

# **Structure of Vertical Wind Profiles**

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## Structure of vertical wind profiles

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An exponential relationship between the vertical wind shear and the layer thickness over which this shear is measured has been derived. From an analysis of the Richardson number it appears that shallow layers reaching maximum shearing conditions under the established power law should be turbulent, irrespective of the prevailing thermal stability conditions.

### TURBULENCE INFORMATION FROM VERTICAL WIND PROFILES

It has been shown by *Essenwanger* [1963, 1967] that vertical wind shears measured by detailed wind soundings, such as the FPS-16 tracks of 'Jimspheres,' yield exponential relationships of the form

$$\langle \Delta v \rangle = a_0 (\Delta h)^{a_1} \quad (1)$$

where  $\langle \Delta v \rangle$  denotes the mean total shear in meters per second (measured as the velocity vector difference over the height increment  $\Delta h$ ),  $a_0$  is a constant, and  $a_1$  is the exponent of the relationship in question. (For further details, see *Essenwanger and Reiter* [1969]). The following exponents  $a_1$  have been found from vertical wind soundings:

Mean wind shears	$a_1 = 1/2$
Mean extreme shears	$a_1 = 1/3$
Transient (nonstationary) fluctuations	$a_1 = 0$
Persistent mesoscale	$a_1 = 4/5$

A transverse structure function may be defined as

$$D_{ii}(r) = \overline{[v_i(r+r_1) - v_i(r_1)]^2} \quad (2)$$

where  $v_i$  is the velocity component transverse to the distance vector  $r_1$  [*Tatarski*, 1961]. For  $r_1 \equiv h$  and  $r \equiv \Delta h$ , it is easily seen that (1) relates to (2) through the expression

$$\sigma_{\Delta h}^2 = -\langle \Delta v \rangle^2 + D_{ii}(r)$$

where  $\sigma_{\Delta h}$  is the standard deviation of the shears  $\Delta v$  measured over the height incremental  $\Delta h$ .

It has been shown by *Tatarski* [1961] that for the structure function

$$D(r) = c^2 r^p \quad \text{for} \quad 0 < p < 2 \quad (3)$$

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the one-dimensional spectral density function

$$E(k) = \frac{\Gamma(p+1)}{2\pi} \sin \frac{\pi p}{2} c^2 k^b$$

holds, where

$$b = -(p+1)$$

From the foregoing it may be seen that  $a_1 = p$ ,

From this it appears that the exponential relationship for mean extreme shears leads to a '-5/3' trum slope.

According to *Kolmogorov* [1941] and *Obu* [1941], conditions in the inertial subrange are characterized by

$$D_{ii}(r) = \frac{4}{3} C \cdot (er)^{2/3} \quad \text{for} \quad l_0 \ll r \ll L$$

where  $l_0$  and  $L$  characterize the inner and the outer scales of turbulence, respectively, and where  $C$  is a constant of the order of unity.

$$a_0 = (\frac{4}{3} C)^{1/2} \cdot e^{1/3}$$

Figure 1 contains the data sample of mean extreme shears obtained by *Essenwanger* [1963] between the ground level and 30 km. Taking  $a_1 = 1/3$  we may evaluate the coefficient as  $a_0 = 1.2$  units of  $m^{2/3} \text{ sec}^{-1}$ .

As a matter of interest, it should be pointed out that *Vinnichenko and Dutton* [1969] found that '-5/3' slope prevails in the horizontal component of perturbation motion from the inertial sub-range through the synoptic scale. The vertical structure of the atmosphere, according to the preceding discussion, seems to align itself in the same '-5/3' exponential relationship of horizontal motions, if one considers the extreme velocity variations only. However, the vertical structuring shows considerably more

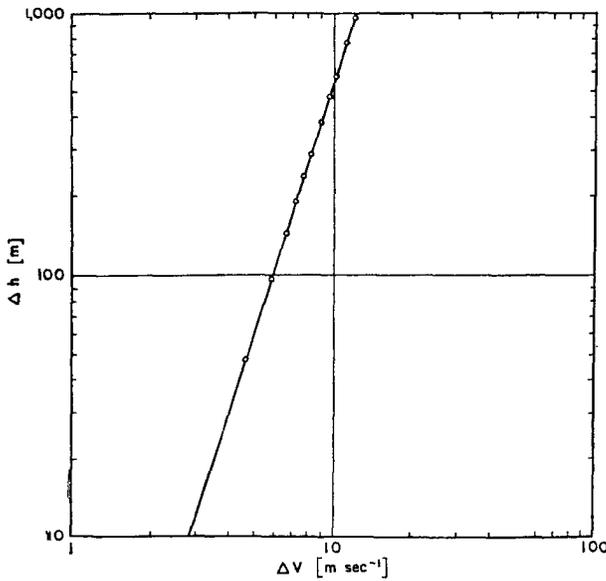


Fig. 1. Wind vector difference  $\Delta V$  ( $m \text{ sec}^{-1}$ ) measured over height increment  $\Delta h(m)$  on logarithmic scale. [From *Essenwanger, 1963.*]

shear than does the horizontal mesoscale. This fact is apparent even from a comparison of the mean large-scale vertical and the horizontal shears around a jet stream.

II RICHARDSON NUMBER

It has been pointed out by *Reiter and Lester [1967, 1968]* that the Richardson numbers evaluated from measurements in the free atmosphere, by virtue of the presence of a pronounced mesoscale in vertical wind profiles, reveal a certain dependence on the scale length  $\Delta h$  over which wind shear and thermal stability are evaluated. From (1) and from the observational evidence supporting it, we have seen that mean extreme wind shears themselves are scale-dependent. We are not aware of any corresponding statistics for the vertical gradient of temperature or potential temperature. Recent developments in small-lag temperature sensors [*Caplan and Camp, 1968*] may, however, allow such an evaluation in the near future.

We will assume that the statistical relationship between mean maximum vertical shear and layer thickness (shown in Figure 1) is brought about by the onset of turbulence that prohibits the development of excessive shears. Using the scale dependence of these maximum shears expressed by (1) and by an exponent  $a_1 = 1/3$ , in the Richardson number, we obtain

$$Ri = \frac{(g/\theta)\Delta\theta/\Delta h}{(\Delta V/\Delta h)^2} \tag{8}$$

and substituting for  $\Delta v$  from (1) (with  $a_1 = 1/3$ ), we arrive at

$$Ri = g \cdot \Delta\theta \cdot \Delta h^{1/3} / \theta \cdot a_0^2 \tag{9}$$

*Businger [1968]* argues that turbulence will develop out of shear flow when the Richardson number is below a critical level of 0.25. Let us assume that this value of  $Ri$  also characterizes the critical limit to which the mean maximum wind shears in expression (9) may develop. With this assumption, we arrive at

$$\Delta\theta = 11.77/(\Delta h)^{1/3} \tag{10}$$

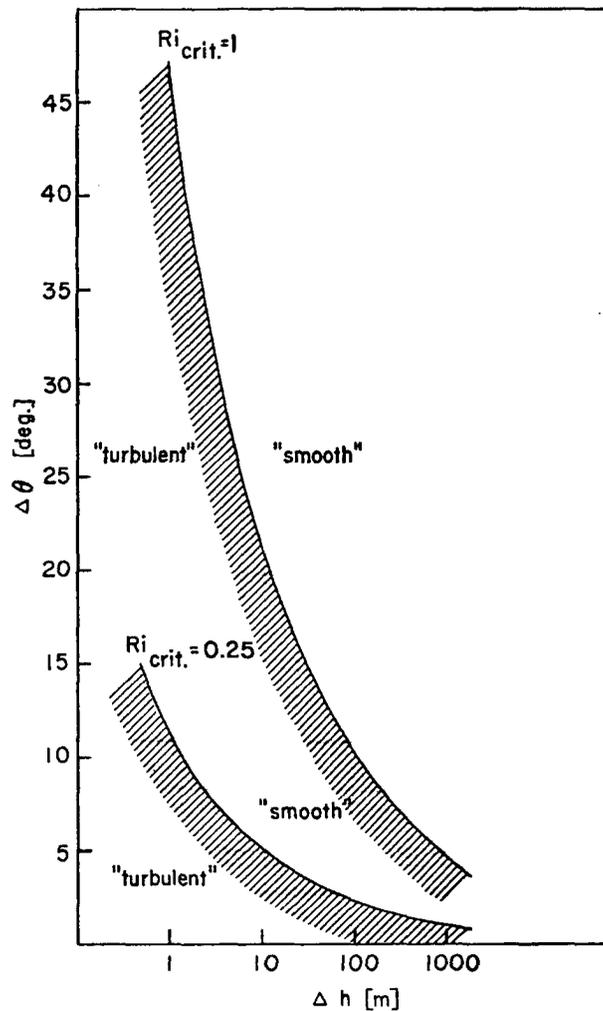


Fig. 2. Maximum vertical temperature differences  $\Delta\theta$  in degrees under conditions of maximum vertical wind shear as given by equation 1 ( $a_0 = 1.22 \text{ m}^{2/3} \text{ sec}^{-1}$ ,  $a_1 = 1/3$ ) for 'critical' Richardson numbers as indicated.

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where  $\theta = 310^\circ$ ,  $g = 9.8 \text{ m sec}^{-2}$ , and  $a_0 = 1.22 \text{ m}^{2/3} \text{ sec}^{-1}$ . A critical Richardson number of 1 would yield, for the same parameter values as above,

$$\Delta\theta = 47.08/(\Delta h)^{1/3} \quad (11)$$

where  $\Delta\theta$  indicates the maximum vertical potential temperature gradient as a function of layer thickness  $\Delta h$ , which would be required to maintain a state of 'just no turbulence' under (mean) extreme shear conditions. The two functional relationships (10) and (11) are shown in Figure 2.

If for a given height increment  $\Delta h$ , the observed temperature difference falls *below* the lines shown in Figure 2, turbulence should be expected, provided that the corresponding wind shear in this layer reached maximum values. From Figure 3 it appears that strong inversion conditions of the order of  $12^\circ/1 \text{ meter}$ , or  $5^\circ/10 \text{ meters}$  should rarely occur

in the atmosphere. We may conclude, therefore, *shallow* layers revealing maximum shear conditions should *always* ensue in turbulent flow. Deep however, may be turbulent or 'smooth,' even the wind shear conditions given by (1) with  $a_1$  depending on the actual temperature structure under isothermal conditions in the stratosphere  $\Delta\theta \sim 10^\circ$  for  $\Delta h = 1000 \text{ meter}$ . Such a value still render 'smooth' conditions for  $Ri_{crit} = 1$ . Turbulence may exist, however, for  $Ri_{crit} = 1$ . *Reiter* [1968], *Reed* [1968], and *Businger* [1968] have speculated that the development of a turbulent region within a relatively thick stratified layer should result in the development of an adiabatic region with a nearly constant wind speed by two stable layers in which strong vertical shears are concentrated. The mixing processes within the turbulent layer also apply to passive

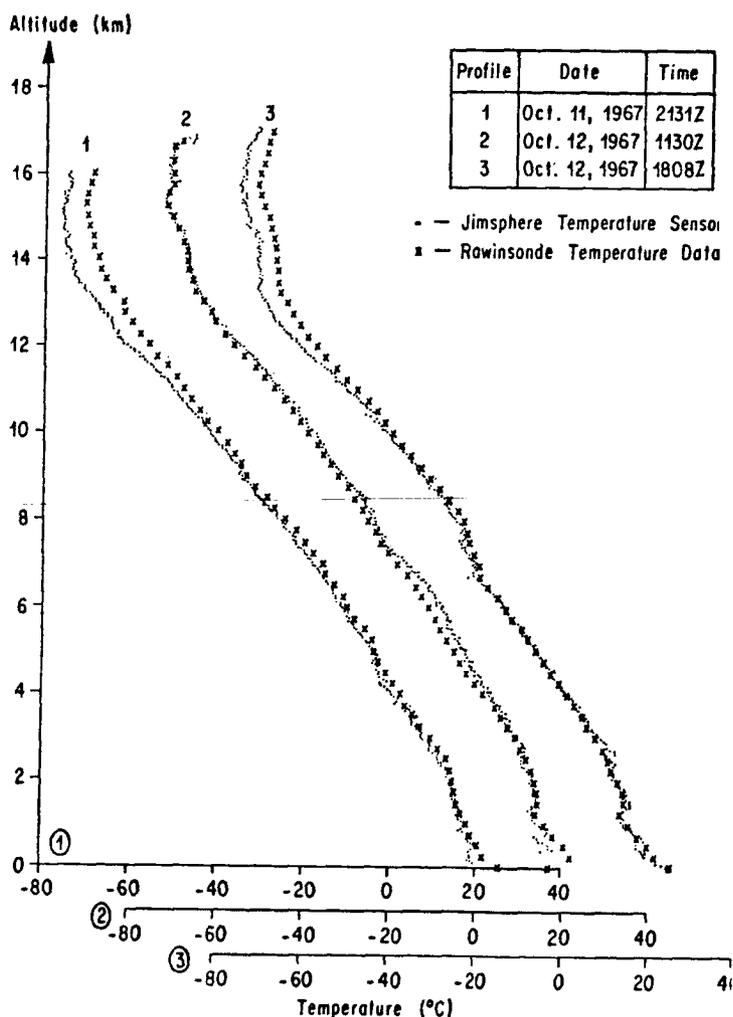


Fig. 3. Temperature measurements over Cape Kennedy with Jimsphere sensor (dots) and rawinsonde (crosses) for dates as indicated. [After Caplan and Camp, 1968.]

mixtures, such as water vapor. If a vertical gradient of this quantity existed prior to the onset of turbulence, the mixing process will 'concentrate' the gradient along the upper and lower boundaries of the turbulent layer. Backscattering of radio or radar signals will be enhanced by the resulting sharp gradients in the refractive index.

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