Dissolved Solids Hazards in the South Platte Basin, Vol. I: Salt Transport in the River

by

Ramon V. Gomez-Ferrer and David W. Hendricks



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DISSOLVED SOLIDS HAZARDS IN THE SOUTH PLATTE BASIN

Volume I: Salt Transport in the River

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Ramon V. Gomez-Ferrer and D. W. Hendricks Department of Civil Engineering Colorado State University

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ABSTRACT

SALT TRANSPORT IN THE LOWER SOUTH PLATTE RIVER

This work demonstrates how river salinity may be characterized, in terms of both time and space variations. Fifteen years of daily and monthly salinity and flow data have been reduced to monthly, seasonal, and annual statistical characterizations for five river stations and three tributary stations for the lower South Platte River. From these characterizations distance profiles were plotted for flow, TDS, and salt mass flows.

The distance profiles and measurements of diversion flows, tributary flows, and point source discharges were the basis for a reach by reach materials balance analysis for four reaches of the South Platte River between Henderson and Julesburg. Return flows and return salt mass flows were computed as residuals.

The analysis showed that there is not a salt balance in the lower South Platte River. A net salt loss to the land of 380 tons per day occurs by irrigation.

The analysis provided can be the basis for a more comprehensive materials balance model. But the results can be used to estimate the impact of new water resources developments upon the salinity regime of the lower South Platte River.

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The research proposal upon which funding was based was developed by the junior author and Dr. Charles D. Turner. The report is based upon the Master of Science thesis of Ramon V. Gomez-Ferrer, completed in December 1981.

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TERMINOLOGY USED

- Return flows diffuse or non-point source return flows from irrigation which seep into a given river reach.
- Point source inflows discrete flows of water into a given river reach which include tributary flows, impoundment spillages, discharges from irrigation outlet flows, and municipal and industrial wastewater discharges.
- Diversion flows irrigation canal flows and any other flows diverted from a given river reach.
- Streamflow volume flow of water per unit time in a natural stream at a given station.
- Flow generic term meaning volume of water passage per unit of time. Units used herein are cubic meters per second (m^3/s) .
- Monthly flow flow of water averaged over a one month period. Units used are cubic meters per second (m³/s), i.e., cubic meters per month divided by seconds per month.
- Seasonal flow flow of water averaged over a season period of time. Units used are cubic meters per second (m³/s), i.e., cubic meters per three month season divided by seconds per season.
- Annual flow flow of water averaged over one year time period. Units used are cubic meters per second (m³/s), i.e., cubic meters per year divided by seconds per year.

Salt mass flow - mass flux of dissolved salts convected by flow of water. Units used are metric tons per day (T/d).

- Monthly salt mass flow flux of dissolved salts averaged over a one month period. Units used are metric tons per day (T/d), i.e., thousands of kilograms of total dissolved solids per month divided by days per month.
- Seasonal salt mass flow flux of dissolved averaged over a season period of time. Units used are metric tons per day (T/d), i.e., thousands of kilograms of total dissolved solids per three month season divided by days per season.
- Annual salt mass flow flux of dissolved salts averaged over a one year time period. Units used are metric tons per day (T/d), i.e., thousands of kilograms of total dissolved solids per year divided by days per year.

Chapter 1

INTRODUCTION

1.1 Background

Because water is a scarce resource in many arid and semi-arid regions of the world, it is often used and reused to the limit of either salinity increase or water availability after losses. The South Platte River Basin in Colorado is an example of the kind of water system found in such regions. Here the accumulation of dissolved solids due to intensive use and reuse is becoming a limiting factor for new water developments.

While salinity is often a rate limiting factor in development there has been little systematic attention given to understand the characteristics of the accumulation and transport of salt loads through developed river basins. Thus there is a need to know how to analyze these salinity characteristics, and then to use such analyses as tools to predict the effects of new development projects upon an existing salinity regime.

1.2 Objective

The first objective of this project is to demonstrate how river salinity may be characterized in terms of time variations and with distance along the stream. The second objective is to ascertain the role of factors, such as return flows, diversions, point source discharges, which shape this characterization. 1.3 Scope

The limits of this study are as follows:

 The salinity characterization was for the lower South Platte River between Henderson and Julesburg.

2) This study investigates phenomena affecting the stream and not upon processes external to it such as evapotranspiration, salinity pickup due to leaching, etc. The work does not encompass a basin-wide hydrologic model.

3) The study is empirical, utilizing published records for the period 1965-79.

1.4 Significance for the South Platte

Salinity increase in the South Platte River and its tributaries begins to be observed from below the mouths of the canyons where intensive abstraction starts for urban and agricultural uses. This activity extends along the system to the lower South Platte River at the Colorado-Nebraska state line. Because of this intensive water use the salinity concentrations in the stream systems, which occur naturally at the mouths of the canyons at levels below 100 mg/1, suffer nearly a twenty-fold increase toward the outlet of the watershed. These values are well above the 500 mg/1 recommended for drinking water supplies and fall into a level which may have adverse effects on many crops and requires careful management practices for irrigation.

In order to meet the increasing water demand in the basin, several water projects, such as the proposed Grey Mountain Project for the Cache La Poudre River or the authorized Narrows Dam Project for the lower South Platte River, are being considered to increase water yield,

while preserving compact requirements at the Colorado-Nebraska state line.

Additional measures being proposed to satisfy future demand include water conservation programs, increased recycling, exchange/ reuse between municipalities and agriculture, and improved management and operation of the existing systems.

Such projects are likely to further increase the concentration of total dissolved solids in the lower South Platte River, jeopardizing its continued use by downstream users.

So it is becoming advisable within the South Platte River Basin to assess how the proposed and contemplated water development projects will affect its salinity regime.

1.5 Past Studies

Salinity in streams has been of long-standing interest in the western United States, and has spawned a variety of project oriented studies. It is a critical concern in the Colorado River Basin where municipal and irrigation uses may be limited because of salinity increases caused by return flows from upstream diversions. This same problem exists in the Sevier River in Utah, the Rio Grande in New Mexico, the Salt River in Arizona, the San Joaquin River in California, and the Arkansas River in Colorado. A review of some of these problems can be found from different authors in the Proceedings of a National Conference on Managing Irrigated Agriculture to Improve Water Quality sponsored by U.S. Environmental Protection Agency and Colorado State University in 1972.

Many of the studies on these various systems are focused upon particular components, such as leaching, salinity in return flows,

in-stream salinity. Of particular interest is a five volume EPA report (1977) on prediction of mineral quality of irrigation return flows. The comprehensive studies in terms of salinity modeling are few. Hyatt (1970) has developed such a model for the Colorado River. Riley and Jurinak (1979) have outlined a comprehensive model for management purposes. Hendricks and Bagley (1969) have proposed a material balance salinity model which takes into account salt build up by consumptive use and pickup by leaching. Its application is demonstrated for annual data.

The salinity characteristics of the South Platte River have not been discerned in detail, although a variety of studies have addressed portions of the problem. Generally, the problem has just been described in narrative terms, such as in studies by Engineering Consultants Inc. (1974) or Hurr et al. (1975). Salinity has been also a concern in the 208 planning activities as can be seen in the Water Quality Management Plan for Larimer and Weld Counties, Colorado, prepared by Pitts et al. (1978).

1.6 Units

The units of expression used throughout this work for flows and salt mass flows are cubic meters per second and metric tons per day, respectively. These units have been used both for daily, monthly, seasonal and annual flow and salt mass flow values, in order to permit easy comparison of these values for different time periods.

Chapter 2

THE LOWER SOUTH PLATTE RIVER

2.1 The South Platte River Basin

The waters of the South Platte River are used very intensively for municipal and irrigation purposes. The irrigated land is estimated at 572,650 Ha (1,415,000 acres) (Bluestein and Hendricks, 1975). The annual native runoff of the South Platte and its tributaries averages about 1,673 MCM (1,355,919 acre feet) (Hendricks et al., 1977), which is augmented by about 460 MCM (373,122 acre feet) (Hendricks et al., 1977) of imported water. The native runoff varies widely, however, averaging only 1,039 MCM (842,040 acre feet) in 1953-56, and 2,347 MCM (1,902,680 acre feet) in 1970. Most of the discharge is snow melt, which occurs in the April-July period. Figure 2-1 is a map of the South Platte River Basin showing the tributary streams, major urban areas, and irrigated lands.

2.2 The Lower South Platte River

Figure 2-2 shows the lower South Platte River between Henderson and Julesburg, which was the portion of the river considered in this study. Of special interest are the gaging stations which are highlighted on the map.

Estimates of irrigated land in the study area, adjacent to the river, range from 123,000 Ha (304,000 acres) by Hurr et al. (1975) to 202,750 Ha (501,000 acres) by Bluestein and Hendricks (1975). Janonis and Gerlek (1977) also estimate about 202,350 Ha (500,000 acres). The



Figure 2-1. The South Platte River Basin (adapted from Hendricks et al., 1977).



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water diverted for irrigation use is about 4,931 MCM (3,997,831 acre feet) for 1970 for the South Platte Basin as a whole by Janonis and Gerlek (1977). They estimated irrigation water diversions for 1970 for the lower South Platte River at 1,264 MCM (1,025,120 acre feet) below Kersey and about 800 MCM (648,858 acre feet) from Kersey to above Denver. In this study the diversions between Henderson and Julesburg were computed to average 1,164 MCM (943,800 acre feet) (WPRS, 1979) for the period comprised by water years 1965 to 1977.

Figure 2-3 is a schematic diagram of the lower South Platte River showing gaging stations and point source inflows considered in this study. Diversions are not shown since they are more numerous.

2.2.1 <u>River flow measurements</u>

U.S. Geological Survey gaging stations are located at Henderson, Kersey, Weldona, Balzac, and Julesburg on the lower South Platte River. Daily flow records are available for each of these stations for various periods of time, but all gaging stations are well-established. The 1965-79 period is of interest for this study.

The daily flows from the USGS records for the period 1965-79 are summarized as monthly, seasonal, and yearly averages in the tables of Appendix D.

Daily records of specific electrical conductance are available since 1945 for Julesburg from the U.S. Geological Survey. Records of total dissolved solids as residue and sum of constituents are available also from monthly grab samples. The other stations provide records of monthly grab samples for TDS as residue, or TDS as sum of constituents, and EC. The salinity data are summarized in Table 4-1.





2.2.2 Tributaries and point source inflows

Most of the tributaries in the plains are ephemeral. They include Big Dry Creek, Crow Creek, Boxelder Creek, Lost Creek, Kiowa Creek, etc. They are not considered in this study. The perennial tributary streams are St. Vrain Creek, the Big Thompson River, the Cache La Poudre River and Lodgepole Creek. Gaging stations for the first three are located at their mouths at Platteville, LaSalle, and Greeley, respectively. Salinity and flow records are similar to those of the main stem of the South Platte. They are summarized also in the tables of Appendix D. The flows of Lodgepole Creek are summarized in the tables in Appendix E.

In addition to major tributaries the point source inflows considered include the South Platte Supply Canal, Jackson Lake Outlet Canal, Bijou N. 2 Outlet Canal, and the Prewitt Reservoir Outlet Canal. Their respective locations are seen in Figure 2-3. Flow records for these canals are summarized in Appendix E. The point source waste discharges (e.g. Gates Cycle Poultry, Stokley Van Camp, etc.) have been listed by Battelle (1974) and have been evaluated by Bluestein and Hendricks (1975). They are omitted from this study because they are small compared with other flows.

2.2.3 Diversions

There are over fifty diversions along the lower South Platte River having an aggregate annual diversion flow of nearly one million acre feet. The diversions are listed in Tables 2-1 through 2-4. The annual diversion flows for the period 1965-79 are listed also. The diversions are grouped by reach and the aggregate monthly diversions for each reach are shown in Appendix E.

Diversion	River						Wate	er Yea	r					
DIVEIBION	Mile	65	66	67	68	69	70	71	72	73	74	75	76	77
(USGS Gaging St.														
Henderson)	301.4												10.1	0 0
Brighton Canal	297.5	8.6	7.7	6.8	10.0	9.2	8.3	7.9	8.0	7.5	9.7	11.3	10.1	0.0
Lupton Bottom Canal												17.0	10.0	17 6
Syst.	291.9	19.9	17.4	14.2	20.3	18.9	18.7	18.5	15.7	16.2	17.2	1/.5	19.0	17.0
Platteville Canal	286.9	16.9	14.1	9.9	18.0	21.7	22.2	18.3	15.4	18.1	17.0	19.5	21.0	1/.1
Side Hill Canal										- /		F 0	E 7	6 1
(Inc. Meadow Island 1)	284.3	0.0	5.1	4.8	6.2	5.9	5.9	5.4	5.1	5.4	5.5	5.0	5.7	0.1
Platte Valley Canal											FF (15 1	F0 0	/.2 E
Svst.	283.7	5.5	23.7	48.7	44.7	51.1	48.9	47.2	56.5	37.3	55.4	45.4	30.2	10.2
Mutual Canal Syst.	279.7	12.1	7.5	8.8	12.2	12.7	11.4	11.0	10.2	9.0	10.9	11.1	11.2	10.5
Bucker Canal	278.2													
Farmers Independent			-											15 1
Canal	276.7	18.9	17.3	14.9	16.6	17.2	17.0	15.0	12.9	12.7	13.6	13.5	14.4	15.1
Western Mutual Ditch														16.6
Syst	272.2	21.1	14.3	22.3	26.5	22.7	21.0	20.3	19.1	15.1	19.0	20.1	21.9	10.0
Jay Thomas Canal	270.2	2.5	3.0	2.0	3.2	2.2	1.8	2.1	1.8	0.7	1.2	1.0	1.1	5.9
(St. Vrain Ck.														
confluence)	270.0										~ ~ ~	~ ~ ~	ac c	20.2
Union Canal Syst.	265.4	37.1	22.0	34.1	29.0	23.7	23.1	23.3	24.3	21.4	26.8	24.0	20.0	0.4
Godfrey Canal	262.3	6.5	8.9	8.6	12.1	8.2	7.0	6.4	10.3	6.5	1.8	8.5	0.0	9.4
(Big Thompson R.														
confluence)	260.4											~ ~ ~	ac a	21. 6
Lower Latham Canal	256.7	51.8	25.4	36.1	41.3	38.4	40.2	39.8	36.2	36.1	36.5	34.9	30.2	54.0
Patterson Canal	253.8	4.6	5.6	4.4	5.3	4.9	4.7	4.4	6.0	4.2	5.2	5.4	4.0).0 / E
Highland & Plum Canal	251.0	4.0	5.0	3.6	5.1	3.4	3.4	4.5	4.9	2.7	4.1	3.8	3.9	4.5
(Cache La Poudre R.														
confluence)	249.0													
(USGS Gaging St. Kerse	y)246.1													
Total annual reach	-									100.0	220.0	222 8	2/3 2	223 5
diversion flow		209.5	177.0	219.2	250.5	246.2	233.6	224.1	220.4	192.9	229.9	-5	243.2	

Table 2-1. Location and annual diversion flow in 1000 AF units of major diversions, water years 1965-77, Henderson-Kersey reach, South Platte River.

To obtain cubic meters per second (cms), multiply acre feet per year by the factor 3.911 x 10^{-5} . Source: Battelle (1974) and WPRS (1979)

Diversion	River	iver Water Year											. <u>.</u>	
	Mile	65	66	67	68	69	70	71	72	73	74	75	76	77
(USGS Gaging St. Kersey	7)246.1			<u></u>		<u></u>								
Hoover Canal	244.1													
Empire Canal Syst.	241.0	87.9	58.9	80.3	70.7	65.9	84.4	77.7	104.1	91.9	65.3	72.3	84.6	53.7
Riverside Canal Syst.	240.2	129.3	71.4	102.2	97.1	136.3	130.0	143.4	100.3	121.3	115.9	147.2	120.8	110.9
Bijou Canal Syst.	233.0	56.6	28.8	63.5	54.4	78.6	61.9	63.1	53.8	39.4	50.8	62.6	42.7	45.0
Jackson Lake Inlet														
Canal	225.5	58.8	28.8	43.5	22.8	40.8	27.1	17.2	58.2	20.2	32.8	43.3	43.8	39.6
Weldon Valley Canal	220.4	30.2	20.8	30.0	32.9	29.6	25.4	31.0	31.1	28.2	35.9	35.2	41.4	36.2
Fort Morgan Canal	210.0	27.6	27.0	43.3	47.2	48.1	43.0	39.1	37.7	38.8	56.7	63.7	55.3	51.3
(USGS Gaging St.														
Weldona)	206.7													
Total annual reach														
diversion flow		390.4	235.7	362.8	325.1	399.3	371.8	371.5	385.2	339.8	357.4	424.3	388.6	336.7

Table 2-2. Location and annual diversion flow in 1000 AF units of major diversions, water years 1965-77, Kersey-Weldona reach, South Platte River.

To obtain cubic meters per second (cms), multiply acre feet per year by the factor 3.911 x 10^{-5} . Source: Battelle (1974) and WPRS (1979)

Diversion	River	iver Water Year												
	Mile	65	66	67	68	69	70	71	72	73	74	75	76	77
(USGS Gaging									· · · · ·					,
St. Weldona)	206.7													
Devel & Snyder Improv.														
Co. Canal	199.0	4.2	15.3	4.4	4.2	3.8	3.7	3.5	4.8	4.4	5.9	6.7	4.1	3.6
Upper Platte &														
Beaver Canal	198.0	18.9	2.9	24.1	28.2	31.8	26.9	25.0	25.8	30.2	30.5	34.0	28.7	25.2
Tremont Canal	191.9	0.5	0.5	2.2	1.8	1.1	0.0	0.0	4.6	5.8	5.3	9.1	8.7	9.1
Lower Platte &														
Beaver Canal Syst.	190.1	26.1	10.0	19.8	16.2	10.6	23.4	17.1	13.0	22.5	19.0	23.6	17.4	18.1
Snyder Canal Syst.	185.2	0.3	0.0	0.5	1.1									
North Sterling Canal														
Syst.	179.4	114.3	49.4	81.6	85.0	108.4	113.3	120.2	106.2	105.5	78.4	123.9	120.0	104.6
Tetsel Canal	176.4	3.6	4.5	4.8	5.0	4.7	4.7	4.3	5.5	3.8	5.5	5.9	5.3	4.5
Prewitt Canal Syst.	176.2	55.0	37.7	50.7	37.4	54.3	48.1	51.8	35.3	57.7	47.9	40.7	35.7	37.8
(USGS Gaging St.														
Balzac)	173.9													
Total annual reach														
diversion flow		222.9	120.3	194.1	178.9	214.7	220.1	221.9	195.2	229.9	192.5	243.9	219.9	202.9

Table 2-3. Location and annual diversion flow in 1000 AF units of major diversions, water years 1965-77, Weldona-Balzac reach, South Platte River.

To obtain cubic meters per second (cms), multiply acre feet per year by the factor 3.911 x 10^{-5} . Source: Battelle (1974) and WPRS (1979)

Diversion	River Mile	Water Year												
		65	66	67	68	69	70	71	72	73	74	75	76	77
USGS Gaging St. Balzac	173.9										/		10.0	0.7
South Platte Ditch	172.3	7.7	6.3	7.3	10.9	9.6	11.9	9.1	8.4	9.5	11.4	14.5	12.3	9.7
Farmers Pawnee Canal	167.5	18.3	16.1	18.0	22.6	4.6	26.8	24.7	20.6	23.3	28.4	34.5	2/./	19.5
Davis Brothers Canal	166.5	2.7	2.3	1.9	1.9	1.2	3.7	1.5	1.1	1.5	2.1	1.5	1.1	1.0
Schneider Canal	161.9	5.8	5.0	6.1	11.2	9.4	9.3	8.0	7.0	6.4	11.6	10.6	11.2	9.4
Springdale Canal	158.6	7.2	4.3	5.5	4.8	5.0	8.0	8.2	4.7	6.1	6.2	8.3	6.8	4.8
Batten Canal	156.6													
Sterling #1 Irr. Co.													~~ ~	10.0
Canal	155.3	14.7	22.9	17.9	21.8	19.6	20.8	22.6	19.7	19.5	26.1	26.9	28.2	12.8
Wenderson & Smith Canal	152.4	2.0	2.1	1.7	2.2	2.5	2.8	2.5	2.5	2.4	2.8	2.5	3.3	2.6
Storling #2 Canal	151.6	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.0	0.0	0.0	0.0	0.4	0.3
Sterring #2 Ganal	150 2	5.4	4.5	4.0	3.7	3.9	5.2	5.4	3.8	5.0	7.9	6.8	4.9	4.7
Low Line Canal	130.2													_ /
Blavo & J. B. Canal	144.7	0.0	4.5	7.1	7.8	7.5	6.5	4.1	5.5	6.4	5.0	8.0	5.2	7.4
Syst. Formers Canal	143.7	1.7	0.9	1.6	0.9	2.4	2.3	1.7	1.3	1.1	0.7	1.6	1.1	0.6
Tliff & Dlatte Valley	1-3.7													
Canal System	141.0	15.9	12.5	12.2	13.3	12.4	16.7	15.3	13.5	14.6	19.8	20.8	9.9	13.4
Lana Tree Canal	137.6	4.0	2.4	5.5	4.0	4.0	2.5	2.2	2.2	1.3	2.9	2.6	1.8	0.1
Douell & Harmony #2	13/10												~ <	<i>,</i> -
Copol Syst	133.1	3.1	3.9	3.7	3.4	3.1	4.0	3.2	2.6	5.2	3.6	3.8	3.6	4./
Pameer Canal	131.5	0.9	1.3	1.1	1.1	0.8	1.4	0.9	0.8	0.3	1.5	0.9	1.3	1./
Chambang Canal	127 7	3.0	0.0	1.5	2.1	4.6	5.8	5.4	3.7	4.0	3.7	0.1	0.0	0.0
Liambers Canal	12/ • /	5.0												
Julesburg Irr. District	. 125 6	15 2	20.7	30 1	27.3	35.1	54.8	20.4	27.9	40.1	32.5	53.7	33.3	41.3
Jumbo Syst.	123.0	40.2	20.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.5	0.9	2.6	1.5
Tamarack Canal	121.0	0.0	0.0	0.0	0.0	0.0								
Settlers Ditch	11/.5	~ 7	~ ~	07	0.8	1.0	07	0.0	0.6	0.0	0.7	1.2	1.0	0.4
Red Lion Canal	109.8	0.7	0.0	6.0	6.0	5.6	57	2 6	3.3	7.1	6.8	5.9	1.1	4.0
Peterson Canal	104./	4.5	2.4	0.0	4.0	2.0	3.7	3 1	3.4	3.0	4.8	4.2	2.8	3.9
South Reservation Canal	99.4	2.9	2.8	3.1	2.2	1.6	2.0	2 1	2.3	1.6	3.1	2.5	2.6	2.4
Liddle Irr. System	96.6	1.4	1.4	2.0	2.1	1.0	0 1	0.0	0.2	0.0	1.2	0.3	0.3	0.0
Carlson Canal	94.8	0.5	0.3	1.5	0.5	0.5	0.1	0.0	0	0.0				
(USGS Gaging St.														
Julesburg)	86.6													
Total annual reach			110 0	100 1	160 0	126 4	10/ /	143 2	135.1	158.4	183.3	212.1	162.5	146.2
diversion flow		14/.0	110.0	123.1	149.0	150.0	194.4	14312						

Table 2-4. Location and annual diversion flow in 1000 AF units of major diversions, water years 1965-77, Balzac-Julesburg reach, South Platte River.

To obtain cubic meters per second (cms), multiply acre feet per year by the factor 3.911×10^{-5} . Source: Battelle (1974) and WPRS (1979)

Chapter 3

METHODOLOGY

In order to characterize river salinity in the lower South Platte River and to ascertain the role of factors, such as return flow, diversion flows, point source discharges, which shape this characterization, the research utilized the following approach:

1) Verification of an empirical relationship between in-stream salt mass and flow for five river stations in the South Platte and three tributaries, using published data.

2) Application of the relationships developed to characterize the salt transport at each river station in terms of space and time.

3) Materials balance analysis of water flows and salt flows to and from each four reaches considered.

3.1 In-Stream Salt Mass Flow Relationships

Salinity is commonly characterized in the water field in terms of total dissolved solids (TDS) as residue. Because specific electrical conductance (EC) data are more abundant than total dissolved solids in the study area, we have obtained first total dissolved solids-specific electrical conductance relationships for each river station. A regression analysis between TDS and EC was done with the data available to ascertain the well-established linear relationship between these parameters in the river stations of the South Platte. All EC values were then converted to total dissolved solids as residue using the established relationships, so that all salinity calculations following are performed using the larger data base of EC values, but the results will be expressed in terms of total dissolved solids.

Once all EC values were converted to TDS values, a relationship between salt mass and water flow was sought. Although it is well-known in practice that such relationship exists, there are several possible forms of the relationship. Arithmetic, semi-log, log-log, reciprocal, power series, and exponential forms have been proposed in past studies, as reviewed by Lane (1975). The log-log form is the more commonly form used, however, and thus this form and the intuitive arithmetic form were compared in this study.

The time of year has been shown also in past studies to affect the salinity-flow relationship, as illustrated by Lane too. This was handled here by partitioning the data into four three-month periods, and performing the statistical analysis for each one of these periods. The four periods adopted are referred to as fall season, winter season, spring season and summer season respectively, and each comprised the following months:

- Fall: October, November and December
- Winter: January, February and March
- Spring: April, May and June
- Summer: July, August and September

The appropriateness of the log-log form of the salt mass-water flow relationship for each season for river stations in the lower South Platte River was tested for the Julesburg station, using fifteen years of daily data. A regression analysis was performed for each season, and acceptability was based on the values of the R^2 coefficients and inspection of the plots of data. The coefficients for the regression

model were then obtained for the five river stations in the South Platte and the three tributaries, for each season, using the more limited data set of monthly grab samples available. These regression lines were used then in the salt transport characterization.

The statistical analysis described above was performed using Minitab II. Minitab II is a statistical computing system developed by the Statistical Department of the Pennsylvania State University and available at Colorado State University Computer Center Library, which is specially useful for regression analysis. The data used in the statistical analysis were taken from U.S. Geological Survey published records for the period 1962-79. Summaries of the data used, together with a discussion of the results of the analysis are presented in Section 4.1.

3.2 Salt Transport Characterization

Using daily flow as an argument, the log salt mass-log flow relationships established previously for each season were used to compute daily salt mass flows at each river station considered in the South Platte, i.e. Henderson, Kersey, Weldona, Balzac and Julesburg. The river stations at the mouth of the three major tributaries, i.e. Platteville on the St. Vrain Creek, La Salle on the Big Thompson River, and Greeley on the Cache La Poudre River, were analyzed simultaneously. Daily records of flow published by the U.S. Geological Survey for the period comprising water years 1965 to 1979 were used in the characterization.

The computed daily salt mass flow values were averaged over the month, the season and the year. Monthly, seasonal and annual flow values were computed at the same time, and flow weighted monthly,

seasonal and annual average concentration of total dissolved solids were obtained also dividing the corresponding salt mass flows and water flows. The monthly, seasonal and annual time increments were chosen to analyze the salt transport charcterization with time because they are commonly used in planning. The salt transport characterization with distance was facilitated by plotting the annual and seasonal computed flow, salt concentration and salt mass flow values versus river mile. The results of the salt mass characterization are discussed in Section 4.2.

3.3 Materials Balance Analysis

The materials balance analysis was performed for all river reaches considered by taking into consideration all the water flows and salt mass flows to and from the reach. Figure 3-1 shows a diagram of a typical river reach in the South Platte River. A certain streamflow Q_i carrying a salt concentration S_i , enters the reach at its upper end, and as it moves along the reach some diversion flows $(QD_{i,k})$, point source inflows $(QP_{i,i})$ and return flows (QR_i) , carrying salt concentrations SD_{i,k}, SP_{i,j}, SR_i, respectively, occur. As a result, a stream flow Q_{i+1} , carrying a salt concentration S_{i+1} , leaves the reach at its lower end. Diversion flows comprise flows abstracted for agriculture, either for direct use during the irrigation season or for storage at out of season periods. Point source inflows include tributary flows, impoundment spillages, discharges from irrigation outlet canals, and municipal and industrial discharges. Return flows include both unaccounted surface and subsurface agriculture return flows, and excess surface and subsurface water runoff.



Materials balance computations

1. Reach flow balance for computation of return flow to reach

$$QR_{i} = Q_{i+1} - Q_{i} + \sum_{k=1}^{K} QD_{i,k} - \sum_{j=1}^{J} QP_{i,j}$$
(1)

2. Reach salt balance for computation of return salt mass flow to reach

$$(QR_{i})(SR_{i}) = (Q_{i+1})(S_{i+1}) - (Q_{i})(S_{i}) + \sum_{k=1}^{K} (QD_{i,k})(SD_{i,k}) - \frac{J}{j=1} (QP_{i,j})(SP_{i,j})$$

$$(2)$$
Notation

$$Q_{i} : \text{ Streamflow at the upstream end of the reach i}$$

۷i Streamflow at the downstream end of the reach i Q_{i+1} : Flow in diversion k of reach i $QD_{i,k}$: Flow in point inflow j of reach i QP_{i,i}: Flow in return flows of reach i QR_i : TDS concentration of upstream end of reach i s, : TDS concentration of downstream end of reach i s_{i+1} : TDS concentration in diversion k of reach i $SD_{i,k}$: TDS concentration in point inflow j to reach i SP_{i,j}: TDS concentration in return flows to reach i SR_i :

Figure 3. Flow diagram of a typical river reach in the South Platte showing material balance computations for water and salt.

The lower South Platte was divided into four reaches linking the gaging stations considered, i.e. reach one: Henderson-Kersey, reach two: Kersey-Weldona, reach three: Weldona-Balzac, reach four: Balzac-Julesburg. Figure 2-3 in Section 2-2 shows a schematic representation of the four reaches considered, and it depicts all point source inflows considered. Diversion flows from each reach considered, are listed in Tables 2-1 to 2-4.

All flows but the return flows are known, therefore the return flows to the reach were computed as the residual of all other known inflows and outflows to the reach, using Equation (3-1) in Figure 3-1. Salt mass flows associated with streamflows entering and leaving each reach were the result of the analysis in Section 3-2. Also, the salt mass flows associated with streamflows of the three major tributaries, i.e. St. Vrain Creek, Big Thompson River and Cache La Poudre River, were computed in Section 3-2. Salt mass associated with diversion flows are not known, but it can be assumed that the salinity associated with all diversion flows from a reach in a given time period has a concentration close to the average concentration of the reach streamflow for the same time period. For the other point source inflows, the salt mass flows associated with them are not known, but since their flows are small, a simplifying assumption or an educated guess was made so that we could proceed with the analysis. The values used to characterize the salinity associated to these point source inflows are as follows:

a) <u>South Platte Supply Canal</u>. It discharges excess water from the Colorado-Big Thompson transbasin scheme. A constant value of 50 mg of TDS/ℓ was been chosen to characterize the discharge, based on water

quality records of CBT import flows at entrance of Olympus Tunnel at Lake Estes. It was later discovered that this assumption is not true because the canal receives return flows. But the effects on the computational results using the value are minor because the canal flows are low relative to other flows in the reach.

b) Jackson Lake Outlet Canal and Prewitt Reservoir Outlet Canal. The flow weighted average salinity concentration of the flows diverted to the lake by the Jackson Lake outlet canal or to the reservoir by the Prewitt Canal system were computed for each period September through August of the following year. Each value was used to characterize any discharge occurring during the corresponding January to December period. The salinity concentrations of the monthly flows diverted by the Jackson Lake inlet canal were taken equal to the salinity associated with the diversion flows from the reach that month. The salinity concentration of the monthly flows diverted to the Prewitt Reservoir were taken equal to those occurring at the Balzac gaging station.

c) <u>Bijou #2 Outlet and Lodgepole Creek</u>. Salt concentrations were assumed to be in the order of 1000 mg/ ℓ .

The salt mass associated with the return flows was then obtained as the residual of all other salt mass flows to and from the reach, using Equation (3-2) in Figure 3-1. Flow weighted average salt concentration in the return flows was computed next dividing the salt mass flow and the water flow. Monthly, seasonal and annual values of water flow, salt concentration and salt mass flow were computed to characterize the return flows to each reach. Plots of average annual salt mass flows and water flows to and from each reach were prepared to
illustrate the findings of the materials balance analysis. Also, plots of average annual and seasonal salt mass flow versus water flow for return flows to each reach were made to depict what relationship best relates them. The results of the materials balance analysis is discussed in Section 4.3.

Chapter 4

RESULTS

There are three categories of results: (1) empirical verification of in-stream functional relationships between salt mass and flow, (2) characterization of salt flows in the South Platte River, and (3) materials balance of water flows and salt flows for four reaches. The latter two tasks are done in terms of space and time, reach by reach, using four river reaches between Henderson and Julesburg. The time increments used were the month, season, and year for the period comprising water years 1965-1979.

4.1 In-Stream Salt Mass-Flow Relationships

Because total dissolved solids data are limited and specific electrical conductance data are abundant a TDS-EC relationship was established for each station. From these relationships all EC data were converted to TDS data. The latter data were used in all statistical analyses involving salinity.

Once all EC data were converted to TDS data a salt mass-flow relationship was sought. Fifteen years of daily records at the Julesburg station were used to test already well-known salt mass-flow relationships. From this testing process the relationship, log (salt mass) = A + B log (flow), was found to have the highest regression coefficient.

After establishing the above regression model for Julesburg its coefficients A and B were ascertained for the stations Henderson,

Kersey, Weldona, Balzac and Julesburg in the main stem of the river, and for tributary stations, Platteville, La Salle, and Greeley, at the mouths of St. Vrain Creek, the Big Thompson River and the Cache La Poudre River, respectively.

4.1.1 TDS-EC relationships

The well-established relationship between TDS and EC has the form:

$$TDS = \alpha + \beta \cdot EC \tag{4-1}$$

This relationship was obtained by regression analysis for each of the five South Platte River stations and the three tributary stations.

Table 4-1 gives the regression coefficients α and β and summarizes the relevant statistical data, including range, median, mean, and standard deviation for each parameter. The R² coefficient and number of cases used are seen also. Flow data are shown for reference purposes. Since the TDS-EC relationship sometimes has the form, TDS = $\beta \cdot EC$, this alternate form is shown, too.

Table 4-1 shows the relationship for two data sources for the TDS parameter: (1) TDS as residue, and (2) TDS as sum of constituents. Plots of TDS versus EC data for both "TDS as residue" and "TDS as sum of constituents" are shown in Appendix A.

The "TDS as sum of constituents" data were converted to "TDS as residue" data for the stations Platteville, La Salle, Greeley, and Weldona, using empirical ratios derived in this work. This was done to enlarge the data base for these stations. The "TDS as residue" was used as the parameter of choice in the regression equation because it gave higher R^2 coefficents.

		TDS as	RESI	DUE	VERSUS	CONDUC	TIVITY			TDS	as SUM	OF C	ONSTIT	UENTS	VERSUS	CONDUC	CTIVITY	
RIVER	S	TATISTICS	OF DAT	A		TDS	(R) ^{1/_} α	+ β * E0	:	S	TATISTICS	OF DAT	'A		TDS (sc) ^{2/} α	'+β' * I	CARTO
STATION	PARAMETERS	RANGE	MEDIAN	MEAN	ST.DV.	α	β	R ²	CASES USED	PARAMETERS	RANGE	MEDIAN	MEAN	ST.DV.	α'	β'	R [∠]	USED
	TDS(R) (mg/1)	181-980	697	674	195	14	0.614	0,967	94	TDS (SC) (mg/1)	239-823	678	581	215	-7	0.617	0,998	15
S.P.R.	EC	308-1470	1120	1031	313	Plott Fl	ed Point GURE A -	s shown 1 (a)	in	EC (µmho/cm)	401-1350	1100	953	348	Plot I	ted Poi IGURE A	nts sho - 1 (b	wn in)
HENDERSON	FLOW (m ³ /s)	0.59-191	5.1	12.1	24.0	Regre	ession li intercept	ne for (: 0.627 EC	0,0)	FLOW (m ³ /s)	3.3-108	8.4	19.6	27.3	Regre Ti	ession 1 inte DS(SC) =	ine for rcept: 0.611	(0 ,0) EC
	TDS(R) (mg/1)	203-1703	1099	1090	264	-127	0.873	0.974	143	TDS(SC) (mg/1)	185-1550	1015	998	244	-112	0.792	0.973	130
ST.V.C.	EC (µm,ho/сm)	315-2000	1440	1394	299	Plot F	ted Point IGURE A -	ts shown - 2 (a)	in	EC (µmho/cm)	315-2000	1450	1401	304	Plot F	ted Poin IGURE A	ts show - 2 (b)	n in
PLATTEVILLE	FLOW (m ³ /s)	1.1-50.4	4.3	5.9	7.2	Regr	ession 1 inter TDS(R) =	ine for (rcept: 0.786 EC	(0,0)	FLOW (m ³ /s)	1.1-39.1	4.3	5.7	6.4	Regr T	inter DS(SC) =	cept: 0,716	EC
	TDS(R) (mg/1)	220-2441	1842	1701	460	-172	0.956	0.959	106	TDS (SC) (mg/1)	195-2160	1630	1491	417	-144	0.842	0.958	96
B.T.R.	EC (umho/cm)	325-2580	2100	1958	471	Plot F	ted Poin IGURE A	ts shown - 3 (a)	in	EC (µmho/cm)	325-2580	2100	1943	486	Plot F	ted Poir IGURE A	nts show - 3 (b)	m in
LA SALLE	FLOW (m ³ /s)	0.10-24.2	2.1	2.9	3.4	Regr	ession 1 inte TDS(R) =	ine for (rcept: 0.873 EC	(0,0) :	FLOW (m ³ /s)	0.21-24.2	2.1	3,1	3.5	Regr 1	ession inter DS(SC) =	line for cept: = 0.772	•(0,0) EC
	TDS(R) (mg/1)	183-1840	1416	1334	309	-89	0.848	0.943	150	TDS (SC) (mg/1)	169-1620	1290	1205	287	-86	0.785	0.957	117
C.L.P.R.	EC (µmho/cm)	277-2350	1755	1680	354	Plot F	ted Poin IGURE A	ts shown - 4 (a)	in	EC (µmho/cm)	277-2140	1750	1644	358	Plot F	IGURE A	nts show - 4 (b)	m in)
GREELEY	FLOW (m ³ /s)	0.18-54.9		4.0	7.9	Regr	ession 1 inte TDS(R) =	ine for rcept: 0.797 E	(0,0) C	FLOW (m ³ /s)	0.23-54.9	2.6	4.4	8.2	, Kegi	ression inte TDS(SC)	line fo: rcept: = 0.735	r(0,0) EC

Table 4-1. Total dissolved solids - conductivity relationhips for five stations in the South Platte River and three tributary stations.

1/ TDS (R) is TOTAL DISSOLVED SOLIDS as RESIDUE

2/ TDS (SC) is TOTAL DISSOLVED SOLIDS as SUM OF CONSTITUENTS

		TDS as	RESID	UE V	ERSUS	CONDU	CTIVITY			TDS	as SUM	OF CO	NSTITU	IENTS	VERSUS	CONDU	CTIVITY	
RIVER	SI	TATISTICS	OF DATA	·		TD	s (R)1/	= α + β	* EC	ST	TATISTICS	OF DATA			TDS	(sc) ^{2/}	= α'+β'	* EC
STATION	PARAMETERS	RANGE	MEDIAN	MEAN	ST.DV.	α	β	R ²	CASES USED	PARAMETERS	RANGE	MEDIAN	MEAN	ST.DV.	α'	β١	R ²	CASES USED
	TDS(R) (mg/1)	373-1530	1290	1210	271	-137	0.859	0.981	61	TDS (SC) (mg/1)	226-1410	1120	1083	211	-61	0.753	0.875	67
S.P.R. Kersey	EC (µmho/cm)	558-1920	1670	1568	313	Plot F	ted Poir IGURE A	nts show - 5 (a)	m in	EC (µmho/cm)	370-1890	1600	1519	262	Plott Fl	ted Poin IGURE A	ts show - 5 (b)	m in
	FLOW (m ³ /s)	1.2-250	12.7	25.1	45,8	Regr	ession 1 inte TDS(R) =	line for ercept: = 0.775	• (0,0) EC	FLOW (m ³ /s)	1.5-317	14.0	19.3	38.4	Regre TI	ession 1 inte DS(SC) =	ine for cept: 0.714	(0,0) EC
	TDS(R) (mg/1)	414-2620	1381	1420	312	-133	0.895	0,900	115	TDS (SC) (mg/1)	375-2240	1250	1278	273	-91	0.791	0.896	105
S.P.R. WELDONA	EC (µmho/cm)	598-2870	1700	1736	330	Plot F	ted Poin IGURE A	nts show - 6 (a)	vn in)	EC (µmho/cm)	598-2800	1700	1730	327	Plot F	ted Poir IGURE A	nts show - 6 (b)	m in
	FLOW (m^3/s)	1.2-311	9.3	16.5	34.5	Regr	ession int TDS(R)	line for ercept: = 0.821	r (0,0) EC	FLOW (m ³ /s)	1.2-311	9.7	17.3	36.2	Regr T	ession I inte DS(SC) =	rcept: = 0.741	EC
	TDS(R) (mg/1)	548-1590	1460	1407	206	-149	0.879	0.977	58	TDS (SC) (mg/l)	1080-1560	1350	1352	125	-374	0.966	0.959	24
S.P.R. BALZAC	EC (µmho/cm)	787-1980	1830	1770	232	Plot F	ted Poi	nts sho - 7 (a	wn in)	EC (µmho/cm)	1520-2020	1795	1786	127	Plot F	ted Poin IGURE A	nts shor - 7 (b)	wn in)
	FLOW (m ³ /s)	0.19-110	3.7	7.2	17.3	Regi	ession int TDS(R)	line fo: ercept: = 0.796	r (0,0) EC	FLOW (m ³ /s)	0.22-28.1	3.3	6.6	7.6	Regr T	ession internet DS(SC)	line fo: ercept: = 0.758	r (0,0) EC
	TDS (R) (mg/1)	508-1890	1555	1479	278	-16	0.803	0.898	134	TDS (SC) (mg/1)	469-1860	1500	1437	247	- 39	0.729	0.857	79
S.P.R. JULESBURG	EC (µmho/cm)	738-2500	1940	1862	328	Plot	ted Poi FIGURE A	nts sho - 8 (a	wn in)	EC (µmho/cm)	738-2500	2000	1917	313	Plot F	ted Point IGURE A	nts sho - 8 (b	wn in)
	FLOW (m ³ /s)	0.31-279	7.1	18.5	36.1	Reg	ression int TDS(R)	line fo ercept: = 0.794	r (0,0) EC	FLOW (m ³ /s)	0.31-279	5,1	16.2	36.4	Regr 1	ession int DS(SC)	line fo ercept: = 0.749	r (0,0) EC

Table 4-1. (continued)

is TOTAL DISSOLVED SOLIDS as RESIDUE <u>1</u>/ TDS (R)

2/ TDS (SC) is TOTAL DISSOLVED SOLIDS as SUM OF CONSTITUENTS

The R^2 coefficients for the TDS-EC regression equations were uniformly high for all stations, as seen in Table 4-1. It should be noted also that, although the α and β coefficients are in the same range for the various stations, they are, nevertheless, unique.

4.1.2 Deriving a Salt Mass-Flow Relationship

Although it is well known in practice that a relationship exists between salt mass and flow there are several possible forms of the relationship. In this work only the arithmetic and log-log salt massflow regression equations were compared. This was done by computing the correlation coefficients for fifteen years of daily data grouped into seasons, as outlined in Section 3.1, for the Julesburg station. The results of the comparison are shown in Table 4-2. Because the R coefficients were slightly higher for the log-log form for all seasons, this form was selected for use. It is expressed:

$$\log(\text{salt mass}) = A + B \log(\text{flow}) \tag{4-2}$$

Table 4-2. Comparison between correlation coefficients for arithmetic and log-log forms of salt mass-flow data vectors at Julesburg.

	R, correlatio	n coefficient
Season	Arithmetic	Log-log
Fall	0.996	0.997
Winter	0.989	0.993
Spring	0.974	0.992
Summer	0.908	0.993

Figure 4-1 shows four log(salt mass) versus log(flow) plots by season for the Julesburg station. The specific log-log regression equations are seen also in each plot, along with the R^2 regression coefficients and number of cases used. It should be noted that the



Figure 4-1. Salinity mass-flow, daily data used in regression analysis, water years 1965-79, South Platte River at Julesburg.

log-log plot for spring appears to be a discontinuous linear function, i.e. there are two-linear equations. For simplicity in this work the function was handled as a single straight line function for all seasons. But the accuracy of the salt mass-flow relationship would be improved if it was broken into two equations for the spring season.

Table 4-3 shows in tabular format the information seen in the plots of Figure 4-1. In addition, Table 4-3 summarizes the statistics of the basic supporting data, i.e. total dissolved solids and flow.

Inspection of Table 4-3 shows that the highest TDS concentrations occur with the very low flows of fall and winter, as might be expected. Lower TDS concentrations, on the other hand, are seen to accompany the runoff flows of spring and early summer.

Visual inspection of the seasonal plots of Figure 4-1 and the statistical summaries in Table 4-3 support strongly the use of Equation (4-2). Furthermore its use is improved markedly by the seasonal resolution (as compared with annual resolution).

4.1.3 <u>Coefficients of Salt Mass-Flow Regression Model for Other</u> <u>Stations</u>

After verification of Equation (4-2), based upon the abundant data available at the Julesburg station, its coefficients A and B were obtained for the other stations, for which data were more limited. Table 4-4 gives the A and B coefficients by season for the eight stations, including Julesburg, along with the R^2 coefficients and number of cases used. For the South Platte stations, i.e. Henderson, Kersey, Weldona, Balzac, and Julesburg, the R^2 regression coefficients are above 0.9. For the tributary stations, i.e. Platteville, La Salle, and Greeley, the R^2 values are generally above 0.8, with a low value of

	REGRESSIO	N EQUATION	: LO	G ₁₀ (S	ALT MAS	s) <u>1/</u> =	A + B * L()G ₁₀ (F	LOW) ^{2/}
CEACON		SO	UTH PLA	TTE R	IVER A	Γ JULESB	URG		
SEASUN		STATISTICS	OF DAT	A		Δ	B	_p 2	CASES
	PARAMETERS	RANGE	MEDIAN	MEAN	ST.DV.	A	D	К	USED
TALL	TDS (mg/1)	1116-2730	1574	1577	163	2.18154	0.937696	0.994	1138
FALL	FLOW (m ³ /s)	.0.28-46.4	5.8	10.5	10.5	Plott F	ed Points IGURE 4 -	shown 1 (a)	in
WINTED	TDS (mg./1)	835-2610	1574	1563	176	2.21865	0.910939	0.986	1186
WINIER	FLOW (m ³ /s)	1.8-71.1	9.5	14.5	11.8	Plott F	ed Points IGURE 4 -	shown 1 (b)	in
CDDINC	TDS (mg/1)	428-2024	1454	1353	316	2.17265	0.878146	0.985	1222
OFRING	FLOW (m ³ /s)	0.54-850	8.2	34.2	65,5	Plott F	ed Points IGURE 4 -	shown 1 (c)	in
CIDAGED	TDS (mg/1)	263-1783	1462	1431	202	2.11175	0.932480	0.987	1192
SUMMER	FLOW (m ³ /s)	0.31-253	1.5	7.3	17.7	Plott F	ed Points IGURE 4 -	shown 1 (d)	in

Table 4-3. Salinity mass-flow regression results using daily records for the South Platte River at Julesburg, water years 1965-79.

 $\frac{1}{2}$ Metric tons of total disolved solids per day

<u>2</u>/ m³/s

					REGRES	SION EQU	JATION :	LOG1	0 (SAL	Γ MASS) <u>1</u> / =	A + B * L(06 ₁₀ (FLO	w).2/					
	(1)	SO	UTH PLAT	TE RI	VER AT	HENDERS	SON		,	(2)	ST	VRAIN	CREEK	NEAR	PLATTEVI	LLE		
SEASON		STATISTICS	OF DAT	ľA.			D	_p 2	CASES		STATISTICS	OF DAT	A			B	_R 2	CASES
	PARAMETERS	RANGE	MEDIAN	MEAN	ST.DV.	A	Б	ĸ	USED	PARAMETERS	RANGE	MEDIAN	MEAN	ST.DV.				USED
	TDS (mg/1)	498-892	757	747	92	1.88972	0.86651	0.983	34	TDS (mg/1)	868-1619	1121	1130	180	2.11151	0.78749	0.880	34
FALL	FLOW (m ³ /s)	0.59-21.8	4.1	5.1	4.4	Plott F	ed Points	s shown - 1 (a)	in	FLOW (m ³ /s)	1.2-7.9	4.4	4.3	1.6	Plotte Fl	ed Points GURE B -	shown 2 (a)	in
	TDS (mg/1)	640-917	806	788	74	1.92490	0.85308	0.981	35	TDS (mg/1)	746-1540	1078	1084	206	2.06051	0.81870	0.834	35
WINTER	FLOW (m ³ /s)	1.8-11.6	4.4	4.9	2.5	Plott F	ed Points IGURE B -	s shown 1 (b)	in	FLOW (m ³ /s)	1.1-6.7	3.6	3.8	1,5	Plotte Fl	d Points GURE B -	shown 2 (b)	in
CDDINC	TDS (mg/1)	203-917	470	520	215	1,95982	0.66988	0.947	39	TDS (mg/1)	148-1462	1069	979	384	2.21640	0.51585	0.802	37
SERING	FLOW (m ³ /s)	0.88-191	10.5	24.4	36.7	Plott F	ed Points IGURE B -	s shown - 1 (c)	in	FLOW (m ³ /s)	1.4-50.4	3.4	9,8	13.1	Plotte Fl	ed Points GURE B -	shown 2 (c)	in
SIMMER	TDS (mg/1)	215-843	581	558	140	2.01677	0.62713	0.941	40	TDS (mg/1)	877-1532	1191	1170	173	2.17309	0.75677	0.811	37
JOUPLER	FLOW (m ³ /s)	2.6-58.3	7.6	11.7	11.6	Plott F	ed Points IGURE B	s shown - 1'(d)	in	FLOW (m^3/s)	2.6-11.5	5.3	5.5	2.0	Plotte Fl	ed Points IGURE B -	shown 2 (d)	in

Table 4-4. Salinity mass-flow regression results for five stations in the South Platte River and three tributary stations.

 $\frac{1}{2}$ Metric tons of total dissolved solids per day $\frac{2}{2}$ m³/s

Table 4-4. (con	tinued).
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					REGRES	SION EQU	ATION :	LOG1	0 (SALT	$MASS)^{1/} =$	A + B * LOG	10 (FLOW) <u>2/</u>					
	(3)	BIG THO	MPSON RI	VER NE	AR LA S	ALLE				(4)	CAC	HE LA PO	UDRE R	IVER NE	AR GREELE	Y		
SEASON		STATISTICS	OF DAT	'A			n	" ²	CASES		STATISTICS	OF DAT	'A		Δ	В	R ²	CASES
	PARAMETERS	RANGE	MEDIAN	MEAN	ST.DV.	A	В	ĸ	USED	PARAMETERS	RANGE	MEDIAN	MEAN	ST.DV.				USED
	TDS (mg/1)	1396-2295	1931	1888	171	2.24150	0.91543	0.878	25	TDS (mg/1)	878-1700	1437	1402	190	2.13052	0.88447	0.952	35
FALL	FLOW (m ³ /s)	1.2-4.2	2.3	2.4	0.63	Plott F	ed Points IGURE B -	s shown - 3 (a)	in	FLOW (m^3/s)	0.40-8.6	2.8	3.3	1.7	Plotted FIG	Points s URE B - 4	shown i (a)	ເກື
	TDS (mg/1)	1644-2275	1941	1936	159	2.22834	0.9778	0,795	26	TDS (mg/1)	1013-1903	1399	1401	180	2.19833	0.73287	0.880	38
WINTER	FLOW (m ³ /s)	1.3-2.6	1.9	1.9	0.32	Plott F	ed Points IGURE B -	s shown - 3 (b)	in	FLOW (m ³ /s)	1.2-4.9	2.7	2.9	0,98	Plotte FI	d Points GURE B-	shown 4 (b)	in
	TDS (mg/1)	139-2218	1817	1483	677	2.17124	0.53669	0.722	28	TDS (mg/1)	146-1709	1353	1155	476	2.07037	0.63708	0.861	39
SPRING	FLOW (m ³ /s)	0.10-24.2	1.9	4.5	6.2	Plott F	ed Points IGURE B	s shown - 3 (c)	in	FLOW (m ³ /s)	0.18-54.9	2.3	8.2	14.7	Plotte Fl	ed Points [GURE B -4	shown (c)	in
	TDS (mg/1)	736-2142	1597	1525	347	2.24276	0.64232	0.847	27	TDS (mg/1)	1056-1726	1395	1384	147	2.07584	0.97904	0.984	1 39
SUMMER	FLOW (m^3/s)	1.1-7.3	2.3	2.8	1.8	Plott F	ed Points IGURE B	s shown - 4 (d)	in	FLOW (m ³ /s)	0.25-5.6	1.2	1.5	1.3	Plotte Fl	ed Points IGURE B -	shown 4 (d)	in

 $\underline{1}$ Metric tons of total dissolved solids per day $\underline{2}$ m³/s

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					REGRESS	SION EQU	ATION :	LOG10	(SALT	$MASS)^{1/} =$	A + B * LOG	10 (FLOW)2/					
	(5)	sc	OUTH PLA	TTE R	VER N	EAR KERS	EY			(6)	SOUT	H PLATT	E RIV	ER NEA	R WELDON	A		
SEASON		STATISTICS	OF DA1	`A				₂ 2	CASES		STATISTICS	OF DAT	A		A	В	R ²	CASES
	PARAMETERS	RANGE	MEDIAN	MEAN	ST.DV.	A	Б	к	USED	PARAMETERS	RANGE	MEDIAN	MEAN	ST.DV.				USED
	TDS (mg/1)	1006-2028	1341	1354	220	2.21943	0.86662	0.905	33	TDS (mg/1)	1334-2435	1490	1612	315	2.28834	0.84017	0.977	26
FALL	FLOW (m ³ /s)	3.9-56.6	14.6	16.9	10.0	Plott	ed Points FIGURE B -	shown 5 (a)	in	FLOW (m ³ /s)	1.8-39.6	9.4	12.2	9.9	Plotte FI	d Points GURE B -	shown ⁶ (a)	in
	TDS (mg/1)	1014-1435	1263	1270	93	2.32168	0.76200	0.927	34	TDS (mg/1)	1164-1835	1365	1393	166	2.17763	0.90709	0.974	26
WINTER	FLOW (m^3/s)	8.8-30.6	15.1	15.8	4.0	Plot	ted Points FIGURE B -	shown 5 (b)	in	FLOW (m ³ /s)	3.2-30.6	14.0	14.0	7.3	Plotte Fl	d Points GURE B -	shown 6 (b)	in
	TDS (mg/1)	181-1512	1199	1038	371	2.23611	0.70748	0.950	42	TDS (mg/1)	401-1925	1347	1256	332	2.24678	0.76104	0.971	32
SPRING	FLOW (m ³ /s)	1.2-317	11.5	41.6	73.1	Plot	ted Points FIGURE B -	s shown 5 (c)	in	FLOW (m ³ /s)	1.2-311	7.7	27.7	64.3	Plotte F	ed Points IGURE B -	shown 6 (c)	. in
	TDS (mg/1)	638-1487	1203	1169	193	2.18826	0.80276	0.971	41	TDS (mg/1)	1074-2283	1414	1459	229	2,20865	0.88332	0.943	33
SUMMER	FLOW (m ³ /s)	2.3-74.2	9.9	13.0	13.8	Plot	ted Point: FIGURE B	s shown 5 (d)	in	FLOW (m ³ /s)	2.2-35.1	9.1	11.1	7.4	Plott F	ed Points IGURE B -	shown 6(d)	in

 $\frac{1}{2}$ Metric tons of total dissolved solids per day $\frac{2}{2}$ m^3/s

					REGRES	SION EQU	VATION :	LOG10) (SALT	MASS) <u>1</u> / =	A + B * LOC	5 ₁₀ (FLOW	n)²/					
SEASON	(7)	S	SOUTH PI	LATTE	RIVER	AT BALZA	C			(8)	sour	H PLATI	E RIV	ER AT	JULESBUR	G		
		STATISTICS	OF DAT	ГA		^	R	_p 2	CASES		STATISTICS	OF DAT	ĨĄ.				_2	CASES
	PARAMETERS	RANGE	MEDIAN	MEAN	ST.DV.	A	Б	ĸ	USED	PARAMETERS	RANGE	MEDIAN	MEAN	ST.DV.	A	В	R	USED
FALL	TDS (mg/1)	1187-1556	1433	1422	87	2.08783	0.980071	0,999	19	TDS (mg/1)	940-1831	1598	1584	192	2.19170	0,92424	0.983	33
INSE	FLOW (m ³ /s)	0.20-28.1	0.57	3.6	7.2	Plott F	ed Points IGURE B -	shown 7 (a)	in	FLOW (m ³ /s)	1.5-43.0	6.4	9.4	10.0	Plotte FI	d Points GURE B -	shown 8 (a)	in
WINTER	TDS (mg/1)	1319-1530	1420	1413	62	2,08587	1.00350	0.999	20	TDS (mg/1)	1253-1992	1510	1554	171	2.22058	0,91375	0,985	35
	FLOW (m ³ /s)	0.22-19.3	0.61	4.8	7.0	Plott F	ed Points IGURE B -	shown 7 (b)	in	FLOW (m ³ /s)	2.3-54.1	14.1	16.4	11.9	Plotte FI	d Points GURE B -	shown 8 (b)	in
SPRING	TDS (mg/1)	543-1627	1495	1363	324	2.15948	0.83840	0.971	21	TDS (mg/1)	577-1757	1349	1307	339	2.17928	0.86453	0.986	39
	FLOW (m ³ /s)	0.19-110	4.2	14.0	27.4	Plott F	ed Points IGURE B -	shown 7 (c)	in	FLOW (m ³ /s)	0,69-279	10.3	38.4	61.4	Plotte FI	d Points GURE B -	shown 8 (c)	in
SUMMER	TDS (mg/1)	1099-1591	1473	1444	114	2.09197	1.00433	0.983	22	TDS (mg/1)	811-1710	1550	1492	187	2.12656	0,94023	0.992	34
	FLOW (m ³ /s)	0.79-14.1	4.5	5.3	2.9	Plott F	ed Points IGURE B _	shown 7 (d)	in	FLOW (m ³ /s)	0.31-66.8	1.3	6.95	13.5	Plotte FI	d Points GURE B -	shown 8 (d)	in

Table 4-4. (continued).

 $\underline{1}/$. Metric tons of total dissolved solids per day $\underline{2}/$ m^3/s

0.722. The cases used were comprised of monthly grab samples and numbered in the range 20 to 40 for each season. These numbers contrast with the thousand cases used in the verification obtained from the Julesburg station.

Based on the evidence presented the linear log-log salt mass-flow relationships contained in Table 4-4 will be applied in the salt transport characterization, described in Section 4.2. They provide the means for this larger purpose.

It should be noted that the A and B coefficients seen in Table 4-4(8) for Julesburg also are based upon the grab samples. It is remarkable to notice that they are virtually identical to the A and B coefficients seen in Table 4-3 for the large sample size using daily data. This similarity is further illustrated in Appendix C. Tables C-1 and C-2 show a comparison between computed seasonal and annual in-stream salt mass flows at Julesburg. The computed salt mass flows in columns C.1 and C.2 were obtained using the regression model for daily data and grab sample data, respectively. Observed averages are shown for reference, and to indicate by their differences with the "computed" columns, the residuals from the regression lines.

Again the statistics of the basic supporting data, i.e. total dissolved solids and flow are also included in Table 4-4. The corresponding plots of salt mass-flow data can be seen in Appendix B. They are grouped into sets of four by season for each station. The linear log-log relationships are evident by visual inspection of each plot, although the discontinuous linear function for the spring season plots that was noticed earlier at Julesburg, can be seen again at other stations.

4.2 Characterization of Salt Flows in the South Platte River

The salt flows in the South Platte River are characterized in terms of distance along the river for different years over the 1965-79 water year period. The five stations along the river were used as the basis for the distance profiles of flow, TDS, and salt mass. For the Julesburg station the time profiles were plotted by season and year; these are discussed first.

4.2.1 <u>Time Profiles of Salt Flows at Julesburg</u>

The variation in annual flow, TDS, and salt mass is seen in Figure 4-2 for Julesburg for the period 1965-79. Figure 4-2(a) shows that annual flow varies over a wide range during the fifteen year period considered. (It should be noted that the flows given are the total annual flow averaged over the year and expressed as cubic meters per second. This is done to permit easy comparison with monthly and seasonal flows.) The range in mean annual flow varies from a low of 2.84 m^3/s in water year 1978 to 43.08 m^3/s in 1973. Figure 4-2(b) shows that the flow weighted average annual salt concentration ranges from 1000 mg/ ℓ at the highest flow to 1600 mg/ ℓ at the lowest flow. The mean annual salt mass flows, seen in Figure 4-2(c), also have a wide range following a pattern similar to the flows, as might be expected. But in some years with similar flows, e.g. (1965, 1966) and (1969, 1974), the salt transport is quite different. Ostensibly this is due to changes in average annual salt concentration as seen in Figure 4-2(b). The behavior is better explained, however, by reference to Figure 4-3, which shows the same information plotted with seasonal resolution. The correlation between seasonal salt mass flow and



Figure 4-2. Flow, salt concentration, and salt mass flow averaged by year, water years 1965-79, South Platte River at Julesburg.



Figure 4-3. Flow, salt concentration and salt mass flow averaged by season, water years 1965-79, South Platte River at Julesburg.

seasonal flow, previously established by regression analysis, is illustrated by the data shown. Thus, meaning is given to the regression equations in terms of seasonal behavior of the three parameters shown, i.e. flow, salt concentration, and salt mass flow. Inspection shows a wide range variation from season to season, especially between fall-winter and spring-summer. Salt concentrations are notably higher in fall and winter than for spring and summer, for comparable flows, as can be seen, by comparing fall-winter 1965 with spring-summer 1966.

The fall and winter salt flows are comprised of the salts that remain from applied irrigation water and the pickup due to leaching. The spring salt load, however, is comprised mainly of those salts carried by the spring runoff. This runoff is also reflected in the summer season runoff statistics which includes July.

4.2.2 Distance Profiles of Salt Flows by Year

Figures 4-4, 4-5, and 4-6 are distance profiles of mean annual flow, flow weighted mean annual concentration, and mean annual salt mass flow for water years 1965-69, 1970-74 and 1975-79, respectively, along the main stem of the South Platte River from Henderson to Julesburg. The annual time variation in these parameters, illustrated in Figures 4-2 for Julesburg, is seen in another form in these three diagrams, together with the four other stations along the river. The basic data used in constructing these plots, i.e. Figures 4-4, 4-5, and 4-6, is seen in Table D-1, Appendix D. Appendix D also contains distance profiles by season in Figure D-1 to D-15, for the years 1965-79. The corresponding tabular data are seen in Table D-2.



Figure 4-4. Distance profiles of flow, salt concentration, and salt mass flow, averaged by year, 1965-69, South Platte River.



Figure 4-5. Distance profiles of flow, salt concentration, and salt mass flow, averaged by year, 1970-74, South Platte River.



Figure 4-6. Distance profiles of flow, salt concentration, and salt mass flow, averaged by year, 1975-79, South Platte River.



Figure 4-7. Distance profiles of flow, salt concentration, and salt mass flow, averaged by season, 1979, South Platte River.

Table D-3 shows monthly averages in event analysis with such resolution is of interest. Figure D-15 is included here as Figure 4-7.

Comparing the fifteen profiles of each of the three parameters, in Figures 4-4, 4-5, and 4-6 shows that they are consistent from year to year for any flow condition. The flow profiles show an increase from Henderson to Kersey. This due mainly to the tributary flows from St. Vrain Creek, and the Big Thompson and Cache La Poudre Rivers. The flow is essentially doubled between these stations for any given year. From Kersey to Weldona the flows decline sharply due to diversions. These flows decline further to Balzac with a slight increase from Balzac to Julesburg.

Salt concentration increases sharply from Henderson to Weldona. During the years of low salt concentration (high flows) the level increases from 300 mg/ ℓ to 800 mg/ ℓ between these stations. For low flow conditions, e.g. 1977, the range is from 600 mg/ ℓ to 1400 mg/ ℓ . The levels increase slightly to Julesburg where the range is 1000 mg/ ℓ to 1600 mg/ ℓ .

The distance profiles of mean annual salt mass flows are similar to those of mean annual flows, except they are generally accentuated by the increasing salt concentration levels. It should be noted that the annual distance profiles, seen in Figures 4-4, 4-5, and 4-6, are the average of a wide range of daily behavior. This range is seen in terms of seasonal resolution in Figure 4-7. This illustrates the idea that a strong seasonal influence exists. But the same trends, as seen in the annual profiles, exist also from season to season.

From the standpoint of salt transport the key point is that while an accumulation of salts occurs from Henderson to Kersey, the river loses salt between Kersey and Balzac. While there is a gain in river salt flow from Balzac to Julesburg, i.e. the reach farthest downstream, there is a net loss to the land, i.e. by irrigation, between Kersey and Julesburg. Table 4-5 gives the salt mass flows for each station averaged over the fifteen year period, expressed as tons of salts transported per day. The net loss to the land is seen as the difference in salt flows between Kersey and Julesburg, which amounts to 379.9 metric tons per day.

Table 4-5. Mean daily salt mass flows at stations in the South Platte River and tributaries averaged over 15 fifteen-years of records.

Station	Mean daily salt mass flow (metric tons/day)
South Platte River at Henderson	523.0
St. Vrain Creek near Platteville	464.3
Big Thompson River near La Salle	312.7
Cache La Poudre River near Greeley	327.7
South Platte River near Kersev	2007.8
South Platte River near Weldona	1713.2
South Platte River at Balzac	1368.0
South Platte River at Julesburg	1627.9

This analysis of changes in salt mass flows for the stations between Henderson and Julesburg is further illustrated in Figure 4-8, which shows plots of the cumulative salt mass flows for the period 1965-79. Figure 4-8 shows that the increases and decreases in salt transport along the stream have the same pattern from year to year. It further points out the need to relate these changes to the other inputs and outputs of flow and salt mass flow to and from each reach. This is, in fact, the focus of Section 4.3.



Figure 4-8. Cumulative salt mass flow at various river stations in the South Platte River between Henderson and Julesburg, water years 1965-79.

4.3 Mass Balance Analysis of Salt Flows by River Reach

The focus of this section is the salt balance analyses for each of the four stream reaches in the lower South Platte River. This has been done in terms of monthly, seasonal, and annual time intervals, with annual results presented in this section. Appendix F contains the results of the monthly, seasonal, and annual analyses in tabular form. The final output of the mass balance analyses consists of the computations of water flows and salt mass flows associated with the return flows.

4.3.1 Data Sources

The river reaches between the stations Henderson, Kersey, Weldona, Balzac, and Julesburg were used in the mass balance analyses for flow and salt mass flow. Measured diversions, point source inflows, and in-stream flows at the beginning and end of the reach were used to calculate the return flows to or from the reach. The salt mass flows associated with the river flows in the South Platte River and the three tributaries considered were taken from Section 4.2 and Appendix D. The salt mass flows associated with reach diversions and with point source inflows (e.g. canals and minor tributaries) were computed as outlined in Section 3.3. Salt mass flows associated with return flows then were computed as the mass balance residuals.

Appendix E contains the monthly flow data for the 1965-77 water year period for all diversions from the South Platte River between Henderson and Julesburg and for all point source inflows. River flows for the gaging stations on the South Platte River and the three tributaries used are given in Appendix D.

4.3.2 Annual Mass Balance Plots

Figures 4-9, 4-11, 4-13, and 4-15 show the annual flow balances for each of the four reaches for the 1965-79 water year period. Figures 4-10, 4-12, 4-14, and 4-16 show the corresponding cumulative salt balances. The basic data used in constructing these plots, i.e. Figures 4-9 to 4-16, is seen in Table F-1, Appendix F. These diagrams show the annual flows of water and salt mass, respectively for all inputs and outputs to and from the reaches.

The mass balance analysis for Henderson-Kersey reach, Reach #1, seen in Figure 4-9 shows that the sharp increase in river flow in the reach is due to the large point source inflows from the three tributary streams. The diversion flows, as noted, are significant also. They vary within a narrow range, while the river flows vary over a large range. The return flows averaged over the year vary generally between 6 and 10 m^3 /sec, with only values for three years lying outside that range. The return flows, of course, are calculated and therefore are subject to any errors in measurement for the other flow components.

Figure 4-10 shows the corresponding salt mass flows for Henderson-Kersey reach plotted as cumulative salt mass. The large increase in river salt mass flow previously noted in Section 4.2 is seen to be due to both point source inflows and return flows. Thus mass balance analysis has utility in explaining the observed behavior of the system.

For the Kersey-Weldona reach, it is seen in Figure 4-11 that the return flows average about 6.5 m^3 /sec while the diversion flows are about 14.5 m^3 /sec, and the point inflows are almost insignificant at about 1 m^3 /sec. This explains the decrease in river flow between the two stations.



Figure 4-9. Annual flow balance by water year for Henderson-Kersey reach, South Platte River, 1965-77.



Figure 4-10. Cumulative salt mass to and from Henderson-Kersey reach, South Platte River, water years 1965-77.



Figure 4-11. Annual flow balance by water year for Kersey-Weldona reach, South Platte River, 1965-77.

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Figure 4-12. Cumulative salt mass to and from Kersey-Weldona reach, South Platte River, water years 1965-77.



Figure 4-13. Annual flow balance by water year for Weldona-Balzac reach, South Platte River, 1965-77.



Figure 4-14. Cumulative salt mass to and from Weldona-Balzac reach, South Platte River, water years 1965-77.



Figure 4-15. Annual flow balance by water year for Balzac-Julesburg reach, South Platte River, 1965-77.



Figure 4-16. Cumulative salt mass to and from Balzac-Julesburg reach, South Platte River, water years 1965-77.

The cumulative salt mass for each component seen in Figure 4-12 is seen to follow the same trends as the flows of water. As noted in Section 4.2 there is a net loss of salt from the reach. This is explained in Figure 4-12 because the salt mass associated with the return flows is less than for the diversion flows, higher salt concentration in the former notwithstanding.

The mass balance analyses of the Weldona-Balzac reach, seen in Figures 4-13 and 4-14, is not marked different in its flow and salt mass flow characteristics than the previous reach. The diversion flows still exceed the return flows, it should be noted, which explains the difference in streamflows between Weldona and Balzac.

The picture changes in the Balzac-Julesburg reach, where the return flows, as seen in Figure 4-15, generally exceed by a small margin the diversion flows. Figure 4-16 shows that a small gain in salt exists between Balzac and Julesburg. The point source inflows in these last three reaches are generally not significant.

When reviewing all reaches the return flows seem to vary within a narrow range. Similarly the associated salt mass flows are almost constant as seen by the nearly straight line in the cumulative salt mass-time plot. Thus a linear relationship between flow and salt mass seems to be likely. Whether this is true or not is explored in the section following.

4.3.3 Plots of Computed Return Salt Mass Flow and Computed Return Flow

In Figure 4-17 the daily mean of the annual computed return salt mass flows is plotted against the daily mean of the annual computed return flows for each of the four reaches. These plots are the computed residuals from the materials balance analyses for each reach


Figure 4-17. Computed return salt mass flow averaged by year associated with computed return flows in four river reaches, South Platte River between Henderson and Julesburg, water years 1965-77 (*based on modified data included in Table F-4).

as described in Section 3.3; the data are given in tabular form in Appendix F. The plots show a linear relationship between return salt mass flow and return flow. But it should be noted that because of the computational procedure, a relationship between return salt mass flow and return flow is expected. The in-stream salt mass flows, the major components in the mass balance, are functions of streamflow for each station, which forces the linear relationships seen in Figure 4-17. Thus these plots do not establish a relationship between two independent parameters. They are presented for convenience in further analyses, since they are the only means available for estimating salt mass flows in return flows. The linear relationship is consistent, however, with the assertion of Riley and Jurinak (1979) that the salt loading from an agricultural system on a long term basis is proportional to the percolating water that passes through the system. These functional relationships could be used in conjunction with a hydrologic model in the simulation of salt flows for the system. Thus salt flows associated with modified development conditions (e.g., new irrigation lands are developed) could be estimated. It should be noted that the relationship is different for each reach.

Figures 4-18, 4-19, 4-20, and 4-21 show the same relationship for each of the four reaches, respectively, but with seasonal resolution. The graphs show different slopes for each season but there seems to be no consistent seasonal trends in comparing the slopes for corresponding seasons. The use of the seasonal relationships could improve the sensitivity of a simulation model.



Figure 4-18. Computed return salt mass flows averaged by season associated with computed return flows, South Platte River between Henderson and Kersey, water years 1965-77.



Figure 4-19. Computed return salt mass flow averaged by season associated with computed return flows, South Platte River between Kersey and Weldona, water years 1965-77 (based on modified data contained in Table F-4).



Figure 4-20. Computed return salt mass flows averaged by season associated with computed return flows, South Platte River between Weldona and Balzac, water years 1965-77.



Figure 4-21. Computed return salt mass flows averaged by season associated with computed return flows, South Platte River between Balzac and Julesburg, water years 1965-77.

Chapter 5

SUMMARY AND CONCLUSIONS

5.1 Summary

1. The results of this study show a need to predict the effect of new water developments upon the salinity regime of the lower South Platte River between Henderson and Julesburg.

2. This work demonstrates how river salinity may be characterized, both in terms of time and space variations. In addition, the role of factors, such as return flows, diversions and point source discharges, which shape this characterization, has been ascertained.

3. A thorough testing of established relationships:

- 1) TDS versus EC
- 2) Salt flow mass versus streamflow

has been accomplished. This testing was necessary prior to their utilization in this work. These relationships have been ascertained for eight river stations and for fifteen years of data. Reference is in Section 4.1.

4. The total dissolved solids-specific electrical conductance relationship has been developed for each river station so that the larger EC data base can be used for the in-stream salinity characterization as total dissolved solids.

5. The log-log form of the regression model between salt mass flow and streamflow has proven to explain the variation in in-stream salinity flow mass found in the lower South Platte River between Henderson and Julesburg.

6. Seasonal variations in the coefficients of the salt mass flow versus streamflow relationship was significant. They can be obtained by dividing the data base into seasons and developing regression lines for each season.

7. The seasonal regression lines developed for each river station have been used to compute its daily salt mass flow using daily flow as argument. The computed salt mass values were then averaged over the month, the season and the year, for the 1965-79 water year period, to analyze the salt transport characteristics of the system. From these data distance profiles of river flow, TDS, and salt mass flow were prepared. Reference is in Section 4.2.

8. The results of the salt transport characterization show that a high increase in river salt transport occurs between Henderson and Kersey, but a sharp decrease follows between Kersey and Weldona. The losses of salt to the land persist to Balzac, whereas from Balzac to Julesburg the stream experiences a slight gain of salt. This latter gain, however, does not compensate the previous losses, so there is a net loss of salt between Kersey and Julesburg. This loss amounts to an average of 380 metric tons of total dissolved solids per day.

9. The pattern of salt mass flow described above is consistent year after year, and season after season, for all flow conditions, irrespective of the fact that the salt concentration increases continuously in the downstream direction.

10. Finally, the in-stream salt mass flow variations along the river have been interpreted in terms of the salt flows to and from the

stream, by means of a materials balance analysis. This was done based upon the results of the in-stream salinity characterization and simplifying assumptions regarding the salinity associated with diversion flows and the point source discharges. The diffuse return flows to each reach and their associated salinity concentration levels were thus obtained as the residual of all other known flows to and from the reach. The materials balance was done for four river reaches, for a thirteen year period, with monthly, seasonal and annual resolution.

The results of the materials balance analysis show how 11. leaching from the land contributes to higher in-stream salt transport the Henderson-Kersey and Balzac-Julesburg reaches. In the in Henderson-Kersey reach, the three tributaries, i.e. the St. Vrain Creek, the Big Thompson River and the Cache River, are shown to contribute also significantly to the reach salt gain. Salt mass flows associated with the diversion flows are shown to exceed consistently those associated with return flows in Kersey-Weldona, Weldona-Balzac Finally a linear relationship between salt mass and return reaches. flow has been shown to be warranted. This relationship varies from reach to reach and from season to season.

5.2 Conclusions

1. A methodology has been demonstrated to characterize a river salinity regime. Fifteen years of daily and monthly flow and salinity data have been reduced in terms of monthly, seasonal, and annual statistical characterizations representative of the salinity behavior of the river.

2. The profiles of river salt mass flow have been interpreted in terms of the external interacting flows reach by reach.

3. The reach by reach materials balance analysis provides the basis for development of a simulation model. This could be used for predictive purposes, e.g. to assess the effects of Narrows Dam on existing salinity regime.

4. The analyses made show that salinity is a concern in the lower South Platte River not only because high concentrations are carried by the streamflows, but also because an accumulation of salt in the land is taking place in certain reaches.

5. These findings stress the need for careful consideration to be given on how new water resource developments will affect the salinity behavior of the system.

6. The results obtained in this study can be used thus as a basis for management.

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APPENDIX A

PLOTS OF TOTAL DISSOLVED SOLIDS VERSUS SPECIFIC ELECTRICAL CONDUCTANCE FOR NINE RIVER STATIONS IN THE SOUTH PLATTE RIVER BASIN

These plots were developed to convert measured EC data to equivalent TDS data. They include plots of both "TDS as residue" versus EC and "TDS as sum of constituents" versus EC. Original data were taken from published USGS records for the 1963-1979 water year period. Figure A-9 contains data for the Cache La Poudre River at the mouth of the canyon. It is included for reference purposes.



Figure A-1. Total dissolved solids - specific conductance data used in regression analysis, South Platte River at Henderson.



Figure A-2. Total dissolved solids - specific conductance data used in regression analysis, St. Vrain Creek near Platteville.



Figure A-3. Total dissolved solids - specific conductance data used in regression analysis, Big Thompson River near La Salle.



Figure A-4. Total dissolved solids - specific conductance data used in regression analysis, Cache La Poudre River near Greeley.



Figure A-5. Total dissolved solids - specific conductance data used in regression analysis, South Platte River near Kersey.



Figure A-6. Total dissolved solids - specific conductance data used in regression analysis, South Platte River near Weldona.



Figure A-7. Total dissolved solids - specific conductance data used in regression analysis, South Platte River at Balzac.



Figure A-8. Total dissolved solids - specific conductance data used in regression analysis, South Platte River at Julesburg.



Figure A-9.

Total dissolved solids - specific conductance data used in regression analysis, Cache La Poudre River at mouth of canyon.

APPENDIX B

PLOTS OF SALT MASS VERSUS FLOW FOR NINE RIVER STATIONS IN THE SOUTH PLATTE RIVER BASIN

Plots of log (salt mass) versus log (flow) are shown by season for each of five stations in the South Platte River and for four tributary stations. The regression equations obtained were used in calculating salt transport in the river. Table B-9 is included for reference purposes; the data for this plot were taken from a station on the Cache La Poudre River at the mouth of the canyon, prior to the influence of any return flows.



Figure B-1. Salinity mass - flow data used in regression analysis, South Platte River at Henderson.



Figure B-2. Salinity mass - flow data used in regression analysis, St. Vrain Creek near Platteville.



Salinity mass - flow data used in regression analysis, Big Thompson River near La Salle. Figure B-3.





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Salinity mass - flow data used in regression analysis, South Platte River at Balzac.



Salinity mass - flow data used in regression analysis, South Platte River at Julesburg.



ire B-9. Daillity mass - Ilow uata useu in regression a Cache La Poudre River at mouth of canyon.

APPENDIX C

COMPARISON BETWEEN OBSERVED AND COMPUTED SALT FLOWS IN THE SOUTH PLATTE RIVER AT JULESBURG

Table C-1 compares computed in-stream salt mass flows at Julesburg by season for the period 1965-79, by two regression equations. The computed salt mass flows were obtained using Equation (4-2), i.e., log (salt mass) = A + B log (flow). The A and B coefficients were obtained by regression analysis using two sets of 1965-79 data (e.g., daily samples and monthly grab samples for columns C.1 and C.2, respectively). Observed averages are shown for reference. Comparisons of observed and computed salt mass flows shows the residuals obtained in using the regression functions. Table C-2 shows the same type of comparisons as given in Table C-1, but on an annual basis.

Table C-3 shows monthly average flows and TDS, and monthly flow weighted average TDS compared with computed values. Tables C-4 and C-5 show the same information for season and annual bases, respectively.

 \mathbf{a}_{i}
Comparison between computed <u>seasonal transport of salt</u> in the South Platte River at Julesburg, using C.1 and C.2 regression equations. Observed seasonal averages are shown for reference. Table C-1.

					-													_	-	-
~	(P/;	JTED	C.2	2322	324	1522	1302	851	885	448	249	1331	296	336	106	170	83	1415	776.0	669.1
S U M M E I	MASS (1	COMPU	c.1	2183	311	1430	1222	802	836	426	239	1257	283	321	103	164	80	1336	732.9	627.7
	SALT	OBCEDVED	OBGENVED	2255	331	1242	1046	702	764	452	266	1128	285	309	103	183	84	1578	715.2	626.8
	(p/	TED	c.2	3009	529	1437	507	4315	5779	4151	496	6166	1354	1925	360	685	416	4170	2603.5	2693.4
PRING	T) MASS (T	COMPU	c.1	3191	533	1484	510	4525	6046	4320	499	10474	1392	1983	361	693	418	4361	2719.3	2845.1
SALT	SALT	Chetten		2781	561	1529	559	3927	5751	4041	522	9084	1779	1847	361	804	444	4124	2540.9	2478.9
~	(/d)	JTED	c.2	506	2854	799	1344	1059	3895	3182	1843	2977	3898	1585	1903	1048	681	1149	1914.9	1156.7
VINTEI	r mass (1	COMPL	C.1	502	2816	792	1329	1049	3839	3139	1821	2937	3843	1567	1880	1038	675	1137	1890.9	1138.9
4	SAL			480	2808	783	1407	1127	3970	3146	1801	3008	3737	1309	1880	1055	692	1188	1892.7	1146.7
	r/d)	UTED	C.2	210	3501	724	695	751	2260	1931	1447	741	3423	745	952	362	388	375	1233.7	1073.1
FALL MASS (T,	COMPI	C.1	206	3580	724	695	751	2302	1958	1461	742	3501	746	957	358	384	371	1249.1	1101.6	
	SAL		UBSERVED -	198	3585	724	731	806	2322	1956	1469	778	3260	657	957	396	397	379	1241.0	1066.1
	WATER	YEAR		65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	Mean	St.Dv.

Observed is measured EC converted to TDS, times measured flow, as daily mean for year, using daily data. C.1 Computed is calculated salt mass made using salt mass-flow regression lines for each season, derived from 15 years of daily records, using daily flow as argument. C.2 Computed is calculated salt mass made using salt mass-flow regression lines for each season,

derived from monthly grab sample data, using daily flow as argument. T/d is metric tons of total dissolved solids per day.

Table C-2. Comparison between computed <u>annual transport of salt</u> in the South Platte River at Julesburg, using C.1 and C.2 regression equations. Observed annual averages are shown for reference.

МАТЕ Ф	S	ALT MASS (T/d))
WAIEK	OBCEDUED	COMPI	UTED
YEAR	OBSERVED	C.1	C.2
65 66 67 68 69 70 71 72 73 74 75 76 77 78 79	1427 1824 1066 937 1635 3186 2391 1012 3488 2265 1028 822 602 397 1818	$ \begin{array}{r} 1519\\ 1813\\ 1104\\ 941\\ 1776\\ 3240\\ 2453\\ 1002\\ 3840\\ 2255\\ 1151\\ 822\\ 556\\ 382\\ 1801 \end{array} $	1511 1805 1117 964 1738 3189 2420 1005 3730 2243 1145 827 559 385 1777
Mean St.Dev.	1593.2 915.0	1643.7 977.5	1627.7 948.4

Observed is measured EC converted to TDS, times measured flow, as daily mean for year, using daily data. C.1 Computed is calculated salt mass made using salt mass-flow regression lines for each season, derived from 15 years of daily records, using daily flow as argument. C.2 Computed is calculated salt mass made using salt mass-flow regression lines for each season, derived from monthly grab sample data, using daily flow as argument. T/d is metric tons of total dissolved solids per day.

M O N CONSID C•1 RE	T H L Y ERED• MIS GRESSION	R E S U SING TOS V LINES.	L T S Alues have	ALL DAYS BEEN ESTIM	HAVE BEEN Ated Using
WATER YEAR	ACTUAL MONTHLY AVERAGE FLOW (CMS)	ACTUAL MONTHLY AVERAGE TDS (MG/L)	ACTUAL MONTHLY F.W.AV. TDS (Mg/L)	ESTIMATED MONTHLY F.W.AV. TDS(C.1)* (MG/L)	ESTIMATED MONTHLY F.W.AV. TDS(C.2)** (MG/L)
			OCTOBER		
667890123456789 77777777777777777777777777777777777	•799088188789175 2333342929333222	136597 3645 1976 1976 1976 1976 1976 1976 1976 1976	348546464453522 971057011.453522 971057011.453722 11111111111111111111111111111111111	$\begin{array}{c} 498657\\ 1111111119514\\ 11111111191514\\ 1111111111111111111111111111111111$	0&6498726550140 58005348001000 5800534800100 836660420807 •••••• 83666042080 ••••• •••• 8366604 85660 85660 85660 •••••• ••••••• ••••••• ••••••••• ••••••
			NOVEMBER		
6667890123456789 77777777777777777777777777777777777	1.48497 2.54972496486884 2.1114735149 2.11147351492	97.651.64.662.651.1458549.4472.54.51.1458549.54.54.54.54.55.45.54.55.45.54.55.45.54.55.45.55.5	244653835522976 9984653835522976 11456644558584 11445654576659 1144565457 118657	524751103422505 745554455445544554455445544554455445544	2779339901536091 16873063189**09 75576716598**09 75584445389**0 111111111111 1111111111111111111111

Table C-3. Monthly average flows and TDS, and monthly flow weighted average TDS compared with computed values, water years 1965-79, South Platte River at Julesburg.

^{*}C.1 is salt mass-flow regression lines for each season derived from 15 years of daily records were used in these computations.

^{**}C.2 is salt mass-flow regression lines for each season derived from monthly grab sample data were used in these computations.

Table C-3. (continued).

WATER YEAR	ACTUAL MONTHLY AVERAGE FLOW	ACTUAL MONTHLY AVERAGE TDS	ACTUAL MONTHLY F.W.AV. TDS	ESTIMATED MONTHLY F.W.AV. TOS(C.1)*	ESTIMATEC MCNTHLY F.W.AV. TDS(C.2)** (MG/L)
	(CMS)	(MG/L)	DECEMBER	C PEG / C /	
6667890123456789 77777777777777777777777777777777777	2 • 1 26 • 55 9 3 5 0 7 • 5 9 3 5 0 1 2 9 8 • 9 2 1 2 9 8 9 2 • 4 1 3 3 • 9 2 • 9	$ \begin{array}{c} 8 \\ 4 \\ 4 \\ 5 \\ 4 \\ 5 \\ 7 \\ 1 \\ 4 \\ 5 \\ 7 \\ 1 \\ 1 \\ 5 \\ 4 \\ 5 \\ 1 \\ 4 \\ 5 \\ 1 \\ 4 \\ 5 \\ 7 \\ 2 \\ 7 \\ 2 \\ 6 \\ 5 \\ 7 \\ 2 \\ 7 \\ 2 \\ 6 \\ 5 \\ 7 \\ 2 \\ 7 \\ 2 \\ 6 \\ 7 \\ 7 \\ 2 \\ 7 \\ 2 \\ 7 \\ 2 \\ 7 \\ 2 \\ 7 \\ 2 \\ 5 \\ 7 \\ 2 \\ 7 \\ 7 \\ 2 \\ 7 \\ 2 \\ 7 \\ 2 \\ 7 \\ 2 \\ 7 \\ 7 \\ 2 \\ 7 \\ 7 \\ 2 \\ 7 \\ 7 \\ 2 \\ 7 \\ 7 \\ 2 \\ 7 \\ 7 \\ 2 \\ 7 \\ 7 \\ 2 \\ 7 \\ 2 \\ 7 \\ 7 \\ 2 \\ 7 \\ 2 \\ 7 \\ 2 \\ 7 \\ 2 \\ 7 \\ 2 \\ 7 \\ 7 \\ 2 \\ 7 $	5588844667 3320 66667744687072493 111111111111111 1145674859 111111111111111111111111111111111111	838170514202493 922087030239593 6365527030239593 64555544554669 84555544546693 	677378488495089 90044697883885 64005344697883883 64005344594308 6405534454545 6405534454545 640555 640555 640555 64055 89 89 89 89 89 89 89 89 89 89 89 89 89
			JANUARY		
6667890 77777777777777777777777777777777777	21.5779334293335564 21.50841.0.9333564 1.4211853643.4 4.34	146536.4 146536.0 17638.0 1455368.0 1455349.9 155749.8 155749.0 12586.000000000000000000000000000000000000	846041960698189 3844960549698 3449605490898 6449605490898 899 11111111111 111111111111111111	853490 9.53490 9.55156.9 1156.9 11580 746380 11580 11580 11580 115534 11480 11558 11111 11558 11111 11558 11111 11558 11111 11558 11111 11558 11111 11558 11111 11568 11111 11568 11111 11568 11111 11568 11111 11568 11111 11568 11111 11568 11111 11568 11111 11568 11111 115688 11568 1	8720000000 20000000700000000000000000000
			FEBRUARY		
65678901233456789 77777777777777777777777777777777777	49.5251651909520 207749870625520 321231255 15	161269.4 164269.1 164269.1 17447.6 14564.7 14445.8 1444.6 107.9 1659.3 1659.3 1669.3 159.3 1669.9 159.3 1669.9 159.1 1659.1 1659.1 1659.1 1659.1 1659.1 1659.1 1659.1 1659.1 1659.1 1659.1 1659.1 1659.1 1659.1 1659.1 1659.1 1659.1 1659.1 1650.2 1650.1 1650	24414 01699645 51699645 51699645 51699645 51699645 5169964 516966564 5169564 5169564 5169564 516956556555555555555555555555555555555	468476204092508 7125554442195556 642279916566 1153444219 1153444219 11568 11556 1111111 111111 111111 111111 111111 1111	1562999210424 0668555646008580 085381138464808580 0465815546008580 0465815546008580 0465815580 0465665

Table C-3. (continued).

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Table C-3. (continued).

M O N CONSID C•1 RE	T H L Y ERED. MIS GRESSION	RESU SINGTDSV LINES•	L T S ALUES HAVE	ALL DAYS BEEN ESTIM	HAVE BEEN MATED USING
WATER Year	ACTUAL MONTHLY AVERAGE FLOW (CMS)	ACTUAL MONTHLY AVERAGE TDS (MG/L)	ACTUAL MONTHLY F.W.AV. TDS (MG/L)	ESTIMATED MONTHLY F•W•AV• TDS(C•1)* (MG/L)	ESTIMATED MONTHLY F.W.AV. TDS(C.2)** (MG/L)
			JUNE		·
6667890123456789 77777777777777777777777777777777777	$125 \cdot 1 43 \cdot 2 99 \cdot 1 105 \cdot 5 105 \cdot 7 38 \cdot 4 3 \cdot 2 105 \cdot 7 38 \cdot 4 3 \cdot 2 124 \cdot 1 124 \cdot 1$	$\begin{array}{c} 1125 \cdot 1 \\ 1519 \cdot 4 \\ 15210 \cdot 6 \\ 9883 \cdot 0 \\ 10524 \cdot 3 \\ 10524 \cdot 4 \\ 13524 \cdot 4 \\ 13524 \cdot 4 \\ 13642 \cdot 0 \\ 14564 \cdot 3 \\ 9375 \cdot 0 \\ 14526 \cdot 8 \\ 15281 \cdot 8 \\ 881 \cdot 8 \end{array}$	745.1 145.1 1113.5 779.8 10164.6 1130.5 1064.6 1130.5 1064.6 113821.5 1382.8 8 2.8 8 2.8 8 2.8 8 1382.8	9904755583245977 14072405583245977 11393054354 11393054354 11393054354 11393054354 11393054354 11393054354 11393054034	96579.4 106579.4 106579.4 106579.4 106779.4 10779.4 1
			JULY		
6667890123456789	28.52 39.97 206.42 9.682 9.682 7.19 1.19 9.1	$\begin{array}{c} 1188 \cdot 7\\ 1443 \cdot 6\\ 11513 \cdot 3\\ 122125 \cdot 0\\ 122125 \cdot 0\\ 115213 \cdot 3\\ 13515 \cdot 0\\ 1157 \cdot 0\\ 13597 \cdot 0\\ 135942 \cdot 0\\ 13542 \cdot 0\\ 15632 \cdot 0\\ 135632 \cdot 0$	$\begin{array}{c} 100\\ 179\\ 989\\ 989\\ 1989\\ 1989\\ 1989\\ 100\\ 1988\\ 992\\ 100\\ 100\\ 103\\ 103\\ 103\\ 103\\ 103\\ 103$	405036945666182 594957038098666 1114452529738666 11145252973705 11145252973703 1111111111111111111111111111111111	1442543545257 2857243545257 24425425757 1442527557 1445545527 145557 145577 145577 145577 145577 145577 1455777 1455777 1455777 1455777 1457777 14577777 1457777777777
			AUGUST		
6567890123456789 7723456789	24.3 1.4 1.4 30.4 1.3 1.3 7 1.2 3.8 2.5 5 1.5 19.6	13456 • 3 14558 • 5 14458 • 5 1458 • 5 1458 • 5 113996 • 7 113996 • 7 1566 • 7 1566 • 5 1566 • 5 1576 • 5 1566 • 5 1566 • 5 1576 • 5 157	$1310 \cdot 1$ $144 \cdot 0$ $144 \cdot 0$ $145 \cdot 0$ $146 \cdot 0$	6950 6950 14410 65579 9250 65579 9250 65579 9250 65579 9250 6 8260 85 6 85 6 957 9250 8 8 8 8 8 8 8 9 8 9 8 9 8 9 8 9 8 9 8	1214.8 15127.5 15127.5 15127.5 15127.5 15127.5 15127.5 15127.5 15127.5 15127.5 1512.5 1515.5 1515.5 1515.5 1515.5 1515.5 1515.5 1515.5 1515.5 1515.5 1515.5 155.

M O N CONSID C•1 RE	T H L Y ERED. MIS GRESSION	R E S U SING TOS V LINES.	L T S VALUES HAVE	ALL DAYS BEEN ESTI	HAVE BEEN MATED USING	
 WATER YEAR	ACTUAL MONTHLY AVERAGE FLOW (CMS)	ACTUAL MONTHLY AVERAGE TDS (MG/L)	ACTUAL MONTHLY F.W.AV. TDS (MG/L)	ESTIMATED MONTHLY F.W.AV. TDS(C.1)* (MG/L)	ESTIMATED MONTHLY F.W.AV. TDS(C.2)** (MG/L)	
			SEPTEMBER			
567890123456789 77777777777777777777777777777777777	11.4 43.14 15.6600783342 253.14 9.	$13554239 \cdot 59445624051456445644562346562346647$	209983974257038 3524459607983961 11111111111111111111111111111111111	455781215197532 48870111119753294 48701111119753298 482707911119753298 111111111111111111111111111111111111	$\begin{array}{c} 1 \\ 1 \\ 1 \\ 1 \\ 2 \\ 6 \\ 8 \\ 0 \\ 1 \\ 1 \\ 1 \\ 2 \\ 6 \\ 2 \\ 1 \\ 1 \\ 1 \\ 2 \\ 5 \\ 3 \\ 6 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1$	

Table C-3. (continued).

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S E A Consid C•1 Re	S O N A L ERED• MIS GRESSION	SING TDS V LINES.	U L T S IALUES HAVE	ALL DAYS BEEN ESTI	HAVE BEEN MATED USING
WATER YEAR	ACTUAL SEASONAL AVERAGE FLOW (CMS)	ACTUAL SEASONAL AVERAGE TDS (MG/L)	ACTUAL SEASONAL F.W.AV. TDS (MG/L)	ESTIMATED SEASONAL F•W•AV• TDS(C•1)* (MG/L)	ESTIMATED SEASONAL F.W.AV. TDS(C.2)** (MG/L)
567890123456789 77777777777777777777777777777777777	413154325552575 295558515852575 111158570575	30 30 30 30 30 30 30 30	FALL 1637.0 16458596.0 164585960.7 164585960.7 145574.5 1653283 1653283 165328 1655588 165588 165588 1655888 1655888 165	5768520616958693 0287768459169546 028774806268572 74555445546566 745554656867 11111111111111111111111111111111111	554049042124469 73587726959677438 73587726959677438 73587726959677438 111111111111111111111111111111111111
667890123456789 77777777777777777777777777777777777	446696949406795575 32597406795575 321251145 8	1935120 35180 114651520 114651520 114650 11520 1509 1509 1509 1509 1509 1509 1509 150	WINTER 1637.9934 1637.9934 164160.938 164160.98 164160.98 146420 14438 14438 15739.9 16420 16420 1650 1670 1670 1671 16420 1650 1670 17600 1760 1760 1760 1760 1760 1760 1770 1760 1770 176	198319523293136 9164720593300017 746553454455565 7465534540208647 111111111111111111111111111111111111	942542148377719 24657133039318664 74657133039318664 746564458776 111111111111111 1111111111111111111

Table C-4. Seasonal average flows and TDS, and seasonal flow weighted average TDS compared with computed values, water years 1965-79, South Platte River at Julesburg.

*C.1 is salt mass-flow regression lines for each season derived from 15 years of daily records were used in these computations. **C.2 is salt mass-flow regression lines for each season derived from

monthly grab sample data were used in these computations.

		· · · · · · · · · · · · · · · · · · ·			
S E A CONSID C•1 RE	S O N A L ERED• MISS GRESSION L	R E S SING TOS V INES•	U L T S ALUES HAVE	ALL DAYS BEEN ESTIM	HAVE BEEN ATED USING
WATER YEAR	ACTUAL SEASONAL AVERAGE FLOW (CMS)	ACTUAL SEASONAL AVERAGE TDS (MG/L)	ACTUAL SEASONAL F.W.AV. TDS (MG/L)	ESTIMATED SEASONAL F.W.AV. TOS(C.1)* (MG/L)	ESTIMATED SEASONAL F.W.AV. TDS(C.2)** (MG/L)
			SPRING		
5567890123456789 77777777777777777777777777777777777	42.2 45.4 154.2 53.0 47.8 131.9 13.8 20.8 50.5	$\begin{array}{c} 1401 \\ 5744 \\ 15162 \\ 597 \\ 4412 \\ 1255 \\ 1201 \\ 1201 \\ 1201 \\ 1201 \\ 1201 \\ 1201 \\ 1201 \\ 1205 \\ 605 \\ 8 \\ 1255 \\ 60 \\ 9 \\ 8 \\ 1255 \\ 12$	762.7 147999 14144.0 15895 99774.1 10950.5 14797.8 99774.8 10950.5 14797.8 10950.5 1510.7 1510.7 1510.3	8661 75266596 14149996 1449996 149996 14997 14997 114997 114997 114997 114932 1 114932 1 114997 1 114932 1 1 114997 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	46141515402688 298535590640 308535590640 108535590840 1182145 1182145 11143245 11143245
			SUMMER		
5567890123456789 77777777777777777777777777777777777	21.5 2.6 14.2 12.3 7.6 9.9 2.0 9.0 11.9 2.7 2.8 2.0 9.4 2.7 2.8 3.6 1.0 9.4 2.5 1.0 9.4 2.5 1.0 9.4 2.5 1.0 9.4 2.5 1.0 9.4 2.5 1.0 9.4 2.5 1.0 9.4 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	13068 1476396 14353960952 14555766 113542433 11356331 155742433 11556331 1556331 1556331 156331 156331 1564332 1156331 1564332 1156331 1156331 1156331 1156331 1156331 1156331 1156331 1156331 11574243331 11564332 1156442 11564444 11564444 11564444 11564444 11564444 11564444 115644444 115644444 115644444	1213.99 12472.72 12472.72 109842.57 111741.26 111741.26 11174972.66 11174972.66 11174972.66 115932.88 1166238 1166238	135386599 13111229825785 11122982577 1225777 1225777 1225777 1225777 122577 1225777 1225777 1225777 1225777 1225777 1225777 12257777 12257777 12257777 12257777 12257777 12257777 12257777 12257777 12257777 12257777 12257777 122577777 122577777 1225777777 122577777 1225777777 122577777 12257777777 12257777777777	1435918855555 5442207349556 11111111111 1111111111 111111111 111111

Table C-4. (continued).

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A N N CONSID C•1 RE	U A L ERED• MIS GRESSION	RESUL SING TOS V LINES.	T S ALUES HAVE	ALL DAYS BEEN ESTI	HAVE BEEN MATED USING
WATER YEAR	ACTUAL ANNUAL AVERAGE FLOW (CMS)	ACTUAL ANNUAL AVERAGE TDS (MG/L)	ACTUAL ANNUAL F.W.AV. TDS (MG/L)	ESTIMATED ANNUAL F.W.AV. TDS(C.1)* (MG/L)	LSTIMATED ANNUAL F.W.AV. TDS(C.2)** (MG/L)
667890123456789 77777777777777777777777777777777777	17.1 14.7 10.1 7.9 18.9 23.0 7.8 19.0 43.1 19.0 4.3 19.0 4.3 19.0 10.5 4.3 18.6	$\begin{array}{c} 9.8\\ 9.8\\ 440955556\\ 11555556\\ 1155556\\ 1155537235\\ 155537235\\ 1156674\\ 115674\\ 115674\\ 115674\\ 115674\\ 11566744\\ 1156674\\ 1156674\\ 1156674\\ 1156674\\ 1156674\\ 1156674\\ 1156674\\$		$\begin{array}{c} 0 \\ 1 \\ 1 \\ 2 \\ 2 \\ 3 \\ - \\ 2 \\ - \\ 2 \\ - \\ 2 \\ - \\ - \\ - \\ -$	10220 220 220 220 220 220 220 220 220 22

Table C-5. Annual average flow and TDS, and annual flow weighted average TDS compared to computed values water years 1965-79, South Platte River at Julesburg.

*C.1 is salt mass-flow regression lines for each season derived from 15 years of daily records were used in these computations.

^{**}C.2 is salt mass-flow regression lines for each season derived from monthly grab sample data were used in these computations.

APPENDIX D

MEAN VALUES OF FLOW AND SALT MASS FLOW AND FLOW WEIGHTED MEAN TOTAL DISSOLVED SOLIDS FOR ANNUAL, SEASONAL, AND MONTHLY TIME INTERVALS, WATER YEARS 1965-79, FOR EIGHT RIVER STATIONS IN THE SOUTH PLATTE RIVER BASIN

Tables D-1, D-2, and D-3 were computed from published USGS daily flow records for the period 1965-79. Table D-1 was used in constructing the distance profile plots of annual averages, shown in Figures 4-4, 4-5, and 4-6. Table D-2 was used to construct the fifteen distance profile plots of seasonal averages, Figure D-1. Table D-3 was added for reference in event analysis using monthly resolution is of interest.

Figures D-1 to D-15 show distance profile plots of mean daily flow, flow weighted mean daily total dissolved solids, and mean daily salt mass flow all averaged over the four seasons. The seasonal profiles are grouped by water years for the period 1965-79. They are included to show additional resolution, which is not seen in the annual plots.

Т	ble D-1.	Mean dai mass flo River Ba	ly flow, w average sin.	flow weig d over ea	hted aver ch water	rage of to year, 190	otal disso 55-79, for	lved soli eight st	ds, and mean daily salt ations in South Platte
WATER Year	1	64	ю	RIVER 1	01NT 5	ų	7	ω	
MEAN A	NNUAL FLOM	(CWS) :							
65	16.33	8.35	1.97	4.35	31-76	17.86	16.92	17.14	I = South Flatte Kiver at
101			6.	2.01	- 000	-010 -010	10.10		Henderson
- an 9-09	5 1 .5	040 1040 1040	1.63	2•1/ 2•04	12*• 12• 505		00°-000	10-147-87	2 = St. Vrain Creek near
69 70	15 • 58 27 • 72	9.09 9.09 1.00	2 • 4 5 • 7 5	0110 • • • • • • • •	00 10 10 10 10 10 10 10 10 10	20.00	914 - 70 90 - 70 90 - 70	18•60 31•60	Platteville
10	14 - 37	100 C	-10 -10 -10 -10 -10 -10 -	20 4 4 20 4 4		29-03	100 100 100		3 = Big Thompson River
-1-1		0 0 0 0 0 0 0 0 0 0	-100 • • • •	- 010	100 100 101 101		-10) -17)(-01 -01	- 41 - 41 - 41	near La Salle
10	1 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	6 • 4 8 6 • 3 7	3. • 98 • 058	5 4 4 5 4 4 7 4 4	200 900 900 900	15.17	10.04	00 ••• •••	4 = Cache La Poudre River
75	0 0 0 0 0 0 0 0 0 0 0 0 0 0	4 m • 1 0 0 0 0	ດາ • • ເບຍ	00 10 10 10 10 10	16.72	9 • 9 19 19	50 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	ф4 ••	near Greeley
80	92 + L	000 00 00 00 00 00 00	1014	01- 10- 10-	199 199 190 190	0.00 10 10 10 10 10 10 10 10 10 10 10 10 1			5 = South Platte River
		•	+ •	•			•	, ,	near Kersey
FLOW W	EIGHTED ME	AN ANNUAL S	SALINITY (N	:(1/9;					6 = South Platte River
5	762.76	700.65	1478.33	794.47	744.09	1014-12	1016.57	1000.36	near Weldona
יסי מיני			1362	1345.37	1223.047		1380.55		7 = South Platte River
- 0.0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1074 • 20	1747.77	1254 • 33	1197.21	14554 145554 1455554 1455564 1455564 1455564 14555676676767676767676767676767676767676			at Balzac
6 U V	0100 0100 0100	1000-28	1199.14 1188.45	011 010 010 010	669.66 775.51	040 000 000	373•75 1004•60	1157.15	8 = South Platte River
		725.85	987.17		100 100 100 100 100		1107.42	1217-78	o - Douch Llacco MIVCL
121	311 • 10	1004 • 80 685 • 36	1000 000 1000	61.067 7.40.19	1000 1000 1000 1000 1000 1000 1000	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	40014 • 400	1001+66	ar Jurespurg
44	514.52	970-56	1484-03	1000 45	982 . 57	1225.96	1305•32	1458 4458 4458 458	
יםי ו-יו-	- 101 - 101 - 101 - 101 - 101 - 101	1091.78	1471.21						
73	004 • 00 00 • 00 00	1107.25 820.25	10444•44 1315•64	-230-470 884-570	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	чн 90- 10- 10- 10- 10- 10-	1286.49		
61	439.49	682.74	949•24	682.90	699•84	947.24	1000.85	1102•3011	
MEAN A	NNUAL SALI	NITY MASS	(T/D) :						
99 99	511.76 350.09	521•21 370•93	251•31 287•36	272.92 240.47	2044.15 1467.30	1564•77 1458•85	1486.24 1257.58	1514.12 1803.28	
67 68	ษณ มณ ••• ••• ••• ••• ••• ••• ••• ••• •••	457•19 392•92	240 240 240 200 200	266.43 221.50	1516.72 1297.17	1029.57 875.17	713,96 351,34	1121.73 560.83	
69 10	497.15 909.71	404 605 10 10 10	253•38 387•58	224•65 396•27	2028 20 3221 • 24	1458 52 3070 952	3058.05	1730 - 04 31930 - 04 496 - 04 496 - 04	
12	651 • ୧୦୦ 474 • ୧୦୦	564•12 413•42	397•01 293•03	491•94 361•59	2666.71	10010 10210 • • • • • •	000 000 000 000 000 000 000 000	2420.00 1005.00 35	
73	811.67 682.08	533•49 459•64	355•43 381•89	417.51	3164.22	3301.75	3108•58 1978•12	3728.32	
501	400 470 47	484•76 392•11	325 • 09 323 • 09 919	268 • 10 24 • • • • • • • • • • • • • • • • • • •	1634.56	1190 • 60	1100.022		
- 66	010-1-1-0 	5 4 5 5 4 5 5 4 5 5 4 5 5 4 5 5 5 4 5	200 200 200 200 200 200 200 200 200 200	ンで14 シート クロート クロート		2015 2015 2015 2015 2015 2015 2015 2015	- 101 - 101 - 100 - 100	1000 1000 1004 1004 1004 1004 1004 1004	
					ŀ				

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Mean daily flow, flow weighted average of total dissolved solids, and mean daily salt mass flow averaged over each seasons, 1965-79, for eight stations in South Platte River Basin. Table D-2.

NITY MASS	kankus svias	-	00000000000000000000000000000000000000		аланики продока солост аланики продока солост аланики продока аланике стала соласта и аланике стала соласта и аланике стала соласта аланике стала соласта аланики соласта аланики соласта аланики соласта аланики соласта аланики соласта отраники соласта отраники отраники соласта отраники отр			
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Figure D-2. Distance profiles of flow, salt concentration and salt mass flow averaged by season, South Platte River, water year 1966.



Figure D-3. Distance profiles of flow, salt concentration and salt mass flow averaged by season, South Platte River, water year 1967.



Figure D-4. Distance profiles of flow, salt concentration and salt mass flow averaged by season, South Platte River, water year 1968.



Figure D-5. Distance profiles of flow, salt concentration and salt mass flow averaged by season, South Platte River, water year 1969.



Figure D-6. Distance profiles of flow, salt concentration and salt mass flow averaged by season, South Platte River, water year 1970.



Figure D-7. Distance profiles of flow, salt concentration and salt mass flow averaged by season, South Platte River, water year 1971.



Figure D-8. Distance profiles of flow, salt concentration and salt mass flow averaged by season, South Platte River, water year 1972.



Figure D-9. Distance profiles of flow, salt concentration and salt mass flow averaged by season, South Platte River, water year 1973.



Figure D-10. Distance profiles of flow, salt concentration and salt mass flow averaged by season, South Platte River, water year 1974.



Figure D-11. Distance profiles of flow, salt concentration and salt mass flow averaged by season, South Platte River, water year 1975.



Figure D-12. Distance profiles of flow, salt concentration and salt mass flow averaged by season, South Platte River, water year 1976.



Figure D-13. Distance profiles of flow, salt concentration and salt mass flow averaged by season, South Platte River, water year 1977.



Figure D-14. Distance profiles of flow, salt concentration and salt mass flow averaged by season, South Platte River, water year 1978.



Figure D-15. Distance profiles of flow, salt concentration and salt mass flow averaged by season, South Platte River, water year 1979.

Mean daily flow, flow weighted average of total dissolved solids, and mean daily salt mass flow, averaged over each month, 1965-79, for eight stations in the South Platte River Basin. Table D-3.

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APPENDIX E

DIVERSION AND POINT SOURCE FLOW DATA, WATER YEARS 1965-77, SOUTH PLATTE RIVER BETWEEN HENDERSON AND JULESBURG

Tables E-1, E-2, E-3, and E-4 contain diversion and point source monthly flow data for water years 1965-77 used in the materials balance analysis discussed in Sections 3-3 and 4-3. Each table contain data for each of the four river reaches considered, i.e. Henderson-Kersey, Kersey-Weldona, Weldona-Balzac, Balzac-Julesburg, respectively. Flow data were taken from WPRS (1979).

Tables E-1, E-3 and E-4 contain also salinity concentration data used to characterize the indicated point source discharges considered. The three subreaches mentioned in Table E-1 are as follow:

- subreach 1: Henderson-St. Vrain Creek confluence
- subreach 2: St. Vrain Creek confluence-Big Thompson confluence
- subreach 3: Big Thompson confluence-Kersey

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APPENDIX F

MEAN VALUES OF FLOW AND SALT MASS AND FLOW WEIGHTED MEAN TOTAL DISSOLVED SOLIDS FOR ANNUAL, SEASONAL, AND MONTHLY TIME INTERVALS, WATER YEARS 1965-77, FOR POINT SOURCE INFLOWS, RETURN FLOWS AND DIVERSION FLOWS TO AND FROM FOUR REACHES IN THE SOUTH PLATTE RIVER

Tables F-1, F-2, and F-3 contain the results of the materials balance analysis, averaged by year, season and month respectively, for the four reaches considered in the lower South Platte River, i.e. Henderson-Kersey, Kersey-Weldona, Weldona-Balzac, Balzac-Julesburg. Each table contain mean values of flow and salt mass flow and flow weighted mean total dissolved solids for point source inflows, diversion flows and return flows to and from the reach. The seasonal and annual tables have been computed using the monthly results. It should be mentioned that negative values of monthly return flows have been omitted in the seasonal and annual averages.

Table F-4 contains revised seasonal and annual averages of flow, salt concentration and salt mass flow for return flows to reach Kersey-Weldona. The revision has been made excluding those monthly flows for which a salt concentration exceeding 3000 mg/ ℓ was obtained in the basic computations. The revised averages were used to construct plot (b) in Figure 4-17 and the plots of Figure 4-19.

Figure F-1 is a sketch included to define the terms used in the computer output of the materials balance analysis.



Sketch to define terms used in computer output of material balance analysis. Figure F-1.

ANN	UAL RE	SULTS		
WATER YEAR	1	RIVER REAC 2	H 3	4. ***
TOTAL	POINT INFLOW	TO REACH (CMS) :	
5567890123456777777777777777777777777777777777777	14.69 8.669 11.8.69 14.69 14.69 14.69 14.69 14.69 14.69 18.88 18.88 19.68 19.68 13.84 19.58 13.84 19.58 13.84 19.58 13.84 19.59 13.84 19.59 13.84 19.59 10.5	548 577 568 577 577 577 5971 5971 2438 3 8 3	0.00 0.007 0.07 0.07 0.07 0.07 0.07 0.0	.34 1.924 .8791 .856796 .56796 .5756 .75704 .7570 .477
SALINI	ITY IN TOTAL	POINT INFLO	W TO REAC	H (MG/L) :
65 667 667 669 71 723 75 77 77 77	823.9 1292.6 960.0 1227.3 750.0 866.7 807.9 1146.5 1073.8 995.7 1210.6 1287.2	1246.5 13216.8 1438.8 1479.9 1195.0 11922.8 1259.1 12258.1 12274.6 12274.6 12274.6 1328.1 1428.1	$\begin{array}{c} 0 & 0 \\ 0 & 0 \\ 1 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 \\ \end{array}$	1041.0 1278.4 1077.8 1252.2 1146.3 1185.8 1189.4 1271.2 1177.7 1197.7 1264.8 1392.5
SALIN	ITY MASS IN T	OTAL POINT	INFLOW TO	REACH (T/D)
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Table F-1. Flow, salt concentration and salt mass flow averaged by year, water years 1965-77, for point source inflows, diversion flows and return flows, South Platte River between Henderson and Julesburg.

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1472.1 10554.2 15865.1 15865.1 1522654.2 1552654.2 155564.2 15556.2 11556.2 11566.2 1556.2 1556.2 1156.2 1556.2 1556.2 1556.2 1556.2 1556.2 1556.2 1556.2 1556.2 1556.2 1556.2 1556.2 1556.2 1556.2 1556.2 1556.2 1556.2 1557.2 15	TOTAL OUT	OUTFLOW F 1115.8 1348.2 1268.4 1351.4 1159.9 1057.6 1055.0 1202.6 1085.4 1055.4 1086.4 1152.6 1270.9 1387.2	M REACH (C 15.27 9.22 14.19 125.32 14.53 14.53 14.53 15.29 13.60 15.29 13.60 15.29 13.15 13.17	RIVER RE 2	SULT
9500. 97649. 97644. 977644. 977644. 9777. 99717. 99717. 10841. 100	FLOW FROM	ROM REACH 1259.7 13852.3 14297.5 12597.5 142927.5 12551.4 12551.4 12551.4 12551.4 12551.9 1459.9 1459.9	MS): 8.72 4.719 7.600 8.9050 8.993 7.6993 8.995540 8.55400 8.55400 8.55400 8.55400 8.55400 8.55400 8.55400 8.55400 8.55400 8.55400 8.55400 8.55400 8.55400 8.55400 8.55400 8.554000 8.55400000000000000000000000000000000000	ACH 3	S
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SULT Ξ A N N U AL R S WATER Year RIVER 2 $R \equiv A C H$ 3 4 1 TOTAL REACH GAIN FLOW (CMS) : 8.94 6.088 7.088 13.099999 11.0959999 20.0657.499 20.67.499 7.267627777 4.99277777 4.99337777 4.096 4.34.096 6399397808302 6399436139312 •••••• 4.714748982770518 4.76666667775655 4.64 4.64 3.83 SALINITY IN TOTAL REACH GAIN FLOW (MG/L) : 1443782490427944564904271443758264271144375934462861144739446286113866466511386466511344134 $2261 \cdot 1$ $1623 \cdot 60$ $1780 \cdot 50$ $1780 \cdot 50$ $24068 \cdot 4$ $1719 \cdot 50$ $1877 \cdot 50$ $1877 \cdot 50$ $1973 \cdot 30$ $1854 \cdot 30$ SALINITY MASS IN TOTAL REACH GAIN FLOW (T/D) : 707.239 1025.085 102520.85 110732.08 8257.11 8257.13 1058.80 1058.80 1058.80 825158.04 919.7 987.66 977.66 977.9 984.0 1152.9 1258.6 1059.0 1058.6 10758 10758 10758 3153202853003 0028271688554051 84536064605548 84536064605548 $971 \cdot 4$ $744 \cdot 9$ $817 \cdot 9$ $769 \cdot 7$ $1378 \cdot 3$ $1049 \cdot 3$ $1431 \cdot 5$ $846 \cdot 6$ $7691 \cdot 6$ $748 \cdot 2$ 1

Flow, salt concentration and salt mass flow averaged by season, water years 1965-77, for point inflows, diversion flows and return flow, South Platte River between Henderson and Table F-2.

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Table F-4. Revised seasonal and annual averages of flow, salt concentration and salt mass flow, for return flows to reach Kersey-Weldona, South Platte River, water years 1965-77.

YEARFALLWINTERSPRINGSUMMERTotal reach return flow (m^3/s) 653.95.84.4-4.8665.19.77.65.97.0676.24.56.27.86.2685.75.06.38.36.3695.65.06.99.87.0713.58.04.89.57.1728.75.210.27.67.9736.47.38.810.78.1747.27.26.08.77.3756.67.68.54.67.2766.89.28.26.17.8766.56.16.25.16.0Salinity in total reach return flow (mg/l)Salinity in total reach return flow (mg/l)652282.61703.21376.01575.01799.61645.11603.91787.51645.11630.21788.72007.71930.570.0161.11830.21676.816845.11603.91787.51648.61677.0 <t< th=""><th>WATER</th><th></th><th>SEASONAL</th><th>AVERAGE</th><th></th><th>ANNUAL AVERAGE</th></t<>	WATER		SEASONAL	AVERAGE		ANNUAL AVERAGE				
Total reach return flow (m^3/s) 653.95.84.4-4.8665.19.77.65.97.0676.24.56.27.86.2685.75.06.99.87.0704.57.2-9.17.6713.58.04.89.57.1728.75.210.27.67.9736.47.38.810.78.1747.27.26.08.77.3756.67.68.54.67.2766.56.16.25.16.0Salinity in total reach return flow (mg/l)652203.51771.41618.81830.21678.41828.01579.01601.11837.01709.61927.91678.41828.21828.21876.51837.61830.21678.41820.71927.91678.41079.61830.217211678.4182.018247.81927.91678.4 </td <td>YEAR</td> <td>FALL</td> <td>WINTER</td> <td>SPRING</td> <td>SUMMER</td> <td></td>	YEAR	FALL	WINTER	SPRING	SUMMER					
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	66	5.1	9.7	7.6	5.9	7.0				
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	67	6.2	4.5	6.2	7.8	6.2				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	68	5.7	5.0	6.3	8.3	6.3				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	69	5.6	5.0	6.9	9.8	7.0				
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728.75.210.27.67.9736.47.38.810.78.1747.27.26.08.77.3756.67.68.54.67.2766.89.28.26.17.8776.56.16.25.16.0Salinity in total reach return flow (mg/l)652203.51771.4661938.71482.61538.11688.6672196.31828.01579.01601.11833.0682270.71716.51645.11603.91787.5692282.61703.21376.01573.01709.6702185.21798.8-2007.71939.5712547.81796.81986.51872.31927.9721678.41819.51490.31809.61672.0732051.31702.11445.51837.41782.0741611.12034.92069.61840.31877.9752074.41608.41466.02346.51740.2761997.01635.61425.41910.91676.0772327.31624.21530.81908.81854.3Salt mass in total reach return flow (T/d)65733.8884.2617.9-764.3661121.2745.1897.01149.1979.6671176.4704.7845	71	3.5	8.0	4.8	9.5	/.1				
736.47.38.810.78.1747.27.26.08.77.3756.67.68.54.67.2766.89.28.26.17.8776.56.16.25.16.0Salinity in total reach return flow (mg/l)Salinity in total reach return flow (mg/l)652203.51771.41618.8-661938.71482.61538.11688.6672196.31828.01579.01601.1882270.71716.51645.11603.9682270.71716.51645.11603.9702185.21798.8-2007.7712547.81796.81986.51872.3721678.41819.51490.31809.6732051.31702.11445.51837.4741611.12034.92069.61840.3752074.41608.41466.02346.5772327.31624.21530.81908.8772327.31624.21530.81907.270851.0119.4-1569.6732051.0119.4-741611.1235.91005.8752074.41608.4761176.4704.7772327.31624.278197.0791149.1979.670851.0<	72	8.7	5.2	10.2	7.6	/.y 0 1				
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756.67.68.54.67.2766.89.28.26.17.8776.56.16.25.16.0Salinity in total reach return flow (mg/l)652203.51771.41618.8-1830.2661938.71482.61538.11688.61623.6672196.31828.01579.01601.11833.0682270.71716.51645.11603.91787.5692282.61703.21376.01573.01709.6702185.21798.8-2007.71939.5712547.81796.81986.51872.31927.9721678.41819.51490.31809.61672.0732051.31702.11445.51837.41782.0741611.12034.92069.61840.31877.9752074.41608.41466.02346.51740.2761997.01635.61425.41910.91676.0772327.31624.21530.81908.81854.3Salt mass in total reach return flow (T/d)65733.8884.2617.9-764.366845.21239.21005.8864.5987.2671176.4704.7845.01074.2977.6681121.2745.1897.01149.1979.669101.9733.3817.31334.	74	7.2	7.2	6.0	8.7	1.0				
766.89.28.20.17.0776.56.16.25.16.0Salinity in total reach return flow (mg/l)652203.51771.41618.8-1830.2661938.71482.61538.11688.61623.6672196.31828.01579.01601.11833.0682270.71716.51645.11603.91787.5692282.61703.21376.01573.01709.6702185.21798.8-2007.71939.5712547.81796.81986.51872.31927.9721678.41819.51490.31809.61672.0732051.31702.11445.51837.41782.0741611.12034.92069.61840.31877.9752074.41608.41466.02346.51740.2761997.01635.61425.41910.91676.0772327.31624.21530.81908.81854.3Salt mass in total reach return flow (T/d)65733.8884.2617.9-764.366845.21239.21005.8864.5987.2671176.4704.7845.01074.2977.6681121.2745.1897.01149.1979.669101.9733.3817.31334.01027.370851.01119.4-	75	6.6	7.6	8.5	4.0 ∠ 1	7 8				
776.56.16.25.110.0Salinity in total reach return flow (mg/l) 65 2203.51771.41618.8-1830.2 66 1938.71482.61538.11688.61623.6 67 2196.31828.01579.01601.11833.0 68 2270.71716.51645.11603.91787.5 69 2282.61703.21376.01573.01709.6 70 2185.21798.8-2007.71939.5 71 2547.81796.81986.51872.31927.9 72 1678.41819.51490.31809.61672.0 73 2051.31702.11445.51837.41782.0 74 1611.12034.92069.61840.31877.9 75 2074.41608.41466.02346.51740.2 76 1997.01635.61425.41910.91676.0 77 2327.31624.21530.81908.81854.3Salt mass in total reach return flow (T/d) 65 733.8884.2617.9-764.3 66 845.21239.21005.8864.5987.2 67 1176.4704.7845.01074.2977.6 68 1121.2745.1897.01149.1979.6 69 1101.9733.3817.31334.01027.3 70 851.01119.4-1569.61274.8 <td>76</td> <td>6.8</td> <td>9.2</td> <td>8.2</td> <td>C 1</td> <td>6.0</td>	76	6.8	9.2	8.2	C 1	6.0				
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	77	1314.0	858.8	822.7	835.3	330.0				