WIND ENGINEERING STUDY OF MOUNTAIN BELL DENVER SERVICE CENTER

by

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for

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Mountain Bell Denver Service Center

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LIST OF SYMBOLS

Symbol [Variable]	Definition
U	Local mean velocity
D	Characteristic dimension (building height, width, etc.)
ν	Kinematic viscosity of approach flow
$\frac{UD}{v}$	Reynolds number
Е	Mean voltage
А	Constant
В	Constant
n	Constant
Urms	Root-mean-square of fluctuating velocity
Erms	Root-mean-square of fluctuating voltage
U_	Reference mean velocity outside the boundary layer
Y	Height above surface
δ	Height of boundary layer
Tu	Turbulence intensity $U_{\rm rms}^{}/U_{\infty}^{}$ or $U_{\rm rms}^{}/U$
C _{pmean}	Mean pressure coefficient, $\frac{(p-p_{\infty})_{mean}}{\frac{1}{2} \rho U_{\infty}^2}$
C prms	Root-mean-square pressure coefficient, $\frac{(p-p_{\infty})_{rms}}{\frac{1}{2} \rho U_{\infty}^2}$
C _{pmax}	Peak maximum pressure coefficient, $\frac{(p-p_{\infty})_{max}}{\frac{l_2}{2} \rho U_{\infty}^2}$
C _{p_{min}}	Peak minimum pressure coefficient, $\frac{(p-p_{\infty})_{\min}}{\frac{1}{2} \rho U_{\infty}^2}$
ρ	Density of approach flow
() _{min}	Minimum value during data record
() _{max}	Maximum value during data record

LIST OF SYMBOLS (Cont.)

Symbol

Definition

р	Fluctuating pressure at a pressure tap on the structure ${}_{\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!$
$\mathbf{p}_{\mathbf{w}}$	Static pressure in the wind tunnel above the model

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1. INTRODUCTION

1.1 General

A significant characteristic of modern tall building design is lighter cladding and more flexible frames. These features combine to produce an increased vulnerability of glass lights and cladding to wind damage. In addition, increased use of pedestrian plazas has brought about a need to consider wind and gustiness in the design of these areas. Techniques have been developed during the past decade for wind-tunnel modeling of proposed structures which allow the prediction of wind pressures on cladding and wind environment about the building. Knowledge of pressures on the structure permits adequate but economical selection of window strength to meet selected maximum design winds while information on sidewalk level gustiness allows plaza areas to be protected by design changes before the structure is constructed. Where exhaust vents from underground parking garages or other obnoxious exhausts can enter pedestrian areas or air ventilation intakes, model tests of concentrations of the exhausts can point to design changes to alleviate the problem.

Modeling the aerodynamic loading on a structure requires special consideration of flow conditions in order to guarantee similitude between model and prototype. A detailed discussion of the similarity requirements and their wind-tunnel implementation can be found in References 1,2 and 3. In general, the requirements are that the model and prototype be scaled in geometry, that the approach mean velocity at the building site have a vertical profile shape similar to the full-scale flow, that the turbulence characteristics of the flows be similar, and that the Reynolds number for the model and prototype be equal. These criteria are satisfied by constructing a scale model of the structure and its surroundings and performing the wind tests in a wind tunnel specifically designed to model atmospheric boundary layer flows. Reynolds number similarity requires that the quantity UD/ ν be similar for model and prototype. Since ν , the kinematic viscosity of air, is identical for both, Reynolds numbers cannot be made precisely equal with reasonable wind velocities. Wind velocity in the wind tunnel would have to be the model scale factor times the prototype wind. However, for sufficiently high Reynolds number (>10⁵) a pressure coefficient at any location on the structure will be essentially constant with Reynolds number. Typical values encountered are 10⁸ for the full scale and 10⁶ for the wind tunnel model. Thus acceptable flow similarity is achieved without precise Reynolds number equality.

1.2 The Mountain Bell Denver Service Center (Telephone Building)*

A wind study was performed for the proposed Telephone Building in Denver, Colorado. The 323 ft high structure was modeled at a 1:180 scale. The objectives of the wind study were to obtain mean and fluctuating pressures on the building as well as wind velocity and gustiness in the plaza adjacent to the structure. In addition, a flow visualization study was performed to define overall flow patterns and regions where local flow features might cause difficulties in panel loading or pedestrian discomfort. Concentration measurements were made at numerous points near the surface around the building and in the plaza to determine the extent to which pedestrians and building air intakes would be subjected to exhaust gases from the underground parking garage vents.

*The designation Telephone Building is used throughout the text.

The Telephone Building will occupy the block between 17th and 18th Streets and between Curtis and Arapahoe Streets in Denver. The structure consists of a tower occupying the half-block nearest to 18th Street with a lower structure and large elevated plaza occupying the remaining area. The site is in the center of the downtown area on flat terrain. Surrounding structures range from nearly the same height on the southwest to parking lots on the north and northwest. The flow approaching the site crosses relatively flat terrain with low structures except for the tall buildings in the downtown area close the the building site.

2. EXPERIMENTAL CONFIGURATION

2.1 Wind Tunnel

The wind study was performed in the meteorological Wind Tunnel located in the Fluid Dynamics and Diffusion Laboratory at Colorado State University, Figure 1. The tunnel is a closed circuit facility driven by a 250 h.p. variable-pitch, variable-speed propeller. The test section is nominally 6 feet square and 88 feet long fed through a 9-to-1 contraction ratio. The test section walls diverge 1 in./10 ft and the roof is adjustable to maintain a zero pressure gradient along the test section. The mean velocity can be adjusted continuously from 1 to 120 fps. The facility is described in detail by Plate and Cermak [4].

2.2 Model

In order to obtain an accurate assessment of local pressures using piezometer taps, the model was constructed to the largest scale that would not produce serious blockage in the wind tunnel. A 1:180 scale model was constructed using 3/4 in. "Lucite" plastic for the tower portion of the structure on which pressure measurements were to be made and using styrofoam for the lower structure and plaza where flow visualization, velocity and diffusion data were required. A site plan is shown in Figure 2.

Piezometer taps (1/16 in. dia.) were drilled normal to the exterior surface at 46 locations on each side of the structure, at 16 locations on the top, and at several special points of interest such as door locations and behind the grillwork on the lower sides. The location of the taps on the structure is shown in Figures 3a to 3c. Of the 206 total

taps on the building, 68 were selected for measurement of fluctuating pressures and are marked by filled circles on Figure 3, 4 were in doors for which fluctuating measurements were obtained, and the remaining 134 taps were designated for mean pressure measurement.

An area of 1100 ft radius surrounding the building site was modeled in detail. Structures located within this region were modeled from styrofoam retaining the overall height and shape but omitting small surface details. The Building model and surrounding area was mounted on a 76 in. dia. turntable centered 84 ft from the test section entrance. That portion of the modeled area which did not fit on the turntable was placed upstream and downstream from the turntable and changed to match the turntable azimuthal position each time the turntable was rotated. The turntable indicated azimuthal orientation to \pm 0.1 degree.

The region upstream from the modeled area was covered with a randomized roughness constructed from bricks. A 12 in. high vortex generator provided a boundary layer trip at the entrance to the test section. The distribution of bricks was designed to provide a boundary layer thickness of approximately 50 in., a velocity profile power law exponent similar to that for a city environment, and a logarithmic velocity profile with a realistic roughness length. A photograph of the complete model in-place in the wind tunnel is shown in Figure 4. The wind-tunnel ceiling was adjusted after placement of the model to obtain a zero pressure gradient along the test section.

3. INSTRUMENTATION AND DATA ACQUISITION

3.1 Flow Visualization

Visualization of the flow in the vicinity of the model is helpful in understanding and interpreting mean and fluctuating pressures, in defining zones of separated flow and reattachment where pressure coefficients may be expected to be high, and in indicating areas where pedestrian discomfort may be a problem. Titanium tetrachloride smoke was released from sources on and near the model and motion pictures records made. Conclusions obtained from these smoke studies are discussed in section 4.1.

3.2 Pressures

Mean and fluctuating pressures were obtained at each of the 68 locations on the building indicated by filled circles on Figure 3. A 12 in. length of 1/16 I.D. plastic tubing connected the 68 pressure ports on the building to a 72 tap pressure switch mounted inside the model. The switch (Model 1) was designed and fabricated in the Fluid Dynamics and Diffusion Laboratory to minimize the attenuation of pressure fluctuations across the switch. Each of the 68 measurement ports was directed in turn by the switch to one of 4 pressure transducers mounted close to the switch. The switch was operated manually by means of a shaft projecting through the floor of the wind tunnel. A mechanical indexing feature locked the switch into each of the 18 required positions while a potentiometer provided an indication of the switch position on a digital voltmeter. The 4 pressure switch input taps not used for transmitting building pressures were connected to a common tube leading outside the wind tunnel and provided a means of performing

in-place calibration of the transducers. A photograph of the pressure switch in place is shown in Figure 5.

The pressure transducers used were "statham" differential straingage transducers (Model PM283TC) with a 0.15 psid range. They were selected for the stability and linearity in the working range required. The frequency response of the transducers was greater than 200 Hz adequately covering the range of frequencies encountered. A reference pressure was obtained by connecting the reference side of the transducer with plastic tubing to the static side of a pitot tube mounted in the wind tunnel free stream above the model building. In this way the transducer measured the instantaneous difference between the local surface pressure and the static pressure in the free stream above the model.

Each pressure transducer bridge was monitored by a Honeywell Accudata 118 Gage Control/Amplifier unit which provided excitation to the bridge and amplified the bridge output. These instruments are characterized by a very stable excitation voltage and amplifier gain. Output from the Honeywell signal conditioners was fed to an on-line 8 channel System Development, Inc., analog-to-digital conversion unit. The data was processed onto digital tape for later data analysis by computer. Resolution of conversion was \pm 0.0016 in pressure coefficient. All 4 transducers were recorded simultaneously for 16 seconds at a 240 sample per second rate. The results of an experiment to determine the length of record required to obtain stable mean and rms pressures is shown in Figure 6. A typical pressure port record was integrated for a number of time periods to obtain the data shown. Fluctuations in results for a 16 second average are within 1 percent for mean

pressure and 2 percent for fluctuating pressure. Definitions for the pressure coefficients are given in section 4.3.

Reduction of the raw data to usable form was performed on the Colorado State University CDC 6400 computer as described in Section 4.3.

The 134 pressure taps for which mean velocity only was recorded were connected to a 256 port pressure switch located outside the wind tunnel by 8 ft lengths of 1/8 I.D. plastic tubing. The 4 position switch (Model 0) was designed and fabricated in the Fluid Dynamics and Diffusion laboratory for this purpose. Each of the 134 measurement ports was connected in three switch positions to one of 64 output taps on the switch. These 64 pressures were directed in turn to a single Statham pressure transducer by a 64 port scanivalve pressure switch. In this way each pressure port on the structure was examined sequentially. The signal from the pressure swith the exception that computations recorded only mean values. The long tube lengths attenuated the fluctuating pressures sufficiently that fluctuating information could not be obtained.

3.3 Velocity

Velocity and turbulence intensity profiles were made upstream from the detailed model area and at the building location (with the model removed) for several approach flow directions. In addition, mean velocity and turbulence intensity measurements were made 0.2 in. (3.0 ft prototype) above the surface for 4 wind directions near the building at locations 1 through 8 shown in Figure 2. The surface measurements were intended to indicate the environment to which a pedestrian in the plaza area would be subjected.

Measurements were made with a single hot-wire anemometer mounted with its axis vertical. The instrumentation used was a DISA constant temperature anemometer (Model 55D05) with a 0.0004 in. dia. platinum (80%) - iridium (20%) sensing element 0.080 in. long. Output was read from a Hewlett-Packard integrating digital voltmeter (Model 2401C) for mean voltage and a DISA RMS meter (Model 55D35) for rms voltage.

Calibration was performed by placing the anemometer in the free stream near the pitot tube used to record wind tunnel velocity and recording the output for several velocities. The calibration data was fit to a variable exponent King's Law relationship

$$E^2 = A + BU^n$$

where E is the hot-wire output voltage, U the approach velocity and A, B and n are coefficients selected to fit the data. A typical calibration showing the linear relationship between E^2 and U^n is plotted in Figure 7. The above relationship was used to recover the mean veloicty at measurement points from the measured mean voltage. The fluctuating veloicty in the form $U_{\rm rms}$ (root-mean-square velocity) was obtained from

$$U_{\rm rms} = \frac{2 E E_{\rm rms}}{B n U^{\rm n-1}}$$

where E_{rms} is the root-mean-square voltage output from the anemometer. All turbulence measurements were divided by either local mean velocity U or mean velocity outside the boundary layer U_{∞} . Division by U gives an indication of the relative unsteadiness at the location while division by U_{∞} permits easy determination of the actual magnitude of rms velocity fluctuations at a point for various approach velocities.

3.4 Diffusion

Concentration measurements were made to determine the extent to which the environment about the structure would be exposed to exhaust gases emitted from the 4 underground garage vents. Surface measurements were made at 14 locations shown on Figure 2. The prototype conditions modeled were 9.5 ft/sec velocity from the vents with an 18 mi/hr ambient wind velocity. The purpose of the low ambient wind was to simulate a typical case where concentrations would be expected to be relatively high in the plaza area. Measurements were taken for each vent operating alone for 4 wind directions.

The exhaust gas used for the experiment was Kr-85, a beta emitting radioactive gas, diluted approximately a million times in air. The mixture was supplied to each vent in turn and regulated with a flow meter. Concentrations at the various plaza locations was determined by placing one end of a 1/8 I.D. plastic tube at the measurement location and drawing air into one of a bank of 16 Geiger-Mueller tubes with a suction pump. Counts emitted by the Geiger-Meuller circuitry were converted to concentrations by a suitable calibration against a known standard. Concentrations measured at each point were divided by the concentration of the gas supplied to the vents to record the concentration as a percentage of the source gas.

4. RESULTS

4.1 Flow Visualization

A 1200 ft. film is included as part of this report showing the characteristics of flow about the structure with smoke. A listing of the contents of the film is shown in Table 1. Several features can be noted from the visualization. With flow approaching the upper portion of the structure from a direction approximately parallel to a face, the flow was seen to separate from the upstream corner of the diagonals on the upstream edge of the side and to remain separated with a thin separated region across the entire face. Fluctuations in the separated flow indicated the possibility of relatively high pressure fluctuations on the side and the upstream diagonal. For flow at other angles, flow separated cleanly from the building with much less evidence of high pressure fluctuations on the surface.

Visualization of smoke near the surface indicated the plaza area should be reasonably well protected from strong winds and exhaust gases except for winds from the west through north. For those directions, a high velocity jet of air swept under the connecting roof between the tower and adjacent structure and continued across the plaza near the tower. Blocking that passageway provided protection to the plaza area. Smoke sources placed at the garage exhaust vents showed that the highest concentrations in the plaza would be expected for west through north winds where the jet discussed above carried garage exhaust into the plaza. Again, blocking the passage prevented some of the smoke from entering the plaza. For easterly winds, smoke from one exhaust vent (Curtis St. nearest 18th St.) was observed in the plaza in the region near the corner of 17th and Curtis St.

4.2 Velocity

Typical approach velocity profiles are shown in Figure 8a and b. One profile was taken 89 in. upstream from the model (1335 ft. prototype) and is characteristic of the boundary layer approaching the model. The boundary layer thickness, δ , was 52 inches corresponding to a prototype value of approximately 800 ft. In the form

$$\frac{U}{U_{\infty}} = \left(\frac{Y}{\delta}\right)^n$$

the velocity profile has an exponent n of 0.215 which is a reasonable value for city environments such as Denver with relatively low building heights extending right to the downtown area. The profiles plotted in Figure 8b are shown in semilogarithmic form. The roughness height indicated by the zero velocity intercept of the best fit line is 7.2 ft which is reasonable for the site modeled. A velocity profile taken at the building site with the building removed is shown in Figure 8a. Some modification to the approach flow is evident in the profile caused by nearby structures.

Profiles of longitudinal turbulence intensity are shown in Figure 9 for the upstream approach conditions and for the building site. Modifications to the profiles due to topography and local structures is evident. For the purpose of this report, turbulence intensity is defined as the root-mean-square of the longitudinal velocity fluctuations divided by the reference mean velocity U_{∞} at the outer edge of the boundary layer,

$$Tu_1 = \frac{U_{rms}}{U_{\infty}},$$

or as the rms velocity divided by the local mean velocity,

1

$$Tu_2 = \frac{U_{rms}}{U}$$

Mean velocity and turbulence intensity at plaza locations 1-8 shown in Figure 2 for 4 wind directions are listed in Table 2. Measurements were taken 0.2 in. (3.0 ft prototype) above the surface. Locations marked 'A' were repeat measurements with the passage from the plaza to Arapahoe adjacent to the tower portion of the structure blocked to prevent occurance of the high velocity jet of air noted in the flow visualization. The largest mean velocities were recorded at point 1 for 0 and 300 degree winds and point 2 for 0 and 90 degrees with velocities ranging from 50 to 85 percent of $U_{\rm m}$. These values dropped sharply when the passage was blocked. The highest 'gustiness' values (U $_{\rm rms}/{\rm U})$ were obtained for locations 8 for 300 degrees at 45 percent, 1A for 180 degrees at 38 percent, 3A for 300 degrees at 29 percent, 3 for 180 degrees at 28 percent, and 6 for 300 degrees at 27 percent. Large values of gustiness must be interpreted in terms of the magnitude of mean velocity since a low wind velocity can lead to large values as effectively as large rms velocities. The large values of U_{rms}/U for these locations are due in large part to low mean velocities. 4.3 Pressures

For each of the 206 pressure ports at each of the 10 wind directions (36 directions for 4 ports) examined (2164 total measurements), the data record was analysed to obtain pressure coefficients. One pressure coefficient was computed for the 134 mean pressure taps while 4 coefficients were computed for each of the fluctuating pressure taps. The first was the mean pressure coefficient

$$C_{p_{mean}} = \frac{(p - p_{\infty})_{mean}}{\frac{l_2}{2} \rho U_{\infty}^2}$$

where the symbols are as defined in the List of Symbols. It represents the mean of the instantaneous pressure difference between building pressure port and static pressure in the wind tunnel outside the boundary layer non-dimensionalized by the dynamic pressure $\frac{1}{2} \rho U_{\infty}^{2}$ outside the boundary layer. The magnitude of the fluctuating pressure was obtained by the rms pressure coefficient

$$C_{p_{rms}} = \frac{(p - p_{\infty})_{rms}}{\frac{l_2 \rho U_{\infty}^2}{2}}$$

in which the numerator is the root-mean-square of the instantaneous pressure difference.

If the pressure fluctuations followed a Gaussian probability distribution, no additional data would be required to predict the frequency with which any given pressure level would be observed. However, the pressure fluctuations do not follow a Gaussian probability distribution so that additional information is required to show the extreme values of pressure expected. The peak maximum and peak minimum pressure coefficients are used to determine these values:

$$C_{p_{max}} = \frac{(p - p_{\infty})_{max}}{\frac{l_{2} \rho U_{\infty}^{2}}{U_{\infty}^{2}}}$$
$$C_{p_{min}} = \frac{(p - p_{\infty})_{min}}{\frac{l_{2} \rho U_{\infty}^{2}}{U_{\infty}^{2}}}$$

The values of $p - p_{\infty}$ which were digitized at 240 samples-per-second for 16 seconds were examined individually by the computer to obtain the most positive and most negative values during the 16 second period. These were converted to Cp_{max} and Cp_{min} by non-dimensionalizing with the free stream dynamic pressure.

The four pressure coefficients were calculated by the CSU CDC 6400 computer and tabulated on microfilm. The list of coefficients is included as Appendix A. The tap code number in the appendix is given in Figure 3. The first digit of the code gives the building side while the second and third give sequential tap numbers on the side. Additional information provided in the appendix includes approach wind azimuth in degrees from true north, temperature in the wind tunnel in degrees F, barametric pressure in inches of Hg, and reference velocity outside the boundary layer in feet per second. The largest values of peak maximum C_p values were 1.25 to 1.43 on and adjacent to the diagonal corners for wind directions perpendicular to the diagonals. The largest values of peak minimum C_n occurred on and adjacent to the diagonal corners and near the top of each side with flow roughly perpendicular to a face. Values of -2.0 to -2.7 were common on and near the corner diagonal for these wind directions. Negative C_p values up to -2.0 were seen on the roof near the corners.

To insure that no flow pattern developed between the azimuths used for approach flow direction which would cause sharply higher pressure coefficients than were anticipated from the normally spaced data, one pressure tap was examined for small angular increments. Tap 422 was selected for examination for a range of approach flow azimuths from 45 to 65 degrees in one degree increments. The tap was chosen because of high negative mean, rms and peak minimum pressure coefficients and because smoke flow indicated a region of large amplitude fluctuations in a separated flow at that point. The results of that investigation are shown in Table 3. The pressure coefficients do reach a maximum value within the 20 degree span higher than indicated by the end-point values alone. However, the largest value of peak minimum pressure coefficient (-1.35 at 49 degrees) was only 7.3 percent larger than the value at 45 degrees indicating that no sharp peak in pressure coefficient appears in that azimuthal range.

In order to determine the pressures acting on the air doors opening from side 1 of the tower onto the plaza (see Figure 2), pressure taps were installed in the door recesses and data was taken for every 10 degrees of wind azimuth. Results of those measurements are listed in Table 4 and shown graphically in Figures 10 and 11. Part 'a' of each figure shows $C_{p_{rms}}$ while the 'b' portion gives $C_{p_{min}}$, $C_{p_{mean}}$, and P_{rms} $C_{p_{max}}$ in order from the center outward. Note that the zero is not placed at the origin on the latter set. The pressures on door 1 (nearest to Arapahoe st) are not large--maximum pressure coefficients are near one. For door 2, the positive peak does not exceed one; however, for an easterly wind, large negative values appear peaking at a $C_{p_{min}}$ of -2.35 for a 90 degree wind azimuth.

Determination of pressures on the two corner doors at 18th St. and Arapahoe St. was accomplished by installing pressure taps at the door locations. Data was obtained for every 10 degrees of wind azimuth. Results of the measurements are listed in Table 5 and are shown graphically in Figures 12 to 14. Table 5 lists pressure coefficients for the corner door on building side 2, for the corner door in building side 3, and for the instantaneous difference between the two doors. The information is presented in Figures 12 to 14 in the same way as for Figures 10 and 11 described above. The positive pressure coefficient on each door was less than one while the peak negative value reached -2.0 only for a wind azimuth of 320 degrees. The pressure coefficients for the instantaneous difference between the two doors reached both +2 and -2 in pressure coefficient for winds from 330 and 50 degrees respectively (Figure 14). Other wind directions showed more moderate pressures.

4.4 Diffusion

Concentration measurements of exhaust gases emitted from the 4 underground garage vents were divided by the concentration of the emitted exhaust gas to obtain a percentage of pollutant at a given location compared to the vented concentration. The data for the 14 points shown in Figure 2 for each exhaust vent for 4 wind directions is shown in Table 6. Presentation of the data for each vent operating alone permits the concentration at a location to be calculated assuming any desired distribution of exhaust gases to the four vents.

The largest concentrations were found at points 12 and 13 located on the sidewalk adjacent to vents 1 and 3. These locations--particulary 12--showed high concentrations from the adjacent vent for several wind directions. The plaza area in general showed low concentrations for all vents for all wind directions. Blocking the passage from the plaza to Arapahoe St. for a 300 degree wind increased concentrations somewhat at locations 1 and 2 but tended to decrease concentrations elsewhere.

CONCLUSIONS

A boundary layer flow over the Telephone Building model was established whose characteristics compared favorably with the expected flow over the Denver area. Flow visualization showed fluctuating separation features around the diagonal corners suggesting high values of pressure coefficient in those regions. Observation of the flow showed rather large velocities in the plaza near the entrances to the main structure. Blocking the passage from the plaza to Arapahoe St. provided a large reduction in velocity.

Measurements of fluctuating velocity in the plaza area indicated the largest value of root-mean-square velocities occurred at plaza points 8, 1 and 1A for 300, 0 and 90 degree wind azimuths respectively. RMS velocities were 6 to 7 percent of the reference velocity above the boundary layer. These correspond to a local turbulence intensity of 45, 7 and 16 percent of the local mean velocity. Only the first of these local values is large. Points experiencing relatively high local turbulence intensity (greater than 30 percent of local mean) were point 8 at 300 degrees and point 1A at 180 degrees. These points both experienced low values of local mean velocity.

Pressure measurements on the structure supported the flow visualization conclusion that the area near the diagonal corners would receive the largest pressure coefficients. The largest peak negative pressure coefficient was -2.72 at tap 228 for a wind azimuth of 330 degrees. Other corner locations showing high negative coefficients were taps 102 and 104 for a 330 degree wind direction. Negative values of above -2.0 were common on the diagonal corners. In addition to showing the largest negative pressures, the corners also showed the largest positive

pressure coefficients. Tap 403 recorded a +1.43 at 180 degrees, tap 201 had a +1.42 at 0 degrees, and tap 228 recorded a +1.35 for 270 degrees. Several other values above +1.2 were also noted.

Diffusion measurements of exhaust gas emitted from the garage vents showed generally low concentrations in the plaza area. The highest concentrations were observed at sidewalk level immediately adjacent to the Curtis Street exhaust vents.

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TABLE 1

MOTION PICTURE SCENE GUIDE

SCENE	WIND	PASSAGE 1	PASSAGE 2	SOURCE	SOURCE
попрык	112. (1)	(2)	(3)	LUDVALION	LOOKITON (4)
1	300°			Ground	Data point 3
2					Data Point 1
3	"	Х			Data Point 1
4					Data Point 5
5					Data Point 13
6	н	Х		11	17th & Arapahoe
7	**			"	Data Point 13
8					Data Point 14
9					Data Point 8
10				"	Data Point 11
11				11	Data Point 12
12					Data Point 2
13					Data Point 13
14			Х	"	Data Point 13
15		Х	Х	11	Data Point 13
16	н	Х			Data Point 13
17				200'	Upwind Side
18				300'	Upwind Side
19				Roof	Penthouse Lee
20				200'	Upwind of Bldg
21	300°-255°			200'	Bldg. rotated CW
22	255°-315°			200'	Bldg. rotated CCW
				5777, 201 GP	0

(1) All data taken at 24 fr./sec. and a wind velocity of 10 ft./sec.

- (2) Passage 1 represents passage from plaza to Arapahoe St. adjacent to tower portion of structure. X indicates passage was closed to air movement.
- (3) Passage 2 represents passage from plaza to 17th St. pedestrian bridge. X indicates passage was closed to air movement.

(4) Data point locations are shown in Figure 2.

TABLE 1 (Cont.)

SCENE NUMBER	WIND AZ.	PASSAGE 1	PASSAGE 2	SOURCE ELEVATION	SOURCE LOCATION
23	000		Х	Ground	Data Point 1
24	"				Data Point 5
25					17th & Arapahoe
26					Data Point 13
27				"	Data Point 14
28	. 11			11	18th & Arapahoe
29					Data Point 3
30	"	Х		"	Data Point 3
31	"			"	Data Point 5
32					Data Point 6
33	"			"	Data Point 12
34	"			н	Data Point 2
35	"			"	Data Point 11
36					18th & Curtis
37	"			"	18th
38	"			11	Plaza from NE
39	090			11	18th & Curtis
40	"			"	Data Point 8
41				11	Data Point 11
42	"			н	Data Point 2
43				п	Data Point 12
44				11	Data Point 5
45			Х	11	Data Point 5
46		Х	Х	11	Data Point 5
47				н	Data Point 5
48					Data Point 14
49					Data Point 3
50		Х		н	Data Point 3
51				н	Data Point 13
52	н			п	Data Point 7
53	"			"	Data Point 2
54	180			п	Data Point 6

TABLE 1 (Cont.)

SCENE NUMBER	WIND AZ.	PASSAGE 1	PASSAGE 2	SOURCE ELEVATION		SOUI LOCAT	RCE FION
55	180			Ground	Data	Point	12
56	"			U	Data	Point	5
57				н	Data	Point	2
58				н	Data	Point	11
59	"			11	Data	Point	8
60	"			н	Data	Point	7
61	"				Data	Point	13
62	"			"	Data	Point	3
63				н	Data	Point	14

TABLE 2

Wind Azimuth	Location	U/U∞ Percent	U _{rms} /U∞ Percent	U _{rms} /U Percent
000	1	84.5	6.24	7.4
	1A*	14.4	3.00	20.8
	2	50.6	7.12	14.1
	2A	23.5	4.97	21.1
	3	25.0	4.63	18.4
	3A	22.1	4.45	20.1
	4	29.9	4.46	15.0
	5	38.6	5.34	13.8
	6	23.5	5.42	23.0
	7	20.8	3.84	18.5
	8	24.5	5.78	23.6
090	1	25.5	5.53	21.7
	1A	38.6	6.26	16.2
	2	77.6	4.21	5.42
	2A			
	3	18.6	4.51	24.2
	3A	15.1	3.44	22.7
	4	20.3	3.96	19.5
	5	22.6	3.88	17.2
	6	31.0	5.61	18.1
	7	23.1	4.12	17.9
	8	63.1	4.29	6.8

MEAN AND FLUCTUATING VELOCITIES IN THE PLAZA

* Locations designated 'A' indicate measurements were taken with passage from plaza to Arapahoe St. closed.

TABLE 2 (Cont.)

Wind Azimuth	Location	U/U_{∞} Percent	U_{rms}/U_{∞} Percent	U _{rms} /U Percent
180	1	20.8	3.28	15.8
	1A	15.1	2.99	37.7
	2	25.5	4.77	18.7
	2A	26.6	4.81	18.1
	3	10.7	2.99	28.0
	3A	21.7	3.95	18.2
	4	15.1	3.58	23.6
	5	15.9	3.65	23.0
	6	26.6	4.33	16.3
	7	32.2	5.49	17.1
	8	14.4	3.33	23.0
300	1	60.1	5.02	8.3
	1A	5.9	1.38	2.3
	2	33.5	5.26	15.7
	2A	14.0	3.63	25.9
	3	17.2	3.58	20.8
	3A	11.2	3.26	29.1
	4	18.1	3.58	19.8
	5	14.0	2.72	19.4
	6	17.2	4.68	27.2
	7	14.8	3.02	20.5
	8	15.5	7.02	45.2

TABLE 3

PRESSURE DATA FOR ONE DEGREE WIND AZIMUTH TAP NO 422

	Primar	y Data			1	Repeat	Data	
Wind Azimuth	Mean	RMS	P.Max	P.Min	Mean	RMS	P.Max	P.Min
045	440	.202	.152	-1.261	436	.203	.199	-1.315
46	423	.194	.261	-1.161	431	. 211	.175	-1.305
47	412	.201	.152	-1.262	395	.191	. 374	-1.142
48	388	.191	.284	-1.129	362	.183	.235	-1.223
49	379	.189	.158	-1.354	353	.182	.155	-1.264
50	352	.176	.186	-1.066	337	.169	.232	-1.091
51	322	.161	.134	-1.057	337	.164	.186	-1.132
52	316	.156	.160	-1.168	296	.143	.170	-1.285
53	297	.134	.109	991	287	.125	.090	-1.035
54	283	.127	.242	-1.186	276	.115	.183	867
55	272	.114	.126	919	262	.104	.255	779
56	263	.100	.163	890	256	.093	.051	959
57	253	.093	.054	862	254	.082	.137	707
58	258	.096	.087	808	248	.079	.082	887
59	244	.076	.044	781	240	.075	.008	823
60	243	.072	.052	647	237	.068	.029	624
61	245	.066	.039	756	236	.065	.042	676
62	238	.060	.042	545	233	.057	.028	505
63	231	.058	020	514	232	.054	.002	606
64	226	.051	.015	738	229	.052	011	514
65	226	.052	046	482				

TABLE 4

PRESSURE DATA FOR THE AIR DOORS

PROJECT NO 6644

AIR DOOR 1

~

HIND DIRECTION	MEAN	RHS	HAXINUH	HINIMUH
	COFFEICIENT	COFFEICIENT	PRESSURE	PRESSURE
	COLFFICIENT	CUEFFICIEN	COEFFICIENT	COEFFICIENT
٥	255	168	/28	
10	- 170	155		/2/
20	- 152	108	877	-,/03
50	181	0.75	. 377	525
40	- 142	054	116	361
50	208	0.74	100	
60	507	.069	- 006	506
70	508	079	- 480	
	255	.095	168	
90	- 174	105	261	492
100	- 184	109	287	529
110	201	126	207	332
120	254	114	REE	/51
1 50	227	107	. 555	/0/
140	260	0.95	. 290	
150	269	108	. 139 E10	590
160	201	127	848	007
170	524	194	. 545	900
180	365	152	204	-1.000
190	590	129		-1.050
200	362	124		-1.058
210	354	115		900
220	511	110		-1.017
230	- 204	096	. 457	-1.055
240	. 059	120	.209	/46
250		157		431
260	.067	187		413
270	050	194		36 /
280	- 181	150	. 132	360
290	- 506	188		
500	- 406	168	. 369	/86
510	- 467	184	.430	825
520	- 407	121	.314	-1.060
350		122		
540	- 368	142	.1/3	/60
350	- 287	150	. 36 /	
334	201	.128	. 374	787

TABLE 4 (CONTINUED)

PRESSURE DATA FOR THE AIR DOORS

PROJECT NO 6644

AIR DOOR 2

		MEAN	RMS	MAXIMUH	MINIMUM
ALAU DIREC	RECTION	PRESSURE	PRESSURE	PRESSURE	PRESSURE
		COEFFICIENT	COEFFICIENT	COEFFICIENT	COEFFICIENT
٥		501	.096	232	- 996
10		431	. 079	150	- 704
20		566	. \$62	159	- 650
30		262	. 057	067	- 479
40		165	.050	002	521
50		200	.072	. 026	- 461
60		337	.077	151	676
70		507	.085	252	818
80		665	.111	341	-1.585
90		795	.172	271	-2.350
100		826	. 192	240	-1.842
110			.211	064	-1.957
120		649	.205	018	-1.777
1 3 0		302	.170	.064	-1,192
140		155	.119	. 356	-1.052
150		033	.105	.291	593
160		020	.110	. 501	622
170		.043	.139	.655	612
1 80		050	.104	. 425	552
190		091	.101	. 421	359
200		139	.120	. 626	418
210		190	.148	. 758	556
220		184	.150	. 454	570
230		176	.111	. 541	755
240		045	.149	.612	475
250		.046	.179	. 890	405
260		021	.209	.952	472
270		140	.161	.717	505
280		275	.108	.227	580
290		410	. 086	008	804
300		504	.076	284	866
310		526	.094	217	900
520		466	.082	176	874
550		458	.077	175	
540		469	. 086	170	954
350		479	.085	176	820
TABLE 5

PRESSURE DATA FOR THE CORNER DOORS

CORNER SIDE 2

PROJECT NO 6644

	MEAN	RMS	MAXIMUM	MINIM
WIND DIRECTION	PRESSURE	PRESSURE	PRESSURE	PRESSURE
	COEFFICIENT	COEFFICIENT	COEFFICIENT	COEFFICIENT
C	.295	.134	. 815	- 121
1 0	. 192	.109	. 777	- 314
20	222	.107	. 349	-1 112
50	508	.217	.090	-1.511
40	580	.210	015	-1 628
50	531	.230	. 151	-1 677
60	441	.199	0.000	-1 689
70	440	.149	0.000	-1.174
	467	.117	121	-1 076
90	496	. 395	201	- 978
1 0 0	499	. 070	- 194	- 869
110	467	. 054	296	- 645
120	451	. 050	240	- 619
1 3 0	375	. 045	199	591
140	529	.046	167	- 490
150	302	. 385	150	862
160	469	.106	157	
170	556	.104	0.000	-1.004
1 🖯 C	456	. 307	044	771
190	344	. 374	.075	758
200	263	. 364	.015	550
210	240	.070	. 029	699
220	210	.067	.224	772
230	196	. 056	025	506
240	243	.045	091	402
250	294	.046	147	467
260	325	.050	129	505
270	304	.057	095	479
280	271	.070	0.000	554
290	251	.082	.101	684
500	254	.107	.206	751
5 1 C	295	. 126	.175	
320	326	. 1 32	.314	879
350	205	.141	. 4 3 6	720
540	.055	.145	.639	579
350	.257	.149	.978	127

TABLE 5 (CONTINUED)

PRESSURE DATA FOR THE CORNER DOORS

PROJECT NO 6644

CORNER SIDE 3

	MEAT	RMS	MAXIMUM	MINIMUM
WIND DIRECTION	PRESSURE	PRESSURE	PRESSURE	PRESSURE
	COEFFICIENT	COEFFICIENT	COEFFICIENT	COEFFICIENT
\$. 156	. 162	. 699	- 441
1 C	.246	.114	. 704	072
20	.176	. 126	. 884	249
30	350	. 124	. 499	415
40	195	.127	. 555	- 684
50	206	. 150	.261	- 884
60	177	.127	.220	- 795
70	199	.096	. 305	665
80	241	.077	. 069	565
90	510	. 370	052	572
100	346	.054	151	559
1 1 0	-,363	.045	186	516
120	354	. 342	167	506
1 3 0	328	. 342	154	499
140	302	.042	150	452
150	306	.115	059	-1.490
160	556	.200	0 7 7	-1.592
170	592	.145	101	-1.664
180	474	.106	098	-1.066
190	365	.071	051	861
200	325	.075	041	766
210	271	.054	088	565
220	237	.064	057	797
230	242	.071	054	761
240	515	.049	168	480
250	389	. 052	252	593
260	447	. 050	201	658
270	455	.065	225	694
200	471	.082	245	995
290	510	.106	185	-1.192
500	563	. 151	154	-1.457
310	659	. 189	.005	-1.625
520	810	.257	252	-2.086
550	789	.221	194	-1.745
340	360	.184	.222	-1.447
350	060	. 157	. 449	925

TABLE 5 (CONTINUED)

PRESSURE DATA FOR THE CORNER DOORS

SIDE 2-SIDE 5

PROJECT NO 6644

.

HIND DIRECTION	MEAN PRESSURE	RMS PRESSURE	PRESSURE	MINIMUM
	COEFFICIENT	COEFFICIENT	COEFFICIENT	COEFFICIENT
٥	.139	.142	1.093	- 205
T G	065	.104	. 302	- 657
20	598	.210	.057	-1.612
30	479	.231	005	-1.898
40	307	.186	002	-1.468
50	525	. 152	.072	-1.618
60	264	.115	.049	-1.195
70	242	.086	. 026	691
	226	.067	024	605
90	187	.054	. 0 3 8	524
100	142	.034	058	359
110	104	. 026	.060	216
120	077	.025	.010	180
130	046	.024	.080	214
140	027	.021	.057	132
150	.004	.095	1.195	590
160	.087	.176	1.244	423
170	. 056	.126	1.101	397
180	. 0 3 8	. 121	. 849	405
190	. 021	.103	.691	648
200	.062	.087	.612	242
210	.051	.079	. 529	485
220	.027	.057	.594	541
230	.045	.045	.415	196
240	.070	.020	.176	.005
250	. 095	.026	.248	.015
260	. 122	.034	.312	041
270	. 152	.041	. 55 1	. 021
200	.200	. 058	.652	026
290	.260	. 0 8 2	.717	.011
300	. 300	.115	.970	134
310	. 346	.136	1.097	060
320	. 484	.235	1.805	016
330	.587	.264	2.084	026
340	. 393	. 190	1.552	070
350	.297	.175	1.200	116

TABLE 6

EXHAUST VENT DIFFUSION DATA

WIND DIRECTION 0 DEGREES

SAMPLING		PERCENT OF	EXHAUST CONCENTR	ATION
LOCATION	VENT 1	VENT 2	VENT 3	VENT 4
1	.007	.000	.030	1.370
2	.306	.116	.356	1.820
3	.000	.000	.031	1.980
4	.082	.000	6.090	1.030
5	.722	.156	1.720	.429
6	.112	.001	2.000	.630
7	.098	.003	3.230	1.130
8	.007	.004	.015	.114
9	.007	.017	.112	2.500
10	.033	2.140	. 226	.194
11	.189	5.960	.048	.073
12	33.100	1.540	.709	.193
13	.006	.000	.362	4.070
14	.034	.007	.106	.865
	WIND	DIRECTION 90	DEGREES	
1	.008	.089	.008	.014
2	.004	.099	.005	.024
3	.048	.123	.730	.157
4	.063	.194	.003	.020
5	.189	.414	.004	.003
6	5.880	3.920	.006	.014
7	.838	.644	.005	.021
8	.002	.006	.000	.000
9	.032	.068	.004	.051
10	.000	.000	.013	.012
11	.006	.304	.003	.000
12	10.500	7.890	.003	.005
13	.668	. 363	32.400	.678
14	1.080	. 294	4.240	3.680

TABLE 6 (Continued)

WIND DIRECTION 180 DEGREES

SAMPLING		PERCENT OF	EXHAUST CONCENT	RATION
LOCATION	VENT 1	VENT 2	VENT 3	VENT 4
1	1.090	.025	.044	.000
2	1.370	.060	.009	.000
3	.537	.008	2.910	.013
4	.762	.033	.001	.000
5	.629	.016	.003	.000
6	.169	.005	.005	.000
7	.501	.027	.009	.000
8	.234	.135	.504	.889
9	1.010	.020	.001	.000
10	.713	.057	.006	.000
11	1.770	4.800	.215	.001
12	17.900	.064	.012	.003
13	.103	.006	31.400	.002
14	.282	.035	2.070	4.840

WIND DIRECTION 300 DEGREES

SAMPLING		PERCEN	Γ ΟΓ ΕΧΗΑυ	IST CONCENTR	ATION	
LOCATION	VENT 1	VENT 2	VENT 3	VENT 3*	VENT 4	VENT 4*
1	.013	.000	.590	1.300	.371	.234
2	.046	.001	.770	1.100	.382	.188
3	.045	.005	.500	.252	1.220	.946
4	.033	.012	2.890	2.750	.258	.188
5	.107	.005	.100	.969	.297	.204
6	.690	.030	3.300	2.360	.279	.146
7	.034	.004	1.950	1.530	.215	.123
8	.147	.230	.056	.068	1.860	1.810
9	.025	.006	.695	1.250	.467	.256
10	1.350	8.510	.450	.612	.158	.140
11	5.450	6.370	.720	.643	.175	.111
12	26.400	.636	.858	.791	.100	.110
13	.024	.010	5.660	4.560	.960	.987
14	.187	.013	.113	.055	.913	.908

* Measurements taken with door from plaza to Arapahoe St. closed.

APPENDIX A

PRESSURE DATA

Notes -

- Pressure coefficients are defined in section 4.3
 Pressure tap designation is explained in Figure 3
- Pressure taps found to have erroneous information have been deleted in the data.

WIND DIRECTION	0		TEMPERAT	TURE	69.50	DEGREES	F
BAROMETRIC PRESS	25.05	1 N	HG V	ELO	CITY	50.67FPS	

PRESSURE	MEAN	RMS	MAXIMUM	HINIHUM
TAP	PRESSURE	PRESSURE	PRESSURE	PRESSURE
NUMBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COFFFICIENT
137	454			COLF COLEMA
136	775	.215	240	-1 502
1 59	524			
140	535			
141	482			
142	469			
145	412	.097	- 118	- 742
144	454			
145	- 440	694	- 151	015
146	515			
201	.639	207	1 124	
202	479	219		010
203	511	170	. 995	560
204	801	1.45		0.000
205	35.0		. (95	15/
206	205			
207	188			
209			.445	255
200	. 178			
210		.000	.114	-,495
211	540			
212	. / 39			
212	.032			
213	. 592			
214	. 555			
215	. 458			
216	. 344			
217	.230			
218	. 058			
219	202			
220	. 523	.200	1.269	178
221	.512			
222	. 345	. 152	. 851	057
225	. 390			
224	.516			
225				
226	006			
227	236	.084	.087	606
229	606	.110	271	-1.556
229	. 365			
230	. 312			
231	. 557			
252	.516			
255	.292			
234	.250			
255	. 154			
256	040			
257	542			
258	.075	. 119	. 493	482
259	. 322			
240				
241	.271			
242	.252			
245	184		544	- 156
244	.017			
2.44				



PRESSURE	MEAN	RMS	MAXIMUM	WITHIN
TAP	PRESSURE	PRESSURE	PRESSURF	Parssigr
NUMBER	COEFFICIENT	COFFFICIENT	COFFEICIENT	CAFFEICIENT
1	155	. 111	EAA	EVEFF ICIEIII
2	- 218	• • • •	. 344	
3	- 705	142	- 207	
	- 277	. 142	29/	-1.456
-				
-	146			
	592			
9	891			
10	895			
11	255			
12	191			
15	297			
14	347	.115	050	959
15	969			
16	-1.115	.185	371	-1.999
17	460			
18	086			
101	603	.096	304	-1,106
102	540	.086	275	911
103	486	.082	227	875
104	516	.092	229	882
105	540			
106	551			
107	571	.107	278	-1.017
108	525	.104	216	959
109				
110	491			
111	557			
112	517			
115	557			
114	512			
115	560			
116	558			
117	550			
118	528			
119	542			
120	598	. 121	- 212	-1.721
121	641			
122				
125	672			
124	- 621			
125	- 565	4.87	- 284	- 021
126	- 521			
127	- 477	100	- 180	- 807
128	- 449			- 788
120	- 768			
150	- 744			
181	- 75.4			
182	- 761			
188	- 724			
184	- 613			
1 85	- 516			
186	- 166			
	. = 0 0			



	IND DIRECTION	0 TE!	PERATURE 69.5	DEGREES F
84	ROMETRIC PRESS	25.05 IN HG	VELOCITY	50.67FPS
PRESSURE	MEAN	RMS	HANTHUN	
TAP	PRESSURE	PRESSURE	PRESSURE	POESSURE
NUMBER	COEFFICIENT	COFFEICIENT	CASESICIENT	CASECICIENT
407	- 459	164	- 361	CULFF ICILL:
409	410	357	- 204	0/8
409	- 359	060	- 145	
410	- 405			04
411	481			
412	- 445			
415	- 454			
414	- 412			
415	591			
416	595			
417	596			
418	385			
419	585			
420	450	071	- 211	761
421	455		• 2 1 1	
422	496	. 158	- 279	- 728
425	410		.2.3	123
424	525			
425	454	. 057	- 227	
426	404			
427	375	. 36 1	- 175	- 604
428	599	.057	- 212	- 645
429	445			
430	495			
451	461			
432	446			
455	449			
434	192			
435	428			
436	429			
437	419			
458	575	.135	261	-1 449
459	495			
440	494	.094	292	- 826
441	465			
442	480			
445	428	.090	211	
444	425			• • • •
445	435	.090	175	-1.360
446	455			

TEMPERATURE 69.50 DEGREES F BAROMETRIC PRESS 25.05 IN HG VELOCITY 50.67FPS PRESSURE MEAN RMS MAXIMUM MINIMUM TAP PRESSURE PRESSURE PRESSURE PRESSURE NUMBER COEFFICIENT COEFFICIENT COEFFICIENT COEFFICIENT 245 -.250 .112 .265 -.692 246 -.472 501 -.457 . 060 -.255 -.755 302 505 .041 . 085 . 361 -.252 304 .145 .097 . 521 -. 186 505 .256 306 .209 507 308 509 . 369 .257 . 985 -.635 510 .679 511 -. 597 312 -.189 515 .001 514 . 156 515 .261 316 . 542 517 .412 518 .481 519 .408 520 -.210 .065 . 047 -. 456 521 -.057 322 .034 . 380 . 525 -.258 325 .217 524 .201 325 526 .404 527 . 356 .242 1.057 -.552 529 .517 .185 1.097 .015 329 -.418 550 -.228 351 -.000 552 . 056 355 . 155 334 . 188 355 .224 356 .235 357 .176 358 -. 555 .064 -.121 -.654 559 -.007 540 -.004 .068 . 385 -.206 541 .136 542 .149 545 .167 . 086 .505 -.096 344 .111 545 .047 .154 .575 -.446 546 .099 401 -. 574 .015 -. 510 -.415 402 -. 468 -. 188 -1.021 405 -. 395 .082 -.119 -.985 404 -. 398 .084 -.087 -.905 405 -.405

WIND DIRECTION O

ŀ.i

36

-. 399

	WIND DIRECTION	2: TE*	PERATURE 60.5:	CERREES F
	BARCHETRIC PRESS	24.95 115	SE. 22174	5: . 72525
PRESS	PE - "E1".	2 M S	WIN WIN	
TAP	PRESSURE	PRESSURE	PRESSURE	PRESSURE
BER	COEFFICIENT	COEFF! CIENT	COEFFICIENT	COEFFICIENT
,	506	. 125	. 52 "	- 814
2	226			
3	546	. 25	. 157	- 956
4	519			
5	- 263			
6	- 274			
-	- 518			
	- 515			
9	- 157			
	- 100			
	- 648			
	045			
1 2				
	0=0		36	
		150	171	
	89		525	59
	52			
18	361			
101	405	. 364		
102	545	. 362	144	650
105	307	. 361	15	601
104	556	. 366	070	6''
105	32			
.06	329			
107	413	.075	091	704
108	369	. 385	101	746
109	350	.010	096	446
110	406			
111	316			
112	524			
113	517			
114	292			
115	355			
:16	559			
117	355			
1.16	552			
119	546			
:2:	526	.056	005	515
121	326			
122	2			
123	540			
124	329			
:25	547	. 067	101	562
:26	52 1			
12	519	. 084	.056	657
126	367	.102	.090	949
129	356			
150	55 5			
131	574			
: 52	349			
151	547			
154	554			
: 55	559			
: 36	554			



PRESSURE	MEAN	RMC	W1	
TAP	PRESSURF	PRESSURE	PPFcc PF	20555.05
MBER	COEFFICIENT	COFFFICIENT		TRESSURE .
: 37	352			
. 58	- 692		- 278	
. 39	- 217		2 0	65.
.40				
141	- 554			
: 42	- 545			
145	- 540	16.7		6.8.2
1 4 4	- 350		22	552
: 45	- 411	* 6 *		70.
:46	- 447			0
201	525		8.2	
2:2	- 695	2.0		
203	150	266		555
204	. 222	183		
205	. 256			2
206	024			
207	- 077	16.4		207
208				20
209	- 195	156		
210	- 515			2
2:*	585			
2:2	- 558			
2.3	- 254			
2:4	181			
2:5	070			
2:6	. 159			
217	022			
219	107			
219	221			
220	580	228	554	-' 666
221	284			. 900
222	059	145	\$27	- 868
223	.041			.095
224	.011			
225				
226	151			
227	203	. 053	020	- 585
220	324	.059	149	547
229	.145			
250	549			
231	56 1			
252	081			
255	000			
234	015			
235	061			
256	149			
237	252			
250	443	. 172	.015	-1,259
259	041			
240				
241	. 020			
242	. 027			
245	000	. 055	.191	207
244	157			

WIND DIRECTION 20 TEMPERATURE 60.50 DEGREES F BAROMETRIC PRESS 24.95 IN HG VELOCITY 50.72FPS

WIND DIRECTION	20		TEMP	RATURE	68.50	CEGREES	F
BAROMETRIC PRES	\$ 24.95	11:	HŞ	VELOC	: 1 4	50.72FPS	

PRESSURE	MEAN	RMS	MAYTMIN	M 7 1 7 M 7 M
TAP	PRESSURE	PRESSURE	PRESSURF	Perscuer
NUMBER	COEFFICIENT	COEFFICIENT	COFFFICIENT	COEFE LAIFA
107	515	.115	- 154	-1 ROE
409	441	.115	- 364	-1 126
409	405	.112	- 146	0.75
410	492			
411	370			
412	495			
413	440			
414	451			
415	595			
416	409			
417	391			
418	378			
419	377			
420	507	.140	105	-1 225
421	447	001 005		
422	517	.078	255	- 802
425	419			
424	516			
425	417	.090	118	-1.062
426	376			
427	360	.096	364	-1.042
428	420	.109	165	-1.508
429	599			
450	500			
451	446			
432	438			
455	446			
434	106			
4 3 5	408			
436	406			
437	401			
459	524	. 152	151	-1.462
439	440			
440	467	.102	201	921
441	465			
442	459			
445	446	.157	007	-1.460
444	596			
445	457	. 150	122	-1.512
446	475			



PRESSURE	MEAN	RMS	MAXIMUM	HINIMUM
TAP	PRESSURE	PRESSURE	PRESSURE	PRESSURE
NUMBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COEFFICIENT
245	320	. 38 3	:36	6:9
246	325			
301	576	.142	261	- ' . 65 '
302			× `	
505	.200	. 135	. 720	195
504	.410	. 151	.975	000
505	.490			
506	. 551			
507	720			
500	. /29			.694
309	. (69	.200	. 559	.2
811				
512	- 005			
818	003			
514	479			
515	599			
316	678			
517	.768			
518	.802			
519	. 754			
520	039	.091	. 555	559
521	.254			
522	. 324	.151	. 75 '	:49
525	. 560			
324	.620			
525	.724	.012	. 759	.688
326	.706		a - 1983	A
527	.657	.206	.205	.046
520	. 306	.207	1.106	999
529	427			
550	074			
551	.179			
332	. 364			
884				
534				
336	594			
557	.511			
358	219	. 091	.224	671
339	.111			
340	.265	.109	. 686	000
341	. 450			
342	.497			
545	. 559	. 157	1.095	. 152
344	. 495			
545	. 326	. 157	. 848	304
346	086			
401	:25	.015	.075	265
402	500	.169	.011	-1.307
405	450	. 156	. 020	-1.045
404	442	. 126	724	-1.024
405	456			
406	447			

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	WIND DIRECTION	45 TEM	PERATURE 69.50	CEGREES F
8	AROMETRIC PRESS	24.95 11 HG	VELOCITY	50.77FPS
			-	
PRESSUR	E MEAN	RMS	HAXIMUM	MINIMUM
TAP	PRESSURE	PRESSURE	PRESSURE	PRESSURE
NUMBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COEFFICIENT
1	281	.198	.472	-1.091
2	254			
3	229	.194	.616	977
4	418			
5	225			
6	401			
7	572			
	545			
9	558			
10	566			
11	686			
12	704			
15	698			
14	604	. 120	165	-1.161
15	674			
16	670	.150	250	-1.495
17	105			
18	. 100			
101	207	.156	.154	-1.011
102	204	.099	.105	616
105	152	.088	. 095	552
104	168	.083	.075	497
105	175			
106	167			
107	241	.082	.035	608
109	190	.095	.095	681
109				2
110	222			
111	217			
112	189			
115	185			
114	135			
115	157			
116	152			
117	165			
119	174			
119	179			
120	176	. 110	.188	715
121	150			
122				
123	132			

.064

.100

.158

124

125

126

127

120

129

150

131

1 52

155

154

1 35

1 36

-.156

-.165

-.155

-.155

-.206

-.206

-.155

-.124

-.100

1-.105

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-.116

-.104

.075	407	ť.
		A.V.
.035	609	
.095	681	1
		F
		:
		ł
		-
		Å
.188	715	
.020	400	
.140	621	
. 152	-1.081	

30.133340	WC 11			
TID	Barccube	RUZ	HAXINUH	HINIHUH
I AF	PHESSURE	PRESSURE	PRESSURE	PRESSURE
TUTBER	CUEFFICIENT	COEFFICIENT	COEFFICIENT	COEFFICIENT
157	156			
58	218	. 386	. 354	678
159	117			
1 2 0				
141	397			
142	100			
143	085	.060	.100	527
144	101			
145	104	. 364	.116	595
146	106			
201	354	. 166	. 069	-1.292
202	766	.167	540	-1.659
205	746	.174	291	-1.548
204	745	.185	313	-1 805
205	616			
206	478			
207	374	.197	276	-1 545
209	•			
209	202	.160	271	-1 017
210	224		••	
211	- 429			
212	- 680			
215	- 657			
214	- 709			
215	- 635			
216	- 521			*
217	- 841			
218	- 251			
219	- 286			
220	- 634	24.8		
221	- 504	.203		-1.805
222	- 748	224		
222	/00	.220		-1.819
223				

.183

.145

.2:4

. 149

.224

.155

-.108

. 222

-1.057

-1.555

-1.026

-. 856

WIND DIRECTION	45	TEMPERATURE	69.50 CE	GREES F
BAROMETRIC PRESS	24.95	IN HG VELOC	ITY 50.	TTEPS

224

225

226

227

229

229

230

252

235

234

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-.259

-.257

-.226

-.565

-. 606 -.615

-.611

-.545

-. 452

-. 501

-.249

-.246

-.669

-.415

-.474

-.545

-.250

-.101

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WIND DIRECTION 45 TEMPERATURE 69.50 DEGREES F BAROMETRIC PRESS 24.95 IN HG VELOCITY 50.77FPS

PRESSURE	MEAN	RMS	MAXIMUM	HINI HILW
TAP	PRESSURE	PRESSURE	PRESSURE	PRESSURE
NUMBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COFFFICIENT
437		.170	297	-1 615
409	740	:56	265	-1 645
409	700	. 160	- 185	-1 760
410	355			
411	219			
412	254			
415	244			
414	555			
415	469			
416	624			
417	672			
418	676			
419	656			
420	215	. 149	175	- 95/
421	245			
422	407	. 195	266	-1 178
425	485			-1.113
424	512			
425	701	. 197	010	-1 728
426				1.123
427	635	175	- 154	-1 420
428	599	. 335	.291	-2 072
429	160			-2.012
450	175			
451	184			
452	255			
455	597			
434	432			
435	658			
436	697			
437	706			
459	196	. 368	.058	- 663
439	118			
440	186	.092	. 119	- 720
441	220			
442	572			
445	621	.258	.149	-1.429
444	704		• • • •	
445	769	.242	114	-2.010
446	494		•	

WIND DIRECTION 45 TEMPERATURE 69.50 DEGREES F BAROMETRIC PRESS 24.95 IN HG VELOCITY 50.77FPS

PRESSURE	MEAN	RMC	MAYIM	
TAP	PRESSURE	PRESSURE	PRESCURE	PARTERIA
NUMBER	COEFFICIENT	COFFFICIENT	COFFEICIENT	CASESICIENT
245	175	.112	227	CUEFFICIEN:
246	.020	• • • •	• 22 1	///
301	947	386	200	
502			.2.3	-2.301
305	. 535	180	1 195	
504	.607	185	1.175	049
305	. 645			
306	.646			
307				
308				
309	.228	. 196	1.055	. 826
310	803			320
511	-1.099			
312	.085			
515	. 491			
514	.687			
315	. 765			
316	.749			
317	. 684			
518	. 545			
519	. 152			
320	.005	.171	. 659	621
521	. 421			
322	.521	. 170	1.055	.070
525	. 666			
324	.679			
325				
326	. 455			
327	.067	. 194	. 774	554
528	-1.012	. 575	.265	-2.345
529	-1.078			
350	050			
551	. 527			
552	.500			
335	.578			
334	.555			
335	. 490			
336	. 325			
557	046			
558	195	. 154	. 549	753
339	.197			
340	. 345	.130	. 874	005
341	.405			
342	.414			
545	. 364	.151	. 956	.005
344	. 162			
345	149	. 155	.588	766
546	957			
401	160	.017	020	285
402	251	. 155	.258	-1.055
403	205	.171	. 522	-1.097
404	306	.207	. 550	-1.264
405	467			
406	636			



	WIND DIRECTION	90 TE	MPERATURE 68.00	DEGREES F
	BAROMETRIC PRESS	24.95 IN HG	VELOCITY	50.70FPS
			-	
PRESSU	RE MEAN	RMS	MAXIMUM	HINIMUM
TAP	PRESSURE	PRESSURE	PRESSURE	PRESSURE
NUMBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COEFFICIENT
137	669			
138	606	.077	58 !	-1 111
139	580			
140	483	.019	- 44:	- 525
141	552			. 520
142	743			
145	795	106	- 500	-1 262
144	- 719			
145	- 704	694	- 861	-1 040
146	- 705			-1.040
201	- 627	179	- 400	-1 000
202	- 546	078		
205	- 590	176	310	919
204	- 594		550	906
205	576	2		800
205	- 599			
207		100		
200	020		545	985
200	- 640			
210	649	. 991	405	-1.145
210	652			
211	566			
2:2	5/1			
215	571			
214	576			
215	587			
216	507			
217	598			
218	606			
219	628			
220	555	.000	268	-1.088
221	544			
222	599	.070	517	875
225	567			
224	570			
225				
226	596			
227	621	.085	566	-1.042
229	620	. 092	279	-1.160
229	552			
230	526			
251	525			
232	534			
255	540			
234	552			
235	560			
236	558			
257	564			
258	556	.099	269	-1.251
259	210			
240	122			
241	525			
242	526			
245	524	. 098	255	-1.215
244	497			



PRESSURE	MEAN	RMS	MAXIMUM	MINIMUM
TAP	PRESSURE	PRESSURE	PRESSURE	PRESSURE
MBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COEFFICIENT
1	744	.158	258	-1.447
2	334			
3	295	. 150	.309	867
4	521			
5				
6	- 414			
7	-1.055			
	- 709			
9	- 598			
10	- 622			
11	- 321			
12	- 650			
18	- 546			
14	-1 826	222	- 725	-2.126
15	-1.520			2
15		180	- 2/5	-1 440
10	040		.245	
10	550			
1.6	.404		. 807	.1 288
101	/14	.101	597	-1.250
102	660	.112	525	
105	677	.096	50/	-1.191
104	669	.105	525	-1.000
105	657			
106	641			
107	687	.000	402	-1.050
108	604	.090	204	951
109	661			
110	641			
111	655			
112	699			
113	671			
114	592			
115	657			
: 16	657			
117	635			
119	626			
119	617			
120	679	.114	525	-1.166
121	654			
122	656	.015	614	704
125	661			
124	666			
125	604	.078	367	959
126	621			
127	615	.078	361	975
129	607	.076	572	993
120				
150	- 648			
181	- 640			
182				
132	- 712			
199	- 787			
1 34	- 704			
1 3 3				
56	0.0			

WIND DIRECTION 90 TEMPERATURE 60.00 DEGREES F BAROMETRIC PRESS 24.95 IN HG VELOCITY 50.70FPS

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E 60.00 DEGREES F OCITY 50.70FPS

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WIND DIRECTION BAROMETRIC PRESS	90	TEMPERATURE 68.00 DEGREES F	
BARUNEIRIC PRESS	24.95	IN HG VELOCITY 50.70FPS	

PRESSURE	MEAN	RMS	MAXIMUM	MINIMIN
TAP	PRESSURE	PRESSURE	PRESSURE	PRESSURE
NUMBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COFFEICIENT
407	. 186	. 123	. 593	- 186
408	. 341	. 141	.857	- 036
409	.289	.245	. 975	- 626
410	.627			
411	620			
412	356			
415	129			
414	.054			
415	. 187			
416	.259			
417	. 348			
418	. 434			
419	. 389			
420	358	. 069	090	637
421	142			
422	018	.084	. 392	250
423	. 155			
424	. 295			
425	. 358	. 118	. 769	.029
426	. 420			
427	. 376	.223	. 956	583
428	.573	.175	1.168	.095
429	651			
430	597			
451	178			
432	.008			
455	. 142			
434	.467			
435	. 314			
436	. 397			
437	. 320			
458	461	.068	382	925
459	191			
440	.026	.064	. 556	140
441	. 142			
442	.211			
443	.290	. 119	. 781	188
444	. 351			
445	. 52 1	. 169	1.099	284
446	. 562			

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HIND DIRECTION 90 TEMPERATURE 60.00 DEGREES F BAROMETRIC PRESS 24.95 IN HG VELOCITY 50.70FPS

PRESSURE	MEAN	RMS	MAXIMUM	MINIMUM		
TAP	PRESSURE	PRESSURE	PRESSURE	PRESSURE		
NUMBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COEFFICIENT		
245	521	.098	- 258	-1 115	1	
246	270					
501	615	194		453		
802			• 2	. 052		
EAE	175					
303	.425	. 157	.892	020		
504	. 509	. 154	. "2 "	069		
505	.226					
506	. 164					
507	.745	.073	.925	188		
309	251	.233	. 764	552		
309	296	.069	. 054	- 529		
510	527					
311	.672					
512	540					/
515	518					1
514	482					1
TIE						1
315	. 522					1
516	.264					
517	.115					
518	075					
319	291					1
320	.449	.260	1.152	515		1
321	. 452					8
322	.813	.149	867	- 717		
323	. 500			•		
524	.214					
525	- 248					p
826	.245		. 823	292		1
827						8
321	505	.077	. 056	621		1
528	555	.001	260	-1.164		1
529	.481					£.1
550	. 526					1
551	. 345					
532	.285					1
333	.214					
554	. 1 36					6
335	.057					
336	119					
557	506					
339						
550	227					
3.40	.221					
340						
341	.141					
542	.0					
545	016	.079	. 589	284		
344	149					
345	522	.077	. 024	715		
346	499			- 11 15 0		
401						
402	517	.074	- 056	- 887		
405	- 170	0.07	176	- 438		
404	0.00					
405						
405	.100					
406	.170					

H	IND DIRECTION	150 TEM	PERATURE 68.80	DEGREES F
BA	ROMETRIC PRESS	25.00 11 HG	VELOCITY	51.69FPS
PRESSURE	MEAN	2 M C		
TAP	PRESSURE	PRESS	PPFCC PF	Porceipe
NUMBER	COEFFICIENT	COFFFICIENT	COFFE : CIENT	CORFEICIEL
157	154			COLFF SC. ETc.
: 59	511	. 153	24	5.1
: 59	270			
140				
141	. : : 2			
: 42	308			
145	050	. \$65	. 3' 2	240
1 1 4	075			
145	149	.112	. 395	640
:46	035			
201	511	. 366	:62	934
202	24	. 352	::	45"
205	268	. : 46	:67	477
204	255	.042	101	450
205	245			
207	242			
208	.256		44	441
209	- 252	142		
210	- 245	• • • 2		410
211	285			
2:2	269			
215	258			
214	249			
215	248			
216	250			
217	243			
219	245			
219	246			
220	271	. 051	059	599
221	259			
222	205	. 058	167	447
223	252			
224	240			
226	- 248			
227	250	041	- 124	
228	246	. 045	- 090	- 596
229	274			
230	265			
251	258			
232	256			
233	252			
234	252			
235	255			
256	252			
237	252			
258	265	. 046	154	487
259	202		105	
240	125	. 251	095	327
241	- 280			
248	- 266	156	. 119	- 181
244	- 274			

WIND DIRECTION 150	EmbEst. SE	68.8: CESPEES F
BARGMETRIC PRESS 25.00	IN HS VELD	11" 51.6grps

PRESSURE	MEAN	RMS	w1, .w. w		
TAP	PRESSURE	PRESS	P9555 95	PPF 55 PF	
BER	COEFFICIENT	COEFFICIENT			
	72:	. '6-	225	- 324	
2	256				
5	:04	.105	. 255	- 671	
1	249				
5	105				
6	'89				
7	545				
8	554				
9	:69				
. 0	270				
11	363				
:2	295				
15	172				
14	501	.158	047	- ' . 6 7 2	
15	255				
16	109	.111	. 46 7	445	
17	. 020				
18	.716				
101	275	. 34 :	'44	456	
102	100	.050	35 t	56 -	
105	:69	.041	016	525	
104	154	.056	.105	540	
: 05	:15				
106	116				
107	152	.077	. '56	552	
:08	175	.142	.209	967	
109	·				
110	056				
111	240				
112	212				
115	175				
114	002				
115	111				
	097				
111	095				
120	- 318	141	- 12/	- 400	
12:	- 170				
122					
128	- 106				
124	- 186				
125	- 135	0.00	\$22	- 405	
126	- 067				
127	21!	192	. 450	-1.009	
129	.056	.164	.670	485	
129	240				
151	2:0				
131	185				
1 52	155				
155	115				
154	075				
1 55	346				
1 56	052				

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HIND DIRE	CTION	150		TEMP	ERATURE	68.80	DECREES	r
BAROMETRIC	PRESS	25.00	IN	HG	VELOC	ITT	50.69FPS	ć

PRESSURE	MEAN	RMS	MAYTHUM	
TAP	PRESSURE	PRESSURE	PRECEMPE	RINIHUM
NUMBER	COEFFICIENT	COEFFICIENT	COFFFICIENT	COEFFICIENT
407	.098	.171	att	CUEFFICIENT
408	.060	.175	788	462
409	196	.171		526
410	684		••••	(27
411	.054			
412	.154			
415	.204			
414	.182			
415	.175			
416	.149			
417	. 095			
418	026			
419	242			
420	.174	.150	787	200
421	. 180			299
422	. 129	.078	408	187
425	. 150			197
424	. 155			
425	. 054	.087	515	- 336
426	065			225
427	269	.115	110	75.0
428	598	.218	- 096	-1 677
429	.098			-1.0//
430	.149			
451	.149			
432	.122			
435	.104			
434	.149			
435	.015			
436	092			
437	269			
438	.018	.085	. 485	- 245
439	.077			
440	.105	. 06 1	. 554	- 088
441	.076			
442	.054			
445	010	.065	. 552	- 101
444	075			
445	201	. 096	. 065	- 657
446	566			



.

	IND DIRECTION	150 TEM	PERATURE 68.80	DEGREES F
BAI	ROMETRIC PRESS	25.00 IN HG	VELOCITY	50.69FPS
RESSURE	WEAN	840		
TAP	PRESSURE	381122388	RECEUSE	HINIWUM
NUMBER	COFFFICIENT	COFFEICIENT	CAFEFICIENT	PRESSURE
245	294	.065	- IAS	COEFFICIENT
246	106			
501	597	.180	127	-1 400
302				
505	624	.160	101	-1.445
504	528	.140	.072	-1.266
305	419			
506	371			
507	200	.017	.046	670
500				
310	313	.085	.018	853
511	- 560			
512	- 552			
313	528			
314	552			
315	461			
516	595			
517	350			
318	295			
319	205			
520	487	. 151	072	-1.568
521	467			
322				
323	416			
325	390			
326	- 201			
327	302	. 066	- 087	- 685
528	285	.057	090	559
329	486			
350	461			
351	455			
552	458			
355	426			
334	575			
355	525			
336	292			
337	. 143			
550	- 475			
340	- 454	117	- 151	-1 185
541	407			
542	546			
345	294	. 085	005	719
344	255			
345	251	.066	042	758
346	258			
401	204	.015	144	247
402	.201	.167	. 892	271
405	. 192	.160	. 929	204
404	.174	. 155	.920	176
405	.171			
406	.147			

HIND D	RECTION TRIC PRESS	0 24.70 In	TEMPERATURE	71.20 DEGREES F	

PRESSURE	MEAN	RMS	MAXIMUM	MET BET MET IM
TAP	PRESSURE	PRESSURE	PRESSURE	PRESSURE
NUMBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COEFFICIENT
157	259			
138				
159	316			
140	205	.155	.252	846
141	094			
142	111			
145				
144				
145	217	.151	.294	977
146	396			1000
201	295	.102	:24	
202	246	. 396	. 029	720
205				
204	246	. :90	. 059	838
205	278			
206	266			
207	220	.060	015	520
208	224	.077	. :26	591
209				
210	261			
211	301			
212	275			
213	259			
214	269			
215	276			
216	274			
217	265			
218	255			
219	251	100 C		
220	301	.075	.075	622
221	204			
222	204	. 053	106	405
223	297			
224	295			
225	200			
220	206			
221	201			
220	284	.961	069	627
229	359			
250	520			
251	510			
232	325			
233	322			
236	307			
237	- 515			
230				
230	- 822		480	
230	522		056	640
239				
241				
242	- 531			
242	320			
243				
244				

WIND DIRECTION ID.		
MIND DIMECTION 103		TEMPERATURE 71.20 DEGREES F
BARCHETRIC PRESS 24.70	IN	HG VELOCITY ST. TIFPS

PRESSURE MEAN RMS MAXIMUM TAP PRESSURE PRESSURE PRESSURE NUMBER COEFFICIENT COEFFICIENT COEFFICIENT 1 1022 .20T 126 2 454 126 126 3 196 .140 .250 4 211 077 609 6 220 609 217 10 285 11 579 11 579 359 217	HINIHUH PRESSURE OEFFICIENT -1.665 -1.027
TAP PRESSURE PRESSURE PRESSURE PRESSURE NUMBER COEFFICIENT COEFFICIENT <td< th=""><th>PRESSURE 0EFFICIENT -1.665 -1.027</th></td<>	PRESSURE 0EFFICIENT -1.665 -1.027
NUMBER COEFFICIENT COEFFICIENT COEFFICIENT C 1	0EFFICIENT -1.665 -1.027
1 .622 .207 126 2 454 .140 .250 3 196 .140 .250 4 211 .140 .250 5 077 .140 .250 6 220 .140 .250 7 609 .150 .140 9 217 .100 .285 11 359 .259	-1.027
2454 3196140 .230 4211 5077 6220 7609 6513 9217 10285 11359	-1.027
5196140 .250 4211 5077 6220 7609 8515 9217 10285 11559 12559	-1.027
4 - 211 5077 6220 7609 8515 9217 10285 11559 12559	-1.02/
5277 6220 7609 8513 9217 10283 11359	
6220 7609 6513 9217 10285 11359	
7609 6515 9217 10285 11559 12559	
•515 •217 10285 11559 12559	
9217 10295 11379 12359	
9217 10283 11379 12358	
10295 11579 12558	
12 358	
12 338	
206	
14014 .160 .462	-1.058
240	
16077 .114 .474	676
17009	
10	
101250 .086 .052	758
102159 .004 .211	606
105	
104065 .119 .542	752
105047	
106054	
107 .011 .138 .560	421
100 .056 .168 .012	720
109	
.246	
111264	
112225	
115196	
114106	
115157	
116126	
117104	
110129	
119508	
120250 .054 .126	469
121255	
122	
125102	
124157	
125110 .074 .291	412
126164	
127	
120099 .125 .425	506
129521	
150269	
131236	
152206	
155167	
134140	
155124	
184 - 181	



WIND DIRECTION 180		TEMPERATURE	71	. 20	DECOFFS	F
BAROMETRIC PRESS 24.70	IN	HE VELO	11	۲	51.11FPS	

PRESSUR	RE MEAN	RMS	MAXIMUM	HET N. T. PETIN
TAP	PRESSURE	PRESSURE	PRESSURE	POFSSIOF
NUMBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COFFEICIENT
407	.148	.155	.555	- 872
408	. 055	.117		- 162
409	.297	.001	500	- 462
410	351			
411	. 1 52			
412	.251			
413	.272			
414	.228			
415	.246			
416	.215			
417	. 122			
418	065			
419				
420	.079	.175	. 908	- 181
421	.125			
422	. 156	.161	. 875	- 104
423	.145			
424	.174			
425	.076	.123	.514	- 207
426	052			
427	.257	.079	.545	- 064
428	353	.085	142	947
429	055			
430	.014			
431	.047			
452	.075			
455	.057			
434	.067			
435	021			
436	114			
437	229			
438	. 0 5 8	.111	.661	507
439	.029			
440	.075	.085	.459	155
441	.036		a. 1312	
442	012			
443	. 571	.075	.608	.087
444	126			
445	255	.074	.038	528
446	414			



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HIND	DIRE	CTION	180		TEMPERATURE	71.20	DEGREES	F
BAROME	TRIC	PRESS	24.70	IN	HG VELOC	ITY	51.11FPS	

PRESSURE	MEAN	RMS	MAXIMUM	MINIMUM
TAP	PRESSURE	PRESSURE	PRESSURE	PRESSURE
NUMBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COEFFICIENT
245	322	. 369	111	- 614
246	117			
501	329	. 386	- 164	- 841
302				
305				
304	- 351	087	***	
505	- 341			
506	- 548			
507	- 358	100	178	
508	- 849	160		
509				/43
510	- 510			
511	- 820			
512	- 315			
515	- 515			
314	- 521			
515	- 343			
516	- 342			
517	- 365			
518	- 385			
519	- 454			
520	- 886		- 117	
521	- 384			-1.019
322	- 346	164	. 167	
325	- 320			
324	- 868			
325	- 860	ACR		
326	- 405			
\$27				
528	- 578	182	- 121	
529	- 575		020	028
330	- 356			
351	- 362			
332	- 357			
355	- 370			
334	- 379			
335	591			
356	- 425			
557	- 449			
358	580	096	- 001	-1 282
559	587			
340	577	101	- 114	-1 111
341	- 407			-1.111
342	405			
345				
344	- 420			
345	441	. 108	- 122	-1.014
346	388			
401				
402	. 505	246	1 144	- 876
405	. 760	215	1 429	116
404	.278	101	AAR.	- 203
405	257			
405	215			
	.2.3			

WIND DIRECTION 210	TEMPERI	TURE 69.0	O DEGREES F
BAROMETRIC PRESS 24.70	It: HG	VELOCITY	ST.COFPS

PRESSURF	MEAN	PHC	ML	
TAP	POFSSURF	201023399	20505105	TINITUR .
MAFR	COFFFICIENT	COFFEICIENT	COFFEICIENT	PRESSURE
: 57	- 356	COLFFICIEN	CUEFF .CIER	COEFFIC.EN"
150	162			
: 59	- 241		. 0	-1288
140				
141	- 177			
147	- 251			
143	- 172	,		
	- 345			5:5
145	- 240			
146	- 272	• • • •		/10
201	- 286			
202	- 292			
205	- 163			025
204	- 205	122		
205	- 501		. 192	
206	- 325			
207	- 355	160		
208	- 375	178		
209	501	251	7/5	- 202
210	- 451		.2	-2.225
211	286			
212	279			
213	281			
214	209			
215	302			
216	516			
217	527			
218	345			
219	343			
220	195	.072	.047	-,475
221	271			
222	205	. 076	351	550
225	205			
224	299			
225				
226	326			
227	199	. 084	. 364	-1.089
228	240	.087	.015	769
229	260			
230	252			
251	241			
232	25!			
255	265			
254	277			
235	316			
256	321			
257	346		10000	
259	252	. 052	051	464
239	185			
240				
241	236			
242	247			
245	157	. 38 1	.077	506
244	304			

WIND DIRECTION 210	"E"PERA	T.RE 69.	CO DEGREES F
BAROMETRIC PRESS 24.70	15. HG	ELOCITY	5

PRESSURE	TEAN .	**5	at y la la	N111108
AP.	PRESSURE	PRESSURE	PRESSURE	PRESSURE
CHBER	COEFFICIENS	COEFFICIENT	COEFFICIENT	COEFFICIENT
1	415	. 49		-1.175
2	205			
5	095	. 92	.709	035
4	095			
5	320			
6	120			
7	220			
8	. 316			
9	118			
10	095			
11	118			
12	105			
13	075			
14	.102	.097	. 420	204
15	.091			
16	.030	.108	.495	5"2
17	144			
18	. 427			
101	525	.295	. 165	-2.259
102	351	. 150	.510	955
105	301	.127	.523	495
104	035	. 150	.557	657
105	055			
106	. 006			
107	. 121	. 161	.746	441
108	.289	.208	1.106	649
109				
110	.510			
111	555			
112	295			
115	241			
114	142			
115	130			
116	062			
117	.074			
118	. 251			
119	. 300			
120	205	.077	.098	642
121	255			
122				
125	175			
124	115			
125	.020	. 121	.611	558
126	.109			
127	. 557	.177	. 999	198
129	.276	.174	.906	518
129	520			
1 50	298			
131	276			
: 52	261			
155	247			
1 54				
: 55				
1 56	114			

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	WIND DIRECTION	210 TE	MPERATURE 69.00	DEGREES E
	BAROMETRIC PRESS	24.70 IN HG	VE: OCITY	ST JAFPS
PRESSU	RE MEAN	RMS	MAXIMUM	HTRITHTW
TAP	PRESSURE	PRESSURE	PRESSURE	PRESSURE
NUMBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COEFFICIENT
407	058	. 362	.203	260
409	306	. 350	. 179	292
409	021	.046	. 165	176
410	209			
41:	. 555			
412	265			
415	020			
414	039			
415	044			
416	075			
417	096			
419	129			
419	170			
420	262	.2:2	.257	-1.152
421	132			
422	125	. 350	. 367	349
425	125			
424	060			
425	147	. 345	. 359	392
426	159			
421	060	.040	.098	254
420	125	.045	.030	512
429				
430	331			
482	- 160			
4 32	100			
- 33	142			
125	089			
486	- 167			
- 30	104			
480				
- 38			. 359	650

. 355

. 051

. 050

-.169 -.152 -.117

-.121 -.009

-.115

-.257

439 440

441 442

445

444 445

446

. 159

. 075

.168

. 359

-.650

-.302

-.206

-.328

HIND DIRECTION 210 TEMPERATURE 69.00 DEGREES F BAROMETRIC PRESS 24.70 IN HG VELOCITY 51.03FPS

PRESSURE	MEAN	RM C	MITTH	
TAP	PRESSURF	PRESSURE	PRECEMPE	Parssure
MUMBER	COEFFICIENT	COFFFICIENT	COFFF : C : F	CAFECICIES.
245	242	104	-95	
246	111			
501	- 212	149		101
502				
505	- 081	2.4.7		
504	- 121		•••••	24.
505	- 215		• • •	204
306	- 216			
507				
538				
309	- 142		* 8 2	
510	- 275			•••
311	213			
312	206			
313	205			
514	207			
315	216			
316	26 1			
517	257			
318	245			
319	263			
320	124	. : 46	5	- \$2*
52 !	209			
322	219	. 343	091	559
525	201			
324	255			
525				
526	25!			
527	149	. 060	. : : : :	475
529	197	. 369	025	552
529	200			
330	201			
551	210			
352	217			
333	224			
334	241			
335	244			
336	250			
537	265			
330	250	. 366	:29	627
339	257			
340	257	. 066	000	541
54 !	244			
342	242			
343	117	. 05 1	.042	540
344	237			
345	165	. 059	. 328	547
346	230			
40:	. 453	.171	. 988	263
402	246	.245	.447	-1.514
105	.144	. 396	.477	220
404	.092	. 383	. 451	234
405	001			
406	319			



	WIND DIRECTION	270 TE	MPERATURE 69.00	DEGREES F
	BAROMETRIC PRESS	5 24.70 IN HG	VE: OCITY	ST CAFPS
				3
PRESSU	RE MEAN	RMC	MAYTHIN	
TAP	PRESSURE	PRESSURE	PPECCUPE	RININUR
NUMBER	COFFFICIENT	COFFEICIENT	COFFEIGLENT	FRESSURE
: 57	- 439	COLITICIEN	COEFFICIEN	CUEFFICIENT
1 38				
139	266			
1.4.0	.200			
1.4.1	215			
142	215			
1.48	145			
144	065	.089	. 366	350
1/5	504			
145	590	-0/6	114	701
140	656			
201	505	.073	240	911
202	286	.056	090	465
205	. 020	.094	. 46 1	278
204	.090	.108	.568	247
205	.086			
206	. 146			
207	. 199	.122	.58!	242
208	.317	.075	.629	158
209	. 394	.264	1.060	606
210	.660			
211	429			
212	255			
213	081			
214	.068			
215	.159			
216	.249			
217	. 356			
219	.410			
219	. 371			
220	179	.063	. 065	585
221	087			
222	.017	.089	. 598	747
223	. 159			
224	.249			
225				
226	. 397			
227	.506	.245	1.084	- 408
228	.705	. 191	1 549	178
229	422			
230	267			
251	115			
252	011			
255	115			
234	199			
235	250			
236	828			
230	. 323			
280	- 345	45/		
230				521
239				
240				
241	.072			

245

244

.124

.295

.219

.075

. 621

.098



150

131

152

135

134

1 35

1 56

. 334

. 322

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Contraction of Contraction	WIND M	
gan was		

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	WIND DIRECTION	270 TE	MPERATURE 69.0	O DEGREES F
	ANONE INIC PRES	5 24.70 IN HG	VELOCITY	ST. OOFPS
PRESSUR	E MEAN			
TAP	PPFSSUPF	RES	MAXIMUM	HINIMUH
NUMBER	COEFFICIENT	PRESSURE	PRESSURE	PRESSURE
407	- 632	CUEFFICIENT	COEFFICIENT	COEFFICIENT
409	- 618	. 104	201	-1.075
409	546	- 121	191	-1.184
410	596	49	109	-1.372
411	525			
412	529			
413	532			
414	556			
415	555			
416	579			
417	606			
419	642			
419	695			
420	460	179		
421	551		62	-1.150
422	606	.070		
423	586		35	951
424	500			
425	608	. 365	- 108	
426	613			869
427	572	. 125	- 247	
428	492	.002	- 165	-1.084
429	597			
450	605			
431	597			
452	626			
455	639			
454	541			
435	593			
456	598			
457	646			
458	696	.097	415	-1.253
459	669			
440	691	. 100	384	-1.260
441	692			
442	651			
443	461	.076	199	
115	547			
447	492	. 386	275	-1.075
440	- 542			

WIND DIRECT!	ON 270	TEMPERATURE	69.0	CEGREES	F
BAROMETRIC PR	ESS 24.70 1%	HG VELO	CITY	51.00FPS	

OBECCUME	-		44.5	
PRESSURE	REAN	RMS	MAXIMUM	HINIMUH
I AP	FRESSURE	PRESSURE	PRESSURE	PRESSURE
NUMBER	CUEFFICIENT	COEFFICIENT	COEFFICIENT	COEFFICIENT
245	.286	.128	. 759	554
246	.449			
501	655	. 146	304	-1.510
502				
505	555	. 095	088	95
504	569	. 391	077	856
505	445			
506	442			
50 -				
500				
509	550	.076	069	657
510	424			
511	605			
512	517			
313	4/1			
314	454			
315	441			
817	435			
319	436			
310	- 425			
520	- 410	477		
521	- 450			-1.050
\$22	- 408	15.6		600
525	- 427		3:2	689
324	- 441			
325				
326	422			
327	306	. 062	- 060	- 545
529	352	. 063	- 090	- 647
529	517			
550	479			
331	469			
552	454			
333	456			
554	450			
335	441			
336	451			
357	428			
359	552	.069	260	
359	496			
340	492	.064	255	697
541	486			
342	401			
345	354	. 064	144	500
344	465			
345	385	.065	145	621
546	457			
401	589	.048	426	761
402	550	.084	240	-1.099
405	455	.002	151	765
404	402	. 302	150	766
405	568			
406	569			



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WIND DIRECTION 300		TEMPERAT	TURE	70.00	DEGREES	F
BAROMETRIC PRESS 25.05	IN	HG	VELOC	ITY	50.69FPS	

PRESSURE	MEAN	RMS	MAXIMUM	Se 1 PJ 1 PFt ; se
TAP	PRESSURE	PRESSURE	PRESSURE	Parssuar
NUMBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COFFFICIENT
137	591			
1 39				
159	306			
140				
141	541			
142	528			
143	464	.083	206	898
144	448			
145	452	.077	110	745
146	470			
201	804	.224	314	-1.754
202	117	.140	. 540	692
205	.289	. 162	.072	297
204	. 422	.172	1.095	121
205	.457			
206	.551			
207	.577	.191	1.102	116
208	. 595	.158	1.042	069
209	.549	.210	1.217	252
210	.019			
211	667			
212	072			
215	.275			
214	. 495			
215	.591			
216	. 662			
217	. /15			
218	. 667			
219	.4/5			
220	000	.150	. 367	653
221	.192			
228	. 391	. 165	.915	.015
223	.516			
225				
226	505			
227	421	200		
228	- 109	274	671	-1 860
229	- 572			-1.369
250	- 141			
251	.144			
252	. 522			
255	. 463			
234	.510			
255	.537			
236	.469			
257	. 306			
258	271	. 113	. 124	768
259	.095			
240		2		
241	. 554	5		
242	. 584			
245	. 435	.150	. 990	029
244	.405			

WIND DIRECTION 300		TE	MPERATURE 70.0	O DEGREES	ş
BAROMETRIC PRESS 25.05	IN	HG	VELOCITY	50.69FPS	

PRESSURE	MEAN	RMS	MAXIMUM	MINIMUM
TAP	PRESSURE	PRESSURE	PRESSURE	PRESSURF
NUMBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COEFFICIENT
1	406	.150	. 095	928
2	676			
5	963	. 159	555	-1.762
4	490			
5	430			
6	965			
7	307			
8	- 469			
9	- 961			
10	954			
11	- 562			
12	- 684			
15	- 895			
14	- 558	140	810	
15	- 726			
16	- 814	158	- 871	.1 641
17	- 550			-1.001
18	- 346			
101	- 302	150	804	0.08
102	-1 344	. 1 3 3	. 394	903
102	- 0/5	-219		-2.089
104		.209	114	-1.749
105		. 192		-1.585
105	- 208			
107	290	103		
107	3/2	. 192	159	-2.295
100	339		152	545
109	509	.036	214	552
110	399			
112	200			
112	-1.102			
113				
115				
115	294			•
110	293			
110	312			
110	343			
120	3/5	264		1 110
120	-1.006	.200		-2.220
121	910			
122				
123	335			
124	320		244	
125	3/4	. 051	200	
120	359			
127	363	. 052	211	544
120		.05/	214	5/5
129	356			
150	-1.061			
191				
152	479			
155	595			
154	595			
1 55	402			
156	395			



HIND DIRECTION 500 TEMPERATURE 70.00 DEGREES F BAROMETRIC PRESS 25.05 IN HG VELOCITY 50.69FPS

PRESSURE	MEAN	RHS	HAXIMUN	
TAP	PRESSURE	PRESSURE	PRESSURE	POFSCUPF
NUMBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COFFEICIENT
407	467	.082	287	B75
408	495	. 101	- 191	- 087
409	482	. 127	091	-1 020
410	547			1.029
411	410			
412	410			
415	416			
414	416			
415	393			
416	425			
417	430			
419	455			
419	482			
420	404	. 060	211	- 606
421	406			
422	452	. 055	279	- 650
425	417			
424	325			
425	453	. 056	225	642
426	431			
427	445	.084	204	854
428	534	.114	224	-1.460
429	395			
450	414			
451	409			
432	429			
455	455			
434	259			
435	404			
436	400			
457	440			
438	515	.079	507	955
439	485			
440	545	.074	556	879
441	475			
442	439			
443	384	.064	160	604
444	300			
445	449	.089	185	854
446	517			

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WIND DIRECTION 300 TEMPERATURE 70.00 DEGREES F BAROMETRIC PRESS 25.05 IN HG VELOCITY 50.69FPS

PRESSURE	MEAN	RMS	MAXIMUM	MINIMUM
TAP	PRESSURE	PRESSURE	PRESSURE	PRESSURE
NUMBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COEFFICIENT
245	.294	.163	1.065	384
246	.198			
301	505	.157	034	-1.405
502				
505	547	.168	. 024	-1.471
304	556	.166	. 024	-1.571
505	581			
306	608			
307	642	.075	405	-1.017
308			0.000	
509	577	.134	126	-1.255
310	573			
511	537			
312	607			
515	568			
314	545			
315	520			
316	553			
517	557			
318	555			
519	525			
320	635	.159	250	-1 245
321	585			
322	599	.106	299	-1.192
523	518			
324	518			
325				
326	505			•
527	509	.142	160	-1.465
528	565	.171	205	-1 725
329	540			
330	646			
331	579			
552	568			
333	526			
334	545			
335	525			
336	488			
357	499			
339	641	.177	275	-1.571
359	575			
340	582	.122	268	-1.255
541	591			
342	556			
545	551	.140	254	-1.264
344	541			
345	527	. 152	204	-1.614
546	579			
401	10100 1000			
402	447	. 062	- 209	678
405	599	. 065	175	- 612
404	417	.066	- 175	- 650
405	- 414			
406	418			



WIND DIRECTION 330	TEMPERA	TURE 68.5	DEGREES	F
BAROMETRIC PRESS 25.05	IN HG	VELOCITY	50.62FPS	

		-		
PRESSURE	MEAN	RMS	MAXIMUM	MINIMUM
IAP	PRESSURE	PRESSURE	PRESSURE	PRESSURE
NURBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COEFFICIENT
157	574	2122		
158	672	.162	150	-1.421
159	651			
140	Sec. 2		14 A. A. A.	
141	417			
142	407			
145	36 1	.088	062	848
144	352			
145	369	.082	042	921
146	400			
201	121	.100	. 425	-1.271
202	.401	.212	.968	284
203	.665	.211	1.255	. 021
204	.640	.195	1.267	. 021
205	. 591			
206	.562			
207	.437	.172	1.009	501
209	.460	.054	. 681	098
209	086	.187	.556	- 603
210	895			
211	216			
212	. 351			
213	.607			
214	. 696			
215	.681			
216	.659			
217	.550			
219	. 500			
219	195			
220	.179	285	062	- 505
221	.481			590
222	.517	200	1 117	- 418
225	.574			
224	535			
225				
226	208			
227	- 220	178	151	. 770
228	-1,160	545	- 018	-2 710
229	- 458			-2.119
230	.065			
251	796			
252	450			
255	442			
254	421			
285	828			
236	181			
287	- 274			
250	- 105	157	447	- 645
250	105		.44/	642
239	. 183			
240	810			
241	. 516			
242	. 506			
245	.268	.112		020
244	.141			

WIND DIRECTION 350		TEMPERAT	URE	68.50	DEGREES	ş
BAROMETRIC PRESS 25.05	IN	NG VI	ELOC	174	50.62FPS	

PRESSURE	MEAN	RHS	HAXINUN	WINI WUW
TAP	PRESSURE	PRESSURE	PRESSURE	PRESSURE
NUMBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COEFFICIENT
1	259	.149	.415	765
2	601			
5	007	.150	455	-1.904
4	408			
5	642			
6	895			
7	078			
	511			
9	926			
10	928			
11	350			
12	102			
15	914			
14	.015	.143	.498	555
15	297			
16	-1.010	.165	474	-1.015
17	426			
18	246			
101	805	.180	392	-1.875
102	984	.198	475	-2.555
105	957	.177	515	-1.806
104	941	.210	.105	-2.442
105	605			
100	601			
107	552	.210	.157	-1.403
108	431	.186	.157	-1.318
109				
	410			
112	022			
118				
114				
115				
116	- 665			
117	- 478			
118	- 580			
119	574			
120	905	.187	265	-2.458
121	901			
122				
125	786			
124	602			
125	495	. 169	.067	-1.528
126	502			
127	356	.106	.047	954
128	500	.105	127	-1.591
129				···
150	-1.019			
151	-1.026			
152	858			
155	620			
154	452			
1 55	589			
156	356			

WIND

WIND DIRECTION 330 TEMPERATURE 60.50 DEGREES F BAROMETRIC PRESS 25.05 IN HG VELOCITY 50.62FPS

	PRESSURE	MEAN	986		
	TAP	PPESSUPE	PRESSURE	MUMIXAM	MINIMUM
	NUMBER	COFFFICIENT	FRESSURE	PRESSURE	PRESSURE
	407	- 374	CUEFFICIENT	COEFFICIENT	COEFFICIENT
	408	- 340	.043	225	567
	409	- 289	.045	175	549
	410	- 313	.04/	140	501
	411	- 377			
	412	541			
	415	550			
	414	- 529			
	415	- 295			
	416	512			
	417	506			
	418	305			
	419	303			
	420	354	670		
	421	330		055	975
	422	409	. 049	- 248	
	423	324		243	617
	424	250			
	425	340	.040	- 205	463
1	426	301		.205	40/
	427	286	.048	- 129	- 516
	428	316	. 053	- 162	- 688
	429	400			
	430	392			
	451	390			
	432	349			
	455	519			
	434	182			
	435	299			
	436	505			
	437	301			
	458	457	.074	205	906
	459	356			
	440	359	.049	219	616
	441	298			
	442	305			
	445	294	.043	149	475
	444	278			
	445	310	. 051	155	559
	446	517			

WIND DIRECTION 330 TEMPERATURE 60.50 DEGREES F BAROMETRIC PRESS 25.05 IN HG VELOCITY 50.62FPS

PRESSURE	MEAN	RMS	MAYTHUM	
TAP	PRESSURE	PRESSURE	PRESSURE	PESSURE
NUMBER	COEFFICIENT	COEFFICIENT	COEFFICIENT	COFFFICIENT
245	094	.162	.642	- 654
246	247			
501	379	.045	201	645
502				
503	172	.042	.020	597
504	155	.048	.044	505
305	158			
306	204			
307	538	.106	225	-1.050
308	2·····4			
309	-1.119	. 22 1	506	-1.959
510	328			
511	306			
512	265			
515	214			
316	170			
315	177			
817	236			
319	00/			
519				
320	- 272	440		
321	- 228		0/0	725
322	- 274	068		241
325	- 222		025	/01
324	- 350	1 m		
325				
326	912			
327	911	200	- 550	-1 854
528	418	. 157	113	-1 277
329	316			
330	267			
351	240			
332	225			
355	275			
334	362			
335	632			
336	791			
557	835			
358	345	. 052	165	647
339	235			
340	251	.070	.013	647
341	234			
542	508			
545	471	.175	.002	-1.529
344	619			
345	645	.184	176	-1.586
346	446			
401	502	.009	268	621
402	585	.094	005	906
403	317	.072	064	670
404	32 (.060	-,144	585
405	- 515			
	309			



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Figure 1. Plan View of Meteorological Wind Tunnel



Figure 2. Site Plan for Telephone Building



Taps 17 and 18 on Side Zero are Located Behind Grillwork on Building Sides I and 4 Respectively



Figure 3a. Pressure Tap Locations



Figure 3b. Pressure Tap Locations



Figure 3c. Pressure Tap Locations





Figure 5. Pressure Switch Installed in the Model



Figure 6. Data Sampling Time Verification

18. 16. 14

E²

12. 10, L 2. \circ 3. 4. Uⁿ 5. 6.

Figure 7. Typical Hot Wire Calibration

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Figure 8a. Mean Velocity Profiles Approaching the Model


Figure 8b. Mean Velocity Profiles Approaching the Model



Figure 9. Turbulence Intensity Profiles



FLUID MECHANICS PROGRAM

PRESSURE COEFFICIENT (R.M.S.)

Figure 10a. Pressure Coefficients for Air Door 1



Figure 10b. Pressure Coefficients for Air Door 1



Figure 11a. Pressure Coefficients for Air Door 2



Figure 11b. Pressure Coefficients for Air Door 2



Figure 12a. Pressure Coefficients for Corner Door Side 2



Figure 12b. Pressure Coefficients for Corner Door Side 2



Figure 13a. Pressure Coefficients for Corner Door Side 3



Figure 13b. Pressure Coefficients for Corner Door Side 3







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Figure 14b. Pressure Coefficients for Corner Door Side 2-3

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