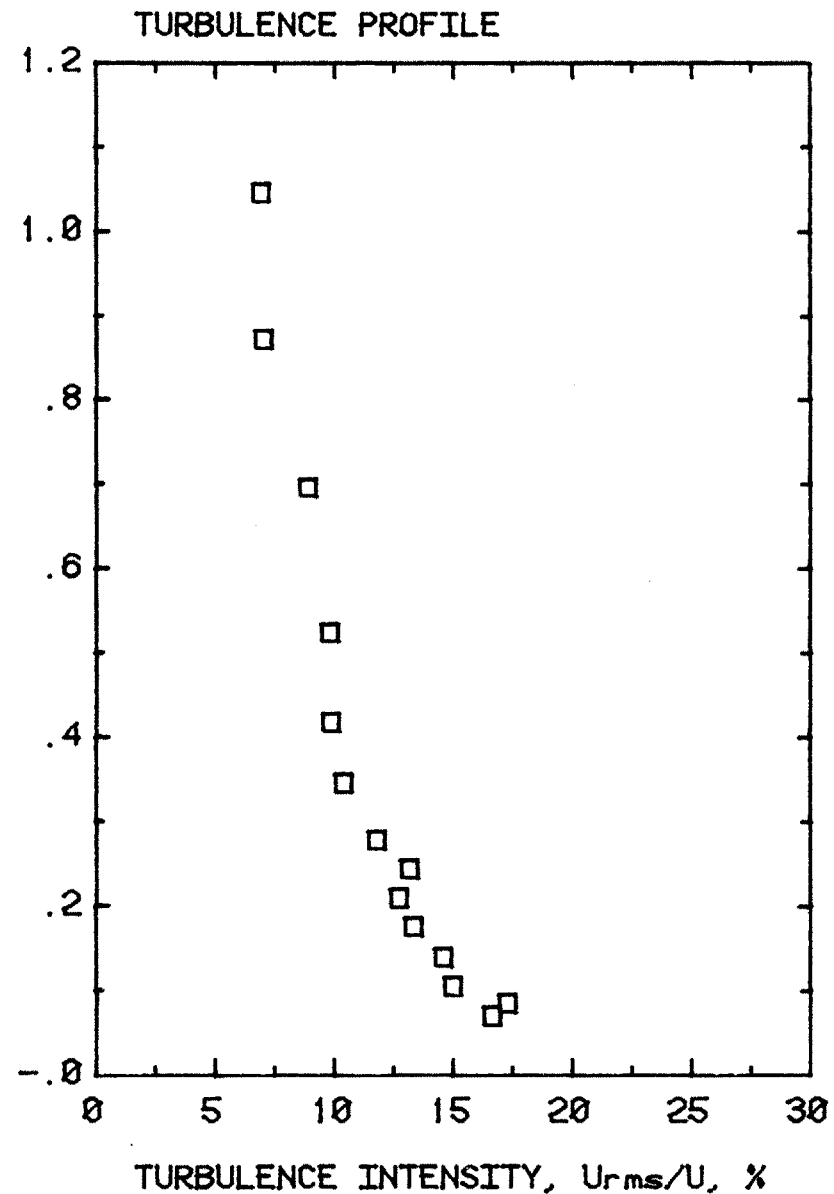
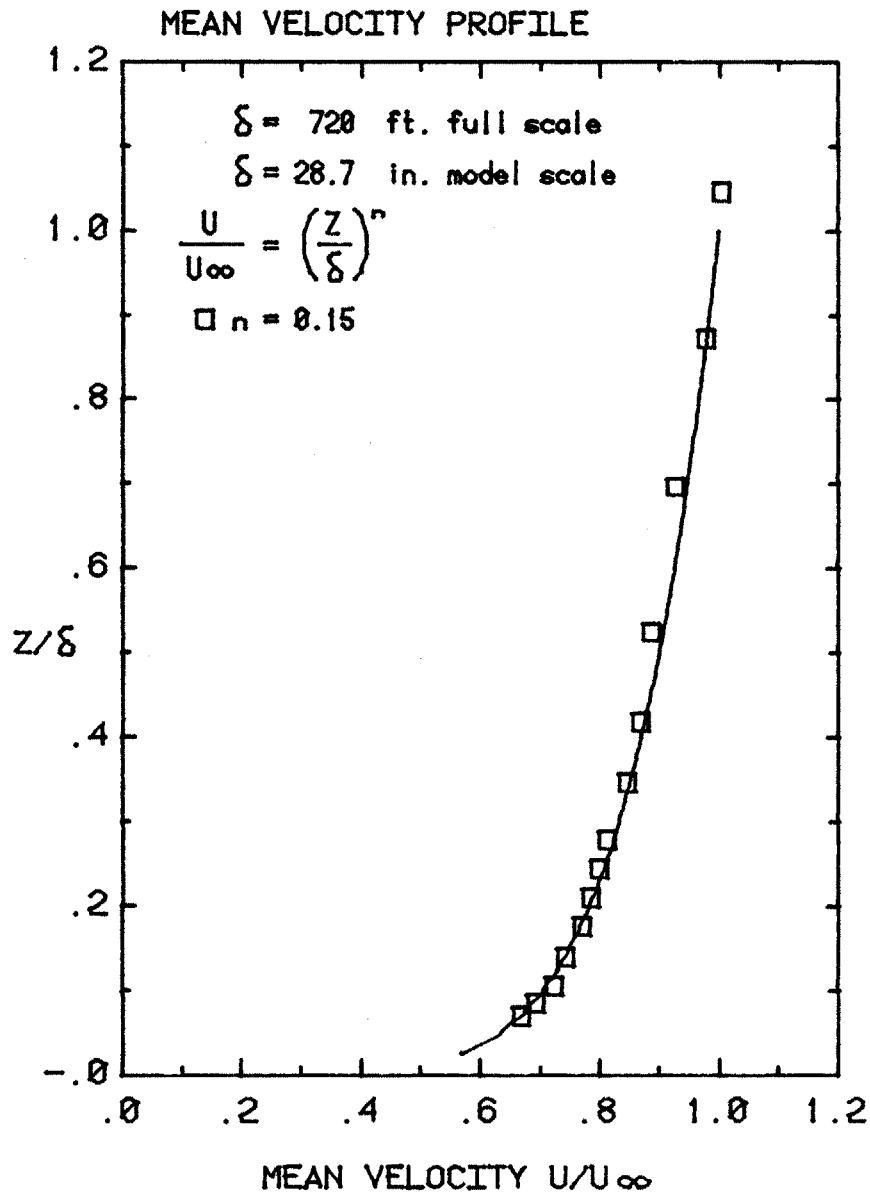


Figure 9. Mean Velocity and Turbulence Profiles Approaching the Model

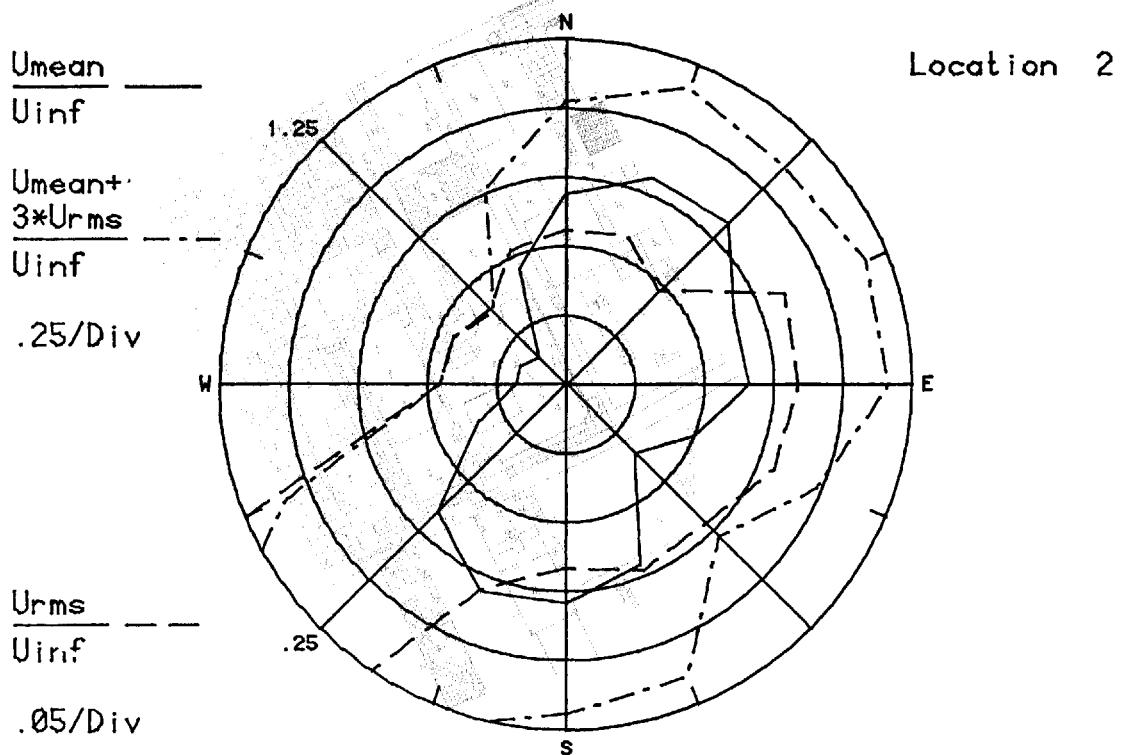
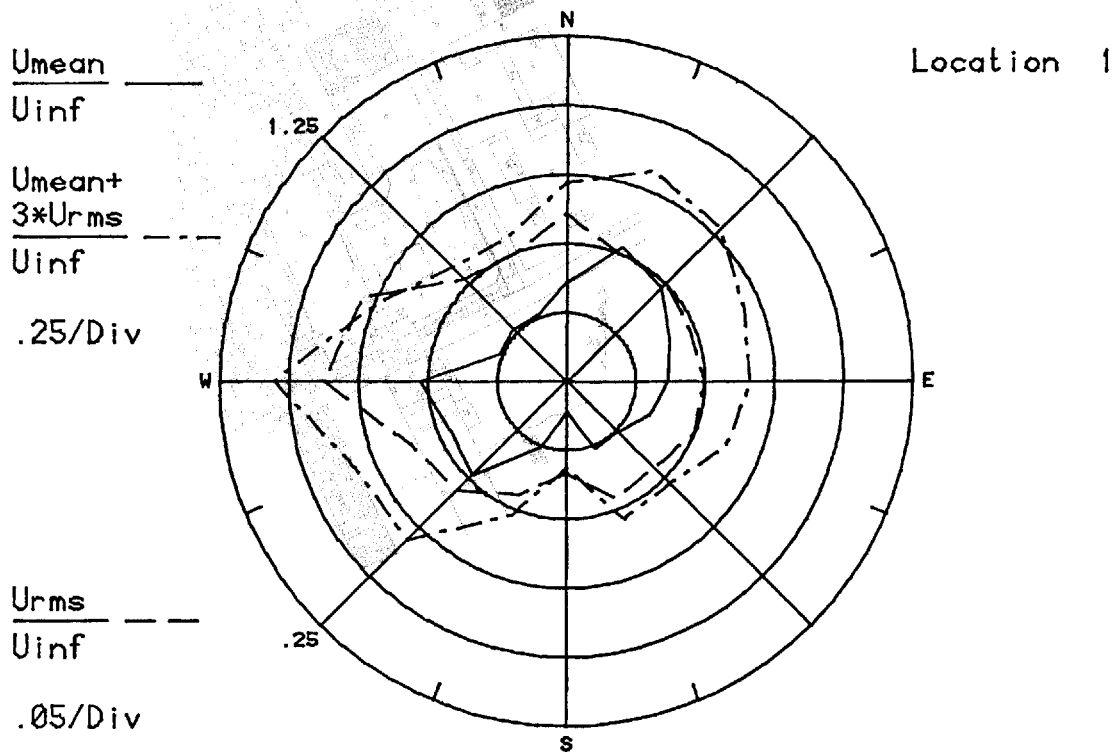


Figure 10a. Mean Velocities and Turbulence Intensities at Pedestrian Locations 1 and 2

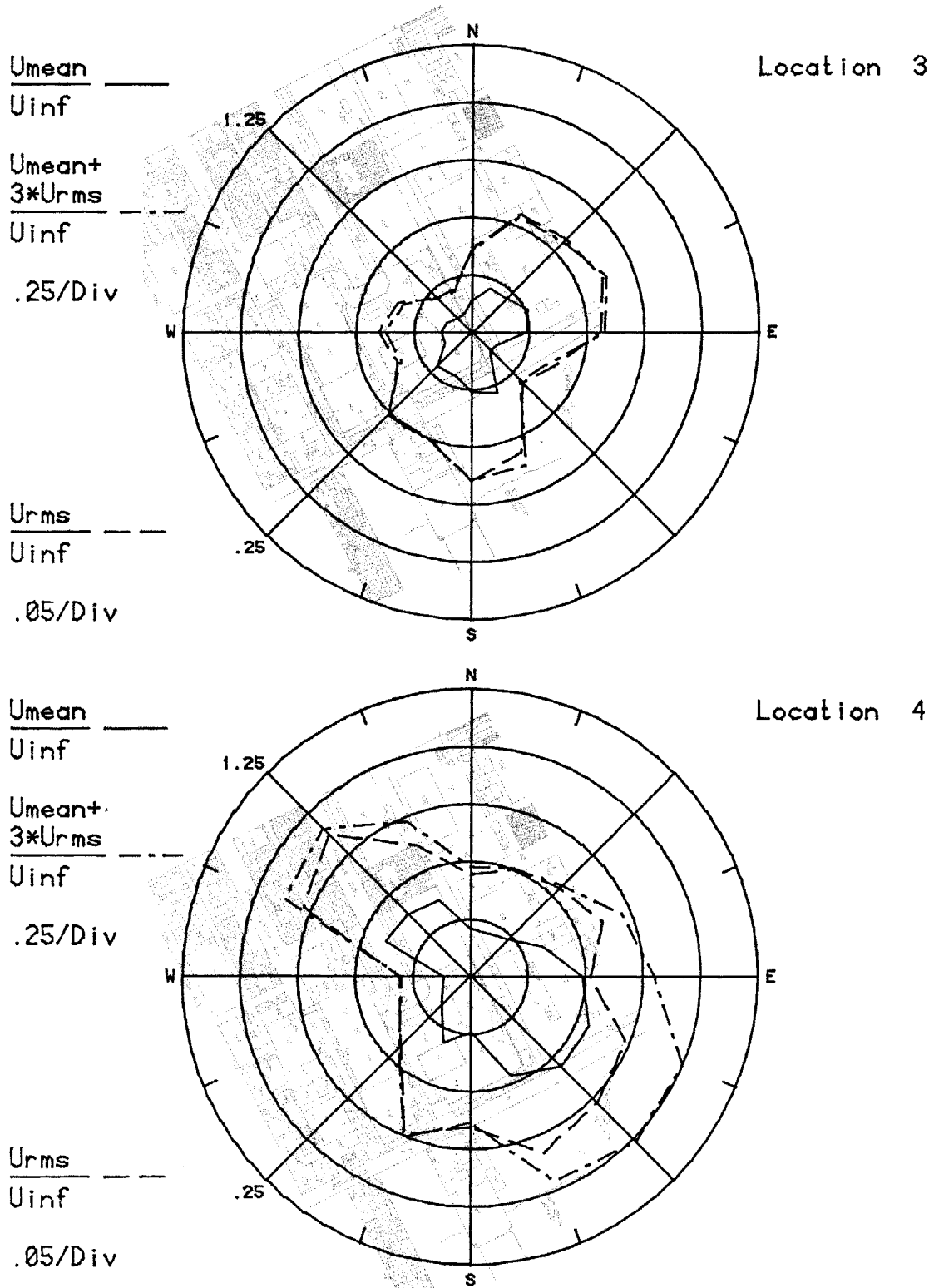


Figure 10b. Mean Velocities and Turbulence Intensities at Pedestrian Locations 3 and 4

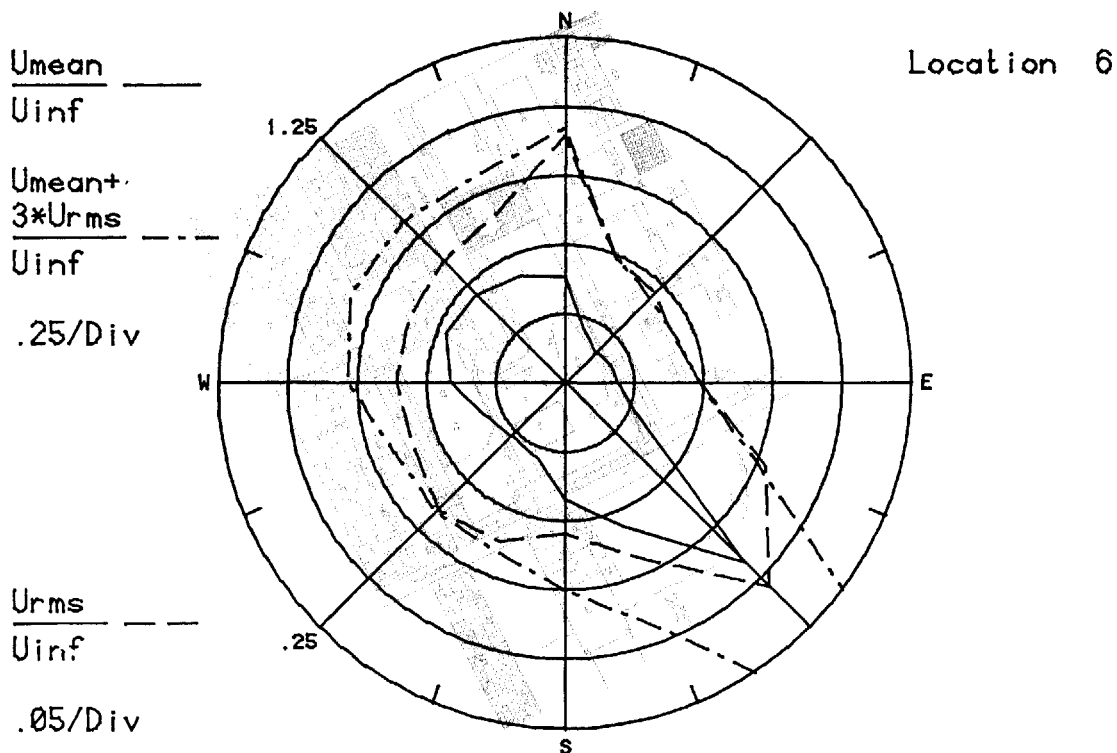
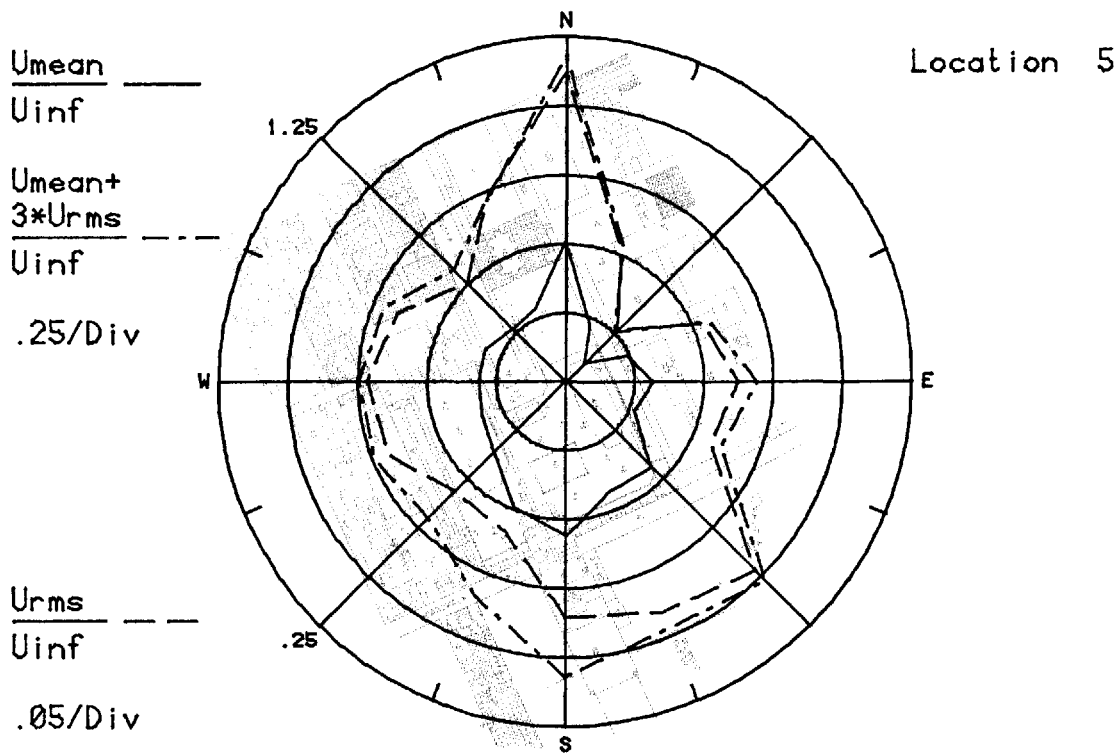


Figure 10c. Mean Velocities and Turbulence Intensities at Pedestrian Locations 5 and 6

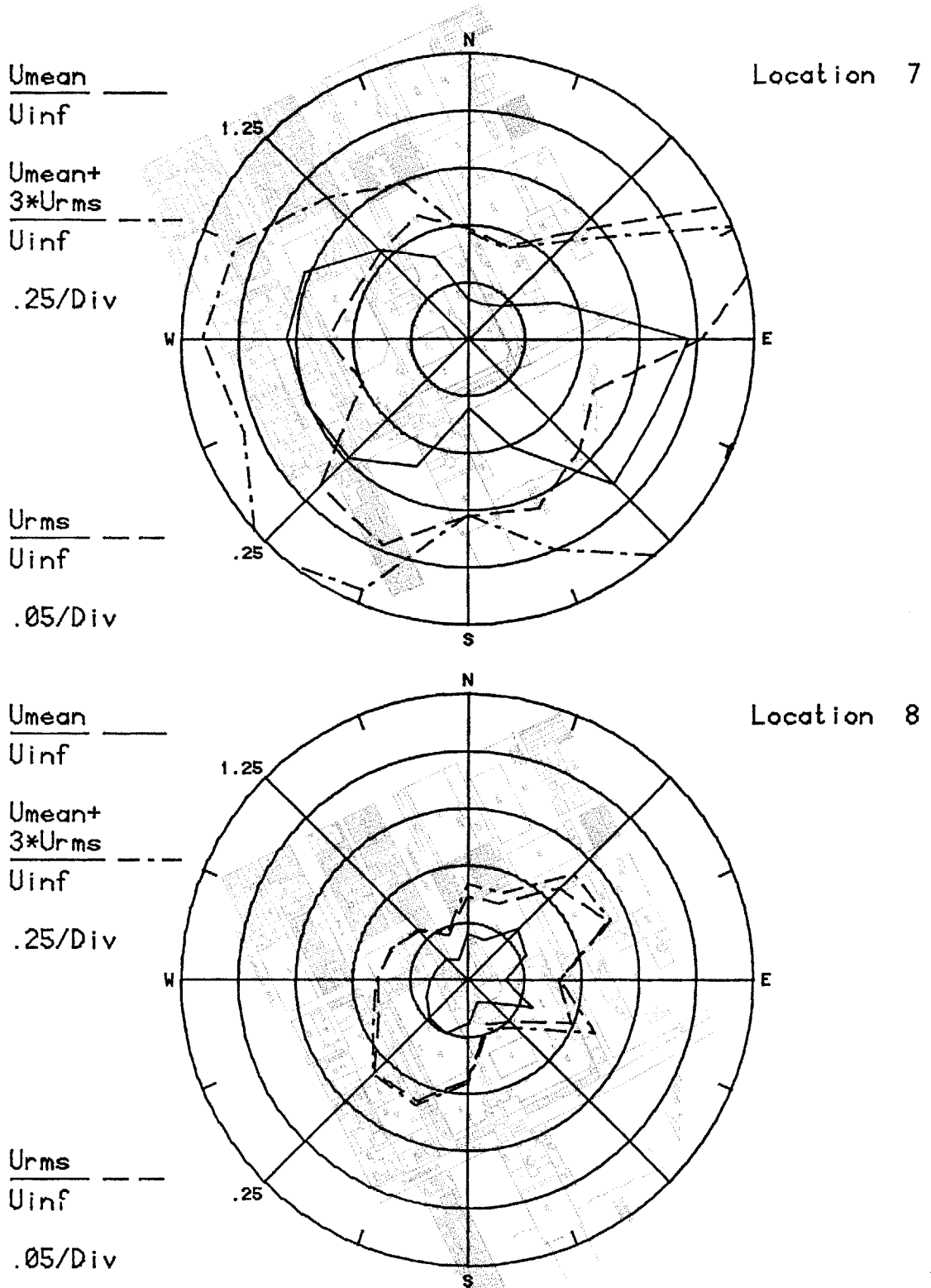


Figure 10d. Mean Velocities and Turbulence Intensities at Pedestrian Locations 7 and 8

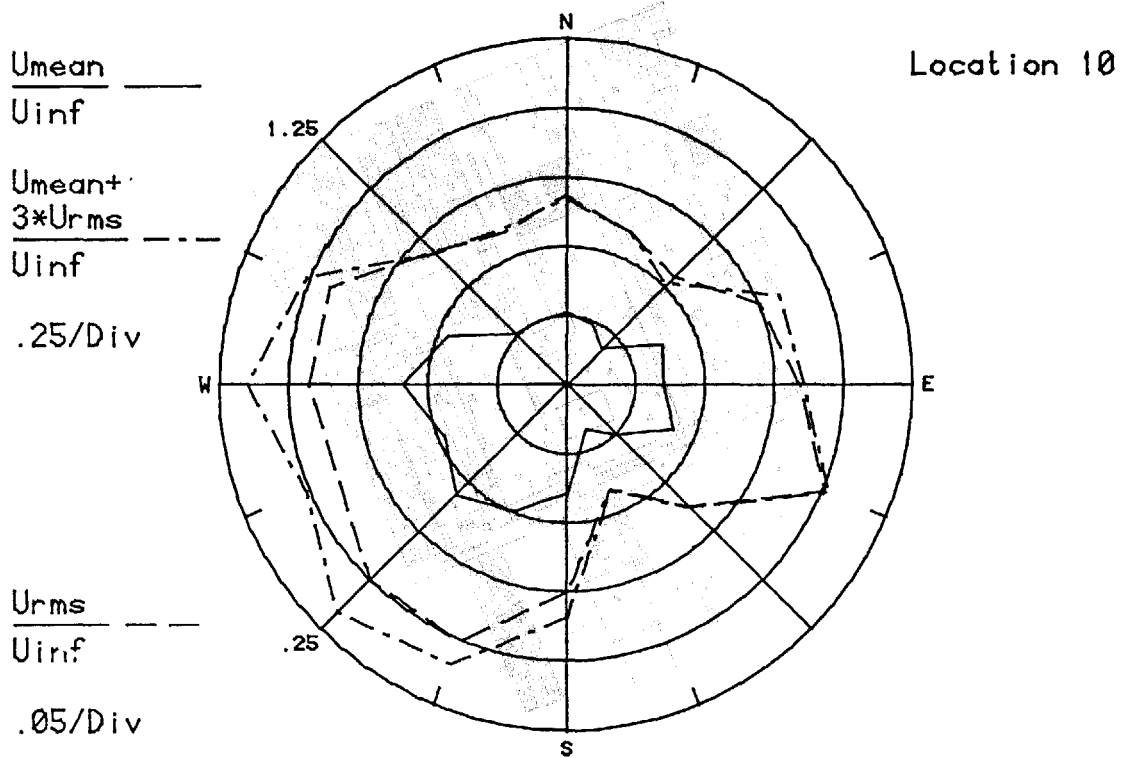
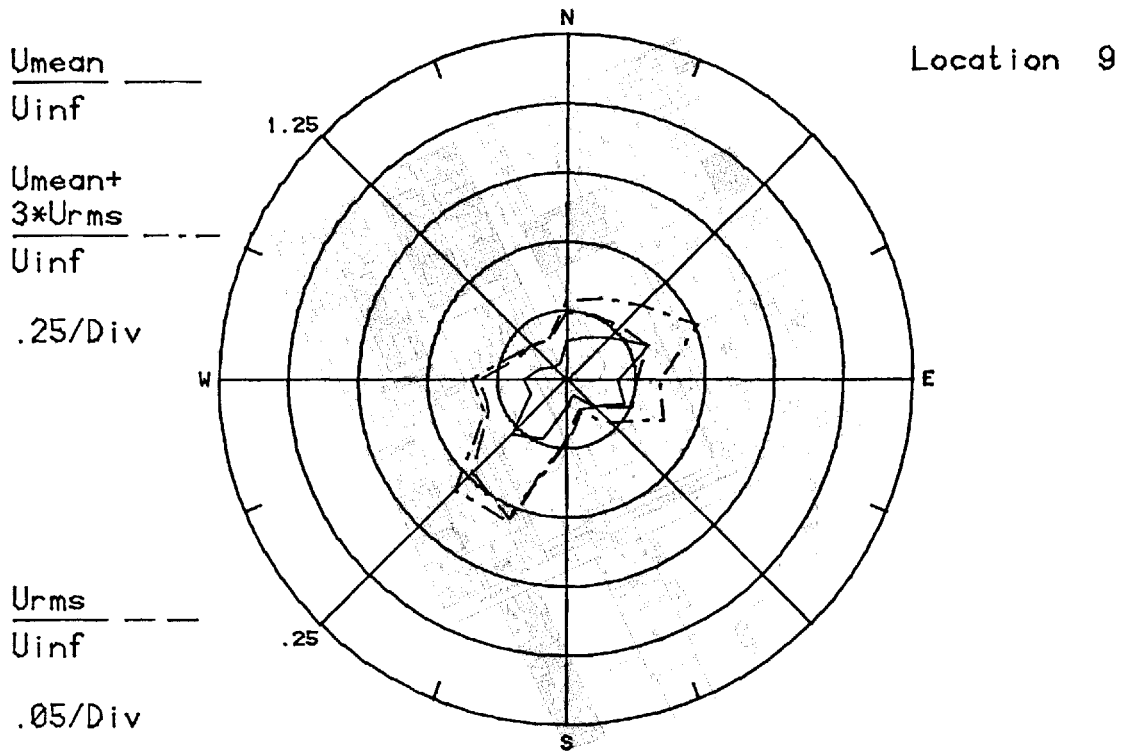


Figure 10e. Mean Velocities and Turbulence Intensities at Pedestrian Locations 9 and 10

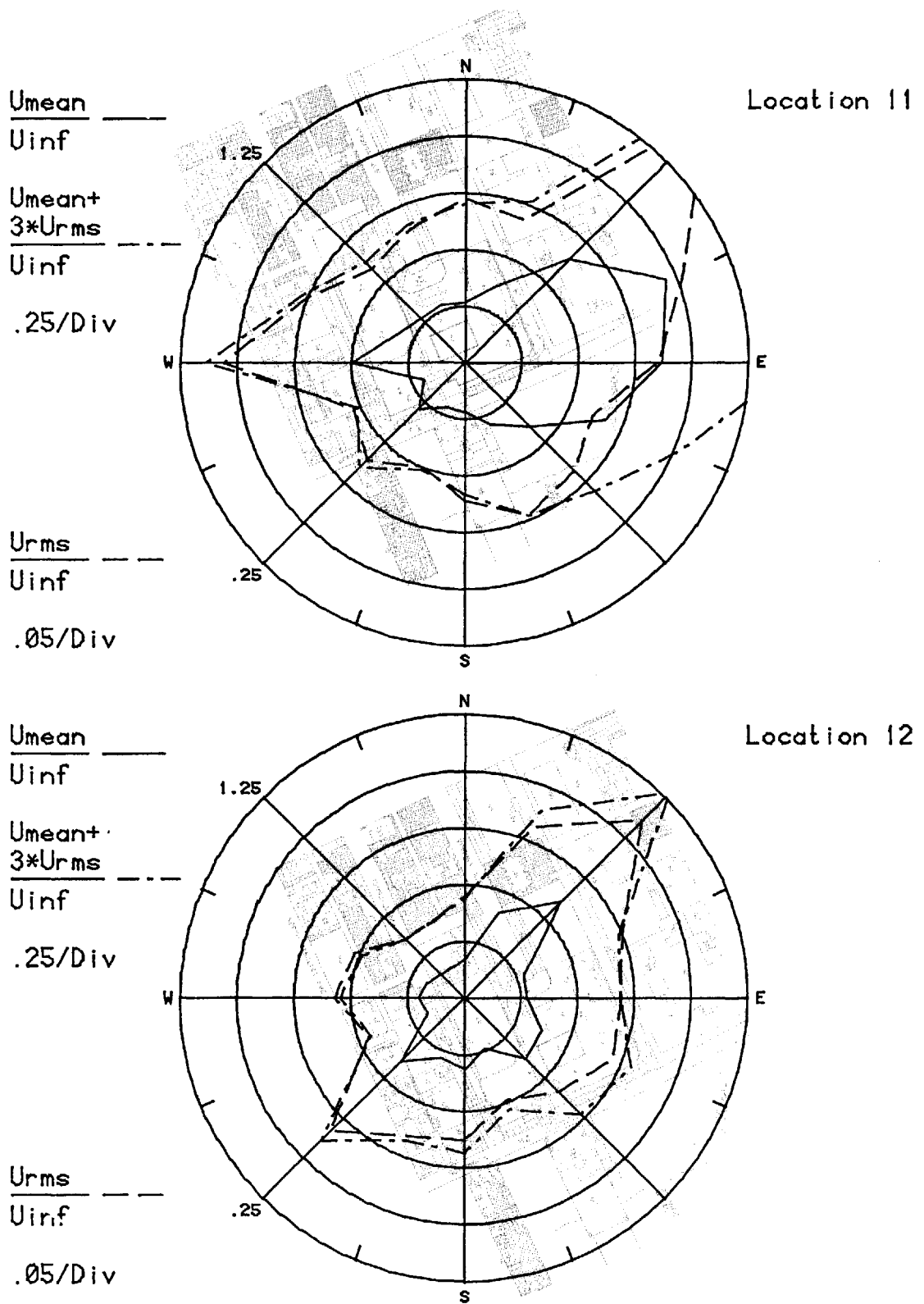


Figure 10f. Mean Velocities and Turbulence Intensities at Pedestrian Locations 11 and 12

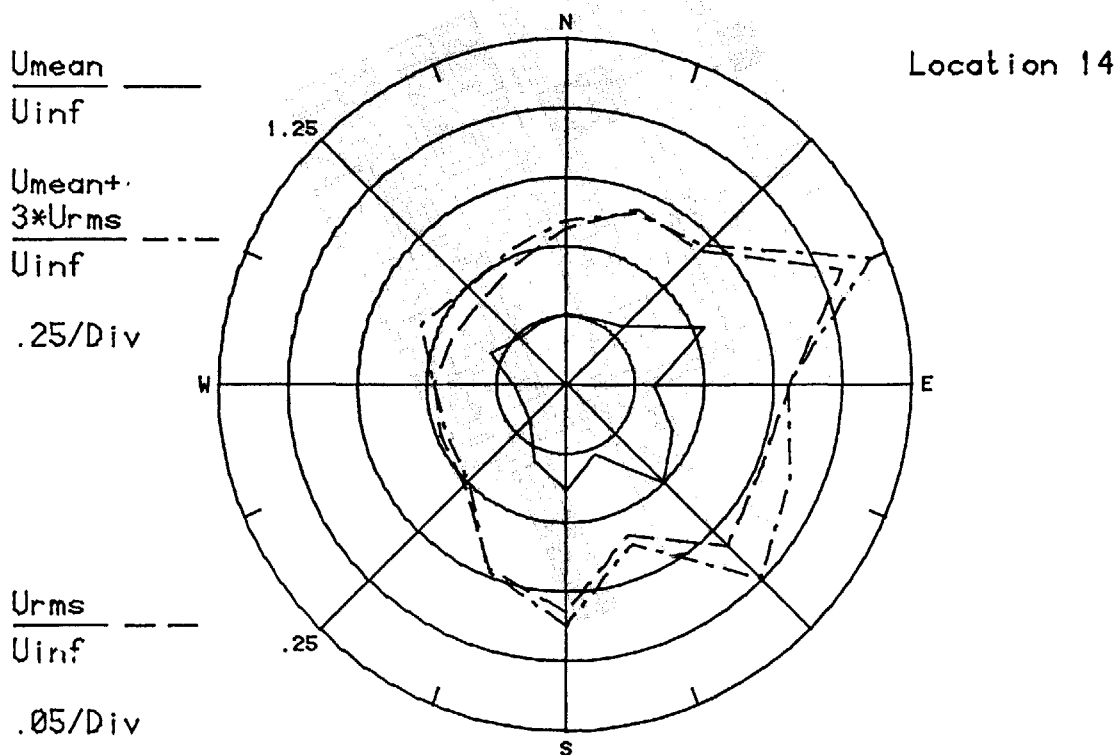
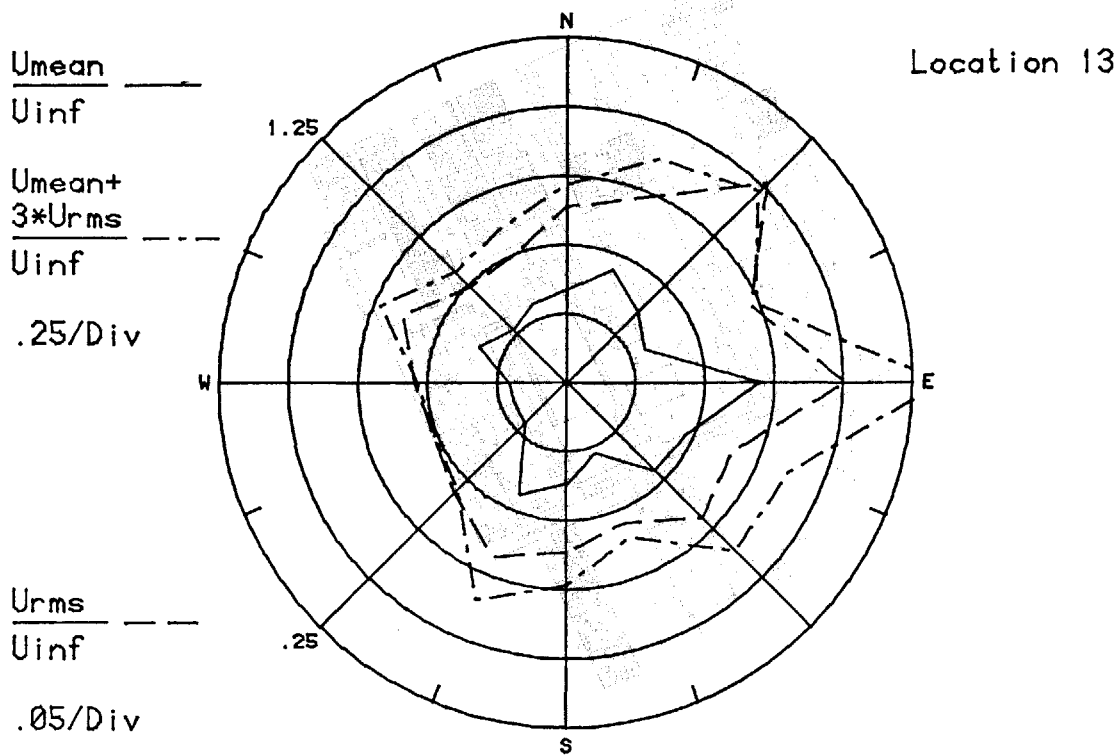


Figure 10g. Mean Velocities and Turbulence Intensities at Pedestrian Locations 13 and 14

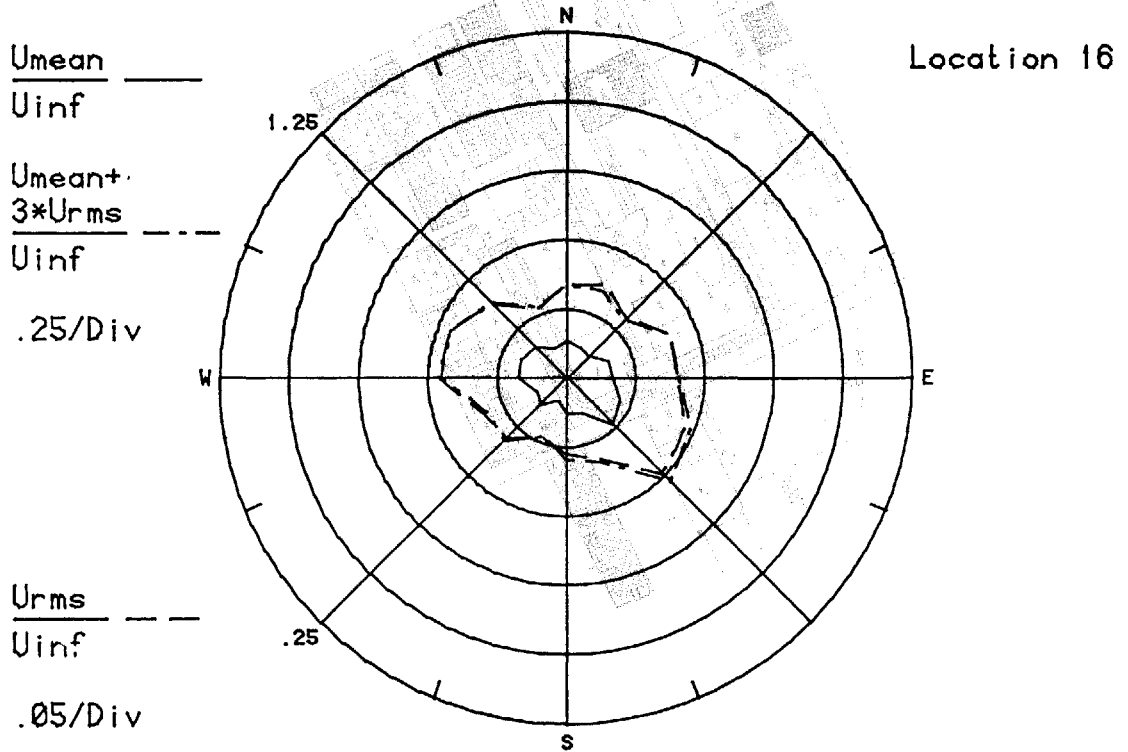
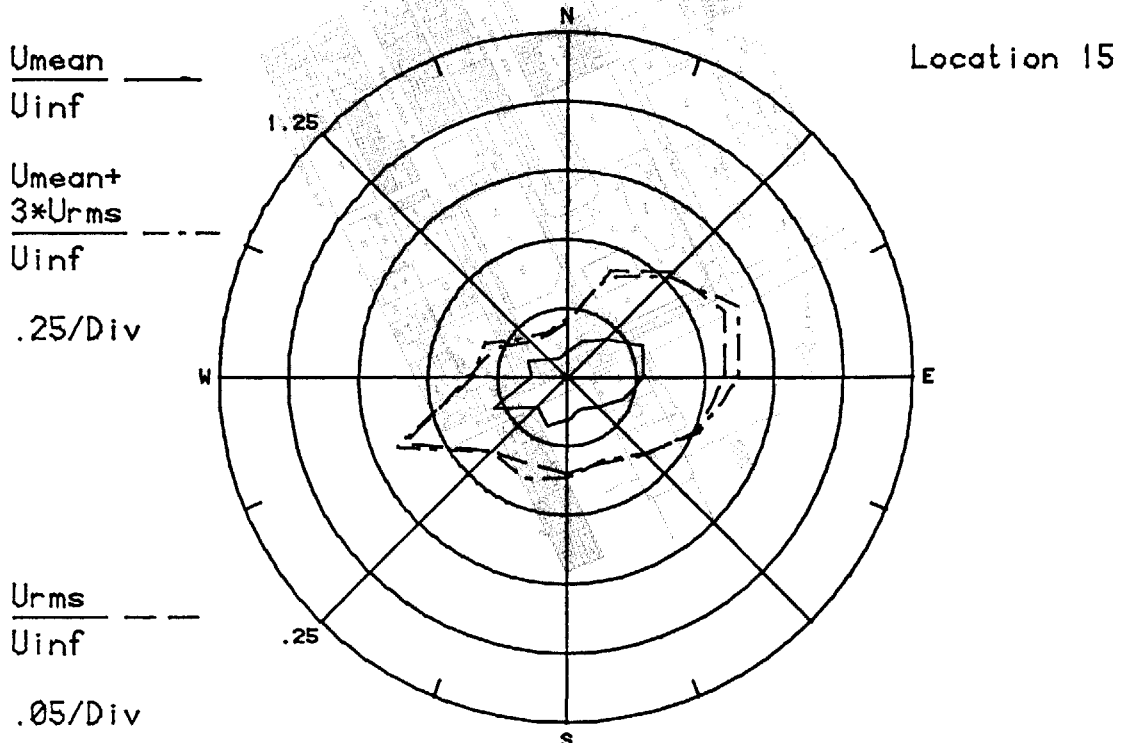


Figure 10h. Mean Velocities and Turbulence Intensities at Pedestrian Locations 15 and 16

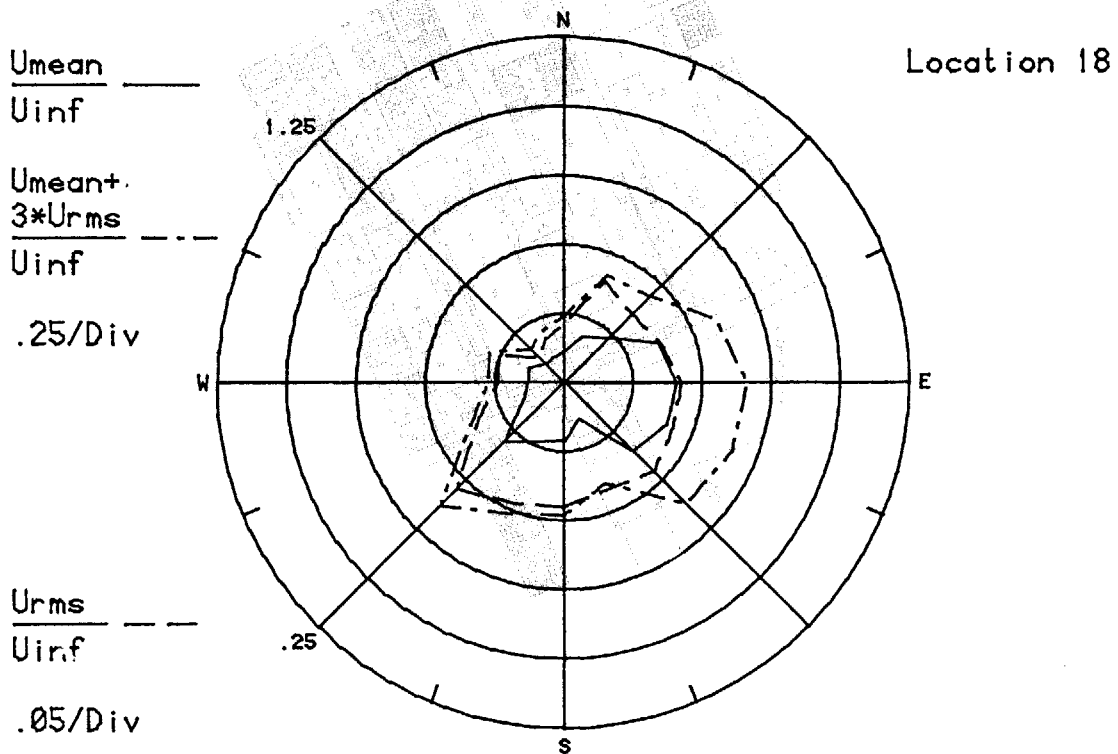
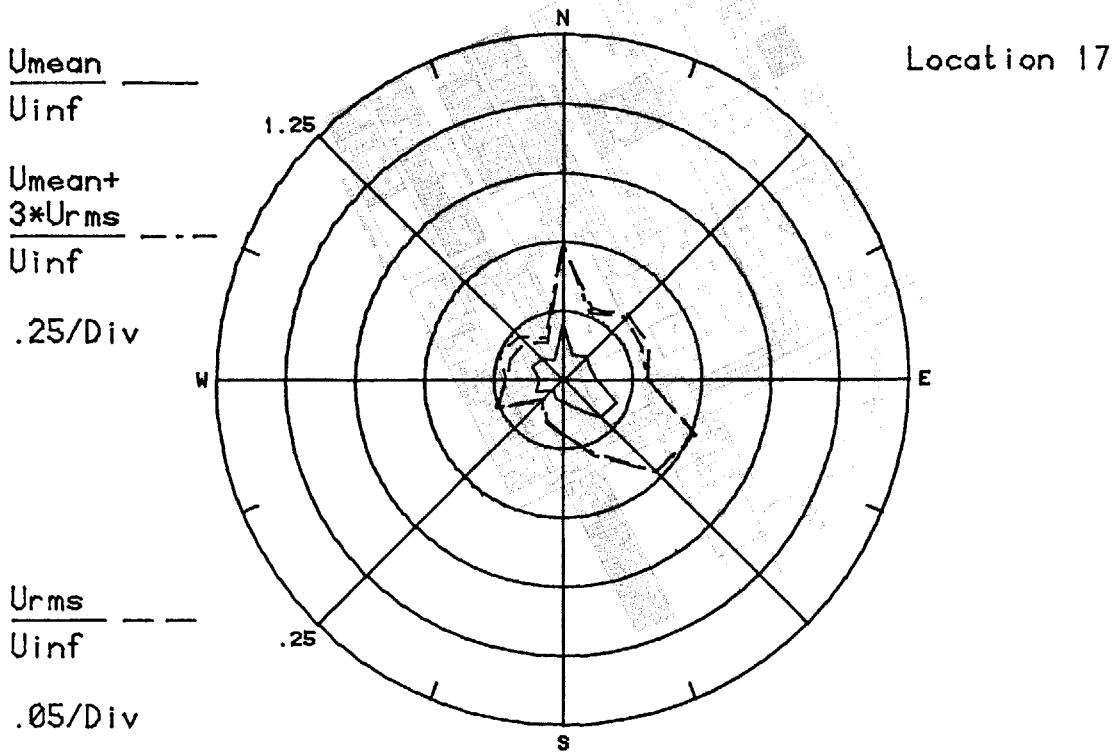


Figure 10i. Mean Velocities and Turbulence Intensities at Pedestrian Locations 17 and 18

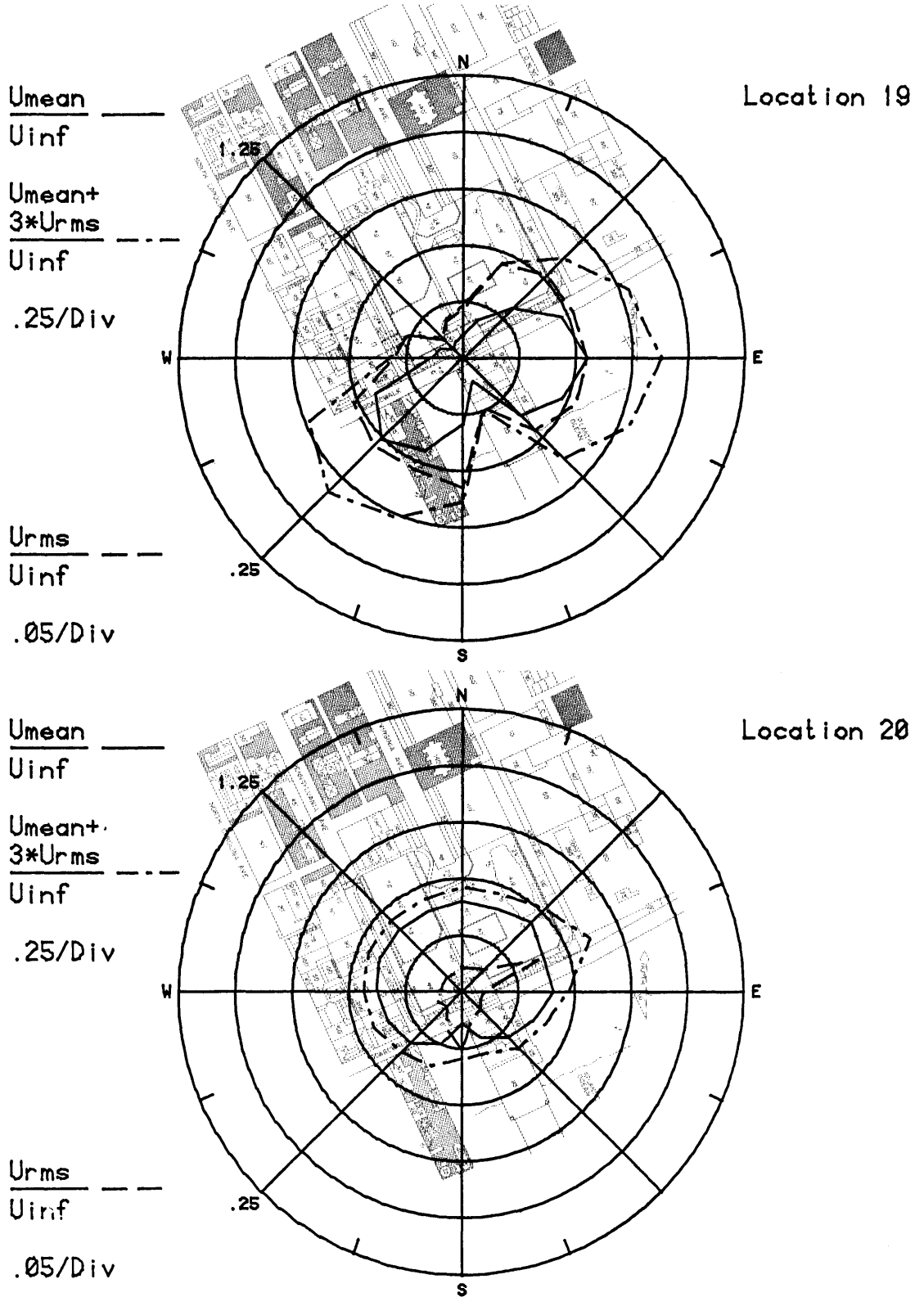


Figure 10j. Mean Velocities and Turbulence Intensities at Pedestrian Locations 19 and 20

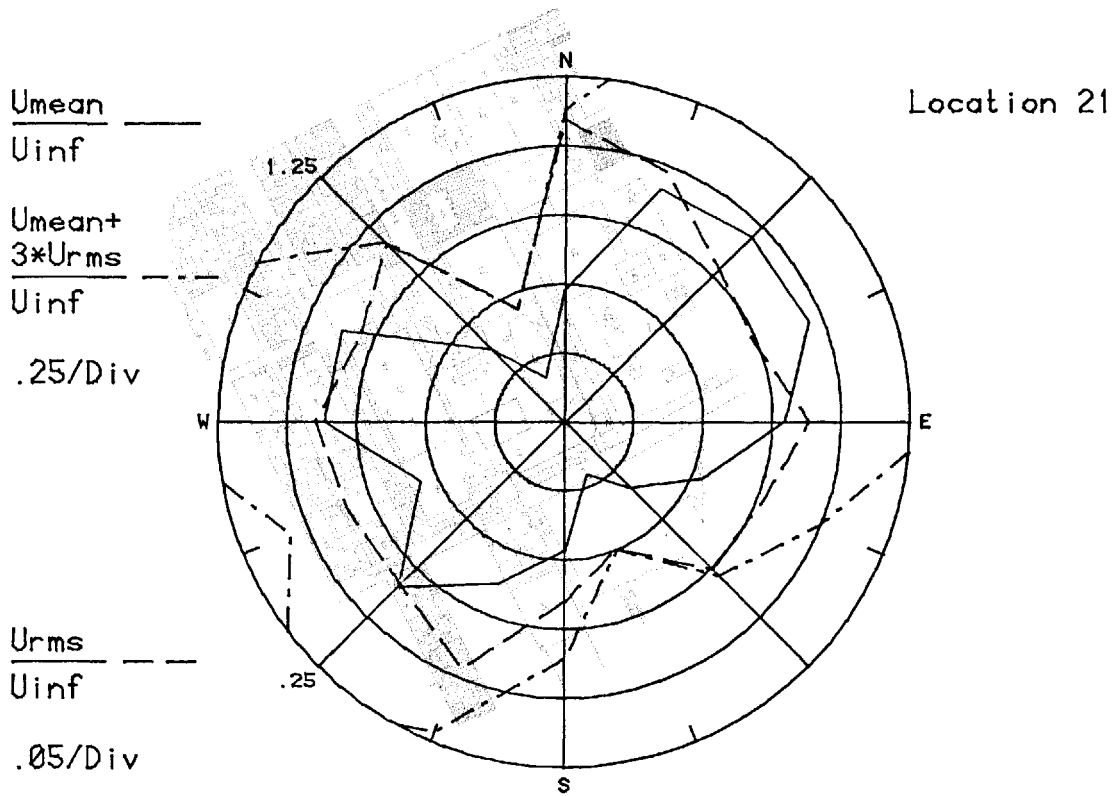


Figure 10k. Mean Velocities and Turbulence Intensities at Pedestrian Location 21

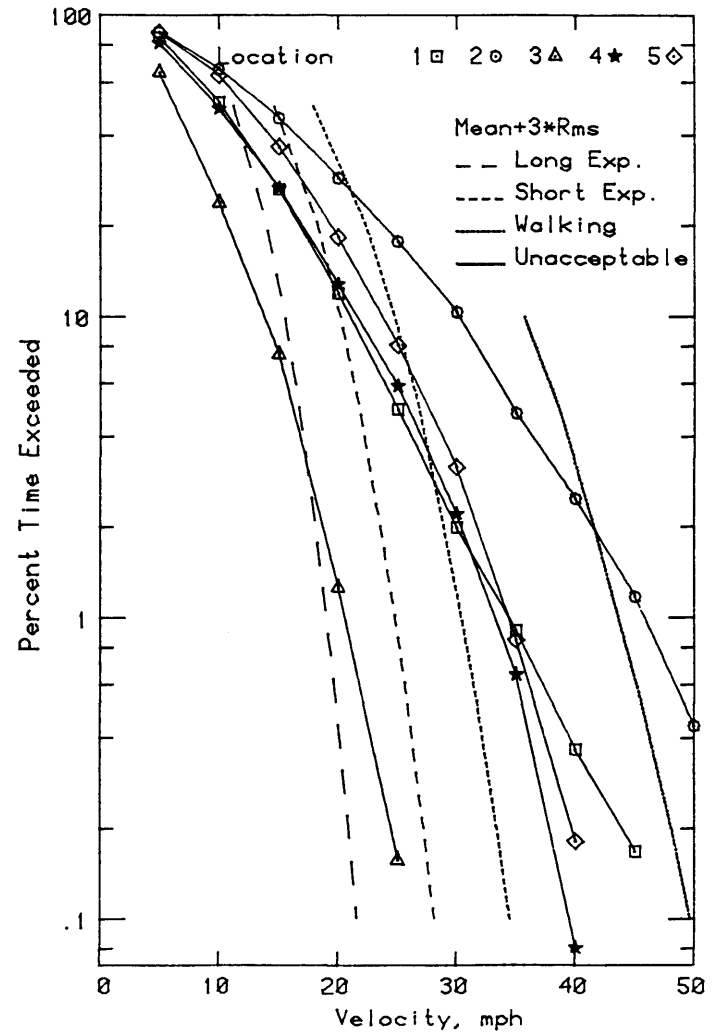
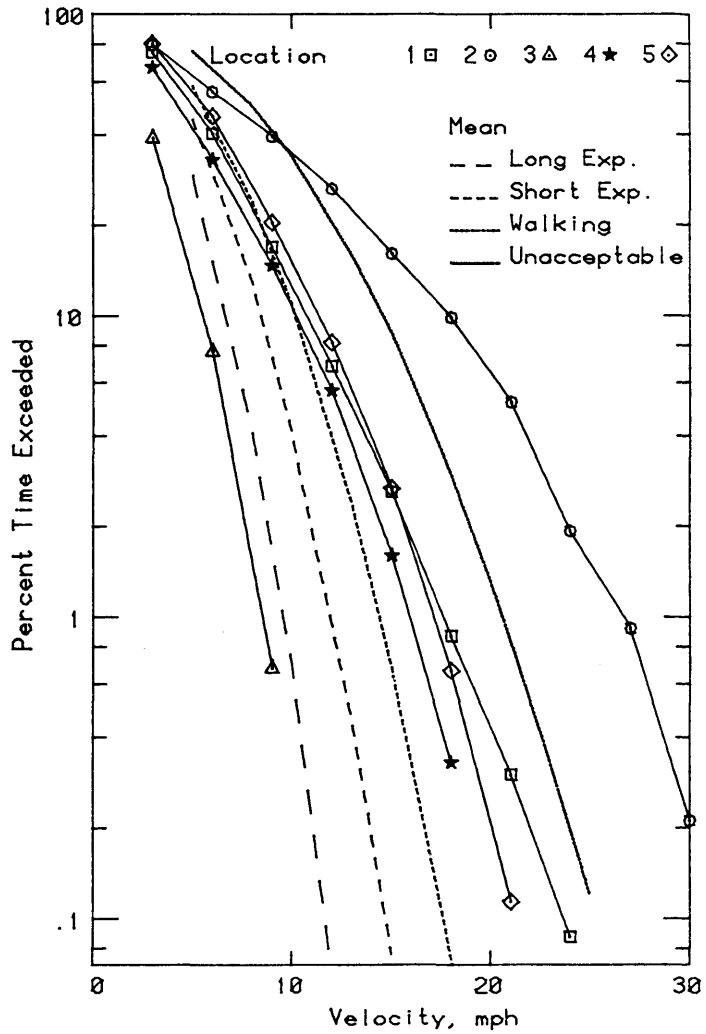


Figure 11a. Wind Velocity Probabilities for Pedestrian Locations

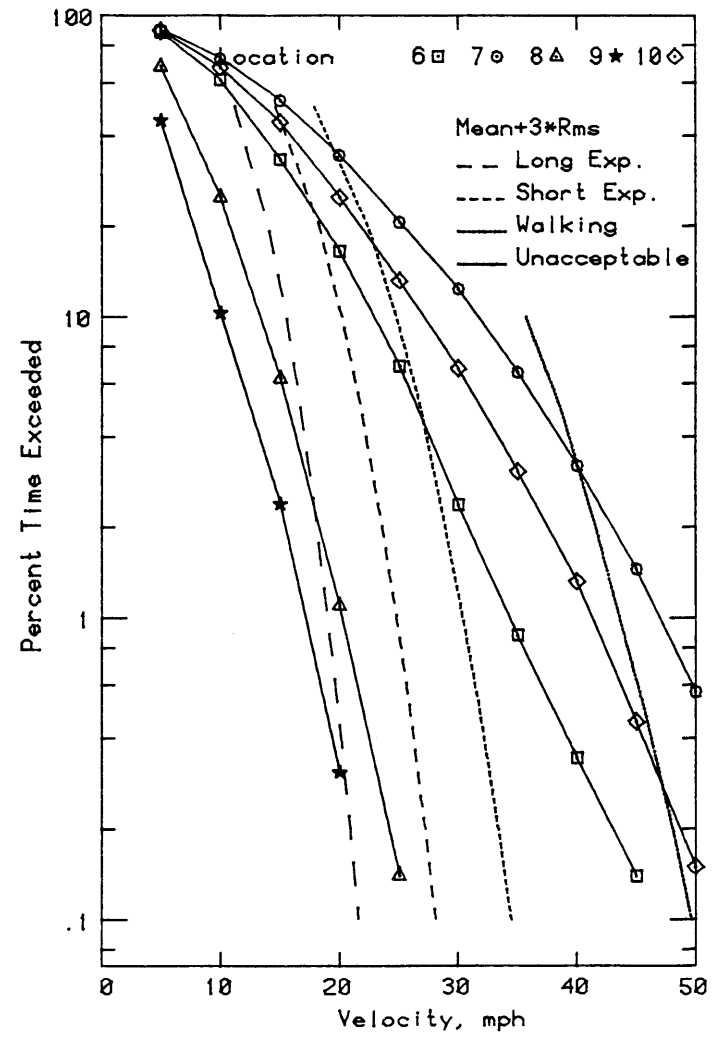
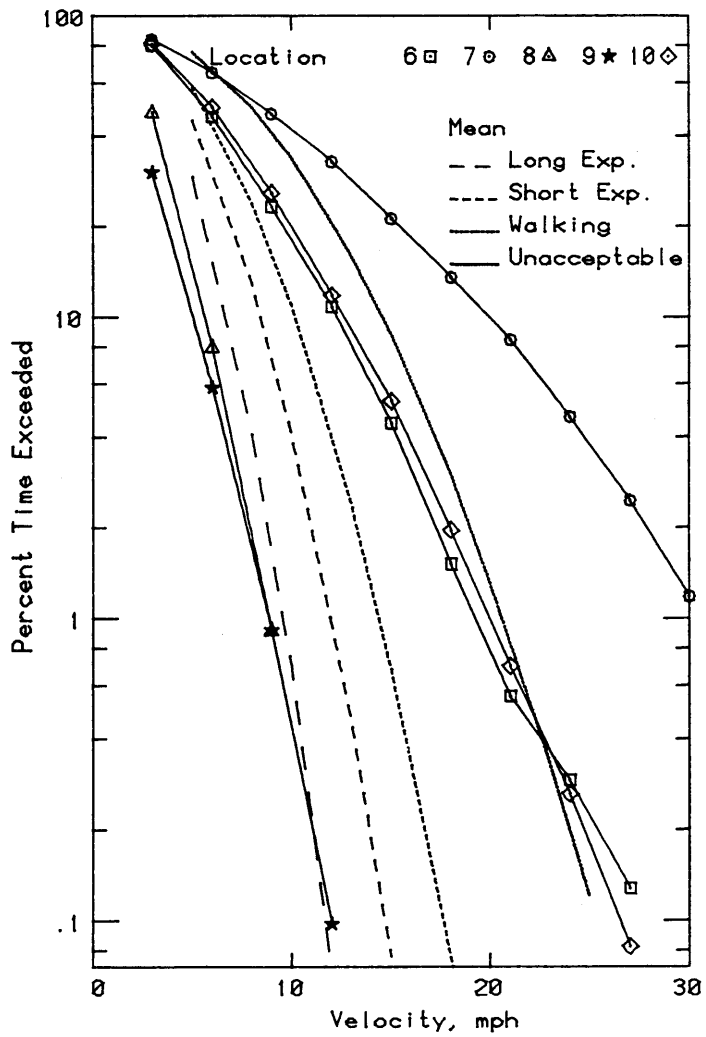


Figure 11b. Wind Velocity Probabilities for Pedestrian Locations

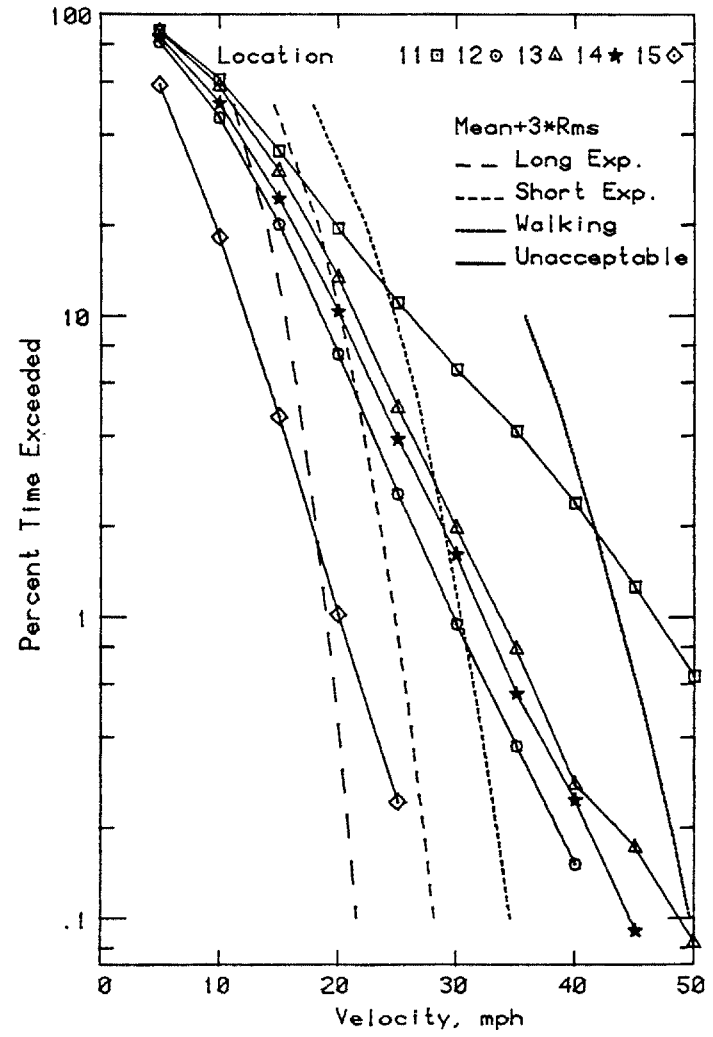
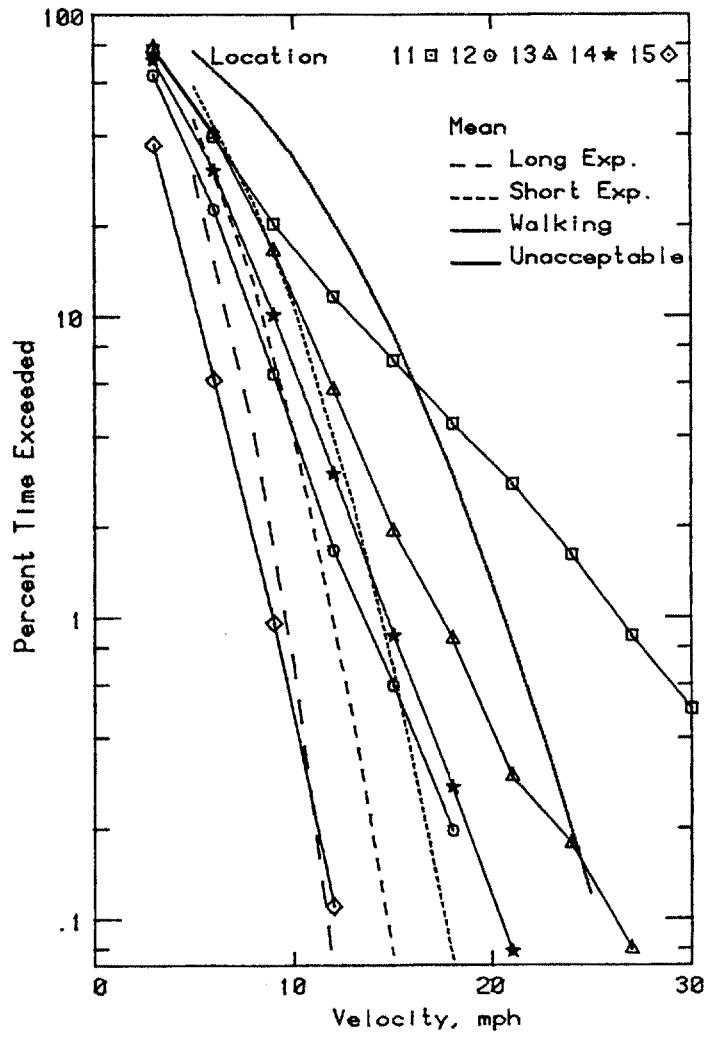


Figure 11c. Wind Velocity Probabilities for Pedestrian Locations

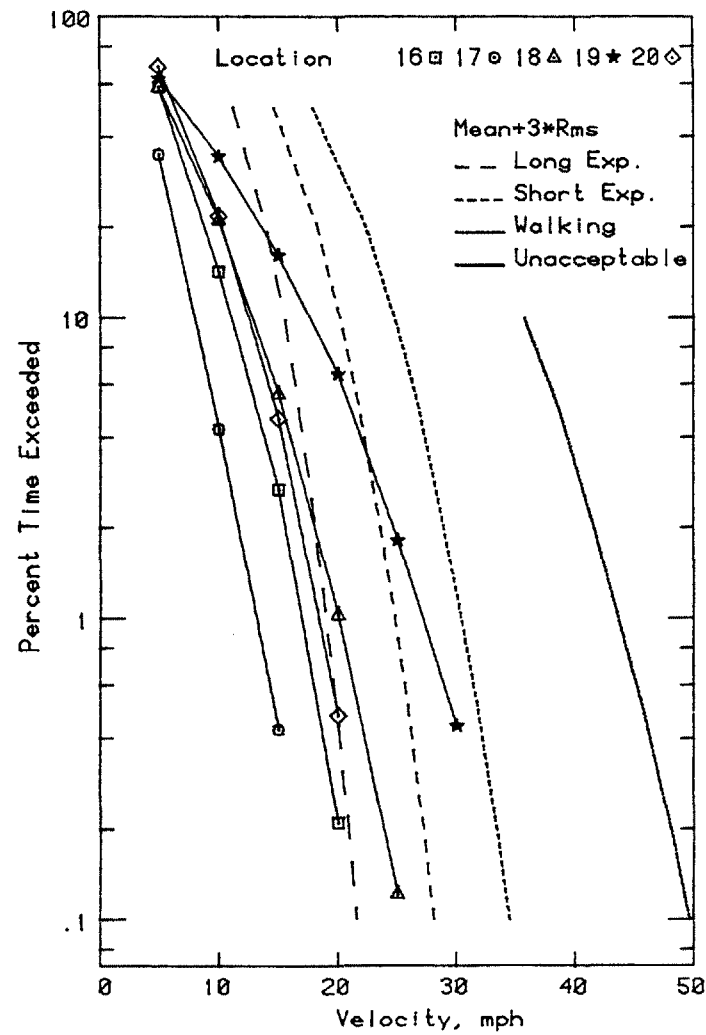
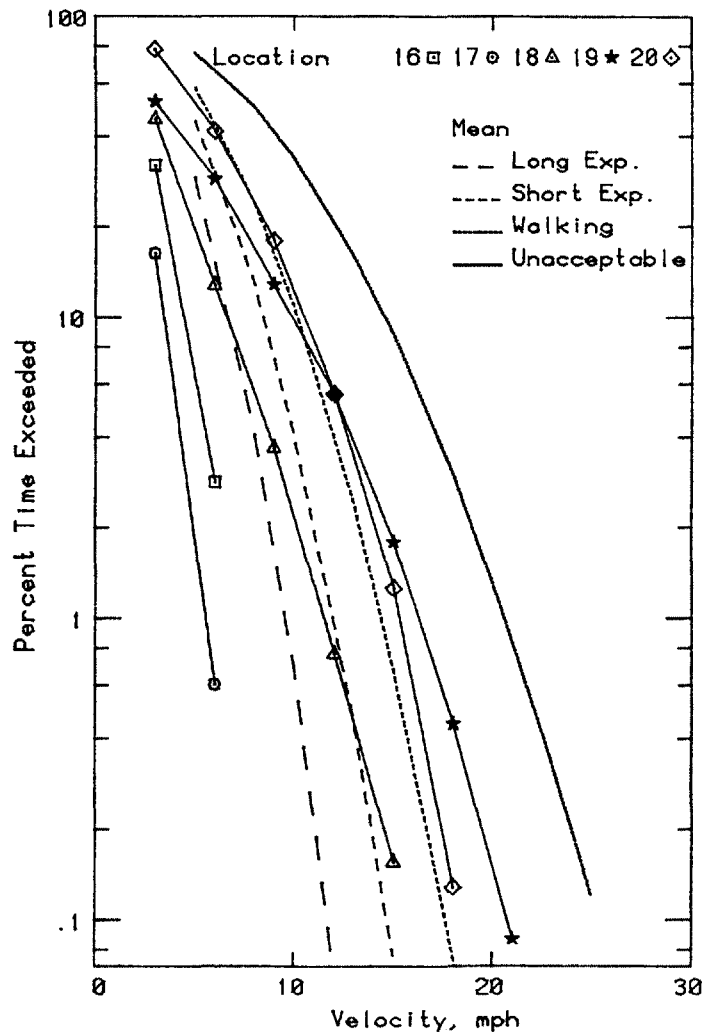


Figure 11d. Wind Velocity Probabilities for Pedestrian Locations

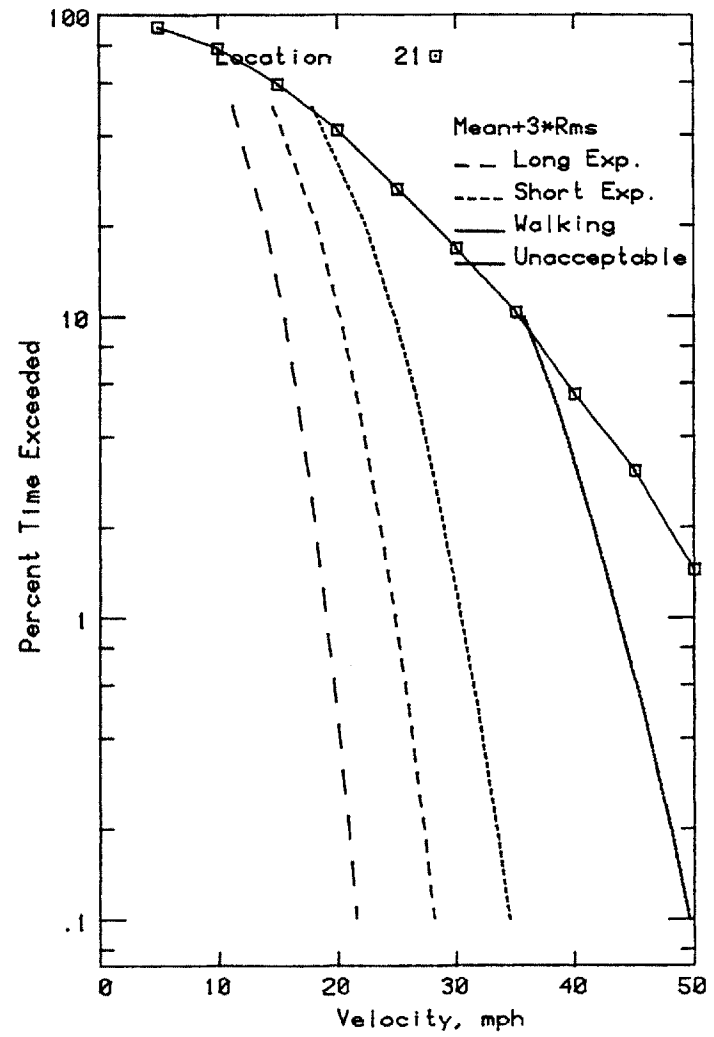
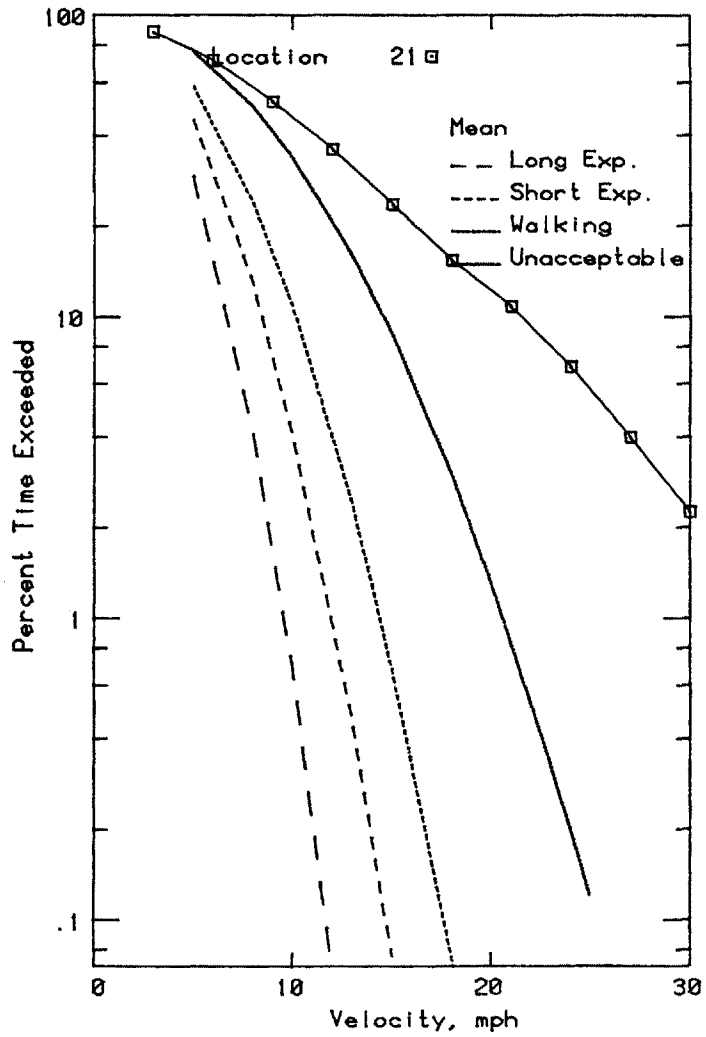


Figure 11e. Wind Velocity Probabilities for Pedestrian Locations

NORTH ELEVATION
NEGATIVE PEAK CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND.
REFERENCE PRESSURE = 30 PSF
WITH WIND DIRECTIONALITY

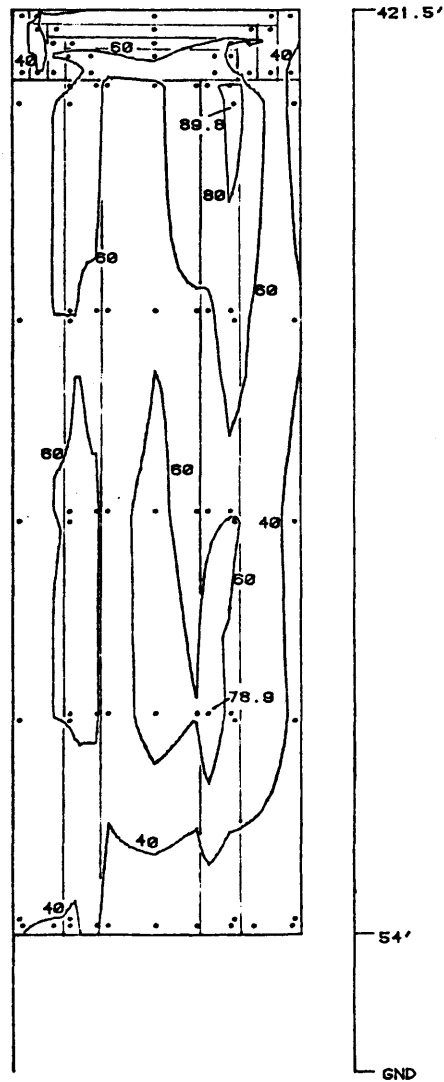


Figure 12a. Peak Pressure Contours on the Building for Cladding Loads

EAST ELEVATION
 NEGATIVE PEAK CLADDING LOADS (PSF)
 FOR 100 YEAR RECURRENCE WIND.
 REFERENCE PRESSURE = 30 PSF
 WITH WIND DIRECTIONALITY

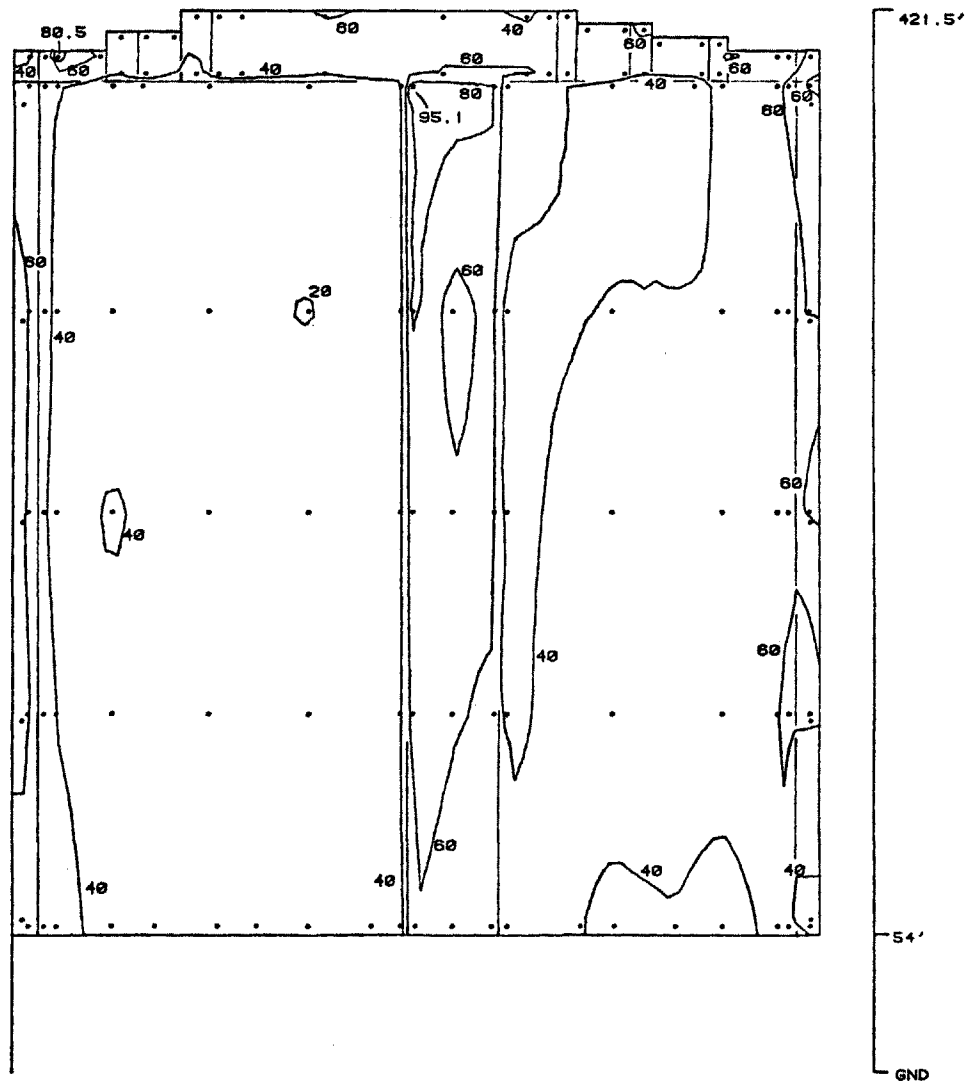


Figure 12b. Peak Pressure Contours on the Building
 for Cladding Loads

SOUTH ELEVATION
NEGATIVE PEAK CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND.
REFERENCE PRESSURE = 30 PSF
WITH WIND DIRECTIONALITY

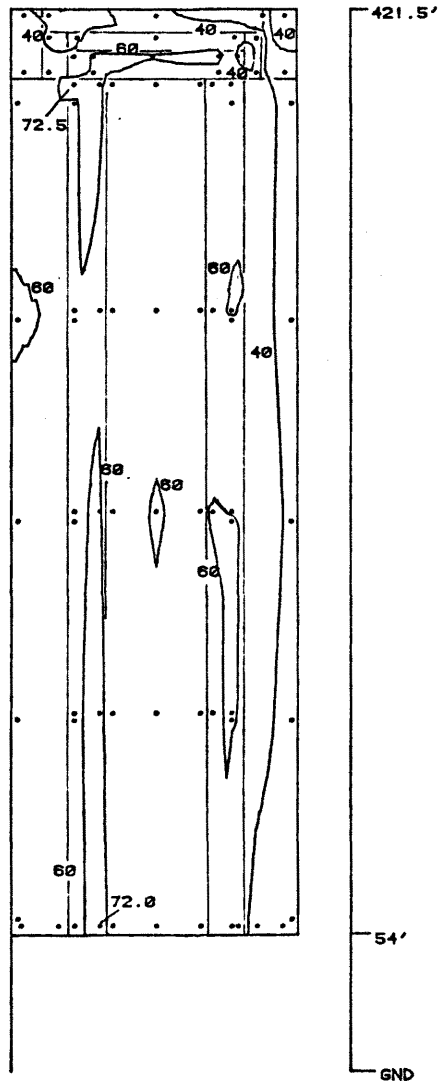


Figure 12c. Peak Pressure Contours on the Building for Cladding Loads

WEST ELEVATION
NEGATIVE PEAK CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND.
REFERENCE PRESSURE = 30 PSF
WITH WIND DIRECTIONALITY

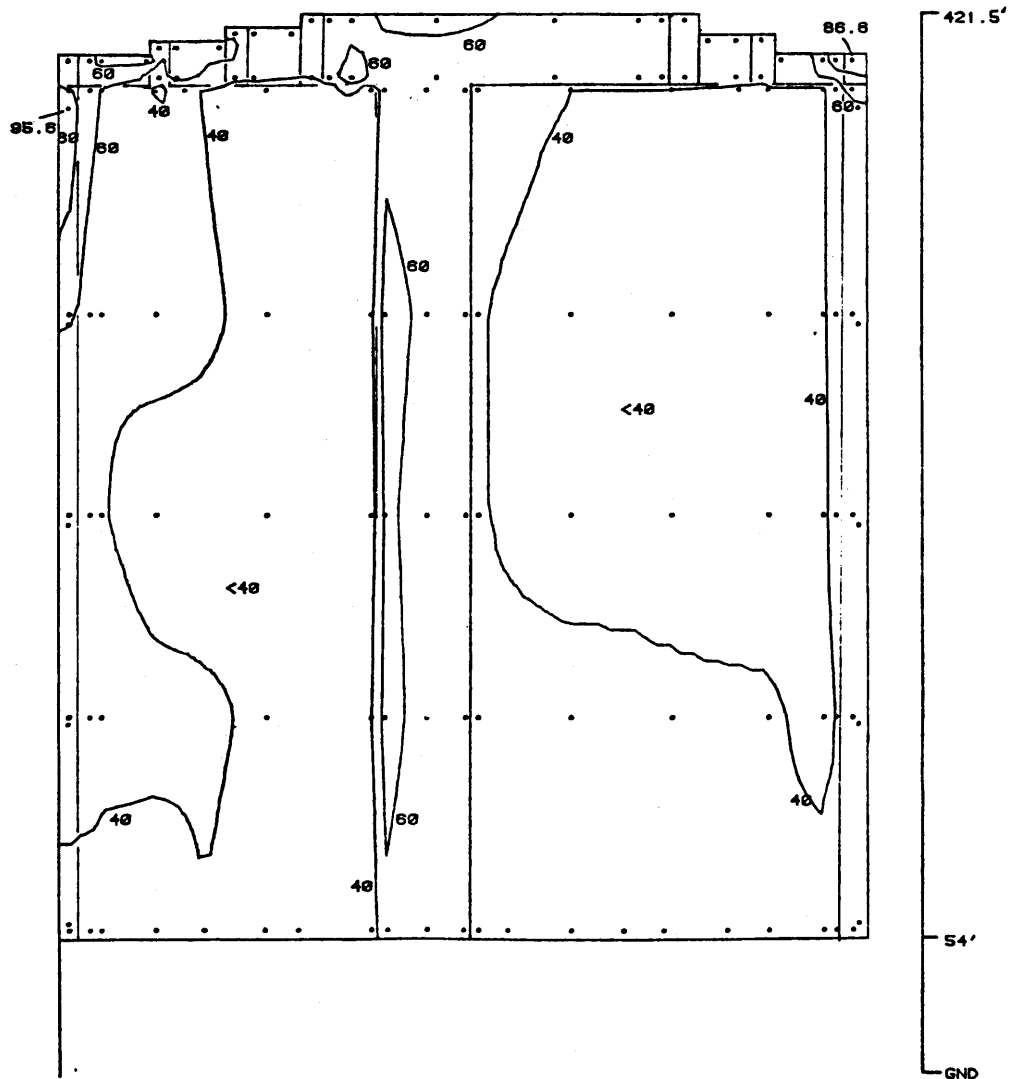
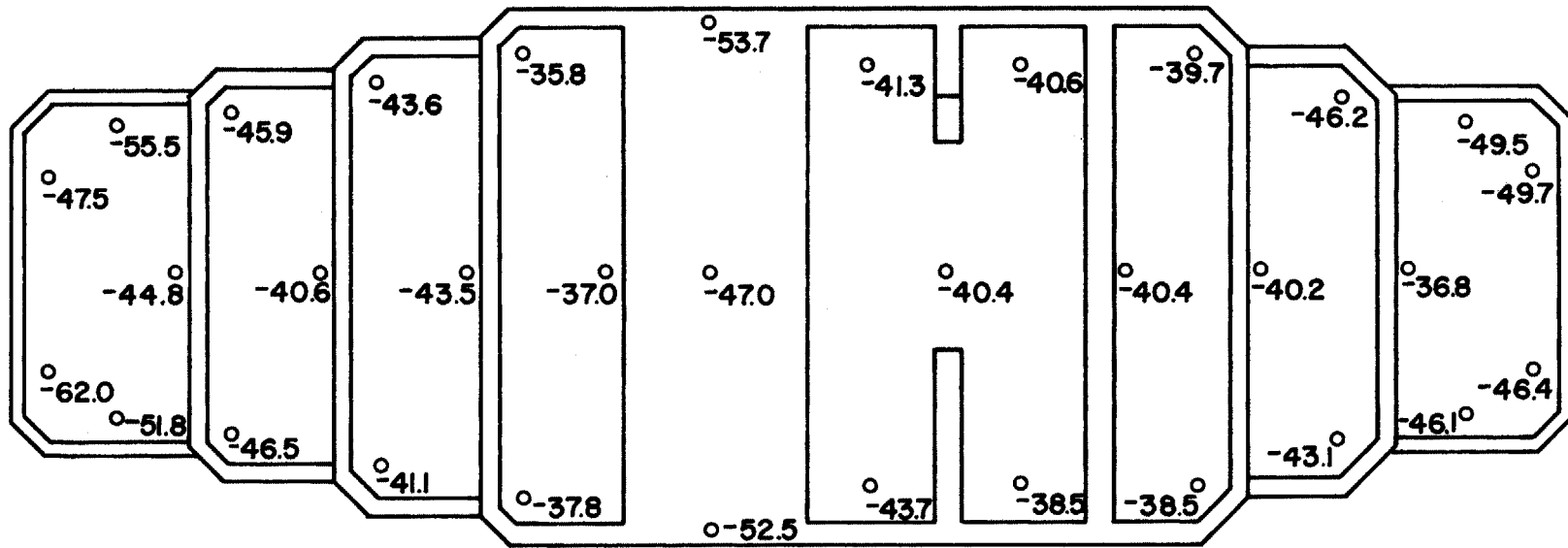


Figure 12d. Peak Pressure Contours on the Building for Cladding Loads



Negative peak cladding loads for 100 year recurrence wind.
 Reference pressure = 30 PSF with wind directionality.

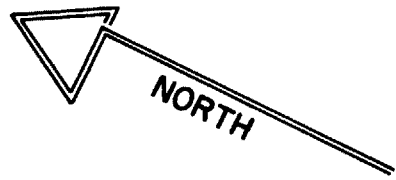


Figure 12e. Peak Pressure Contours on the Building for Cladding Loads

NORTH ELEVATION
POSITIVE PEAK CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND.
REFERENCE PRESSURE = 30 PSF
WITH WIND DIRECTIONALITY

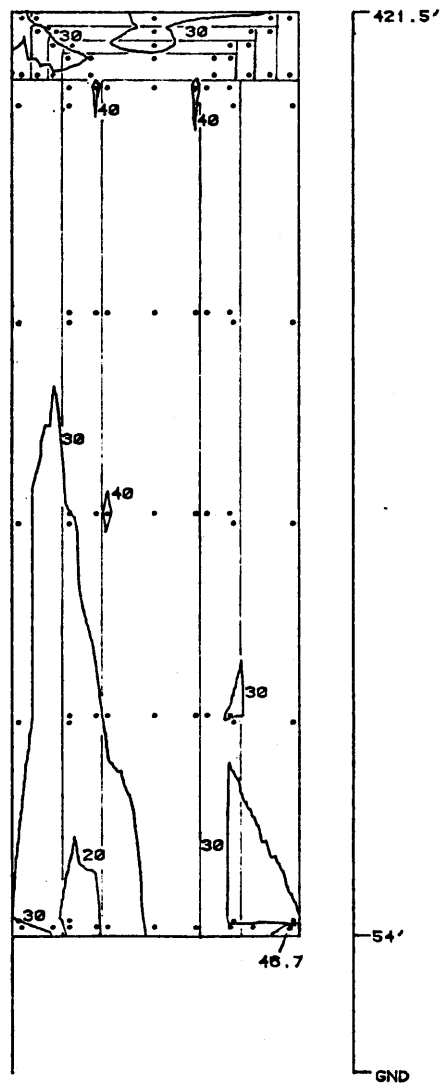


Figure 12f. Peak Pressure Contours on the Building for Cladding Loads

EAST ELEVATION
 POSITIVE PEAK CLADDING LOADS (PSF)
 FOR 100 YEAR RECURRENCE WIND.
 REFERENCE PRESSURE = 30 PSF
 WITH WIND DIRECTIONALITY

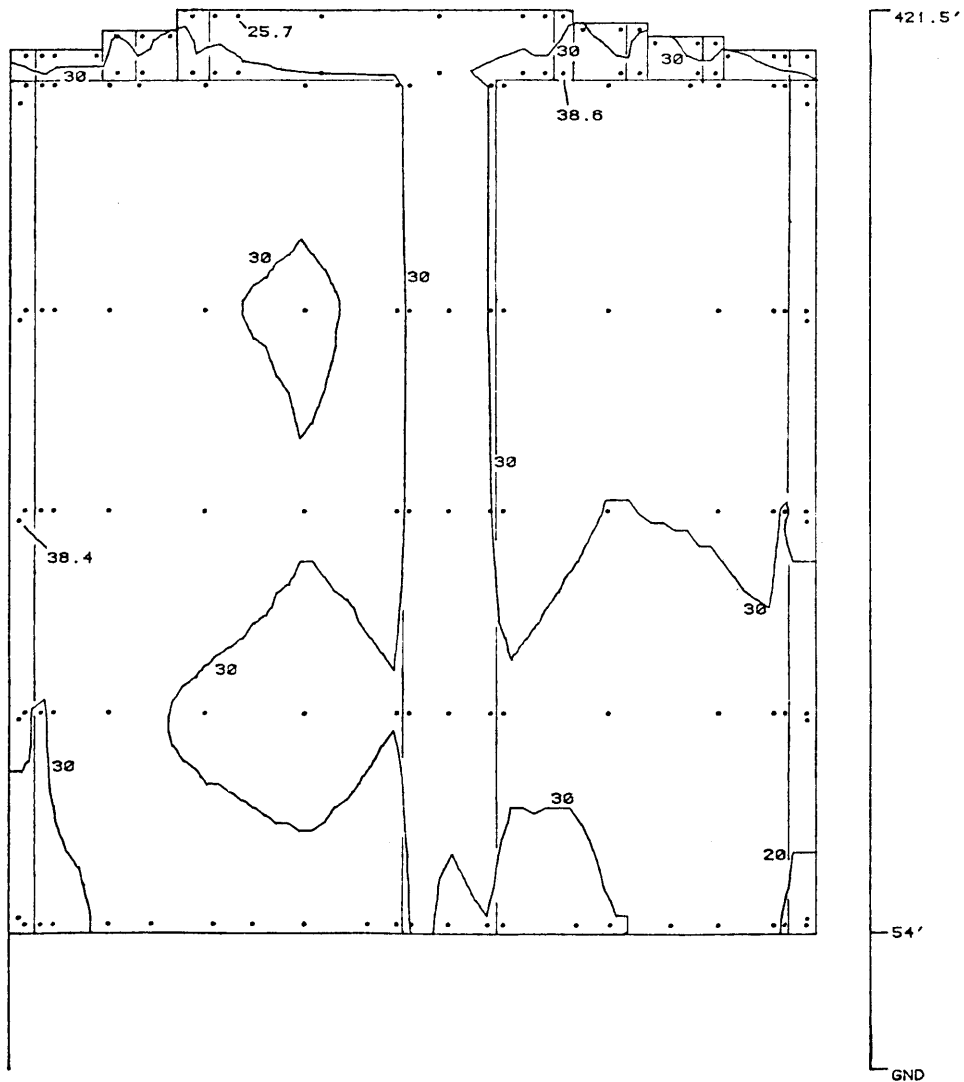


Figure 12g. Peak Pressure Contours on the Building for Cladding Loads

SOUTH ELEVATION
 POSITIVE PEAK CLADDING LOADS (PSF)
 FOR 100 YEAR RECURRENCE WIND.
 REFERENCE PRESSURE = 30 PSF
 WITH WIND DIRECTIONALITY

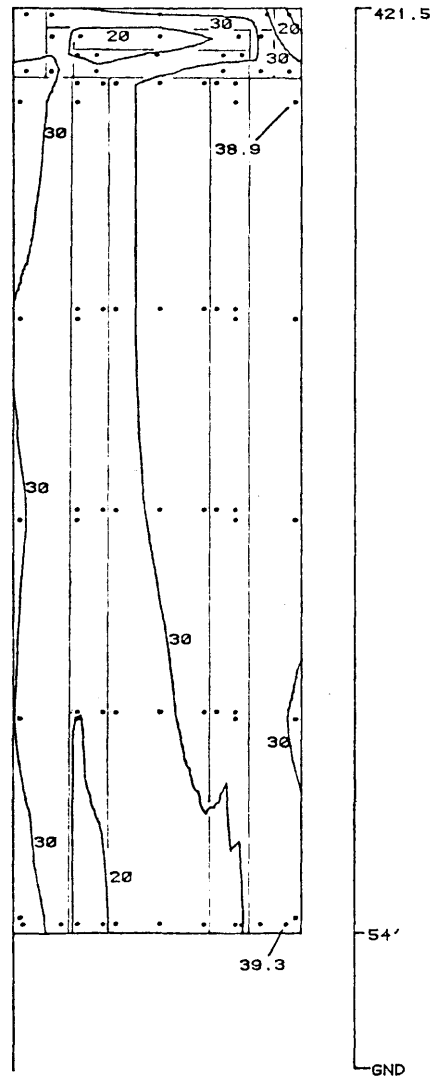


Figure 12h. Peak Pressure Contours on the Building for Cladding Loads

WEST ELEVATION
POSITIVE PEAK CLADDING LOADS (PSF)
FOR 100 YEAR RECURRENCE WIND.
REFERENCE PRESSURE = 30 PSF
WITH WIND DIRECTIONALITY

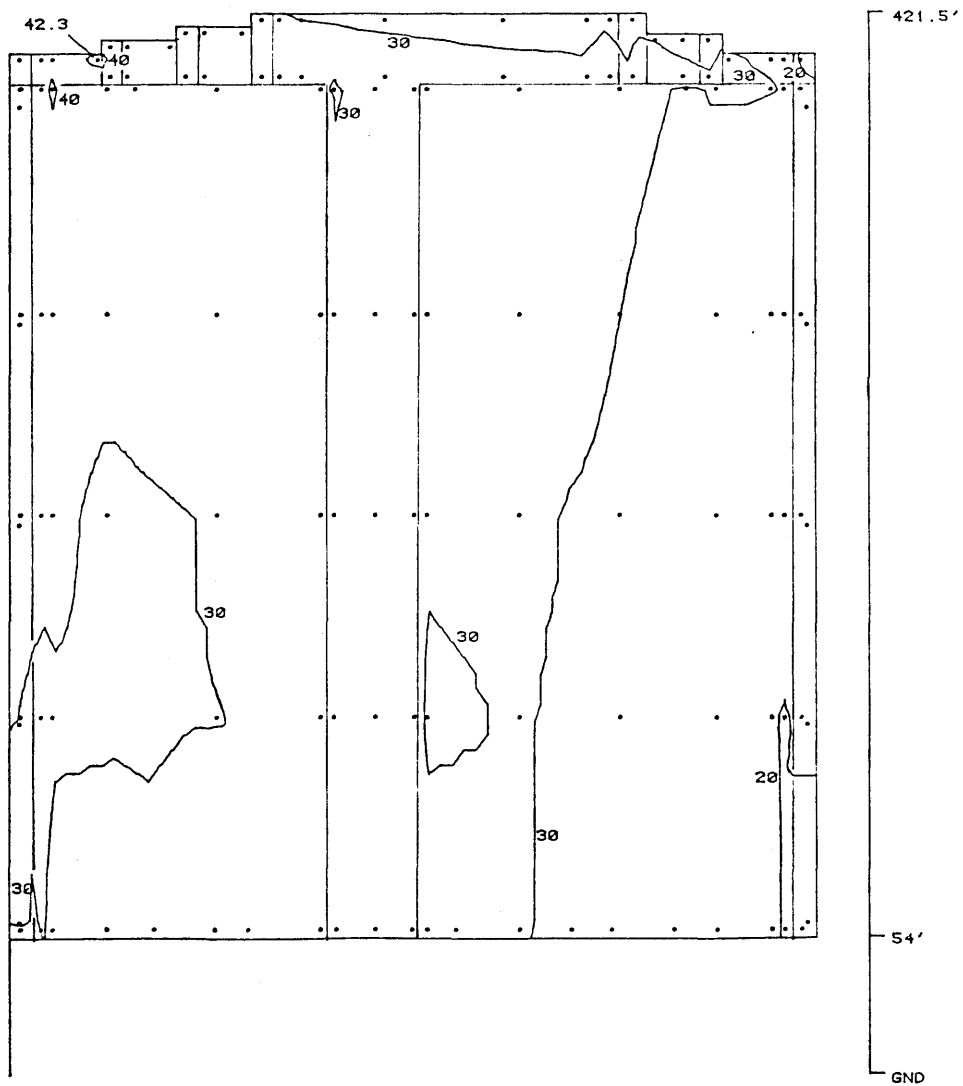
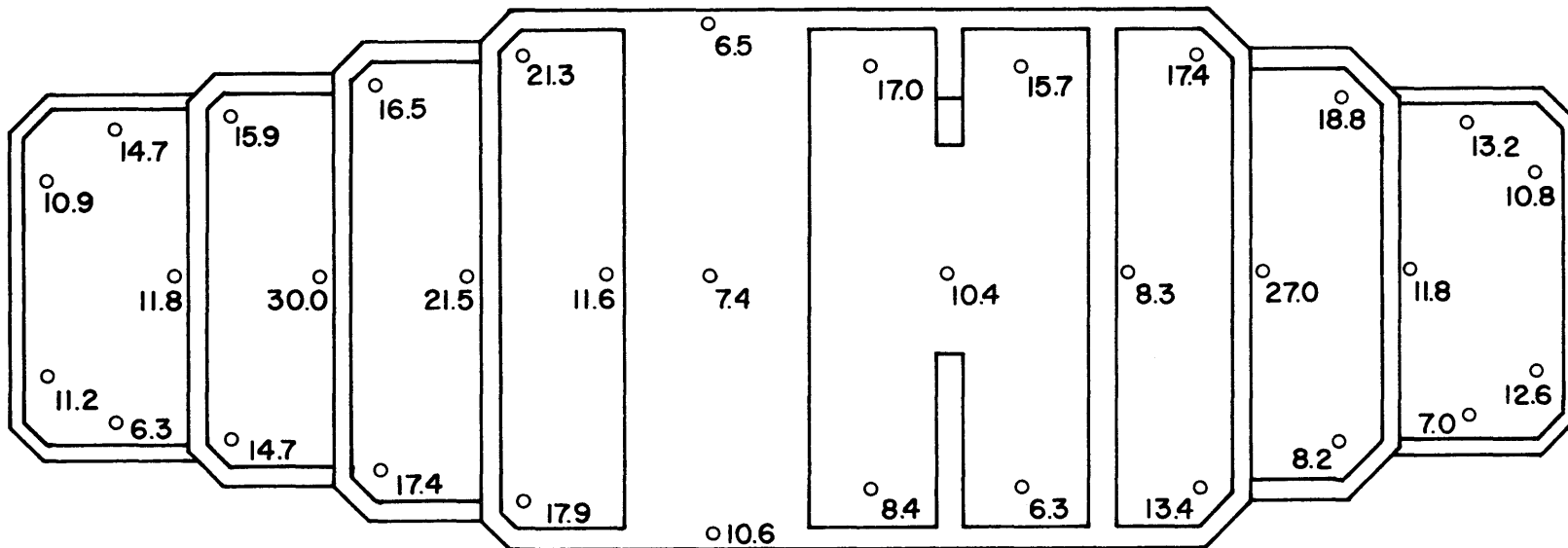


Figure 12i. Peak Pressure Contours on the Building
for Cladding Loads



Positive peak cladding loads for 100 year recurrence wind
 Reference pressure = 30 PSF with wind directionality

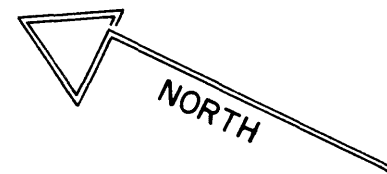
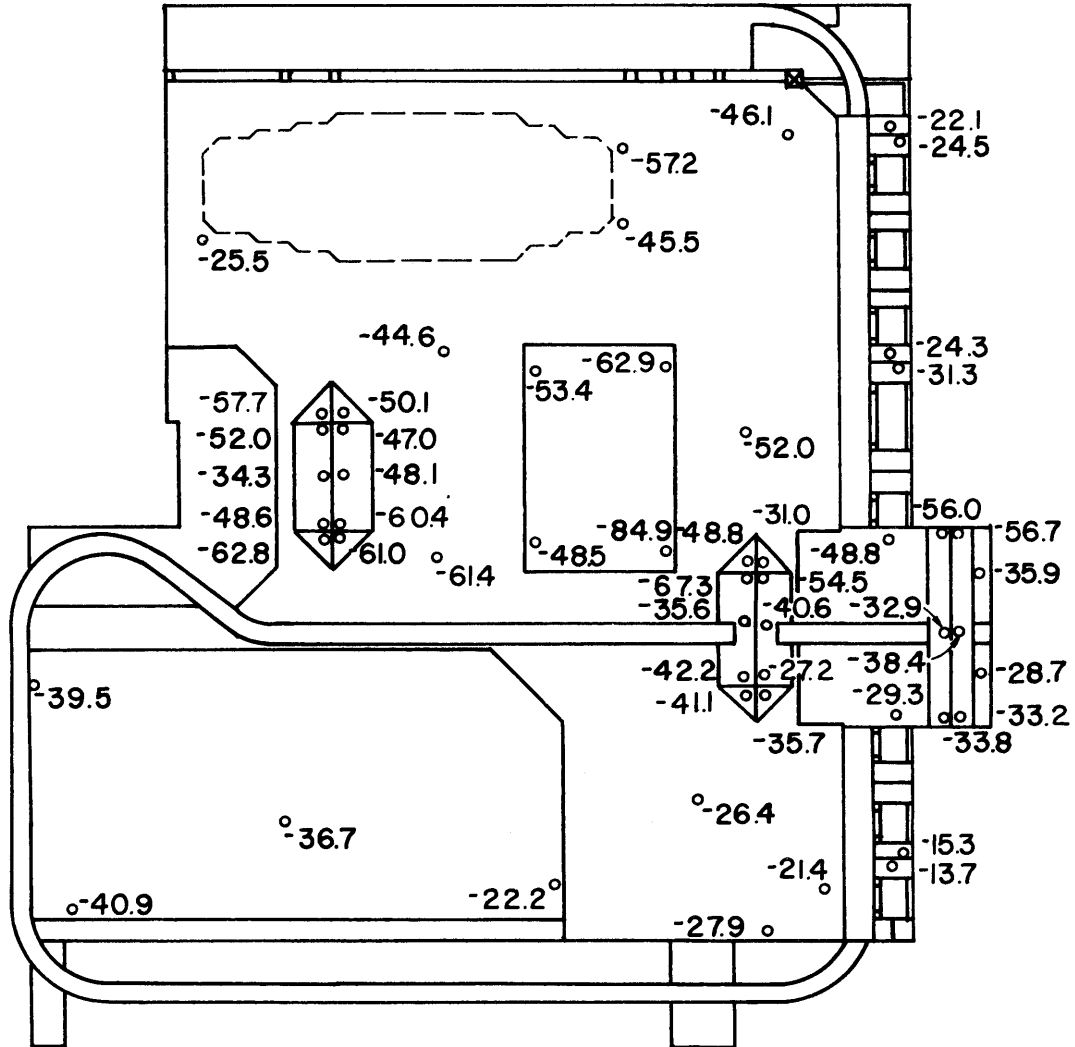


Figure 12j. Peak Pressure Contours on the Building for Cladding Loads

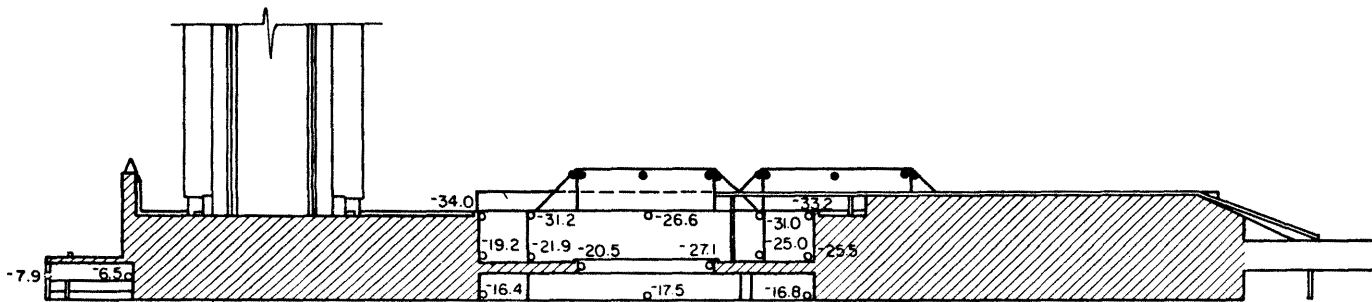


ROOF PLAN

NEGATIVE PEAK CLADDING LOADS (PSF) FOR 100 YEAR RECURRENCE WIND.

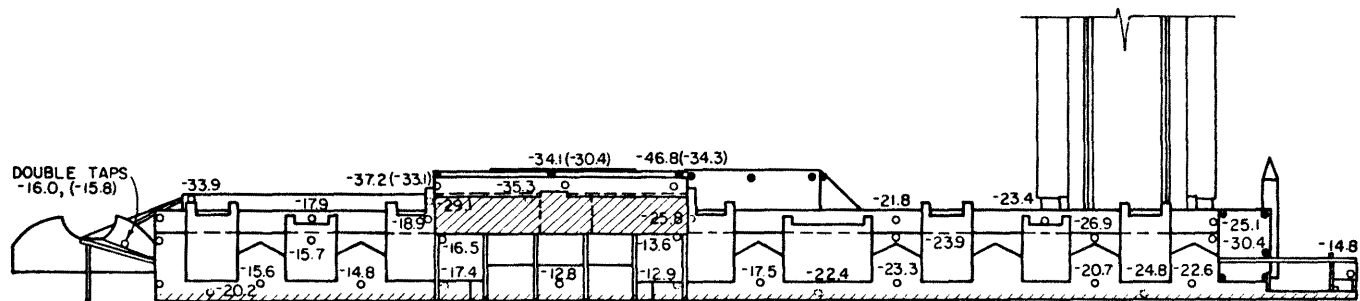
REFERENCE PRESSURE = 30 PSF WITH WIND DIRECTIONALITY

Figure 12k. Peak Pressure Contours on the Building for Cladding Loads



NORTH

Negative peak cladding loads for 100 year recurrence wind. Reference pressure = 30PSF wind directionality.



SOUTH

Figure 121. Peak Pressure Contours on the Building for Cladding Loads

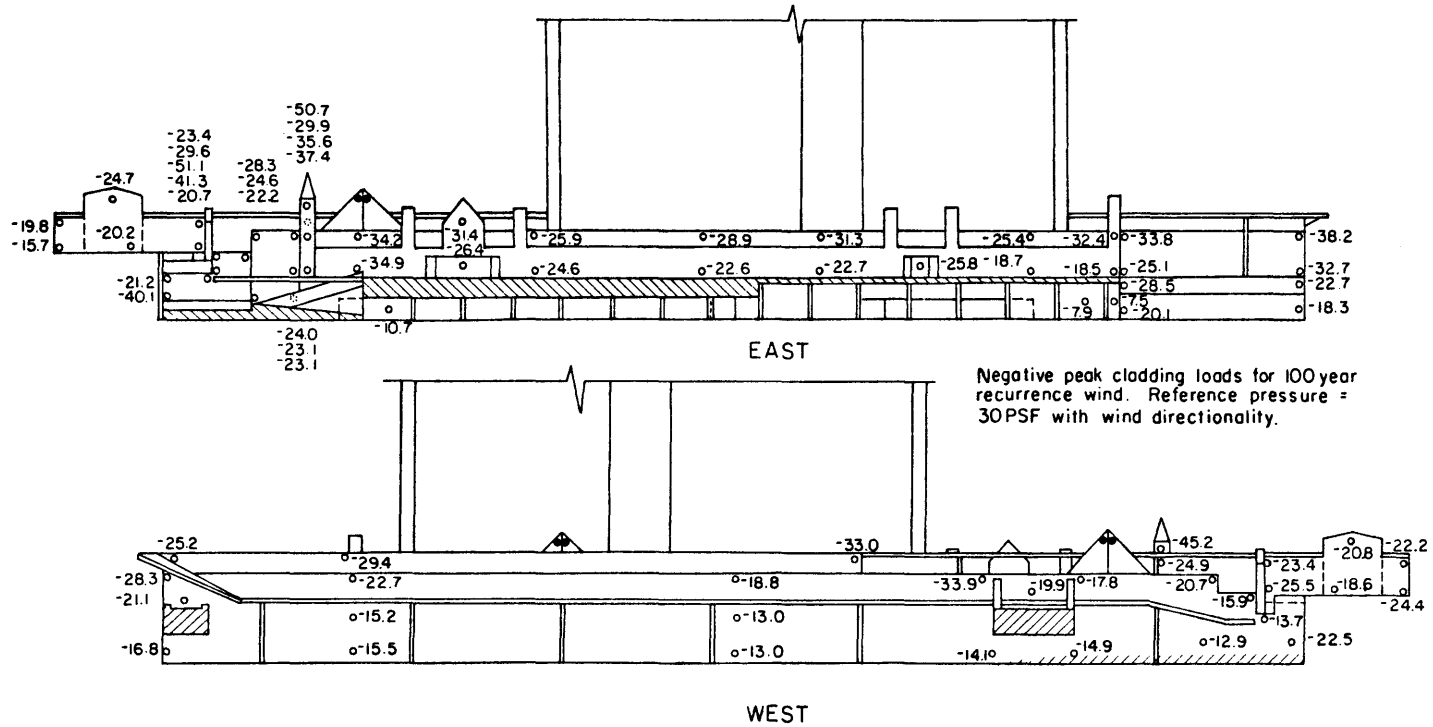
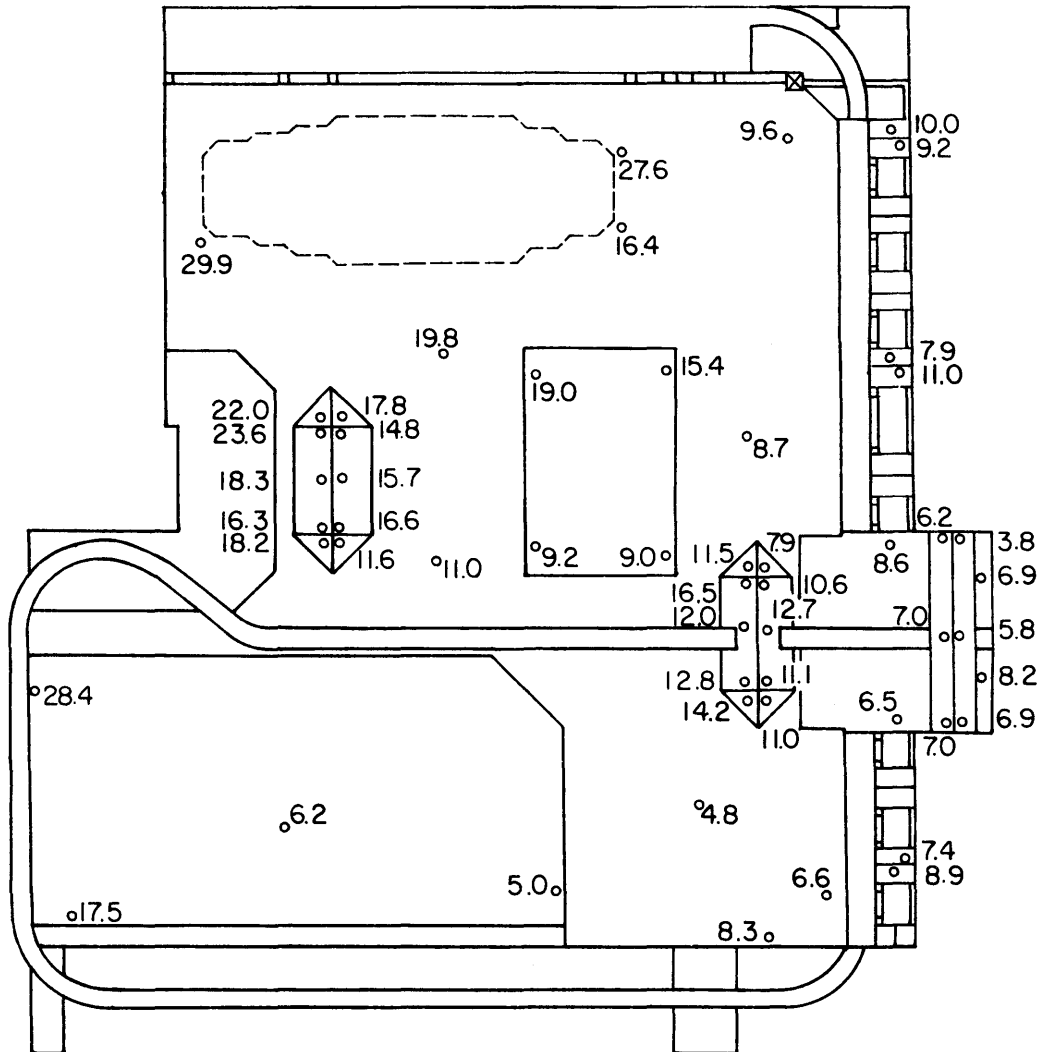
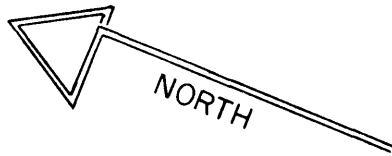


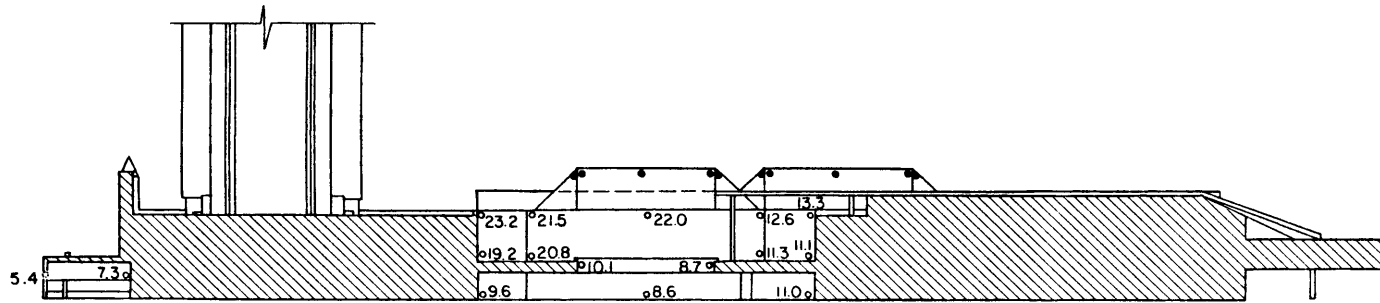
Figure 12m. Peak Pressure Contours on the Building for Cladding Loads



ROOF PLAN

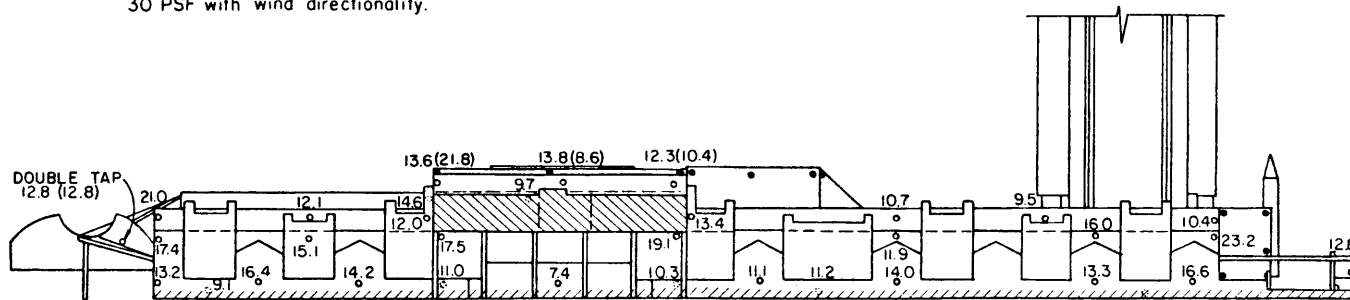
POSITIVE PEAK CLADDING LOADS FOR 100 YEAR RECURRENCE WIND.
 REFERENCE PRESSURE = 30 PSF WITH WIND DIRECTIONALITY.

Figure 12n. Peak Pressure Contours on the Building
 for Cladding Loads



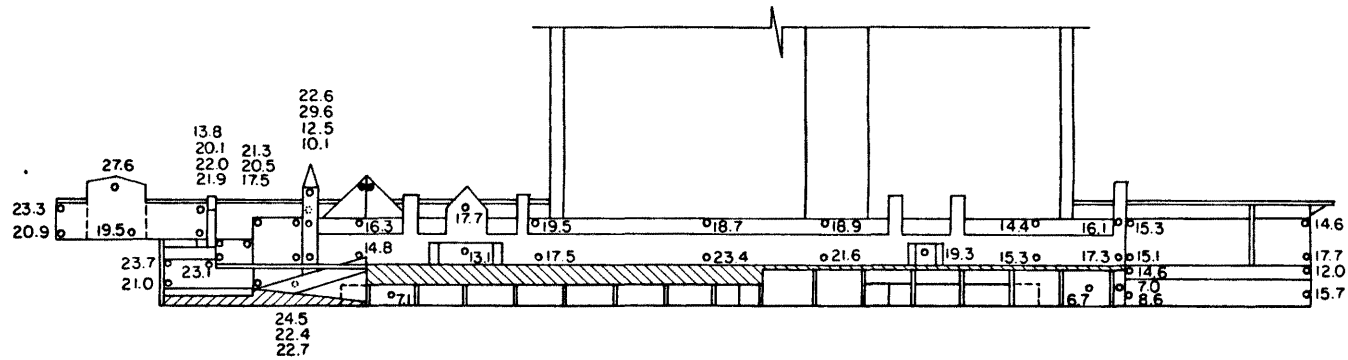
NORTH

Positive peak cladding loads for 100 year recurrence wind. Reference pressure = 30 PSF with wind directionality.



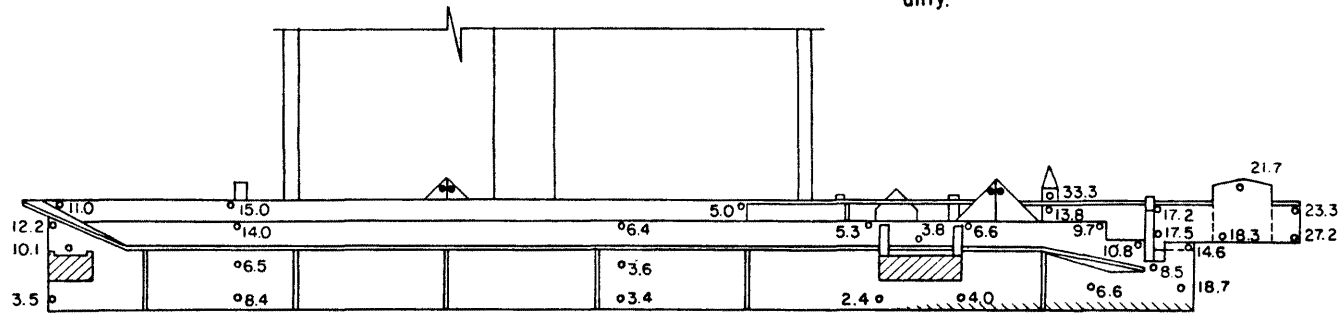
SOUTH

Figure 12o. Peak Pressure Contours on the Building for Cladding Loads



EAST

Positive peak cladding loads for 100 year recurrence wind. Reference pressure = 30 PSF with wind directionality.



WEST

Figure 12p. Peak Pressure Contours on the Building for Cladding Loads

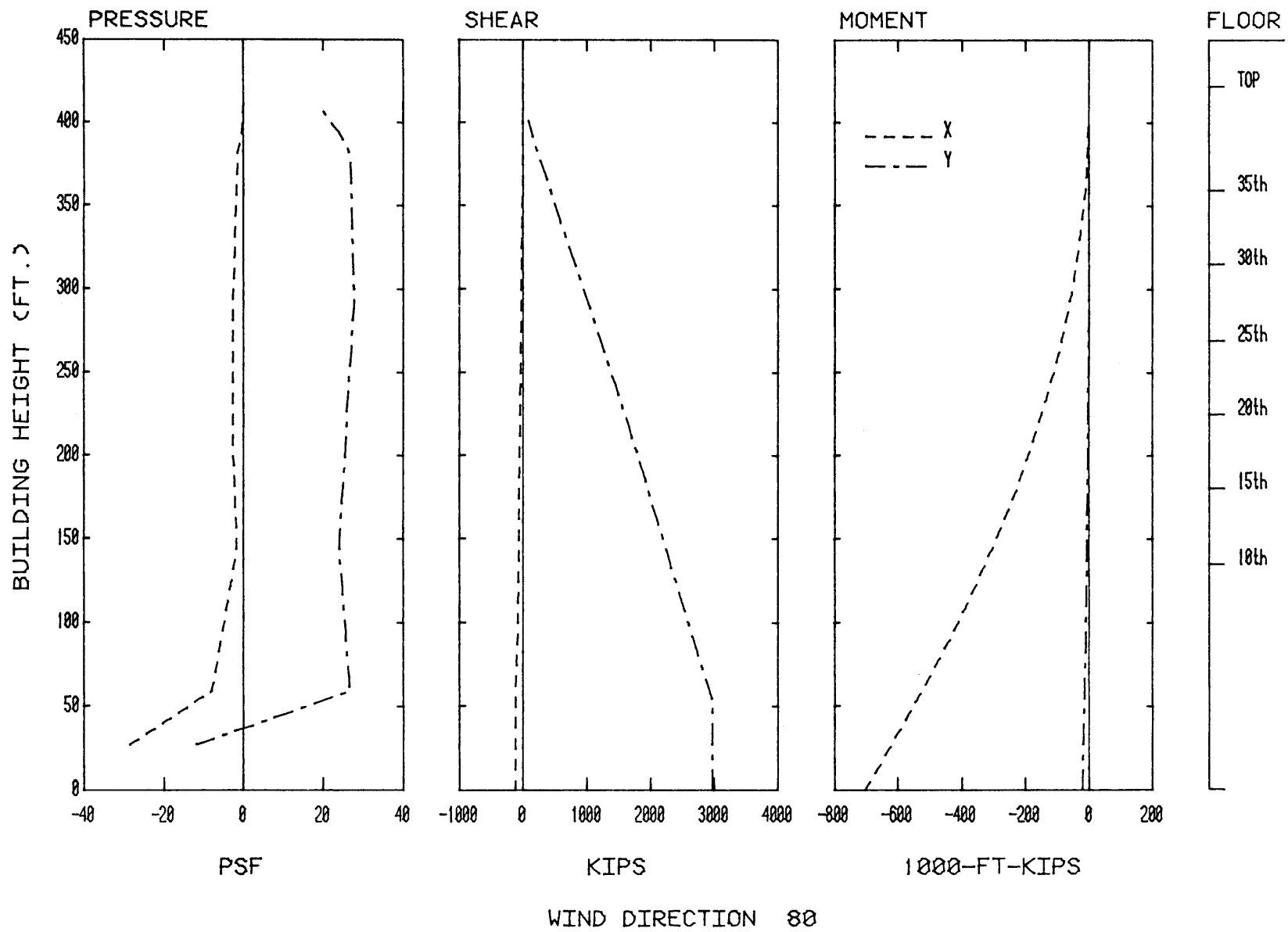


Figure 13. Load, Shear, and Moment Diagrams for Selected Wind Directions

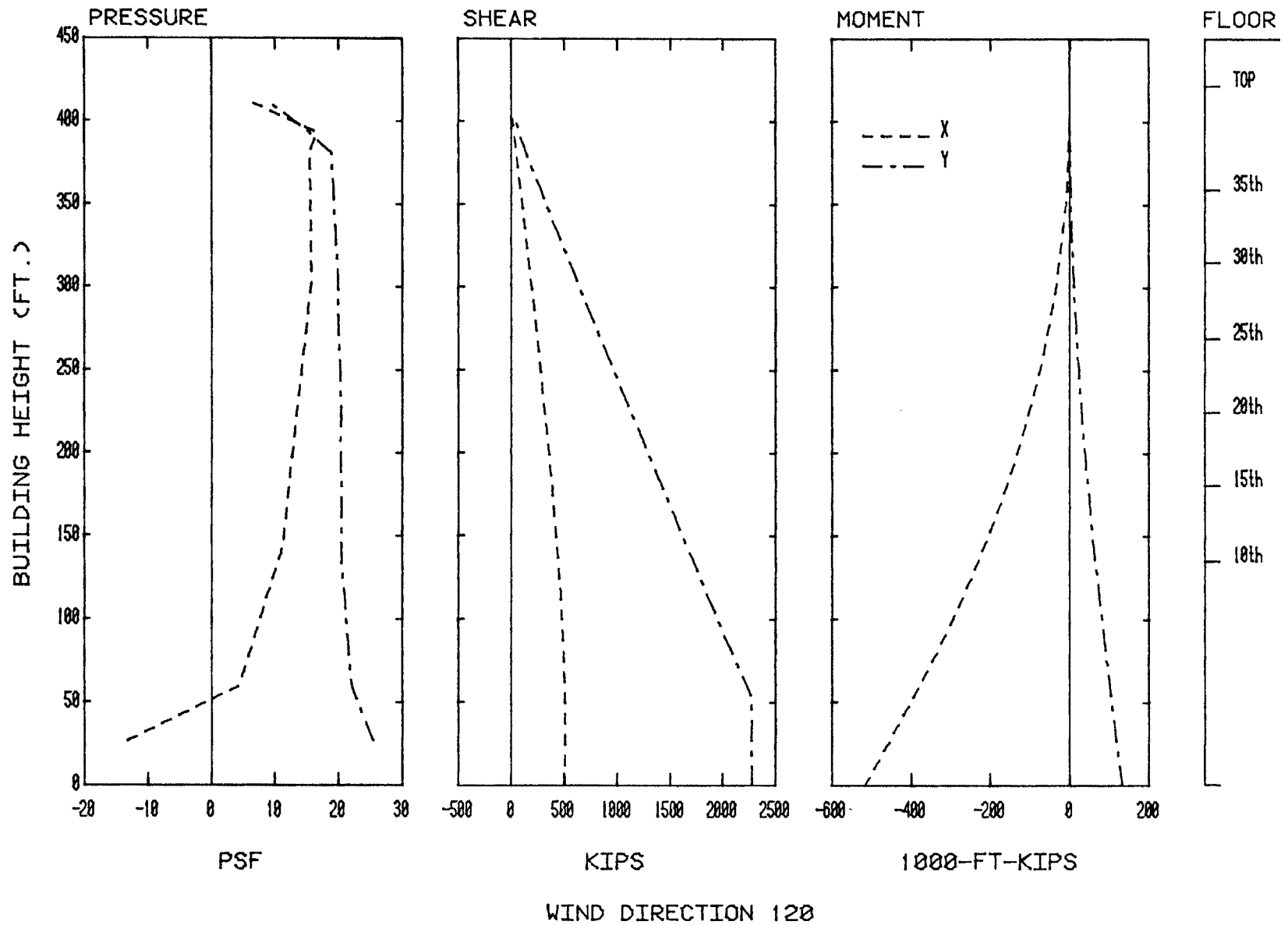
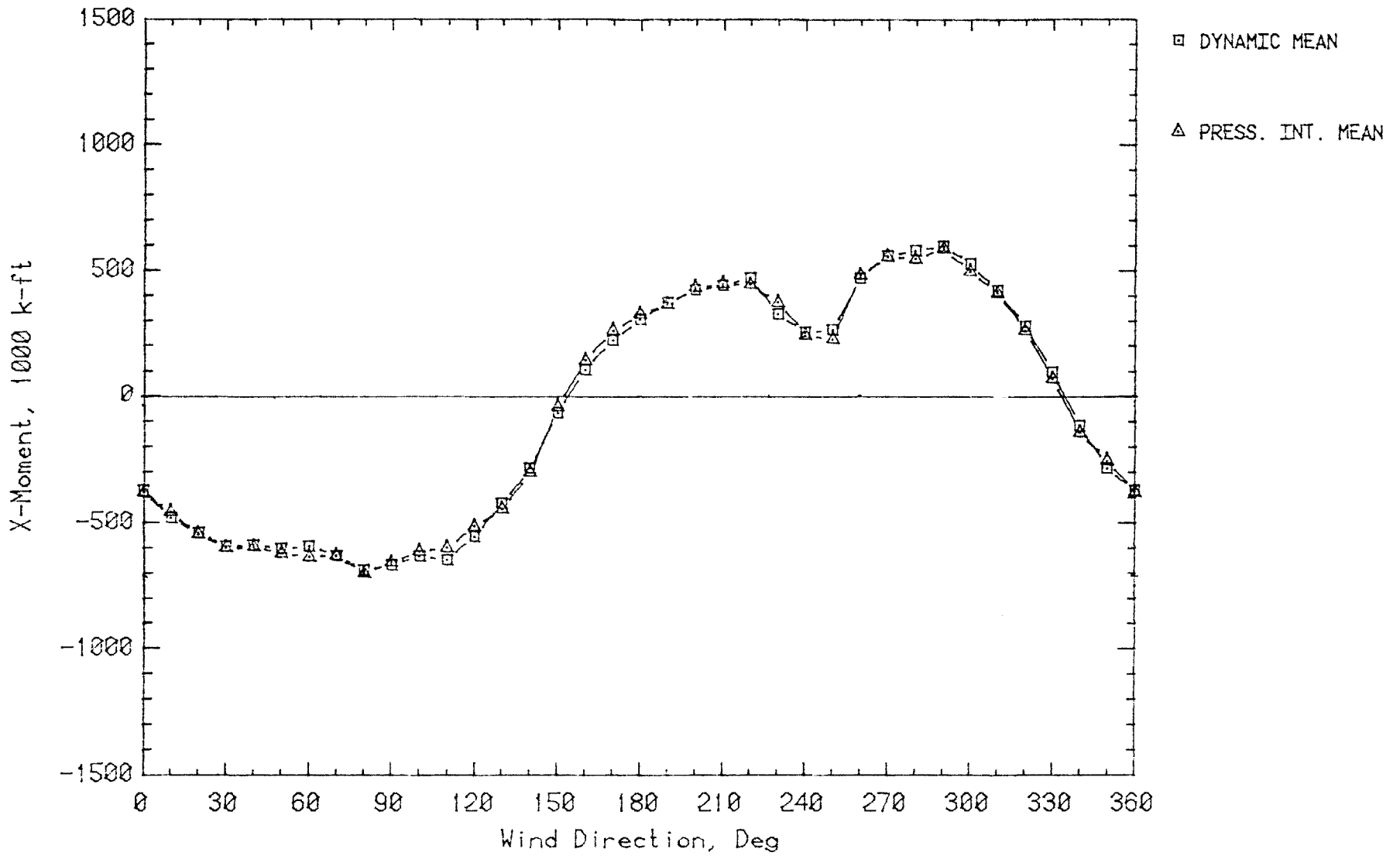
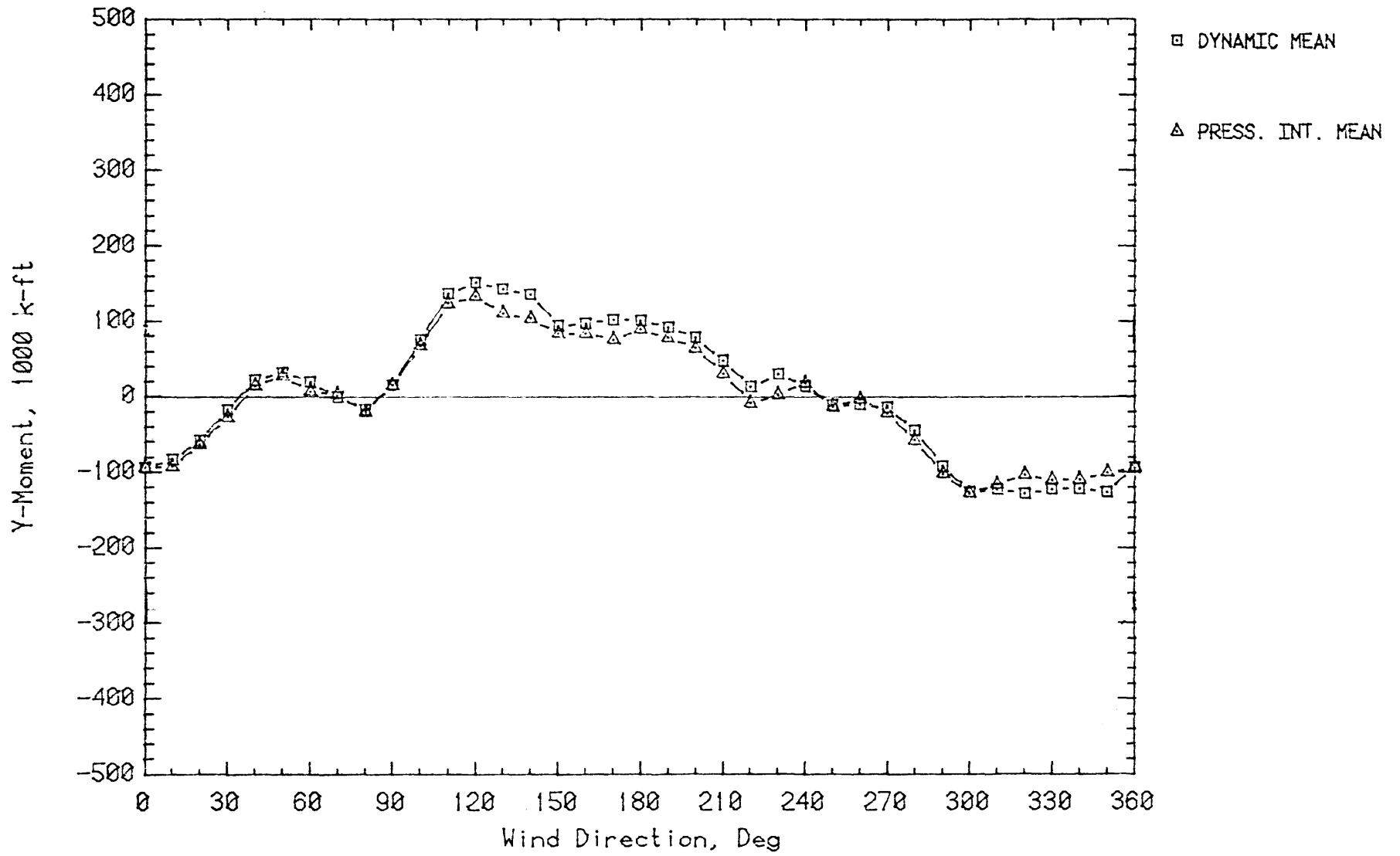


Figure 13. Load, Shear, and Moment Diagrams for Selected Wind Directions



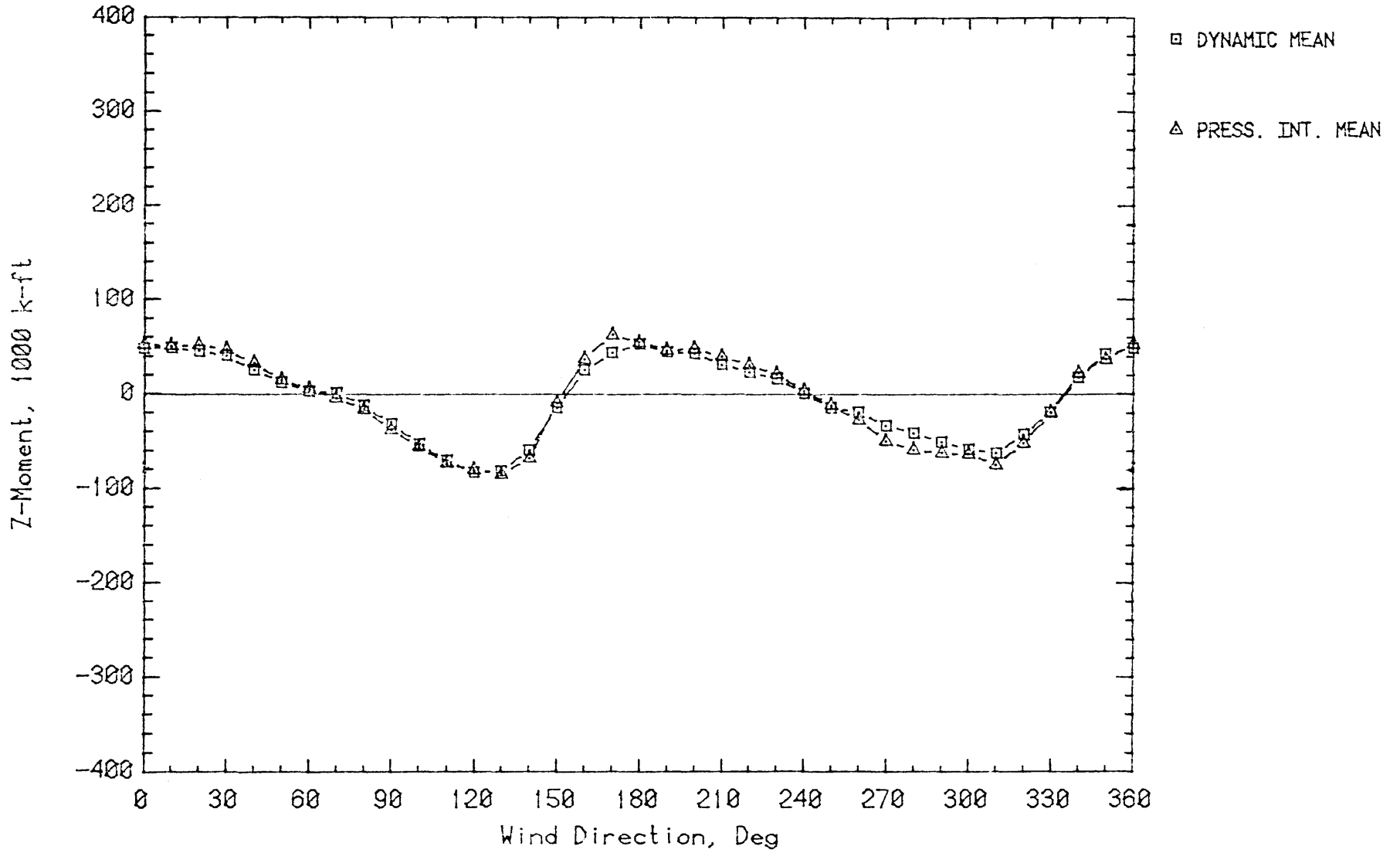
RESORTS HOTEL BASE MOMENTS FOR 100-YR WIND

Figure 14a. Comparison of Mean Base Moments Model Data



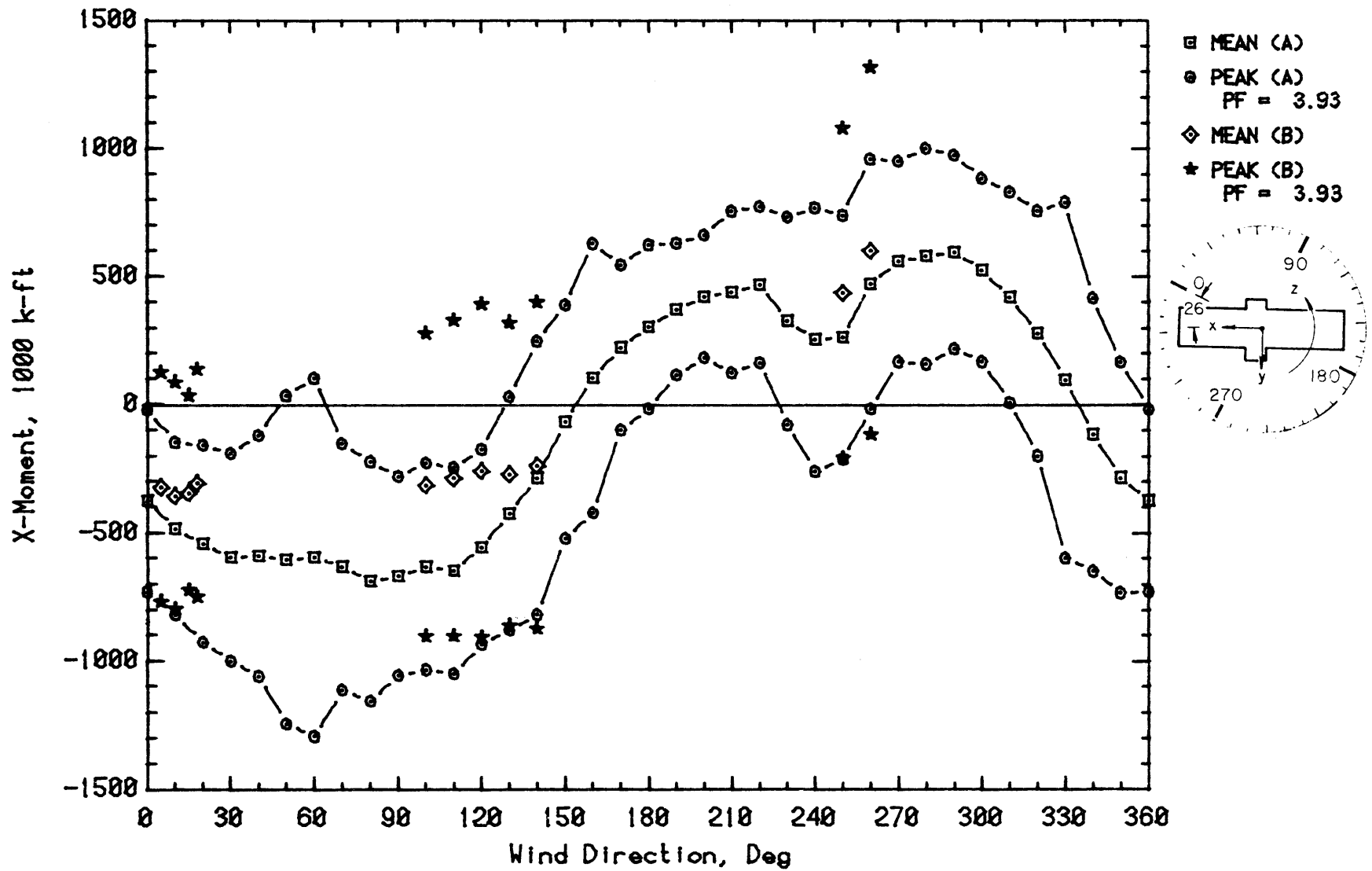
RESORTS HOTEL BASE MOMENTS FOR 100-YR WIND

Figure 14b. Comparison of Mean Base Moments Model Data



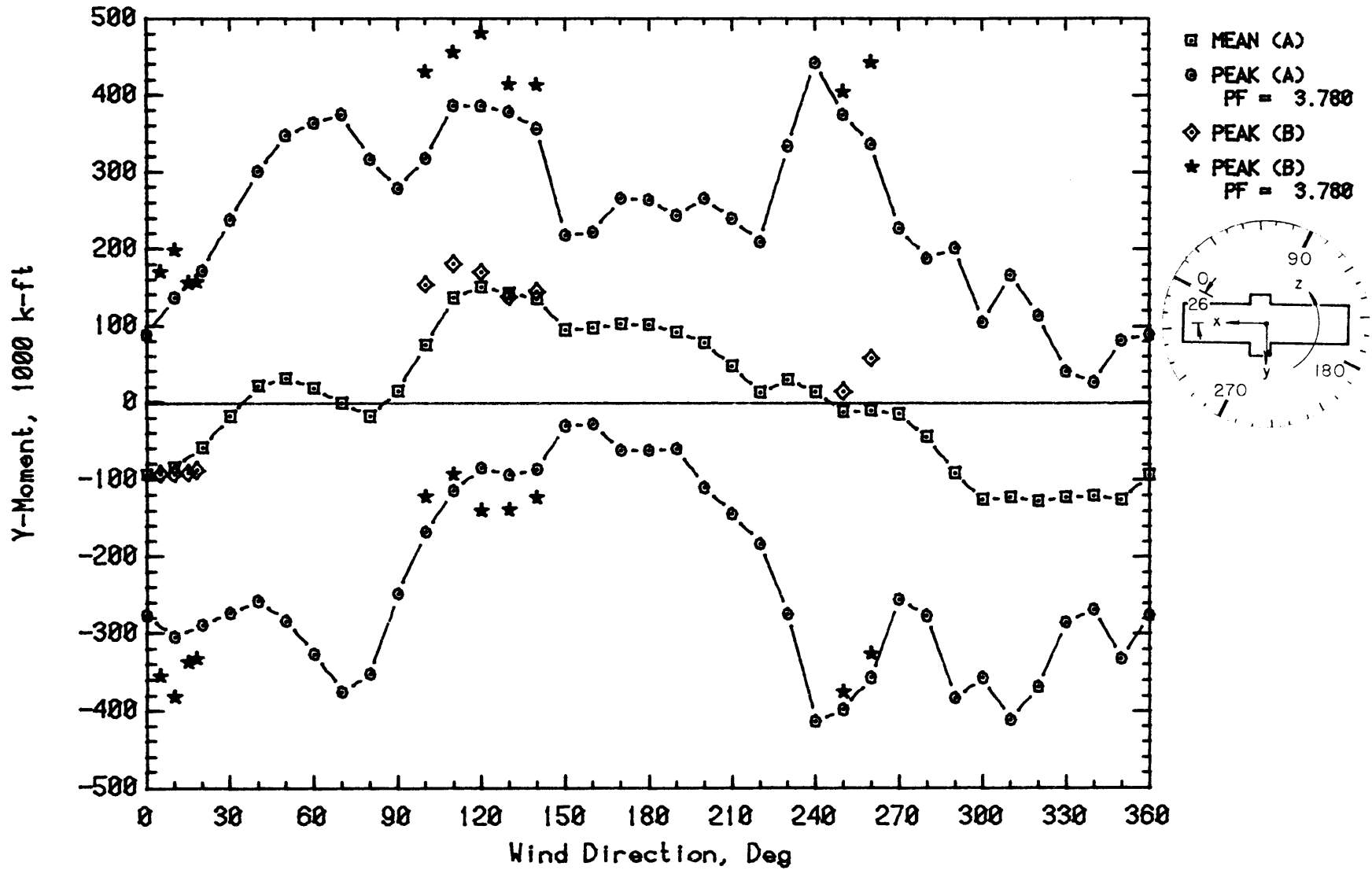
RESORTS HOTEL BASE MOMENTS FOR 100-YR WIND

Figure 14c. Comparison of Mean Base Moments Model Data



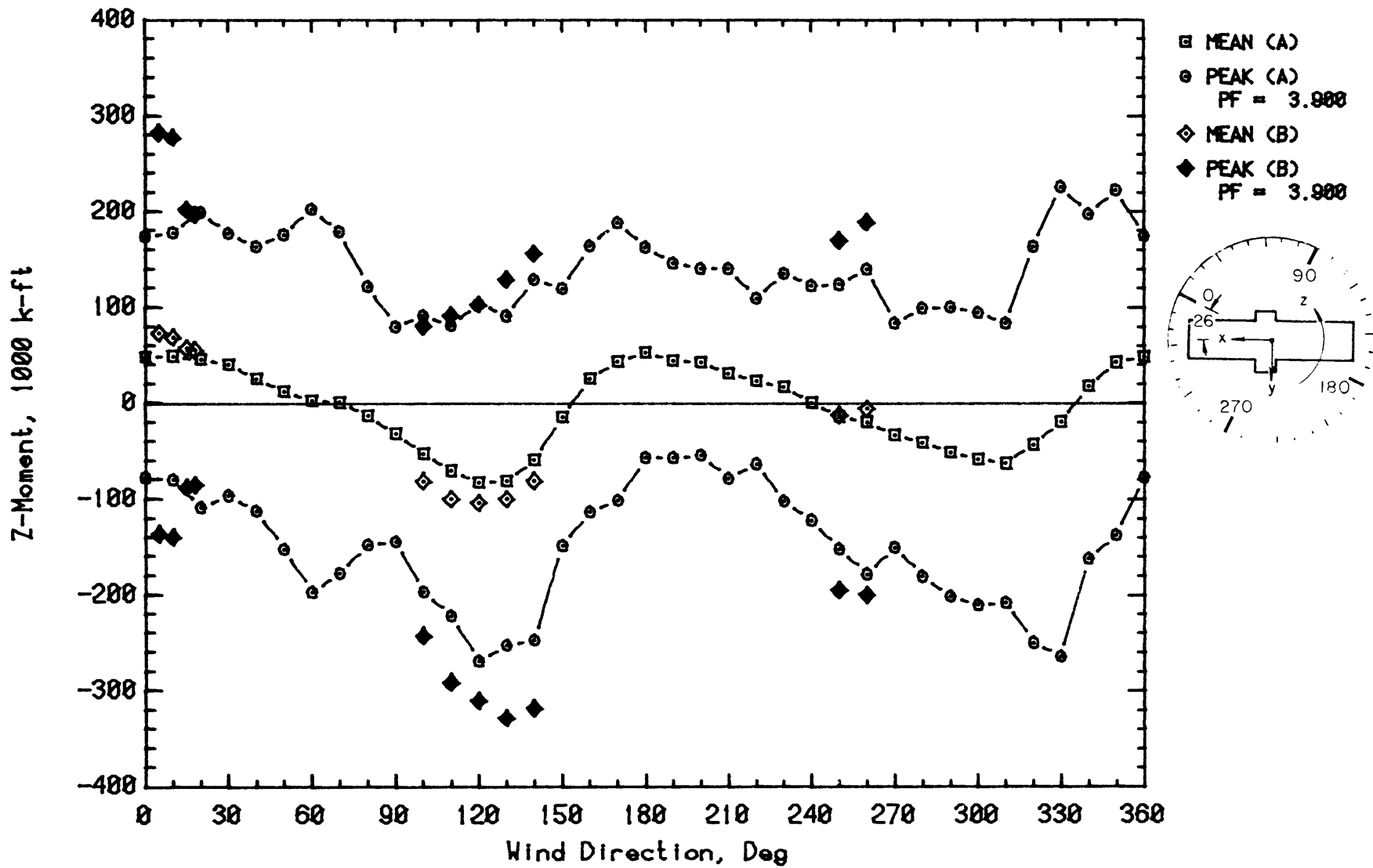
RESORTS HOTEL RESPONSE BASE MOMENTS FOR 100-YR WIND

Figure 15a. Base Moment versus Wind Direction for a 100-year Recurrence Wind



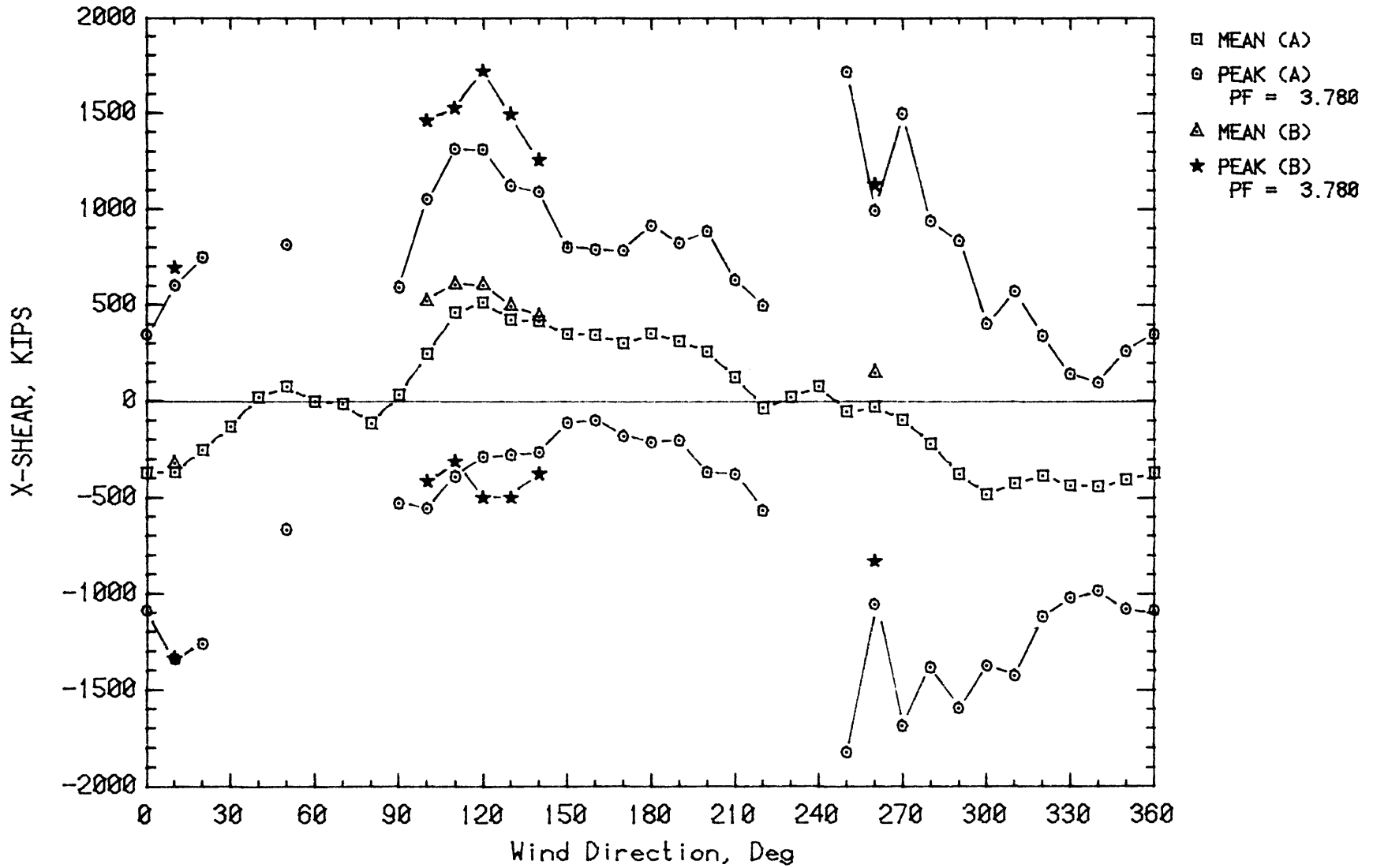
RESORTS HOTEL RESPONSE BASE MOMENTS FOR 100-YR WIND

Figure 15b. Base Moment versus Wind Direction for a 100-year Recurrence Wind



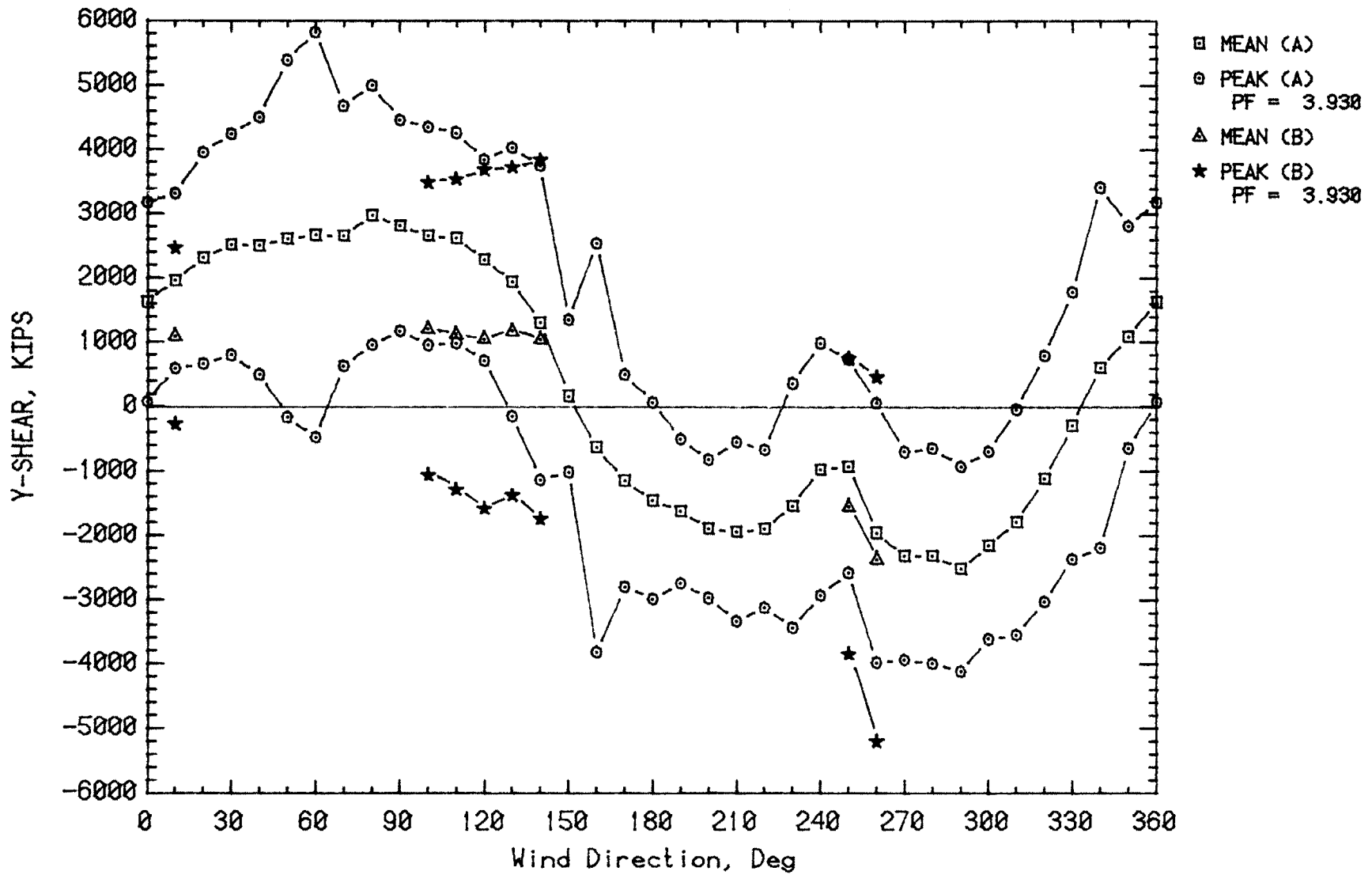
RESORTS HOTEL RESPONSE BASE MOMENTS FOR 100-YR WIND

Figure 15c. Base Moment versus Wind Direction for a 100-year Recurrence Wind



RESORTS HOTEL BASE SHEARS FOR 100-YR WIND

Figure 16a. Base Shear versus Wind Direction for a 100-year Recurrence Wind



RESORTS HOTEL BASE SHEARS FOR 100-YR WIND

Figure 16b. Base Shear versus Wind Direction for a 100-year Recurrence Wind

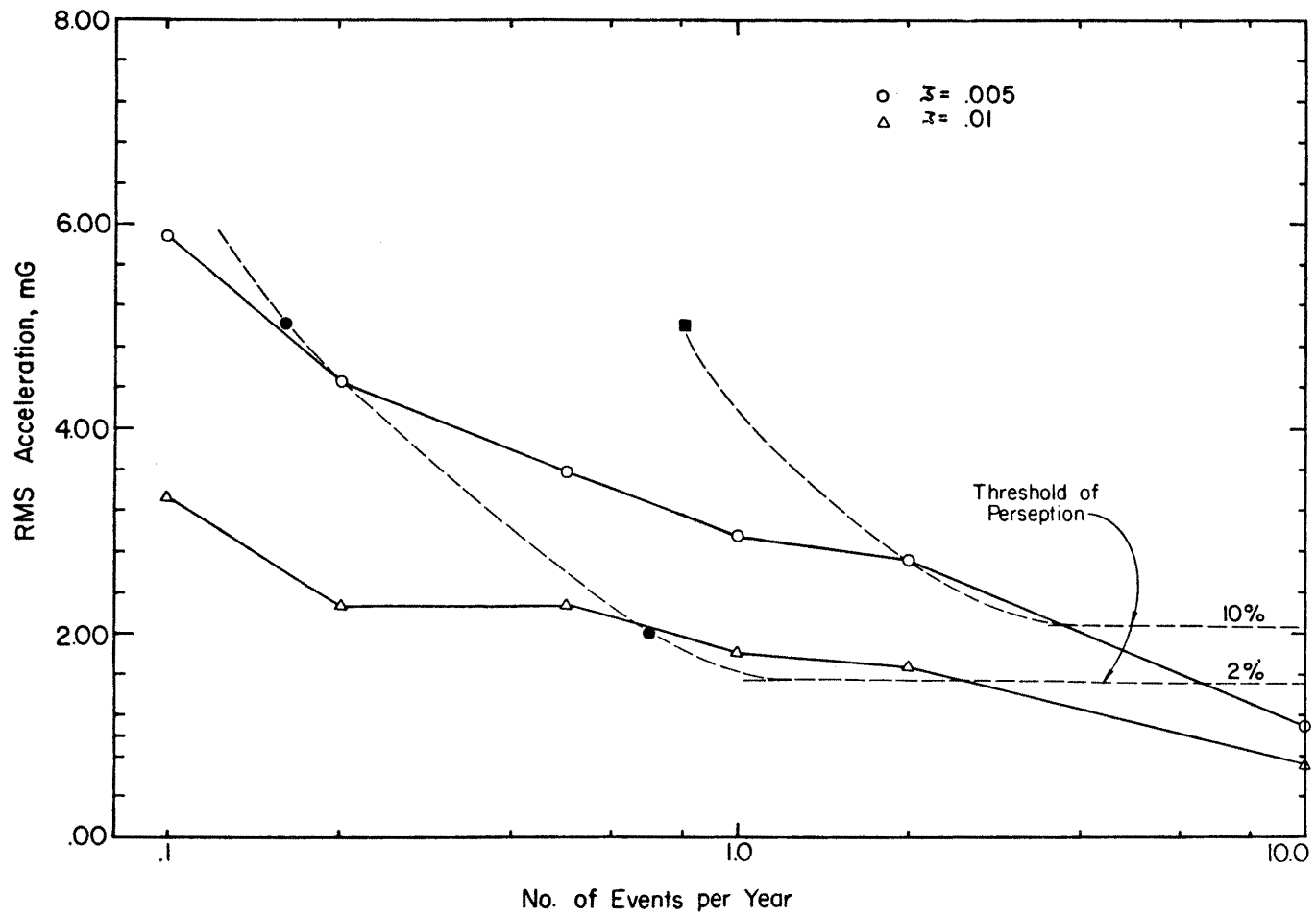


Figure 17. Top Floor Corner Acceleration versus Frequency of Occurrence

TABLES

TABLE 1
MOTION PICTURE SCENE GUIDE

1. Introduction
2. Purposes for model testing
3. Procedures for conducting tests
4. Specific flow visualization scenes for

RESORTS INTERNATIONAL HOTEL CASINO,
ATLANTIC CITY

HIGH PRESSURE AREAS

<u>Run No.</u>		<u>Tap No.</u>	<u>Wind Direction</u>
1	Configuration A	222	180°
2	" "	1925	60°
3	Configuration B	248	100°
4	" "	540, 124	270°

PEDESTRIAN AREA HIGH WIND VELOCITIES

<u>Run No.</u>		<u>Ped. Loc. No.</u>	<u>Wind Direction</u>
5	Configuration A	11	67.5°
6	" "	21	67.5°
7	" "	7	90°

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES
PROPOSED BUILDINGS OUT

LOCATION 1

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	35.6	12.1	71.9
22.50	52.4	10.0	62.3
45.00	48.1	10.1	78.3
67.50	40.2	9.6	69.1
90.00	36.4	9.9	66.3
112.50	32.1	9.9	61.9
135.00	25.8	9.9	52.6
157.50	26.3	9.9	52.7
180.00	11.5	8.9	32.6
202.50	26.0	8.9	32.4
225.00	47.9	11.2	81.4
247.50	45.9	12.1	82.3
270.00	53.2	17.4	105.5
292.50	26.2	15.9	73.8
315.00	26.8	10.4	58.1
337.50	26.4	9.9	56.1

LOCATION 2

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	68.8	11.2	102.2
22.50	81.1	11.6	115.9
45.00	82.7	9.5	111.2
67.50	65.7	17.1	117.1
90.00	66.1	16.8	116.4
112.50	49.3	16.2	97.9
135.00	35.2	14.2	77.9
157.50	70.6	14.6	114.4
180.00	79.2	13.3	119.2
202.50	80.8	16.1	128.9
225.00	65.7	33.5	166.1
247.50	34.2	24.9	108.9
270.00	18.1	9.1	45.3
292.50	17.9	8.7	44.1
315.00	13.7	7.7	36.8
337.50	44.9	10.5	76.4

LOCATION 3

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	13.9	7.2	35.4
22.50	20.8	11.1	54.0
45.00	21.0	11.4	53.3
67.50	26.3	12.3	63.2
90.00	24.1	11.2	57.7
112.50	12.6	7.7	35.8
135.00	11.0	6.3	29.8
157.50	28.6	11.1	62.6
180.00	25.8	12.9	64.7
202.50	20.2	10.0	50.1
225.00	20.9	10.1	51.2
247.50	12.3	6.9	33.0
270.00	13.4	8.1	37.6
292.50	11.3	6.9	31.9
315.00	8.8	4.1	21.1
337.50	8.7	3.8	20.3

LOCATION 4

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	20.9	8.8	47.4
22.50	20.3	10.0	50.4
45.00	22.9	10.9	55.6
67.50	33.9	12.4	71.1
90.00	48.8	10.4	80.0
112.50	55.9	14.6	99.8
135.00	55.0	15.5	101.6
157.50	46.3	16.6	96.1
180.00	24.4	13.1	63.7
202.50	30.9	14.9	75.6
225.00	18.1	8.6	43.9
247.50	12.9	6.7	32.8
270.00	11.6	6.1	30.0
292.50	40.4	15.6	87.2
315.00	38.4	17.4	90.5
337.50	35.9	12.3	72.8

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES
PROPOSED BUILDINGS OUT

LOCATION 5

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0 00	50.7	22.4	117.7
22 50	22.7	10.5	54.3
45 00	9.3	5.5	25.2
67 50	23.8	10.8	56.2
90 00	31.9	12.5	69.3
112 50	26.8	11.3	60.8
135 00	44.1	19.4	102.3
157 50	42.7	18.1	97.0
180 00	55.7	17.1	107.0
202 50	49.2	11.7	84.3
225 00	36.5	11.3	70.3
247 50	32.8	13.9	74.3
270 00	31.6	14.3	74.5
292 50	31.2	13.1	70.4
315 00	27.0	10.0	57.1
337 50	28.7	14.6	72.7

LOCATION 6

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0 00	38.3	17.8	91.8
22 50	19.8	9.7	48.9
45 00	15.8	9.2	43.4
67 50	17.8	8.5	43.4
90 00	19.1	9.8	48.4
112 50	27.7	15.7	74.8
135 00	92.2	20.9	154.9
157 50	56.3	13.7	97.3
180 00	42.3	10.9	75.1
202 50	28.5	12.4	65.8
225 00	27.2	13.0	66.1
247 50	30.9	11.9	66.4
270 00	41.6	12.2	78.2
292 50	46.9	12.2	83.4
315 00	45.1	12.4	82.4
337 50	42.0	13.1	81.3

LOCATION 7

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0 00	17.5	9.6	46.5
22 50	16.7	8.8	43.0
45 00	20.7	13.3	60.6
67 50	41.8	28.4	127.1
90 00	96.3	20.4	157.6
112 50	87.6	11.8	123.1
135 00	89.6	13.7	130.9
157 50	51.4	16.0	99.6
180 00	30.5	15.5	77.1
202 50	60.2	19.5	118.7
225 00	73.3	18.2	128.0
247 50	76.2	19.9	105.8
270 00	79.2	12.2	115.8
292 50	77.1	10.7	109.2
315 00	55.3	10.8	87.6
337 50	38.8	11.7	73.8

LOCATION 8

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0 00	20.0	7.2	41.8
22 50	19.0	7.2	40.6
45 00	31.5	11.3	65.4
67 50	27.9	13.3	67.8
90 00	16.3	8.0	40.4
112 50	31.0	9.8	60.4
135 00	13.9	5.2	29.3
157 50	10.4	4.2	23.1
180 00	19.1	8.8	45.5
202 50	25.0	11.5	59.4
225 00	23.8	11.5	58.3
247 50	19.7	8.4	44.8
270 00	16.2	7.8	39.7
292 50	13.6	7.2	35.2
315 00	12.9	6.0	30.8
337 50	9.6	4.2	22.3

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES
PROPOSED BUILDINGS OUT

LOCATION 9

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	13.9	4.8	28.3
22.50	16.7	5.0	31.8
45.00	21.6	5.4	37.9
67.50	32.2	6.3	51.2
90.00	18.8	5.0	33.6
112.50	22.5	5.1	38.1
135.00	1	2.9	22.2
157.50	5.5	2.3	13.0
180.00	9.9	4.4	23.0
202.50	23.3	9.6	55.7
225.00	27.8	9.9	56.6
247.50	13.7	6.1	31.9
270.00	15.3	6.3	34.3
292.50	10.2	3.9	21.9
315.00	6.8	3.5	17.2
337.50	6.8	3.1	15.8

LOCATION 10

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	26.1	13.6	66.9
22.50	24.0	11.9	59.7
45.00	18.2	11.0	51.2
67.50	37.9	15.1	83.3
90.00	35.2	16.8	83.3
112.50	42.0	20.2	102.6
135.00	25.3	12.5	62.8
157.50	17.1	8.2	41.7
180.00	39.4	15.1	84.6
202.50	49.2	20.1	109.6
225.00	56.6	20.0	116.7
247.50	47.9	17.8	101.3
270.00	59.4	18.5	114.9
292.50	45.7	18.4	100.8
315.00	26.1	13.5	66.6
337.50	24.9	11.8	60.4

LOCATION 11

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	26.7	14.5	70.2
22.50	36.4	13.6	77.1
45.00	64.4	27.7	147.4
67.50	95.5	20.7	157.7
90.00	86.5	17.0	137.9
112.50	66.0	12.1	102.4
135.00	39.2	13.6	80.4
157.50	29.4	14.6	73.2
180.00	21.6	10.0	58.2
202.50	21.3	10.2	51.2
225.00	29.1	12.2	65.7
247.50	19.4	10.6	51.3
270.00	49.8	21.2	113.4
292.50	32.4	15.0	77.3
315.00	27.7	11.6	62.3
337.50	27.6	12.8	65.8

LOCATION 12

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	17.1	8.9	43.7
22.50	40.6	16.3	89.5
45.00	60.1	22.1	126.5
67.50	28.4	15.1	73.6
90.00	27.7	13.8	69.1
112.50	37.3	14.1	79.7
135.00	37.6	11.7	72.6
157.50	23.7	9.8	53.1
180.00	30.8	12.5	68.3
202.50	28.3	13.2	67.8
225.00	39.3	16.6	89.1
247.50	17.2	9.0	44.3
270.00	20.5	11.4	54.6
292.50	17.5	10.4	48.6
315.00	14.6	7.3	36.6
337.50	14.3	7.3	36.2

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES
PROPOSED BUILDINGS OUT

LOCATION 13

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	33.5	12.7	71.5
22.50	44.1	14.5	87.6
45.00	36.6	20.4	97.8
67.50	30.8	14.4	74.0
90.00	70.0	20.2	130.5
112.50	47.4	13.0	86.4
135.00	44.7	13.9	88.3
157.50	27.5	11.0	60.5
180.00	36.6	12.3	73.9
202.50	44.1	13.6	83.0
225.00	20.9	11.4	53.3
247.50	20.3	10.3	51.2
270.00	20.7	11.0	53.1
292.50	34.3	12.7	72.5
315.00	27.1	9.8	56.4
337.50	30.6	9.9	60.6

LOCATION 14

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	25.5	11.3	59.3
22.50	25.7	13.7	66.8
45.00	29.8	13.6	70.6
67.50	54.3	21.7	119.3
90.00	31.9	16.2	80.3
112.50	41.8	15.3	87.8
135.00	49.6	16.3	99.1
157.50	27.2	11.8	62.5
180.00	37.7	16.3	87.1
202.50	29.9	14.4	73.2
225.00	18.3	10.3	49.2
247.50	17.3	9.7	46.4
270.00	19.0	9.5	47.4
292.50	29.9	8.8	56.4
315.00	23.8	8.5	49.5
337.50	24.0	9.4	52.5

LOCATION 15

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	9.1	3.9	20.8
22.50	14.1	8.3	39.0
45.00	19.3	10.7	51.4
67.50	29.9	12.3	66.9
90.00	28.0	11.4	62.1
112.50	21.3	10.1	51.7
135.00	15.4	8.0	39.3
157.50	12.6	6.8	32.2
180.00	15.6	7.0	33.0
202.50	19.1	6.8	33.9
225.00	15.4	7.6	33.3
247.50	28.7	12.6	66.3
270.00	12.5	7.7	33.6
292.50	15.3	7.5	32.0
315.00	9.2	5.5	20.2
337.50	7.5	5.4	17.6

LOCATION 16

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	13.4	6.6	33.3
22.50	12.2	7.3	34.0
45.00	11.1	6.1	29.4
67.50	16.3	8.1	40.7
90.00	16.6	8.1	40.8
112.50	20.8	9.3	48.8
135.00	23.5	9.8	52.8
157.50	13.6	6.3	32.6
180.00	13.0	5.5	29.4
202.50	8.8	4.6	22.7
225.00	13.5	6.1	31.8
247.50	11.9	6.6	31.6
270.00	17.5	9.3	45.3
292.50	18.0	9.1	45.2
315.00	15.8	7.5	38.3
337.50	11.5	5.4	27.8

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES
PROPOSED BUILDINGS OUT

LOCATION 17

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	20.4	9.6	49.3
22.50	9.5	5.6	26.2
45.00	12.0	6.6	31.8
67.50	10.6	6.7	30.8
90.00	12.2	6.1	30.4
112.50	21.2	10.3	52.0
135.00	18.7	9.5	47.1
157.50	10.8	5.9	28.5
180.00	7.9	3.5	19.7
202.50	7.3	3.2	16.9
225.00	5.3	1.9	11.1
247.50	10.9	5.1	26.2
270.00	8.5	4.1	20.7
292.50	12.6	4.1	25.0
315.00	10.8	3.8	22.3
337.50	7.6	2.9	16.3

LOCATION 18

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	11.3	4.2	23.7
22.50	18.0	7.9	41.7
45.00	23.0	7.0	43.9
67.50	36.9	7.5	59.5
90.00	40.7	8.5	66.1
112.50	40.1	8.5	65.7
135.00	34.8	9.2	62.2
157.50	14.2	8.4	39.3
180.00	21.0	9.0	48.1
202.50	22.9	9.4	51.2
225.00	30.3	10.9	63.1
247.50	15.9	6.6	35.7
270.00	13.0	4.7	27.2
292.50	13.6	5.0	28.7
315.00	9.4	2.5	16.9
337.50	9.8	3.4	20.1

LOCATION 19

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	10.1	4.3	22.9
22.50	18.4	8.9	45.2
45.00	30.9	10.4	62.1
67.50	47.2	10.6	78.9
90.00	55.2	10.9	88.0
112.50	47.1	10.8	79.5
135.00	35.9	9.1	63.0
157.50	11.0	4.8	25.3
180.00	29.5	11.5	63.9
202.50	44.2	10.7	76.5
225.00	50.8	11.0	83.8
247.50	42.1	10.4	75.5
270.00	13.9	6.5	32.1
292.50	10.5	5.3	26.3
315.00	6.0	2.2	12.6
337.50	8.1	3.6	18.9

LOCATION 20

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	39.8	2.1	46.0
22.50	39.6	2.3	46.4
45.00	43.5	2.7	51.7
67.50	39.2	2.4	46.3
90.00	40.8	2.0	46.8
112.50	33.7	1.8	39.1
135.00	28.5	2.3	35.4
157.50	21.8	2.5	29.2
180.00	14.3	3.1	29.6
202.50	24.8	3.5	35.4
225.00	32.0	1.9	37.6
247.50	35.3	2.3	42.1
270.00	37.9	1.9	43.5
292.50	39.3	1.8	44.8
315.00	38.9	1.9	44.5
337.50	38.6	1.7	43.8

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES
PROPOSED BUILDINGS OUT

LOCATION 21

WIND AZIMUTH	U _{MEAN} /U _{INF} (PERCENT)	U _{RMS} /U _{INF} (PERCENT)	U _{MEAN} +3*U _{RMS} /U _{INF} (PERCENT)
0.00	47.6	21.8	113.0
22.50	91.3	19.5	150.0
45.00	94.9	15.7	142.0
67.50	95.3	14.8	139.8
90.00	79.4	17.7	132.5
112.50	53.2	15.3	99.2
135.00	33.4	15.1	78.6
157.50	20.4	10.0	50.2
180.00	46.8	13.0	85.9
202.50	63.4	19.3	121.3
225.00	84.9	16.7	134.5
247.50	56.0	16.9	106.6
270.00	86.6	18.0	140.5
292.50	86.5	15.9	134.3
315.00	37.2	18.2	91.8
337.50	17.3	8.9	43.9

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES
PROPOSED BUILDINGS OUT

* * GREATEST VALUES * *

U _{MEAN} /U _{INF} (PERCENT)					U _{RMS} /U _{INF} (PERCENT)					U _{MEAN+3*RMS} /U _{INF} (PERCENT)				
LOC	AZ	MEAN	RMS	M+3RMS	LOC	AZ	MEAN	RMS	M+3RMS	LOC	AZ	MEAN	RMS	M+3RMS
7	90.0	96.3	20.4	157.6	2	225.0	65.7	33.5	166.1	2	225.0	65.7	33.5	166.1
11	67.5	95.5	20.7	157.7	7	67.5	41.8	28.4	127.1	11	67.5	95.5	20.7	157.7
21	67.5	95.3	14.8	139.8	11	45.0	64.4	27.7	147.4	7	90.0	96.3	20.4	157.6
21	45.0	94.9	15.7	142.0	2	247.5	34.2	24.9	108.9	6	135.0	92.2	20.9	154.9
6	135.0	92.2	20.9	154.9	5	0.0	50.7	22.4	117.7	21	22.5	91.3	19.5	150.0
21	22.5	91.3	19.5	150.0	12	45.0	60.1	22.1	126.5	11	45.0	64.4	27.7	147.4
7	135.0	89.6	13.7	130.9	21	0.0	47.6	21.8	113.0	21	45.0	94.9	15.7	142.0
7	112.5	87.6	11.8	123.1	14	67.5	54.3	21.7	119.3	21	270.0	86.6	18.0	140.5
21	270.0	86.6	18.0	140.5	11	270.0	49.8	21.2	113.4	21	67.5	95.3	14.8	139.8
21	292.5	86.5	15.9	134.3	6	135.0	92.2	20.9	154.9	11	90.0	86.5	17.0	137.5

TABLE 3

PERCENTAGE FREQUENCY OF WIND DIRECTION AND SPEED

ATLANTIC CITY, NEW JERSEY NAT. AV. FAC. EXP. CTR.

SEASON : ANNUAL NO. OF OBS. = 29216 HT. OF MEAS. = 984. FT.

VELOCITY LEVELS IN MPH

DIRECTION	0- 7	8-14	15-22	23-33	34-41	42-49	50-56	57 +	TOTAL
N	.30	2.40	3.30	1.50	.20	0.00	0.00	0.00	7.70
NNE	.20	1.00	1.10	.60	.10	0.00	0.00	0.00	2.90
NE	.10	1.00	1.10	.80	.20	0.00	0.00	0.00	3.30
ENE	.20	.90	1.20	1.30	.30	.10	0.00	0.00	4.00
E	.20	1.20	1.90	1.20	.20	.10	0.00	0.00	4.80
ESE	.20	.90	1.40	.70	.10	0.00	0.00	0.00	3.30
SE	.10	.80	1.20	.50	.10	0.00	0.00	0.00	2.80
SSE	.10	.80	1.40	.60	.10	0.00	0.00	0.00	3.10
S	.30	2.30	4.10	3.80	.60	.10	0.00	0.00	11.10
SSW	.20	1.60	2.70	1.90	.40	.10	0.00	0.00	6.90
SW	.20	1.70	2.30	1.30	.30	0.00	0.00	0.00	5.80
WSW	.20	2.20	3.00	1.60	.30	.10	0.00	0.00	7.40
W	.20	1.80	3.40	2.40	.80	.30	.10	0.00	9.00
WNW	.20	1.70	3.00	3.00	1.20	.40	.10	0.00	9.70
NW	.20	2.20	2.80	2.40	.90	.30	0.00	0.00	8.60
NNW	.20	1.50	1.80	1.40	.30	0.00	0.00	0.00	5.30
CALM	4.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	4.30
TOT	7.50	24.10	35.50	25.20	6.00	1.50	.30	0.00	100.00

TABLE 4
SUMMARY OF WIND EFFECTS ON PEOPLE

	<u>Beaufort number</u>	<u>Speed (mph)</u>	<u>Effects</u>
Calm, light air	0, 1	0- 3	Calm, no noticeable wind
Light breeze	2	4- 7	Wind felt on face
Gentle breeze	3	8-12	Wind extends light flag Hair is disturbed Clothing flaps
Moderate breeze	4	13-18	Raises dust, dry soil and loose paper Hair disarranged
Fresh breeze	5	19-24	Force of wind felt on body Drifting snow becomes airborne Limit of agreeable wind on land
Strong breeze	6	25-31	Umbrellas used with difficulty Hair blown straight Difficult to walk steadily Wind noise on ears unpleasant Windborne snow above head height (blizzard)
Near gale	7	32-38	Inconvenience felt when walking
Gale	8	39-46	Generally impedes progress Great difficulty with balance in gusts
Strong gale	9	47-54	People blown over by gusts

Note: Table from Reference 4, p. 40.

TABLE 5

SELECTION OF WIND SPEEDS AND REFERENCE DYNAMIC PRESSURE

1. Basic wind speeds from predictions of hurricane wind speeds* and ANSI A58.1, 1982.

Largest 100-year fastest mile at 33 ft = 89 mph for south winds.

Mean hourly wind speed at 33 ft = $\frac{89}{1.28} = 69.5$ mph.

Mean hourly gradient wind speed = $69.5 \left(\frac{717}{33} \right)^{.14} = 107$ mph.

Reference pressure at site of gradient height of 717 ft = $(0.00256) (107^2) = 29.3$ psf. Use 30 psf

2. Loads including directional effects for Atlantic City.*

Wind Direction	Mean Hourly Gradient Wind Speed (WS) mph	Load Ratio for Dynamic Pressure at Gradient $(WS/107)^2$
N 0°	100	0.87
NNE 22.5°	100	0.87
NE 45°	97	0.82
ENE 67.5°	95	0.79
E 90°	101	0.89
ESE 112.5°	106	0.98
SE 135°	104	0.94
SSE 157.5°	89	0.69
S 180°	86	0.65
SSW 202.5°	89	0.69
SW 225°	90	0.71
WSW 247.5°	95	0.79
W 270°	103	0.93
WNW 292.5°	107	1.00
NW 315°	106	0.98
NNW 337.5°	106	0.98

*Batts, M. E., M. R. Cordes, L. R. Russel, J. R. Shaver, E. Simiu, "Hurricane Wind Speeds in the United States," NBS Building Science Series 124, National Bureau of Standards, 1980.

TABLE 6A. PEAK LOADS FOR CONFIGURATION A : RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

TAP	RZI - MUTH	PRESS COEFF	NEGATIVE PEAK PSF	POSITIVE PEAK PSF	TAP	RZI - MUTH	PRESS COEFF	NEGATIVE PEAK PSF	POSITIVE PEAK PSF	TAP	RZI - MUTH	PRESS COEFF	NEGATIVE PEAK PSF	POSITIVE PEAK PSF
101	260	-1.42			114	310	-1.11			22	310	-1.11		
102	290	-1.56			115	320	-1.11			23	310	-1.11		
103	300	-1.29			116	330	-1.11			24	310	-1.11		
104	290	-1.21			117	340	-1.11			25	310	-1.11		
105	300	-1.49			118	350	-1.11			26	310	-1.11		
106	40	-1.51			119	360	-1.11			27	310	-1.11		
107	40	-1.47			120	370	-1.11			28	310	-1.11		
108	110	-1.92			121	380	-1.11			29	310	-1.11		
109	40	-1.82			122	390	-1.11			30	310	-1.11		
110	60	-1.99			123	400	-1.11			31	310	-1.11		
111	60	-1.60			124	410	-1.11			32	310	-1.11		
112	60	-1.60			125	420	-1.11			33	310	-1.11		
113	60	-1.60			126	430	-1.11			34	310	-1.11		
114	60	-1.60			127	440	-1.11			35	310	-1.11		
115	60	-1.60			128	450	-1.11			36	310	-1.11		
116	60	-1.60			129	460	-1.11			37	310	-1.11		
117	60	-1.60			130	470	-1.11			38	310	-1.11		
118	60	-1.60			131	480	-1.11			39	310	-1.11		
119	60	-1.60			132	490	-1.11			40	310	-1.11		
120	60	-1.60			133	500	-1.11			41	310	-1.11		
121	60	-1.60			134	510	-1.11			42	310	-1.11		
122	60	-1.60			135	520	-1.11			43	310	-1.11		
123	60	-1.60			136	530	-1.11			44	310	-1.11		
124	60	-1.60			137	540	-1.11			45	310	-1.11		
125	60	-1.60			138	550	-1.11			46	310	-1.11		
126	60	-1.60			139	560	-1.11			47	310	-1.11		
127	60	-1.60			140	570	-1.11			48	310	-1.11		
128	60	-1.60			141	580	-1.11			49	310	-1.11		
129	60	-1.60			142	590	-1.11			50	310	-1.11		
130	60	-1.60			143	600	-1.11			51	310	-1.11		
131	60	-1.60			144	610	-1.11			52	310	-1.11		
132	60	-1.60			145	620	-1.11			53	310	-1.11		
133	60	-1.60			146	630	-1.11			54	310	-1.11		
134	60	-1.60			147	640	-1.11			55	310	-1.11		
135	60	-1.60			148	650	-1.11			56	310	-1.11		
136	60	-1.60			149	660	-1.11			57	310	-1.11		
137	60	-1.60			150	670	-1.11			58	310	-1.11		
138	60	-1.60			151	680	-1.11			59	310	-1.11		
139	60	-1.60			152	690	-1.11			60	310	-1.11		
140	60	-1.60			153	700	-1.11			61	310	-1.11		
141	60	-1.60			154	710	-1.11			62	310	-1.11		
142	60	-1.60			155	720	-1.11			63	310	-1.11		
143	60	-1.60			156	730	-1.11			64	310	-1.11		
144	60	-1.60			157	740	-1.11			65	310	-1.11		
145	60	-1.60			158	750	-1.11			66	310	-1.11		
146	60	-1.60			159	760	-1.11			67	310	-1.11		
147	60	-1.60			160	770	-1.11			68	310	-1.11		
148	60	-1.60			161	780	-1.11			69	310	-1.11		
149	60	-1.60			162	790	-1.11			70	310	-1.11		
150	60	-1.60			163	800	-1.11			71	310	-1.11		
151	60	-1.60			164	810	-1.11			72	310	-1.11		
152	60	-1.60			165	820	-1.11			73	310	-1.11		
153	60	-1.60			166	830	-1.11			74	310	-1.11		
154	60	-1.60			167	840	-1.11			75	310	-1.11		
155	60	-1.60			168	850	-1.11			76	310	-1.11		
156	60	-1.60			169	860	-1.11			77	310	-1.11		
157	60	-1.60			170	870	-1.11			78	310	-1.11		
158	60	-1.60			171	880	-1.11			79	310	-1.11		
159	60	-1.60			172	890	-1.11			80	310	-1.11		
160	60	-1.60			173	900	-1.11			81	310	-1.11		
161	60	-1.60			174	910	-1.11			82	310	-1.11		
162	60	-1.60			175	920	-1.11			83	310	-1.11		
163	60	-1.60			176	930	-1.11			84	310	-1.11		
164	60	-1.60			177	940	-1.11			85	310	-1.11		
165	60	-1.60			178	950	-1.11			86	310	-1.11		
166	60	-1.60			179	960	-1.11			87	310	-1.11		
167	60	-1.60			180	970	-1.11			88	310	-1.11		
168	60	-1.60			181	980	-1.11			89	310	-1.11		
169	60	-1.60			182	990	-1.11			90	310	-1.11		
170	60	-1.60			183	1000	-1.11			91	310	-1.11		

TABLE 6A. PEAK LOADS FOR CONFIGURATION # 1: RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK PSF	POSITIVE PEAK PSF	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK PSF	POSITIVE PEAK PSF	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK PSF	POSITIVE PEAK PSF
222	110	-1.10	-1.60	3.74	322	310	-1.10	-1.30	3.10	444	110	-1.10	-1.77	3.77
222	110	-1.10	-1.43	3.50	322	310	-1.10	-1.10	3.10	444	110	-1.10	-1.88	3.88
222	110	-1.10	-1.27	3.33	322	310	-1.10	-1.10	3.10	444	110	-1.10	-1.99	3.99
222	110	-1.10	-1.11	3.17	322	310	-1.10	-1.10	3.10	444	110	-1.10	-2.10	4.10
222	110	-1.10	-0.94	3.00	322	310	-1.10	-1.10	3.10	444	110	-1.10	-2.21	4.21
222	110	-1.10	-0.78	2.83	322	310	-1.10	-1.10	3.10	444	110	-1.10	-2.32	4.32
222	110	-1.10	-0.62	2.67	322	310	-1.10	-1.10	3.10	444	110	-1.10	-2.43	4.43
222	110	-1.10	-0.46	2.50	322	310	-1.10	-1.10	3.10	444	110	-1.10	-2.54	4.54
222	110	-1.10	-0.30	2.33	322	310	-1.10	-1.10	3.10	444	110	-1.10	-2.65	4.65
222	110	-1.10	-0.14	2.17	322	310	-1.10	-1.10	3.10	444	110	-1.10	-2.76	4.76
222	110	-1.10	0.02	2.00	322	310	-1.10	-1.10	3.10	444	110	-1.10	-2.87	4.87
222	110	-1.10	0.18	1.83	322	310	-1.10	-1.10	3.10	444	110	-1.10	-2.98	4.98
222	110	-1.10	0.34	1.67	322	310	-1.10	-1.10	3.10	444	110	-1.10	-3.09	5.09
222	110	-1.10	0.50	1.50	322	310	-1.10	-1.10	3.10	444	110	-1.10	-3.20	5.20
222	110	-1.10	0.66	1.33	322	310	-1.10	-1.10	3.10	444	110	-1.10	-3.31	5.31
222	110	-1.10	0.82	1.17	322	310	-1.10	-1.10	3.10	444	110	-1.10	-3.42	5.42
222	110	-1.10	0.98	1.00	322	310	-1.10	-1.10	3.10	444	110	-1.10	-3.53	5.53
222	110	-1.10	1.14	0.83	322	310	-1.10	-1.10	3.10	444	110	-1.10	-3.64	5.64
222	110	-1.10	1.30	0.67	322	310	-1.10	-1.10	3.10	444	110	-1.10	-3.75	5.75
222	110	-1.10	1.46	0.50	322	310	-1.10	-1.10	3.10	444	110	-1.10	-3.86	5.86
222	110	-1.10	1.62	0.33	322	310	-1.10	-1.10	3.10	444	110	-1.10	-3.97	5.97
222	110	-1.10	1.78	0.17	322	310	-1.10	-1.10	3.10	444	110	-1.10	-4.08	6.08
222	110	-1.10	1.94	0.00	322	310	-1.10	-1.10	3.10	444	110	-1.10	-4.19	6.19
222	110	-1.10	2.10	-0.17	322	310	-1.10	-1.10	3.10	444	110	-1.10	-4.30	6.30
222	110	-1.10	2.26	-0.33	322	310	-1.10	-1.10	3.10	444	110	-1.10	-4.41	6.41
222	110	-1.10	2.42	-0.50	322	310	-1.10	-1.10	3.10	444	110	-1.10	-4.52	6.52
222	110	-1.10	2.58	-0.66	322	310	-1.10	-1.10	3.10	444	110	-1.10	-4.63	6.63
222	110	-1.10	2.74	-0.83	322	310	-1.10	-1.10	3.10	444	110	-1.10	-4.74	6.74
222	110	-1.10	2.90	-1.00	322	310	-1.10	-1.10	3.10	444	110	-1.10	-4.85	6.85
222	110	-1.10	3.06	-1.17	322	310	-1.10	-1.10	3.10	444	110	-1.10	-4.96	6.96
222	110	-1.10	3.22	-1.33	322	310	-1.10	-1.10	3.10	444	110	-1.10	-5.07	7.07
222	110	-1.10	3.38	-1.50	322	310	-1.10	-1.10	3.10	444	110	-1.10	-5.18	7.18
222	110	-1.10	3.54	-1.66	322	310	-1.10	-1.10	3.10	444	110	-1.10	-5.29	7.29
222	110	-1.10	3.70	-1.83	322	310	-1.10	-1.10	3.10	444	110	-1.10	-5.40	7.40
222	110	-1.10	3.86	-2.00	322	310	-1.10	-1.10	3.10	444	110	-1.10	-5.51	7.51
222	110	-1.10	4.02	-2.17	322	310	-1.10	-1.10	3.10	444	110	-1.10	-5.62	7.62
222	110	-1.10	4.18	-2.33	322	310	-1.10	-1.10	3.10	444	110	-1.10	-5.73	7.73
222	110	-1.10	4.34	-2.50	322	310	-1.10	-1.10	3.10	444	110	-1.10	-5.84	7.84
222	110	-1.10	4.50	-2.66	322	310	-1.10	-1.10	3.10	444	110	-1.10	-5.95	7.95
222	110	-1.10	4.66	-2.83	322	310	-1.10	-1.10	3.10	444	110	-1.10	-6.06	8.06
222	110	-1.10	4.82	-3.00	322	310	-1.10	-1.10	3.10	444	110	-1.10	-6.17	8.17
222	110	-1.10	4.98	-3.17	322	310	-1.10	-1.10	3.10	444	110	-1.10	-6.28	8.28
222	110	-1.10	5.14	-3.33	322	310	-1.10	-1.10	3.10	444	110	-1.10	-6.39	8.39
222	110	-1.10	5.30	-3.50	322	310	-1.10	-1.10	3.10	444	110	-1.10	-6.50	8.50
222	110	-1.10	5.46	-3.66	322	310	-1.10	-1.10	3.10	444	110	-1.10	-6.61	8.61
222	110	-1.10	5.62	-3.83	322	310	-1.10	-1.10	3.10	444	110	-1.10	-6.72	8.72
222	110	-1.10	5.78	-4.00	322	310	-1.10	-1.10	3.10	444	110	-1.10	-6.83	8.83
222	110	-1.10	5.94	-4.17	322	310	-1.10	-1.10	3.10	444	110	-1.10	-6.94	8.94
222	110	-1.10	6.10	-4.33	322	310	-1.10	-1.10	3.10	444	110	-1.10	-7.05	9.05
222	110	-1.10	6.26	-4.50	322	310	-1.10	-1.10	3.10	444	110	-1.10	-7.16	9.16
222	110	-1.10	6.42	-4.66	322	310	-1.10	-1.10	3.10	444	110	-1.10	-7.27	9.27
222	110	-1.10	6.58	-4.83	322	310	-1.10	-1.10	3.10	444	110	-1.10	-7.38	9.38
222	110	-1.10	6.74	-5.00	322	310	-1.10	-1.10	3.10	444	110	-1.10	-7.49	9.49
222	110	-1.10	6.90	-5.17	322	310	-1.10	-1.10	3.10	444	110	-1.10	-7.60	9.60
222	110	-1.10	7.06	-5.33	322	310	-1.10	-1.10	3.10	444	110	-1.10	-7.71	9.71
222	110	-1.10	7.22	-5.50	322	310	-1.10	-1.10	3.10	444	110	-1.10	-7.82	9.82
222	110	-1.10	7.38	-5.66	322	310	-1.10	-1.10	3.10	444	110	-1.10	-7.93	9.93
222	110	-1.10	7.54	-5.83	322	310	-1.10	-1.10	3.10	444	110	-1.10	-8.04	10.04
222	110	-1.10	7.70	-6.00	322	310	-1.10	-1.10	3.10	444	110	-1.10	-8.15	10.15
222	110	-1.10	7.86	-6.17	322	310	-1.10	-1.10	3.10	444	110	-1.10	-8.26	10.26
222	110	-1.10	8.02	-6.33	322	310	-1.10	-1.10	3.10	444	110	-1.10	-8.37	10.37
222	110	-1.10	8.18	-6.50	322	310	-1.10	-1.10	3.10	444	110	-1.10	-8.48	10.48
222	110	-1.10	8.34	-6.66	322	310	-1.10	-1.10	3.10	444	110	-1.10	-8.59	10.59
222	110	-1.10	8.50	-6.83	322	310	-1.10	-1.10	3.10	444	110	-1.10	-8.70	10.70
222	110	-1.10	8.66	-7.00	322	310	-1.10	-1.10	3.10	444	110	-1.10	-8.81	10.81
222	110	-1.10	8.82	-7.17	322	310	-1.10	-1.10	3.10	444	110	-1.10	-8.92	10.92
222	110	-1.10	8.98	-7.33	322	310	-1.10	-1.10	3.10	444	110	-1.10	-9.03	11.03
222	110	-1.10	9.14	-7.50	322	310	-1.10	-1.10	3.10	444	110	-1.10	-9.14	11.14
222	110	-1.10	9.30	-7.66	322	310	-1.10	-1.10	3.10	444	110	-1.10	-9.25	11.25
222	110	-1.10	9.46	-7.83	322	310	-1.10	-1.10	3.10	444	110	-1.10	-9.36	11.36
222	110	-1.10	9.62	-8.00	322	310	-1.10	-1.10	3.10	444	110	-1.10	-9.47	11.47
222	110	-1.10	9.78	-8.17	322	310	-1.10	-1.10	3.10	444	110	-1.10	-9.58	11.58
222	110	-1.10	9.94	-8.33	322	310	-1.10	-1.10	3.10	444	110	-1.10	-9.69	11.69
222	110	-1.10	10.10	-8.50	322	310	-1.10	-1.10	3.10	444	110	-1.10	-9.80	11.80
222	110	-1.10	10.26	-8.66	322	310	-1.10	-1.10	3.10	444	110	-1.10	-9.91	11.91
222	110	-1.10	10.42	-8.83	322	310	-1.10	-1.10	3.10	444	110	-1.10	-10.02	12.02
222	110	-1.10	10.58	-9.00	322	310	-1.10	-1.10	3.10	444	110	-1.10	-10.13	12.13
222	110	-1.10	10.74	-9.17	322	310	-1.10	-1.10	3.10	444	110	-1.10	-10.24	12.24
222	110	-1.10	10.90	-9.33	322	310	-1.10	-1.10	3.10	444	110	-1.10	-10.35	12.35
222	110	-1.10	11.06	-9.50	322	310	-1.10	-1.10	3.10	444	110	-1.10	-10.46	12.46
222	110	-1.10	11.22	-9.66	322	310	-1.10	-1.10	3.10	444	110	-1.10	-10.57	12.57
222	110	-1.10	11.38	-9.83	322	310	-1.10	-1.10	3.10	444	110	-1.10	-10.68	12.68
222	110	-1.10	11.54	-10.00	322	310	-1.10	-1.10	3.10	444	110	-1.10	-10.79	12.79
222	110	-1.10	11.70	-10.17	322	310	-1.10	-1.10	3.10	444	110	-1.10	-10.90	12.90
222	110	-1.10	11.86	-10.33	322	310	-1.10	-1.10	3.10	444	110	-1.10	-11.01	13.01
222	110	-1.10	12.02	-10.50	322	310	-1.10	-1.10	3.10	444	110	-1.10	-11.12	13.12
222	110	-1.10	12.18	-10.66	322	310	-1.10	-1.10	3.10	444	110	-1.10	-11.23	13.23
222	110	-1.10	12.34	-10.83	322	310	-1.10	-1.10	3.10	444	110	-1.10	-11.34	13.34
222	110	-1.10	12.50	-11.00	322	310	-1.10	-1.10	3.10	444	110	-1.10	-11.45	13.45
222	110	-1.10	12.66	-11.17	322	310	-1.10	-1.10	3.10	444				

TABLE 6A. PEAK LOADS FOR CONFIGURATION A : RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK
			PSF	PSF				PSF	PSF				PSF	PSF
9		-1	1.51	-4.0	1		-1	1.51	-4.0	133		4	-1	1.51
933		-1	1.70	-4.1	102		-1	1.70	-4.1	133		4	-1	1.70
9332		-1	1.26	-3.7	102		-1	1.26	-3.7	133		4	-1	1.26
1101		-1	1.21	-3.4	102		-1	1.21	-3.4	133		4	-1	1.21
11011		-1	1.04	-3.1	102		-1	1.04	-3.1	133		4	-1	1.04
110111		-1	1.12	-3.6	102		-1	1.12	-3.6	133		4	-1	1.12
11054		-1	1.05	-3.3	102		-1	1.05	-3.3	133		4	-1	1.05
110544		-1	1.13	-3.9	102		-1	1.13	-3.9	133		4	-1	1.13
1105444		-1	1.22	-4.6	102		-1	1.22	-4.6	133		4	-1	1.22
11054444		-1	1.33	-5.9	102		-1	1.33	-5.9	133		4	-1	1.33
110544444		-1	1.44	-7.3	102		-1	1.44	-7.3	133		4	-1	1.44
1105444444		-1	1.55	-8.8	102		-1	1.55	-8.8	133		4	-1	1.55
11054444444		-1	1.66	-10.4	102		-1	1.66	-10.4	133		4	-1	1.66
110544444444		-1	1.77	-12.1	102		-1	1.77	-12.1	133		4	-1	1.77
1105444444444		-1	1.88	-13.9	102		-1	1.88	-13.9	133		4	-1	1.88
11054444444444		-1	1.99	-15.8	102		-1	1.99	-15.8	133		4	-1	1.99
110544444444444		-1	2.10	-17.7	102		-1	2.10	-17.7	133		4	-1	2.10
1105444444444444		-1	2.21	-19.7	102		-1	2.21	-19.7	133		4	-1	2.21
11054444444444444		-1	2.32	-21.7	102		-1	2.32	-21.7	133		4	-1	2.32
110544444444444444		-1	2.43	-23.8	102		-1	2.43	-23.8	133		4	-1	2.43
1105444444444444444		-1	2.54	-25.9	102		-1	2.54	-25.9	133		4	-1	2.54
11054444444444444444		-1	2.65	-28.1	102		-1	2.65	-28.1	133		4	-1	2.65
110544444444444444444		-1	2.76	-30.3	102		-1	2.76	-30.3	133		4	-1	2.76
1105444444444444444444		-1	2.87	-32.6	102		-1	2.87	-32.6	133		4	-1	2.87
11054444444444444444444		-1	2.98	-34.9	102		-1	2.98	-34.9	133		4	-1	2.98
110544444444444444444444		-1	3.09	-37.3	102		-1	3.09	-37.3	133		4	-1	3.09
1105444444444444444444444		-1	3.20	-39.7	102		-1	3.20	-39.7	133		4	-1	3.20
11054444444444444444444444		-1	3.31	-42.1	102		-1	3.31	-42.1	133		4	-1	3.31
110544444444444444444444444		-1	3.42	-44.6	102		-1	3.42	-44.6	133		4	-1	3.42
1105444444444444444444444444		-1	3.53	-47.1	102		-1	3.53	-47.1	133		4	-1	3.53
11054444444444444444444444444		-1	3.64	-49.6	102		-1	3.64	-49.6	133		4	-1	3.64
110544444444444444444444444444		-1	3.75	-52.1	102		-1	3.75	-52.1	133		4	-1	3.75
1105444444444444444444444444444		-1	3.86	-54.6	102		-1	3.86	-54.6	133		4	-1	3.86
11054444444444444444444444444444		-1	3.97	-57.1	102		-1	3.97	-57.1	133		4	-1	3.97
110544444444444444444444444444444		-1	4.08	-59.6	102		-1	4.08	-59.6	133		4	-1	4.08
1105444444444444444444444444444444		-1	4.19	-62.1	102		-1	4.19	-62.1	133		4	-1	4.19
11054444444444444444444444444444444		-1	4.30	-64.6	102		-1	4.30	-64.6	133		4	-1	4.30
110544444444444444444444444444444444		-1	4.41	-67.1	102		-1	4.41	-67.1	133		4	-1	4.41
1105444444444444444444444444444444444		-1	4.52	-69.6	102		-1	4.52	-69.6	133		4	-1	4.52
11054444444444444444444444444444444444		-1	4.63	-72.1	102		-1	4.63	-72.1	133		4	-1	4.63
110544444444444444444444444444444444444		-1	4.74	-74.6	102		-1	4.74	-74.6	133		4	-1	4.74
1105444444444444444444444444444444444444		-1	4.85	-77.1	102		-1	4.85	-77.1	133		4	-1	4.85
11054444444444444444444444444444444444444		-1	4.96	-79.6	102		-1	4.96	-79.6	133		4	-1	4.96
110544444444444444444444444444444444444444		-1	5.07	-82.1	102		-1	5.07	-82.1	133		4	-1	5.07
1105444444444444444444444444444444444444444		-1	5.18	-84.6	102		-1	5.18	-84.6	133		4	-1	5.18
110544		-1	5.29	-87.1	102		-1	5.29	-87.1	133		4	-1	5.29
1105444		-1	5.40	-89.6	102		-1	5.40	-89.6	133		4	-1	5.40
110544		-1	5.51	-92.1	102		-1	5.51	-92.1	133		4	-1	5.51
1105444		-1	5.62	-94.6	102		-1	5.62	-94.6	133		4	-1	5.62
110544		-1	5.73	-97.1	102		-1	5.73	-97.1	133		4	-1	5.73
1105444		-1	5.84	-99.6	102		-1	5.84	-99.6	133		4	-1	5.84
110544		-1	5.95	-102.1	102		-1	5.95	-102.1	133		4	-1	5.95
1105444		-1	6.06	-104.6	102		-1	6.06	-104.6	133		4	-1	6.06
110544		-1	6.17	-107.1	102		-1	6.17	-107.1	133		4	-1	6.17
1105444		-1	6.28	-109.6	102		-1	6.28	-109.6	133		4	-1	6.28
110544		-1	6.39	-112.1	102		-1	6.39	-112.1	133		4	-1	6.39
1105444		-1	6.50	-114.6	102		-1	6.50	-114.6	133		4	-1	6.50
110544		-1	6.61	-117.1	102		-1	6.61	-117.1	133		4	-1	6.61
1105444		-1	6.72	-119.6	102		-1	6.72	-119.6	133		4	-1	6.72
110544		-1	6.83	-122.1	102		-1	6.83	-122.1	133		4	-1	6.83
1105444		-1	6.94	-124.6	102		-1	6.94	-124.6	133		4	-1	6.94
110544		-1	7.05	-127.1	102		-1	7.05	-127.1	133		4	-1	7.05
1105444		-1	7.16	-129.6	102		-1	7.16	-129.6	133		4	-1	7.16
110544		-1	7.27	-132.1	102		-1	7.27	-132.1	133		4	-1	7.27
1105444		-1	7.38	-134.6	102		-1	7.38	-134.6	133		4	-1	7.38
110544		-1	7.49	-137.1	102		-1	7.49	-137.1	133		4	-1	7.49
1105444		-1	7.60	-139.6	102		-1	7.60	-139.6	133		4	-1	7.60
110544		-1	7.71	-142.1	102		-1	7.71	-142.1	133		4	-1	7.71
1105444		-1	7.82	-144.6	102		-1	7.82	-144.6	133		4	-1	7.82
110544		-1	7.93	-147.1	102		-1	7.93	-147.1	133		4	-1	7.93
1105444		-1	8.04	-149.6	102		-1	8.04	-149.6	133		4	-1	8.04
110544		-1	8.15	-152.1	102		-1	8.15	-152.1	133		4	-1	8.15
110544		-1	8.26	-154.6	102		-1	8.26	-154.6	133		4	-1	8.26
1105444		-1	8.37	-157.1	102		-1	8.37	-157.1	133		4	-1	8.37
110544		-1	8.48	-159.6	102		-1	8.48	-159.6	133		4	-1	8.48
1105444		-1	8.59	-162.1	102		-1	8.59	-162.1	133		4	-1	8.59
110544		-1	8.70	-164.6	102		-1	8.70	-164.6	133		4	-1	8.70
1105444		-1	8.81	-167.1	102		-1	8.81	-167.1	133		4	-1	8.81
110544		-1	8.92	-169.6	102		-1	8.92	-169.6	133		4	-1	8.92
1105444		-1	9.03	-172.1	102		-1	9.03	-172.1	133		4	-1	9.03
110544		-1	9.14	-174.6	102		-1	9.14	-174.6	133		4	-1	9.14
1105444		-1	9.25	-177.1	102		-1	9.25	-					

TABLE 6A. PEAK LOADS FOR CONFIGURATION A : RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

TAP	AZI- MUTH	PRESS COEFF	NEGATIVE POSITIVE		TAP	AZI- MUTH	PRESS COEFF	NEGATIVE POSITIVE		TAP	AZI- MUTH	PRESS COEFF	NEGATIVE POSITIVE	
			PEAK PSF	PEAK PSF				PEAK PSF	PEAK PSF				PEAK PSF	PEAK PSF
19001	260	-1.80	-5.0	2.7	19001	60	-1.44	-3.4	1.6	19337	40	-1.56	-3.8	5.8
19002	290	-1.54	-4.6	2.7	19002	60	-1.44	-3.4	1.6	19338	60	-1.56	-3.8	28.4
19003	270	-1.79	-2.2	1.0	19003	200	-1.48	-3.4	1.6	19339	50	-1.72	-4.2	12.8
19004	330	-1.94	-2.4	2.9	19004	50	-1.69	-4.1	1.6	19440	290	-1.91	-2.7	11.1
19005	299	-1.00	-2.2	2.9	19005	80	-1.84	-4.9	11.0	19441	80	-1.07	-2.8	8.2
19006	50	-1.85	-4.2	1.8	19006	10	-1.86	-4.8	9.2	19442	50	-1.67	-4.1	14.2
19007	110	-1.36	-3.3	1.9	19007	10	-1.74	-4.8	9.2	19443	290	-1.10	-3.3	11.0
19008	290	-1.78	-3.3	1.9	19008	300	-1.88	-4.8	9.2	19444	30	-1.12	-3.3	6.5
19009	30	-2.56	-3.3	1.9	19009	200	-1.88	-4.8	9.2	19445	200	-1.10	-3.3	7.7
19010	30	-1.93	-3.3	1.9	19010	1	-1.88	-4.8	9.2	19446	200	-1.10	-3.3	6.9
19011	1	-1.20	-3.3	1.9	19011	1	-1.88	-4.8	9.2	19447	30	-1.11	-3.3	6.6
19012	240	-2.79	-4.7	2.2	19012	50	-2.66	-3.3	1.9	19448	60	-1.11	-2.6	4.8
19013	100	-1.72	-4.4	1.1	19013	50	-2.66	-3.3	1.9	19449	40	-1.11	-2.6	7.7
19014	200	-1.51	-4.4	1.1	19014	50	-2.66	-3.3	1.9	19550	50	-1.11	-2.6	5.9
19015	20	-1.80	-4.4	1.1	19015	50	-2.66	-3.3	1.9	19551	80	-1.11	-2.6	1
19016	30	-1.99	-4.4	1.1	19016	50	-2.66	-3.3	1.9	19552	60	-1.11	-2.6	5.0
19017	50	-1.19	-3.3	1.9	19017	50	-2.66	-3.3	1.9	19553	110	-1.11	-2.6	6.6
19118	50	-1.57	-3.3	1.9	19118	30	-2.66	-3.3	1.9	19554	50	-1.11	-2.6	8.3

TABLE 6A. PEAK LOADS FOR CONFIGURATION A : RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

* * 15 GREATEST PRESSURE MAGNITUDES * *

TAP	AZI- MUTH	PRESS COEFF	NEGATIVE PEAK ----- PSF	POSITIVE PEAK -----
1925	60	-3.58	-84.9	9.0
220	310	-2.74	-80.5	21.6
151	230	-3.36	-71.6	31.5
461	80	-2.66	-71.0	17.7
517	120	-2.36	-69.5	30.0
409	80	-2.55	-68.0	25.1
123	50	-2.75	-67.5	32.6
1931	60	-2.84	-67.3	16.5
446	130	-2.32	-65.6	23.6
521	130	-2.32	-65.5	31.2
135	260	-2.34	-65.4	37.3
140	60	-2.73	-64.6	38.2
596	320	-2.20	-64.5	20.5
281	140	-2.28	-64.2	28.7
257	50	-2.61	-64.2	33.2

TABLE 6A. PEAK LOADS FOR CONFIGURATION B : RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

TAP	AZI-NUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-NUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-NUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK
			PSF	PSF				PSF	PSF				PSF	PSF
101	260	-1.44	-40.1	29.2	149	300	-2.11	-60.9	21.6	225	300	-2.14	-44.4	22.5
102	260	-1.73	-48.4	35.9	150	150	-1.11	-30.0	15.0	226	80	-1.11	-33.3	15.5
103	240	-1.78	-43.3	29.4	151	260	-2.22	-60.0	26.0	227	260	-1.11	-33.3	26.0
104	260	-1.11	-33.3	26.0	152	260	-2.17	-55.0	21.7	228	90	-1.11	-33.3	22.8
105	300	-1.11	-33.3	30.0	153	270	-2.33	-63.0	27.0	229	140	-1.11	-33.3	22.9
106	300	-1.11	-33.3	30.0	153	260	-2.33	-63.0	26.0	230	80	-1.11	-33.3	23.0
107	340	-1.11	-33.3	34.0	153	120	-1.11	-33.3	12.0	231	130	-1.11	-33.3	13.0
108	300	-1.11	-33.3	30.0	153	310	-2.22	-55.5	31.0	232	120	-1.11	-33.3	12.0
109	300	-2.25	-67.5	25.3	157	270	-2.33	-63.0	27.0	233	300	-1.11	-33.3	30.0
110	80	-2.47	-65.8	30.0	158	340	-1.11	-33.3	34.0	234	80	-1.11	-33.3	8.0
111	260	-2.22	-55.5	32.2	159	120	-1.11	-33.3	12.0	235	80	-1.11	-33.3	8.0
112	260	-2.83	-78.9	32.2	160	100	-1.11	-33.3	10.0	236	80	-1.11	-33.3	8.0
113	260	-2.34	-67.7	33.7	161	350	-1.11	-35.5	35.0	237	120	-1.11	-33.3	12.0
114	260	-2.77	-75.9	35.4	162	130	-1.11	-33.3	13.0	238	320	-1.11	-33.3	32.0
115	260	-2.77	-75.9	35.4	163	130	-1.11	-33.3	13.0	239	90	-1.11	-33.3	9.0
116	260	-2.72	-75.6	35.4	164	90	-1.11	-33.3	9.0	240	60	-1.11	-33.3	6.0
117	260	-1.93	-52.2	37.3	165	110	-1.11	-33.3	11.0	241	140	-1.11	-33.3	14.0
118	260	-2.76	-75.6	35.4	166	110	-1.11	-33.3	11.0	242	80	-1.11	-33.3	8.0
119	270	-2.76	-75.6	35.4	167	120	-1.11	-33.3	12.0	243	80	-1.11	-33.3	8.0
120	260	-2.81	-78.3	38.5	168	80	-1.11	-33.3	8.0	244	90	-1.11	-33.3	9.0
121	270	-2.82	-78.2	38.5	169	260	-2.82	-78.2	26.0	245	80	-1.11	-33.3	8.0
122	270	-2.44	-66.4	32.7	171	350	-2.28	-55.5	35.0	246	40	-1.11	-33.3	4.0
123	270	-2.22	-55.5	32.2	172	260	-2.22	-55.5	26.0	247	80	-1.11	-33.3	8.0
124	270	-2.22	-55.5	32.2	173	260	-2.22	-55.5	26.0	248	110	-1.11	-33.3	11.0
125	270	-2.22	-55.5	32.2	201	260	-1.11	-33.3	26.0	250	80	-1.11	-33.3	8.0
126	80	-2.31	-66.9	33.3	202	140	-1.11	-33.3	14.0	251	110	-1.11	-33.3	11.0
127	120	-2.92	-81.6	33.3	203	260	-1.11	-33.3	26.0	252	120	-1.11	-33.3	12.0
128	270	-2.64	-79.2	34.5	204	260	-1.11	-33.3	26.0	253	50	-1.11	-33.3	5.0
129	270	-2.64	-79.2	34.5	205	320	-1.11	-33.3	32.0	254	300	-1.11	-33.3	30.0
130	270	-2.64	-79.2	34.5	206	300	-1.11	-33.3	30.0	255	340	-1.11	-33.3	34.0
131	270	-2.64	-79.2	34.5	207	330	-1.11	-33.3	33.0	256	340	-1.11	-33.3	34.0
132	270	-2.64	-79.2	34.5	208	330	-1.11	-33.3	33.0	257	90	-1.11	-33.3	9.0
133	270	-2.64	-79.2	34.5	209	330	-1.11	-33.3	33.0	258	50	-1.11	-33.3	5.0
134	270	-2.64	-79.2	34.5	210	330	-1.11	-33.3	33.0	259	60	-1.11	-33.3	6.0
135	270	-2.64	-79.2	34.5	211	120	-1.11	-33.3	12.0	260	110	-1.11	-33.3	11.0
136	270	-2.64	-79.2	34.5	212	20	-1.11	-33.3	2.0	261	90	-1.11	-33.3	9.0
137	270	-2.64	-79.2	34.5	213	30	-1.11	-33.3	3.0	262	90	-1.11	-33.3	9.0
138	270	-2.64	-79.2	34.5	214	30	-1.11	-33.3	3.0	263	90	-1.11	-33.3	9.0
139	270	-2.64	-79.2	34.5	215	30	-1.11	-33.3	3.0	264	110	-1.11	-33.3	11.0
140	270	-2.64	-79.2	34.5	216	30	-1.11	-33.3	3.0	265	140	-1.11	-33.3	14.0
141	270	-2.64	-79.2	34.5	217	30	-1.11	-33.3	3.0	266	120	-1.11	-33.3	12.0
142	270	-2.64	-79.2	34.5	218	140	-1.11	-33.3	14.0	267	340	-1.11	-33.3	34.0
143	270	-2.64	-79.2	34.5	219	140	-1.11	-33.3	14.0	268	120	-1.11	-33.3	12.0
144	270	-2.64	-79.2	34.5	220	310	-1.11	-33.3	31.0	269	120	-1.11	-33.3	12.0
145	270	-2.64	-79.2	34.5	221	140	-1.11	-33.3	14.0	270	320	-1.11	-33.3	32.0
146	270	-2.64	-79.2	34.5	222	280	-1.11	-33.3	28.0	271	280	-1.11	-33.3	28.0
147	270	-2.64	-79.2	34.5	223	300	-1.11	-33.3	30.0	272	90	-1.11	-33.3	9.0
148	270	-2.64	-79.2	34.5	224	300	-1.11	-33.3	30.0	273	80	-1.11	-33.3	8.0

TABLE 6A. PEAK LOADS FOR CONFIGURATION B : RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK		POSITIVE PEAK		TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK		POSITIVE PEAK		TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK		POSITIVE PEAK	
			PSF	PSF	PSF	PSF				PSF	PSF	PSF	PSF							
5524	3	-1.74	-45	24	57	22	57	-1.25	-1	120	1	1	6	120	-1	-1	-45	24	57	22
525	3	-1.64	-40	11	22	22	25	-1.25	-1	140	1	1	140	1	-1	-1	-40	11	22	22
525	2	-1.74	-48	44	44	44	10	-1.25	-1	140	1	1	140	1	-1	-1	-48	44	44	10
527	1300	-2.49	-70	33	33	33	10	-1.92	-1	150	1	1	150	1	-1	-1	-70	33	33	10
528	1300	-1.48	-41	44	44	44	10	-1.43	-1	140	1	1	140	1	-1	-1	-41	44	44	10
529	1300	-1.62	-45	66	66	66	10	-1.90	-1	140	1	1	140	1	-1	-1	-45	66	66	10
530	310	-1.35	-39	33	33	33	10	-1.31	-1	130	1	1	130	1	-1	-1	-39	33	33	10
531	1300	-1.75	-49	44	44	44	10	-1.12	-1	130	1	1	130	1	-1	-1	-49	44	44	10
532	330	-2.18	-64	22	22	22	10	-2.28	-1	90	1	1	90	1	-1	-1	-64	22	22	10
533	330	-1.54	-43	77	77	77	10	-1.63	-1	200	1	1	200	1	-1	-1	-43	77	77	10
534	1110	-2.01	-56	77	77	77	10	-1.37	-1	200	1	1	200	1	-1	-1	-56	77	77	10
535	1110	-1.91	-53	66	66	66	10	-1.41	-1	200	1	1	200	1	-1	-1	-53	66	66	10
536	2200	-2.83	-80	00	00	00	10	-1.29	-1	200	1	1	200	1	-1	-1	-80	00	00	10
537	2200	-2.32	-66	77	77	77	10	-1.19	-1	200	1	1	200	1	-1	-1	-66	77	77	10
538	3300	-1.34	-50	77	77	77	10	-1.20	-1	200	1	1	200	1	-1	-1	-50	77	77	10
539	3300	-1.53	-45	88	88	88	10	-1.12	-1	200	1	1	200	1	-1	-1	-45	88	88	10
540	3300	-2.43	-75	77	77	77	10	-2.07	-1	200	1	1	200	1	-1	-1	-75	77	77	10
541	3300	-1.98	-63	33	33	33	10	-1.78	-1	200	1	1	200	1	-1	-1	-63	33	33	10
542	3300	-2.38	-73	44	44	44	10	-1.17	-1	200	1	1	200	1	-1	-1	-73	44	44	10
543	3300	-1.98	-63	66	66	66	10	-1.16	-1	200	1	1	200	1	-1	-1	-63	66	66	10
544	3300	-1.36	-48	44	44	44	10	-1.63	-1	200	1	1	200	1	-1	-1	-48	44	44	10
545	3300	-1.46	-48	44	44	44	10	-1.63	-1	200	1	1	200	1	-1	-1	-46	44	44	10
546	3300	-1.40	-46	66	66	66	10	-1.48	-1	200	1	1	200	1	-1	-1	-40	66	66	10
547	3300	-1.51	-44	55	55	55	10	-1.48	-1	200	1	1	200	1	-1	-1	-44	55	55	10
548	3300	-1.77	-48	33	33	33	10	-1.39	-1	200	1	1	200	1	-1	-1	-48	33	33	10
549	3300	-1.60	-44	55	55	55	10	-1.42	-1	200	1	1	200	1	-1	-1	-40	55	55	10
550	3300	-1.42	-44	55	55	55	10	-1.39	-1	200	1	1	200	1	-1	-1	-42	55	55	10
551	3300	-1.41	-44	55	55	55	10	-1.42	-1	200	1	1	200	1	-1	-1	-41	55	55	10
552	3300	-1.27	-43	33	33	33	10	-1.49	-1	200	1	1	200	1	-1	-1	-27	33	33	10
553	3300	-1.26	-43	33	33	33	10	-1.49	-1	200	1	1	200	1	-1	-1	-26	33	33	10
554	3300	-1.35	-43	55	55	55	10	-1.37	-1	200	1	1	200	1	-1	-1	-35	55	55	10
555	3300	-1.89	-55	66	66	66	10	-1.95	-1	200	1	1	200	1	-1	-1	-89	66	66	10
556	3300	-1.15	-44	44	44	44	10	-1.85	-1	200	1	1	200	1	-1	-1	-15	44	44	10
557	3300	-2.11	-58	88	88	88	10	-1.87	-1	200	1	1	200	1	-1	-1	-11	88	88	10
558	3300	-1.28	-45	88	88	88	10	-1.99	-1	200	1	1	200	1	-1	-1	-28	88	88	10
559	3300	-1.43	-45	88	88	88	10	-1.99	-1	200	1	1	200	1	-1	-1	-43	88	88	10
560	3300	-1.73	-50	00	00	00	10	-1.88	-1	200	1	1	200	1	-1	-1	-73	00	00	10
561	3300	-1.38	-43	66	66	66	10	-1.88	-1	200	1	1	200	1	-1	-1	-38	66	66	10
562	3300	-2.52	-74	00	00	00	10	-1.34	-1	200	1	1	200	1	-1	-1	-52	00	00	10
563	3300	-1.79	-52	66	66	66	10	-1.77	-1	200	1	1	200	1	-1	-1	-79	66	66	10
564	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
565	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
566	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
567	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
568	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
569	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
570	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
571	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
572	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
573	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
574	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
575	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
576	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
577	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
578	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
579	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
580	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
581	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
582	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
583	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
584	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
585	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
586	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
587	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
588	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
589	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
590	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
591	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
592	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
593	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
594	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
595	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
596	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
597	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
598	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
599	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10
600	3300	-1.11	-45	66	66	66	10	-1.14	-1	200	1	1	200	1	-1	-1	-11	66	66	10

TABLE 6A. PEAK LOADS FOR CONFIGURATION B : RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK
			PSF	PSF				PSF	PSF				PSF	PSF
9331	90	-1.61	-43.1	11.6	1230	90	-.70	-17.7	18.7	1331	320	-.31	-9.1	6.1
9332	110	-1.57	-44.1	11.1	1231	90	-.70	-17.7	18.7	1332	300	-.42	-12.6	9.0
9333	225	-1.96	-46.4	11.9	1232	260	-.76	-19.2	11.7	1333	310	-.39	-11.2	10.9
1101	225	-1.44	-40.2	11.0	1233	120	-.85	-23.9	12.1	1334	300	-.42	-12.6	9.0
1102	225	-1.86	-42.4	11.7	1234	120	-.75	-20.0	14.1	1335	300	-.42	-12.6	9.0
1103	225	-1.05	-29.2	11.7	1235	226	-.84	-23.9	14.1	1336	200	-.83	-24.4	15.4
1104	225	-2.05	-48.5	12.1	1236	120	-.97	-27.8	14.1	1337	300	-.42	-12.6	9.0
1105	130	-1.66	-46.7	11.7	1237	120	-1.17	-33.5	19.3	1338	300	-.42	-12.6	9.0
1107	300	-.29	-8.0	6.0	1238	300	-1.21	-34.5	20.4	1339	260	-.56	-16.6	14.0
1108	300	-.26	-7.5	5.5	1239	235	-.90	-25.9	17.9	1401	200	-.63	-18.2	14.0
1109	300	-.95	-27.7	11.0	1240	130	-.93	-26.9	26.3	1402	110	-.64	-18.2	14.0
1110	440	-.88	-24.9	11.9	1241	260	-.75	-21.7	14.7	1403	350	-.16	-4.4	15.5
1111	220	-2.08	-49.4	13.3	1242	110	-.90	-25.9	14.7	1404	330	-.13	-3.9	15.5
1112	110	-1.06	-31.2	14.4	1243	300	-.89	-25.9	11.0	1405	100	-.49	-14.0	9.9
1113	110	-1.04	-30.4	14.1	1244	440	-.42	-11.1	6.6	1406	310	-.87	-24.4	15.4
1114	110	-.92	-26.9	11.1	1245	260	-.41	-11.1	6.6	1407	80	-.77	-22.0	11.1
1115	110	-.52	-15.2	11.0	1246	66	-.55	-15.5	9.5	1408	100	-.77	-22.0	11.1
1116	110	-.53	-15.5	11.0	1247	110	-.53	-15.5	11.0	1409	270	-.58	-16.6	11.1
1117	70	-.56	-16.5	11.1	1248	300	-.32	-9.1	15.2	1410	130	-.28	-7.7	11.1
1201	30	-1.12	-31.3	11.0	1249	880	-.18	-5.0	11.0	1411	330	-.74	-21.9	11.1
1202	30	-.99	-28.3	11.0	1250	880	-.18	-5.0	11.0	1412	40	-.03	-0.9	11.1
1203	40	-1.70	-47.1	16.4	1251	120	-.88	-24.4	17.1	1413	300	-.42	-12.6	9.0
1204	2	-1.32	-36.9	11.1	1252	90	-.93	-26.9	12.3	1414	140	-.75	-21.9	11.1
1205	300	-1.11	-32.0	11.7	1253	90	-1.14	-32.0	15.4	1415	140	-.87	-24.4	15.4
1206	250	-1.33	-37.4	13.3	1254	40	-1.01	-28.3	15.4	1416	140	-.70	-20.0	11.1
1207	100	-.83	-24.9	11.1	1255	60	-1.10	-30.4	15.4	1417	140	-.56	-16.6	11.1
1208	90	-.71	-19.9	11.0	1256	30	-1.08	-29.9	4.9	1418	80	-.65	-18.2	11.1
1209	200	-.70	-20.0	11.1	1257	30	-.95	-27.7	8.8	1419	140	-.67	-19.9	11.1
1210	225	-1.79	-49.5	13.3	1258	30	-.94	-27.7	8.8	1420	240	-.74	-21.9	11.1
1211	100	-1.01	-28.3	11.0	1259	30	-.74	-21.7	8.8	1421	110	-.81	-22.0	11.1
1212	120	-.76	-21.7	11.0	1260	30	-.86	-24.4	17.1	1422	100	-.71	-20.0	11.1
1213	110	-1.07	-30.4	13.3	1261	140	-.77	-22.0	6.6	1423	100	-.78	-22.0	11.1
1214	10	-1.23	-34.2	13.3	1262	90	-.59	-16.6	12.6	1424	130	-.56	-16.6	11.1
1215	2	-1.21	-33.6	13.3	1263	130	-.60	-17.7	12.6	1425	340	-.96	-27.7	15.4
1216	90	-1.01	-28.3	11.0	1264	290	-.42	-11.1	11.1	1426	100	-.69	-20.0	11.1
1217	90	-1.39	-37.7	13.3	1265	50	-.48	-13.3	14.1	1427	100	-.69	-20.0	11.1
1218	110	-1.07	-30.4	11.0	1266	260	-.56	-16.6	15.5	1428	110	-.53	-15.5	11.1
1219	200	-.89	-24.4	11.0	1267	90	-.55	-15.5	14.1	1429	90	-.47	-13.3	11.1
1220	110	-1.17	-33.4	14.4	1268	260	-.55	-15.5	15.5	1430	90	-.44	-13.3	11.1
1221	110	-1.27	-35.7	14.4	1269	130	-.69	-20.0	14.4	1431	140	-.81	-22.0	11.1
1222	130	-1.27	-35.7	14.4	1270	30	-.69	-20.0	11.0	1432	20	-.49	-13.3	11.1
1223	110	-.79	-21.9	11.0	1271	220	-.82	-23.9	14.4	1433	240	-.67	-19.9	11.1
1224	440	-.81	-23.9	11.0	1272	300	-.82	-23.9	11.0	1434	120	-.52	-15.5	11.1
1225	200	-.81	-23.9	11.0	1273	300	-.82	-23.9	11.0	1435	120	-.52	-15.5	11.1
1226	200	-.81	-23.9	11.0	1274	260	-.82	-23.9	11.0	1436	40	-.44	-13.3	11.1
1227	200	-.81	-23.9	11.0	1275	90	-.82	-23.9	11.0	1437	300	-.42	-12.6	9.0
1228	200	-.81	-23.9	11.0	1276	90	-.82	-23.9	11.0	1438	250	-.68	-20.0	11.1
1229	200	-.81	-23.9	11.0	1277	140	-.82	-23.9	11.0	1439	90	-.34	-9.9	11.1
1230	200	-.81	-23.9	11.0	1278	140	-.82	-23.9	11.0	1440	110	-.49	-13.3	11.1

TABLE 6A. PEAK LOADS FOR CONFIGURATION B : RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD
 REFERENCE PRESSURE = 30.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK
			----- PSF -----	----- PSF -----				----- PSF -----	----- PSF -----				----- PSF -----	----- PSF -----
1901	280	-2.05	-57.2	29.0	1919	100	-1.82	-48.6	13.9	1937	90	-1.20	-32.0	6.5
1902	280	-1.28	-35.8	7.8	1920	280	-2.16	-60.4	11.1	1938	120	1.11	30.8	22.2
1903	280	-1.73	-50.2	9.9	1921	110	-2.14	-62.8	25.5	1939	40	-1.03	-25.4	14.4
1904	280	-1.89	-53.3	10.9	1922	280	-2.19	-61.0	12.8	1940	310	-1.90	-56.4	11.6
1905	330	-1.98	-55.5	23.5	1923	90	-2.30	-61.4	10.5	1941	90	-1.86	-53.1	1.1
1906	280	-1.41	-41.9	20.0	1924	90	-1.43	-42.7	8.6	1942	110	-1.91	-55.7	1.1
1907	100	-1.67	-49.4	21.8	1925	90	-1.23	-37.1	10.5	1943	310	-1.21	-35.7	9.9
1908	110	-1.32	-38.8	12.3	1926	90	-1.48	-44.4	4.9	1944	280	-1.85	-53.8	6.6
1909	130	-1.88	-52.9	11.8	1927	1220	-1.65	-48.4	8.0	1945	280	-1.21	-33.8	6.6
1910	30	-1.79	-50.7	8.1	1928	90	-2.12	-56.7	8.0	1946	280	-1.19	-31.9	4.4
1911	30	-1.83	-51.5	9.6	1929	100	-1.53	-45.9	11.6	1947	100	-1.19	-31.9	4.4
1912	100	-1.46	-39.0	16.5	1930	70	-1.04	-24.7	5.4	1948	100	-1.63	-46.8	4.4
1913	100	-1.88	-50.1	16.1	1931	80	-1.55	-41.5	15.3	1949	100	-1.56	-44.9	8.6
1914	280	-1.28	-35.7	16.2	1932	80	-1.49	-39.8	10.0	1950	100	-1.51	-43.6	8.6
1915	100	-1.51	-40.4	14.4	1933	90	-1.19	-33.7	9.9	1951	320	-1.39	-40.9	1.1
1916	40	-1.34	-32.1	13.1	1934	90	-1.00	-30.6	11.1	1952	130	-1.76	-42.2	2.2
1917	110	-1.17	-34.3	13.3	1935	330	-1.81	-53.7	9.9	1953	120	-1.73	-41.1	1.1
1918	280	-1.72	-48.1	13.7	1936	80	-1.15	-33.8	9.6	1954	30	-1.11	-31.7	7.0

TABLE 6A. PEAK LOADS FOR CONFIGURATION B : RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

* * 15 GREATEST PRESSURE MAGNITUDES * *

TAP	AZI- MUTH	PRESS COEFF	NEGATIVE PEAK ----- PSF	POSITIVE PEAK -----
540	270	-3.43	-95.7	36.6
248	110	-3.24	-95.2	25.9
124	270	-3.22	-89.8	35.7
521	130	-3.07	-86.6	42.3
520	130	-3.04	-85.8	34.0
250	0	-3.18	-83.0	30.3
121	270	-2.94	-82.0	34.6
265	140	-2.89	-81.5	11.8
153	270	-2.83	-79.6	34.2
112	260	-2.83	-78.9	32.1
114	260	-2.83	-78.9	35.4
120	260	-2.81	-78.4	38.5
119	270	-2.75	-76.7	40.4
522	0	-2.93	-76.3	29.7
564	320	-2.52	-74.0	36.0

TABLE 6A. PEAK LOADS FOR CONFIGURATION C : RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

TAP	AZI- NUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI- NUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI- NUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK
			----- PSF	-----				----- PSF	-----				----- PSF	-----
123	54	-2.40	-59.0	11.1	222	182	-2.67	-52.0	26.4	1912	234	-2.32	-49.3	12.4
151	240	-2.75	-65.3	3.9	451	70	-2.38	-56.3	2.1	1925	60	-4.26	-100.9	9.7

TABLE 6A. PEAK LOADS FOR CONFIGURATION C : RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

* * 6 GREATEST PRESSURE MAGNITUDES * *

TAP	AZI- MUTH	PRESS COEFF	NEGATIVE PEAK ----- PSF -----	POSITIVE PEAK -----
1925	60	-4.26	-100.9	9.7
151	240	-2.75	-65.3	3.9
123	54	-2.40	-59.0	11.1
451	70	-2.38	-56.3	2.1
222	182	-2.67	-52.0	26.4
1912	234	-2.32	-49.3	12.4

TABLE 6A. PEAK LOADS FOR CONFIGURATION D : RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

TAP	AZI- MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI- MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI- MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK
			---- PSF ----	----				---- PSF ----	----				---- PSF ----	----
112	260	-2.58	-71.9	15.6	250	358	-2.64	-68.8	22.5	520	130	-2.96	-83.5	35.2
124	260	-3.47	-96.9	35.0	412	254	-3.13	-74.3	16.0	540	264	-3.31	-92.3	29.6
248	82	-4.18	-111.6	29.0										

TABLE 6A. PEAK LOADS FOR CONFIGURATION D : RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

* * 7 GREATEST PRESSURE MAGNITUDES * *

TAP	AZI- MUTH	PRESS COEFF	NEGATIVE PEAK ----- PSF -----	POSITIVE PEAK -----
248	82	-4.18	-111.6	29.0
124	260	-3.47	-96.9	35.0
540	264	-3.31	-92.3	29.6
520	130	-2.96	-83.5	35.2
412	254	-3.13	-74.3	16.0
112	260	-2.58	-71.9	15.6
250	358	-2.64	-68.8	22.5

TABLE 6A. PEAK LOADS FOR CONFIGURATION W : RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

TAP	AZI- RUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI- RUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI- RUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK
			PSF	PSF				PSF	PSF				PSF	PSF
101	260	-1.44	-4.1	36.2	149	310	-2.15	-63.3	28.4	225	300	-2.14	-64.1	26.3
102	260	-1.73	-4.8	28.6	150	260	-1.60	-46.1	31.6	226	310	-1.44	-42.3	26.6
103	40	-1.78	-4.3	32.5	151	230	-3.36	-71.6	31.5	227	310	-1.60	-47.1	22.9
104	260	-1.84	-4.4	34.6	152	260	-2.17	-60.6	33.6	228	260	-1.27	-35.5	34.4
105	260	-1.85	-4.5	29.4	153	270	-2.83	-79.0	34.2	229	140	-1.76	-49.7	36.9
106	300	-1.81	-4.5	33.4	154	260	-1.95	-54.3	30.0	230	80	-1.85	-49.5	31.6
107	340	-1.83	-4.9	33.4	155	310	-1.44	-42.3	32.0	231	290	-1.38	-41.3	33.8
108	20	-1.25	-3.3	25.9	156	310	-2.22	-60.4	35.5	232	120	-2.09	-61.5	33.8
109	300	-2.25	-4.3	30.0	157	270	-1.31	-39.5	31.3	233	0	-2.43	-63.3	33.7
110	80	-2.47	-4.8	30.8	158	340	-1.28	-37.6	33.4	234	0	-2.20	-57.3	33.7
111	260	-2.00	-4.5	32.1	159	120	-1.63	-48.8	28.8	235	80	-1.90	-50.8	33.6
112	260	-2.83	-4.7	32.2	160	100	-1.46	-38.8	18.0	236	310	-1.48	-43.4	33.5
113	50	-2.60	-4.9	33.7	161	280	-1.98	-52.4	27.4	237	310	-1.36	-39.9	33.5
114	260	-2.83	-4.9	35.4	162	130	-1.18	-33.3	29.8	238	320	-1.49	-43.3	33.5
115	50	-2.37	-4.4	32.8	163	130	-1.43	-40.3	36.9	239	90	-1.57	-41.8	33.5
116	80	-2.72	-4.6	40.9	164	30	-1.16	-24.4	30.2	240	60	-2.09	-49.6	32.2
117	80	-2.96	-4.4	33.3	165	110	-1.32	-38.9	17.4	241	310	-1.37	-40.3	32.2
118	260	-2.77	-4.9	36.4	166	110	-1.43	-41.7	17.4	242	310	-1.41	-41.4	34.5
119	270	-2.73	-4.4	33.3	167	120	-1.17	-34.4	24.5	243	80	-1.29	-31.6	34.5
120	260	-2.81	-4.4	33.5	168	30	-2.20	-54.3	31.9	244	110	-1.26	-32.5	34.4
121	270	-2.82	-4.8	33.7	169	340	-1.05	-22.9	30.8	245	80	-1.28	-27.7	34.4
122	110	-2.30	-4.4	32.2	171	270	-1.26	-28.6	33.3	246	90	-1.27	-28.2	33.3
123	50	-2.75	-4.7	32.6	172	270	-1.21	-22.2	33.6	247	80	-1.29	-30.9	33.3
124	270	-2.22	-4.8	37.6	173	260	-1.67	-32.5	46.7	248	110	-1.33	-35.2	33.3
125	260	-2.46	-4.6	33.2	201	260	-1.66	-47.2	20.3	250	0	-3.18	-83.0	33.3
126	80	-2.31	-4.8	34.2	202	140	-1.69	-47.6	23.8	251	310	-1.52	-44.7	33.2
127	120	-2.92	-4.9	33.5	203	300	-1.47	-44.1	25.7	252	310	-1.25	-36.8	34.4
128	270	-2.64	-4.8	33.5	204	300	-2.03	-61.0	23.7	253	50	-1.40	-33.1	34.6
129	270	-2.09	-4.5	33.9	205	300	-1.79	-52.7	22.2	254	300	-1.49	-44.6	33.3
130	270	-2.09	-4.5	33.9	206	310	-1.30	-38.8	25.5	255	340	-1.50	-44.0	33.3
131	270	-2.08	-4.5	33.5	207	290	-1.53	-46.5	24.0	256	340	-2.42	-71.1	33.3
132	270	-2.33	-4.6	33.6	208	310	-1.80	-53.3	23.8	257	90	-2.49	-66.4	33.3
133	520	-2.33	-4.6	30.7	209	300	-1.46	-43.3	31.6	258	80	-2.31	-61.7	33.3
134	50	-2.33	-4.5	33.1	210	300	-1.46	-43.3	25.1	259	70	-2.18	-51.6	34.4
135	60	-2.33	-4.4	33.7	211	120	-1.34	-39.8	24.3	260	110	-1.17	-29.9	34.4
136	20	-2.22	-4.4	33.4	212	310	-1.47	-43.3	31.2	261	90	-1.20	-28.7	34.4
137	40	-2.33	-4.4	33.0	213	300	-1.93	-57.9	25.8	262	80	-1.16	-22.6	34.4
138	90	-2.33	-4.6	33.5	214	300	-1.69	-48.1	35.0	263	80	-1.07	-19.5	34.4
139	80	-2.09	-4.0	40.1	215	180	-2.71	-52.2	36.3	264	80	-1.22	-25.5	34.4
140	60	-2.33	-4.4	33.8	216	310	-1.41	-41.1	22.2	265	140	-1.89	-61.5	34.4
141	270	-2.85	-4.6	33.6	217	80	-1.63	-43.3	27.7	266	120	-1.77	-52.2	34.4
142	260	-2.00	-4.7	33.8	218	70	-1.57	-37.2	25.6	267	340	-2.25	-66.3	34.4
143	260	-2.00	-4.8	34.7	219	310	-1.65	-48.5	24.7	268	310	-1.29	-38.1	34.4
144	310	-2.71	-4.7	34.7	220	110	-2.74	-80.6	26.0	269	120	-1.38	-40.6	34.4
145	310	-2.11	-4.0	32.8	221	0	-1.99	-57.5	27.4	270	320	-1.40	-41.3	34.4
146	270	-2.27	-4.3	33.7	222	160	-3.30	-63.3	28.1	271	280	-1.56	-43.5	33.3
147	330	-2.15	-4.3	32.3	223	300	-1.44	-43.3	28.8	272	90	-1.77	-47.2	33.3
148	60	-2.70	-4.9	25.4	224	340	-1.66	-48.8	23.4	273	80	-2.05	-54.7	33.3

TABLE 6A. PEAK LOADS FOR CONFIGURATION W : RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK
			PSF	PSF				PSF	PSF				PSF	PSF
274	80	-2.26	-60.4	38.4	322	310	-1.30	-38.2	29.9	444	160	-1.77	-36.7	34.1
275	80	-1.63	-43.5	35.9	323	330	-1.10	-25.0	28.8	445	140	-2.04	-57.4	30.0
276	80	-1.28	-31.2	34.2	324	320	-1.65	-48.4	27.5	446	130	-2.32	-65.6	27.0
277	140	-1.51	-42.6	32.8	325	320	-1.79	-52.5	18.8	447	80	-2.10	-59.9	23.0
278	80	1.33	-26.3	35.4	326	110	-1.17	-34.4	17.6	448	250	-2.18	-53.7	21.5
279	70	1.31	-28.7	31.0	401	80	-1.44	-38.4	25.7	449	250	-2.11	-49.9	22.4
280	100	1.24	-29.1	33.1	402	260	-1.49	-41.5	30.4	450	260	-2.03	-56.8	22.4
281	140	-1.57	-72.4	28.7	403	300	-1.20	-36.1	31.3	451	60	-2.64	-62.5	19.9
282	120	-2.12	-62.2	29.2	404	110	-1.32	-38.9	15.5	452	140	-1.93	-54.4	22.9
283	20	-2.51	-65.5	29.2	405	140	-1.45	-40.9	11.8	453	260	-2.04	-56.9	22.6
284	310	-1.29	-37.7	35.5	406	140	-1.65	-46.5	23.4	454	80	-1.70	-51.1	23.0
285	310	-1.52	-44.8	30.0	407	250	-2.72	-64.4	16.6	455	180	-1.62	-50.6	22.0
286	320	-1.80	-53.0	31.0	408	250	-2.61	-61.9	21.5	456	130	-1.83	-52.2	20.4
287	280	-1.59	-44.3	33.1	409	80	-2.55	-68.0	25.5	457	80	-1.83	-52.2	20.4
288	280	-2.94	-54.1	29.2	410	240	-2.59	-61.4	33.3	458	130	-1.55	-47.7	24.1
289	50	-2.30	-56.6	33.3	411	80	-2.02	-54.0	33.3	459	140	-1.63	-53.3	24.1
290	80	-2.33	-63.5	32.3	412	220	-2.06	-72.2	25.0	460	140	-1.85	-52.2	21.1
291	80	-1.82	-48.6	32.3	413	250	-2.65	-62.2	25.5	461	80	-2.66	-62.2	21.1
292	140	-1.40	-39.9	35.9	414	250	-2.39	-54.2	27.7	462	260	-1.82	-57.3	25.8
293	150	-1.67	-34.4	32.2	415	80	-1.93	-55.5	11.1	463	260	-2.05	-57.7	25.8
294	160	-1.48	-30.7	32.2	416	80	-1.67	-44.4	34.4	464	260	-2.03	-56.6	25.8
295	180	-1.90	-37.0	27.7	417	250	-2.47	-58.6	32.2	465	260	-1.78	-54.4	25.8
296	80	1.10	-29.2	31.3	418	50	-2.16	-53.3	33.3	466	80	-2.13	-59.9	25.8
297	130	-2.49	-70.3	27.2	419	140	-2.01	-56.6	31.1	467	170	-1.63	-47.7	25.8
298	110	-2.10	-61.8	27.2	420	240	-2.39	-56.6	35.5	468	80	1.47	-11.1	25.8
299	330	-1.96	-57.7	24.2	421	80	-2.13	-57.9	38.0	501	0	-1.62	-42.2	22.1
300	120	-1.21	-35.7	28.7	422	100	-1.46	-34.9	39.0	502	330	-1.67	-49.7	22.1
301	310	-1.85	-54.3	24.8	423	140	-2.09	-59.0	29.9	503	110	-1.96	-55.5	23.3
302	310	-2.00	-58.8	27.4	424	220	-2.40	-56.6	25.5	504	120	-2.26	-66.4	23.3
303	320	-1.89	-53.5	35.5	425	250	-2.46	-51.1	25.5	505	130	-1.87	-52.2	23.3
304	320	-2.07	-69.1	25.9	426	220	-2.59	-64.4	34.4	506	130	-1.88	-52.2	23.3
305	310	-2.37	-60.9	25.7	427	220	-2.70	-66.6	36.6	507	130	-2.19	-60.4	23.3
306	80	-2.05	-54.7	24.2	428	250	-2.32	-54.4	44.4	508	120	-1.45	-42.2	24.4
307	140	-1.69	-47.7	29.1	429	80	-2.27	-60.9	31.1	509	120	-1.69	-47.7	25.8
308	140	-1.64	-46.1	28.5	430	130	-2.17	-61.1	21.0	510	120	-1.75	-47.7	25.8
309	160	-1.62	-46.6	28.5	431	250	-2.50	-59.2	44.4	511	120	-1.88	-51.1	25.8
310	280	-1.19	-33.3	31.1	432	80	-2.17	-57.9	33.3	512	130	-1.82	-51.1	25.8
311	80	1.26	-28.0	33.5	433	170	-1.67	-44.4	37.7	513	80	-2.15	-56.0	25.8
312	80	1.24	-32.3	33.3	434	140	-2.02	-62.2	22.2	514	130	-1.40	-42.2	25.8
313	180	-1.67	-32.6	33.3	435	140	-2.23	-62.2	33.3	515	130	-2.31	-66.4	25.8
314	170	-2.12	-41.4	33.3	436	60	-1.99	-54.4	28.2	516	130	-2.16	-51.1	25.8
315	80	-1.49	-31.4	39.7	437	250	-2.25	-62.2	34.4	517	120	-2.36	-66.4	25.8
316	120	-1.02	-27.0	33.0	438	260	-2.81	-50.5	66.6	518	260	-1.80	-47.7	25.8
317	120	-1.88	-53.8	32.4	439	260	-2.18	-60.0	7.7	519	130	-2.21	-62.2	25.8
318	310	-1.59	-46.6	30.0	440	80	-2.21	-59.9	9.9	520	130	-3.04	-83.3	25.8
319	120	-1.62	-47.6	31.9	441	1	-1.99	-56.6	11.1	521	130	-3.07	-86.6	25.8
320	120	-1.40	-41.2	35.5	442	80	-2.33	-55.5	22.2	522	0	-2.93	-76.6	25.8
321	120	-1.14	-33.5	30.6	443	80	-2.39	-55.5	22.2	523	0	-2.77	-72.2	25.8

TABLE 6A. PEAK LOADS FOR CONFIGURATION W : RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK	POSITIVE PEAK
			PSF	PSF				PSF	PSF				PSF	PSF
524	350	-1.74	-45.3	26.1	572	250	-2.25	-53.3	25.4	621	120	-1.88	-57.3	22.9
525	50	-1.64	-40.3	18.9	573	240	-2.38	-56.5	25.5	622	140	-1.55	-42.5	22.4
526	260	-1.74	-48.7	37.0	574	250	-2.10	-49.7	24.4	623	140	-1.51	-42.6	22.6
527	130	-2.49	-70.3	37.8	575	280	-1.92	-53.5	33.1	624	150	-2.20	-45.5	22.9
528	130	-1.48	-41.7	44.4	576	330	-1.43	-42.7	33.3	625	140	-1.74	-49.0	24.4
529	130	-1.68	-45.6	26.6	577	330	-1.98	-52.0	33.3	626	140	-1.82	-51.3	24.4
530	310	-1.35	-39.6	35.5	578	300	-1.31	-38.8	33.3	627	130	-1.51	-44.9	24.4
531	120	-2.00	-58.3	33.3	579	290	-1.24	-42.8	22.2	628	130	-1.53	-45.3	24.9
532	310	-2.18	-64.2	11.1	580	310	-2.28	-67.5	11.1	629	90	-2.03	-54.4	24.9
533	130	-1.54	-43.4	36.7	581	140	-1.63	-45.9	36.6	630	170	-2.19	-51.1	24.9
534	130	-2.01	-56.7	34.3	582	160	-2.18	-45.5	33.3	631	180	-2.16	-51.1	24.9
535	130	-2.09	-58.8	30.9	583	130	-1.44	-40.7	33.3	632	110	-1.21	-33.3	27.7
536	290	-1.83	-54.8	27.2	584	140	-1.29	-36.6	33.3	633	310	-1.55	-47.7	24.9
537	250	-2.32	-54.9	22.2	585	130	-1.35	-36.6	33.3	634	320	-1.34	-49.9	22.2
538	300	-1.94	-50.7	22.2	586	140	-1.20	-33.3	33.3	635	350	-1.64	-53.3	22.2
539	300	-1.53	-43.8	22.2	587	140	-1.12	-33.3	33.3	636	140	-2.22	-53.3	22.2
540	270	-3.43	-69.7	8.8	588	440	-1.89	-51.0	44.4	637	130	-1.28	-49.9	22.2
541	260	-2.48	-69.3	4.4	589	130	-1.84	-51.1	44.4	638	130	-1.58	-53.3	22.2
542	310	-1.98	-58.2	4.4	590	270	-2.17	-60.6	0.0	639	300	-1.58	-53.3	22.2
543	130	-1.36	-38.5	34.4	591	270	-2.16	-60.0	0.0	640	340	-1.89	-55.5	22.2
544	320	-1.46	-43.0	6.8	592	340	-1.81	-53.3	22.2	641	260	-1.65	-49.9	22.2
545	220	1.40	28.3	0.0	593	130	-1.31	-37.7	33.3	642	260	-1.56	-47.7	22.2
546	290	1.20	26.8	0.0	594	330	-1.34	-37.3	33.3	643	110	-1.22	-33.3	24.4
547	320	-1.64	-48.3	9.9	595	320	-2.48	-73.3	0.0	644	80	-2.01	-53.3	24.4
548	130	-1.52	-42.1	4.4	596	130	-1.66	-46.6	2.2	645	260	-1.48	-41.1	24.4
549	120	-1.72	-50.5	33.3	597	140	-2.09	-58.8	33.3	646	120	-1.38	-41.1	22.1
550	130	-1.60	-45.0	4.4	598	130	-1.49	-42.3	33.3	647	120	-1.55	-45.5	22.1
551	140	-1.42	-40.2	4.4	599	130	-1.54	-42.3	33.3	648	270	-1.66	-49.9	22.1
552	130	-1.41	-39.7	5.5	600	130	-1.46	-41.1	4.4	649	140	-1.75	-49.9	22.1
553	140	-1.27	-35.8	2.2	601	140	-1.49	-42.2	22.2	650	130	-1.76	-49.9	22.1
554	130	-1.31	-37.0	0.0	602	140	-1.27	-35.5	9.9	651	250	-1.89	-44.4	22.1
555	140	-1.35	-38.0	0.0	603	140	-1.37	-38.8	0.0	652	250	-1.71	-40.6	22.1
556	250	-1.89	-54.8	2.2	604	140	-1.95	-55.5	4.4	653	250	-1.56	-43.3	22.1
557	250	-2.15	-58.9	0.0	605	140	-1.01	-32.3	1.1	654	200	-1.42	-37.7	22.1
558	280	-2.11	-58.3	6.6	606	300	-2.93	-82.6	0.0	655	300	-1.76	-47.7	22.1
559	270	-1.86	-51.9	5.5	607	220	-1.22	-33.3	33.3	656	120	-1.37	-40.0	22.1
560	340	-1.43	-42.1	6.6	608	270	-1.21	-32.6	6.6	657	110	-1.38	-40.0	22.1
561	310	-1.70	-50.0	6.6	609	120	-1.35	-39.9	8.8	658	110	-1.37	-40.0	22.1
562	260	-1.38	-34.7	8.8	610	120	-1.32	-33.3	7.7	659	80	-1.38	-40.0	22.1
563	290	1.1	29.5	7.7	611	260	-1.24	-34.4	4.4	660	260	-2.22	-62.2	22.1
564	320	-2.32	-57.4	0.0	612	270	-1.26	-34.1	6.6	661	260	-1.86	-51.1	22.1
565	310	-1.79	-52.6	0.0	613	270	-1.93	-54.4	2.2	662	300	-1.78	-46.6	22.1
566	160	-2.43	-50.4	8.8	614	330	-1.96	-53.9	2.2	663	200	-1.57	-41.1	22.1
567	130	-1.44	-40.7	8.8	615	300	-1.35	-36.6	8.8	664	80	-1.42	-37.7	22.1
568	260	-1.35	-34.9	8.8	616	130	-1.72	-48.8	8.8	665	70	-2.22	-53.3	22.1
569	140	-1.30	-36.6	8.8	617	130	-2.11	-53.9	4.4	666	120	-1.49	-41.1	22.1
570	130	-1.21	-34.2	1.1	618	120	-1.65	-48.4	6.6	667	110	-1.31	-36.6	22.1
571	140	-1.14	-32.3	9.9	619	130	-1.64	-46.2	9.9	668	110	-1.31	-36.6	22.1
					620	130			0.0	669	110			0.0

TABLE 6A. PEAK LOADS FOR CONFIGURATION W : RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK		POSITIVE PEAK		TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK		POSITIVE PEAK		TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK		POSITIVE PEAK	
			PSF	PSF	PSF	PSF				PSF	PSF	PSF	PSF							
9331	90	-1.61	-43.1	11.6	1230	270	-.88	-24.6	18.7	1331	40	-.52	-12.8	7.4						
9332	110	-1.57	-46.1	11.2	1231	70	-.99	-22.6	23.4	1332	30	-.49	-17.7	10.3						
9333	250	-1.96	-46.4	13.9	1232	290	-.76	-22.2	21.6	1333	30	-.67	-17.5	11.1						
1101	260	-1.44	-40.2	25.0	1233	290	-.86	-22.8	19.3	1334	20	-.86	-22.4	11.2						
1102	260	-1.86	-52.0	21.5	1234	260	-.75	-21.9	15.3	1335	270	-.83	-22.3	11.0						
1103	260	-1.05	-29.2	22.2	1235	260	-.84	-23.1	17.3	1336	20	-.83	-22.2	15.4						
1104	250	-1.86	-52.0	21.5	1236	120	-.97	-28.8	15.1	1337	30	-.95	-24.4	11.1						
1105	130	-1.66	-46.7	13.3	1237	120	-1.17	-34.5	19.3	1338	30	-.87	-22.6	16.6						
1107	260	-.29	-8.0	6.0	1238	280	-1.44	-40.1	21.0	1339	260	-.56	-15.5	12.8						
1108	320	-.26	-7.7	6.0	1239	270	-.80	-22.2	17.9	1401	30	-1.73	-22.2	33.3						
1109	260	-.95	-23.5	22.5	1240	130	-.93	-23.3	26.3	1402	240	-.92	-20.8	21.7						
1110	60	-.93	-21.9	21.0	1241	280	-.39	-11.1	7.1	1403	350	-1.16	-30.0	25.4						
1111	240	-2.08	-49.4	13.0	1242	100	-1.07	-28.7	14.7	1404	330	-1.13	-33.3	15.0						
1112	110	-1.06	-31.2	14.3	1243	300	-.89	-28.6	12.0	1405	100	-1.49	-33.9	6.5						
1113	110	-1.04	-30.4	21.1	1244	260	-.42	-11.1	6.7	1406	310	-.87	-25.5	15.6						
1114	110	-.92	-26.9	11.1	1245	260	-.41	-11.4	7.0	1407	30	-.90	-25.4	17.3						
1115	80	-.61	-16.4	12.1	1246	80	-.75	-20.1	9.5	1408	250	-.98	-22.2	23.3						
1116	80	-.65	-17.7	13.3	1247	80	-.69	-18.3	15.7	1409	270	-.58	-14.4	12.2						
1117	100	-.63	-16.5	15.5	1301	250	-1.57	-37.7	15.2	1410	130	-1.28	-33.6	10.1						
1201	70	1.12	22.0	22.5	1302	80	-1.28	-34.1	13.8	1411	90	-.85	-22.2	14.0						
1202	50	1.12	22.4	27.7	1303	50	-1.90	-46.8	12.3	1412	40	-1.03	-22.2	6.4						
1203	50	-.95	-23.4	16.4	1304	40	-1.35	-33.3	21.8	1413	30	-1.30	-33.3	5.3						
1204	280	-1.82	-50.7	27.1	1305	30	-1.16	-30.0	12.3	1414	140	-.75	-21.0	10.6						
1205	30	-1.15	-29.9	29.6	1306	50	-1.40	-34.4	10.4	1415	60	-.87	-20.0	7.7						
1206	250	-1.33	-31.4	29.3	1307	30	-1.30	-33.9	20.9	1416	140	-.74	-20.0	7.6						
1207	100	-.83	-15.7	22.1	1308	70	-1.23	-33.3	15.7	1417	140	-.56	-15.5	10.8						
1208	40	-.82	-20.2	19.5	1309	80	-1.32	-35.3	9.7	1418	130	-.90	-25.5	17.3						
1209	30	-1.14	-29.9	29.6	1310	30	-.99	-25.5	13.4	1419	130	-.85	-24.0	14.6						
1210	270	-1.83	-46.1	22.2	1311	30	-.84	-22.0	10.7	1420	30	-.71	-18.6	18.3						
1211	100	-1.01	-24.4	26.9	1312	30	-.90	-22.3	9.5	1421	260	-.97	-24.4	27.7						
1212	270	-1.01	-24.4	26.9	1313	280	-.90	-22.3	20.4	1422	100	-.71	-19.0	6.5						
1213	110	-1.07	-24.4	31.1	1314	50	-.97	-23.3	21.0	1423	100	-.78	-20.0	3.6						
1214	30	-1.37	-35.4	19.4	1315	50	-.73	-17.9	12.1	1424	130	-.96	-15.7	8.5						
1215	270	-1.23	-35.3	16.3	1316	260	-.68	-18.9	12.9	1425	340	-.96	-28.8	8.5						
1216	90	-1.01	-26.9	26.9	1317	60	-.67	-16.0	12.8	1426	100	-.69	-18.4	8.4						
1217	90	-1.39	-35.7	18.8	1318	50	-1.48	-36.3	14.5	1427	100	-.69	-18.4	4.4						
1218	110	-1.07	-24.4	18.8	1319	260	-.81	-22.7	17.4	1428	110	-.53	-15.5	3.3						
1219	290	-.85	-23.5	19.8	1320	80	-.59	-15.7	15.1	1429	50	-.60	-14.9	4.0						
1220	110	-1.17	-34.4	16.1	1321	260	-.63	-16.5	17.5	1430	60	-.54	-12.2	6.6						
1221	120	-1.27	-34.3	15.3	1322	130	-.69	-16.6	19.4	1431	140	-1.21	-34.4	18.7						
1222	120	-1.30	-34.8	14.6	1323	30	-.91	-23.3	12.2	1801	260	-.51	-14.3	8.2						
1223	100	-.89	-23.2	23.7	1324	30	-.03	-2.9	16.0	1802	100	-.65	-17.4	12.0						
1224	110	-.81	-20.0	23.8	1325	30	-1.16	-30.4	25.2	1803	80	-.63	-17.3	9.3						
1225	270	-1.48	-44.7	22.7	1326	50	-.97	-23.8	13.2	1804	50	-.93	-24.4	7.7						
1226	280	-.83	-22.1	22.4	1327	40	-.82	-20.0	9.1	1805	40	-.44	-10.9	8.4						
1227	280	-1.34	-34.4	10.9	1328	140	-.58	-15.6	16.4	1806	250	-.68	-16.1	7.7						
1228	270	-1.25	-34.9	14.8	1329	100	-.56	-15.0	14.2	1807	80	-.72	-9.6	5.8						
1229	270	-.95	-24.4	13.1	1330	40	-.71	-17.4	11.0	1808	210	-.72	-14.9	3.9						

TABLE 6A. PEAK LOADS FOR CONFIGURATION W : RESORTS HOTEL CASINO, ATLANTIC CITY
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

TAP	AZI- MUTH	PRESS COEFF	NEGATIVE POSITIVE		TAP	AZI- MUTH	PRESS COEFF	NEGATIVE POSITIVE		TAP	AZI- MUTH	PRESS COEFF	NEGATIVE POSITIVE	
			PEAK	PEAK				PEAK	PEAK				PEAK	PEAK
			PSF	PSF				PSF	PSF				PSF	PSF
1901	260	-2.05	-57.2	29.0	1919	100	-1.82	-48.6	16.3	1937	40	-1.56	-33.4	6.5
1902	290	-1.54	-46.1	9.6	1920	280	-2.16	-60.4	16.6	1938	60	-1.67	-39.5	32.7
1903	270	-.79	-22.1	10.0	1921	110	-2.14	-62.8	25.5	1939	50	-1.72	-42.3	14.3
1904	30	-.94	-24.5	10.8	1922	280	-2.19	-61.0	12.8	1940	290	-.91	-27.2	11.4
1905	290	-1.00	-25.5	29.9	1923	90	-2.30	-61.4	11.0	1941	80	-1.07	-30.7	8.2
1906	50	-1.85	-45.5	16.4	1924	10	-1.86	-48.5	9.2	1942	50	-1.67	-44.1	14.2
1907	100	-1.67	-44.6	21.2	1925	60	-3.58	-84.9	10.5	1943	310	-1.21	-33.7	11.0
1908	290	-1.78	-53.4	19.0	1926	50	-1.98	-58.8	8.6	1944	30	-1.12	-32.3	6.5
1909	30	-2.56	-62.9	15.4	1927	50	-2.28	-56.0	8.2	1945	260	-1.21	-33.8	7.0
1910	30	-.93	-24.3	8.1	1928	90	-2.12	-56.7	8.0	1946	260	-1.19	-33.2	6.9
1911	20	-1.20	-31.3	11.0	1929	60	-2.06	-48.8	11.6	1947	90	-1.38	-37.7	6.2
1912	210	-2.79	-57.7	22.0	1930	50	-1.26	-31.0	7.3	1948	60	-1.11	-33.4	4.8
1913	100	-1.88	-50.1	17.8	1931	60	-2.84	-67.3	16.5	1949	40	-.62	-13.3	8.7
1914	200	-2.51	-52.0	23.6	1932	50	-2.22	-54.5	10.6	1950	50	-.56	-13.5	9.8
1915	20	-1.80	-47.0	14.8	1933	80	-1.35	-35.9	8.2	1951	320	-1.39	-40.0	17.5
1916	30	-1.99	-52.0	8.7	1934	60	-1.50	-45.6	12.0	1952	120	-.76	-22.2	5.0
1917	110	-1.17	-34.3	18.3	1935	50	-1.65	-40.6	12.9	1953	120	-.73	-21.7	6.6
1918	280	-1.72	-46.1	15.7	1936	30	-1.26	-32.9	7.0	1954	50	-1.14	-27.9	8.3

TABLE 6A. PEAK LOADS FOR CONFIGURATION W : RESORTS HOTEL CASINO, ATLANTIC CITY
 LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 30.0 PSF

* * 15 GREATEST PRESSURE MAGNITUDES * *

TAP	AZI- MUTH	PRESS COEFF	NEGATIVE PEAK ----- PSF	POSITIVE PEAK -----
540	270	-3.43	-95.7	36.8
249	110	-3.24	-95.2	26.0
124	270	-3.22	-89.8	37.6
521	130	-3.07	-86.6	42.3
520	130	-3.04	-85.8	34.0
1925	60	-3.58	-84.9	10.5
250	0	-3.18	-83.0	30.3
121	270	-2.94	-82.0	37.2
265	140	-2.89	-81.5	29.5
220	310	-2.74	-80.5	26.0
153	270	-2.83	-79.0	34.2
112	260	-2.83	-78.9	32.1
114	260	-2.83	-78.9	35.4
120	260	-2.81	-78.4	38.5
119	270	-2.75	-76.7	40.4

TABLE 7. BASE SHEAR AND MOMENT SUMMARY : RESORTS HOTEL CASINO, ATLANTIC CITY
 CONFIGURATION A REFERENCE PRESSURE 30.0 GUST FACTOR 1.00

AZIMUTH	SHEAR (KIPS)		MOMENT (1000-FT-KIPS)			ECCEN (FT)	
	X	Y	X	Y	Z	X	Y
0	-369.4	1630.7	-379.3	-93.7	53.0	31	7
10	-366.1	1960.9	-458.4	-91.7	51.1	25	5
20	-252.7	2231.7	-546.2	-62.9	52.3	22	2
30	-132.1	2252.8	-600.4	-27.4	47.4	19	1
40	72.6	2261.6	-599.7	14.6	32.6	13	-0
50	111.1	2267.5	-633.0	27.9	14.8	6	-0
60	113.3	2265.3	-633.0	7.7	5.5	2	-0
70	43.8	2297.8	-700.3	-33.3	-4.0	-1	-0
80	24.8	2281.7	-659.5	15.3	-16.4	-5	-0
90	24.8	2265.6	-614.1	67.4	-37.7	-13	2
100	46.6	2262.8	-599.9	123.1	-56.6	-21	5
110	64.4	2228.2	-515.0	132.4	-73.2	-27	8
120	64.4	1944.4	-445.1	109.9	-80.7	-34	8
130	44.4	1300.9	-301.1	103.3	-84.0	-42	9
140	44.4	1633.3	-40.9	83.3	-99.6	-47	5
150	44.4	1148.8	261.1	75.7	-99.6	-45	5
160	44.4	1148.8	228.6	89.2	-62.7	-51	5
170	44.4	1622.2	333.0	78.1	-54.8	-36	5
180	44.4	1822.2	433.3	63.9	-46.4	-28	5
190	44.4	1822.2	447.7	30.8	-39.6	-20	5
200	44.4	1533.3	443.9	1.1	-30.4	-16	5
210	44.4	1533.3	443.9	1.1	-21.3	-14	5
220	44.4	1533.3	443.9	1.1	-13.0	-11	5
230	44.4	1533.3	443.9	1.1	-13.0	-11	5
240	44.4	1533.3	443.9	1.1	-12.0	-11	5
250	44.4	1533.3	443.9	1.1	-12.0	-11	5
260	44.4	1533.3	443.9	1.1	-12.0	-11	5
270	44.4	1533.3	443.9	1.1	-12.0	-11	5
280	44.4	1533.3	443.9	1.1	-12.0	-11	5
290	44.4	1533.3	443.9	1.1	-12.0	-11	5
300	44.4	1533.3	443.9	1.1	-12.0	-11	5
310	44.4	1533.3	443.9	1.1	-12.0	-11	5
320	44.4	1533.3	443.9	1.1	-12.0	-11	5
330	44.4	1533.3	443.9	1.1	-12.0	-11	5
340	44.4	1533.3	443.9	1.1	-12.0	-11	5
350	44.4	1533.3	443.9	1.1	-12.0	-11	5
360	44.4	1533.3	443.9	1.1	-12.0	-11	5

TABLE 7. RESORTS HOTEL CASINO, ATLANTIC CITY
 PROJECT 5530 CONFIGURATION A
 SCALE = 300 REF. PRESSURE = 30.0
 GUST FACTOR = 1.00 STANDARD FLOOR HEIGHT = 8.83
 NUMBER OF SIDES = 4 NO. OF FLOORS = 40

SIDE	ANGLE	Z-AXIS	FLOOR #	LABEL	HEIGHT-FT	WIND AZIMUTH	LOAD FACTOR
1	0.0	2.275	1	GRND	54.00	0	.87
2	90.0	6.400	2	1ST	10.50	10	.87
3	180.0	2.275	3	2ND	8.83	20	.87
4	270.0	6.400	4	3RD	8.83	30	.87
			5	4TH	8.83	40	.82
			6	5TH	8.83	50	.82
			7	6TH	8.83	60	.79
			8	7TH	8.83	70	.79
			9	8TH	8.83	80	.89
			10	9TH	8.83	90	.89
			11	10TH	8.83	100	.89
			12	11TH	8.83	110	.98
			13	12TH	8.83	120	.98
			14	13TH	10.50	130	.94
			15	14TH	8.83	140	.94
			16	15TH	8.83	150	.69
			17	16TH	8.83	160	.69
			18	17TH	8.83	170	.65
			19	18TH	8.83	180	.65
			20	19TH	8.83	190	.65
			21	20TH	8.83	200	.69
			22	21ST	8.83	210	.69
			23	22ND	8.83	220	.71
			24	23RD	8.83	230	.71
			25	24TH	8.83	240	.79
			26	25TH	8.83	250	.79
			27	26TH	10.50	260	.93
			28	27TH	8.83	270	.93
			29	28TH	8.83	280	.93
			30	29TH	8.83	290	1.00
			31	30TH	8.83	300	1.00
			32	31ST	8.83	310	.98
			33	32ND	8.83	320	.98
			34	33RD	8.83	330	.98
			35	34TH	8.83	340	.98
			36	35TH	8.83	350	.87
			37	36TH	8.83		
			38	37TH	8.83		
			39	38TH	15.67		
			40	ROOF	20.00		

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 0 CONFIGURATION A

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00									-369.4	1630.7	-379.3	-93.7	53.0
1ST	54.00	-1.8	.8	79	222	-23.1	3.6	137	312	-367.6	1629.9	-291.2	-73.8	52.3
2ND	64.50	-10.9	40.7	1194	3360	-9.1	12.1	24	6	-356.7	1589.2	-274.3	-70.0	51.2
3RD	73.33	-8.5	35.3	1005	2827	-8.5	12.5	26	6	-348.2	1554.0	-260.4	-66.9	50.3
4TH	82.17	-8.0	36.2	1005	2827	-8.0	12.8	27	6	-340.1	1517.7	-246.9	-63.9	49.2
5TH	91.00	-7.5	37.2	1005	2827	-7.5	13.2	28	6	-332.6	1480.5	-233.6	-60.9	48.2
6TH	99.83	-7.0	38.2	1005	2827	-7.0	13.5	29	5	-325.6	1442.3	-220.7	-58.0	47.0
7TH	108.67	-6.5	39.2	1005	2827	-6.5	13.9	30	5	-319.1	1403.1	-208.1	-55.2	45.8
8TH	117.50	-6.0	40.1	1005	2827	-6.0	14.2	30	5	-313.1	1363.0	-195.9	-52.4	44.6
9TH	126.33	-5.5	41.1	1005	2827	-5.5	14.5	31	4	-307.6	1321.9	-184.1	-49.6	43.3
10TH	126.33	-5.0	42.1	1005	2827	-5.0	14.9	32	4	-302.6	1279.8	-172.6	-46.9	41.9
11TH	135.16	-4.5	43.1	1005	2827	-4.5	15.2	33	3	-298.0	1236.7	-161.5	-44.3	40.5
12TH	144.00	-4.5	43.2	1005	2827	-4.9	15.3	32	4	-293.1	1193.5	-150.7	-41.7	39.1
13TH	152.83	-5.5	43.0	1005	2827	-5.4	15.2	32	4	-287.6	1150.5	-140.4	-39.1	37.7
14TH	161.66	-7.2	50.9	1194	3360	-6.0	15.2	31	4	-280.5	1099.6	-128.6	-36.1	36.1
15TH	172.16	-6.6	42.6	1005	2827	-6.5	15.1	31	5	-273.9	1056.9	-119.0	-33.7	34.7
16TH	181.00	-7.1	42.5	1005	2827	-7.1	15.0	31	5	-266.8	1014.4	-109.9	-31.3	33.4
17TH	189.83	-7.6	42.3	1005	2827	-7.6	15.0	31	5	-259.2	972.1	-101.1	-29.0	32.0
18TH	198.66	-8.1	42.1	1005	2827	-8.1	14.9	30	6	-251.1	930.0	-92.7	-26.7	30.7
19TH	207.50	-8.6	41.9	1005	2827	-8.6	14.8	30	6	-242.5	888.1	-84.7	-24.5	29.4
20TH	216.33	-9.2	41.8	1005	2827	-9.1	14.8	29	6	-233.3	846.3	-77.0	-22.4	28.1
21ST	225.16	-9.5	41.7	1005	2827	-9.4	14.8	29	7	-223.8	804.6	-69.7	-20.4	26.9
22ND	233.99	-9.7	41.6	1005	2827	-9.6	14.7	29	7	-214.2	763.0	-62.8	-18.5	25.6
23RD	242.83	-9.9	41.6	1005	2827	-9.9	14.7	29	7	-204.2	721.4	-56.3	-16.6	24.3
24TH	251.66	-10.2	41.5	1005	2827	-10.1	14.7	29	7	-194.1	679.8	-50.1	-14.9	23.0
	260.49	-10.4	41.5	1005	2827	-10.4	14.7	30	7					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : RESORTS HOTEL CASINO, ATLANTIC CITY														
WIND DIRECTION 0° CONFIGURATION A REFERENCE PRESSURE 30.0 PSF GUST FACTOR 1.00														
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33	-10.6	41.4	1005	2827	-10.6	14.7	30	8	-183.7	638.3	-44.3	-13.2	21.7
26TH	278.16	-13.0	49.2	1194	3360	-10.8	14.6	30	8	-173.0	596.9	-38.8	-11.6	20.4
27TH	288.66	-11.2	41.3	1005	2827	-11.1	14.6	30	8	-160.1	547.7	-32.8	-9.9	18.8
28TH	297.49	-11.5	41.2	1005	2827	-11.5	14.6	29	8	-148.9	506.4	-28.1	-8.5	17.5
29TH	306.33	-11.5	41.0	1005	2827	-11.5	14.5	30	8	-137.4	465.3	-23.8	-7.2	16.2
30TH	315.16	-11.5	40.9	1005	2827	-11.5	14.5	31	9	-125.9	424.2	-19.9	-6.1	14.9
31ST	323.99	-11.6	40.8	1005	2827	-11.5	14.4	31	9	-114.3	383.3	-16.3	-5.0	13.5
32ND	332.82	-11.6	40.7	1005	2827	-11.5	14.4	32	9	-102.8	342.4	-13.1	-4.1	12.1
33RD	341.66	-11.6	40.6	1005	2827	-11.5	14.4	33	9	-91.2	301.7	-10.3	-3.2	10.7
34TH	350.49	-11.6	40.5	1005	2827	-11.5	14.3	33	10	-79.7	261.1	-7.8	-2.5	9.3
35TH	359.32	-11.6	40.4	1005	2827	-11.5	14.3	34	10	-68.1	220.6	-5.7	-1.8	7.8
36TH	368.16	-11.6	40.3	1005	2827	-11.6	14.3	35	10	-56.5	180.1	-3.9	-1.2	6.3
37TH	376.99	-11.6	40.2	1005	2827	-11.6	14.2	35	10	-44.8	139.8	-2.5	-.8	4.8
38TH	385.82	-22.2	62.4	1782	5013	-12.5	12.4	37	13	-33.2	99.6	-1.4	-.5	3.3
ROOF	401.49	-11.0	37.2	2276	4508	-4.8	8.3	17	5	-11.0	37.2	-.4	-.1	.7
TOP	421.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 10 CONFIGURATION A

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00	-1.9	.8	79	222	-24.7	3.4	135	347	-367.1	1960.9	-458.4	-91.7	51.1
1ST	54.00	-11.2	55.5	1194	3360	-9.4	16.5	19	4	-365.1	1960.1	-352.5	-72.0	50.3
2ND	64.50	-8.8	46.6	1005	2827	-8.7	16.5	20	4	-353.9	1904.7	-332.2	-68.2	49.2
3RD	73.33	-8.3	46.6	1005	2827	-8.3	16.5	20	4	-345.1	1858.0	-315.6	-65.1	48.2
4TH	82.17	-7.9	46.6	1005	2827	-7.9	16.5	21	3	-336.8	1811.4	-299.4	-62.1	47.2
5TH	91.00	-7.5	46.6	1005	2827	-7.4	16.5	21	3	-328.9	1764.8	-283.6	-59.1	46.2
6TH	99.83	-7.0	46.6	1005	2827	-7.0	16.5	21	3	-321.4	1718.2	-268.2	-56.3	45.2
7TH	108.67	-6.6	46.6	1005	2827	-6.6	16.5	21	3	-314.4	1671.6	-253.2	-53.5	44.2
8TH	117.50	-6.1	46.6	1005	2827	-6.1	16.5	22	3	-307.8	1625.0	-238.7	-50.7	43.2
9TH	126.33	-5.7	46.6	1005	2827	-5.7	16.5	22	3	-301.7	1578.4	-224.5	-48.0	42.2
10TH	135.16	-5.4	46.6	1005	2827	-5.4	16.5	22	3	-296.0	1531.8	-210.8	-45.4	41.1
11TH	144.00	-5.8	47.1	1005	2827	-5.8	16.7	23	3	-290.6	1485.1	-197.5	-42.8	40.1
12TH	152.83	-6.1	47.5	1005	2827	-6.1	16.8	23	3	-284.8	1438.0	-184.6	-40.2	39.0
13TH	161.66	-7.7	56.9	1194	3360	-6.4	16.9	23	3	-278.6	1390.6	-172.1	-37.8	37.9
14TH	172.16	-6.8	48.3	1005	2827	-6.8	17.1	24	3	-270.9	1333.7	-157.8	-34.9	36.5
15TH	181.00	-7.1	48.7	1005	2827	-7.1	17.2	24	4	-264.1	1285.4	-146.2	-32.5	35.4
16TH	189.83	-7.4	49.1	1005	2827	-7.4	17.4	24	4	-257.0	1236.7	-135.1	-30.2	34.2
17TH	198.66	-7.8	49.4	1005	2827	-7.7	17.5	24	4	-249.5	1187.6	-124.4	-28.0	33.0
18TH	207.50	-8.1	49.8	1005	2827	-8.0	17.6	25	4	-241.8	1138.2	-114.1	-25.8	31.7
19TH	216.33	-8.7	50.3	1005	2827	-8.7	17.8	25	4	-233.7	1088.4	-104.2	-23.7	30.4
20TH	225.16	-9.0	50.4	1005	2827	-9.0	17.8	25	4	-225.0	1038.1	-94.9	-21.7	29.2
21ST	233.99	-9.2	50.4	1005	2827	-9.2	17.8	25	5	-216.0	987.7	-85.9	-19.7	27.9
22ND	242.83	-9.4	50.4	1005	2827	-9.4	17.8	25	5	-206.7	937.3	-77.4	-17.9	26.6
23RD	251.66	-9.6	50.5	1005	2827	-9.6	17.9	25	5	-197.3	886.9	-69.3	-16.1	25.3
24TH	260.49	-9.9	50.5	1005	2827	-9.8	17.9	25	5	-187.6	836.4	-61.7	-14.4	23.9

TABLE 7. SHEAR AND MOMENT DIAGRAMS : RESORTS HOTEL CASINO, ATLANTIC CITY															
WIND DIRECTION 10		CONFIGURATION A										REFERENCE PRESSURE 30.0 PSF		GUST FACTOR 1.00	
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)			
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z	
25TH	269.33									-177.8	785.9	-54.6	-12.8	22.6	
26TH	278.16	-10.1	50.5	1005	2827	-10.0	17.9	26	5	-167.7	735.4	-47.9	-11.2	21.3	
27TH	288.66	-12.2	60.1	1194	3360	-10.3	17.9	26	5	-155.5	675.3	-40.4	-9.5	19.6	
28TH	297.49	-10.5	50.6	1005	2827	-10.5	17.9	26	5	-144.9	624.7	-34.7	-8.2	18.3	
29TH	306.33	-11.1	50.7	1005	2827	-11.1	17.9	25	6	-133.8	574.0	-29.4	-7.0	16.9	
30TH	315.16	-11.2	50.6	1005	2827	-11.1	17.9	26	6	-122.6	523.4	-24.6	-5.9	15.5	
31ST	323.99	-11.3	50.5	1005	2827	-11.2	17.9	27	6	-111.3	473.0	-20.2	-4.8	14.1	
32ND	332.82	-11.3	50.4	1005	2827	-11.3	17.8	27	6	-100.0	422.6	-16.2	-3.9	12.7	
33RD	341.66	-11.4	50.3	1005	2827	-11.3	17.8	28	6	-88.7	372.3	-12.7	-3.1	11.2	
34TH	350.49	-11.4	50.2	1005	2827	-11.4	17.7	28	6	-77.2	322.2	-9.6	-2.3	9.8	
35TH	359.32	-11.5	50.1	1005	2827	-11.4	17.7	29	7	-65.8	272.1	-7.0	-1.7	8.2	
36TH	368.16	-11.5	50.0	1005	2827	-11.5	17.7	29	7	-54.2	222.1	-4.8	-1.2	6.7	
37TH	376.99	-11.6	49.9	1005	2827	-11.5	17.6	30	7	-42.6	172.2	-3.1	-.7	5.1	
38TH	385.82	-11.7	49.8	1005	2827	-11.6	17.6	30	7	-31.0	122.5	-1.8	-.4	3.5	
ROOF	401.49	-21.8	76.4	1782	5013	-12.2	15.2	34	10	-9.2	46.0	-.5	-.1	.8	
TOP	421.50	-9.2	46.0	2276	4508	-4.0	10.2	16	3	0.0	0.0	0.0	0.0	0.0	

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 20 CONFIGURATION A

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00	-2.0	1.0	79	222	-25.3	4.3	160	336	-252.7	2317.8	-546.2	-62.9	52.3
1ST	54.00	-10.4	66.8	1194	3360	-8.7	19.9	17	3	-250.7	2316.8	-421.1	-49.3	51.5
2ND	64.50	-7.9	55.8	1005	2827	-7.8	19.7	17	2	-240.3	2250.0	-397.1	-46.7	50.4
3RD	73.33	-7.2	55.4	1005	2827	-7.2	19.6	18	2	-232.4	2194.2	-377.5	-44.6	49.4
4TH	82.17	-6.6	55.1	1005	2827	-6.6	19.5	18	2	-225.2	2138.8	-358.3	-42.6	48.4
5TH	91.00	-5.9	54.7	1005	2827	-5.9	19.3	18	2	-218.6	2083.7	-339.7	-40.6	47.4
6TH	99.83	-5.3	54.3	1005	2827	-5.3	19.2	18	2	-212.7	2029.0	-321.5	-38.7	46.4
7TH	108.67	-4.6	54.0	1005	2827	-4.6	19.1	19	2	-207.4	1974.7	-303.9	-36.9	45.4
8TH	117.50	-4.0	53.6	1005	2827	-4.0	19.0	19	1	-202.7	1920.7	-286.6	-35.0	44.4
9TH	126.33	-3.4	53.2	1005	2827	-3.3	18.8	19	1	-198.7	1867.2	-269.9	-33.3	43.3
10TH	135.16	-2.8	52.9	1005	2827	-2.8	18.7	20	1	-195.4	1814.0	-253.7	-31.5	42.3
11TH	144.00	-3.2	53.4	1005	2827	-3.1	18.9	20	1	-192.5	1761.0	-237.9	-29.8	41.3
12TH	152.83	-3.4	53.9	1005	2827	-3.4	19.1	20	1	-189.4	1707.7	-222.6	-28.1	40.2
13TH	161.66	-4.3	64.8	1194	3360	-3.6	19.3	20	1	-186.0	1653.8	-207.7	-26.5	39.1
14TH	172.16	-3.8	55.0	1005	2827	-3.8	19.5	21	1	-181.7	1589.0	-190.7	-24.5	37.8
15TH	181.00	-4.0	55.6	1005	2827	-4.0	19.7	21	2	-177.9	1534.0	-176.9	-23.0	36.7
16TH	189.83	-4.2	56.1	1005	2827	-4.2	19.8	21	2	-173.9	1478.4	-163.6	-21.4	35.5
17TH	198.66	-4.5	56.6	1005	2827	-4.4	20.0	21	2	-169.6	1422.3	-150.8	-19.9	34.3
18TH	207.50	-4.7	57.1	1005	2827	-4.6	20.2	22	2	-165.2	1365.7	-138.5	-18.4	33.1
19TH	216.33	-5.2	57.7	1005	2827	-5.2	20.4	22	2	-160.5	1308.6	-126.7	-17.0	31.8
20TH	225.16	-5.5	58.2	1005	2827	-5.5	20.6	22	2	-155.3	1250.9	-115.3	-15.6	30.6
21ST	233.99	-5.7	58.6	1005	2827	-5.7	20.7	22	2	-149.8	1192.7	-104.6	-14.2	29.3
22ND	242.83	-5.9	59.0	1005	2827	-5.8	20.9	22	2	-144.1	1134.0	-94.3	-12.9	28.0
23RD	251.66	-6.1	59.5	1005	2827	-6.0	21.0	22	2	-138.2	1075.0	-84.5	-11.7	26.7
24TH	260.49	-6.2	59.9	1005	2827	-6.2	21.2	23	2	-132.2	1015.5	-75.3	-10.5	25.3

TABLE 7. SHEAR AND MOMENT DIAGRAMS : RESORTS HOTEL CASINO, ATLANTIC CITY														
WIND DIRECTION 20		CONFIGURATION A								REFERENCE PRESSURE 30.0 PSF			GUST FACTOR 1.00	
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33									-125.9	955.7	-66.6	-9.3	24.0
26TH	278.16	-6.4	60.3	1005	2827	-6.4	21.3	23	2	-119.5	895.3	-58.4	-8.3	22.6
27TH	286.66	-7.9	72.2	1194	3360	-6.6	21.5	23	3	-111.6	823.1	-49.4	-7.0	20.9
28TH	297.49	-6.8	61.2	1005	2827	-6.8	21.7	23	3	-104.8	761.9	-42.4	-6.1	19.5
29TH	306.33	-7.6	61.8	1005	2827	-7.6	21.9	23	3	-97.2	700.1	-35.9	-5.2	18.0
30TH	315.16	-7.7	61.6	1005	2827	-7.7	21.8	23	3	-89.4	638.5	-30.0	-4.4	16.6
31ST	323.99	-7.8	61.5	1005	2827	-7.8	21.8	24	3	-81.6	577.0	-24.7	-3.6	15.1
32ND	332.82	-7.9	61.3	1005	2827	-7.9	21.7	24	3	-73.7	515.6	-19.8	-2.9	13.6
33RD	341.66	-8.0	61.2	1005	2827	-8.0	21.7	25	3	-65.7	454.4	-15.5	-2.3	12.0
34TH	350.49	-8.1	61.1	1005	2827	-8.1	21.6	25	3	-57.6	393.4	-11.8	-1.8	10.4
35TH	359.32	-8.2	60.9	1005	2827	-8.2	21.6	26	3	-49.4	332.4	-8.6	-1.3	8.8
36TH	368.16	-8.3	60.8	1005	2827	-8.2	21.5	26	4	-41.1	271.7	-5.9	-.9	7.2
37TH	376.99	-8.4	60.6	1005	2827	-8.3	21.5	27	4	-32.7	211.0	-3.8	-.6	5.5
38TH	385.82	-8.5	60.5	1005	2827	-8.4	21.4	27	4	-24.2	150.5	-2.2	-.3	3.8
ROOF	401.49	-16.7	93.6	1782	5013	-9.3	18.7	31	5	-7.6	56.9	-.6	-.1	.9
TOP	421.50	-7.6	56.9	2276	4508	-3.3	12.6	15	2	0.0	0.0	0.0	0.0	0.0

RESORTS HOTEL CASINO, ATLANTIC CITY														
GUST FACTOR 1.00														
WIND DIRECTION 30 CONFIGURATION A REFERENCE PRESSURE 30.0 PSF														
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00													
		-2.1	.0	79	222	-27.1	.1	6	393	-132.1	2528.0	-600.4	-27.4	47.4
1ST	54.00													
		-11.6	72.8	1194	3360	-9.7	21.7	17	3	-130.0	2528.0	-463.9	-20.3	46.5
2ND	64.50													
		-8.6	60.6	1005	2827	-8.5	21.4	17	2	-118.4	2455.1	-437.7	-19.0	45.3
3RD	73.33													
		-7.7	59.9	1005	2827	-7.6	21.2	17	2	-109.8	2394.6	-416.3	-18.0	44.2
4TH	82.17													
		-6.8	59.3	1005	2827	-6.8	21.0	17	2	-102.1	2334.6	-395.4	-17.0	43.2
5TH	91.00													
		-5.9	58.6	1005	2827	-5.9	20.7	17	2	-95.3	2275.3	-375.1	-16.2	42.2
6TH	99.83													
		-5.0	58.0	1005	2827	-5.0	20.5	17	1	-89.4	2216.7	-355.2	-15.3	41.2
7TH	108.67													
		-4.1	57.3	1005	2827	-4.1	20.3	17	1	-84.4	2158.8	-335.9	-14.6	40.2
8TH	117.50													
		-3.2	56.7	1005	2827	-3.2	20.0	17	1	-80.3	2101.4	-317.1	-13.8	39.3
9TH	126.33													
		-2.4	56.0	1005	2827	-2.3	19.8	17	1	-77.0	2044.8	-298.8	-13.2	38.3
10TH	135.16													
		-1.5	55.4	1005	2827	-1.5	19.6	17	0	-74.7	1988.8	-281.0	-12.5	37.4
11TH	144.00													
		-1.5	56.1	1005	2827	-1.5	19.8	17	0	-73.1	1933.4	-263.6	-11.8	36.5
12TH	152.83													
		-1.5	56.9	1005	2827	-1.5	20.1	17	0	-71.7	1877.3	-246.8	-11.2	35.5
13TH	161.66													
		-1.7	68.7	1194	3360	-1.5	20.4	17	0	-70.2	1820.4	-230.5	-10.6	34.6
14TH	172.16													
		-1.5	58.7	1005	2827	-1.4	20.8	17	0	-68.4	1751.7	-211.7	-9.8	33.4
15TH	181.00													
		-1.4	59.5	1005	2827	-1.4	21.1	17	0	-67.0	1693.0	-196.5	-9.2	32.4
16TH	189.83													
		-1.4	60.4	1005	2827	-1.4	21.4	17	0	-65.5	1633.5	-181.8	-8.7	31.4
17TH	198.66													
		-1.4	61.2	1005	2827	-1.4	21.6	17	0	-64.1	1573.1	-167.7	-8.1	30.3
18TH	207.50													
		-1.4	62.0	1005	2827	-1.4	21.9	18	0	-62.7	1511.9	-154.0	-7.5	29.3
19TH	216.33													
		-1.4	62.0	1005	2827	-1.4	21.9	18	0	-61.3	1449.9	-141.0	-7.0	28.2
20TH	225.16													
		-1.8	63.1	1005	2827	-1.8	22.3	18	1	-59.5	1386.7	-128.4	-6.4	27.0
21ST	233.99													
		-1.9	63.8	1005	2827	-1.9	22.6	18	1	-57.5	1323.0	-116.5	-5.9	25.9
22ND	242.83													
		-2.0	64.4	1005	2827	-2.0	22.8	18	1	-55.5	1258.6	-105.1	-5.4	24.7
23RD	251.66													
		-2.0	64.9	1005	2827	-2.0	23.0	18	1	-53.6	1193.7	-94.2	-4.9	23.5
24TH	260.49													
		-2.0	66.1	1005	2827	-2.0	23.4	18	1	-51.5	1128.2	-84.0	-4.5	22.3

TABLE 7. SHEAR AND MOMENT DIAGRAMS : RESORTS HOTEL CASINO, ATLANTIC CITY															
WIND DIRECTION 30		CONFIGURATION A								REFERENCE PRESSURE 30.0 PSF				GUST FACTOR 1.00	
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)			
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z	
25TH	269.33			1005	2827	-2.0	23.6	18	1	-49.5	1062.1	-74.3	-4.0	21.1	
26TH	278.16	-2.1	66.6	1194	3360	-2.1	23.8	18	1	-47.5	995.5	-65.2	-3.6	19.8	
27TH	288.66	-2.5	79.9	1005	2827	-2.1	24.0	18	1	-45.0	915.6	-55.2	-3.1	18.4	
28TH	297.49	-2.1	67.9	1005	2827	-2.1	24.0	18	1	-42.9	847.7	-47.4	-2.7	17.1	
29TH	306.33	-2.6	68.6	1005	2827	-2.6	24.3	18	1	-40.3	779.1	-40.2	-2.4	15.9	
30TH	315.16	-2.7	68.4	1005	2827	-2.6	24.2	19	1	-37.7	710.7	-33.6	-2.0	14.6	
31ST	323.99	-2.7	68.2	1005	2827	-2.7	24.1	19	1	-34.9	642.5	-27.6	-1.7	13.2	
32ND	332.82	-2.8	68.0	1005	2827	-2.8	24.0	20	1	-32.1	574.6	-22.3	-1.4	11.9	
33RD	341.66	-2.9	67.7	1005	2827	-2.9	24.0	20	1	-29.2	506.8	-17.5	-1.1	10.5	
34TH	350.49	-3.0	67.5	1005	2827	-3.0	23.9	21	1	-26.2	439.3	-13.3	-.9	9.1	
35TH	359.32	-3.1	67.3	1005	2827	-3.0	23.8	21	1	-23.2	372.0	-9.7	-.7	7.6	
36TH	368.16	-3.1	67.1	1005	2827	-3.1	23.7	22	1	-20.0	304.9	-6.7	-.5	6.2	
37TH	376.99	-3.2	66.9	1005	2827	-3.2	23.7	22	1	-16.8	238.0	-4.3	-.3	4.7	
38TH	385.82	-3.3	66.6	1005	2827	-3.3	23.6	23	1	-13.5	171.4	-2.5	-.2	3.1	
ROOF	401.49	-9.4	104.3	1782	5013	-5.3	20.8	24	2	-4.1	67.1	-.7	-.0	.6	
TOP	421.50	-4.1	67.1	2276	4508	-1.8	14.9	8	1	0.0	0.0	0.0	0.0	0.0	

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 40 CONFIGURATION A

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00	-2.2	-3	79	222	-28.2	-1.4	-53	383	22.3	2503.9	-596.7	14.6	32.6
1ST	54.00	-11.3	72.5	1194	3360	-9.4	21.6	15	2	24.6	2504.2	-461.5	13.3	31.8
2ND	64.50	-8.1	60.2	1005	2827	-8.0	21.3	15	2	35.8	2431.7	-435.6	13.0	30.7
3RD	73.33	-7.0	59.5	1005	2827	-6.9	21.0	15	2	43.9	2371.5	-414.4	12.6	29.7
4TH	82.17	-5.8	58.8	1005	2827	-5.8	20.8	15	1	50.9	2312.0	-393.7	12.2	28.8
5TH	91.00	-4.7	58.1	1005	2827	-4.7	20.5	15	1	56.7	2253.3	-373.5	11.7	28.0
6TH	99.83	-3.6	57.4	1005	2827	-3.6	20.3	14	1	61.4	2195.2	-353.9	11.2	27.1
7TH	108.67	-2.5	56.7	1005	2827	-2.5	20.0	14	1	65.0	2137.8	-334.7	10.7	26.3
8TH	117.50	-1.4	55.9	1005	2827	-1.4	19.8	14	0	67.5	2081.2	-316.1	10.1	25.5
9TH	126.33	-3	55.2	1005	2827	-3	19.5	14	0	68.9	2025.2	-298.0	9.5	24.7
10TH	135.16	.9	54.6	1005	2827	.9	19.3	13	-0	69.2	1970.0	-280.3	8.9	24.0
11TH	144.00	1.4	55.1	1005	2827	1.4	19.5	13	-0	68.3	1915.4	-263.2	8.3	23.2
12TH	152.83	1.6	55.9	1005	2827	1.6	19.8	13	-0	66.9	1860.3	-246.5	7.7	22.5
13TH	161.66	2.1	67.4	1194	3360	1.7	20.1	13	-0	65.4	1804.4	-230.3	7.1	21.8
14TH	172.16	1.9	57.6	1005	2827	1.9	20.4	12	-0	63.3	1737.0	-211.7	6.4	20.9
15TH	181.00	2.1	58.4	1005	2827	2.1	20.6	12	-0	61.4	1679.4	-196.6	5.8	20.2
16TH	189.83	2.3	59.1	1005	2827	2.3	20.9	12	-0	59.3	1621.0	-182.0	5.3	19.5
17TH	198.66	2.4	59.9	1005	2827	2.4	21.2	12	-0	57.0	1561.9	-168.0	4.8	18.8
18TH	207.50	2.6	60.7	1005	2827	2.6	21.5	11	-0	54.6	1501.9	-154.5	4.3	18.1
19TH	216.33	2.9	61.7	1005	2827	2.9	21.8	12	-1	52.0	1441.2	-141.5	3.8	17.4
20TH	225.16	2.9	62.4	1005	2827	2.9	22.1	12	-1	49.1	1379.5	-129.0	3.4	16.7
21ST	233.99	3.0	63.0	1005	2827	3.0	22.3	12	-1	46.1	1317.1	-117.1	3.0	16.0
22ND	242.83	3.1	63.6	1005	2827	3.0	22.5	11	-1	43.1	1254.1	-105.7	2.6	15.3
23RD	251.66	3.1	64.2	1005	2827	3.1	22.7	11	-1	40.1	1190.5	-94.9	2.2	14.5
24TH	260.49	3.2	64.9	1005	2827	3.1	22.9	11	-1	37.0	1126.2	-84.7	1.9	13.8

TABLE 7. SHEAR AND MOMENT DIAGRAMS :														
WIND DIRECTION 40		RESORTS HOTEL CASINO, ATLANTIC CITY										GUST FACTOR 1.00		
		CONFIGURATION A										REFERENCE PRESSURE 30.0 PSF		
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33									33.8	1061.4	-75.0	1.6	13.1
		3.2	65.5	1005	2827	3.2	23.2	11	-1	30.6	995.9	-66.0	1.3	12.3
26TH	278.16	3.9	78.6	1194	3360	3.2	23.4	11	-1	26.8	917.3	-55.9	1.0	11.5
27TH	288.66	3.3	66.8	1005	2827	3.3	23.6	11	-1	23.4	850.4	-48.1	.7	10.7
28TH	297.49	3.4	67.6	1005	2827	3.4	23.9	11	-1	20.0	782.9	-40.9	.6	10.0
29TH	306.33	3.2	67.5	1005	2827	3.2	23.9	11	-1	16.8	715.4	-34.3	.4	9.2
30TH	315.16	3.0	67.4	1005	2827	3.0	23.8	12	-1	13.7	648.0	-28.3	.3	8.4
31ST	323.99	2.9	67.3	1005	2827	2.9	23.8	12	-1	10.9	580.8	-22.8	.1	7.6
32ND	332.82	2.7	67.2	1005	2827	2.7	23.8	13	-1	8.2	513.6	-18.0	.1	6.7
33RD	341.66	2.5	67.1	1005	2827	2.5	23.7	13	-0	5.7	446.6	-13.8	.0	5.8
34TH	350.49	2.3	67.0	1005	2827	2.3	23.7	14	-0	3.4	379.6	-10.1	-0.0	4.9
35TH	359.32	2.1	66.9	1005	2827	2.1	23.7	14	-0	1.3	312.8	-7.0	-0.1	4.0
36TH	368.16	1.9	66.7	1005	2827	1.9	23.6	14	-0	-.7	246.0	-4.6	-0.1	3.0
37TH	376.99	1.8	66.6	1005	2827	1.8	23.6	15	-0	-2.4	179.4	-2.7	-0.0	2.0
38TH	385.82	-.8	106.6	1782	5013	-.4	21.3	16	0	-1.7	72.8	-.7	-0.0	.3
ROOF	401.49	-1.7	72.8	2276	4508	-.7	16.1	4	0	0.0	0.0	0.0	0.0	0.0
TOP	421.50													

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 50 CONFIGURATION A

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00	-2.2	-1.5	79	222	-28.2	-2.2	-89	412	76.6	2616.4	-623.0	27.9	14.8
1ST	54.00	-10.2	78.3	1194	3360	-8.6	23.3	10	1	78.8	2616.9	-481.7	23.7	13.8
2ND	64.50	-7.2	64.8	1005	2827	-7.1	22.9	9	1	89.0	2538.6	-454.6	22.8	13.0
3RD	73.33	-6.0	63.7	1005	2827	-6.0	22.5	9	1	96.2	2473.8	-432.5	22.0	12.4
4TH	82.17	-4.9	62.7	1005	2827	-4.9	22.2	8	1	102.2	2410.1	-410.9	21.1	11.9
5TH	91.00	-3.7	61.6	1005	2827	-3.7	21.8	8	0	107.1	2347.4	-389.9	20.2	11.3
6TH	99.83	-2.6	60.6	1005	2827	-2.6	21.4	7	0	110.8	2285.8	-369.4	19.2	10.9
7TH	108.67	-1.4	59.5	1005	2827	-1.4	21.1	6	0	113.4	2225.2	-349.5	18.2	10.4
8TH	117.50	-.3	58.5	1005	2827	-.3	20.7	6	0	114.8	2165.7	-330.1	17.2	10.1
9TH	126.33	.8	57.4	1005	2827	.8	20.3	5	-0	115.1	2107.3	-311.3	16.2	9.7
10TH	135.16	2.1	56.3	1005	2827	2.1	19.9	4	-0	114.3	2049.8	-292.9	15.2	9.4
11TH	144.00	2.7	56.8	1005	2827	2.7	20.1	4	-0	112.2	1993.5	-275.0	14.2	9.2
12TH	152.83	2.9	57.6	1005	2827	2.9	20.4	4	-0	109.4	1936.7	-257.7	13.2	9.0
13TH	161.66	3.6	69.6	1194	3360	3.1	20.7	4	-0	106.5	1879.1	-240.8	12.3	8.7
14TH	172.16	3.2	59.5	1005	2827	3.2	21.1	4	-0	102.9	1809.5	-221.5	11.2	8.4
15TH	181.00	3.4	60.4	1005	2827	3.4	21.4	4	-0	99.7	1749.9	-205.7	10.3	8.2
16TH	189.83	3.5	61.2	1005	2827	3.5	21.7	4	-0	96.3	1689.6	-190.6	9.4	8.0
17TH	198.66	3.7	62.1	1005	2827	3.7	22.0	4	-0	92.7	1628.3	-175.9	8.6	7.7
18TH	207.50	3.9	63.0	1005	2827	3.8	22.3	4	-0	89.0	1566.2	-161.8	7.8	7.5
19TH	216.33	4.4	63.9	1005	2827	4.4	22.6	4	-0	85.1	1503.2	-148.2	7.0	7.3
20TH	225.16	4.5	64.7	1005	2827	4.5	22.9	4	-0	80.8	1439.3	-135.2	6.3	7.0
21ST	233.99	4.5	65.3	1005	2827	4.5	23.1	4	-0	76.3	1374.6	-122.8	5.6	6.7
22ND	242.83	4.5	66.0	1005	2827	4.5	23.4	4	-0	71.7	1309.3	-111.0	4.9	6.4
23RD	251.66	4.6	66.7	1005	2827	4.5	23.6	4	-0	67.2	1243.2	-99.7	4.3	6.1
24TH	260.49	4.6	67.4	1005	2827	4.5	23.8	4	-0	62.6	1176.5	-89.0	3.7	5.9

TABLE 7. SHEAR AND MOMENT DIAGRAMS :														
WIND DIRECTION 50		RESORTS HOTEL CASINO, ATLANTIC CITY										GUST FACTOR 1.00		
		CONFIGURATION A										REFERENCE PRESSURE 30.0 PSF		
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33									58.1	1109.1	-78.9	3.2	5.6
26TH	278.16	4.6	68.1	1005	2827	4.6	24.1	4	-0	53.5	1041.1	-69.4	2.7	5.3
27TH	288.66	5.5	81.8	1194	3360	4.6	24.3	4	-0	48.0	959.3	-58.9	2.2	5.0
28TH	297.49	4.6	69.6	1005	2827	4.6	24.6	4	-0	43.4	889.7	-50.7	1.8	4.7
29TH	306.33	5.2	70.1	1005	2827	5.1	24.8	4	-0	38.2	819.6	-43.2	1.4	4.4
30TH	315.16	5.0	70.0	1005	2827	5.0	24.8	5	-0	33.2	749.6	-36.3	1.1	4.1
31ST	323.99	4.8	69.9	1005	2827	4.8	24.7	5	-0	28.4	679.7	-29.9	.8	3.8
32ND	332.82	4.6	69.8	1005	2827	4.6	24.7	5	-0	23.8	609.9	-24.2	.6	3.4
33RD	341.66	4.4	69.7	1005	2827	4.4	24.6	5	-0	19.4	540.2	-19.2	.4	3.0
34TH	350.49	4.2	69.5	1005	2827	4.2	24.6	6	-0	15.2	470.7	-14.7	.2	2.6
35TH	359.32	4.1	69.4	1005	2827	4.0	24.6	6	-0	11.1	401.3	-10.9	.1	2.2
36TH	368.16	3.9	69.3	1005	2827	3.9	24.5	6	-0	7.2	332.0	-7.6	.0	1.8
37TH	376.99	3.7	69.2	1005	2827	3.7	24.5	7	-0	3.5	262.8	-5.0	-0	1.3
38TH	385.82	3.5	69.1	1005	2827	3.5	24.4	7	-0	.0	193.7	-3.0	-0	.8
ROOF	401.49	1.4	112.2	1782	5013	.8	22.4	8	-0	-1.4	81.5	-.8	-0	-0
TOP	421.50	-1.4	81.5	2276	4508	-.6	18.1	-0	-0	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 60° CONFIGURATION A

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00	-2.1	-1.0	79	222	-26.6	-4.7	-204	410	-1	2675.8	-636.2	7.0	5.5
1ST	54.00	-9.8	79.0	1194	3360	-8.2	23.5	6	1	2.0	2676.9	-491.6	7.0	4.4
2ND	64.50	-7.0	65.6	1005	2827	-6.9	23.2	6	1	11.8	2597.9	-464.0	6.9	3.9
3RD	73.33	-6.0	64.6	1005	2827	-5.9	22.9	5	1	18.7	2532.3	-441.3	6.8	3.5
4TH	82.17	-4.9	63.7	1005	2827	-4.9	22.5	5	0	24.7	2467.7	-419.2	6.6	3.2
5TH	91.00	-3.9	62.8	1005	2827	-3.9	22.2	4	0	29.6	2404.0	-397.7	6.4	2.9
6TH	99.83	-2.9	61.9	1005	2827	-2.9	21.9	4	0	33.6	2341.2	-376.7	6.1	2.6
7TH	108.67	-1.9	61.0	1005	2827	-1.9	21.6	3	0	36.5	2279.3	-356.3	5.8	2.4
8TH	117.50	-1.9	60.0	1005	2827	-1.9	21.2	2	0	38.5	2218.3	-336.5	5.4	2.2
9TH	126.33	1	59.1	1005	2827	1	20.9	2	-0	39.4	2158.3	-317.1	5.1	2.0
10TH	135.16	1.2	58.2	1005	2827	1.2	20.6	1	-0	39.3	2099.1	-298.3	4.7	1.9
11TH	144.00	1.6	58.6	1005	2827	1.6	20.7	1	-0	38.2	2041.0	-280.1	4.4	1.9
12TH	152.83	1.6	59.5	1005	2827	1.5	21.0	1	-0	36.5	1982.4	-262.3	4.1	1.8
13TH	161.66	1.8	71.9	1194	3360	1.5	21.4	1	-0	35.0	1922.9	-245.0	3.8	1.7
14TH	172.16	1.4	61.5	1005	2827	1.4	21.8	1	-0	33.2	1851.0	-225.2	3.4	1.6
15TH	181.00	1.4	62.5	1005	2827	1.4	22.1	1	-0	31.8	1789.5	-209.1	3.1	1.5
16TH	189.83	1.3	63.4	1005	2827	1.3	22.4	1	-0	30.4	1727.0	-193.6	2.8	1.5
17TH	198.66	1.3	64.3	1005	2827	1.3	22.8	1	-0	29.1	1663.6	-178.6	2.6	1.4
18TH	207.50	1.2	65.2	1005	2827	1.2	23.1	1	-0	27.8	1599.3	-164.2	2.3	1.4
19TH	216.33	1.4	66.0	1005	2827	1.4	23.4	1	-0	26.6	1534.1	-150.4	2.1	1.3
20TH	225.16	1.5	66.7	1005	2827	1.5	23.6	1	-0	25.2	1468.1	-137.1	1.8	1.2
21ST	233.99	1.5	67.4	1005	2827	1.4	23.8	1	-0	23.7	1401.4	-124.5	1.6	1.2
22ND	242.83	1.5	68.1	1005	2827	1.4	24.1	1	-0	22.3	1334.0	-112.4	1.4	1.1
23RD	251.66	1.5	68.8	1005	2827	1.4	24.3	1	-0	20.8	1265.9	-100.9	1.2	1.0
24TH	260.49	1.4	69.5	1005	2827	1.4	24.6	1	-0	19.4	1197.1	-90.0	1.1	.9

TABLE 7. SHEAR AND MOMENT DIAGRAMS : RESORTS HOTEL CASINO, ATLANTIC CITY															
WIND DIRECTION 60		CONFIGURATION A										REFERENCE PRESSURE 30.0 PSF		GUST FACTOR 1.00	
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)			
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z	
25TH	269.33									17.9	1127.7	-79.7	.9	.8	
26TH	278.16	1.4	70.2	1005	2827	1.4	24.8	1	-0	16.5	1057.5	-70.1	.7	.8	
27TH	288.66	1.7	84.3	1194	3360	1.4	25.1	1	-0	14.8	973.2	-59.4	.6	.7	
28TH	297.49	1.4	71.7	1005	2827	1.4	25.4	1	-0	13.3	901.5	-51.2	.5	.6	
29TH	306.33	1.8	72.2	1005	2827	1.8	25.5	2	-0	11.5	829.3	-43.5	.3	.5	
30TH	315.16	1.7	71.9	1005	2827	1.7	25.4	1	-0	9.8	757.5	-36.5	.3	.4	
31ST	323.99	1.7	71.5	1005	2827	1.6	25.3	1	-0	8.1	685.9	-30.1	.2	.3	
32ND	332.82	1.6	71.2	1005	2827	1.6	25.2	1	-0	6.6	614.7	-24.4	.1	.2	
33RD	341.66	1.5	70.9	1005	2827	1.5	25.1	1	-0	5.1	543.8	-19.3	.1	.1	
34TH	350.49	1.4	70.5	1005	2827	1.4	25.0	1	-0	3.7	473.3	-14.8	.0	.0	
35TH	359.32	1.3	70.2	1005	2827	1.3	24.8	1	-0	2.3	403.1	-10.9	-0.0	-0.0	
36TH	368.16	1.3	69.9	1005	2827	1.3	24.7	1	-0	1.1	333.3	-7.7	-0.0	-0.1	
37TH	376.99	1.2	69.5	1005	2827	1.2	24.6	1	-0	-0.1	263.8	-5.0	-0.0	-0.2	
38TH	385.82	1.1	69.2	1005	2827	1.1	24.5	1	-0	-1.2	194.6	-3.0	-0.0	-0.2	
ROOF	401.49	-0.6	112.3	1782	5013	-0.3	22.4	1	0	-0.6	82.3	-0.8	-0.0	-0.3	
TOP	421.50	-0.6	82.3	2276	4508	-0.3	18.3	-4	-0	0.0	0.0	0.0	0.0	0.0	

TABLE 7. SHEAR AND MOMENT DIAGRAMS : RESORTS HOTEL CASINO, ATLANTIC CITY
 WIND DIRECTION 70 CONFIGURATION A REFERENCE PRESSURE 30.0 PSF

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00									-13.9	2658.1	-630.9	3.0	-4.0
1ST	54.00	-2.1	-1.9	79	222	-26.3	-8.7	-317	342	-11.8	2660.1	-487.4	3.7	-5.3
2ND	64.50	-9.7	78.0	1194	3360	-8.2	23.2	5	1	-2.0	2582.0	-459.8	3.8	-5.7
3RD	73.33	-7.0	64.9	1005	2827	-6.9	23.0	4	0	4.9	2517.1	-437.3	3.8	-5.9
4TH	82.17	-5.9	64.1	1005	2827	-5.9	22.7	3	0	10.9	2453.0	-415.4	3.7	-6.1
5TH	91.00	-4.9	63.3	1005	2827	-4.9	22.4	2	0	15.7	2389.7	-394.0	3.6	-6.3
6TH	99.83	-3.8	62.5	1005	2827	-3.8	22.1	2	0	19.6	2327.2	-373.1	3.4	-6.4
7TH	108.67	-2.8	61.7	1005	2827	-2.8	21.8	1	0	22.4	2265.5	-352.9	3.2	-6.4
8TH	117.50	-1.7	61.0	1005	2827	-1.7	21.6	-0	-0	24.1	2204.5	-333.1	3.0	-6.4
9TH	126.33	-.7	60.2	1005	2827	-.7	21.3	-1	-0	24.8	2144.4	-313.9	2.8	-6.3
10TH	135.16	.3	59.4	1005	2827	.3	21.0	-2	0	24.5	2085.0	-295.2	2.6	-6.2
11TH	144.00	1.5	58.4	1005	2827	1.5	20.7	-2	0	23.0	2026.6	-277.1	2.4	-6.1
12TH	152.83	1.8	58.4	1005	2827	1.7	20.7	-1	0	21.3	1968.2	-259.4	2.2	-6.0
13TH	161.66	1.6	59.4	1005	2827	1.6	21.0	-1	0	19.7	1908.7	-242.3	2.0	-5.9
14TH	172.16	1.7	71.9	1194	3360	1.4	21.4	-2	0	18.0	1836.9	-222.6	1.8	-5.8
15TH	181.00	1.3	61.5	1005	2827	1.3	21.8	-2	0	16.7	1775.3	-206.7	1.7	-5.7
16TH	189.83	1.1	62.5	1005	2827	1.1	22.1	-2	0	15.6	1712.8	-191.3	1.5	-5.6
17TH	198.66	1.0	63.5	1005	2827	1.0	22.5	-3	0	14.6	1649.3	-176.4	1.4	-5.4
18TH	207.50	.8	64.5	1005	2827	.8	22.8	-3	0	13.8	1584.9	-162.2	1.3	-5.2
19TH	216.33	.7	65.4	1005	2827	.7	23.1	-3	0	13.1	1519.4	-148.4	1.1	-5.0
20TH	225.16	.8	65.7	1005	2827	.8	23.2	-1	0	12.3	1453.7	-135.3	1.0	-4.9
21ST	233.99	.8	66.3	1005	2827	.8	23.5	-1	0	11.5	1387.5	-122.8	.9	-4.8
22ND	242.83	.8	67.0	1005	2827	.8	23.7	-2	0	10.8	1320.4	-110.8	.8	-4.7
23RD	251.66	.7	67.8	1005	2827	.7	24.0	-2	0	10.1	1252.7	-99.4	.7	-4.6
24TH	260.49	.7	68.5	1005	2827	.7	24.2	-2	0	9.4	1184.2	-88.7	.6	-4.4
		.6	69.2	1005	2827	.6	24.5	-3	0					

TABLE 7. SHEAR AND MOMENT DIAGRAMS :														
WIND DIRECTION 70		RESORTS HOTEL CASINO, ATLANTIC CITY								GUST FACTOR 1.00				
		CONFIGURATION A								REFERENCE PRESSURE 30.0 PSF				
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33									8.8	1115.0	-78.5	.6	-4.3
26TH	278.16	.6	70.0	1005	2827	.6	24.7	-3	0	8.2	1045.0	-69.0	.5	-4.1
27TH	288.66	.6	84.1	1194	3360	.5	25.0	-3	0	7.6	960.9	-58.5	.4	-3.8
28TH	297.49	.5	71.6	1005	2827	.5	25.3	-4	0	7.1	889.4	-50.3	.3	-3.5
29TH	306.33	.8	71.4	1005	2827	.7	25.3	-2	0	6.3	818.0	-42.7	.3	-3.4
30TH	315.16	.7	71.1	1005	2827	.7	25.2	-2	0	5.6	746.9	-35.8	.2	-3.3
31ST	323.99	.7	70.8	1005	2827	.7	25.0	-2	0	4.9	676.1	-29.5	.2	-3.1
32ND	332.82	.7	70.5	1005	2827	.7	24.9	-3	0	4.3	605.6	-23.9	.1	-2.9
33RD	341.66	.6	70.2	1005	2827	.6	24.8	-3	0	3.6	535.3	-18.8	.1	-2.6
34TH	350.49	.6	69.9	1005	2827	.6	24.7	-4	0	3.0	465.4	-14.4	.1	-2.4
35TH	359.32	.6	69.7	1005	2827	.6	24.6	-4	0	2.4	395.7	-10.6	.1	-2.1
36TH	368.16	.5	69.4	1005	2827	.5	24.5	-5	0	1.9	326.4	-7.4	.0	-1.8
37TH	376.99	.5	69.1	1005	2827	.5	24.4	-5	0	1.4	257.3	-4.9	.0	-1.5
38TH	385.82	.5	68.8	1005	2827	.5	24.3	-5	0	.9	188.5	-2.9	.0	-1.1
ROOF	401.49	.7	109.5	1782	5013	.4	21.8	-4	0	.2	78.9	-.8	.0	-.6
TOP	421.50	.2	79.0	2276	4508	.1	17.5	-8	0	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 80 CONFIGURATION A

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00	-2.2	-2.6	79	222	-28.4	-11.8	-357	305	-113.1	2978.3	-700.3	-20.3	-16.4
1ST	54.00	-9.4	89.7	1194	3360	-7.9	26.7	2	0	-110.8	2980.9	-539.4	-14.3	-18.0
2ND	64.50	-7.1	74.7	1005	2827	-7.0	26.4	1	0	-101.4	2891.1	-508.6	-13.2	-18.2
3RD	73.33	-6.4	73.9	1005	2827	-6.4	26.2	0	0	-94.3	2816.4	-483.4	-12.3	-18.3
4TH	82.17	-5.8	73.1	1005	2827	-5.8	25.9	0	0	-87.9	2742.5	-458.8	-11.5	-18.3
5TH	91.00	-5.2	72.3	1005	2827	-5.1	25.6	-1	0	-82.1	2669.4	-434.9	-10.8	-18.3
6TH	99.83	-4.5	71.5	1005	2827	-4.5	25.3	-2	0	-76.9	2597.1	-411.7	-10.1	-18.2
7TH	108.67	-3.9	70.7	1005	2827	-3.9	25.0	-3	0	-72.4	2525.6	-389.0	-9.4	-18.0
8TH	117.50	-3.2	69.9	1005	2827	-3.2	24.7	-4	0	-68.5	2454.8	-367.1	-8.8	-17.8
9TH	126.33	-2.6	69.1	1005	2827	-2.6	24.5	-5	0	-65.3	2384.9	-345.7	-8.2	-17.5
10TH	135.16	-1.9	68.1	1005	2827	-1.9	24.1	-6	0	-62.7	2315.8	-324.9	-7.6	-17.2
11TH	144.00	-1.6	67.9	1005	2827	-1.6	24.0	-5	0	-60.8	2247.7	-304.8	-7.1	-16.8
12TH	152.83	-1.8	68.6	1005	2827	-1.8	24.3	-5	0	-59.2	2179.9	-285.2	-6.5	-16.5
13TH	161.66	-2.3	82.5	1194	3360	-1.9	24.6	-6	0	-57.4	2111.3	-266.3	-6.0	-16.1
14TH	172.16	-2.1	70.2	1005	2827	-2.1	24.8	-6	0	-55.1	2028.8	-244.5	-5.4	-15.6
15TH	181.00	-2.3	70.9	1005	2827	-2.2	25.1	-7	0	-53.0	1958.6	-226.9	-5.0	-15.2
16TH	189.83	-2.3	71.7	1005	2827	-2.4	25.3	-7	0	-50.7	1887.7	-209.9	-4.5	-14.7
17TH	198.66	-2.4	71.7	1005	2827	-2.4	25.3	-7	0	-48.3	1816.0	-193.6	-4.1	-14.2
18TH	207.50	-2.6	72.4	1005	2827	-2.5	25.6	-8	0	-45.7	1743.6	-177.8	-3.7	-13.7
19TH	216.33	-2.7	73.1	1005	2827	-2.7	25.9	-8	0	-43.0	1670.5	-162.8	-3.3	-13.1
20TH	225.16	-2.6	73.0	1005	2827	-2.6	25.8	-7	0	-40.4	1597.5	-148.3	-2.9	-12.6
21ST	233.99	-2.6	73.5	1005	2827	-2.6	26.0	-6	0	-37.8	1524.0	-134.5	-2.6	-12.1
22ND	242.83	-2.6	74.2	1005	2827	-2.6	26.3	-6	0	-35.2	1449.7	-121.4	-2.2	-11.7
23RD	251.66	-2.6	74.9	1005	2827	-2.6	26.5	-7	0	-32.6	1374.8	-108.9	-1.9	-11.2
24TH	260.49	-2.6	75.6	1005	2827	-2.6	26.8	-7	0	-29.9	1299.1	-97.1	-1.7	-10.7
		-2.6	76.4	1005	2827	-2.6	27.0	-7	0					

TABLE 7. SHEAR AND MOMENT DIAGRAMS :		RESORTS HOTEL CASINO, ATLANTIC CITY										GUST FACTOR 1.00		
WIND DIRECTION 80		CONFIGURATION A										REFERENCE PRESSURE 30.0 PSF		
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33	-2.6	77.1	1005	2827	-2.6	27.3	-7	-0	-27.3	1222.8	-86.0	-1.4	-10.1
26TH	278.16	-3.2	92.5	1194	3360	-2.6	27.5	-7	-0	-24.7	1145.7	-75.5	-1.2	-9.6
27TH	288.66	-2.7	78.6	1005	2827	-2.6	27.8	-7	-0	-21.5	1053.2	-64.0	-.9	-9.0
28TH	297.49	-2.4	78.1	1005	2827	-2.4	27.6	-5	-0	-18.9	974.6	-55.0	-.7	-8.4
29TH	306.33	-2.3	77.9	1005	2827	-2.2	27.6	-6	-0	-16.5	896.5	-46.8	-.6	-8.0
30TH	315.16	-2.2	77.6	1005	2827	-2.1	27.5	-6	-0	-14.2	818.6	-39.2	-.5	-7.5
31ST	323.99	-2.0	77.3	1005	2827	-2.0	27.4	-7	-0	-12.1	741.0	-32.3	-.3	-7.0
32ND	332.82	-1.9	77.1	1005	2827	-1.9	27.3	-8	-0	-10.0	663.6	-26.1	-.2	-6.5
33RD	341.66	-1.8	76.8	1005	2827	-1.8	27.2	-8	-0	-8.1	586.6	-20.6	-.2	-5.9
34TH	350.49	-1.7	76.6	1005	2827	-1.7	27.1	-9	-0	-6.3	509.7	-15.7	-.1	-5.3
35TH	359.32	-1.6	76.3	1005	2827	-1.6	27.0	-10	-0	-4.6	433.2	-11.6	-.1	-4.6
36TH	368.16	-1.5	76.0	1005	2827	-1.5	26.9	-10	-0	-3.0	356.9	-8.1	-.0	-3.8
37TH	376.99	-1.4	75.8	1005	2827	-1.4	26.8	-11	-0	-1.5	280.9	-5.3	-.0	-3.1
38TH	385.82	-.5	120.3	1782	5013	-.3	24.0	-11	-0	-.1	205.1	-3.1	.0	-2.2
ROOF	401.49	.4	84.8	2276	4508	.2	18.8	-11	0	.4	84.8	-.8	.0	-.9
TOP	421.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 90

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00									33.0	2817.0	-659.5	15.3	-37.7
1ST	54.00	-2.0	-2.1	79	222	-25.3	-9.6	-378	355	35.0	2819.1	-507.3	13.5	-39.2
2ND	64.50	-5.7	84.4	1194	3360	-4.8	25.1	-2	-0	40.7	2734.7	-478.2	13.1	-39.1
3RD	73.33	-3.9	70.5	1005	2827	-3.9	24.9	-3	-0	44.6	2664.3	-454.3	12.7	-38.8
4TH	82.17	-3.4	69.9	1005	2827	-3.4	24.7	-5	-0	48.0	2594.4	-431.1	12.3	-38.5
5TH	91.00	-2.8	69.3	1005	2827	-2.8	24.5	-6	-0	50.8	2525.1	-408.5	11.8	-38.1
6TH	99.83	-2.2	68.7	1005	2827	-2.2	24.3	-8	-0	53.0	2456.4	-386.5	11.4	-37.6
7TH	108.67	-1.7	68.1	1005	2827	-1.6	24.1	-9	-0	54.7	2388.2	-365.1	10.9	-37.0
8TH	117.50	-1.1	67.5	1005	2827	-1.1	23.9	-10	-0	55.8	2320.7	-344.3	10.4	-36.2
9TH	126.33	-.5	67.0	1005	2827	-.5	23.7	-12	-0	56.3	2253.7	-324.1	9.9	-35.4
10TH	135.16	.1	66.4	1005	2827	.1	23.5	-13	0	56.2	2187.3	-304.5	9.4	-34.6
11TH	144.00	.8	65.7	1005	2827	.8	23.2	-15	0	55.4	2121.7	-285.4	8.9	-33.6
12TH	152.83	1.1	65.6	1005	2827	1.1	23.2	-14	0	54.3	2056.1	-267.0	8.4	-32.7
13TH	161.66	1.1	66.1	1005	2827	1.1	23.4	-14	0	53.2	1989.9	-249.1	8.0	-31.7
14TH	172.16	1.3	79.3	1194	3360	1.1	23.6	-15	0	51.8	1910.6	-228.6	7.4	-30.5
15TH	181.00	1.1	67.3	1005	2827	1.1	23.8	-15	0	50.7	1843.3	-212.1	7.0	-29.5
16TH	189.83	1.1	67.8	1005	2827	1.1	24.0	-15	0	49.6	1775.5	-196.1	6.5	-28.5
17TH	198.66	1.1	68.4	1005	2827	1.1	24.2	-15	0	48.5	1707.1	-180.7	6.1	-27.5
18TH	207.50	1.1	68.9	1005	2827	1.1	24.4	-16	0	47.4	1638.2	-165.9	5.7	-26.4
19TH	216.33	1.1	69.4	1005	2827	1.1	24.6	-16	0	46.3	1568.8	-151.8	5.3	-25.3
20TH	225.16	1.3	69.4	1005	2827	1.3	24.6	-15	0	45.0	1499.4	-138.2	4.9	-24.2
21ST	233.99	1.4	69.9	1005	2827	1.4	24.7	-15	0	43.6	1429.5	-125.3	4.5	-23.2
22ND	242.83	1.4	70.5	1005	2827	1.4	24.9	-15	0	42.2	1359.0	-113.0	4.1	-22.1
23RD	251.66	1.5	71.1	1005	2827	1.5	25.1	-15	0	40.8	1288.0	-101.3	3.7	-21.0
24TH	260.49	1.5	71.6	1005	2827	1.5	25.3	-15	0	39.3	1216.3	-90.2	3.4	-20.0
		1.5	72.2	1005	2827	1.5	25.5	-15	0					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : RESORTS HOTEL CASINO, ATLANTIC CITY														
WIND DIRECTION 90		CONFIGURATION A								REFERENCE PRESSURE 30.0 PSF		GUST FACTOR 1.00		
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33									37.7	1144.1	-79.8	3.0	-18.9
26TH	278.16	1.6	72.8	1005	2827	1.6	25.8	-15	0	36.1	1071.3	-70.0	2.7	-17.8
27TH	288.66	1.9	87.3	1194	3360	1.6	26.0	-15	0	34.2	984.0	-59.2	2.3	-16.5
28TH	297.49	1.7	74.1	1005	2827	1.7	26.2	-15	0	32.5	909.9	-50.9	2.0	-15.3
29TH	306.33	1.9	73.7	1005	2827	1.9	26.1	-14	0	30.6	836.2	-43.1	1.8	-14.3
30TH	315.16	2.0	73.5	1005	2827	2.0	26.0	-14	0	28.6	762.7	-36.1	1.5	-13.3
31ST	323.99	2.1	73.2	1005	2827	2.1	25.9	-15	0	26.5	689.5	-29.7	1.2	-12.2
32ND	332.82	2.2	73.0	1005	2827	2.2	25.8	-16	0	24.3	616.5	-23.9	1.0	-11.1
33RD	341.66	2.3	72.8	1005	2827	2.2	25.7	-16	1	22.0	543.7	-18.8	.8	-9.9
34TH	350.49	2.3	72.5	1005	2827	2.3	25.7	-17	1	19.7	471.2	-14.3	.6	-8.7
35TH	359.32	2.4	72.3	1005	2827	2.4	25.6	-18	1	17.3	398.9	-10.4	.5	-7.4
36TH	368.16	2.5	72.0	1005	2827	2.5	25.5	-18	1	14.8	326.9	-7.2	.3	-6.1
37TH	376.99	2.6	71.8	1005	2827	2.6	25.4	-19	1	12.2	255.1	-4.7	.2	-4.7
38TH	385.82	2.7	71.6	1005	2827	2.7	25.3	-20	1	9.5	183.5	-2.7	.1	-3.3
ROOF	401.49	7.3	110.9	1782	5013	4.1	22.1	-20	1	2.3	72.6	-.7	.0	-1.1
TOP	421.50	2.3	72.6	2276	4508	1.0	16.1	-15	0	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 100

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00									248.5	2656.6	-614.1	67.4	-56.1
1ST	54.00	-1.7	1.3	79	222	-21.2	5.7	290	371	250.1	2655.3	-470.7	54.0	-57.0
2ND	64.50	-.9	81.0	1194	3360	-.7	24.1	-10	-0	251.0	2574.3	-443.2	51.4	-56.2
3RD	73.33	.2	67.8	1005	2827	.2	24.0	-11	0	250.8	2506.5	-420.8	49.1	-55.5
4TH	82.17	.9	67.4	1005	2827	.9	23.8	-12	0	249.9	2439.1	-398.9	46.9	-54.7
5TH	91.00	1.6	66.9	1005	2827	1.6	23.7	-13	0	248.4	2372.2	-377.7	44.7	-53.8
6TH	99.83	2.2	66.5	1005	2827	2.2	23.5	-15	0	246.1	2305.7	-357.0	42.5	-52.8
7TH	108.67	2.9	66.0	1005	2827	2.9	23.4	-16	1	243.2	2239.7	-336.9	40.4	-51.8
8TH	117.50	3.6	65.6	1005	2827	3.6	23.2	-17	1	239.6	2174.1	-317.4	38.2	-50.6
9TH	126.33	4.3	65.1	1005	2827	4.2	23.0	-18	1	235.4	2109.0	-298.5	36.1	-49.5
10TH	135.16	4.9	64.7	1005	2827	4.9	22.9	-19	1	230.4	2044.3	-280.2	34.1	-48.2
11TH	144.00	5.7	64.1	1005	2827	5.7	22.7	-20	2	224.7	1980.2	-262.4	32.1	-46.9
12TH	152.83	6.0	63.9	1005	2827	6.0	22.6	-21	2	218.7	1916.3	-245.2	30.1	-45.5
13TH	161.66	6.1	64.2	1005	2827	6.0	22.7	-21	2	212.6	1852.1	-228.6	28.2	-44.2
14TH	172.16	7.3	76.8	1194	3360	6.1	22.8	-21	2	205.4	1775.3	-209.5	26.0	-42.5
15TH	181.00	6.2	64.9	1005	2827	6.1	23.0	-22	2	199.2	1710.4	-194.1	24.2	-41.1
16TH	189.83	6.2	65.2	1005	2827	6.2	23.1	-22	2	193.0	1645.2	-179.3	22.5	-39.6
17TH	198.66	6.2	65.5	1005	2827	6.2	23.2	-23	2	186.8	1579.7	-165.0	20.8	-38.2
18TH	207.50	6.3	65.8	1005	2827	6.2	23.3	-23	2	180.5	1513.9	-151.4	19.2	-36.6
19TH	216.33	6.3	66.1	1005	2827	6.3	23.4	-23	2	174.2	1447.8	-138.3	17.6	-35.1
20TH	225.16	6.5	66.0	1005	2827	6.5	23.4	-23	2	167.7	1381.8	-125.8	16.1	-33.5
21ST	233.99	6.8	66.2	1005	2827	6.7	23.4	-23	2	160.9	1315.6	-113.9	14.7	-32.0
22ND	242.83	6.9	66.6	1005	2827	6.9	23.6	-23	2	154.0	1249.0	-102.6	13.3	-30.4
23RD	251.66	7.1	66.9	1005	2827	7.1	23.7	-23	2	146.9	1182.1	-91.8	12.0	-28.9
24TH	260.49	7.3	67.2	1005	2827	7.3	23.8	-23	2	139.6	1114.8	-81.7	10.7	-27.3
		7.5	67.6	1005	2827	7.4	23.9	-23	3					

TABLE 7. SHEAR AND MOMENT DIAGRAMS 1		RESORTS HOTEL CASINO, ATLANTIC CITY								GUST FACTOR 1.00				
WIND DIRECTION 100		CONFIGURATION A				REFERENCE PRESSURE 30.0 PSF								
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33	7.6	67.9	1005	2827	7.6	24.0	-23	3	132.1	1047.3	-72.1	9.5	-25.8
26TH	278.16	9.3	81.1	1194	3360	7.8	24.2	-23	3	124.5	979.4	-63.2	8.4	-24.2
27TH	288.66	8.0	68.6	1005	2827	8.0	24.3	-23	3	115.2	898.2	-53.3	7.1	-22.3
28TH	297.49	8.4	68.4	1005	2827	8.4	24.2	-22	3	107.1	829.6	-45.7	6.1	-20.8
29TH	306.33	8.4	68.1	1005	2827	8.4	24.1	-23	3	98.7	761.2	-38.7	5.2	-19.2
30TH	315.16	8.4	67.9	1005	2827	8.3	24.0	-23	3	90.3	693.0	-32.3	4.4	-17.7
31ST	323.99	8.3	67.6	1005	2827	8.3	23.9	-24	3	81.9	625.2	-26.4	3.6	-16.1
32ND	332.82	8.3	67.3	1005	2827	8.3	23.8	-24	3	73.6	557.6	-21.2	2.9	-14.5
33RD	341.66	8.3	67.0	1005	2827	8.2	23.7	-25	3	65.3	490.3	-16.6	2.3	-12.8
34TH	350.49	8.2	66.7	1005	2827	8.2	23.6	-25	3	57.0	423.3	-12.5	1.8	-11.1
35TH	359.32	8.2	66.5	1005	2827	8.1	23.5	-26	3	48.8	356.5	-9.1	1.3	-9.4
36TH	368.16	8.1	66.2	1005	2827	8.1	23.4	-26	3	40.6	290.1	-6.2	.9	-7.7
37TH	376.99	8.1	65.9	1005	2827	8.1	23.3	-27	3	32.5	223.9	-4.0	.6	-5.9
38TH	385.82	16.3	99.0	1782	5013	9.2	19.7	-28	5	24.4	158.0	-2.3	.3	-4.1
ROOF	401.49	8.1	59.0	2276	4508	3.5	13.1	-22	3	8.1	59.0	-.6	.1	-1.3
TOP	421.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 110 CONFIGURATION A

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCHN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00	-1.4	4.2	79	222	-17.5	18.9	119	39	463.6	2626.8	-599.1	123.1	-73.2
1ST	54.00	2.9	83.2	1194	3360	2.4	24.7	-17	1	465.0	2622.7	-457.4	98.0	-73.7
2ND	64.50	3.4	69.4	1005	2827	3.4	24.6	-18	1	462.1	2539.5	-430.3	93.1	-72.3
3RD	73.33	4.2	68.8	1005	2827	4.1	24.3	-20	1	458.7	2470.1	-408.2	89.1	-71.0
4TH	82.17	4.9	68.2	1005	2827	4.9	24.1	-21	1	454.5	2401.3	-386.6	85.0	-69.7
5TH	91.00	5.6	67.6	1005	2827	5.6	23.9	-22	2	449.6	2333.1	-365.7	81.0	-68.3
6TH	99.83	6.3	67.0	1005	2827	6.3	23.7	-23	2	444.0	2265.4	-345.4	77.1	-66.8
7TH	108.67	7.1	66.4	1005	2827	7.0	23.5	-24	3	437.7	2198.4	-325.7	73.2	-65.2
8TH	117.50	7.8	65.8	1005	2827	7.7	23.3	-25	3	430.6	2132.0	-306.6	69.4	-63.6
9TH	126.33	8.5	65.3	1005	2827	8.5	23.1	-27	3	422.9	2066.1	-288.0	65.6	-61.9
10TH	135.16	9.3	64.6	1005	2827	9.2	22.9	-28	4	414.4	2000.9	-270.1	61.9	-60.1
11TH	144.00	9.8	64.6	1005	2827	9.7	22.9	-28	4	405.1	1936.2	-252.7	58.3	-58.3
12TH	152.83	10.0	64.8	1005	2827	10.0	22.9	-28	4	395.3	1871.6	-235.9	54.7	-56.4
13TH	161.66	12.3	77.2	1194	3360	10.3	23.0	-28	4	385.3	1806.8	-219.6	51.3	-54.6
14TH	172.16	10.6	65.2	1005	2827	10.6	23.1	-28	5	373.1	1729.6	-201.1	47.3	-52.4
15TH	181.00	10.9	65.4	1005	2827	10.8	23.1	-28	5	362.4	1664.4	-186.1	44.1	-50.5
16TH	189.83	11.2	65.5	1005	2827	11.1	23.2	-27	5	351.5	1599.0	-171.7	40.9	-48.7
17TH	198.66	11.4	65.7	1005	2827	11.4	23.3	-27	5	340.4	1533.5	-157.8	37.8	-46.8
18TH	207.50	11.7	65.9	1005	2827	11.6	23.3	-27	5	329.0	1467.8	-144.6	34.9	-45.0
19TH	216.33	12.1	65.9	1005	2827	12.0	23.3	-27	5	317.3	1401.9	-131.9	32.0	-43.1
20TH	225.16	12.4	66.0	1005	2827	12.4	23.3	-27	5	305.2	1336.0	-119.8	29.3	-41.3
21ST	233.99	12.7	66.1	1005	2827	12.7	23.4	-27	5	292.8	1270.1	-108.3	26.6	-39.4
22ND	242.83	13.1	66.2	1005	2827	13.0	23.4	-27	5	280.0	1204.0	-97.4	24.1	-37.5
23RD	251.66	13.4	66.4	1005	2827	13.3	23.5	-27	5	267.0	1137.7	-87.0	21.7	-35.7
24TH	260.49	13.7	66.5	1005	2827	13.7	23.5	-27	6	253.6	1071.4	-77.3	19.4	-33.8

TABLE 7. SHEAR AND MOMENT DIAGRAMS :														
WIND DIRECTION 110		RESORTS HOTEL CASINO, ATLANTIC CITY								GUST FACTOR 1.00				
		CONFIGURATION A								REFERENCE PRESSURE 30.0 PSF				
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33									239.8	1004.9	-68.1	17.2	-31.9
26TH	278.16	14.1	66.7	1005	2827	14.0	23.6	-27	6	225.8	938.2	-59.5	15.2	-30.0
27TH	288.66	17.1	79.4	1194	3360	14.3	23.6	-27	6	208.7	858.8	-50.1	12.9	-27.8
28TH	297.49	14.8	67.0	1005	2827	14.7	23.7	-27	6	193.9	791.8	-42.8	11.1	-25.9
29TH	306.33	15.2	66.9	1005	2827	15.1	23.7	-27	6	178.7	724.9	-36.1	9.5	-24.0
30TH	315.16	15.2	66.5	1005	2827	15.1	23.5	-28	6	163.5	658.4	-30.0	7.9	-22.0
31ST	323.99	15.1	66.2	1005	2827	15.0	23.4	-28	6	148.4	592.3	-24.5	6.6	-20.0
32ND	332.82	15.1	65.8	1005	2827	15.0	23.3	-29	7	133.4	526.5	-19.5	5.3	-18.0
33RD	341.66	15.0	65.4	1005	2827	14.9	23.2	-30	7	118.4	461.0	-15.2	4.2	-16.0
34TH	350.49	14.9	65.1	1005	2827	14.9	23.0	-30	7	103.4	395.9	-11.4	3.2	-13.9
35TH	359.32	14.9	64.7	1005	2827	14.8	22.9	-31	7	88.5	331.2	-8.2	2.4	-11.8
36TH	368.16	14.8	64.4	1005	2827	14.8	22.8	-32	7	73.7	266.9	-5.5	1.7	-9.7
37TH	376.99	14.8	64.0	1005	2827	14.7	22.6	-32	7	58.9	202.9	-3.4	1.1	-7.5
38TH	385.82	14.7	63.6	1005	2827	14.6	22.5	-33	8	44.2	139.2	-1.9	.6	-5.3
ROOF	401.49	28.3	91.9	1782	5013	15.9	18.3	-36	11	16.0	47.3	-.5	.2	-1.6
TOP	421.50	16.0	47.3	2276	4508	7.0	10.5	-31	11	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : RESORTS HOTEL CASINO, ATLANTIC CITY
WIND DIRECTION 120 CONFIGURATION A REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00									512.9	2282.9	-515.0	132.4	-80.6
1ST	54.00	-1.0	5.6	79	222	-13.1	25.5	30	6	513.9	2277.2	-391.8	104.7	-80.7
2ND	64.50	5.0	74.3	1194	3360	4.1	22.1	-24	2	509.0	2203.0	-368.3	99.3	-78.9
3RD	73.33	5.2	61.8	1005	2827	5.1	21.9	-25	2	503.8	2141.1	-349.1	94.9	-77.4
4TH	82.17	5.9	61.3	1005	2827	5.9	21.7	-26	2	497.9	2079.8	-330.5	90.4	-75.8
5TH	91.00	6.6	60.8	1005	2827	6.6	21.5	-27	3	491.3	2019.0	-312.4	86.1	-74.1
6TH	99.83	7.3	60.3	1005	2827	7.3	21.3	-28	3	484.0	1958.7	-294.8	81.8	-72.4
7TH	108.67	8.1	59.8	1005	2827	8.0	21.1	-29	4	475.9	1899.0	-277.8	77.5	-70.6
8TH	117.50	8.8	59.3	1005	2827	8.8	21.0	-30	4	467.1	1839.7	-261.3	73.4	-68.8
9TH	126.33	9.5	58.7	1005	2827	9.5	20.8	-31	5	457.6	1781.0	-245.3	69.3	-67.0
10TH	135.16	10.3	58.2	1005	2827	10.2	20.6	-32	6	447.3	1722.7	-229.8	65.3	-65.1
11TH	144.00	11.0	57.8	1005	2827	11.0	20.5	-33	6	436.2	1664.9	-214.8	61.4	-63.1
12TH	152.83	11.5	58.0	1005	2827	11.4	20.5	-33	7	424.8	1606.9	-200.4	57.6	-61.1
13TH	161.66	11.7	57.9	1005	2827	11.7	20.5	-33	7	413.1	1549.0	-186.5	53.9	-59.1
14TH	172.16	14.2	68.7	1194	3360	11.9	20.5	-33	7	398.8	1480.3	-170.5	49.6	-56.7
15TH	181.00	12.2	57.8	1005	2827	12.2	20.4	-33	7	386.6	1422.5	-157.7	46.1	-54.7
16TH	189.83	12.5	57.7	1005	2827	12.4	20.4	-33	7	374.1	1364.8	-145.4	42.8	-52.7
17TH	198.66	12.7	57.6	1005	2827	12.6	20.4	-33	7	361.4	1307.2	-133.6	39.5	-50.7
18TH	207.50	12.9	57.6	1005	2827	12.9	20.4	-33	7	348.5	1249.6	-122.3	36.4	-48.7
19TH	216.33	13.2	57.5	1005	2827	13.1	20.3	-33	8	335.3	1192.1	-111.5	33.4	-46.7
20TH	225.16	13.5	57.8	1005	2827	13.4	20.4	-34	8	321.8	1134.3	-101.3	30.5	-44.7
21ST	233.99	13.7	57.7	1005	2827	13.7	20.4	-34	8	308.1	1076.6	-91.5	27.7	-42.6
22ND	242.83	14.0	57.5	1005	2827	13.9	20.3	-34	8	294.1	1019.2	-82.2	25.0	-40.6
23RD	251.66	14.3	57.3	1005	2827	14.2	20.3	-34	8	279.8	961.9	-73.5	22.5	-38.5
24TH	260.49	14.5	57.1	1005	2827	14.5	20.2	-34	9	265.3	904.8	-65.3	20.1	-36.5
		14.8	56.9	1005	2827	14.7	20.1	-33	9					

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 120

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33	15.0	56.7	1005	2827	15.0	20.0	-33	9	250.5	848.0	-57.5	17.8	-34.4
26TH	278.16	18.2	67.1	1194	3360	15.2	20.0	-33	9	235.4	791.3	-50.3	15.7	-32.4
27TH	288.66	15.6	56.2	1005	2827	15.5	19.9	-33	9	217.2	724.2	-42.3	13.3	-30.0
28TH	297.49	15.9	56.4	1005	2827	15.8	19.9	-34	10	201.6	668.0	-36.2	11.4	-28.0
29TH	306.33	15.8	56.1	1005	2827	15.8	19.8	-35	10	185.8	611.6	-30.5	9.7	-25.9
30TH	315.16	15.8	55.7	1005	2827	15.7	19.7	-36	10	169.9	555.5	-25.4	8.2	-23.8
31ST	323.99	15.8	55.4	1005	2827	15.7	19.6	-36	10	154.1	499.8	-20.7	6.7	-21.7
32ND	332.82	15.8	55.1	1005	2827	15.7	19.5	-37	11	138.3	444.4	-16.5	5.4	-19.5
33RD	341.66	15.7	54.8	1005	2827	15.7	19.4	-38	11	122.5	389.3	-12.8	4.3	-17.3
34TH	350.49	15.7	54.5	1005	2827	15.6	19.3	-38	11	106.8	334.5	-9.7	3.3	-15.0
35TH	359.32	15.7	54.1	1005	2827	15.6	19.2	-39	11	91.1	280.1	-6.9	2.4	-12.8
36TH	368.16	15.7	53.8	1005	2827	15.6	19.0	-40	12	75.4	225.9	-4.7	1.7	-10.5
37TH	376.99	15.6	53.5	1005	2827	15.6	18.9	-41	12	59.7	172.1	-2.9	1.1	-8.1
38TH	385.82	29.6	77.6	1782	5013	16.6	15.5	-45	17	44.1	118.6	-1.7	.6	-5.8
ROOF	401.49	14.5	41.0	2276	4508	6.4	9.1	-38	13	14.5	41.0	-.4	.1	-1.7
TOP	421.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS
WIND DIRECTION 130

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00	-4.4	4.7	79	222	-4.7	21.2	-21	-2	423.2	1942.4	-445.1	109.9	-84.7
1ST	54.00	4.6	57.5	1194	3360	3.8	17.1	-42	3	423.6	1937.7	-340.4	87.0	-84.6
2ND	64.50	4.6	48.5	1005	2827	4.6	17.2	-42	4	419.0	1880.2	-320.3	82.6	-82.2
3RD	73.33	5.1	48.7	1005	2827	5.0	17.2	-41	4	414.5	1831.7	-303.9	78.9	-80.1
4TH	82.17	5.6	48.9	1005	2827	5.5	17.3	-41	5	409.4	1783.0	-287.9	75.3	-78.1
5TH	91.00	6.1	49.1	1005	2827	6.0	17.4	-40	5	403.8	1734.1	-272.4	71.7	-76.1
6TH	99.83	6.6	49.3	1005	2827	6.5	17.4	-40	5	397.8	1685.0	-257.3	68.1	-74.1
7TH	108.67	7.1	49.5	1005	2827	7.0	17.5	-40	6	391.2	1635.8	-242.6	64.7	-72.1
8TH	117.50	7.6	49.7	1005	2827	7.5	17.6	-39	6	384.1	1586.3	-228.4	61.2	-70.0
9TH	126.33	8.1	49.9	1005	2827	8.0	17.6	-39	6	376.6	1536.6	-214.6	57.9	-68.1
10TH	135.16	8.6	50.3	1005	2827	8.5	17.8	-39	7	368.5	1486.8	-201.3	54.6	-66.1
11TH	144.00	8.9	50.5	1005	2827	8.8	17.9	-40	7	360.0	1436.5	-188.4	51.4	-64.0
12TH	152.83	9.1	50.1	1005	2827	9.1	17.7	-40	7	351.1	1386.0	-175.9	48.2	-61.9
13TH	161.66	11.1	59.1	1194	3360	9.3	17.6	-40	8	342.0	1335.9	-163.9	45.2	-59.9
14TH	172.16	9.6	49.3	1005	2827	9.6	17.4	-40	8	330.9	1276.7	-150.2	41.6	-57.4
15TH	181.00	9.8	48.9	1005	2827	9.8	17.3	-40	8	321.3	1227.4	-139.1	38.7	-55.4
16TH	189.83	10.1	48.6	1005	2827	10.0	17.2	-40	8	311.4	1178.5	-128.5	36.0	-53.3
17TH	198.66	10.3	48.2	1005	2827	10.3	17.0	-40	8	301.4	1129.9	-118.3	33.2	-51.3
18TH	207.50	10.5	47.8	1005	2827	10.5	16.9	-39	9	291.1	1081.7	-108.5	30.6	-49.3
19TH	216.33	10.7	48.3	1005	2827	10.7	17.1	-42	9	280.5	1033.9	-99.2	28.1	-47.3
20TH	225.16	11.0	48.3	1005	2827	11.0	17.1	-42	10	269.8	985.7	-90.2	25.7	-45.2
21ST	233.99	11.4	48.1	1005	2827	11.3	17.0	-41	10	258.8	937.4	-81.8	23.3	-43.1
22ND	242.83	11.7	48.0	1005	2827	11.6	17.0	-41	10	247.4	889.3	-73.7	21.1	-41.0
23RD	251.66	12.0	47.8	1005	2827	12.0	16.9	-41	10	235.7	841.3	-66.0	19.0	-38.9
24TH	260.49	12.4	47.7	1005	2827	12.3	16.9	-40	10	223.7	793.5	-58.8	16.9	-36.9

TABLE 7. SHEAR AND MOMENT DIAGRAMS :		RESORTS HOTEL CASINO, ATLANTIC CITY								GUST FACTOR 1.00				
WIND DIRECTION 130		CONFIGURATION A				REFERENCE PRESSURE 30.0 PSF								
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33									211.3	745.8	-52.0	15.0	-34.8
26TH	278.16	12.7	47.5	1005	2827	12.6	16.8	-40	11	198.6	698.2	-45.6	13.2	-32.8
27TH	288.66	15.5	56.3	1194	3360	13.0	16.8	-40	11	183.0	641.9	-38.6	11.2	-30.4
28TH	297.49	13.4	47.2	1005	2827	13.4	16.7	-39	11	169.6	594.7	-33.1	9.7	-28.4
29TH	306.33	13.6	48.0	1005	2827	13.5	17.0	-42	12	156.0	546.7	-28.1	8.2	-26.2
30TH	315.16	13.5	48.0	1005	2827	13.4	17.0	-42	12	142.5	498.7	-23.5	6.9	-24.0
31ST	323.99	13.4	47.9	1005	2827	13.3	16.9	-43	12	129.1	450.8	-19.3	5.7	-21.8
32ND	332.82	13.3	47.8	1005	2827	13.2	16.9	-43	12	115.9	403.0	-15.5	4.6	-19.6
33RD	341.66	13.2	47.7	1005	2827	13.1	16.9	-44	12	102.7	355.3	-12.2	3.6	-17.4
34TH	350.49	13.1	47.6	1005	2827	13.0	16.9	-44	12	89.6	307.7	-9.2	2.8	-15.1
35TH	359.32	12.9	47.5	1005	2827	12.9	16.8	-45	12	76.7	260.2	-6.7	2.1	-12.9
36TH	368.16	12.8	47.5	1005	2827	12.8	16.8	-45	12	63.9	212.7	-4.7	1.4	-10.6
37TH	376.99	12.7	47.4	1005	2827	12.7	16.8	-46	12	51.1	165.3	-3.0	.9	-8.2
38TH	385.82	12.6	47.3	1005	2827	12.6	16.7	-46	12	38.5	118.0	-1.7	.5	-5.9
ROOF	401.49	25.1	72.7	1782	5013	14.1	14.5	-49	17	13.4	45.3	-.5	.1	-1.9
TOP	421.50	13.4	45.3	2276	4508	5.9	10.0	-39	11	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS
WIND DIRECTION 140

RESORTS HOTEL CASINO, ATLANTIC CITY
CONFIGURATION A
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00	.5	3.5	79	222	6.5	15.7	-84	12	414.0	1305.9	-301.1	103.3	-68.0
1ST	54.00	6.8	36.1	1194	3360	5.7	10.7	-66	12	413.5	1302.4	-230.7	81.0	-67.7
2ND	64.50	6.4	30.8	1005	2827	6.3	10.9	-62	13	406.7	1266.3	-217.2	76.7	-65.3
3RD	73.33	6.7	31.2	1005	2827	6.7	11.0	-60	13	400.4	1235.6	-206.1	73.1	-63.3
4TH	82.17	7.1	31.6	1005	2827	7.1	11.2	-58	13	393.6	1204.4	-195.4	69.6	-61.3
5TH	91.00	7.5	32.0	1005	2827	7.5	11.3	-56	13	386.5	1172.8	-184.9	66.2	-59.4
6TH	99.83	7.9	32.4	1005	2827	7.9	11.5	-54	13	379.0	1140.9	-174.6	62.8	-57.5
7TH	108.67	8.3	32.8	1005	2827	8.3	11.6	-52	13	371.0	1108.5	-164.7	59.5	-55.6
8TH	117.50	8.7	33.2	1005	2827	8.6	11.7	-50	13	362.8	1075.7	-155.1	56.2	-53.8
9TH	126.33	9.1	33.6	1005	2827	9.0	11.9	-48	13	354.1	1042.5	-145.7	53.1	-52.1
10TH	135.16	9.4	34.2	1005	2827	9.4	12.1	-47	13	345.0	1008.9	-136.6	50.0	-50.3
11TH	144.00	9.6	34.4	1005	2827	9.5	12.2	-47	13	335.5	974.7	-127.9	47.0	-48.6
12TH	152.83	9.7	34.2	1005	2827	9.6	12.1	-47	13	326.0	940.3	-119.4	44.1	-46.9
13TH	161.66	11.6	40.3	1194	3360	9.7	12.0	-46	13	316.3	906.1	-111.3	41.2	-45.1
14TH	172.16	9.9	33.6	1005	2827	9.9	11.9	-45	13	304.7	865.8	-102.0	38.0	-43.1
15TH	181.00	10.0	33.3	1005	2827	10.0	11.8	-44	13	294.8	832.2	-94.5	35.3	-41.5
16TH	189.83	10.1	33.1	1005	2827	10.1	11.7	-43	13	284.8	798.9	-87.3	32.8	-39.9
17TH	198.66	10.2	32.8	1005	2827	10.2	11.6	-42	13	274.7	765.8	-80.4	30.3	-38.3
18TH	207.50	10.3	32.6	1005	2827	10.3	11.5	-41	13	264.5	733.0	-73.7	27.9	-36.8
19TH	216.33	10.3	33.0	1005	2827	10.3	11.7	-43	13	254.1	700.4	-67.4	25.6	-35.4
20TH	225.16	10.4	32.9	1005	2827	10.3	11.6	-43	13	243.8	667.5	-61.4	23.4	-33.8
21ST	233.99	10.5	32.7	1005	2827	10.5	11.6	-42	14	233.4	634.5	-55.6	21.3	-32.3
22ND	242.83	10.6	32.6	1005	2827	10.6	11.5	-42	14	222.9	601.8	-50.2	19.3	-30.7
23RD	251.66	10.7	32.4	1005	2827	10.7	11.5	-42	14	212.3	569.2	-45.0	17.4	-29.2
24TH	260.49	10.8	32.2	1005	2827	10.8	11.4	-41	14	201.6	536.8	-40.1	15.5	-27.7

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 140
CONFIGURATION A

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33	11.0	32.0	1005	2827	10.9	11.3	-41	14	190.7	504.6	-35.5	13.8	-26.2
26TH	278.16	13.2	37.8	1194	3360	11.0	11.3	-41	14	179.8	472.6	-31.2	12.2	-24.8
27TH	288.66	11.2	31.6	1005	2827	11.2	11.2	-40	14	166.6	434.7	-26.4	10.4	-23.0
28TH	297.49	11.2	32.5	1005	2827	11.2	11.5	-44	15	155.4	403.1	-22.7	8.9	-21.6
29TH	306.33	11.4	32.3	1005	2827	11.4	11.4	-44	16	144.2	370.6	-19.3	7.6	-20.0
30TH	315.16	11.7	32.2	1005	2827	11.6	11.4	-45	16	132.8	338.3	-16.2	6.4	-18.4
31ST	323.99	11.9	32.1	1005	2827	11.8	11.4	-46	17	121.1	306.1	-13.3	5.3	-16.8
32ND	332.82	12.1	32.0	1005	2827	12.1	11.3	-46	18	109.2	274.0	-10.8	4.2	-15.1
33RD	341.66	12.4	31.8	1005	2827	12.3	11.3	-47	18	97.1	242.0	-8.5	3.3	-13.4
34TH	350.49	12.6	31.7	1005	2827	12.5	11.2	-47	19	84.7	210.2	-6.5	2.5	-11.7
35TH	359.32	12.8	31.6	1005	2827	12.8	11.2	-48	19	72.1	178.4	-4.8	1.8	-10.0
36TH	368.16	13.1	31.5	1005	2827	13.0	11.1	-48	20	59.3	146.9	-3.3	1.3	-8.2
37TH	376.99	13.3	31.3	1005	2827	13.2	11.1	-49	21	46.2	115.4	-2.2	.8	-6.4
38TH	385.82	22.6	48.3	1782	5013	12.7	9.6	-52	24	32.9	84.1	-1.3	.4	-4.6
ROOF	401.49	10.3	35.8	2276	4508	4.5	7.9	-39	11	10.3	35.8	-.4	.1	-1.5
TOP	421.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS
WIND DIRECTION 150

RESORTS HOTEL CASINO, ATLANTIC CITY
CONFIGURATION A
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00									346.5	169.8	-40.9	83.1	-9.6
1ST	54.00	.6	1.1	79	222	8.2	5.0	-101	59	345.8	168.7	-31.8	64.5	-9.4
2ND	64.50	6.9	2.4	1194	3360	5.7	.7	-23	65	339.0	166.3	-30.0	60.9	-8.9
3RD	73.33	6.3	2.2	1005	2827	6.3	.8	-20	55	332.7	164.1	-28.5	57.9	-8.5
4TH	82.17	6.7	2.5	1005	2827	6.7	.9	-19	50	326.0	161.6	-27.1	55.0	-8.1
5TH	91.00	7.1	2.8	1005	2827	7.0	1.0	-18	45	318.9	158.8	-25.7	52.1	-7.8
6TH	99.83	7.4	3.0	1005	2827	7.4	1.1	-17	41	311.5	155.7	-24.3	49.4	-7.4
7TH	108.67	7.8	3.3	1005	2827	7.8	1.2	-16	37	303.7	152.4	-22.9	46.6	-7.1
8TH	117.50	8.2	3.6	1005	2827	8.1	1.3	-15	34	295.5	148.9	-21.6	44.0	-6.7
9TH	126.33	8.5	3.8	1005	2827	8.5	1.4	-14	31	287.0	145.0	-20.3	41.4	-6.4
10TH	135.16	8.9	4.1	1005	2827	8.9	1.5	-13	28	278.1	140.9	-19.0	38.9	-6.1
11TH	144.00	9.2	4.4	1005	2827	9.2	1.6	-13	27	268.9	136.5	-17.8	36.5	-5.8
12TH	152.83	9.1	4.6	1005	2827	9.1	1.6	-14	28	259.8	131.9	-16.6	34.2	-5.5
13TH	161.66	9.0	4.6	1005	2827	8.9	1.6	-13	26	250.8	127.3	-15.5	31.9	-5.2
14TH	172.16	10.6	5.5	1194	3360	8.8	1.6	-13	25	240.2	121.8	-14.2	29.3	-4.9
15TH	181.00	8.8	4.7	1005	2827	8.7	1.7	-12	23	231.5	117.1	-13.1	27.3	-4.6
16TH	189.83	8.7	4.7	1005	2827	8.6	1.7	-12	22	222.8	112.4	-12.1	25.3	-4.4
17TH	198.66	8.6	4.7	1005	2827	8.5	1.7	-11	20	214.2	107.6	-11.1	23.3	-4.1
18TH	207.50	8.5	4.8	1005	2827	8.4	1.7	-11	19	205.8	102.9	-10.2	21.5	-3.9
19TH	207.50	8.4	4.8	1005	2827	8.3	1.7	-10	18	197.4	98.1	-9.3	19.7	-3.7
20TH	216.33	8.2	5.1	1005	2827	8.2	1.8	-13	20	189.2	92.9	-8.5	18.0	-3.5
21ST	225.16	8.3	5.1	1005	2827	8.2	1.8	-12	20	180.9	87.9	-7.7	16.3	-3.3
22ND	233.99	8.3	5.0	1005	2827	8.3	1.8	-11	19	172.6	82.9	-6.9	14.8	-3.1
23RD	242.83	8.4	4.8	1005	2827	8.4	1.7	-10	18	164.2	78.1	-6.2	13.3	-2.9
24TH	251.66	8.5	4.7	1005	2827	8.4	1.7	-9	17	155.7	73.4	-5.6	11.9	-2.7
	260.49	8.5	4.6	1005	2827	8.5	1.6	-8	15					

TABLE 7. SHEAR AND MOMENT DIAGRAMS :												RESORTS HOTEL CASINO, ATLANTIC CITY		
WIND DIRECTION 150		CONFIGURATION A				REFERENCE PRESSURE 30.0 PSF				GUST FACTOR 1.00				
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33									147.2	68.8	-4.9	10.5	-2.5
26TH	278.16	8.6	4.5	1005	2827	8.5	1.6	-7	14	138.6	64.3	-4.3	9.3	-2.4
27TH	288.66	10.3	5.1	1194	3360	8.6	1.5	-6	13	128.3	59.2	-3.7	7.9	-2.2
28TH	297.49	8.7	4.2	1005	2827	8.7	1.5	-5	11	119.6	55.0	-3.2	6.8	-2.1
29TH	306.33	8.6	4.4	1005	2827	8.6	1.6	-8	15	111.0	50.6	-2.7	5.8	-1.9
30TH	315.16	8.9	4.4	1005	2827	8.8	1.5	-7	15	102.1	46.2	-2.3	4.8	-1.7
31ST	323.99	9.1	4.3	1005	2827	9.0	1.5	-7	15	93.0	41.9	-1.9	4.0	-1.6
32ND	332.82	9.3	4.3	1005	2827	9.3	1.5	-6	14	83.7	37.7	-1.5	3.2	-1.4
33RD	341.66	9.5	4.2	1005	2827	9.5	1.5	-6	14	74.2	33.4	-1.2	2.5	-1.3
34TH	350.49	9.8	4.2	1005	2827	9.7	1.5	-6	13	64.4	29.3	-1.0	1.9	-1.1
35TH	359.32	10.0	4.1	1005	2827	9.9	1.5	-5	13	54.4	25.2	-.7	1.3	-1.0
36TH	368.16	10.2	4.1	1005	2827	10.1	1.4	-5	12	44.2	21.1	-.5	.9	-.8
37TH	376.99	10.4	4.0	1005	2827	10.4	1.4	-5	12	33.8	17.1	-.3	.6	-.7
38TH	385.82	10.6	4.0	1005	2827	10.6	1.4	-4	11	23.2	13.1	-.2	.3	-.5
ROOF	401.49	15.6	7.0	1782	5013	8.8	1.4	-8	17	7.5	6.1	-.1	.1	-.2
TOP	421.50	7.5	6.1	2276	4508	3.3	1.3	-14	18	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 160

RESORTS HOTEL CASINO, ATLANTIC CITY
CONFIGURATION A REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00									345.6	-633.8	141.6	83.3	37.1
1ST	54.00	.8	-1.6	79	222	10.0	-7.3	-109	-53	344.8	-632.2	107.4	64.7	36.9
2ND	64.50	7.2	-20.8	1194	3360	6.0	-6.2	-48	-16	337.6	-611.4	100.9	61.1	35.8
3RD	73.33	6.5	-17.5	1005	2827	6.4	-6.2	-49	-18	331.2	-593.9	95.6	58.1	34.8
4TH	82.17	6.8	-17.4	1005	2827	6.7	-6.2	-49	-19	324.4	-576.4	90.4	55.2	33.9
5TH	91.00	7.1	-17.4	1005	2827	7.0	-6.1	-50	-20	317.3	-559.1	85.4	52.4	32.8
6TH	99.83	7.4	-17.3	1005	2827	7.3	-6.1	-50	-21	310.0	-541.8	80.5	49.6	31.8
7TH	108.67	7.7	-17.2	1005	2827	7.6	-6.1	-51	-23	302.8	-524.6	75.8	46.9	30.8
8TH	117.50	8.0	-17.1	1005	2827	7.9	-6.1	-51	-24	294.3	-507.5	71.3	44.3	29.7
9TH	126.33	8.3	-17.0	1005	2827	8.2	-6.0	-51	-25	286.1	-490.4	66.9	41.7	28.6
10TH	135.16	8.6	-17.0	1005	2827	8.5	-6.0	-52	-26	277.5	-473.4	62.6	39.2	27.5
11TH	144.00	8.8	-16.9	1005	2827	8.7	-6.0	-52	-27	268.7	-456.5	58.5	36.8	26.4
12TH	152.83	8.7	-16.8	1005	2827	8.6	-6.0	-52	-27	260.1	-439.7	54.5	34.5	25.3
13TH	161.66	8.6	-16.7	1005	2827	8.6	-5.9	-50	-26	251.5	-423.0	50.7	32.2	24.2
14TH	172.16	10.2	-19.7	1194	3360	8.5	-5.9	-48	-25	241.3	-403.2	46.4	29.7	23.0
15TH	181.00	8.5	-16.5	1005	2827	8.5	-5.8	-46	-24	232.7	-386.7	42.9	27.6	22.1
16TH	189.83	8.5	-16.4	1005	2827	8.4	-5.8	-45	-23	224.2	-370.3	39.6	25.5	21.1
17TH	198.66	8.4	-16.3	1005	2827	8.4	-5.8	-43	-22	215.8	-354.1	36.4	23.6	20.3
18TH	207.50	8.4	-16.2	1005	2827	8.4	-5.7	-41	-21	207.4	-337.9	33.3	21.7	19.4
19TH	216.33	8.4	-16.0	1005	2827	8.3	-5.7	-39	-21	199.0	-321.9	30.4	19.9	18.6
20TH	225.16	8.2	-16.1	1005	2827	8.2	-5.7	-39	-20	190.8	-305.8	27.6	18.2	17.8
21ST	233.99	8.3	-16.0	1005	2827	8.2	-5.6	-39	-20	182.6	-289.8	25.0	16.6	17.0
22ND	242.83	8.3	-15.8	1005	2827	8.3	-5.6	-39	-21	174.3	-274.0	22.5	15.0	16.2
23RD	251.66	8.4	-15.6	1005	2827	8.3	-5.5	-40	-21	165.9	-258.4	20.1	13.5	15.4
24TH	260.49	8.4	-15.5	1005	2827	8.4	-5.5	-40	-22	157.5	-243.0	17.9	12.1	14.6
		8.5	-15.3	1005	2827	8.4	-5.4	-40	-22					

TABLE 7. SHEAR AND MOMENT DIAGRAMS :														
WIND DIRECTION 160		CONFIGURATION A		RESORTS HOTEL CASINO, ATLANTIC CITY						GUST FACTOR 1.00				
				REFERENCE PRESSURE 30.0 PSF										
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33									149.1	-227.7	15.9	10.7	13.8
26TH	278.16	8.5	-15.1	1005	2827	8.5	-5.4	-40	-22	140.5	-212.5	13.9	9.4	13.1
27TH	288.66	10.2	-17.8	1194	3360	8.5	-5.3	-40	-23	130.4	-194.8	11.8	8.0	12.1
28TH	297.49	8.6	-14.8	1005	2827	8.6	-5.2	-40	-23	121.8	-180.0	10.1	6.9	11.3
29TH	306.33	8.6	-14.8	1005	2827	8.6	-5.2	-42	-24	113.1	-165.2	8.6	5.8	10.5
30TH	315.16	8.9	-14.7	1005	2827	8.9	-5.2	-42	-26	104.3	-150.5	7.2	4.9	9.6
31ST	323.99	9.2	-14.6	1005	2827	9.1	-5.2	-42	-27	95.1	-135.9	5.9	4.0	8.8
32ND	332.82	9.5	-14.4	1005	2827	9.4	-5.1	-42	-28	85.6	-121.5	4.8	3.2	7.9
33RD	341.66	9.8	-14.3	1005	2827	9.7	-5.1	-43	-29	75.8	-107.2	3.8	2.5	7.0
34TH	350.49	10.0	-14.2	1005	2827	10.0	-5.0	-42	-30	65.8	-93.1	2.9	1.9	6.1
35TH	359.32	10.3	-14.0	1005	2827	10.3	-5.0	-42	-31	55.4	-79.0	2.1	1.3	5.2
36TH	368.16	10.6	-13.9	1005	2827	10.6	-4.9	-42	-32	44.8	-65.1	1.5	.9	4.2
37TH	376.99	10.9	-13.8	1005	2827	10.9	-4.9	-42	-33	33.9	-51.4	1.0	.5	3.3
38TH	385.82	11.2	-13.6	1005	2827	11.1	-4.8	-42	-35	22.7	-37.8	.6	.3	2.3
ROOF	401.49	16.1	-21.1	1782	5013	9.1	-4.2	-46	-35	6.6	-16.6	.2	.1	.8
TOP	421.50	6.6	-16.6	2276	4508	2.9	-3.7	-41	-16	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 170

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00	1.0	-4.0	79	222	12.3	-17.9	-119	-29	301.3	-1148.9	261.3	75.7	62.7
1ST	54.00	5.7	-36.3	1194	3360	4.7	-10.8	-38	-6	300.3	-1144.9	199.3	59.5	62.2
2ND	64.50	5.0	-30.4	1005	2827	5.0	-10.7	-40	-7	294.7	-1108.6	187.5	56.4	60.7
3RD	73.33	5.2	-30.2	1005	2827	5.2	-10.7	-41	-7	289.7	-1078.3	177.8	53.8	59.5
4TH	82.17	5.4	-30.1	1005	2827	5.4	-10.6	-42	-8	284.5	-1048.1	168.5	51.2	58.2
5TH	91.00	5.6	-29.9	1005	2827	5.6	-10.6	-44	-8	279.1	-1018.0	159.3	48.7	56.9
6TH	99.83	5.8	-29.8	1005	2827	5.8	-10.5	-45	-9	273.5	-988.1	150.5	46.3	55.5
7TH	108.67	6.0	-29.6	1005	2827	6.0	-10.5	-46	-9	267.7	-958.3	141.9	43.9	54.2
8TH	117.50	6.2	-29.5	1005	2827	6.2	-10.4	-47	-10	261.7	-928.6	133.5	41.6	52.7
9TH	126.33	6.4	-29.4	1005	2827	6.4	-10.4	-49	-11	255.5	-899.1	125.5	39.3	51.3
10TH	135.16	6.6	-29.3	1005	2827	6.5	-10.4	-50	-11	249.1	-869.8	117.7	37.1	49.8
11TH	144.00	6.6	-29.4	1005	2827	6.5	-10.4	-51	-11	242.5	-840.4	110.1	34.9	48.2
12TH	152.83	6.6	-29.2	1005	2827	6.6	-10.3	-51	-12	235.9	-811.0	102.8	32.8	46.6
13TH	161.66	7.9	-34.5	1194	3360	6.6	-10.3	-51	-12	229.3	-781.8	95.8	30.7	45.1
14TH	172.16	6.7	-28.9	1005	2827	6.6	-10.3	-51	-12	221.4	-747.2	87.7	28.4	43.2
15TH	181.00	6.7	-28.7	1005	2827	6.7	-10.2	-51	-12	214.7	-718.4	81.3	26.4	41.7
16TH	189.83	6.7	-28.7	1005	2827	6.7	-10.2	-51	-12	207.9	-689.7	75.1	24.6	40.1
17TH	198.66	6.8	-28.5	1005	2827	6.7	-10.1	-51	-12	201.2	-661.1	69.1	22.8	38.6
18TH	207.50	6.8	-28.4	1005	2827	6.8	-10.0	-51	-12	194.4	-632.8	63.4	21.0	37.1
19TH	216.33	6.9	-28.2	1005	2827	6.8	-10.0	-51	-12	187.5	-604.6	57.9	19.3	35.6
20TH	225.16	6.8	-28.4	1005	2827	6.8	-10.0	-52	-12	180.7	-576.2	52.7	17.7	34.0
21ST	233.99	7.0	-28.4	1005	2827	6.9	-10.0	-52	-13	173.7	-547.8	47.7	16.1	32.4
22ND	242.83	7.2	-28.3	1005	2827	7.1	-10.0	-52	-13	166.6	-519.5	43.0	14.6	30.9
23RD	251.66	7.4	-28.2	1005	2827	7.3	-10.0	-52	-13	159.2	-491.2	38.6	13.2	29.3
24TH	260.49	7.6	-28.1	1005	2827	7.5	-10.0	-51	-14	151.6	-463.1	34.3	11.8	27.8
		7.8	-28.0	1005	2827	7.7	-9.9	-51	-14					

TABLE 7. SHEAR AND MOMENT DIAGRAMS :		RESORTS HOTEL CASINO, ATLANTIC CITY								GUST FACTOR 1.00				
WIND DIRECTION 170		CONFIGURATION A				REFERENCE PRESSURE 30.0 PSF								
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	Z		
25TH	269.33									143.8	-435.1	30.4	10.5	26.2
26TH	278.16	8.0	-27.9	1005	2827	8.0	-9.9	-51	-15	135.8	-407.1	26.7	9.3	24.7
27TH	288.66	9.8	-33.1	1194	3360	8.2	-9.9	-51	-15	126.1	-374.0	22.6	7.9	22.9
28TH	297.49	8.4	-27.7	1005	2827	8.4	-9.8	-51	-15	117.6	-346.3	19.4	6.8	21.3
29TH	306.33	8.6	-27.9	1005	2827	8.6	-9.9	-54	-17	109.0	-318.4	16.4	5.8	19.7
30TH	315.16	8.7	-27.8	1005	2827	8.7	-9.8	-54	-17	100.3	-290.6	13.7	4.9	18.0
31ST	323.99	8.8	-27.8	1005	2827	8.8	-9.8	-55	-17	91.5	-262.8	11.3	4.1	16.4
32ND	332.82	8.9	-27.8	1005	2827	8.9	-9.8	-55	-18	82.6	-235.0	9.1	3.3	14.7
33RD	341.66	9.0	-27.7	1005	2827	9.0	-9.8	-56	-18	73.6	-207.3	7.1	2.6	13.0
34TH	350.49	9.1	-27.7	1005	2827	9.1	-9.8	-56	-19	64.4	-179.6	5.4	2.0	11.2
35TH	359.32	9.3	-27.6	1005	2827	9.2	-9.8	-57	-19	55.2	-152.0	4.0	1.5	9.5
36TH	368.16	9.4	-27.6	1005	2827	9.3	-9.8	-57	-19	45.8	-124.4	2.8	1.0	7.8
37TH	376.99	9.5	-27.6	1005	2827	9.4	-9.7	-57	-20	36.3	-96.9	1.8	.7	6.0
38TH	385.82	9.6	-27.5	1005	2827	9.5	-9.7	-58	-20	26.7	-69.4	1.0	.4	4.2
ROOF	401.49	17.5	-41.4	1782	5013	9.8	-8.3	-59	-25	9.2	-27.9	.3	.1	1.3
TOP	421.50	9.2	-27.9	2276	4508	4.1	-6.2	-43	-14	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 180

RESORTS HOTEL CASINO, ATLANTIC CITY
CONFIGURATION A
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00	1.2	-4.5	79	222	15.6	-20.3	-99	-27	351.7	-1456.4	328.6	89.2	54.8
1ST	54.00	5.4	-48.5	1194	3360	4.6	-14.4	-19	-2	350.4	-1451.9	250.1	70.2	54.3
2ND	64.50	4.9	-49.3	1005	2827	4.8	-14.2	-21	-3	345.0	-1403.4	235.1	66.6	53.3
3RD	73.33	5.1	-39.8	1005	2827	5.1	-14.1	-23	-3	340.1	-1363.1	222.9	63.6	52.5
4TH	82.17	5.4	-39.4	1005	2827	5.4	-13.9	-24	-3	335.0	-1323.3	211.0	60.6	51.6
5TH	91.00	5.7	-38.9	1005	2827	5.7	-13.8	-26	-4	329.6	-1284.0	199.5	57.6	50.6
6TH	99.83	6.0	-38.5	1005	2827	5.9	-13.6	-28	-4	323.9	-1245.0	188.3	54.7	49.6
7TH	108.67	6.2	-38.0	1005	2827	6.2	-13.5	-29	-5	318.0	-1206.6	177.5	51.9	48.5
8TH	117.50	6.5	-37.6	1005	2827	6.5	-13.3	-31	-5	311.7	-1168.5	167.0	49.1	47.3
9TH	126.33	6.8	-37.2	1005	2827	6.7	-13.1	-33	-6	305.2	-1130.9	156.8	46.4	46.1
10TH	135.16	7.1	-36.8	1005	2827	7.0	-13.0	-35	-7	298.5	-1093.7	147.0	43.7	44.9
11TH	144.00	7.3	-36.9	1005	2827	7.3	-13.0	-36	-7	291.4	-1056.9	137.5	41.1	43.6
12TH	152.83	7.6	-36.8	1005	2827	7.5	-13.0	-36	-7	284.1	-1020.1	128.3	38.6	42.2
13TH	161.66	9.3	-43.6	1194	3360	7.8	-13.0	-36	-8	276.5	-983.3	119.5	36.1	40.8
14TH	172.16	8.1	-36.6	1005	2827	8.0	-12.9	-36	-8	267.2	-939.7	109.4	33.3	39.2
15TH	181.00	8.3	-36.5	1005	2827	8.2	-12.9	-36	-8	259.2	-903.1	101.3	30.9	37.8
16TH	189.83	8.5	-36.4	1005	2827	8.5	-12.9	-36	-8	250.9	-866.7	93.4	28.7	36.4
17TH	198.66	8.5	-36.4	1005	2827	8.5	-12.9	-36	-8	242.4	-830.3	86.0	26.5	35.0
18TH	207.50	8.7	-36.3	1005	2827	8.7	-12.8	-36	-9	233.7	-794.0	78.8	24.4	33.6
19TH	216.33	9.0	-36.2	1005	2827	8.9	-12.8	-36	-9	224.7	-757.9	71.9	22.4	32.2
20TH	225.16	9.2	-36.3	1005	2827	9.2	-12.8	-37	-9	215.5	-721.6	65.4	20.4	30.8
21ST	233.99	9.4	-36.1	1005	2827	9.3	-12.8	-37	-10	206.1	-685.5	59.2	18.6	29.4
22ND	242.83	9.5	-36.0	1005	2827	9.5	-12.7	-37	-10	196.6	-649.5	53.3	16.8	28.0
23RD	251.66	9.7	-35.8	1005	2827	9.6	-12.7	-37	-10	187.0	-613.7	47.7	15.1	26.6
24TH	260.49	9.8	-35.7	1005	2827	9.8	-12.6	-37	-10	177.1	-578.0	42.4	13.5	25.1
		10.0	-35.5	1005	2827	9.9	-12.6	-37	-10					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : RESORTS HOTEL CASINO, ATLANTIC CITY
 WIND DIRECTION 180 CONFIGURATION A REFERENCE PRESSURE 30.0 PSF

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33									167.2	-542.5	37.5	12.0	23.7
26TH	278.16	10.1	-35.3	1005	2827	10.1	-12.5	-37	-10	157.1	-507.2	32.9	10.5	22.3
27TH	288.66	12.2	-41.8	1194	3360	10.2	-12.4	-37	-11	144.8	-465.3	27.7	9.0	20.7
28TH	297.49	10.5	-35.0	1005	2827	10.4	-12.4	-37	-11	134.4	-430.3	23.8	7.7	19.3
29TH	306.33	10.6	-35.0	1005	2827	10.6	-12.4	-37	-11	123.8	-395.3	20.1	6.6	17.9
30TH	315.16	10.5	-35.0	1005	2827	10.5	-12.4	-38	-11	113.2	-360.4	16.8	5.5	16.4
31ST	323.99	10.5	-34.9	1005	2827	10.4	-12.4	-38	-12	102.7	-325.4	13.8	4.6	15.0
32ND	332.82	10.4	-34.9	1005	2827	10.4	-12.3	-39	-12	92.3	-290.6	11.1	3.7	13.5
33RD	341.66	10.4	-34.8	1005	2827	10.3	-12.3	-40	-12	81.9	-255.7	8.6	3.0	12.0
34TH	350.49	10.3	-34.8	1005	2827	10.2	-12.3	-41	-12	71.7	-220.9	6.5	2.3	10.4
35TH	359.32	10.2	-34.7	1005	2827	10.2	-12.3	-42	-12	61.4	-186.2	4.7	1.7	8.9
36TH	368.16	10.2	-34.7	1005	2827	10.1	-12.3	-42	-12	51.3	-151.5	3.3	1.2	7.3
37TH	376.99	10.1	-34.7	1005	2827	10.0	-12.3	-43	-13	41.2	-116.8	2.1	.8	5.6
38TH	385.82	10.0	-34.6	1005	2827	10.0	-12.2	-44	-13	31.1	-82.2	1.2	.5	4.0
ROOF	401.49	19.0	-51.8	1782	5013	10.7	-10.3	-47	-17	12.1	-30.5	.3	.1	1.2
TOP	421.50	12.1	-30.5	2276	4508	5.3	-6.8	-34	-14	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 190

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00	1.4	-4.0	79	222	17.9	-18.2	-78	-27	311.2	-1622.9	366.0	78.1	46.4
1ST	54.00	5.6	-55.0	1194	3360	4.7	-16.4	-10	-1	309.8	-1618.9	278.4	61.3	46.0
2ND	64.50	5.0	-45.5	1005	2827	4.9	-16.1	-11	-1	304.2	-1563.9	261.7	58.1	45.5
3RD	73.33	5.2	-44.8	1005	2827	5.1	-15.9	-13	-2	299.2	-1518.4	248.1	55.4	45.0
4TH	82.17	5.4	-44.1	1005	2827	5.3	-15.6	-15	-2	294.1	-1473.6	234.9	52.8	44.4
5TH	91.00	5.6	-43.5	1005	2827	5.5	-15.4	-17	-2	288.7	-1429.4	222.1	50.2	43.7
6TH	99.83	5.8	-42.8	1005	2827	5.7	-15.1	-18	-2	283.1	-1385.9	209.6	47.7	43.0
7TH	108.67	6.0	-42.1	1005	2827	5.9	-14.9	-20	-3	277.4	-1343.2	197.6	45.2	42.2
8TH	117.50	6.2	-41.4	1005	2827	6.1	-14.7	-22	-3	271.4	-1301.1	185.9	42.8	41.3
9TH	126.33	6.4	-40.7	1005	2827	6.3	-14.4	-24	-4	265.3	-1259.7	174.6	40.4	40.4
10TH	135.16	6.6	-40.1	1005	2827	6.5	-14.2	-26	-4	258.9	-1218.9	163.7	38.1	39.4
11TH	144.00	6.7	-40.2	1005	2827	6.7	-14.2	-27	-5	252.4	-1178.8	153.1	35.8	38.3
12TH	152.83	6.9	-40.3	1005	2827	6.8	-14.2	-28	-5	245.6	-1138.7	142.8	33.6	37.2
13TH	161.66	8.4	-48.0	1194	3360	7.0	-14.3	-28	-5	238.8	-1098.4	133.0	31.5	36.0
14TH	172.16	7.2	-40.4	1005	2827	7.2	-14.3	-28	-5	230.4	-1050.5	121.7	29.0	34.6
15TH	181.00	7.4	-40.5	1005	2827	7.3	-14.3	-29	-5	223.2	-1010.0	112.6	27.0	33.5
16TH	189.83	7.5	-40.6	1005	2827	7.5	-14.4	-29	-5	215.8	-969.5	103.8	25.1	32.3
17TH	198.66	7.7	-40.7	1005	2827	7.6	-14.4	-30	-6	208.3	-928.9	95.4	23.2	31.0
18TH	207.50	7.8	-40.8	1005	2827	7.8	-14.4	-30	-6	200.7	-888.2	87.4	21.4	29.8
19TH	216.33	8.0	-41.0	1005	2827	7.9	-14.5	-30	-6	192.8	-847.4	79.8	19.7	28.5
20TH	225.16	8.0	-40.9	1005	2827	8.0	-14.5	-30	-6	184.9	-806.4	72.5	18.0	27.2
21ST	233.99	8.0	-40.8	1005	2827	8.0	-14.4	-30	-6	176.9	-765.5	65.5	16.4	25.9
22ND	242.83	8.0	-40.6	1005	2827	8.0	-14.4	-30	-6	168.8	-724.8	58.9	14.9	24.7
23RD	251.66	8.1	-40.5	1005	2827	8.0	-14.3	-30	-6	160.8	-684.1	52.7	13.4	23.4
24TH	260.49	8.1	-40.3	1005	2827	8.0	-14.3	-30	-6	152.7	-643.7	46.8	12.0	22.2

TABLE 7. SHEAR AND MOMENT DIAGRAMS :														
WIND DIRECTION 190		CONFIGURATION A				RESORTS HOTEL CASINO, ATLANTIC CITY				GUST FACTOR 1.00				
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33									144.6	-603.3	41.3	10.7	20.9
26TH	278.16	8.1	-40.2	1005	2827	8.1	-14.2	-29	-6	136.6	-563.2	36.2	9.5	19.7
27TH	288.66	9.6	-47.6	1194	3360	8.1	-14.2	-29	-6	126.9	-515.6	30.5	8.1	18.2
28TH	297.49	8.1	-39.9	1005	2827	8.1	-14.1	-29	-6	118.8	-475.7	26.1	7.0	17.0
29TH	306.33	8.3	-39.8	1005	2827	8.3	-14.1	-29	-6	110.4	-435.9	22.1	6.0	15.8
30TH	315.16	8.5	-39.5	1005	2827	8.5	-14.0	-30	-6	102.0	-396.4	18.4	5.1	14.6
31ST	323.99	8.6	-39.2	1005	2827	8.6	-13.9	-31	-7	93.3	-357.2	15.1	4.2	13.3
32ND	332.82	8.8	-38.9	1005	2827	8.8	-13.8	-31	-7	84.5	-318.2	12.1	3.4	12.0
33RD	341.66	9.0	-38.6	1005	2827	8.9	-13.7	-32	-7	75.6	-279.6	9.5	2.7	10.7
34TH	350.49	9.1	-38.4	1005	2827	9.1	-13.6	-33	-8	66.4	-241.2	7.2	2.1	9.4
35TH	359.32	9.3	-38.1	1005	2827	9.2	-13.5	-33	-8	57.2	-203.2	5.2	1.5	8.0
36TH	368.16	9.4	-37.8	1005	2827	9.4	-13.4	-34	-9	47.8	-165.4	3.6	1.1	6.7
37TH	376.99	9.6	-37.5	1005	2827	9.5	-13.3	-35	-9	38.2	-127.9	2.3	.7	5.3
38TH	385.82	9.7	-37.2	1005	2827	9.7	-13.2	-36	-9	28.5	-90.7	1.3	.4	3.9
ROOF	401.49	18.1	-55.7	1782	5013	10.1	-11.1	-41	-13	10.4	-35.0	.4	.1	1.3
TOP	421.50	10.4	-35.0	2276	4508	4.6	-7.8	-35	-11	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 200

RESORTS HOTEL CASINO, ATLANTIC CITY
CONFIGURATION A
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00	1.6	-3.9	79	222	20.7	-17.8	-47	-20	259.2	-1895.6	433.1	63.9	48.2
1ST	54.00	5.7	-63.8	1194	3360	4.8	-19.0	-4	-0	257.6	-1891.6	330.8	50.0	48.0
2ND	64.50	4.9	-52.7	1005	2827	4.9	-18.6	-6	-1	251.9	-1827.8	311.3	47.3	47.7
3RD	73.33	5.0	-51.7	1005	2827	5.0	-18.3	-8	-1	247.0	-1775.1	295.4	45.1	47.4
4TH	82.17	5.1	-50.7	1005	2827	5.0	-17.9	-10	-1	242.0	-1723.4	279.9	42.9	47.0
5TH	91.00	5.2	-49.7	1005	2827	5.1	-17.6	-12	-1	237.0	-1672.7	265.0	40.8	46.4
6TH	99.83	5.2	-48.7	1005	2827	5.2	-17.2	-14	-2	231.8	-1623.0	250.4	38.7	45.8
7TH	108.67	5.3	-47.7	1005	2827	5.3	-16.9	-17	-2	226.6	-1574.2	236.3	36.7	45.1
8TH	117.50	5.4	-46.7	1005	2827	5.4	-16.5	-19	-2	221.3	-1526.5	222.6	34.7	44.3
9TH	126.33	5.5	-45.7	1005	2827	5.5	-16.2	-21	-3	215.8	-1479.8	209.3	32.8	43.4
10TH	135.16	5.6	-44.8	1005	2827	5.6	-15.8	-24	-3	210.4	-1434.1	196.4	30.9	42.4
11TH	144.00	5.7	-44.8	1005	2827	5.7	-15.9	-25	-3	204.7	-1389.3	184.0	29.1	41.4
12TH	152.83	5.8	-45.1	1005	2827	5.7	-15.9	-25	-3	199.0	-1344.5	171.9	27.3	40.3
13TH	161.66	6.9	-53.9	1194	3360	5.8	-16.1	-26	-3	193.3	-1299.4	160.2	25.6	39.1
14TH	172.16	5.8	-45.7	1005	2827	5.8	-16.2	-26	-3	186.4	-1245.5	146.9	23.6	37.7
15TH	181.00	5.9	-46.0	1005	2827	5.8	-16.3	-27	-3	180.5	-1199.8	136.1	22.0	36.5
16TH	189.83	5.9	-46.2	1005	2827	5.9	-16.4	-27	-3	174.7	-1153.8	125.7	20.4	35.2
17TH	198.66	5.9	-46.5	1005	2827	5.9	-16.5	-28	-4	168.8	-1107.6	115.7	18.9	33.9
18TH	207.50	6.0	-46.8	1005	2827	5.9	-16.6	-28	-4	162.8	-1061.0	106.1	17.4	32.6
19TH	216.33	6.1	-46.9	1005	2827	6.1	-16.6	-28	-4	156.9	-1014.2	96.9	16.0	31.3
20TH	225.16	6.2	-47.0	1005	2827	6.2	-16.6	-28	-4	150.8	-967.3	88.2	14.6	29.9
21ST	233.99	6.3	-47.0	1005	2827	6.3	-16.6	-28	-4	144.6	-920.4	79.8	13.3	28.6
22ND	242.83	6.4	-47.1	1005	2827	6.4	-16.7	-28	-4	138.3	-873.3	71.9	12.1	27.2
23RD	251.66	6.5	-47.2	1005	2827	6.5	-16.7	-28	-4	131.9	-826.2	64.4	10.9	25.8
24TH	260.49	6.6	-47.2	1005	2827	6.6	-16.7	-29	-4	125.3	-779.1	57.3	9.8	24.5

TABLE 7. SHEAR AND MOMENT DIAGRAMS :		RESORTS HOTEL CASINO, ATLANTIC CITY								GUST FACTOR 1.00				
WIND DIRECTION 200		CONFIGURATION A								REFERENCE PRESSURE 30.0 PSF				
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33	6.8	-47.3	1005	2827	6.7	-16.7	-29	-4	118.7	-731.9	50.6	8.7	23.1
26TH	278.16	8.2	-56.3	1194	3360	6.8	-16.8	-29	-4	111.9	-684.6	44.4	7.7	21.7
27TH	288.66	7.0	-47.4	1005	2827	7.0	-16.8	-29	-4	103.8	-628.3	37.5	6.5	20.1
28TH	297.49	7.2	-47.3	1005	2827	7.1	-16.7	-28	-4	96.8	-580.9	32.2	5.6	18.7
29TH	306.33	7.2	-47.2	1005	2827	7.2	-16.7	-29	-4	89.6	-533.6	27.2	4.8	17.3
30TH	315.16	7.3	-47.1	1005	2827	7.2	-16.7	-30	-5	82.4	-486.3	22.7	4.1	15.9
31ST	323.99	7.3	-47.0	1005	2827	7.3	-16.6	-30	-5	75.1	-439.2	18.6	3.4	14.5
32ND	332.82	7.4	-46.9	1005	2827	7.4	-16.6	-31	-5	67.8	-392.1	15.0	2.7	13.0
33RD	341.66	7.5	-46.8	1005	2827	7.4	-16.6	-31	-5	60.4	-345.2	11.7	2.2	11.6
34TH	350.49	7.5	-46.7	1005	2827	7.5	-16.5	-32	-5	52.9	-298.4	8.9	1.7	10.1
35TH	359.32	7.6	-46.6	1005	2827	7.5	-16.5	-32	-5	45.4	-251.7	6.4	1.2	8.5
36TH	368.16	7.6	-46.5	1005	2827	7.6	-16.5	-33	-5	37.8	-205.0	4.4	.9	7.0
37TH	376.99	7.7	-46.4	1005	2827	7.6	-16.4	-33	-6	30.2	-158.5	2.8	.6	5.4
38TH	385.82	14.2	-69.9	1782	5013	8.0	-14.0	-36	-7	22.5	-112.1	1.6	.3	3.8
ROOF	401.49	8.3	-42.1	2276	4508	3.7	-9.3	-28	-6	8.3	-42.1	.4	.1	1.2
TOP	421.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 210 CONFIGURATION A

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00									125.3	-1939.7	447.6	30.8	39.6
1ST	54.00	1.8	-3.8	79	222	22.4	-17.4	-10	-5	123.5	-1935.9	343.0	24.1	39.6
2ND	64.50	2.6	-64.7	1194	3360	2.2	-19.3	-1	-0	120.8	-1871.1	323.0	22.8	39.5
3RD	73.33	2.3	-53.6	1005	2827	2.3	-19.0	-3	-0	118.6	-1817.6	306.7	21.8	39.3
4TH	82.17	2.4	-52.5	1005	2827	2.4	-18.6	-5	-0	116.2	-1765.1	290.9	20.7	39.1
5TH	91.00	2.4	-51.4	1005	2827	2.4	-18.2	-6	-0	113.7	-1713.7	275.5	19.7	38.7
6TH	99.83	2.5	-50.3	1005	2827	2.5	-17.8	-8	-0	111.2	-1663.3	260.6	18.7	38.3
7TH	108.67	2.6	-49.3	1005	2827	2.6	-17.4	-10	-1	108.6	-1614.1	246.1	17.7	37.8
8TH	117.50	2.7	-48.2	1005	2827	2.6	-17.0	-12	-1	106.0	-1565.9	232.1	16.8	37.2
9TH	126.33	2.7	-47.1	1005	2827	2.7	-16.7	-14	-1	103.2	-1518.8	218.5	15.9	36.6
10TH	135.16	2.8	-46.0	1005	2827	2.8	-16.3	-16	-1	100.4	-1472.8	205.3	15.0	35.8
11TH	144.00	2.9	-44.9	1005	2827	2.9	-15.9	-18	-1	97.5	-1427.9	192.5	14.1	35.0
12TH	152.83	2.9	-44.7	1005	2827	2.9	-15.8	-19	-1	94.6	-1383.3	180.0	13.2	34.2
13TH	161.66	2.9	-44.9	1005	2827	2.9	-15.9	-19	-1	91.7	-1338.4	168.0	12.4	33.3
14TH	172.16	3.4	-53.7	1194	3360	2.8	-16.0	-20	-1	88.3	-1284.6	154.2	11.5	32.2
15TH	181.00	2.8	-45.5	1005	2827	2.8	-16.1	-21	-1	85.5	-1239.1	143.1	10.7	31.3
16TH	189.83	2.8	-45.8	1005	2827	2.7	-16.2	-22	-1	82.8	-1193.4	132.4	10.0	30.3
17TH	198.66	2.7	-46.0	1005	2827	2.7	-16.3	-23	-1	80.1	-1147.4	122.0	9.2	29.2
18TH	207.50	2.7	-46.3	1005	2827	2.7	-16.4	-23	-1	77.4	-1101.1	112.1	8.6	28.2
19TH	216.33	2.6	-46.5	1005	2827	2.6	-16.5	-24	-1	74.8	-1054.6	102.6	7.9	27.0
20TH	225.16	2.7	-46.7	1005	2827	2.7	-16.5	-24	-1	72.1	-1007.9	93.5	7.2	25.9
21ST	233.99	2.8	-46.9	1005	2827	2.8	-16.6	-24	-1	69.3	-960.9	84.8	6.6	24.8
22ND	242.83	2.8	-47.2	1005	2827	2.8	-16.7	-24	-1	66.5	-913.7	76.5	6.0	23.6
23RD	251.66	2.9	-47.5	1005	2827	2.9	-16.8	-24	-1	63.6	-866.3	68.6	5.4	22.4
24TH	260.49	2.9	-47.7	1005	2827	2.9	-16.9	-25	-2	60.7	-818.5	61.2	4.9	21.3
		3.0	-48.0	1005	2827	3.0	-17.0	-25	-2					

TABLE 7. SHEAR AND MOMENT DIAGRAMS :															
WIND DIRECTION 210		CONFIGURATION A		RESORTS HOTEL CASINO, ATLANTIC CITY						REFERENCE PRESSURE 30.0 PSF				GUST FACTOR 1.00	
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)			
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z	
25TH	269.33									57.8	-770.5	54.2	4.4	20.1	
26TH	278.16	3.0	-48.3	1005	2827	3.0	-17.1	-25	-2	54.7	-722.2	47.6	3.9	18.9	
27TH	288.66	3.6	-57.8	1194	3360	3.1	-17.2	-25	-2	51.1	-664.4	40.3	3.3	17.4	
28TH	297.49	3.1	-48.9	1005	2827	3.1	-17.3	-25	-2	48.0	-615.5	34.6	2.9	16.2	
29TH	306.33	3.3	-48.9	1005	2827	3.3	-17.3	-24	-2	44.7	-566.6	29.4	2.5	15.0	
30TH	315.16	3.4	-48.9	1005	2827	3.4	-17.3	-25	-2	41.3	-517.7	24.6	2.1	13.7	
31ST	323.99	3.4	-48.9	1005	2827	3.4	-17.3	-25	-2	37.8	-468.8	20.3	1.7	12.5	
32ND	332.82	3.5	-48.9	1005	2827	3.5	-17.3	-26	-2	34.3	-419.9	16.3	1.4	11.2	
33RD	341.66	3.6	-48.9	1005	2827	3.6	-17.3	-26	-2	30.7	-371.0	12.9	1.1	10.0	
34TH	350.49	3.6	-48.9	1005	2827	3.6	-17.3	-27	-2	27.1	-322.0	9.8	.9	8.6	
35TH	359.32	3.7	-48.9	1005	2827	3.7	-17.3	-27	-2	23.4	-273.1	7.2	.6	7.3	
36TH	368.16	3.8	-49.0	1005	2827	3.8	-17.3	-27	-2	19.6	-224.1	5.0	.5	6.0	
37TH	376.99	3.9	-49.0	1005	2827	3.8	-17.3	-28	-2	15.7	-175.2	3.2	.3	4.6	
38TH	385.82	3.9	-49.0	1005	2827	3.9	-17.3	-28	-2	11.8	-126.2	1.9	.2	3.2	
ROOF	401.49	7.1	-76.4	1782	5013	4.0	-15.2	-29	-3	4.7	-49.8	.5	.0	1.0	
TOP	421.50	4.7	-49.8	2276	4508	2.1	-11.0	-20	-2	0.0	0.0	0.0	0.0	0.0	

TABLE 7. SHEAR AND MOMENT DIAGRAMS ;
WIND DIRECTION 220

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00									-35.4	-1894.0	443.9	-8.9	30.4
1ST	54.00	1.8	-4.1	79	222	22.9	-18.5	-2	-1	-37.2	-1889.9	341.7	-6.9	30.4
2ND	64.50	-.6	-62.3	1194	3360	-.5	-18.5	1	-0	-36.6	-1827.7	322.2	-6.5	30.5
3RD	73.33	-.5	-51.4	1005	2827	-.5	-18.2	-1	0	-36.1	-1776.3	306.3	-6.2	30.4
4TH	82.17	-.5	-50.3	1005	2827	-.5	-17.8	-3	0	-35.6	-1726.0	290.8	-5.9	30.2
5TH	91.00	-.5	-49.1	1005	2827	-.5	-17.4	-5	0	-35.1	-1676.9	275.8	-5.6	30.0
6TH	99.83	-.5	-47.9	1005	2827	-.5	-17.0	-7	0	-34.6	-1629.0	261.2	-5.3	29.7
7TH	108.67	-.5	-46.7	1005	2827	-.5	-16.5	-9	0	-34.1	-1582.3	247.0	-5.0	29.3
8TH	117.50	-.5	-45.6	1005	2827	-.5	-16.1	-11	0	-33.5	-1536.7	233.2	-4.7	28.8
9TH	126.33	-.5	-44.4	1005	2827	-.5	-15.7	-13	0	-33.0	-1492.3	219.9	-4.4	28.3
10TH	135.16	-.6	-43.2	1005	2827	-.6	-15.3	-15	0	-32.4	-1449.0	206.9	-4.1	27.6
11TH	144.00	-.6	-41.9	1005	2827	-.6	-14.8	-16	0	-31.9	-1407.1	194.3	-3.8	26.9
12TH	152.83	-.6	-41.5	1005	2827	-.6	-14.7	-16	0	-31.2	-1365.7	182.0	-3.5	26.3
13TH	161.66	-.8	-41.9	1005	2827	-.8	-14.8	-16	0	-30.5	-1323.8	170.1	-3.3	25.6
14TH	172.16	-1.0	-50.3	1194	3360	-.9	-15.0	-17	0	-29.4	-1273.5	156.5	-2.9	24.7
15TH	181.00	-1.0	-42.7	1005	2827	-1.0	-15.1	-18	0	-28.4	-1230.8	145.4	-2.7	23.9
16TH	189.83	-1.1	-43.1	1005	2827	-1.1	-15.3	-19	0	-27.3	-1187.6	134.8	-2.4	23.1
17TH	198.66	-1.2	-43.5	1005	2827	-1.2	-15.4	-20	1	-26.1	-1144.1	124.5	-2.2	22.2
18TH	207.50	-1.3	-43.9	1005	2827	-1.3	-15.5	-21	1	-24.8	-1100.2	114.5	-2.0	21.3
19TH	216.33	-1.3	-43.9	1005	2827	-1.3	-15.5	-21	1	-24.8	-1100.2	114.5	-2.0	21.3
20TH	225.16	-1.4	-44.3	1005	2827	-1.4	-15.7	-22	1	-23.4	-1055.9	105.0	-1.8	20.3
21ST	233.99	-1.4	-44.3	1005	2827	-1.4	-15.7	-21	1	-22.0	-1011.6	95.9	-1.6	19.4
22ND	242.83	-1.4	-44.7	1005	2827	-1.4	-15.8	-20	1	-20.5	-966.9	87.2	-1.4	18.5
23RD	251.66	-1.4	-45.2	1005	2827	-1.4	-16.0	-20	1	-19.1	-921.7	78.8	-1.2	17.6
24TH	260.49	-1.4	-45.7	1005	2827	-1.4	-16.2	-20	1	-17.7	-876.1	70.9	-1.0	16.6
		-1.4	-46.2	1005	2827	-1.4	-16.3	-20	1	-16.3	-829.9	63.3	-.9	15.7
		-1.4	-46.7	1005	2827	-1.4	-16.5	-20	1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS :														
WIND DIRECTION 220		RESORTS HOTEL CASINO, ATLANTIC CITY								GUST FACTOR 1.00				
		CONFIGURATION A				REFERENCE PRESSURE 30.0 PSF								
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33									-14.8	-783.2	56.2	-0.8	14.8
26TH	278.16	-1.4	-47.2	1005	2827	-1.4	-16.7	-20	1	-13.4	-736.1	49.5	-0.6	13.9
27TH	288.66	-1.7	-56.7	1194	3360	-1.4	-16.9	-20	1	-11.7	-679.4	42.1	-0.5	12.8
28TH	297.49	-1.4	-48.2	1005	2827	-1.4	-17.1	-19	1	-10.3	-631.2	36.3	-0.4	11.8
29TH	306.33	-1.3	-48.2	1005	2827	-1.3	-17.1	-17	0	-8.9	-582.9	30.9	-0.3	11.0
30TH	315.16	-1.3	-48.4	1005	2827	-1.2	-17.1	-18	0	-7.7	-534.5	26.0	-0.2	10.1
31TH	323.99	-1.2	-48.7	1005	2827	-1.2	-17.2	-18	0	-6.5	-485.8	21.5	-0.2	9.2
32ND	332.82	-1.1	-48.9	1005	2827	-1.1	-17.3	-18	0	-5.4	-436.9	17.4	-0.1	8.3
33RD	341.66	-1.0	-49.1	1005	2827	-1.0	-17.4	-19	0	-4.4	-387.9	13.8	-0.1	7.4
34TH	350.49	-1.0	-49.3	1005	2827	-1.0	-17.4	-19	0	-3.4	-338.6	10.6	-0.1	6.5
35TH	359.32	-0.9	-49.5	1005	2827	-0.9	-17.5	-19	0	-2.5	-289.0	7.8	-0.0	5.5
36TH	368.16	-0.8	-49.7	1005	2827	-0.8	-17.6	-20	0	-1.7	-239.3	5.5	-0.0	4.5
37TH	376.99	-0.8	-49.9	1005	2827	-0.8	-17.7	-20	0	-0.9	-189.4	3.6	0.0	3.5
38TH	385.82	-0.7	-50.2	1005	2827	-0.7	-17.7	-20	0	-0.2	-139.2	2.1	0.0	2.5
ROOF	401.49	-0.6	-82.1	1782	5013	-0.4	-16.4	-21	0	0.4	-57.1	0.6	0.0	0.8
TOP	421.50	0.4	-57.1	2276	4508	0.2	-12.7	-15	0	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 230

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00	1.5	-2.9	79	222	19.4	-13.1	25	13	22.4	-1533.9	372.3	2.9	21.3
1ST	54.00	1.8	-48.9	1194	3360	1.5	-14.5	-0	-0	20.8	-1531.0	289.6	1.7	21.4
2ND	64.50	1.5	-39.9	1005	2827	1.5	-14.1	-2	-0	19.0	-1482.1	273.8	1.5	21.4
3RD	73.33	1.4	-38.8	1005	2827	1.4	-13.7	-3	-0	17.5	-1442.2	260.8	1.3	21.3
4TH	82.17	1.4	-37.7	1005	2827	1.4	-13.4	-5	-0	16.1	-1403.4	248.3	1.2	21.2
5TH	91.00	1.3	-36.7	1005	2827	1.3	-13.0	-7	-0	14.7	-1365.7	236.0	1.0	21.0
6TH	99.83	1.3	-35.6	1005	2827	1.3	-12.6	-9	-0	13.4	-1329.0	224.1	.9	20.7
7TH	108.67	1.2	-34.5	1005	2827	1.2	-12.2	-11	-0	12.1	-1293.4	212.6	.8	20.4
8TH	117.50	1.2	-33.4	1005	2827	1.2	-11.8	-13	-0	10.9	-1258.9	201.3	.7	20.0
9TH	126.33	1.1	-32.3	1005	2827	1.1	-11.4	-15	-1	9.7	-1225.5	190.3	.6	19.6
10TH	135.16	1.1	-31.2	1005	2827	1.1	-11.0	-17	-1	8.6	-1193.2	179.6	.5	19.1
11TH	144.00	1.2	-31.0	1005	2827	1.2	-11.0	-17	-1	7.5	-1162.0	169.2	.5	18.5
12TH	152.83	1.1	-31.2	1005	2827	1.1	-11.0	-18	-1	6.3	-1131.0	159.1	.4	18.0
13TH	161.66	1.1	-31.2	1194	3360	.9	-11.1	-19	-1	5.3	-1099.8	149.3	.3	17.4
14TH	172.16	.8	-31.6	1005	2827	.8	-11.2	-20	-1	4.2	-1062.4	137.9	.3	16.7
15TH	181.00	.7	-31.8	1005	2827	.7	-11.3	-21	-0	3.4	-1030.8	128.7	.3	16.1
16TH	189.83	.6	-32.0	1005	2827	.6	-11.3	-22	-0	2.7	-999.0	119.7	.2	15.4
17TH	198.66	.4	-32.2	1005	2827	.4	-11.4	-23	-0	2.1	-967.0	111.0	.2	14.7
18TH	207.50	.3	-32.4	1005	2827	.3	-11.5	-24	-0	1.7	-934.7	102.6	.2	14.0
19TH	216.33	.3	-32.4	1005	2827	.3	-11.5	-23	-0	1.3	-902.3	94.5	.2	13.2
20TH	225.16	.3	-33.2	1005	2827	.3	-11.7	-22	-0	1.0	-869.9	86.7	.2	12.5
21ST	233.99	.2	-34.1	1005	2827	.2	-12.1	-21	-0	.7	-836.7	79.1	.2	11.7
22ND	242.83	.1	-35.0	1005	2827	.1	-12.4	-20	-0	.5	-802.6	71.9	.2	11.0
23RD	251.66	.1	-35.9	1005	2827	.1	-12.7	-19	-0	.4	-767.7	65.0	.2	10.3
24TH	260.49	.0	-36.7	1005	2827	.0	-13.0	-18	0	.3	-731.8	58.3	.2	9.7

TABLE 7. SHEAR AND MOMENT DIAGRAMS :															
WIND DIRECTION 230		CONFIGURATION A								RESORTS HOTEL CASINO, ATLANTIC CITY		REFERENCE PRESSURE 30.0 PSF		GUST FACTOR 1.00	
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)			
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z	
25TH	269.33	-.1	-37.6	1005	2827	-.1	-13.3	-17	0	.3	-695.1	52.0	.2	9.0	
26TH	278.16	-.2	-45.9	1194	3360	-.2	-13.7	-17	0	.4	-657.4	46.1	.2	8.3	
27TH	288.66	-.2	-39.6	1005	2827	-.2	-14.0	-16	0	.6	-611.6	39.4	.1	7.6	
28TH	297.49	-.2	-40.1	1005	2827	-.2	-14.2	-14	0	.8	-572.0	34.2	.1	6.9	
29TH	306.33	-.2	-40.7	1005	2827	-.2	-14.4	-13	0	1.0	-531.9	29.3	.1	6.4	
30TH	315.16	-.1	-41.4	1005	2827	-.1	-14.6	-13	0	1.2	-491.2	24.8	.1	5.9	
31ST	323.99	-.1	-42.1	1005	2827	-.1	-14.9	-13	0	1.3	-449.8	20.6	.1	5.3	
32ND	332.82	-.0	-42.7	1005	2827	-.0	-15.1	-13	0	1.4	-407.7	16.8	.1	4.8	
33RD	341.66	.0	-43.4	1005	2827	.0	-15.4	-12	-0	1.4	-365.0	13.4	.1	4.2	
34TH	350.49	.1	-44.1	1005	2827	.1	-15.6	-12	-0	1.4	-321.6	10.4	.1	3.7	
35TH	359.32	.1	-44.7	1005	2827	.1	-15.8	-12	-0	1.4	-277.5	7.7	.1	3.2	
36TH	368.16	.1	-45.4	1005	2827	.1	-16.1	-12	-0	1.3	-232.7	5.5	.0	2.6	
37TH	376.99	.2	-46.1	1005	2827	.2	-16.3	-11	-0	1.1	-187.3	3.6	.0	2.1	
38TH	385.82	-.3	-80.6	1782	5013	-.1	-16.1	-12	0	.9	-141.2	2.2	.0	1.6	
ROOF	401.49	1.2	-60.6	2276	4508	.5	-13.4	-10	-0	1.2	-60.6	.6	.0	.6	
TOP	421.50									0.0	0.0	0.0	0.0	0.0	

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 240

RESORTS HOTEL CASINO, ATLANTIC CITY
CONFIGURATION A REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00									79.5	-968.8	242.7	18.1	3.1
1ST	54.00	1.1	-1.8	79	222	14.3	-8.0	73	47	78.4	-967.0	190.4	13.9	3.3
2ND	64.50	.8	-35.3	1194	3360	.7	-10.5	4	0	77.5	-931.7	180.4	13.0	3.4
3RD	73.33	.8	-28.1	1005	2827	.8	-9.9	5	0	76.7	-903.6	172.3	12.4	3.6
4TH	82.17	1.0	-26.7	1005	2827	1.0	-9.4	5	0	75.8	-876.9	164.5	11.7	3.7
5TH	91.00	1.1	-25.2	1005	2827	1.1	-8.9	5	0	74.7	-851.7	156.8	11.0	3.8
6TH	99.83	1.3	-23.8	1005	2827	1.2	-8.4	6	0	73.4	-827.9	149.4	10.4	4.0
7TH	108.67	1.4	-22.4	1005	2827	1.4	-7.9	6	0	72.0	-805.5	142.2	9.7	4.1
8TH	117.50	1.5	-20.9	1005	2827	1.5	-7.4	7	1	70.5	-784.6	135.2	9.1	4.3
9TH	126.33	1.7	-19.5	1005	2827	1.7	-6.9	7	1	68.8	-765.1	128.3	8.5	4.4
10TH	135.16	1.8	-18.0	1005	2827	1.8	-6.4	8	1	66.9	-747.0	121.7	7.9	4.6
11TH	144.00	2.0	-16.7	1005	2827	2.0	-5.9	8	1	64.9	-730.3	115.1	7.3	4.7
12TH	152.83	2.2	-16.5	1005	2827	2.2	-5.9	7	1	62.7	-713.8	108.8	6.7	4.8
13TH	161.66	2.3	-16.5	1005	2827	2.3	-5.8	6	1	60.4	-697.3	102.5	6.2	4.9
14TH	172.16	2.9	-19.5	1194	3360	2.4	-5.8	5	1	57.6	-677.8	95.3	5.6	5.0
15TH	181.00	2.5	-16.4	1005	2827	2.5	-5.8	4	1	55.1	-661.4	89.4	5.1	5.1
16TH	189.83	2.6	-16.3	1005	2827	2.6	-5.8	3	0	52.5	-645.1	83.6	4.6	5.1
17TH	198.66	2.7	-16.3	1005	2827	2.7	-5.8	2	0	49.8	-628.8	78.0	4.2	5.2
18TH	207.50	2.8	-16.2	1005	2827	2.8	-5.7	1	0	47.0	-612.6	72.5	3.7	5.2
19TH	216.33	2.9	-16.2	1005	2827	2.9	-5.7	0	0	44.0	-596.4	67.2	3.3	5.2
20TH	225.16	3.1	-16.5	1005	2827	3.1	-5.8	-3	-0	40.9	-579.9	62.0	3.0	5.1
21ST	233.99	3.0	-17.4	1005	2827	3.0	-6.2	-3	-1	37.9	-562.6	56.9	2.6	5.1
22ND	242.83	2.9	-18.3	1005	2827	2.9	-6.5	-4	-1	35.0	-544.2	52.0	2.3	5.0
23RD	251.66	2.8	-19.2	1005	2827	2.8	-6.8	-4	-1	32.2	-525.0	47.3	2.0	4.9
24TH	260.49	2.7	-20.2	1005	2827	2.7	-7.1	-4	-1	29.5	-504.8	42.8	1.7	4.9
		2.6	-21.1	1005	2827	2.6	-7.5	-4	-1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 240

RESORTS HOTEL CASINO, ATLANTIC CITY
CONFIGURATION A
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33									27.0	-483.7	38.4	1.5	4.8
26TH	278.16	2.4	-22.0	1005	2827	2.4	-7.8	-4	-0	24.5	-461.7	34.2	1.2	4.7
27TH	288.66	2.8	-27.4	1194	3360	2.3	-8.2	-5	-0	21.8	-434.3	29.5	1.0	4.5
28TH	297.49	2.2	-24.1	1005	2827	2.2	-8.5	-5	-0	19.6	-410.2	25.8	.8	4.4
29TH	306.33	2.2	-25.2	1005	2827	2.2	-8.9	-5	-0	17.3	-385.0	22.3	.6	4.3
30TH	315.16	2.2	-26.1	1005	2827	2.2	-9.2	-6	-1	15.2	-358.9	19.0	.5	4.1
31ST	323.99	2.1	-27.1	1005	2827	2.1	-9.6	-7	-1	13.1	-331.8	15.9	.4	3.9
32ND	332.82	2.0	-28.0	1005	2827	2.0	-9.9	-8	-1	11.1	-303.8	13.1	.3	3.7
33RD	341.66	1.9	-28.9	1005	2827	1.9	-10.2	-9	-1	9.1	-274.9	10.6	.2	3.5
34TH	350.49	1.9	-29.9	1005	2827	1.9	-10.6	-10	-1	7.2	-245.0	8.3	.1	3.2
35TH	359.32	1.8	-30.8	1005	2827	1.8	-10.9	-10	-1	5.4	-214.2	6.3	.1	2.9
36TH	368.16	1.7	-31.7	1005	2827	1.7	-11.2	-11	-1	3.7	-182.4	4.5	.0	2.5
37TH	376.99	1.6	-32.7	1005	2827	1.6	-11.6	-12	-1	2.1	-149.8	3.0	-0	2.1
38TH	385.82	1.6	-33.6	1005	2827	1.6	-11.9	-12	-1	.5	-116.1	1.9	-0	1.7
ROOF	401.49	2.1	-62.6	1782	5013	1.2	-12.5	-16	-1	-1.6	-53.6	.5	-0	.7
TOP	421.50	-1.6	-53.6	2276	4508	-.7	-11.9	-14	0	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 250 CONFIGURATION A

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00	.8	-2.4	79	222	10.4	-10.9	-6	-2	-53.4	-921.5	224.9	-13.0	-12.0
1ST	54.00	-2.7	-30.5	1194	3360	-2.2	-9.1	16	-1	-54.3	-919.1	175.3	-10.1	-12.0
2ND	64.50	-2.0	-24.6	1005	2827	-2.0	-8.7	15	-1	-51.6	-888.6	165.8	-9.6	-11.5
3RD	73.33	-1.9	-23.7	1005	2827	-1.9	-8.4	14	-1	-49.5	-864.0	158.0	-9.1	-11.1
4TH	82.17	-1.8	-22.8	1005	2827	-1.8	-8.1	13	-1	-47.6	-840.3	150.5	-8.7	-10.8
5TH	91.00	-1.7	-21.9	1005	2827	-1.7	-7.7	12	-1	-45.8	-817.4	143.2	-8.3	-10.5
6TH	99.83	-1.6	-21.0	1005	2827	-1.6	-7.4	11	-1	-44.1	-795.5	136.0	-7.9	-10.2
7TH	108.67	-1.5	-20.1	1005	2827	-1.5	-7.1	10	-1	-42.4	-774.5	129.1	-7.5	-10.0
8TH	117.50	-1.4	-19.2	1005	2827	-1.4	-6.8	9	-1	-40.9	-754.5	122.4	-7.1	-9.8
9TH	126.33	-1.3	-18.3	1005	2827	-1.3	-6.5	8	-1	-39.6	-735.3	115.8	-6.8	-9.6
10TH	135.16	-1.2	-17.3	1005	2827	-1.2	-6.1	6	-0	-38.3	-717.0	109.4	-6.4	-9.4
11TH	144.00	-1.2	-17.2	1005	2827	-1.2	-6.1	7	-0	-37.1	-699.7	103.1	-6.1	-9.3
12TH	152.83	-1.1	-17.5	1005	2827	-1.1	-6.2	7	-0	-35.9	-682.5	97.0	-5.8	-9.2
13TH	161.66	-1.3	-21.0	1194	3360	-1.1	-6.3	8	-0	-34.7	-665.0	91.1	-5.5	-9.1
14TH	172.16	-1.0	-17.9	1005	2827	-1.0	-6.3	8	-0	-33.4	-644.0	84.2	-5.1	-8.9
15TH	181.00	-.9	-18.1	1005	2827	-.9	-6.4	8	-0	-32.4	-626.0	78.6	-4.8	-8.8
16TH	189.83	-.9	-18.4	1005	2827	-.8	-6.5	9	-0	-31.5	-607.9	73.1	-4.5	-8.6
17TH	198.66	-.8	-18.6	1005	2827	-.8	-6.6	9	-0	-30.7	-589.5	67.8	-4.3	-8.5
18TH	207.50	-.7	-18.8	1005	2827	-.7	-6.7	10	-0	-29.9	-571.0	62.7	-4.0	-8.3
19TH	216.33	-.8	-19.0	1005	2827	-.8	-6.7	9	-0	-29.2	-552.2	57.8	-3.7	-8.1
20TH	225.16	-.8	-19.6	1005	2827	-.8	-6.9	10	-0	-28.4	-533.2	53.0	-3.5	-7.9
21ST	233.99	-.7	-20.3	1005	2827	-.7	-7.2	11	-0	-27.6	-513.6	48.3	-3.2	-7.7
22ND	242.83	-.7	-21.0	1005	2827	-.7	-7.4	11	-0	-26.8	-493.2	43.9	-3.0	-7.5
23RD	251.66	-.6	-21.8	1005	2827	-.6	-7.7	12	-0	-26.2	-472.2	39.6	-2.8	-7.3
24TH	260.49	-.6	-22.5	1005	2827	-.6	-7.9	13	-0	-25.5	-450.4	35.5	-2.5	-7.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 250

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33	-0.5	-23.2	1005	2827	-0.5	-8.2	14	-0	-24.9	-428.0	31.7	-2.3	-6.7
26TH	278.16	-0.6	-28.5	1194	3360	-0.5	-8.5	14	-0	-24.4	-404.8	28.0	-2.1	-6.4
27TH	288.66	-0.4	-24.7	1005	2827	-0.4	-8.8	15	-0	-23.8	-376.3	23.9	-1.8	-6.0
28TH	297.49	-0.6	-25.2	1005	2827	-0.6	-8.9	14	-0	-23.4	-351.6	20.7	-1.6	-5.6
29TH	306.33	-0.8	-25.6	1005	2827	-0.8	-9.1	15	-0	-22.8	-326.3	17.7	-1.4	-5.3
30TH	315.16	-1.1	-26.0	1005	2827	-1.1	-9.2	16	-1	-21.9	-300.7	14.9	-1.2	-4.9
31ST	323.99	-1.3	-26.4	1005	2827	-1.3	-9.3	16	-1	-20.9	-274.7	12.4	-1.0	-4.5
32ND	332.82	-1.5	-26.7	1005	2827	-1.5	-9.5	16	-1	-19.6	-248.3	10.1	-0.9	-4.1
33RD	341.66	-1.7	-27.1	1005	2827	-1.7	-9.6	17	-1	-18.1	-221.6	8.0	-0.7	-3.6
34TH	350.49	-1.9	-27.5	1005	2827	-1.9	-9.7	17	-1	-16.4	-194.5	6.1	-0.5	-3.2
35TH	359.32	-2.1	-27.9	1005	2827	-2.1	-9.9	18	-1	-14.5	-166.9	4.6	-0.4	-2.7
36TH	368.16	-2.4	-28.3	1005	2827	-2.3	-10.0	18	-2	-12.3	-139.1	3.2	-0.3	-2.2
37TH	376.99	-2.6	-28.6	1005	2827	-2.6	-10.1	19	-2	-10.0	-110.8	2.1	-0.2	-1.7
38TH	385.82	-4.4	-48.4	1782	5013	-2.5	-9.7	19	-2	-7.4	-82.2	1.2	-0.1	-1.1
ROOF	401.49	-3.0	-33.7	2276	4508	-1.3	-7.5	5	-0	-3.0	-33.7	.3	-0.0	-0.2
TOP	421.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS 1															
WIND DIRECTION 260		CONFIGURATION A		RESORTS HOTEL CASINO, ATLANTIC CITY						REFERENCE PRESSURE 30.0 PSF			GUST FACTOR 1.00		
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)			
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z	
GRND	0.00														
		1.4	-4.2	79	222	17.5	-19.0	-27	-9	-30.4	-1956.3	482.7	-3.4	-27.1	
1ST	54.00														
		-4.5	-61.6	1194	3360	-3.8	-18.3	14	-1	-31.8	-1952.1	377.1	-1.7	-27.2	
2ND	64.50														
		-3.4	-49.9	1005	2827	-3.4	-17.7	13	-1	-27.3	-1890.5	357.0	-1.4	-26.4	
3RD	73.33														
		-3.2	-48.1	1005	2827	-3.2	-17.0	13	-1	-23.9	-1840.6	340.5	-1.1	-25.7	
4TH	82.17														
		-3.0	-46.3	1005	2827	-3.0	-16.4	13	-1	-20.6	-1792.4	324.4	-.9	-25.0	
5TH	91.00														
		-2.9	-44.6	1005	2827	-2.8	-15.8	13	-1	-17.6	-1746.1	308.8	-.8	-24.4	
6TH	99.83														
		-2.7	-42.8	1005	2827	-2.7	-15.1	12	-1	-14.7	-1701.5	293.6	-.6	-23.9	
7TH	108.67														
		-2.5	-41.0	1005	2827	-2.5	-14.5	12	-1	-12.1	-1658.7	278.7	-.5	-23.4	
8TH	117.50														
		-2.3	-39.2	1005	2827	-2.3	-13.9	11	-1	-9.6	-1617.7	264.3	-.4	-22.9	
9TH	126.33														
		-2.1	-37.5	1005	2827	-2.1	-13.3	11	-1	-7.3	-1578.5	250.1	-.3	-22.4	
10TH	135.16														
		-2.0	-35.7	1005	2827	-2.0	-12.6	10	-1	-5.2	-1541.0	236.4	-.3	-22.0	
11TH	144.00														
		-1.9	-35.9	1005	2827	-1.9	-12.7	10	-1	-3.2	-1505.3	222.9	-.3	-21.7	
12TH	152.83														
		-1.7	-36.5	1005	2827	-1.7	-12.9	12	-1	-1.3	-1469.5	209.8	-.2	-21.3	
13TH	161.66														
		-1.7	-44.3	1194	3360	-1.4	-13.2	13	-0	.4	-1432.9	197.0	-.2	-20.9	
14TH	172.16														
		-1.1	-38.0	1005	2827	-1.1	-13.4	14	-0	2.0	-1388.6	182.1	-.2	-20.3	
15TH	181.00														
		-.9	-38.7	1005	2827	-.9	-13.7	15	-0	3.1	-1350.7	170.0	-.3	-19.8	
16TH	189.83														
		-.6	-39.3	1005	2827	-.6	-13.9	16	-0	4.0	-1312.0	158.3	-.3	-19.2	
17TH	198.66														
		-.4	-40.0	1005	2827	-.4	-14.2	17	-0	4.6	-1272.7	146.9	-.3	-18.6	
18TH	207.50														
		-.1	-40.7	1005	2827	-.1	-14.4	17	-0	5.0	-1232.7	135.8	-.4	-17.9	
19TH	216.33														
		-.2	-41.2	1005	2827	-.2	-14.6	17	-0	5.1	-1192.0	125.1	-.4	-17.2	
20TH	225.16														
		-.0	-42.6	1005	2827	-.0	-15.1	17	-0	5.3	-1150.8	114.8	-.5	-16.5	
21ST	233.99														
		.2	-44.0	1005	2827	.2	-15.6	16	0	5.4	-1108.2	104.8	-.5	-15.8	
22ND	242.83														
		.5	-45.5	1005	2827	.5	-16.1	16	0	5.1	-1064.2	95.2	-.6	-15.1	
23RD	251.66														
		.7	-46.9	1005	2827	.7	-16.6	16	0	4.7	-1018.7	86.0	-.6	-14.3	
24TH	260.49														
		.9	-48.4	1005	2827	.9	-17.1	15	0	4.0	-971.8	77.2	-.6	-13.6	

TABLE 7. SHEAR AND MOMENT DIAGRAMS 1														
WIND DIRECTION 260		RESORTS HOTEL CASINO, ATLANTIC CITY								GUST FACTOR 1.00				
		CONFIGURATION A				REFERENCE PRESSURE 30.0 PSF								
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33									3.1	-923.4	68.8	-.7	-12.9
26TH	278.16	1.2	-49.8	1005	2827	1.2	-17.6	15	0	1.9	-873.6	60.9	-.7	-12.1
27TH	288.66	1.7	-61.1	1194	3360	1.4	-18.2	15	0	.2	-812.4	52.0	-.7	-11.2
28TH	297.49	1.7	-53.0	1005	2827	1.7	-18.8	15	0	-1.5	-759.4	45.1	-.7	-10.4
29TH	306.33	1.5	-54.1	1005	2827	1.5	-19.1	13	0	-3.1	-705.3	38.6	-.7	-9.7
30TH	315.16	1.3	-54.9	1005	2827	1.3	-19.4	13	0	-4.4	-650.4	32.6	-.6	-9.0
31ST	323.99	1.1	-55.6	1005	2827	1.1	-19.7	14	0	-5.6	-594.8	27.1	-.6	-8.2
32ND	332.82	.9	-56.4	1005	2827	.9	-19.9	14	0	-6.5	-538.4	22.1	-.5	-7.4
33RD	341.66	.7	-57.1	1005	2827	.7	-20.2	14	0	-7.2	-481.3	17.6	-.5	-6.6
34TH	350.49	.5	-57.8	1005	2827	.5	-20.5	15	0	-7.7	-423.5	13.6	-.4	-5.8
35TH	359.32	.3	-58.6	1005	2827	.3	-20.7	15	0	-8.0	-364.9	10.1	-.4	-4.9
36TH	368.16	.1	-59.3	1005	2827	.1	-21.0	15	0	-8.1	-305.6	7.2	-.3	-4.0
37TH	376.99	-.1	-60.1	1005	2827	-.1	-21.3	16	-0	-8.0	-245.5	4.8	-.2	-3.0
38TH	385.82	-.3	-60.8	1005	2827	-.3	-21.5	16	-0	-7.6	-184.7	2.9	-.1	-2.1
ROOF	401.49	-2.9	-105.8	1782	5013	-1.6	-21.1	16	-0	-4.7	-78.8	.8	-.0	-.3
TOP	421.50	-4.7	-78.8	2276	4508	-2.1	-17.5	4	-0	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 270

RESORTS HOTEL CASINO, ATLANTIC CITY
CONFIGURATION A REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00									-94.0	-2317.3	556.0	-22.0	-50.0
1ST	54.00	1.4	-5.2	79	222	18.1	-23.4	4	1	-95.4	-2312.1	431.0	-16.9	-49.9
2ND	64.50	-4.2	-69.1	1194	3360	-3.5	-20.6	21	-1	-91.2	-2242.9	407.1	-15.9	-48.5
3RD	73.33	-3.3	-57.0	1005	2827	-3.2	-20.2	21	-1	-87.9	-2185.9	387.5	-15.1	-47.3
4TH	82.17	-3.1	-55.9	1005	2827	-3.1	-19.8	22	-1	-84.8	-2130.0	368.5	-14.4	-46.1
5TH	91.00	-3.0	-54.8	1005	2827	-3.0	-19.4	22	-1	-81.8	-2075.2	349.9	-13.6	-44.8
6TH	99.83	-2.9	-53.8	1005	2827	-2.9	-19.0	22	-1	-78.9	-2021.4	331.8	-12.9	-43.6
7TH	108.67	-2.7	-52.7	1005	2827	-2.7	-18.6	23	-1	-76.1	-1968.7	314.2	-12.2	-42.4
8TH	117.50	-2.6	-51.6	1005	2827	-2.6	-18.3	23	-1	-73.5	-1917.1	297.0	-11.6	-41.3
9TH	126.33	-2.5	-50.5	1005	2827	-2.5	-17.9	23	-1	-71.0	-1866.6	280.3	-10.9	-40.1
10TH	135.16	-2.4	-49.5	1005	2827	-2.4	-17.5	24	-1	-68.7	-1817.1	264.0	-10.3	-38.9
11TH	144.00	-2.4	-48.4	1005	2827	-2.4	-17.1	24	-1	-66.3	-1768.7	248.2	-9.7	-37.7
12TH	152.83	-2.6	-48.7	1005	2827	-2.6	-17.2	23	-1	-63.7	-1720.0	232.8	-9.1	-36.6
13TH	161.66	-2.5	-49.4	1005	2827	-2.4	-17.5	24	-1	-61.2	-1670.6	217.8	-8.6	-35.4
14TH	172.16	-2.7	-59.7	1194	3360	-2.3	-17.8	24	-1	-58.5	-1610.9	200.6	-8.0	-34.0
15TH	181.00	-2.1	-51.0	1005	2827	-2.1	-18.0	24	-1	-56.3	-1560.0	186.6	-7.5	-32.8
16TH	189.83	-2.0	-51.7	1005	2827	-2.0	-18.3	24	-1	-54.3	-1508.3	173.0	-7.0	-31.5
17TH	198.66	-1.9	-52.4	1005	2827	-1.9	-18.5	24	-1	-52.4	-1455.9	159.9	-6.5	-30.2
18TH	207.50	-1.7	-53.1	1005	2827	-1.7	-18.8	25	-1	-50.7	-1402.8	147.3	-6.0	-28.9
19TH	216.33	-1.6	-53.8	1005	2827	-1.6	-19.0	25	-1	-49.1	-1349.0	135.2	-5.6	-27.6
20TH	225.16	-1.8	-54.3	1005	2827	-1.8	-19.2	24	-1	-47.3	-1294.7	123.5	-5.2	-26.3
21ST	233.99	-1.8	-55.2	1005	2827	-1.8	-19.5	23	-1	-45.5	-1239.5	112.3	-4.8	-25.0
22ND	242.83	-1.8	-56.1	1005	2827	-1.8	-19.9	23	-1	-43.7	-1183.4	101.6	-4.4	-23.7
23RD	251.66	-1.7	-57.1	1005	2827	-1.7	-20.2	22	-1	-42.0	-1126.3	91.4	-4.0	-22.5
24TH	260.49	-1.6	-58.0	1005	2827	-1.6	-20.5	22	-1	-40.4	-1068.4	81.7	-3.6	-21.2
		-1.5	-58.9	1005	2827	-1.5	-20.8	22	-1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : RESORTS HOTEL CASINO, ATLANTIC CITY
 WIND DIRECTION 270 CONFIGURATION A REFERENCE PRESSURE 30.0 PSF

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33									-38.9	-1009.4	72.5	-3.3	-19.9
26TH	278.16	-1.5	-59.9	1005	2827	-1.5	-21.2	21	-1	-37.4	-949.6	63.9	-2.9	-18.6
27TH	288.66	-1.7	-72.4	1194	3360	-1.4	-21.5	21	-0	-35.7	-877.2	54.3	-2.6	-17.1
28TH	297.49	-1.3	-61.9	1005	2827	-1.3	-21.9	21	-0	-34.4	-815.3	46.8	-2.2	-15.8
29TH	306.33	-1.8	-62.4	1005	2827	-1.7	-22.1	19	-1	-32.6	-752.9	39.9	-1.9	-14.6
30TH	315.16	-1.9	-62.7	1005	2827	-1.9	-22.2	19	-1	-30.8	-690.2	33.5	-1.7	-13.4
31ST	323.99	-2.0	-63.0	1005	2827	-2.0	-22.3	20	-1	-28.7	-627.2	27.7	-1.4	-12.2
32ND	332.82	-2.2	-63.2	1005	2827	-2.1	-22.4	20	-1	-26.6	-564.0	22.4	-1.2	-10.9
33RD	341.66	-2.3	-63.5	1005	2827	-2.3	-22.5	20	-1	-24.3	-500.5	17.7	-.9	-9.7
34TH	350.49	-2.4	-63.8	1005	2827	-2.4	-22.6	20	-1	-21.9	-436.7	13.6	-.7	-8.4
35TH	359.32	-2.6	-64.1	1005	2827	-2.5	-22.7	21	-1	-19.3	-372.6	10.0	-.6	-7.0
36TH	368.16	-2.7	-64.4	1005	2827	-2.7	-22.8	21	-1	-16.6	-308.2	7.0	-.4	-5.7
37TH	376.99	-2.8	-64.6	1005	2827	-2.8	-22.9	21	-1	-13.8	-243.6	4.6	-.3	-4.3
38TH	385.82	-2.9	-64.9	1005	2827	-2.9	-23.0	22	-1	-10.9	-178.7	2.7	-.1	-2.9
ROOF	401.49	-7.4	-105.9	1782	5013	-4.1	-21.1	22	-2	-3.5	-72.8	.7	-.0	-.5
TOP	421.50	-3.5	-72.8	2276	4508	-1.5	-16.1	7	-0	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 280

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00	1.4	-5.6	79	222	18.3	-25.3	-27	-7	-221.6	-2313.1	547.2	-57.7	-59.4
1ST	54.00	-6.2	-71.1	1194	3360	-5.2	-21.2	22	-2	-223.1	-2307.5	422.4	-45.7	-59.6
2ND	64.50	-4.8	-58.4	1005	2827	-4.8	-20.7	23	-2	-216.8	-2236.4	398.6	-43.3	-58.0
3RD	73.33	-4.6	-57.3	1005	2827	-4.6	-20.3	23	-2	-212.0	-2178.0	379.1	-41.5	-56.7
4TH	82.17	-4.4	-56.2	1005	2827	-4.4	-19.9	24	-2	-207.4	-2120.6	360.1	-39.6	-55.3
5TH	91.00	-4.2	-55.1	1005	2827	-4.2	-19.5	24	-2	-203.0	-2064.4	341.6	-37.8	-54.0
6TH	99.83	-4.0	-54.0	1005	2827	-3.9	-19.1	25	-2	-198.8	-2009.3	323.6	-36.0	-52.6
7TH	108.67	-3.7	-52.9	1005	2827	-3.7	-18.7	25	-2	-194.8	-1955.4	306.1	-34.3	-51.3
8TH	117.50	-3.5	-51.8	1005	2827	-3.5	-18.3	26	-2	-191.1	-1902.5	289.1	-32.6	-49.9
9TH	126.33	-3.3	-50.6	1005	2827	-3.3	-17.9	27	-2	-187.6	-1850.8	272.5	-30.9	-48.6
10TH	135.16	-3.3	-49.7	1005	2827	-3.3	-17.6	26	-2	-184.3	-1800.1	256.4	-29.3	-47.2
11TH	144.00	-3.7	-50.4	1005	2827	-3.7	-17.8	24	-2	-181.0	-1750.4	240.7	-27.6	-45.9
12TH	152.83	-3.8	-51.0	1005	2827	-3.8	-18.1	25	-2	-177.3	-1700.0	225.5	-26.1	-44.7
13TH	161.66	-4.7	-61.5	1194	3360	-3.9	-18.3	26	-2	-173.5	-1648.9	210.7	-24.5	-43.4
14TH	172.16	-4.0	-52.4	1005	2827	-4.0	-18.5	26	-2	-168.8	-1587.5	193.7	-22.7	-41.9
15TH	181.00	-4.1	-53.0	1005	2827	-4.1	-18.8	27	-2	-164.8	-1535.1	179.9	-21.2	-40.5
16TH	189.83	-4.2	-53.6	1005	2827	-4.2	-19.0	28	-2	-160.7	-1482.1	166.6	-19.8	-39.1
17TH	198.66	-4.3	-54.2	1005	2827	-4.3	-19.2	28	-2	-156.5	-1428.5	153.7	-18.4	-37.6
18TH	207.50	-4.4	-54.8	1005	2827	-4.4	-19.4	29	-2	-152.2	-1374.2	141.3	-17.0	-36.0
19TH	216.33	-4.9	-55.7	1005	2827	-4.9	-19.7	27	-2	-147.8	-1319.4	129.4	-15.7	-34.4
20TH	225.16	-5.1	-56.5	1005	2827	-5.1	-20.0	26	-2	-142.9	-1263.7	118.0	-14.4	-32.9
21ST	233.99	-5.3	-57.1	1005	2827	-5.2	-20.2	26	-2	-137.8	-1207.2	107.1	-13.2	-31.4
22ND	242.83	-5.4	-57.8	1005	2827	-5.4	-20.5	26	-2	-132.6	-1150.1	96.7	-12.0	-29.9
23RD	251.66	-5.5	-58.5	1005	2827	-5.5	-20.7	26	-2	-127.2	-1092.2	86.8	-10.9	-28.4
24TH	260.49	-5.7	-59.2	1005	2827	-5.6	-20.9	26	-2	-121.6	-1033.7	77.4	-9.8	-26.9

TABLE 7. SHEAR AND MOMENT DIAGRAMS :														
WIND DIRECTION 280		RESORTS HOTEL CASINO, ATLANTIC CITY										GUST FACTOR 1.00		
		CONFIGURATION A		REFERENCE PRESSURE 30.0 PSF					MOMENT (1000-FT-KIPS)					
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		X	Y	Z
		X	Y	X	Y	X	Y	X	Y	X	Y			
25TH	269.33	-5.8	-59.9	1005	2827	-5.8	-21.2	26	-3	-116.0	-974.5	68.5	-8.7	-25.3
26TH	278.16	-7.1	-72.0	1194	3360	-5.9	-21.4	26	-3	-110.2	-914.7	60.2	-7.7	-23.8
27TH	288.66	-6.1	-61.4	1005	2827	-6.1	-21.7	26	-3	-103.1	-842.6	51.0	-6.6	-21.9
28TH	297.49	-6.9	-62.1	1005	2827	-6.9	-22.0	24	-3	-97.0	-781.3	43.8	-5.7	-20.3
29TH	306.33	-7.0	-62.2	1005	2827	-7.0	-22.0	25	-3	-90.0	-719.2	37.2	-4.9	-18.7
30TH	315.16	-7.1	-62.2	1005	2827	-7.1	-22.0	25	-3	-83.0	-657.0	31.1	-4.1	-17.2
31ST	323.99	-7.2	-62.3	1005	2827	-7.2	-22.0	25	-3	-75.9	-594.7	25.6	-3.4	-15.6
32ND	332.82	-7.3	-62.4	1005	2827	-7.3	-22.1	26	-3	-68.7	-532.4	20.6	-2.8	-14.0
33RD	341.66	-7.4	-62.5	1005	2827	-7.4	-22.1	26	-3	-61.4	-470.0	16.2	-2.2	-12.4
34TH	350.49	-7.5	-62.5	1005	2827	-7.5	-22.1	27	-3	-54.0	-407.6	12.3	-1.7	-10.7
35TH	359.32	-7.6	-62.6	1005	2827	-7.6	-22.1	27	-3	-46.5	-345.1	9.0	-1.2	-9.0
36TH	368.16	-7.7	-62.7	1005	2827	-7.7	-22.2	27	-3	-38.9	-282.5	6.2	-.9	-7.3
37TH	376.99	-7.8	-62.7	1005	2827	-7.8	-22.2	28	-3	-31.2	-219.8	4.0	-.6	-5.6
38TH	385.82	-7.8	-62.7	1005	2827	-7.8	-22.2	28	-3	-23.4	-157.1	2.3	-.3	-3.8
ROOF	401.49	-15.9	-97.2	1782	5013	-8.9	-19.4	30	-5	-7.5	-59.9	.6	-.1	-.8
TOP	421.50	-7.5	-59.9	2276	4508	-3.3	-13.3	14	-2	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 290 CONFIGURATION A

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)			
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z	
GRND	0.00														
		1.4	-5.5	79	222	17.4	-24.6	-39	-10	-379.4	-2518.1	586.1	-101.4	-62.2	
1ST	54.00														
		-5.5	-77.7	1194	3360	-4.6	-23.1	18	-1	-380.8	-2512.6	450.3	-80.9	-62.4	
2ND	64.50														
		-4.7	-64.5	1005	2827	-4.7	-22.8	19	-1	-375.3	-2434.9	424.3	-76.9	-61.0	
3RD	73.33														
		-4.9	-63.7	1005	2827	-4.9	-22.5	19	-1	-370.5	-2370.5	403.1	-73.6	-59.8	
4TH	82.17														
		-5.0	-62.9	1005	2827	-5.0	-22.3	19	-2	-365.7	-2306.8	382.4	-70.4	-58.6	
5TH	91.00														
		-5.2	-62.2	1005	2827	-5.2	-22.0	20	-2	-360.6	-2243.8	362.3	-67.2	-57.4	
6TH	99.83														
		-5.4	-61.4	1005	2827	-5.3	-21.7	20	-2	-355.4	-2181.7	342.8	-64.0	-56.2	
7TH	108.67														
		-5.5	-60.6	1005	2827	-5.5	-21.5	20	-2	-350.1	-2120.3	323.8	-60.9	-54.9	
8TH	117.50														
		-5.7	-59.9	1005	2827	-5.7	-21.2	21	-2	-344.6	-2059.6	305.3	-57.8	-53.7	
9TH	126.33														
		-5.8	-59.1	1005	2827	-5.8	-20.9	21	-2	-338.9	-1999.7	287.4	-54.8	-52.4	
10TH	135.16														
		-6.2	-58.3	1005	2827	-6.1	-20.6	21	-2	-333.0	-1940.6	270.0	-51.8	-51.2	
11TH	144.00														
		-6.7	-58.4	1005	2827	-6.7	-20.7	22	-3	-326.9	-1882.3	253.1	-48.9	-49.9	
12TH	152.83														
		-6.9	-58.8	1005	2827	-6.9	-20.8	22	-3	-320.1	-1823.9	236.7	-46.1	-48.6	
13TH	161.66														
		-7.0	-58.8	1005	2827	-7.2	-21.0	23	-3	-313.2	-1765.1	220.9	-43.3	-47.3	
14TH	172.16														
		-8.6	-70.5	1194	3360	-7.2	-21.0	23	-3	-304.6	-1694.7	202.7	-40.0	-45.7	
15TH	181.00														
		-7.5	-59.8	1005	2827	-7.5	-21.1	23	-3	-297.1	-1634.9	188.0	-37.4	-44.3	
16TH	189.83														
		-7.8	-60.2	1005	2827	-7.7	-21.3	24	-3	-289.3	-1574.7	173.8	-34.8	-42.8	
17TH	198.66														
		-8.0	-60.7	1005	2827	-8.0	-21.5	24	-3	-281.3	-1514.0	160.2	-32.3	-41.3	
18TH	207.50														
		-8.2	-61.1	1005	2827	-8.2	-21.6	24	-3	-273.1	-1452.9	147.1	-29.8	-39.8	
19TH	216.33														
		-8.5	-61.5	1005	2827	-8.4	-21.8	25	-3	-264.6	-1391.4	134.5	-27.4	-38.3	
20TH	225.16														
		-9.3	-61.8	1005	2827	-9.2	-21.9	25	-4	-255.3	-1329.6	122.5	-25.1	-36.7	
21ST	233.99														
		-9.6	-62.2	1005	2827	-9.6	-22.0	25	-4	-245.7	-1267.4	111.0	-22.9	-35.1	
22ND	242.83														
		-9.9	-62.6	1005	2827	-9.9	-22.1	25	-4	-235.8	-1204.8	100.1	-20.8	-33.5	
23RD	251.66														
		-10.2	-63.0	1005	2827	-10.1	-22.3	25	-4	-225.6	-1141.8	89.7	-18.8	-31.9	
24TH	260.49														
		-10.5	-63.4	1005	2827	-10.4	-22.4	25	-4	-215.1	-1078.5	79.9	-16.8	-30.3	
		-10.7	-63.8	1005	2827	-10.7	-22.6	25	-4						

TABLE 7. SHEAR AND MOMENT DIAGRAMS :		RESORTS HOTEL CASINO, ATLANTIC CITY								GUST FACTOR 1.00				
WIND DIRECTION 290		CONFIGURATION A								REFERENCE PRESSURE 30.0 PSF				
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33									-204.4	-1014.7	70.7	-15.0	-28.6
26TH	278.16	-11.0	-64.2	1005	2827	-11.0	-22.7	25	-4	-193.4	-950.5	62.0	-13.2	-27.0
27TH	288.66	-13.4	-76.8	1194	3360	-11.3	-22.9	25	-4	-179.9	-873.7	52.4	-11.2	-25.0
28TH	297.49	-11.6	-65.1	1005	2827	-11.6	-23.0	25	-5	-168.3	-808.6	45.0	-9.7	-23.3
29TH	306.33	-12.4	-65.3	1005	2827	-12.3	-23.1	25	-5	-156.0	-743.3	38.2	-8.3	-21.6
30TH	315.16	-12.5	-65.2	1005	2827	-12.5	-23.1	26	-5	-143.5	-678.1	31.9	-7.0	-19.8
31ST	323.99	-12.7	-65.1	1005	2827	-12.6	-23.0	26	-5	-130.8	-613.0	26.2	-5.7	-18.1
32ND	332.82	-12.8	-65.1	1005	2827	-12.8	-23.0	27	-5	-117.9	-547.9	21.0	-4.6	-16.2
33RD	341.66	-13.0	-65.0	1005	2827	-12.9	-23.0	27	-5	-104.9	-483.0	16.5	-3.7	-14.4
34TH	350.49	-13.1	-64.9	1005	2827	-13.1	-23.0	28	-6	-91.8	-418.0	12.5	-2.8	-12.5
35TH	359.32	-13.3	-64.8	1005	2827	-13.2	-22.9	28	-6	-78.5	-353.2	9.1	-2.0	-10.6
36TH	368.16	-13.5	-64.8	1005	2827	-13.4	-22.9	29	-6	-65.0	-288.5	6.3	-1.4	-8.7
37TH	376.99	-13.6	-64.7	1005	2827	-13.6	-22.9	29	-6	-51.4	-223.8	4.0	-.9	-6.8
38TH	385.82	-13.8	-64.6	1005	2827	-13.7	-22.9	30	-6	-37.6	-159.2	2.3	-.5	-4.8
ROOF	401.49	-26.3	-98.8	1782	5013	-14.7	-19.7	34	-9	-11.4	-60.4	.6	-.1	-1.1
TOP	421.50	-11.4	-60.4	2276	4508	-5.0	-13.4	18	-3	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 300 CONFIGURATION A

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00	.8	-4.6	79	222	10.1	-21.0	-39	-7	-485.5	-2149.1	494.7	-128.0	-63.6
1ST	54.00	-6.2	-65.4	1194	3360	-5.2	-19.5	24	-2	-486.3	-2144.5	378.8	-101.7	-63.8
2ND	64.50	-5.5	-54.7	1005	2827	-5.5	-19.3	24	-2	-480.1	-2079.1	356.6	-96.7	-62.2
3RD	73.33	-5.8	-54.4	1005	2827	-5.8	-19.3	25	-3	-474.6	-2024.4	338.5	-92.5	-60.9
4TH	82.17	-6.2	-54.2	1005	2827	-6.1	-19.2	25	-3	-468.7	-1970.0	320.8	-88.3	-59.5
5TH	91.00	-6.5	-53.9	1005	2827	-6.4	-19.1	25	-3	-462.6	-1915.8	303.7	-84.2	-58.1
6TH	99.83	-6.8	-53.7	1005	2827	-6.8	-19.0	26	-3	-456.1	-1861.8	287.0	-80.1	-56.7
7TH	108.67	-7.1	-53.5	1005	2827	-7.1	-18.9	26	-3	-449.3	-1808.1	270.8	-76.1	-55.3
8TH	117.50	-7.4	-53.2	1005	2827	-7.4	-18.8	26	-4	-442.2	-1754.7	255.0	-72.2	-53.9
9TH	126.33	-7.7	-53.0	1005	2827	-7.7	-18.7	27	-4	-434.8	-1701.4	239.8	-68.3	-52.5
10TH	135.16	-8.2	-52.8	1005	2827	-8.2	-18.7	27	-4	-427.0	-1648.5	225.0	-64.5	-51.0
11TH	144.00	-8.9	-52.8	1005	2827	-8.9	-18.7	27	-5	-418.8	-1595.7	210.7	-60.8	-49.6
12TH	152.83	-9.4	-52.9	1005	2827	-9.3	-18.7	27	-5	-409.9	-1542.9	196.8	-57.1	-48.1
13TH	161.66	-11.7	-63.0	1194	3360	-9.8	-18.8	27	-5	-400.5	-1489.9	183.4	-53.5	-46.6
14TH	172.16	-10.4	-53.1	1005	2827	-10.3	-18.8	27	-5	-388.8	-1426.9	168.1	-49.4	-44.9
15TH	181.00	-10.8	-53.2	1005	2827	-10.8	-18.8	27	-6	-378.4	-1373.8	155.7	-46.0	-43.4
16TH	189.83	-11.3	-53.3	1005	2827	-11.2	-18.9	27	-6	-367.6	-1320.6	143.8	-42.7	-41.9
17TH	198.66	-11.7	-53.4	1005	2827	-11.7	-18.9	27	-6	-356.3	-1267.3	132.4	-39.5	-40.4
18TH	207.50	-12.2	-53.5	1005	2827	-12.1	-18.9	27	-6	-344.6	-1213.9	121.4	-36.4	-38.8
19TH	216.33	-12.9	-53.6	1005	2827	-12.8	-19.0	28	-7	-332.4	-1160.4	110.9	-33.4	-37.3
20TH	225.16	-13.2	-53.9	1005	2827	-13.2	-19.1	28	-7	-319.5	-1106.6	100.9	-30.5	-35.7
21ST	233.99	-13.5	-53.9	1005	2827	-13.4	-19.1	28	-7	-306.3	-1052.7	91.4	-27.8	-34.1
22ND	242.83	-13.8	-53.9	1005	2827	-13.7	-19.1	28	-7	-292.8	-998.8	82.3	-25.1	-32.5
23RD	251.66	-14.0	-53.9	1005	2827	-14.0	-19.1	28	-7	-279.0	-944.9	73.8	-22.6	-30.9
24TH	260.49	-14.3	-53.9	1005	2827	-14.2	-19.1	28	-8	-265.0	-890.9	65.6	-20.2	-29.3

TABLE 7. SHEAR AND MOMENT DIAGRAMS ;
WIND DIRECTION 300

RESORTS HOTEL CASINO, ATLANTIC CITY
CONFIGURATION A
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33	-14.6	-54.0	1005	2827	-14.5	-19.1	28	-8	-250.7	-837.0	58.0	-17.9	-27.7
26TH	278.16	-17.7	-64.2	1194	3360	-14.8	-19.1	29	-8	-236.1	-783.0	50.9	-15.8	-26.0
27TH	288.66	-15.2	-54.0	1005	2827	-15.1	-19.1	29	-8	-218.4	-718.8	43.0	-13.4	-24.1
28TH	297.49	-15.7	-54.2	1005	2827	-15.7	-19.2	29	-8	-203.2	-664.8	36.9	-11.5	-22.4
29TH	306.33	-15.8	-54.0	1005	2827	-15.7	-19.1	30	-9	-187.5	-610.7	31.2	-9.8	-20.7
30TH	315.16	-15.8	-53.9	1005	2827	-15.8	-19.1	30	-9	-171.7	-556.6	26.1	-8.2	-18.9
31ST	323.99	-15.9	-53.7	1005	2827	-15.8	-19.0	30	-9	-155.9	-502.7	21.4	-6.8	-17.2
32ND	332.82	-15.9	-53.6	1005	2827	-15.8	-19.0	31	-9	-140.0	-449.0	17.2	-5.5	-15.4
33RD	341.66	-16.0	-53.4	1005	2827	-15.9	-18.9	31	-9	-124.1	-395.4	13.5	-4.3	-13.6
34TH	350.49	-16.0	-53.3	1005	2827	-15.9	-18.9	32	-10	-108.1	-341.9	10.2	-3.3	-11.8
35TH	359.32	-16.0	-53.1	1005	2827	-16.0	-18.8	32	-10	-92.1	-288.6	7.4	-2.4	-9.9
36TH	368.16	-16.1	-53.0	1005	2827	-16.0	-18.8	33	-10	-76.1	-235.5	5.1	-1.6	-8.1
37TH	376.99	-16.1	-52.9	1005	2827	-16.1	-18.7	33	-10	-60.0	-182.5	3.3	-1.0	-6.2
38TH	385.82	-30.5	-80.7	1782	5013	-17.1	-16.1	37	-14	-43.9	-129.6	1.9	-.6	-4.3
ROOF	401.49	-13.4	-48.9	2276	4508	-5.9	-10.9	17	-5	-13.4	-48.9	.5	-.1	-.9
TOP	421.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 310

RESORTS HOTEL CASINO, ATLANTIC CITY
CONFIGURATION A
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	Z		
GRND	0.00									-425.0	-1769.9	419.7	-115.7	-74.9
1ST	54.00	.3	-3.6	79	222	3.3	-16.0	-23	-2	-425.3	-1786.3	314.1	-92.7	-75.0
2ND	64.50	-4.0	-49.6	1194	3360	-3.4	-14.8	37	-3	-421.3	-1736.7	295.7	-88.3	-73.1
3RD	73.33	-3.6	-42.3	1005	2827	-3.6	-15.0	38	-3	-417.6	-1694.5	280.5	-84.6	-71.5
4TH	82.17	-3.9	-42.9	1005	2827	-3.9	-15.2	38	-4	-413.7	-1651.6	265.7	-80.9	-69.9
5TH	91.00	-4.2	-43.5	1005	2827	-4.2	-15.4	39	-4	-409.5	-1608.0	251.3	-77.3	-68.2
6TH	99.83	-4.5	-44.1	1005	2827	-4.5	-15.6	40	-4	-405.0	-1563.9	237.3	-73.7	-66.4
7TH	108.67	-4.8	-44.7	1005	2827	-4.7	-15.8	41	-4	-400.3	-1519.2	223.7	-70.1	-64.5
8TH	117.50	-5.0	-45.3	1005	2827	-5.0	-16.0	41	-5	-395.2	-1473.8	210.5	-66.6	-62.6
9TH	126.33	-5.3	-46.0	1005	2827	-5.3	-16.3	42	-5	-389.9	-1427.9	197.7	-63.1	-60.7
10TH	135.16	-5.6	-46.6	1005	2827	-5.6	-16.5	43	-5	-384.3	-1381.3	185.3	-59.7	-58.6
11TH	144.00	-5.9	-47.2	1005	2827	-5.9	-16.7	43	-5	-378.4	-1334.1	173.3	-56.3	-56.6
12TH	152.83	-6.6	-47.2	1005	2827	-6.5	-16.7	43	-6	-371.8	-1286.9	161.7	-53.0	-54.5
13TH	161.66	-7.1	-47.0	1005	2827	-7.1	-16.6	42	-6	-364.7	-1239.9	150.5	-49.8	-52.5
14TH	172.16	-9.2	-55.6	1194	3360	-7.7	-16.5	42	-7	-355.5	-1184.3	137.8	-46.0	-50.1
15TH	181.00	-8.4	-46.5	1005	2827	-8.3	-16.5	41	-7	-347.2	-1137.8	127.5	-42.9	-48.1
16TH	189.83	-8.9	-46.3	1005	2827	-8.9	-16.4	41	-8	-338.2	-1091.5	117.7	-39.9	-46.1
17TH	198.66	-9.5	-46.1	1005	2827	-9.4	-16.3	40	-8	-328.8	-1045.4	108.3	-36.9	-44.2
18TH	207.50	-10.0	-45.9	1005	2827	-10.0	-16.2	40	-9	-318.7	-999.5	99.2	-34.1	-42.3
19TH	216.33	-10.6	-45.7	1005	2827	-10.5	-16.2	39	-9	-308.1	-953.8	90.6	-31.3	-40.4
20TH	225.16	-11.2	-45.7	1005	2827	-11.1	-16.2	39	-10	-297.0	-908.1	82.4	-28.6	-38.5
21ST	233.99	-11.6	-45.5	1005	2827	-11.5	-16.1	39	-10	-285.4	-862.6	74.6	-26.0	-36.6
22ND	242.83	-12.0	-45.3	1005	2827	-11.9	-16.0	38	-10	-273.4	-817.2	67.1	-23.6	-34.8
23RD	251.66	-12.4	-45.1	1005	2827	-12.3	-16.0	38	-10	-261.0	-772.1	60.1	-21.2	-32.9
24TH	260.49	-12.8	-44.9	1005	2827	-12.7	-15.9	38	-11	-248.2	-727.2	53.5	-19.0	-31.1
		-13.2	-44.7	1005	2827	-13.1	-15.8	38	-11					

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 310 CONFIGURATION A

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33	-13.6	-44.5	1005	2827	-13.5	-15.8	37	-11	-235.0	-682.4	47.3	-16.8	-29.3
26TH	278.16	-16.7	-52.7	1194	3360	-14.0	-15.7	37	-12	-221.4	-637.9	41.4	-14.8	-27.4
27TH	288.66	-14.5	-44.1	1005	2827	-14.4	-15.6	36	-12	-204.7	-585.3	35.0	-12.6	-25.3
28TH	297.49	-14.9	-44.0	1005	2827	-14.8	-15.6	37	-12	-190.2	-541.2	30.1	-10.8	-23.5
29TH	306.33	-14.8	-43.9	1005	2827	-14.8	-15.5	37	-13	-175.3	-497.2	25.5	-9.2	-21.7
30TH	315.16	-14.8	-43.8	1005	2827	-14.8	-15.5	38	-13	-160.5	-453.2	21.3	-7.7	-19.9
31ST	323.99	-14.8	-43.7	1005	2827	-14.8	-15.5	38	-13	-145.7	-409.4	17.5	-6.4	-18.0
32ND	332.82	-14.8	-43.6	1005	2827	-14.7	-15.4	39	-13	-130.8	-365.8	14.0	-5.2	-16.2
33RD	341.66	-14.8	-43.4	1005	2827	-14.7	-15.4	40	-13	-116.0	-322.2	11.0	-4.1	-14.3
34TH	350.49	-14.8	-43.3	1005	2827	-14.7	-15.3	40	-14	-101.2	-278.7	8.3	-3.1	-12.3
35TH	359.32	-14.8	-43.2	1005	2827	-14.7	-15.3	41	-14	-86.4	-235.4	6.1	-2.3	-10.4
36TH	368.16	-14.8	-43.1	1005	2827	-14.7	-15.2	41	-14	-71.7	-192.2	4.2	-1.6	-8.4
37TH	376.99	-14.8	-43.0	1005	2827	-14.7	-15.2	42	-14	-56.9	-149.1	2.7	-1.0	-6.5
38TH	385.82	-27.6	-66.1	1782	5013	-15.5	-13.2	44	-18	-42.1	-106.2	1.5	-.6	-4.5
ROOF	401.49	-14.5	-40.1	2276	4508	-6.4	-8.9	24	-8	-14.5	-40.1	.4	-.1	-1.1
TOP	421.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 320 CONFIGURATION A

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00									-387.1	-1114.7	261.2	-103.4	-51.9
1ST	54.00	-1.2	-1.9	79	222	-2.3	-8.5	-152	15	-387.0	-1112.8	201.0	-82.5	-52.2
2ND	64.50	-4.4	-26.0	1194	3360	-3.7	-7.7	39	-7	-382.5	-1086.9	189.5	-78.5	-51.1
3RD	73.33	-3.9	-22.6	1005	2827	-3.9	-8.0	42	-7	-378.7	-1064.3	180.0	-75.1	-50.2
4TH	82.17	-4.2	-23.3	1005	2827	-4.2	-8.2	44	-8	-374.4	-1041.0	170.7	-71.8	-49.1
5TH	91.00	-4.6	-24.0	1005	2827	-4.5	-8.5	47	-9	-369.9	-1017.0	161.6	-68.5	-47.9
6TH	99.83	-4.9	-24.8	1005	2827	-4.9	-8.8	49	-10	-365.0	-992.2	152.7	-65.3	-46.7
7TH	108.67	-5.2	-25.5	1005	2827	-5.2	-9.0	51	-10	-359.7	-966.7	144.1	-62.1	-45.3
8TH	117.50	-5.6	-26.3	1005	2827	-5.5	-9.3	53	-11	-354.2	-940.4	135.6	-58.9	-43.9
9TH	126.33	-5.9	-27.0	1005	2827	-5.9	-9.6	55	-12	-348.3	-913.4	127.5	-55.8	-42.3
10TH	135.16	-6.3	-27.8	1005	2827	-6.2	-9.8	56	-13	-342.0	-885.6	119.5	-52.8	-40.7
11TH	144.00	-6.5	-28.5	1005	2827	-6.5	-10.1	58	-13	-335.5	-857.1	111.8	-49.8	-39.0
12TH	152.83	-6.7	-29.7	1005	2827	-6.6	-10.2	56	-13	-328.9	-828.4	104.4	-46.9	-37.3
13TH	161.66	-7.0	-29.0	1005	2827	-7.0	-10.2	54	-13	-321.8	-799.4	97.2	-44.0	-35.6
14TH	172.16	-8.9	-34.7	1194	3360	-7.4	-10.3	51	-13	-312.9	-764.7	89.0	-40.6	-33.7
15TH	181.00	-7.9	-29.4	1005	2827	-7.9	-10.4	49	-13	-305.0	-735.3	82.4	-37.9	-32.2
16TH	189.83	-8.3	-29.6	1005	2827	-8.3	-10.5	47	-13	-296.7	-705.7	76.0	-35.3	-30.7
17TH	198.66	-8.7	-29.8	1005	2827	-8.7	-10.5	45	-13	-288.0	-675.9	69.9	-32.7	-29.2
18TH	207.50	-9.1	-30.0	1005	2827	-9.0	-10.6	42	-13	-278.9	-645.9	64.0	-30.2	-27.9
19TH	207.50	-9.5	-30.2	1005	2827	-9.4	-10.7	40	-13	-269.4	-615.6	58.5	-27.8	-26.5
20TH	216.33	-9.7	-30.7	1005	2827	-9.6	-10.9	39	-12	-259.8	-584.9	53.2	-25.4	-25.2
21ST	225.16	-9.9	-30.4	1005	2827	-9.9	-10.8	39	-13	-249.8	-554.5	48.1	-23.2	-23.9
22ND	233.99	-10.3	-30.1	1005	2827	-10.2	-10.6	38	-13	-239.6	-524.5	43.4	-21.0	-22.6
23RD	242.83	-10.6	-29.7	1005	2827	-10.5	-10.5	38	-13	-229.0	-494.8	38.9	-18.9	-21.3
24TH	251.66	-10.9	-29.3	1005	2827	-10.8	-10.4	37	-14	-218.1	-465.5	34.6	-17.0	-20.1
24TH	260.49	-11.2	-29.0	1005	2827	-11.2	-10.2	37	-14					

TABLE 7. SHEAR AND MOMENT DIAGRAMS :		RESORTS HOTEL CASINO, ATLANTIC CITY								GUST FACTOR 1.00				
WIND DIRECTION 320		CONFIGURATION A				REFERENCE PRESSURE 30.0 PSF								
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33									-206.9	-436.5	30.6	-15.1	-18.9
26TH	278.16	-11.5	-28.6	1005	2827	-11.5	-10.1	36	-15	-195.3	-407.9	26.9	-13.3	-17.7
27TH	288.66	-14.1	-33.5	1194	3360	-11.8	-10.0	36	-15	-181.2	-374.4	22.8	-11.3	-16.3
28TH	297.49	-12.2	-27.8	1005	2827	-12.2	-9.8	35	-16	-169.0	-346.6	19.6	-9.8	-15.1
29TH	297.49	-12.0	-27.9	1005	2827	-12.0	-9.9	36	-16	-156.9	-318.7	16.7	-8.3	-13.9
29TH	306.33	-12.3	-27.7	1005	2827	-12.2	-9.8	36	-16	-144.6	-291.0	14.0	-7.0	-12.7
30TH	315.16	-12.6	-27.6	1005	2827	-12.5	-9.8	36	-16	-132.0	-263.4	11.5	-5.8	-11.5
31ST	323.99	-12.8	-27.4	1005	2827	-12.8	-9.7	36	-17	-119.2	-236.0	9.3	-4.7	-10.3
32ND	332.82	-13.1	-27.3	1005	2827	-13.0	-9.7	36	-17	-106.1	-208.7	7.4	-3.7	-9.1
33RD	341.66	-13.4	-27.2	1005	2827	-13.3	-9.6	36	-18	-92.8	-181.5	5.7	-2.8	-7.9
34TH	350.49	-13.6	-27.0	1005	2827	-13.6	-9.6	36	-18	-79.2	-154.4	4.2	-2.0	-6.7
35TH	359.32	-13.9	-26.9	1005	2827	-13.8	-9.5	36	-18	-65.3	-127.5	2.9	-1.4	-5.5
36TH	368.16	-14.1	-26.8	1005	2827	-14.1	-9.5	35	-19	-51.1	-100.8	1.9	-.9	-4.3
37TH	376.99	-14.4	-26.6	1005	2827	-14.3	-9.4	35	-19	-36.7	-74.1	1.1	-.5	-3.0
38TH	385.82	-24.4	-42.4	1782	5013	-13.7	-8.5	39	-22	-12.4	-31.8	.3	-.1	-.9
ROOF	401.49	-12.4	-31.8	2276	4508	-5.4	-7.0	24	-9	0.0	0.0	0.0	0.0	0.0
TOP	421.50													

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 330 CONFIGURATION A

RESORTS HOTEL CASINO, ATLANTIC CITY
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00	- .8	- .6	79	222	-9.7	-2.6	-248	325	-437.7	-288.8	69.5	-110.7	-20.1
1ST	54.00	-7.5	-5.4	1194	3360	-6.2	-1.6	15	-21	-436.9	-288.2	53.9	-87.1	-20.5
2ND	64.50	-6.5	-4.8	1005	2827	-6.4	-1.7	19	-25	-429.5	-282.8	50.9	-82.6	-20.2
3RD	73.33	-6.8	-5.0	1005	2827	-6.7	-1.8	21	-29	-423.0	-278.1	48.4	-78.8	-20.0
4TH	82.17	-7.1	-5.2	1005	2827	-7.1	-1.8	24	-32	-416.3	-273.1	46.0	-75.1	-19.7
5TH	91.00	-7.4	-5.4	1005	2827	-7.4	-1.9	26	-35	-409.2	-267.9	43.6	-71.4	-19.3
6TH	99.83	-7.7	-5.7	1005	2827	-7.7	-2.0	28	-38	-401.7	-262.5	41.2	-67.9	-18.9
7TH	106.67	-8.1	-5.9	1005	2827	-8.0	-2.1	30	-41	-394.0	-256.8	39.0	-64.4	-18.5
8TH	117.50	-8.4	-6.1	1005	2827	-8.3	-2.2	32	-43	-385.9	-250.9	36.7	-60.9	-18.0
9TH	126.33	-8.7	-6.4	1005	2827	-8.7	-2.3	33	-46	-377.6	-244.8	34.5	-57.5	-17.4
10TH	135.16	-8.9	-6.8	1005	2827	-8.8	-2.4	37	-49	-368.9	-238.4	32.4	-54.2	-16.8
11TH	144.00	-8.9	-7.3	1005	2827	-8.8	-2.6	41	-50	-360.0	-231.6	30.3	-51.0	-16.1
12TH	152.83	-9.2	-7.4	1005	2827	-9.2	-2.6	38	-47	-351.1	-224.3	28.3	-47.9	-15.4
13TH	161.66	-11.4	-9.0	1194	3360	-9.5	-2.7	36	-45	-341.9	-216.9	26.4	-44.8	-14.6
14TH	172.16	-9.9	-7.7	1005	2827	-9.9	-2.7	33	-43	-330.6	-207.8	24.1	-41.3	-13.8
15TH	181.00	-10.3	-7.9	1005	2827	-10.2	-2.8	31	-41	-320.6	-200.1	22.3	-38.4	-13.1
16TH	189.83	-10.6	-8.0	1005	2827	-10.5	-2.8	29	-39	-310.4	-192.3	20.6	-35.6	-12.5
17TH	198.66	-10.9	-8.1	1005	2827	-10.9	-2.9	28	-37	-299.8	-184.3	18.9	-32.9	-11.8
18TH	207.50	-11.3	-8.2	1005	2827	-11.2	-2.9	26	-35	-288.8	-176.2	17.3	-30.3	-11.2
19TH	216.33	-11.3	-9.0	1005	2827	-11.3	-3.2	29	-37	-277.6	-167.9	15.8	-27.8	-10.6
20TH	225.16	-11.4	-8.9	1005	2827	-11.4	-3.2	28	-36	-266.2	-158.9	14.4	-25.4	-9.9
21ST	233.99	-11.5	-8.7	1005	2827	-11.5	-3.1	26	-35	-254.8	-150.0	13.0	-23.1	-9.2
22ND	242.83	-11.7	-8.4	1005	2827	-11.6	-3.0	24	-33	-243.3	-141.4	11.7	-20.9	-8.6
23RD	251.66	-11.8	-8.2	1005	2827	-11.7	-2.9	22	-32	-231.6	-133.0	10.5	-18.8	-8.0
24TH	260.49	-11.9	-7.9	1005	2827	-11.9	-2.8	20	-30	-219.8	-124.8	9.4	-16.8	-7.5

TABLE 7. SHEAR AND MOMENT DIAGRAMS : RESORTS HOTEL CASINO, ATLANTIC CITY
 WIND DIRECTION 330 CONFIGURATION A REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	Z		
25TH	269.33	-12.0	-7.7	1005	2827	-12.0	-2.7	18	-28	-207.9	-116.9	8.3	-14.9	-7.0
26TH	278.16	-14.5	-8.8	1194	3360	-12.1	-2.6	16	-26	-195.9	-109.3	7.3	-13.2	-6.5
27TH	288.66	-12.3	-7.1	1005	2827	-12.3	-2.5	14	-24	-181.4	-100.5	6.2	-11.2	-6.0
28TH	297.49	-12.0	-7.5	1005	2827	-12.0	-2.7	16	-26	-169.1	-93.4	5.3	-9.6	-5.6
29TH	306.33	-12.4	-7.4	1005	2827	-12.3	-2.6	16	-26	-157.0	-85.9	4.6	-8.2	-5.1
30TH	315.16	-12.7	-7.4	1005	2827	-12.7	-2.6	15	-26	-144.7	-78.5	3.8	-6.9	-4.7
31ST	323.99	-13.1	-7.3	1005	2827	-13.0	-2.6	14	-25	-131.9	-71.1	3.2	-5.6	-4.3
32ND	332.82	-13.4	-7.3	1005	2827	-13.4	-2.6	14	-25	-118.8	-63.7	2.6	-4.5	-3.8
33RD	341.66	-13.8	-7.2	1005	2827	-13.7	-2.6	13	-25	-105.4	-56.5	2.0	-3.5	-3.4
34TH	350.49	-14.1	-7.2	1005	2827	-14.1	-2.5	12	-24	-91.6	-49.2	1.6	-2.7	-3.0
35TH	359.32	-14.5	-7.1	1005	2827	-14.4	-2.5	12	-24	-77.5	-42.1	1.2	-1.9	-2.5
36TH	368.16	-14.8	-7.1	1005	2827	-14.8	-2.5	11	-24	-63.0	-35.0	.8	-1.3	-2.1
37TH	376.99	-15.2	-7.0	1005	2827	-15.1	-2.5	11	-23	-48.2	-27.9	.6	-.8	-1.7
38TH	385.82	-21.9	-11.3	1782	5013	-12.3	-2.3	17	-32	-33.0	-20.9	.3	-.5	-1.2
ROOF	401.49	-11.1	-9.6	2276	4508	-4.9	-2.1	15	-17	-11.1	-9.6	.1	-.1	-.3
TOP	421.50									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 340

RESORTS HOTEL CASINO, ATLANTIC CITY
CONFIGURATION A REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00									-442.6	613.1	-144.1	-109.2	22.1
1ST	54.00	-1.3	4	79	222	-16.4	1.7	111	373	-441.3	612.7	-111.0	-85.3	21.6
2ND	64.50	-10.9	12.0	1194	3360	-9.1	3.6	28	25	-430.3	600.8	-104.6	-80.8	21.0
3RD	73.33	-9.1	10.9	1005	2827	-9.1	3.9	30	25	-421.2	589.9	-99.3	-77.0	20.4
4TH	82.17	-9.1	11.6	1005	2827	-9.1	4.1	31	24	-412.1	578.2	-94.2	-73.3	19.9
5TH	91.00	-9.1	12.4	1005	2827	-9.0	4.4	32	24	-403.0	565.9	-89.1	-69.7	19.2
6TH	99.83	-9.1	13.1	1005	2827	-9.0	4.6	33	23	-394.0	552.8	-84.2	-66.2	18.6
7TH	108.67	-9.1	13.9	1005	2827	-9.0	4.9	34	22	-384.9	538.9	-79.4	-62.8	17.9
8TH	117.50	-9.1	14.6	1005	2827	-9.0	5.2	35	22	-375.9	524.3	-74.7	-59.4	17.2
9TH	126.33	-9.0	15.3	1005	2827	-9.0	5.4	35	21	-366.8	509.0	-70.1	-56.1	16.5
10TH	135.16	-9.0	16.1	1005	2827	-9.0	5.7	36	20	-357.8	492.9	-65.7	-52.9	15.7
11TH	144.00	-8.9	16.7	1005	2827	-8.8	5.9	36	19	-348.9	476.2	-61.4	-49.8	15.0
12TH	152.83	-8.7	16.6	1005	2827	-8.6	5.9	34	18	-340.2	459.6	-57.3	-46.8	14.3
13TH	161.66	-9.0	16.7	1005	2827	-8.9	5.9	33	18	-331.3	442.9	-53.3	-43.8	13.5
14TH	172.16	-11.0	20.1	1194	3360	-9.3	6.0	32	17	-320.2	422.8	-48.7	-40.4	12.7
15TH	181.00	-9.6	17.0	1005	2827	-9.6	6.0	31	17	-310.6	405.8	-45.1	-37.6	12.0
16TH	189.83	-9.9	17.2	1005	2827	-9.9	6.1	30	17	-300.7	388.6	-41.6	-34.9	11.3
17TH	198.66	-10.2	17.3	1005	2827	-10.1	6.1	29	17	-290.5	371.2	-38.2	-32.3	10.6
18TH	207.50	-10.5	17.5	1005	2827	-10.4	6.2	29	17	-280.0	353.8	-35.0	-29.8	10.0
19TH	216.33	-10.8	17.6	1005	2827	-10.7	6.2	28	17	-269.3	336.1	-32.0	-27.3	9.3
20TH	225.16	-10.7	17.4	1005	2827	-10.6	6.2	26	16	-258.6	318.7	-29.1	-25.0	8.7
21ST	233.99	-10.7	17.1	1005	2827	-10.7	6.1	24	15	-247.9	301.6	-26.3	-22.8	8.1
22ND	242.83	-10.9	16.9	1005	2827	-10.8	6.0	24	15	-237.0	284.7	-23.7	-20.6	7.5
23RD	251.66	-11.0	16.6	1005	2827	-11.0	5.9	23	15	-225.9	268.1	-21.3	-18.6	7.0
24TH	260.49	-11.2	16.3	1005	2827	-11.1	5.8	22	15	-214.7	251.8	-19.0	-16.6	6.5
		-11.3	16.1	1005	2827	-11.3	5.7	21	15					

TABLE 7. SHEAR AND MOMENT DIAGRAMS :														
WIND DIRECTION 340		RESORTS HOTEL CASINO, ATLANTIC CITY										GUST FACTOR 1.00		
CONFIGURATION A REFERENCE PRESSURE 30.0 PSF														
FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33									-203.4	235.7	-16.8	-14.8	6.0
26TH	278.16	-11.5	15.8	1005	2827	-11.4	5.6	20	14	-191.9	219.9	-14.8	-13.0	5.5
27TH	288.66	-13.9	18.4	1194	3360	-11.6	5.5	19	14	-178.1	201.5	-12.6	-11.1	5.0
28TH	297.49	-11.8	15.2	1005	2827	-11.8	5.4	18	14	-166.2	186.3	-10.9	-9.6	4.5
29TH	306.33	-11.6	14.6	1005	2827	-11.6	5.2	15	12	-154.6	171.7	-9.3	-8.2	4.2
30TH	315.16	-12.0	14.5	1005	2827	-11.9	5.1	14	12	-142.6	157.2	-7.9	-6.8	3.8
31ST	323.99	-12.3	14.4	1005	2827	-12.3	5.1	14	12	-130.3	142.8	-6.6	-5.6	3.5
32ND	332.82	-12.7	14.3	1005	2827	-12.6	5.0	14	12	-117.6	128.6	-5.4	-4.5	3.1
33RD	341.66	-13.1	14.1	1005	2827	-13.0	5.0	13	12	-104.6	114.4	-4.3	-3.6	2.8
34TH	350.49	-13.4	14.0	1005	2827	-13.3	5.0	13	12	-91.1	100.4	-3.3	-2.7	2.4
35TH	359.32	-13.8	13.9	1005	2827	-13.7	4.9	13	13	-77.4	86.5	-2.5	-2.0	2.1
36TH	368.16	-14.1	13.8	1005	2827	-14.1	4.9	12	13	-63.2	72.7	-1.8	-1.3	1.7
37TH	376.99	-14.5	13.7	1005	2827	-14.4	4.8	12	13	-48.8	59.0	-1.2	-.8	1.4
38TH	385.82	-14.8	13.6	1005	2827	-14.8	4.8	12	13	-33.9	45.5	-.8	-.5	1.0
ROOF	401.49	-22.3	22.8	1782	5013	-12.5	4.5	15	14	-11.6	22.7	-.2	-.1	.4
TOP	421.50	-11.6	22.7	2276	4508	-5.1	5.0	13	7	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : RESORTS HOTEL CASINO, ATLANTIC CITY
 WIND DIRECTION 350 CONFIGURATION A REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
GRND	0.00									-407.9	1088.9	-252.5	-100.6	36.5
1ST	54.00	-1.5	.3	79	222	-19.3	1.3	72	388	-406.4	1088.6	-193.7	-78.7	35.9
2ND	64.50	-12.6	23.6	1194	3360	-10.6	7.0	24	13	-393.7	1065.0	-182.4	-74.5	35.1
3RD	73.33	-10.1	21.2	1005	2827	-10.1	7.5	27	13	-383.6	1043.8	-173.1	-71.0	34.4
4TH	82.17	-9.7	22.4	1005	2827	-9.7	7.9	28	12	-373.9	1021.4	-164.0	-67.7	33.7
5TH	82.17	-9.3	23.7	1005	2827	-9.3	8.4	30	12	-364.6	997.7	-155.1	-64.4	32.9
6TH	91.00	-8.9	24.9	1005	2827	-8.9	8.8	31	11	-355.7	972.8	-146.4	-61.2	32.0
7TH	99.83	-8.5	26.2	1005	2827	-8.5	9.3	33	11	-347.2	946.7	-137.9	-58.1	31.0
8TH	108.67	-8.1	27.4	1005	2827	-8.1	9.7	34	10	-339.1	919.2	-129.6	-55.1	30.0
9TH	117.50	-7.7	28.7	1005	2827	-7.7	10.1	35	9	-331.4	890.6	-121.7	-52.1	28.9
10TH	126.33	-7.3	29.9	1005	2827	-7.3	10.6	36	9	-324.1	860.7	-113.9	-49.2	27.8
11TH	135.16	-6.8	31.1	1005	2827	-6.8	11.0	37	8	-317.3	829.5	-106.5	-46.4	26.6
12TH	144.00	-6.9	31.2	1005	2827	-6.8	11.0	36	8	-310.4	798.4	-99.3	-43.6	25.5
13TH	152.83	-7.2	30.9	1005	2827	-7.2	10.9	35	8	-303.2	767.5	-92.3	-40.9	24.3
14TH	161.66	-9.0	36.3	1194	3360	-7.6	10.8	34	8	-294.2	731.2	-84.5	-37.8	23.0
15TH	172.16	-8.0	30.2	1005	2827	-8.0	10.7	33	9	-286.2	701.0	-78.2	-35.2	22.0
16TH	181.00	-8.4	29.9	1005	2827	-8.3	10.6	32	9	-277.8	671.1	-72.1	-32.7	21.0
17TH	189.83	-8.7	29.6	1005	2827	-8.7	10.5	30	9	-269.1	641.5	-66.3	-30.3	20.0
18TH	198.66	-9.1	29.3	1005	2827	-9.0	10.4	29	9	-260.0	612.2	-60.8	-28.0	19.0
19TH	207.50	-9.4	29.0	1005	2827	-9.4	10.3	28	9	-250.6	583.3	-55.5	-25.7	18.1
20TH	216.33	-9.5	28.6	1005	2827	-9.5	10.1	27	9	-241.1	554.7	-50.5	-23.6	17.3
21ST	225.16	-9.7	28.3	1005	2827	-9.6	10.0	26	9	-231.4	526.4	-45.7	-21.5	16.5
22ND	233.99	-9.9	28.1	1005	2827	-9.8	9.9	26	9	-221.6	498.3	-41.2	-19.5	15.6
23RD	242.83	-10.1	27.9	1005	2827	-10.0	9.9	26	9	-211.5	470.4	-36.9	-17.6	14.8
24TH	251.66	-10.3	27.6	1005	2827	-10.2	9.8	26	10	-201.2	442.8	-32.8	-15.7	14.0
	260.49	-10.5	27.4	1005	2827	-10.4	9.7	26	10					

TABLE 7. SHEAR AND MOMENT DIAGRAMS :
WIND DIRECTION 350

RESORTS HOTEL CASINO, ATLANTIC CITY
CONFIGURATION A
REFERENCE PRESSURE 30.0 PSF

GUST FACTOR 1.00

FLOOR	HEIGHT	FORCE (KIPS)		AREA (SQ FT)		PRESSURE (PSF)		ECCEN (FT)		SHEAR (KIPS)		MOMENT (1000-FT-KIPS)		
		X	Y	X	Y	X	Y	X	Y	X	Y	X	Y	Z
25TH	269.33	-10.7	27.2	1005	2827	-10.6	9.6	26	10	-190.7	415.4	-29.1	-14.0	13.2
26TH	278.16	-13.0	32.0	1194	3360	-10.9	9.5	26	10	-180.0	388.2	-25.5	-12.4	12.4
27TH	288.66	-11.1	26.7	1005	2827	-11.1	9.4	26	11	-167.0	356.2	-21.6	-10.6	11.4
28TH	297.49	-11.0	26.3	1005	2827	-11.0	9.3	25	10	-155.9	329.6	-18.6	-9.1	10.6
29TH	306.33	-11.3	26.2	1005	2827	-11.2	9.3	25	11	-144.8	303.3	-15.8	-7.8	9.8
30TH	315.16	-11.5	26.2	1005	2827	-11.4	9.3	26	11	-133.6	277.1	-13.2	-6.6	9.0
31ST	323.99	-11.7	26.2	1005	2827	-11.6	9.3	26	12	-122.1	250.8	-10.9	-5.4	8.2
32ND	332.82	-11.9	26.2	1005	2827	-11.9	9.3	26	12	-110.4	224.7	-8.8	-4.4	7.4
33RD	341.66	-12.1	26.1	1005	2827	-12.1	9.2	27	12	-98.5	198.5	-6.9	-3.5	6.6
34TH	350.49	-12.4	26.1	1005	2827	-12.3	9.2	27	13	-86.4	172.4	-5.3	-2.7	5.7
35TH	359.32	-12.6	26.1	1005	2827	-12.5	9.2	27	13	-74.0	146.3	-3.9	-2.0	4.9
36TH	368.16	-12.8	26.0	1005	2827	-12.7	9.2	28	14	-61.4	120.2	-2.7	-1.4	4.0
37TH	376.99	-13.0	26.0	1005	2827	-13.0	9.2	28	14	-48.6	94.2	-1.7	-.9	3.1
38TH	385.82	-22.7	40.9	1782	5013	-12.7	8.2	30	17	-35.6	68.2	-1.0	-.5	2.2
ROOF	401.49	-12.9	27.2	2276	4508	-5.7	6.0	17	8	-12.9	27.2	-.3	-.1	.6
TOP	421.50									0.0	0.0	0.0	0.0	0.0

Table 8. Generalized Dynamic Properties of Prototype Structure

Symbol	Property	Units	Original (used for moments)			Revised 12/83 (used for accelerations)		
			x	y	z	x	y	z
m^*	Generalized Mass	$k\text{-ft-sec}^2$	3.180E8	3.180E8	1.460E7	3.180E8	3.180E8	1.460E7
k^*	Generalized Stiffness	$k\cdot\text{ft}$	1.351E9	4.45E8	4.716E7	1.395E9	3.140E9	4.716E7
ζ	Generalized Damping	C/C_{cr} ratio	0.01	0.01	0.01	0.01	0.01	0.01
f_o	Natural Frequency	Hz	0.328	0.190	0.286	0.333	0.500	0.286

- NOTES:
1. Generalized mass is approximately equal to moment of inertia, I
 2. Generalized stiffness is equal to the rotational stiffness k_θ of the approximating straight-line mode shape
 3. Damping values indicated are those most commonly assumed; some results are presented with additional values
 4. $f_o = \frac{1}{2\pi} \sqrt{\frac{k^*}{m^*}}$