A STUDY OF WIND EFFECTS ON HOUSTON TWIN OFFICE BUILDINGS

by

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Symbol	
C_p	Mean pressure coefficient, $\dfrac{(\overline{p - p_\infty})}{(1/2)\rho U_H^2}$
$C_{p_{rms}}$	Root-mean-square (RMS) pressure coefficient, $\dfrac{\Delta P_{rms}}{(1/2)\rho U_H^2}$
$C_{p_{inst}}$	Instantaneous peak pressure coefficient, $\dfrac{(p' - p_\infty)}{(1/2)\rho U_H^2}$
p	Pressure at a measurement port
p_∞	Reference static pressure in the free stream
ΔP	Mean pressure difference, $(\overline{p - p_\infty})$
ΔP_{rms}	Root-mean-square pressure, $[(\overline{p - p_\infty})^2]^{1/2}$
Δh	Difference between static and dynamic pressure above boundary layer
p'	Instantaneous peak pressure
u	Local instantaneous velocity
U	Local mean velocity
U_H	Reference velocity of approach wind at the top of the structure
$(\overline{\quad})$	Time average
$(\quad)_A$	Reference conditions outside the boundary layer influence
z	Height above surface level
δ	Height of boundary layer
ρ	Mass density of air
ν	Kinematic viscosity of air
ε	Energy dissipation in the turbulent flow
κ	Wavenumber, $2\pi f/U$
f	Frequency, cycles per second

1. INTRODUCTION

The aerodynamic loading on tall buildings produced by strong winds represents an important problem for structural designers. Where local building codes are conservative in specifying wind loads, the design of outer skin panels and windows may be significantly more expensive than that required by the actual loadings on the structure. If the design loading is too lenient, expensive cladding damage may result after the structure is placed into service. The determination of wind forces on structures can be accomplished through the use of scale models placed in a wind tunnel capable of simulating the atmospheric boundary layer winds. Knowledge of the real aerodynamic forces to be experienced by the structure permit a realistic and economic design while maintaining an adequate safety margin.

Laboratory measurements of pressure distributions on the structure under a variety of wind directions corresponding to known high-wind experience allows the mean forces and moments to be calculated. The fluctuating-pressure and instantaneous-peak-pressure magnitudes are of importance in insuring adequate design for cladding. Visualization of flow about the building identifies possible problem areas where detailed measurements are required and provides valuable information on sidewalk wind magnitude and gustiness which might be induced by the structure.

The objective of this investigation was to obtain mean, fluctuating (root-mean-square), and instantaneous peak pressures on a scaled model of the twin towers proposed to be built in downtown Houston. In addition, a flow visualization study was designed to determine the flow pattern about the structure and to identify possible sidewalk environmental problems.

The study objectives were met by installing a scale model of the structure with a suitable model of the surrounding city in the Colorado State University meteorological wind tunnel. Wind was blown across the model from azimuths corresponding to frequent high-wind directions. A thick turbulent-boundary-layer flow was generated upwind in order to appropriately model the prototype environment. Measurements on the building included a comprehensive survey of mean pressure, a selective survey of fluctuating and peak pressures and several pressure-fluctuation spectra. Measurements about the building included flow visualization with smoke, velocity measurements in the sidewalk environment, velocity and turbulence profiles upstream from the structure and, with the building removed, velocity and turbulence intensity profiles at the building site. In addition, several turbulent energy spectra were taken at the building site.

2. MODELING CONFIGURATION

Modeling the aerodynamic loading on a structure requires special consideration of flow conditions in order to guarantee similitude between model and prototype. A detailed discussion of the similarity requirements and their wind-tunnel implementation can be found in References 1, 2 and 3. In general, the requirements are that the model and prototype be scaled in geometry, that the approach mean velocity at the building site have a vertical profile shape similar to the full-scale flow, that the turbulence characteristics of the flows be similar, and that the Reynolds number for the model and prototype be equal.

Proper similarity of mean velocity profiles and turbulence characteristics have not been obtained in a conventional aerodynamic

wind tunnel with a short test section. Proper profiles can be generated only by natural development of the boundary layer over a rough surface for a long distance. The wind tunnel used for this study was developed specifically to generate the thick turbulent boundary layers necessary to simulate atmospheric flows on a scale consistent with the building-model scales required to adequately model actual buildings.

Reynolds-number similarity guarantees that the flow dynamics will be the same in the model and the prototype. In this event, the drag coefficient and thus the pressure coefficient will be identical for both. Although it is impossible to obtain equality of Reynolds numbers between wind-tunnel model and prototype, this is not a severe drawback [3]. The Reynolds number for a typical large structure in a moderately strong wind will be in the order of 10^7 while the wind-tunnel model will have a Reynolds number of about 10^5. At these large Reynolds numbers, the flow dynamics about a bluff body with sharp edges and thus the value of the pressure coefficient is virtually independent of Reynolds number. Acceptable flow similarity is achieved despite the difference in Reynolds number.

2.1 Wind Tunnel

The study was performed in the meteorological wind tunnel located in the Fluid Dynamics and Diffusion Laboratory at Colorado State University (Figure 1). The tunnel is a closed circuit facility driven by a 250 h.p. variable-pitch, variable-speed propeller. The test section is nominally 6 feet square and 88 feet long fed through a contraction with a 9-to-1 area ratio. The test section walls diverge 1 in./10 ft and the roof is adjustable to maintain a zero pressure gradient

along the test section. The mean velocity in the test section can be adjusted continuously from 1 to 120 fps. The facility is described in detail by Plate and Cermak [4].

2.2 Model

In order to obtain an accurate assessment of local pressures using piezometer taps, the model was constructed to the largest scale that would not produce serious blockage in the wind tunnel. A 1:192 scale model was constructed from 3/4 in. "Lucite". Recent studies indicate that the mullion scale should be larger than that of the structure to correctly include the local pressure effects caused by the mullions [5]. A scale of 1:96 was selected. Mullions were made from 0.125 x 0.030 in. spring steel pressed into 0.065 in. deep slots milled into the surface leaving 0.060 in. exposed.

Piezometer taps (1/16 in. dia.) were drilled normal to the exterior surface at 213 locations on one building and galleria cover. Because of symmetry of the two towers involved in the study, only one was constructed with mullions and pressure ports. The data for the second tower was obtained by reversing the position of the instrumented tower. Figure 2 shows a photograph of the completed model. Figure 3 indicates the location of the pressure taps on the building and the code designation of the ports.

The model was mounted at the center of a 72 in. diameter turn-table flush with the wind-tunnel floor at the downstream end of the 88 foot test section. The turntable indicated the azimuthal orientation of the building model to ±0.1 degree.

The city surrounding the building site was constructed from styrofoam blocks cut to the proper shapes. This detailed modeling was

used for a two-block radius surrounding the building and was mounted on the turntable with the model. In the four to five blocks upstream from the finely detailed region, bricks stacked to conform to approximate building geometry were used. These bricks were rearranged every time the turntable was rotated so that appropriate buildings were represented. The region farther upstream was modeled by a randomized roughness constructed from bricks with gradually increasing roughness toward the city model. The purpose of this roughness was to generate a thick turbulent boundary layer with characteristics similar to those expected in the field environment. The detailed modeling near the structure under investigation insured that flow disturbances in the vicinity of the structure would produce the correct influence on surface pressures. The city model installed in the wind tunnel is shown in Figure 4. The wind-tunnel ceiling was adjusted with the model in place to obtain a zero pressure gradient along the test section.

3. INSTRUMENTATION AND DATA ACQUISITION

3.1 Flow Visualization

Visualization of the flow in the vicinity of the model is helpful in understanding and interpreting mean and fluctuating pressures, in defining zones of separated flow and reattachment where pressure coefficients may be expected to be high, and in indicating areas where pedestrian discomfort may be a problem. To accomplish this end, titanium tetrachloride smoke was released from sources on and near the model and motion-picture records made. The conclusions obtained from these smoke studies are discussed in Sec. 4.2.

3.2 Mean Pressures

Mean pressures were obtained by a pressure transducer attached to tubes leading to the various ports. A total of 213 tubes (1/8 in. I.D.)--one from each piezometric tap--were brought down through the turntable to a plate with 256 holes. A matching plate which can be rotated to four different positions brought the pressure from 64 tubes at a time to a mechanical scanning valve which sampled each tube in turn. The pressure from each tube was read from an MKS Baratron pressure transducer. The reference pressure for each measurement was taken as the static pressure measured at the side tap of a pitot tube mounted in the free stream directly above the model. This pitot tube was also used to measure the reference velocity.

3.3 Fluctuating Pressures

Four "Statham" differential strain-gauge transducers (Model PM283) were used to measure fluctuating pressures. The transducers were mounted inside the model as close to the pressure taps as possible. Three-inch long flexible vinyl tubing (1/8 in. I.D.) connected one side of the transducer to the port of interest. The other side of the transducer was connected to the static side of the reference pitot tube by a tube brought up through the floor. In this way the transducer measured the instantaneous difference between the local surface pressure and the static pressure in the free stream.

The transducer was mounted in a bridge circuit followed by a DC amplifier. Output was recorded on a Hewlett-Packard digital voltmeter, a B & K True-RMS and peak-to-peak meter, a Tektronix oscilloscope, a Brush (model 280) strip chart recorder, and a General Radio Corporation wave analyzer. Figure 5 shows a block diagram of the measuring system.

The transducers, having a demonstrated linear output, were calibrated indirectly. The mean voltage measured by the transducer was identified with the mean pressure previously measured by a directly calibrated transducer so that RMS and peak-to-peak pressures could be determined.

3.4 Velocity Measurements

Vertical profiles of mean velocity using a pitot tube were taken at the intersection of Main and Prairie (two diagonal blocks upwind from the structure) and at the building site without the model in place. Ambient wind azimuth was 80 degrees. Mean velocity and turbulence intensity at both sites were recorded by hot-wire anemometry. In addition, power spectral density measurements were made at three heights in the boundary layer at the building site. Hot-wire measurements of velocity and fluctuations in the street-level environment with the structure in place were made for the worst case identified through the flow visualization.

A Colorado State University hot-wire anemometer was used with a Thermo-Systems probe to obtain the measurements. Output was recorded by the digital voltmeter, RMS voltmeter, oscilloscope, and wave analyzer discussed above.

4. RESULTS

4.1 Velocity Measurements

Velocity profile and turbulence intensity measurements were made to define the characteristics of the flow approaching the model. It is recognized that atmospheric boundary-layer velocity profiles can be well represented by a velocity the varies logarithmically with height for strong wind without thermal stratification.

Figure 6 shows two mean velocity profiles taken in the wind tunnel--one two blocks upwind of the model, the other at the building site (with model removed). Both show the expected logarithmic relationship. Deviation from the straight line behavior is anticipated near the ground where roughness elements provide local disturbances.

Turbulence intensity profiles are shown in Figure 7. Turbulence intensity is defined as the root-mean-square of the velocity fluctuations divided by the local mean velocity. As expected, the turbulence level was highest at elevations corresponding to the effective height of neighboring buildings with decreasing turbulence above and below. Substantial turbulence intensity (7.5%) remained up to an elevation of 650 feet. Figures 6 and 7 show that the 31 inch height of the model was still well within the boundary-layer flow. The boundary-layer thickness corresponded to a field value of nearly 800 feet--a realistic value.

Power-spectral-density measurements were made at the building site at three separate elevations. The purpose of the measurements was to compare the spectral structure of the turbulence with typical values from the atmosphere and from previous wind tunnel measurements. Figure 8 shows this relationship for the longitudinal component of turbulence. The variables plotted are the power spectral density and wave number shown in Kolmogorov nondimensionalized form. The agreement with previous data is excellent.

4.2 Flow Visulization

A 1200 foot, 16 mm motion picture was the primary product of the flow visualization studies. Figure 9 gives a reference grid for smoke-release points and Table 2 shows the sequence of release points shown in the

motion picture. Review of that record revealed a number of flow characteristics worthy of emphasis. The entire environment about the two towers is characterized by a highly complex, three-dimensional, unsteady flow. When flow is directed into the triangular shaped (as seen from above) notch above the galleria cover and between the structures, a vigorous clockwise vortex is observed (Figure 11). Combined with the vortex is a strong downward flow at elevations below about 250 feet above the street. This downward flow is deflected by the galleria cover causing the downwash to hit the street along the galleria intersection with the ground. A particularly strong flow occurs in the adjacent intersection. The unsteadiness of the overall flow is reflected in the downwash which causes large velocities with strong fluctuations on the sidewalk areas of adjacent streets.

The most severe effects were noted for a flow approaching from the southeast. For a wind azimuth of 120^{o}, a street-level velocity at the intersection of Rusk and Milam (See Figure 9) was measured as approximately 60% of the velocity at the building-top level. Fluctuations are irregular but gust magnitude is approximately 50% of the velocity measured. The wind magnitude drops somewhat away from the intersection. At a position one-half block away (on Milam between Walker and Rusk), the velocity is 40% of the building height with fluctuations about 50% of the measured velocity. In front of the galleria entrance measurements showed 20% of ambient velocity. Because of difficulty in properly orienting the probe to the mean flow at this location, this measurement was low; the acutual value may be as high as 40%. The downwash effect decreases as the ambient flow direction varied from southeasterly.

A significant flow feature identified by smoke flow is an intermittent flow separation along sides of the structure that are nearly parallel to the approach flow. The flow along the wall can alternately separate from and reattach to the structure. This effect was noted over a range of approach azimuths of approximately 15^{o}. The effect is confined to the upper half of the structure -- the interference of surrounding buildings disrupting the effect at lower elevations. The alternating separation and reattachment phenomena will have a significant influence on RMS-pressure fluctuations and possibly on noise generation.

Several smoke experiments were performed with two large buildings located on blocks adjacent to the twin towers. The buildings were modeled as parallelopipeds completely filling their blocks with buildings as high as the towers. Their effect in all cases was to decrease the magnitude of the above noted phenomena. When the towers were located directly in the wake of one of these structures, the flow patterns were altered completely with all wind magnitudes surrounding the towers substantially reduced.

4.3 Mean Pressures

The mean pressure coefficient C_p is defined as

$$C_p = \frac{\overline{(p - p_\infty)}}{(1/2)\rho U_H^2} \qquad (1)$$

where p is the locally measured pressure in the structure, p_∞ is the static pressure in the freestream, ρ is the air mass density, and U_H is the reference wind speed at the elevation of the building top. Pressures were measured at 213 locations on each of the two buildings for 15 azimuthal directions--a total of 6390 measurements.

Eleven directions from east through south and four northerly approach flow conditions were used to represent the most likely directions for high winds. The measured $p - p_\infty$ values in millimeters of mercury and the computed C_p values are listed in Appendix A. The pressure-tap code is described in Figure 3.

Typical maps of constant pressure coefficient are shown in Figures 12 and 13 for a wind azimuth of 120^o. It should be noted than in some cases the contour interval is changed in order to provide maximum information with minimum clutter. The regions of high negative pressure are generally found in the separated regions near corners. No anomalies are seen in the pressure distribution in the vicinity of the gap between the structures.

4.4 Fluctuating Pressures

Fluctuating measurements were taken at 26 locations under a variety of approach directions. The taps were selected to identify the largest positive and negative pressure coefficients and to give a general indication of conditions in regions of moderate fluctuation activity. The pressure coefficients are listed in Figure 14. Two pressure coefficients are defined for that data in addition to the mean pressure coefficient.

$$C_{p_{rms}} = \frac{\Delta P_{rms}}{(1/2)\rho U_H^2}$$

where ΔP_{rms} is the rms of the fluctuating pressure difference $p - p_\infty$ and the other variables are as previously defined. $C_{p_{rms}}$ is the pressure coefficient for the fluctuating component of the pressure acting on the structure. If the pressure fluctuations were of a regular form (such as a sine wave), the relationship of peak-to-peak and root-mean-square

pressures would be known and instantaneous peak pressures could be determined from $C_{p_{rms}}$. For the present data, this relationship varied from location to location and the peak pressures were not symmetrically distributed on both sides of the mean. Because the peak instantaneous pressures on the structure are of interest, another pressure coefficient was defined as follows:

$$C_{p_{inst}} = \frac{(p' - p_\infty)}{(1/2)\rho U_H^2} \tag{3}$$

where p' is the peak instantaneous pressure identified from a high-frequency-response strip-chart recording. A typical strip chart is shown in Figure 15. The largest negative $C_{p_{inst}}$ obtained was -2.95 while the largest positive value found was +1.07.

A spectral analysis of the pressure fluctuations showed no indications of frequency peaks that could cause single-frequency loading of the structure. A semiperiodic frequency of approximately 1/2 to 1 cycle per second was observed from the smoke visualization. However, autocorrelation measurements failed to reveal coherence in that frequency.

5. CONCLUSIONS

The velocity and turbulence profiles along with the power-spectral-density measurements indicated that the atmospheric flow characteristics were adequately modeled. The low-frequency end of the power spectrum followed the atmospheric data more closely than previous wind tunnel measurements indicating that the modeling was more representative of prototype conditions than previous wind-tunnel modeling.

The maximum $C_{p_{inst}}$ value obtained on the model was -2.95 for the peak pressure at port FC1 on Building I for a wind azimuth of 120 degrees.

The peak $C_{p_{inst}}$ on the roof was -1.79 at port TC1 on building I for a wind azimuth of 120 degrees. The largest positive $C_{p_{inst}}$ was 1.37 at port DC3 on building II for an approach azimuth of 80 degrees. Large values of negative mean and fluctuating values of C_p were characteristically found near corners in separated regions or in intermittent separated regions. The presence of additional large buildings near the towers can be expected to decrease rather than intensify the values of C_p reported.

Flow visulization showed the flow about the structure to be highly unsteady. Intermittent separation on the building was noted for certain ranges of wind directions which added to the magnitude of $C_{p_{inst}}$ values and which might be significant in terms of noise generation. The influence of the towers on the ambient flow gave rise to strong wind currents at sidewalk level for generally southeast winds. Wind magnitudes of up to 60% of the velocity at building height with strong fluctuations were measured in the model.

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TABLE I

MOTION PICTURE SCENE LISTING

Titles list: 1) the run number (consecutive 1 through 27), with a letter for the model configuration (A as presently existing with the addition of the Towers and B as proposed with other major buildings added), 2) the wind direction in degrees True Azimuth with 0° being N, 90° being E, etc., 3) the location of the source and 4) the elevation of the source in feet above the ground.

Run		Wind AZ		Source		El.	
	1A		80		I-5		0'
	2A		80		I-5		0'
	3A		80		I-7		0'
	4A		80		F-5		0'
	5A		80		I-5		320'
	6A		80		I-6		320'
	7A		80		I-5		320'
	8A		80		H-7		144'
	8B		80		I-5		0'
	9B		80		I-5		0'
	10B		80		I-7		0'
	11B		80		I-6		320'
	12B		80				
	13B		80		E-6		0'
	14A		125		I-8		0'
	15A		125		I-7		0'
	16A		125		I-9		0'
	17A		125		E-6		0'
	18A		125		I-8		320'
	19A		125		I-8		160'
	20A		125		H-8		192'
	21A				H-9		320'
	22A		150-240		G-7, H-8		320'
	23A		300-60		G-7, F-9		320'
	24B		125		H-7		192'
	25B		125		E-7		320'
	26B		125		J-6		320'
	27B		125		I-5		0'

TABLE 2

FLUCTUATING PRESSURE DATA

Bldg	Wind Azimuth	Sensor	Sensor Location	C_p	$C_{p_{rms}}$	$C_{p_{inst}}$
I	120°	1	TC1	-1.07	.46	-1.79
		2	FC1	-1.00	.59	-2.95
		3	DB10	- .53	.29	-1.16
		4	SD2	+ .51	.32	+1.07
I	180°	1	FC13	- .51	.37	-1.18
		2	DC3	- .56	.26	± .80
		3	BC3	+ .09	.36	
I	120°	1	FC13	- .26	.11	
		2	DC3	- .30	.20	
		3	BC3	+ .35	.13	
I	80°	1	FC13	- .15	.05	
		2	DC3	- .52	.36	
		3	BC3	+ .28	.08	
II	0°	1	FC13	- .67	.22	-1.07
		2	DC3	- .59	.18	- .96
		3	BC3	+ .25	.23	
II	80°	1	FC13	- .64	.13	- .826
		2	DC5	+ .09	.54	
		3	BC3	- .46	.13	
		2'	DC3	+ .46	.54	+1.37
II	120°	1	FC13	- .63	.43	-1.30
		2	DC5	+ .31	.13	+ .94
		3	BB3	- .26	.09	
II	170°	1	FC13	- .04	.16	- .27
		2	DC5	- .07	.28	
		3	BB3	- .50	.10	

APPENDIX A

MEAN PRESSURE DATA

NOTES

1. The following ports indicated pressures which are probably incorrect due to tube crimping:

SC8	All Data
B6	Building II Data
GA1	Building II, 120^{o}

2. An * by a ΔP reading indicates higher than average fluctuations in the pressure transducer output.

3. ΔP's listed are in millimeters of mercury-- 1mm of Hg = 2.79 lb/ft^2 at $0^{o}C$.

4. WIND SPEED indicated is U_A -- above the influence of the boundary layer.

DATE 3-28-72 WIND DIRECTION: 80° Δh = 1.836 mm Hg P_A = 24.69 in. Hg WIND SPEED: 73.33 fps

TIME 7:00 p.m. Building I T = 60°F ρ_A = 0.001902 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	+.126*	+.087	1	+.169*	+.117	1	+.562*	+.390	1	+.824*	+.571
	2	+.164*	+.113	2	+.230*	+.159	2	+.541*	+.375	2	+.780*	+.541
	3	+.150*	+.104	3	+.200*	+.139	3	+.482*	+.334	3	+.730*	+.506
	4	--	--	4	+.120*	+.083	4	+.409*	+.284	4	+.601*	+.417
	5	+.123*	+.085	5	+.096*	+.067	5	+.360*	+.250	5	+.654*	+.453
	6	+.126*	+.087	6	+.086*	+.060	6	+.316*	+.219	6	+.502*	+.348
	7	+.113*	+.078	7	+.028*	+.019	7	+.223*	+.155	7	+.358*	+.248
	8	+.110*	+.076	8	+.131*	+.091	8	+.462*	+.320	8	+.724*	+.502
	9	-.056*	-.039	9	-.037*	-.026	9	+.220*	+.153	9	+.354*	+.245
	10	-.114*	-.079	10	-.169*	-.117	10	+.160*	+.111	10	+.313*	+.217
	11	-.174*	-.121	11	-.228*	-.158	11	+.044*	+.031	11	+.141*	+.098
	12	-.248*	-.172	12	-.232*	-.161	12	-.078*	-.054	12	-.010*	-.007
	13	-.293*	-.203	13	-.375*	-.260	13	-.217*	-.150	13	-.120*	-.083
	14	-.468*	-.324	14	-.567*	-.393	14	-.526*	-.345	14	-.339*	-.235
	15	--	--	15	--	--	15	--	--	15	-.545*	-.378

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.770*	-.534	1	-.620*	-.430	1	-.686	-.476	1	-.637	-.442
	2	-.770*	-.534	2	-.751*	-.521	2	-.722	-.500	2	-.672	-.466
	3	-.770*	-.534	3	-.770*	-.534	3	-.748	-.519	3	-.724	-.502
	4	-.772*	-.535	4	-.700*	-.485	4	-.772	-.535	4	-.770	-.534
	5	-.758*	-.525	5	-.769*	-.533	5	-.789	-.547	5	-.806	-.559
				6	-.758*	-.525	6	-.768	-.532	6	-.824	-.571
				7	-.644*	-.446	7	-.752	-.521	7	-.800	-.555
				8	-.764*	-.530	8	-.744	-.516	8	-.802	-.556
				9	-.776*	-.538	9	-.738	-.512	9	-.800	-.555
				10	-.890*	-.617	10	-.755	-.523	10	-.800	-.555

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	+.090*	+.062	1	-.044*	-.031	1	-.20*	-.139	1	-.200*	-.139	1	+.728	+.505
	2	+.085*	+.059	2	+.050*	+.035	2	-.050*	-.347	2	0*	0			
	3	+.110*	+.076	3	+.088*	+.061	3	--	--	3	+.150*	+.104			
	4	+.128*	+.089	4	+.146*	+.101	4	+.220	+.153	4	+.340*	+.236			
	5	+.134*	+.093	5	+.196*	+.136	5	+.312	+.216	5	+.448*	+.311			
	6	+.168*	+.116	6	+.240*	+.166	6	+.396	+.275	6	+.544*	+.377			
	7	+.178*	+.123	7	+.270*	+.187	7	+.450*	+.312	7	+.692*	+.480			
	8	+.190*	+.132	8	+.326*	+.226	8	+.543*	+.376	8	+.775*	+.537			
	9	+.194*	+.134	9	+.342*	+.237	9	+.576*	+.399	9	+.788*	+.546			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	+.060*	+.042	1	-.350*	-.243	1	-.330*	-.229	1	-.354*	-.245	1	-.638	-.442
	2	-.068*	-.047	2	+.090*	+.062	2	+.185*	+.128	2	+.228*	+.158	2	-.470	-.326
	3	--	--	3	+.276*	+.191	3	+.408*	+.283	3	+.502*	+.348	3	-.580	-.402
	4	+.050*	+.035	4	+.070*	+.049	4	+.193*	+.134	4	+.136*	+.094	4	-.784	-.543
				5	-.230*	-.159	5	-.380*	-.263	5	-.690*	-.478	5	-.835	-.579
				6	-.343*	-.238	6	-.690*	-.478	6	-1.007	-.698	6	-.723	-.501
				7	-.274*	-.190	7	-.520*	-.360	7	-.768	-.532	7	-.676	-.469
				8	-.170*	-.118	8	-.438*	-.304	8	-.616	-.427	8	-.640	-.444
							9	-.398*	-.276	9	-.274*	-.190			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	+.537	+.372	1	+.006*	+.004	1	+.30	+.208
	2	+.566	+.392	2	+.41*	+.284	2	.204*	+.141
	3	.41	+.284	3	+.318*	+.220	3	.086*	+.060
	4	.255*	+.177	4	.232*	+.161	4	-.025*	-.017
	5	.142*	+.098	5	.152*	+.105	5	-.076*	-.053
	6	.108*	+.075	6	.07*	+.049	6	-.226	-.157
	7	.024*	+.017	7	-.057*	-.040	7	-.338	-.234
	8	-.21	-.146	8	-.276	-.191			
	9	-.40	-.277	9	-.45	-.312			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p
	1	-.727	-.504	1	-.742	-.514	1	-.754	-.523	1	-.752	-.521
	2	-.74	-.513	2	-.756	-.524	2	-.758	-.525	2	-.752	-.521
	3	-.74	-.513	3	-.758	-.525	3	-.758	-.525			
	4	-.752	-.521	4	-.758	-.525						
	5	-.745	-.516									

MISC.

DE	ΔP	C_p
1	-.9	-.624
2	-.9	-.624
3	-.9	-.624

BC 9 -.106* -.073

DATE 3-28-72 WIND DIRECTION: 90° Δh = 1.836 mm Hg P_A = 24.69 in. Hg WIND SPEED: 73.33 fps

TIME 1:00 p.m. Building I T = 60°F ρ_A = 0.001902 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	.042*	+.029	1	-.1*	-.069	1	+.07*	+.048	1	+.229*	+.159
	2	.075*	+.052	2	+.06*	+.041	2	+.250*	+.173	2	+.401*	+.278
	3	.075*	+.052	3	+.05*	+.035	3	+.245*	+.170	3	+.386*	+.268
	4	--	--	4	+.02*	+.014	4	.174*	+.121	4	+.250*	+.173
	5	.001*	+.007	5	0*	0	5	.135*	+.094	5	+.330*	+.229
	6	0*	0	6	-.02*	-.014	6	.139*	+.096	6	+.254*	+.176
	7	0*	0	7	-.06*	-.041	7	.014*	+.010	7	+.088*	+.061
	8	0	0	8	+.02*	+.014	8	+.236*	+.164	8	+.395*	+.274
	9	-.17*	-.118	9	-.13*	-.090	9	+.033*	+.023	9	+.080*	+.055
	10	-.24*	-.166	10	-.256*	-.177	10	-.036*	-.025	10	+.059*	+.041
	11	-.3	-.208	11	-.295*	-.204	11	-.104*	-.072	11	-.079*	-.055
	12	-.345	-.239	12	-.28*	-.194	12	-.234*	-.162	12	-.207	-.143
	13	-.31	-.215	13	-.384	-.266	13	-.335*	-.232	13	-.282	-.195
	14	-.5	-.347	14	-.53	-.367	14	-.582*	-.403	14	-.474*	-.329
	15			15			15			15	-.591*	-.410

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.625*	-.433	1	-.452	-.313	1	-.625	-.433	1	-.650	-.45
	2	-.645*	-.447	2	-.596	-.413	2	-.660	-.458	2	-.672	-.466
	3	-.648*	-.449	3	-.616*	-.427	3	-.678*	-.470	3	-.698	-.484
	4	-.638*	-.442	4	-.562*	-.390	4	-.718	-.498	4	-.716	-.496
	5	-.663*	-.460	5	-.700*	-.485	5	-.740	-.513	5	-.710	-.492
				6	-.725*	-.502	6	-.732	-.507	6	-.707	-.490
				7	-.495*	-.343	7	-.725	-.503	7	-.680	-.471
				8	-.757*	-.525	8	-.724	-.502	8	-.680	-.471
				9	-.784*	-.543	9	-.725	-.503	9	-.680	-.471
				10	-.987*	-.684	10	-.740	-.513	10	-.692	-.480

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	+.215*	+.149	1	+.065*	+.045	1	+.004*	+.003	1	+.034	+.023	1	+.299*	+.207
	2	+.210*	+.146	2	+.168*	+.116	2	+.155*	+.107	2	+.230	+.159			
	3	+.212*	+.147	3	+.210*	+.146	3	--	--	3	+.462*	+.320			
	4	+.222*	+.154	4	+.280*	+.194	4	+.410*	+.284	4	+.570*	+.395			
	5	+.222*	+.154	5	+.292*	+.202	5	+.520*	+.36	5	+.705*	+.489			
	6	+.227*	+.157	6	+.325*	+.225	6	+.568*	+.394	6	+.828*	+.574			
	7	+.235*	+.163	7	+.362*	+.251	7	+.648*	+.449	7	+.921*	+.638			
	8	+.235*	+.163	8	+.380*	+.263	8	+.720	+.499	8	+1.018*	+.706			
	9	+.235*	+.163	9	+.350*	+.243	9	+.736*	+.51	9	+1.048*	+.726			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	+.156*	+.108	1	-.298	-.207	1	-.300	-.208	1	-.251	-.174	1	-.473	-.328
	2	+.016	+.011	2	+.220*	+.152	2	+.254*	+.176	2	+.326*	+.226	2	-.321	-.222
	3	--	--	3	+.428*	+.297	3	+.560*	+.388	3	+.644*	+.446	3	-.507*	-.351
	4	+.154	+.107	4	+.230*	+.159	4	+.455*	+.315	4	+.374*	+.259	4	-.782*	-.542
				5	-.129	-.089	5	-.170*	-.118	5	-.518	-.359	5	-.872	-.604
				6	-.235	-.163	6	-.614*	-.426	6	-.994	-.689	6	-.686	-.476
				7	-.142	-.098	7	-.410	-.284	7	-.654*	-.453	7	-.624	-.432
				8	-.055	-.038	8	-.278	-.193	8	-.488	-.338	8	-.570	-.395
							9	-.264	-.183	9	-.216	-.150			

DATE 3-29-72 Δh = 1.833 P_A = 24.66 in Hg

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	.000*	0	1	-.778	-.540	1	-.032	-.022
	2	+.225*	+.156	2	+.156	+.108	2	-.008*	-.005
	3	+.209*	+.145	3	+.116	+.080	3	-.040	-.028
	4	+.086	+.06	4	+.067	+.046	4	-.122	-.085
	5	-.023	-.016	5	-.010	-.007	5	-.153	-.106
	6	-.076	-.053	6	-.076	-.053	6	-.286	-.199
	7	-.164	-.114	7	-.165	-.114	7	-.380	-.264
	8	-.310	-.215	8	-.330	-.229			
	9	-.467	-.324	9	-.457	-.317			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p	MISC. DE	ΔP	C_p
	1	-.616	-.428	1	-.665	-.462	1	-.684	-.475	1	-.692	-.48	1	-.690	-.479
	2	-.640	-.444	2	-.663	-.460	2	-.696	-.483	2	-.691	-.48	2	-.694	-.482
	3	-.647	-.492	3	-.678	-.470	3	-.678	-.471				3	-.694	-.482
	4	-.681	-.473	4	-.694	-.482									
	5	-.708	-.492												

BC 9 0.00* 0

DATE 3-29-72 WIND DIRECTION: 100° Δh = 1.83 mm Hg P_A = 24.62 in. Hg WIND SPEED: 73.33 fps

TIME 7:00 p.m. Building I T = 60°F ρ_A = 0.001902 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.075	-.052	1	-.535	-.372	1	-.763	-.531	1	-.940	-.654
	2	.038	+.026	2	-.220	-.153	2	-.400	-.278	2	-.340	-.236
	3	.035	+.024	3	-.148	-.103	3	-.244	-.170	3	-.100	-.070
	4	--	--	4	-.150	-.104	4	-.130	-.090	4	-.100	-.070
	5	-.048	-.033	5	-.136	-.095	5	-.121	-.084	5	.000	0
	6	-.069	-.048	6	-.128	-.089	6	-.079	-.055	6	+.024	+.017
	7	-.095	-.066	7	-.128	-.089	7	-.153	-.106	7	-.107	-.074
	8	-.058	-.040	8	-.059	-.041	8	.000	0	8	+.118	+.082
	9	-.230	-.160	9	-.224	-.156	9	-.162	-.113	9	-.148	-.103
	10	-.320	-.223	10	-.340	-.236	10	-.192	-.134	10	-.148	-.103
	11	-.370	-.257	11	-.372	-.259	11	-.245	-.170	11	-.244	-.170
	12	-.414	-.288	12	-.342	-.238	12	-.358	-.249	12	-.350	-.243
	13	-.440	-.306	13	-.443	-.308	13	-.436	-.303	13	-.400	-.278
	14	-.532	-.370	14	-.575	-.400	14	-.636	-.442	14	-.548	-.386
	15	--	--	15	--	--	15	--	--	15	-.668	-.465

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.568	-.395	1	-.500	-.348	1	-.600	-.417	1	-.600	-.417
	2	-.574	-.399	2	-.610	-.424	2	-.630	-.438	2	-.640	-.445
	3	-.586	-.408	3	-.610	-.424	3	-.636	-.442	3	-.670	-.466
	4	-.600	-.417	4	-.620	-.431	4	-.664	-.462	4	-.672	-.467
	5	-.614	-.427	5	-.664	-.462	5	-.678	-.472	5	-.696	-.484
				6	-.670	-.466	6	-.672	-.467	6	-.684	-.476
				7	-.566	-.394	7	-.666	-.463	7	-.660	-.459
				8	-.728	-.506	8	-.666	-.463	8	-.660	-.459
				9	-.760	-.529	9	-.660	-.459	9	-.652	-.453
				10	-.960	-.668	10	-.660	-.459	10	-.652	-.453

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	+.362	+.252	1	+.206	+.143	1	+.260	+.181	1	+.350	+.243	1	+.546	+.380
	2	+.340	+.236	2	+.350	+.243	2	+.398	+.277	2	+.550	+.386			
	3	+.340	+.236	3	+.350	+.243	3	--	--	3	+.700	+.487			
	4	+.340	+.236	4	+.390	+.271	4	+.654	+.455	4	+.862	+.560			
	5	+.340	+.236	5	+.458	+.319	5	+.750	+.522	5	+.950	+.661			
	6	+.336	+.234	6	+.458	+.319	6	+.782	+.544	6	+1.050	+.730			
	7	+.306	+.213	7	.498	+.346	7	+.850	+.591	7	+1.100	+.765			
	8	+.302	+.210	8	+.470	+.327	8	+.960	+.668	8	+1.100	+.765			
	9	+.276	+.192	9	+.460	+.320	9	+.700	+.487	9	+.946	+.658			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	+.178	+.124	1	-.154	-.107	1	-.230	-.160	1	-.228	-.159	1	-.400	-.278
	2	+.116	+.080	2	+.400	+.278	2	+.318	+.221	2	+.388	+.270	2	-.170	-.118
	3	--	--	3	+.578	+.402	3	+.700	+.487	3	+.818	+.569	3	-.230	-.160
	4	+.245	+.170	4	+.400	+.278	4	+.700	+.487	4	+.700	+.487	4	-.630	-.438
				5	-.032	-.022	5	+.102	+.071	5	-.262	-.182	5	-.860	-.598
				6	-.140	-.097	6	-.478	-.332	6	-.838	-.583	6	-.620	-.431
				7	-.034	-.024	7	-.246	-.171	7	-.478	-.332	7	-.545	-.379
				8	+.072	+.050	8	-.100	-.067	8	-.315	-.219	8	-.470	-.327
							9	-.050	-.034	9	.000	0			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-1.010	-.702	1	-.078*	-.054	1	-.594	-.413
	2	-.436*	-.303	2	-.500*	-.348	2	-.410	-.285
	3	-.032*	-.022	3	-.246*	-.171	3	-.225*	-.156
	4	-.112*	-.078	4	-.122*	-.085	4	-.225*	-.156
	5	-.190*	-.132	5	-.148*	-.103	5	-.226*	-.157
	6	-.214*	-.149	6	-.190*	-.132	6	-.356	-.248
	7	-.290*	-.202	7	-.269*	-.187	7	-.434	-.302
	8	-.382	-.266	8	-.425	-.296			
	9	-.520	-.362	9	-.537	-.373			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p
	1	-.577	-.401	1	-.605	-.421	1	-.624	-.434	1	-.618	-.430
	2	-.576	-.401	2	-.605	-.421	2	-.624	-.434	2	-.620	-.431
	3	-.600	-.417	3	-.610	-.424	3	-.618	-.430			
	4	-.600	-.417	4	-.626	-.435						
	5	-.605	-.421									

MISC

DE	ΔP	C_p
1	-.676	-.470
2	-.682	-.474
3	-.674	-.469

BC 9 +.090* +.063

DATE 3-30-72 WIND DIRECTION: 110° Δh = 1.836 mm Hg P_A = 24.65 in. Hg WIND SPEED: 73.33 fps

TIME 11:00 a.m. Building I T = 60°F ρ_A = 0.001902 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.20*	-.139	1	-.960*	-.665	1	-1.255	-.870	1	-1.38	-.957
	2	-.068*	-.047	2	-.578*	-.401	2	-1.006	-.697	2	-1.248	-.865
	3	-.058*	-.040	3	-.402*	-.279	3	-.804*	-.557	3	-.923	-.640
	4	--	--	4	-.316*	-.219	4	-.573*	-.397	4	-.616	-.427
	5	-.136*	-.094	5	-.234*	-.162	5	-.391*	-.271	5	-.308*	-.214
	6	-.144*	-.100	6	-.198*	-.137	6	-.268*	-.186	6	-.216	-.150
	7	-.178*	-.123	7	-.253*	-.175	7	-.31*	-.215	7	-.28*	-.194
	8	-.098*	-.068	8	-.121*	-.084	8	-.188*	-.130	8	-.06*	-.042
	9	-.260*	-.180	9	-.276*	-.191	9	-.312	-.216	9	-.294	-.204
	10	-.336	-.233	10	-.378	-.262	10	-.29	-.201	10	-.255	-.177
	11	-.370	-.256	11	-.376	-.261	11	-.29	-.201	11	-.330	-.229
	12	-.401	-.278	12	-.334	-.232	12	-.37	-.256	12	-.40	-.277
	13	-.412	-.286	13	-.418	-.290	13	-.42	-.291	13	-.461	-.288
	14	-.462	-.320	14	-.500	-.347	14	-.248	-.172	14	-.502	-.348
	15	--	--	15	--	--	15	--	--	15	-.552	-.383

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.456	-.316	1	-.234	-.162	1	-.506	-.351	1	-.50	-.347
	2	-.454	-.315	2	-.478	-.331	2	-.532	-.369	2	-.525	-.364
	3	-.454	-.315	3	-.48	-.333	3	-.530	-.367	3	-.548	-.380
	4	-.458	-.317	4	-.488	-.338	4	-.56	-.388	4	-.562	-.390
	5	-.470	-.326	5	-.514	-.356	5	-.577	-.400	5	-.574	-.398
				6	-.555	-.385	6	-.582	-.403	6	-.550	-.381
				7	-.396	-.275	7	-.582	-.403	7	-.547	-.379
				8	-.611	-.424	8	-.58	-.402	8	-.534	-.370
				9	-.658	-.455	9	-.58	-.402	9	-.534	-.370
				10	-.988	-.685	10	-.58	-.402	10	-.543	-.376

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.325*	-.225	1	-.221*	-.153	1	+.375*	+.259	1	+.530*	+.367	1	+.743*	+.515
	2	-.310*	-.215	2	-.321*	-.223	2	+.492*	+.341	2	+.707*	+.490			
	3	-.309*	-.214	3	-.320*	-.222	3	--	--	3	+.868*	+.602			
	4	-.310*	-.215	4	-.364*	-.252	4	+.730*	+.506	4	+.982*	+.681			
	5	-.310*	-.215	5	-.434*	-.301	5	+.792*	+.549	5	+1.059*	+.734			
	6	-.270*	-.187	6	-.455*	-.315	6	+.845*	+.586	6	+1.068*	+.740			
	7	-.216*	-.150	7	-.464*	-.322	7	+.818*	+.567	7	+1.072*	+.743			
	8	-.162*	-.112	8	-.440*	-.305	8	+1.025	+.711	8	+.970*	+.672			
	9	-.116*	-.080	9	+.255*	+.177	9	+.463*	+.321	9	+.637*	+.442			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	+.223*	+.155	1	-.116*	-.080	1	-.180	-.125	1	-.141	-.098	1	-.300	-.208
	2	+.184*	+.128	2	+.467*	+.324	2	+.326*	+.226	2	+.422	+.293	2	-.047	-.033
	3	--	--	3	+.664*	+.460	3	+.680*	+.471	3	+.788*	+.546	3	-.023	-.016
	4	+.224*	+.155	4	+.467*	+.324	4	+.665*	+.461	4	+.788*	+.546	4	+.492	+.341
				5	+.065*	+.045	5	+.162*	+.112	5	+.003*	+.002	5	-.892*	-.618
				6	-.050	-.035	6	-.347*	-.241	6	-.641*	-.444	6	-.561	-.389
				7	+.043	+.030	7	-.100	-.069	7	-.320*	-.222	7	-.442	-.306
				8	+.108*	+.075	8	0*	0	8	-.180*	-.125	8	-.372	-.258
							9	+.055*	+.038	9	+.472	+.327			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-1.346*	-.933	1	-.343	-.238	1	-1.085	-.752
	2	-1.122*	-.778	2	-1.036*	-.718	2	-.930*	-.645
	3	-.486	-.337	3	-.771*	-.534	3	-.461*	-.320
	4	-.269	-.186	4	-.456	-.316	4	-.357	-.247
	5	-.270	-.187	5	-.328	-.227	5	-.310	-.215
	6	-.291	-.202	6	-.310	-.215	6	-.385	-.267
	7	-.341	-.236	7	-.322	-.223	7	-.414	-.287
	8	-.390	-.270	8	-.412	-.286			
	9	-.472	-.327	9	-.479	-.332			

MISC.

	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p	DE	ΔP	C_p
	1	-.444	-.308	1	-.465	-.322	1	-.474*	-.329	1	-.480	-.333	1	-.542	-.376
	2	-.454	-.315	2	-.467	-.324	2	-.474	-.329	2	-.480	-.333	2	-.542	-.376
	3	-.459	-.318	3	-.478	-.331	3	-.480	-.333				3	-.542	-.376
	4	-.468	-.324	4	-.474	-.329									
	5	-.470	-.326												

BC 9 +.142 +.098

DATE 3-30-72 WIND DIRECTION: 120° Δh = 1.825 mm Hg P_A = 24.55 in. Hg WIND SPEED: 73.33 fps

TIME 8.00 p.m. Building I T = 60° ρ_A = 0.001902 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.324	-.226	1	-.966	-.674	1	-1.440	-1.004	1	-1.320	-.921
	2	-.232	-.162	2	-.590	-.411	2	-1.340	- .935	2	-1.370	-.955
	3	-.204	-.142	3	-.440	-.307	3	-1.130	- .788	3	-1.320	-.921
	4	--	--	4	-.350	-.244	4	- .850	- .593	4	-1.120	-.781
	5	-.200	-.139	5	-.300	-.209	5	- .640	- .446	5	- .770	-.537
	6	-.218	-.152	6	-.270	-.188	6	- .440	- .307	6	- .546	-.381
	7	-.234	-.163	7	-.300	-.209	7	- .460	- .321	7	- .546	-.381
	8	-.174	-.121	8	-.190	-.133	8	- .300	- .209	8	- .500	-.349
	9	-.300	-.209	9	-.300	-.209	9	- .350	- .244	9	- .450	-.314
	10	-.340	-.237	10	-.370	-.258	10	- .310	- .216	10	- .350	- 244
	11	-.344	-.240	11	-.350	-.241	11	- .288	- .201	11	- .350	- .244
	12	-.354	-.247	12	-.310	-.216	12	-..366	- .234	12	- .390	-.272
	13	-.354	-.247	13	-.350	-.244	13	- .372	- .259	13	- .380	-.265
	14	-.374	-.261	14	-.392	-.273	14	- .460	- .321	14	- .420	-.293
	15	--	--	15	--	--	15	--	--	15	- .440	-.307

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.354	-.247	1	-.270	-.188	1	- .410	- .286	1	- .410	-.286
	2	-.340	-.257	2	-.370	-.258	2	- .430	- .300	2	- .420	-.293
	3	-.340	-.237	3	-.370	-.258	3	- .430	- .300	3	- .450	-.314
	4	-.340	-.237	4	-.340	-.237	4	- .455	- .317	4	- .450	-.314
	5	-.344	-.240	5	-.390	-.272	5	- .480	- .335	5	- .460	-.321
				6	-.390	-.272	6	- .490	- .342	6	- .460	-.321
				7	-.490	-.342	7	- .490	- .342	7	- .455	-.317
				8	-.460	-.321	8	- .490	- .342	8	- .455	-.317
				9	-.500	-.349	9	- .495	- .345	9	- .450	-.314
				10	-.760	-.53	10	- .495	- .345	10	- .450	-.314

DATE 3-31-72 TIME 8:45 Δh = 1.836 ρ_A = 24.72 in Hg

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	+.270	+.188	1	+.165	+.115	1	+ .313*	+ .217	1	+ .529*	+.367	1	+.706	+.489
	2	+.250	+.174	2	+.165	+.115	2	+ .424	+ .234	2	+ .734*	+.509			
	3	+.255	+.178	3	+.180	+.126	3	--	--	3	+ .894*	+.620			
	4	+.230	+.160	4	+.200	+.139	4	+ .597*	+ .414	4	+1.014*	+.703			
	5	+.220	+.153	5	+.180	+.126	5	+ .64*	+ .444	5	+1.100*	+.763			
	6	+.170	+.119	6	+.180	+.126	6	+ .688	+ .463	6	+1.072*	+.743			
	7	+.110	+.077	7	+.170	+.119	7	+ 655*	+ .454	7	+1.046*	+.725			
	8	+.025	+.017	8	+.130	+.091	8	+ .276	+ .191	8	+ .864*	+.599			
	9	-.055	-.038	9	-.017	-.012	9	+ .210*	+ .146	9	+ .500*	+.347			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	+.228*	+.158	1	-.132*	-.092	1	-.173*	-.120	1	-.117*	-.081	1	-.274	-.190
	2	+.184*	+.128	2	+.316*	+.219	2	+.229*	+.159	2	+.350*	+.243	2	-.074*	-.051
	3	--	--	3	+.462*	+.320	3	+.500*	+.347	3	+.67	+.464	3	-.018*	-.012
	4	+.141*	+.098	4	+.337*	+.234	4	+.453*	+.314	4	+.613	+.425	4	-.358	-.248
				5	+.138*	+.096	5	+.062*	+.043	5	-.062*	-.043	5	-.708	-.491
				6	+.064*	+.044	6	-.171*	-.119	6	-.468	-.324	6	-.456	-.316
				7	+.082*	+.057	7	-.067*	-.046	7	-.268*	-.186	7	-.380	-.263
				8	+.137*	+.095	8	0*	0	8	-.174	-.121	8	-.346	-.240
							9	+.012*	+.008	9	+.058*	+.040			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-1.380	-.957	1	-.071*	-.049	1	-1.546	-1.072
	2	-1.406	-.975	2	-1.314	-.911	2	-1.318	-.914
	3	-1.072	-.743	3	-1.144	-.793	3	-.652	-.452
	4	-0.608	-.421	4	-.806	-.559	4	-.518	-.359
	5	-.470	-.326	5	-.532	-.369	5	-.430	-.298
	6	-.390	-.270	6	-.432	-.299	6	-.444	-.308
	7	-.376	-.261	7	-.385	-.267	7	-.422	-.293
	8	-.376	-.261	8	-.414	-.287			
	9	-.426	-.295	9	-.446	-.309			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p	MISC. DE	ΔP	C_p
	1	-.352	-.244	1	-.360	-.250	1	-.368	-.255	1	-.368	-.255	1	-.468	-.324
	2	-.358	-.248	2	-.360	-.250	2	-.368	-.255	2	-.368	-.255	2	-.472	-.327
	3	-.360	-.250	3	-.366	-.254	3	-.368	-.255				3	-.465	-.322
	4	-.360	-.250	4	-.368	-.255									
	5	-.366	-.254												

BC 9 +.140* +.097

DATE 3-31-72 WIND DIRECTION: 130° Δh = 1.836 mm Hg P_A = 24.73 in. Hg WIND SPEED: 73.33 fps

TIME 11:50 Building I T = 60°F ρ_A = 0.001902 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.626	-.434	1	-1.102*	-.764	1	-1.264	-.876	1	-1.17	-.811
	2	-.548	-.380	2	-.952*	-.660	2	-1.248	-.865	2	-1.18	-.818
	3	-.421	-.292	3	-.778	-.539	3	-1.148	-.796	3	-1.14	-.790
	4	--	--	4	-.607	-.421	4	-1.013	-.702	4	-1.02	-.707
	5	-.262	-.182	5	-.490	-.340	5	-.835	-.579	5	-.817	-.562
	6	-.244	-.169	6	-.389	-.270	6	-.636	-.441	6	-.664	-.457
	7	-.253	-.175	7	-.390	-.270	7	-.636	-.441	7	-.662	-.455
	8	-.174	-.121	8	-.30*	-.208	8	-.616	-.427	8	-.672	-.462
	9	-.278	-.193	9	-.33	-.229	9	-.555	-.385	9	-.616	-.424
	10	-.316	-.219	10	-.358	-.248	10	-.47	-.326	10	-.530	-.365
	11	-.322	-.223	11	-.338	-.234	11	-.408	-.283	11	-.472	-.325
	12	-.326	-.226	12	-.294	-.204	12	-.404	-.280	12	-.458	-.315
	13	-.27	-.187	13	-.332	-.230	13	-.402	-.279	13	-.444	-.305
	14	-.336	-.233	14	-.358	-.248	14	-.438	-.304	14	-.452	-.311
	15	--	--	15	--	--	15	--	--	15	-.420	-.289

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	318	-.219	1	-.702	-.483	1	-.434	-.299	1	-.458	-.315
	2	318	-.219	2	-.350	-.241	2	-.444	-.305	2	-.462	-.318
	3	-.322	-.222	3	-.360	-.248	3	-.453	-.312	3	-.464	-.319
	4	-.316	-.217	4	-.358	-.246	4	-.464	-.320	4	-.468	-.322
	5	-.322	-.222	5	-.392	-.270	5	-.516	-.355	5	-.482	-.332
				6	-.416	-.286	6	-.515	-.354	6	-.484	-.333
				7	-.418	-.288	7	-.520	-.358	7	-.482	-.332
				8	-.448	-.308	8	-.520	-.358	8	-.476	-.327
				9	-.506	-.348	9	-.516	-.355	9	-.478	-.329
				10	-.916	-.630	10	-.524	-.360	10	-.480	-.330

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	+.204*	+.140	1	+.158*	+.109	1	+.408*	+.281	1	+.555	+.382	1	+.601*	+.413
	2	+.206*	+.142	2	+.210*	+.144	2	+.410*	+.282	2	+.566*	+.389			
	3	+.210*	+.144	3	+.178*	+.122	3	--	--	3	+.571*	+.393			
	4	+.192*	+.132	4	+.180*	+.124	4	+.413*	+.284	4	+.474*	+.326			
	5	+.160*	+.110	5	+.138*	+.095	5	+.400*	+.275	5	+.438*	+.301			
	6	+.114*	+.078	6	+.126*	+.087	6	+.390*	+.268	6	+.385*	+.265			
	7	+.056*	+.039	7	+.068*	+.047	7	+.302	+.208	7	+.300*	+.206			
	8	-.060*	-.042	8	+.036*	+.025	8	+.395	+.272	8	+.136*	+.094			
	9	-.170*	-.117	9	-.230*	-.158	9	-.114*	-.078	9	-.166*	-.114			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	+.352*	+.242	1	-.134*	-.092	1	-.204*	-.140	1	-.158*	-.109	1	-.346	-.238
	2	+.274*	+.189	2	+.368*	+.253	2	+.200*	+.138	2	+.282*	+.194	2	-.114*	-.078
	3	--	--	3	+.540*	+.372	3	+.418*	+.288	3	+.548*	+.377	3	+.039*	+.027
	4	+.105*	+.072	4	+.522*	+.359	4	+.454*	+.312	4	+.571*	+.393	4	+.064*	+.044
				5	+.434*	+.299	5	+.448*	+.308	5	+.556*	+.383	5	+.110*	+.076
				6	+.319*	+.219	6	+.373*	+.257	6	+.514*	+.354	6	+.139*	+.096
				7	+.270*	+.186	7	+.363*	+.250	7	+.480*	+.330	7	-.210*	-.145
				8	+.205*	+.141	8	+.334*	+.230	8	+.450*	+.310	8	+.410*	+.284
							9	+.275*	+.189	9	+.590*	+.406			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	+.414*	+.286	1	+.540*	+.374	1	+.346*	+.239
	2	--	--	2	+.568*	+.393	2	+.280*	+.194
	3	+.406	+.281	3	+.466*	+.322	3	+.1540	+.107
	4	+.378*	+.261	4	+.436*	+.302	4	+.083*	+.057
	5	+.362*	+.250	5	+.370*	+.256	5	-.148*	-.102
	6	+.310*	+.214	6	+.284*	+.196	6	+.340*	+.235
	7	+.952	+.659	7	+.124*	+.086	7	+.554*	+.383
	8	+.106*	+.073	8	-.152*	-.105			
	9	+.561*	+.388	9	+.600*	+.415			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p
	1	+.500*	+.346	1	-.195*	-.135	1	+.436*	+.302	1	+.302*	+.209
	2	+.426*	+.295	2	+.180*	+.125	2	+.400*	+.277	2	+.260*	+.180
	3	+.300*	+.208	3	+.432*	+.299	3	+.340*	+.235			
	4	+.255*	+.176	4	+.468*	+.324						
	5	+.200*	+.138									

MISC.

DE	ΔP	C_p
1	-.152*	-.105
2	+.253*	+.175
3	+.524*	+.362

BC 9 +.600* +.415

DATE 4-1-72 WIND DIRECTION: 140° Δh = 1.84 mm Hg P_A = 24.78 in. Hg WIND SPEED: 73.33 fps

TIME 1:00 p.m. Building I T = 60°F ρ_A = .00191 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.812*	-.562	1	-1.300	-.899	1	-1.080	-.747	1	-.976*	-.675
	2	-.714*	-.494	2	-1.338	-.926	2	-1.121	-.775	2	-1.008	-.697
	3	-.506*	-.350	3	-1.300	-.899	3	-1.156	-.800	3	-1.029	-.712
	4	--	--	4	-1.193	-.825	4	-1.140	-.789	4	-1.068	-.739
	5	-.288*	-.199	5	-1.006	-.696	5	-1.154	-.798	5	-1.078	-.746
	6	-.280*	-.194	6	-.752*	-.520	6	-.962*	-.665	6	-.926*	-.64
	7	-.270*	-.187	7	-.700*	-.484	7	-.998*	-.690	7	-1.000	-.69
	8	-.200*	-.138	8	-.660*	-.457	8	-1.024	-.708	8	-1.010	-.699
	9	-.326	-.225	9	-.502*	-.347	9	-.960*	-.664	9	-.954*	-.660
	10	-.368	-.255	10	-.434*	-.300	10	-.809*	-.560	10	-.848*	-.587
	11	-.388	-.268	11	-.378*	-.261	11	-.668*	-.462	11	-.736*	-.509
	12	-.409	-.283	12	-.340*	-.235	12	-.660*	-.457	12	-.663*	-.459
	13	-.356	-.246	13	-.389*	-.269	13	-.570*	-.394	13	-.620*	-.429
	14	-.448	-.310	14	-.470*	-.325	14	-.566	-.392	14	-.610*	-.422
	15	--	--	15	--	--	15	--	--	15	-.507*	-.394

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.462	-.320	1	-.370	-.256	1	-.564	-.390	1	-.620	-.429
	2	-.460	-.320	2	-.515	-.356	2	-.576	-.398	2	-.600	-.415
	3	-.459	-.317	3	-.520	-.360	3	-.562	-.389	3	-.616	-.426
	4	-.462	-.320	4	-.474	-.328	4	-.578	-.400	4	-.610	-.422
	5	-.462	-.320	5	-.540	-.373	5	-.611	-.423	5	-.621	-.430
				6	-.550	-.380	6	-.610	-.422	6	-.617	-.427
				7	-.350	-.242	7	-.614	-.425	7	-.614	-.425
				8	-.594	-.411	8	-.612	-.423	8	-.612	-.423
				9	-.645	-.446	9	-.610	-.422	9	-.600	-.415
				10	-1.074	-.743	10	-.610	-.422	10	-.604	-.418

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	+.136*	+.094	1	+.010*	+.007	1	+.570*	+.394	1	+1.017	+.703	1	+1.104	+.764
	2	+.152*	+.105	2	+.010*	+.007	2	+.612*	+.423	2	+1.000	+.692			
	3	+.167*	+.116	3	+.010*	+.007	3	--	--	3	+.918*	+.635			
	4	+.132*	+.091	4	+.024*	+.017	4	+.504	+.349	4	+.800*	+.553			
	5	+.088*	+.061	5	-.010*	-.007	5	+.440*	+.304	5	+.690*	+.477			
	6	+.030*	+.021	6	-.020*	-.014	6	+.322*	+.223	6	+.520*	+.360			
	7	-.044*	-.030	7	-.075*	-.052	7	+.206*	+.142	7	+.357*	+.247			
	8	-.162*	-.112	8	-.210*	-.145	8	+.484	+.335	8	+.062*	+.043			
	9	-.305*	-.211	9	-.430*	-.297	9	-.388	-.268	9	-.350*	-.242			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	+.358*	+.248	1	-.144*	-.100	1	-.278*	-.192	1	-.211*	-.146	1	-.437	-.302
	2	+.294*	+.203	2	+.430*	+.297	2	+.148*	+.102	2	+.316*	+.219	2	-.074*	-.051
	3	--	--	3	+.658*	+.455	3	+.440*	+.304	3	+.708	+.490	3	+.243*	+.168
	4	+.060*	+.042	4	+.576*	+.398	4	+.490*	+.339	4	+.816*	+.564	4	+.329*	+.228
				5	+.486*	+.336	5	+.552*	+.382	5	+.800*	+.553	5	+.368*	+.255
				6	+.374*	+.359	6	+.500*	+.346	6	+.762*	+.527	6	+.358*	+.248
				7	+.237*	+.164	7	+.430*	+.297	7	+.724*	+.501	7	+.396*	+.277
				8	+.148*	+.102	8	+.340*	+.235	8	+.695*	+.481	8	+.385*	+.269
							9	+.230*	+.159	9	+.648*	+.448			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-1.218	-.852	1	-.60*	-.420	1	-1.50*	-1.05
	2	-1.180	-.825	2	-1.36	-.951	2	-1.575*	-1.10
	3	-1.232	-.862	2	-1.38	-.965	3	-1.27*	-.888
	4	-1.120	-.783	4	-1.30	-.909	4	-1.074	-.751
	5	-1.048	-.733	5	-1.09	-.762	5	-.976	-.683
	6	-.936*	-.655	6	-.918*	-.642	6	-.977	-.683
	7	-.738*	-.516	7	-.756*	-.529	7	-.977	-.683
	8	-.608*	-.425	8	-.706	-.494			
	9	-.608	-.425	9	-.708	-.495			

MISC.

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p	DE	ΔP	C_p
	1	-.438	-.306	1	-.443	-.310	1	-.472	-.330	1	-.466	-.326	1	-.684	-.478
	2	-.448	-.313	2	-.460	-.322	2	-.472	-.330	2	-.465	-.325	2	-.684	-.478
	3	-.452	-.316	3	-.476	-.333	3	-.470	-.329				3	-.688	-.481
	4	-.452	-.316	4	-.476	-.333									
	5	-.462	-.323												

BC 9 +.062 +.043

DATE 4-2-72 WIND DIRECTION: 150° Δh = 1.82 mm Hg P_A = 24.52 in. Hg WIND SPEED: 73.33 fps

TIME 11:00 a.m. Building I T = 60°F ρ_A = 0.001885 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.759*	-.531	1	-1.151*	-.805	1	-.977*	-.683	1	-.860*	-.601
	2	-.721*	-.504	2	-1.144*	-.800	2	-1.000*	-.699	2	-.864*	-.604
	3	-.569*	-.398	3	-1.155*	-.808	3	-1.023*	-.715	3	-.873*	-.611
	4	--	--	4	-1.118*	-.782	4	-1.023*	-.715	4	-.882*	-.617
	5	-.394	-.276	5	-1.093*	-.764	5	-1.044*	-.730	5	-.884*	-.618
	6	-.377	-.264	6	-.914*	-.639	6	-.950*	-.664	6	-.884*	-.618
	7	-.352	-.246	7	-.894*	-.625	7	-.962*	-.673	7	-.929*	-.650
	8	-.258*	-.180	8	-.840*	-.587	8	-.980*	-.685	8	-.948*	-.663
	9	-.374	-.262	9	-.737*	-.515	9	-.964*	-.674	9	-.919*	-.643
	10	-.434*	-.304	10	-.629*	-.440	10	-.917*	-.641	10	-.857*	-.599
	11	-.448*	-.313	11	-.502*	-.351	11	-.856*	-.599	11	-.800*	-.559
	12	-.467	-.327	12	-.465	-.325	12	-.790*	-.552	12	-.736	-.515
	13	-.475	-.332	13	-.500*	-.350	13	-.766	-.536	13	-.709	-.496
	14	-.522	-.365	14	-.553*	-.387	14	-.737	-.515	14	-.700	-.490
	15	--	--	15	--	--	15	--	--	15	-.653*	-.457

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.571*	-.399	1	-.474*	-.331	1	-.657	-.459	1	-.650	-.455
	2	-.582	-.407	2	-.640	-.448	2	-.657	-.459	2	-.628	-.439
	3	-.582	-.407	3	-.640	-.448	3	-.639	-.447	3	-.653	-.457
	4	-.594*	-.415	4	-.640	-.448	4	-.658	-.460	4	-.630	-.441
	5	-.600*	-.420	5	-.667*	-.466	5	-.646	-.452	5	-.630	-.441
				6	-.674*	-.471	6	-.666	-.466	6	-.632	-.442
				7	-.530	-.371	7	-.660*	-.462	7	-.640	-.448
				8	-.687*	-.480	8	-.660	-.462	8	-.635	-.444
				9	-.723*	-.506	9	-.663	-.464	9	-.635	-.444
				10	-.911*	-.637	10	-.650	-.455	10	-.635	-.444

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	+.007	+.003	1	-.220*	-.154	1	+.244*	+.171	1	+.920*	+.643	1	+.957*	+.669
	2	+.004	+.003	2	-.180*	-.126	2	+.258*	+.180	2	+.908*	+.635			
	3	+.024	+.017	3	-.200	-.140	3	--	--	3	+.873*	+.611			
	4	+.026	+.018	4	-.188	-.131	4	+.302*	+.211	4	+.745*	+.521			
	5	-.004	-.003	5	-.217	-.152	5	+.248*	+.173	5	+.678*	+.474			
	6	-.066	-.046	6	-.217	-.152	6	+.177*	+.124	6	+.540*	+.378			
	7	-.123	-.086	7	-.258	-.180	7	+.090*	+.063	7	+.360*	+.252			
	8	-.245	-.171	8	-.366	-.256	8	+.242*	+.169	8	+.110	+.077			
	9	-.345	-.241	9	-.521	-.264	9	-.421	-.294	9	-.324	-.277			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	+.195*	+.136	1	-.151*	-.106	1	-.370	-.259	1	-.263	-.184	1	-.369	-.258
	2	+.150	+.105	2	+.360*	+.252	2	+.018*	+.013	2	+.269	+.188	2	.000*	0
	3	--	--	3	+.552*	+.386	3	+.278*	+.194	3	+.630	+.441	3	+.362	+.253
	4	-.100	-.070	4	+.462*	+.323	4	+.300*	+.210	4	+.730*	+.510	4	+.437	+.306
				5	+.310*	+.217	5	+.288*	+.201	5	+.730*	+.510	5	+.486	+.340
				6	+.185*	+.129	6	+.234*	+.164	6	+.707*	+.494	6	+.537	+.376
				7	+.087*	+.061	7	+.175*	+.122	7	+.707*	+.494	7	+.615*	+.430
				8	+.005*	+.003	8	+.115*	+.080	8	+.674*	+.471	8	+.649*	+.454
							9	.000*	0	9	+.637*	+.445			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.950*	-.664	1	-.741*	-.518	1	-1.200*	-.839
	2	-.936*	-.655	2	-.973*	-.680	2	-1.242*	-.869
	3	-.992*	-.694	3	-1.062*	-.743	3	-1.014*	-.709
	4	-.978*	-.684	4	-1.092*	-.764	4	-.979*	-.685
	5	-.964*	-.674	5	-1.020*	-.713	5	-.929*	-.650
	6	-.908*	-.635	6	-.930*	-.650	6	-.943*	-.659
	7	-.792*	-.554	7	-.845*	-.591	7	-.962*	-.673
	8	-.757*	-.529	8	-.858*	-.600			
	9	-.757*	-.529	9	-.862*	-.603			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p
	1	-.542	-.379	1	-.590*	-.413	1	-.610*	-.427	1	.616	-.431
	2	-.572	-.400	2	-.609	-.426	2	-.641*	-.448	2	-.621	-.434
	3	-.580	-.406	3	-.643*	-.450	3	-.641*	-.448			
	4	-.597	-.417	4	-.638*	-.446						
	5	-.597	-.417									

MISC.

DE	ΔP	C_p
1	-.648	-.453
2	-.648	-.453
3	-.648	-.453

BC 9 -.100 -.070

DATE 4-2-72 WIND DIRECTION: 160° Δh = 1.82 mm Hg P_A = 24.50 in. Hg WIND SPEED: 73.33 fps

TIME 5:50 Building I T = 60°F ρ_A = .001885 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.815	-.570	1	-.930	-.650	1	-.880	-.615	1	-.722	-.505
	2	-.762	-.533	2	-.930	-.650	2	-.880	-.615	2	-.741	-.518
	3	-.633	-.443	3	-.942	-.659	3	-.897	-.627	3	-.756	-.529
	4	--	--	4	-.942	-.659	4	-.885	-.619	4	-.752	-.526
	5	-.526	-.368	5	-.952	-.666	5	-.885	-.619	5	-.770	-.538
	6	-.518	-.362	6	-.876	-.613	6	-.856	-.599	6	-.764	-.534
	7	-.455	-.318	7	-.886	-.620	7	-.853	-.597	7	-.776	-.543
	8	-.358	-.250	8	-.877	-.613	8	-.846	-.592	8	-.818	-.572
	9	-.495	-.346	9	-.842	-.589	9	-.890	-.622	9	-.828	-.579
	10	-.558	-.390	10	-.751	-.525	10	-.880	-.615	10	-.820	-.573
	11	-.565	-.395	11	-.658	-.460	11	-.872	-.610	11	-.795	-.556
	12	-.573	-.401	12	-.605	-.423	12	-.836	-.585	12	-.772	-.540
	13	-.578	-.404	13	-.624	-.436	13	-.806	-.564	13	-.764	-.534
	14	-.614	-.429	14	-.670	-.469	14	-.791	-.553	14	-.756	-.529
	15	--	--	15	--	--	15	--	--	15	-.742	-.519

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.718	-.502	1	-.782	-.547	1	-.730	-.510	1	-.689	-.482
	2	-.700	-.490	2	-.738	-.516	2	-.725	-.507	2	-.667	-.466
	3	-.700	-.490	3	-.738	-.516	3	-.716	-.501	3	-.682	-.477
	4	-.715	-.500	4	-.714	-.499	4	-.716	-.501	4	-.690	-.483
	5	-.717	-.501	5	-.738	-.516	5	-.705	-.493	5	-.668	-.467
				6	-.744	-.520	6	-.707	-.494	6	-.662	-.463
				7	-.786	-.550	7	-.706	-.494	7	-.662	-.463
				8	-.756	-.529	8	-.706	-.494	8	-.662	-.463
				9	-.756	-.529	9	-.706	-.494	9	-.662	-.463
				10	-.776	-.543	10	-.704	-.492	10	-.662	-.463

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.272*	-.190	1	-.585	-.409	1	-.344*	-.241	1	+.496*	+.347	1	+.632	+.442
	2	-.277	-.194	2	-.491	-.343	2	-.290*	-.203	2	+.558*	+.390			
	3	-.262	-.183	3	-.434	-.304	3	--	--	3	+.558*	+.390			
	4	-.246	-.172	4	-.400	-.280	4	-.246*	-.172	4	+.427	+.167			
	5	-.250	-.175	5	-.422	-.295	5	-.246	-.172	5	+.370	+.259			
	6	-.250	-.175	6	-.410	-.287	6	-.292	-.204	6	+.332	+.232			
	7	-.292	-.204	7	-.442	-.309	7	-.315	-.220	7	+.152	+.106			
	8	-.372	-.260	8	-.522	-.365	8	+.011	+.008	8	-.100	-.070			
	9	-.442	-.309	9	-.626	-.438	9	-.614	-.429	9	-.362	-.253			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	-.022	-.015	1	-.145	-.101	1	-.451	-.315	1	-.300	-.210	1	-.272	-.191
	2	-.096	-.067	2	+.350	+.245	2	-.074	-.052	2	+.238*	+.166	2	+.128*	+.090
	3	--	--	3	+.519	+.363	3	+.150	+.105	3	+.578*	+.404	3	+.527*	+.369
	4	-.373	-.261	4	+.380*	+.266	4	+.209	+.146	4	+.677*	+.473	4	+.600*	+.420
				5	+.180	+.126	5	+.209	+.146	5	+.736*	+.515	5	+.718*	+.502
				6	+.020	+.014	6	+.158*	+.110	6	+.748*	+.523	6	+.748*	+.523
				7	-.100*	-.070	7	+.112*	+.078	7	+.748*	+.523	7	+.856*	+.599
				8	-.183	-.138	8	+.112	+.078	8	+.765*	+.535	8	+.958*	+.670
							9	+.020	+.014	9	+.838*	+.586			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.652	-.456	1	-1.140	-.797	1	-.681	-.476
	2	-.619	-.433	2	-.652	-.456	2	-.672	-.470
	3	-.690	-.483	3	-.652	-.456	3	-.660	-.462
	4	-.704	-.492	4	-.674	-.471	4	-.660	-.462
	5	-.726	-.508	5	-.674	-.471	5	-.668	-.467
	6	-.746	-.522	6	-.690	-.483	6	-.690	-.483
	7	-.746	-.522	7	-.708	-.495	7	-.714	-.499
	8	-.746	-.522	8	-.716	-.501			
	9	-.758	-.530	9	-.722	-.505			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p
	1	-.636	-.445	1	-.682	-.477	1	-.736	-.515	1	-.736	-.515
	2	-.662	-.463	2	-.734	-.513	2	-.736	-.515	2	-.774	-.541
	3	-.676	-.473	3	-.734	-.513	3	-.736	-.515			
	4	-.676	-.473	4	-.712	-.498						
	5	-.654	-.457									

MISC

DE	ΔP	C_p
1	-.654	-.457
2	-.642	-.449
3	-.642	-.449

BC	ΔP	C_p
9	-.330	-.231

DATE 4-3-72 WIND DIRECTION: 170° Δh = 1.851 P_A = 24.9 in. Hg WIND SPEED: 73.33 fps

TIME 9:00 a.m. Building I T = 60°F ρ_A = .00196 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.808	-.556	1	-.884*	-.608	1	-.878*	-.604	1	-.694*	-.477
	2	-.804	-.553	2	-.907*	-.624	2	-.883*	-.607	2	-.716*	-.492
	3	-.750	-.516	3	-.886*	-.609	3	-.901*	-.620	3	-.730*	-.502
	4	--	--	4	-.924*	-.635	4	-.895*	-.615	4	-.747*	-.514
	5	-.602	-.414	5	-.943*	-.648	5	-.925*	-.636	5	-.714*	-.491
	6	-.563	-.387	6	-.867*	-.596	6	-.874*	-.601	6	-.715*	-.492
	7	-.524	-.360	7	-.862	-.593	7	-.872*	-.600	7	-.768*	-.528
	8	-.447*	-.307	8	-.879*	-.604	8	-.835*	-.574	8	-.794*	-.546
	9	-.429*	-.364	9	-.844*	-.580	9	-.903*	-.621	9	-.786*	-.540
	10	-.562*	-.386	10	-.742*	-.510	10	-.894*	-.615	10	-.759*	-.522
	11	-.566	-.389	11	-.661*	-.455	11	-.862*	-.593	11	-.751*	-.516
	12	-.561*	-.586	12	-.627*	-.431	12	-.817*	-.562	12	-.738	-.507
	13	-.535*	-.368	13	-.627*	-.431	13	-.777*	-.534	13	-.736	-.506
	14	-.613*	-.421	14	-.663*	-.456	14	-.743*	-.511	14	-.712	-.490
	15	--	--	15	--	--	15	--	--	15	-.678	-.466

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.752	-.517	1	-.579	-.398	1	-.768	-.528	1	-.734	-.505
	2	-.752	-.517	2	-.772	-.531	2	-.764	-.525	2	-.714	-.491
	3	-.752	-.517	3	-.768	-.528	3	-.746	-.513	3	-.714	-.491
	4	-.742	-.510	4	-.768	-.528	4	-.746	-.513	4	-.714	-.491
	5	-.758	-.512	5	-.780	-.536	5	-.742	-.510	5	-.706	-.485
				6	-.780	-.536	6	-.738	-.507	6	-.692	-.476
				7	-.878	-.604	7	-.738	-.507	7	-.668	-.459
				8	-.787	-.541	8	-.734	-.505	8	-.676	-.465
				9	-.782	-.528	9	-.734	-.505	9	-.672	-.462
				10	-.800	-.550	10	-.734	-.505	10	-.672	-.462

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.408	-.281	1	-.591	-.406	1	-.440*	-.303	1	+.210*	+.144	1	+.204*	+.140
	2	-.408*	-.281	2	-.474	-.326	2	-.295	-.203	2	+.304*	+.209			
	3	-.388	-.267	3	-.456	-.314	3	--	--	3	+.304*	+.209			
	4	-.364	-.250	4	-.456	-.314	4	-.234	-.161	4	+.254*	+.175			
	5	-.356	-.245	5	-.456	-.314	5	-.272	-.187	5	+.197*	+.135			
	6	-.368	-.253	6	-.456	-.314	6	-.332	-.228	6	+.092*	+.063			
	7	-.415	-.285	7	-.482	-.331	7	-.391	-.269	7	-.048*	-.033			
	8	-.476	-.327	8	-.534	-.367	8	-.200	-.138	8	-.190*	-.131			
	9	-.551	-.379	9	-.636	-.437	9	-.712	-.490	9	-.464*	-.319			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	-.070	-.048	1	-.174	-.120	1	-.466	-.320	1	-.300	-.206	1	-.284	-.195
	2	-.144	-.099	2	+.368*	+.253	2	-.066	-.045	2	+.247	+.170	2	+.112	+.077
	3	--	--	3	+.488*	+.336	3	+.194*	+.133	3	+.607*	+.417	3	+.613*	+.421
	4	-.448	-.308	4	+.362*	+.249	4	+.238*	+.164	4	+.730*	+.502	4	+.718*	+.494
				5	+.162	+.111	5	+.248	+.171	5	+.776*	+.534	5	+.875*	+.602
				6	-.048	-.033	6	+.246*	+.169	6	+.827*	+.569	6	+.962	+.661
				7	-.132	-.091	7	+.256*	+.176	7	+.864*	+.594	7	+1.100*	+.756
				8	-.176	-.121	8	+.272*	+.187	8	+.963*	+.662	8	+1.200*	+.825
							9	+.232*	+.160	9	+1.060*	+.729			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.640	-.440	1	-.438	-.301	1	-.624	-.429
	2	-.620	-.426	2	-.606	-.417	2	-.640	-.440
	3	-.672	-.462	3	-.652	-.448	3	-.644	-.443
	4	-.672	-.462	4	-.654	-.450	4	-.648	-.446
	5	-.710	-.488	5	-.662	-.455	5	-.666	-.458
	6	-.712	-.490	6	-.670	-.461	6	-.674	-.463
	7	-.724	-.498	7	-.670	-.461	7	-.674	-.463
	8	-.724	-.498	8	-.690	-.474			
	9	-.754	-.518	9	-.690	-.474			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p
	1	-.674	-.463	1	-.718	-.494	1	-.793	-.545	1	-.788	-.542
	2	-.722	-.496	2	-.754	-.518	2	-.793	-.545	2	-.788	-.542
	3	-.728	-.501	3	-.744	-.512	3	-.793	-.545			
	4	-.728	-.501	4	-.744*	-.512						
	5	-.718	-.494									

MISC.

DE	ΔP	C_p
1	-.656	-.451
2	-.664	-.457
3	-.664	-.457

BC	9	-.264	-.182

DATE 4-3-72 WIND DIRECTION: 180° Δh = 1.844 mm Hg P_A = 24.81 in. Hg WIND SPEED: 73.33 fps

TIME 3:00 p.m. Building I T = 60°F ρ_A = .00196 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.914	-.631	1	-.910	-.628	1	-.846	-.584	1	-.706	-.487
	2	-.950	-.656	2	-.900	-.621	2	-.860	-.596	2	-.724	-.499
	3	-.954	-.658	3	-.900	-.621	3	-.864	-.584	3	-.726	-.501
	4	--	--	4	-.896	-.618	4	-.871	-.601	4	-.750	-.518
	5	-.796	-.549	5	-.930	-.642	5	-.890	-.614	5	-.736	-.508
	6	-.628	-.433	6	-.850	-.587	6	-.854	-.589	6	-.730	-.504
	7	-.624	-.431	7	-.860	-.594	7	-.864	-.596	7	-.760	-.524
	8	-.572	-.395	8	-.914	-.631	8	-.850	-.587	8	-.780	-.538
	9	-.495	-.342	9	-.840	-.58	9	-.875	-.604	9	-.790	-.545
	10	-.486	-.335	10	-.700	-.483	10	-.865	-.597	10	-.788	-.544
	11	-.480	-.331	11	-.626	-.432	11	-.819	-.565	11	-.766	-.529
	12	-.500	-.345	12	-.600	-.414	12	-.770	-.531	12	-.753	-.520
	13	-.470	-.324	13	-.624	-.431	13	-.740	-.511	13	-.735	-.507
	14	-.554	-.384	14	-.659	-.455	14	-.720	-.497	14	-.740	-.511
	15	--	--	15	--	--	15	--	--	15	-.712	-.491

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.780	-.538	1	-.544	-.375	1	-.814	-.562	1	-.800	-.552
	2	-.750	-.518	2	-.846	-.584	2	-.805	-.556	2	-.784	-.541
	3	-.770	-.513	3	-.832	-.574	3	-.804	-.555	3	-.772	-.533
	4	-.793	-.547	4	-.805	-.556	4	-.791	-.546	4	-.763	-.527
	5	-.800	-.552	5	-.850	-.587	5	-.790	-.545	5	-.762	-.526
				6	-.871	-.601	6	-.784	-.541	6	-.760	-.524
				7	-.730	-.504	7	-.786	-.542	7	-.760	-.524
				8	-.850	-.587	8	-.786	-.542	8	-.750	-.524
				9	-.864	-.596	9	-.785	-.541	9	-.744	-.513
				10	-.886	-.611	10	-.790	-.545	10	-.754	-.52

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.518	-.357	1	-.430	-.300	1	-.180	-.124	1	-.010	-.007	1	-.496*	-.342
	2	-.506	-.349	2	-.377	-.260	2	-.144	-.099	2	+.110	+.076			
	3	-.464	-.320	3	-.400	-.276	3	--	--	3	+.100	+.690			
	4	-.436	-.301	4	-.420	-.290	4	-.254	-.175	4	-.018	-.012			
	5	-.434	-.299	5	-.439	-.303	5	-.297	-.205	5	-.053	-.037			
	6	-.444	-.306	6	-.452	-.312	6	-.272	-.188	6	-.149	-.103			
	7	-.481	-.332	7	-.500	-.345	7	-.436	-.301	7	-.248	-.171			
	8	-.550	-.38	8	-.585	-.404	8	0	0	8	-.366	-.253			
	9	-.650	-.449	9	-.697	-.481	9	-.742	-.512	9	-.596	-.411			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	-.298	-.206	1	-.172*	-.119	1	-.485	-.335	1	-.326	-.225	1	-.365	-.252
	2	-.338	-.233	2	+.256*	+.177	2	-.076	-.052	2	+.210*	+.145	2	0	0
	3	--	--	3	+.272*	+.188	3	+.132	+.091	3	+.586*	+.404	3	+.494	+.341
	4	-.447	-.308	4	+.074*	+.051	4	+.132	+.091	4	+.586*	+.404	4	+.672*	+.464
				5	-.162	-.112	5	+.132	+.091	5	+.586*	+.404	5	+.887*	+.612
				6	-.330	-.228	6	0	0	6	+.586*	+.404	6	+1.059*	+.731
				7	-.381	-.263	7	0	0	7	+.692*	+.478	7	+1.187	+.819
				8	-.357	-.246	8	+.200*	+.138	8	+.871*	+.601	8	+1.218	+.841
							9	+.362*	+.25	9	+1.028*	+.71			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.682	-.470	1	-.723	-.499	1	-.777	-.536
	2	-.648	-.447	2	-.622	-.429	2	-.685	-.473
	3	-.713	-.492	3	-.700	-.483	3	-.685	-.473
	4	-.730	-.504	4	-.695	-.48	4	-.685	-.473
	5	-.730	-.504	5	-.695	-.48	5	-.685	-.473
	6	-.745	-.514	6	-.708	-.488	6	-.685	-.473
	7	-.745	-.514	7	-.708	-.488	7	-.700	-.483
	8	-.772	-.533	8	-.732	-.505			
	9	-.758	-.523	9	-.732	-.505			

MISC.

	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p	DE	ΔP	C_p
	1	-.666	-.46	1	-.733	-.506	1	-.820	-.566	1	-.832	-.574	1	-.724	-.45
	2	-.690	-.476	2	-.764	-.527	2	-.820	-.566	2	-.832	-.574	2	-.724	-.45
	3	-.690	-.476	3	-.774	-.534	3	-.790	-.545				3	-.705	-.487
	4	-.697	-.481	4	-.760	-.525									
	5	-.683	-.471												

BC 9 -.332 -.229

DATE 4-3-72 WIND DIRECTION 340° Δh = 1.842 mm Hg P_A = 24.78 in. Hg WIND SPEED: 73.33 fps

TIME 9:00 p.m. Building I T = 60°F ρ_A = 0.00191 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.800	-.553	1	-.817	-.565	1	-.993	-.686	1	-.878	-.607
	2	-.473	-.327	2	-.493	-.341	2	-.460	-.318	2	-.424	-.293
	3	-.380	-.263	3	-.416	-.287	3	-.345	-.238	3	-.239	-.165
	4	--	--	4	-.342	-.236	4	-.263	-.182	4	-.156	-.108
	5	-.333	-.230	5	-.272	-.188	5	-.174	-.120	5	-.026	-.018
	6	-.166	-.115	6	-.144	-.099	6	-.068	-.047	6	+.140	+.097
	7	-.166	-.115	7	-.204	-.141	7	-.144	-.099	7	-.150	-.104
	8	-.160	-.111	8	-.164	-.113	8	-.086	-.059	8	+.052	+.036
	9	-.177	-.122	9	-.164	-.113	9	-.036	-.025	9	+.072	+.050
	10	-.085	-.059	10	-.083	-.057	10	+.110	+.076	10	+.174	+.120
	11	-.018	-.012	11	-.009	-.006	11	+.076	+.053	11	+.273	+.189
	12	+.071	+.049	12	+.074*	+.051	12	+.130*	+.090	12	+.344*	+.238
	13	+.071	+.049	13	+.028*	+.019	13	+.130*	+.090	13	+.400*	+.276
	14	+.013	+.009	14	+.014*	+.010	14	+.130*	+.090	14	+.409*	+.283
	15	--	--	15	--	--	15	--	--	15	+.336*	+.228

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	+.300*	+.207	1	+.886	+.612	1	+.590*	+.408	1	+.728*	+.503
	2	+.390*	+.269	2	+.419*	+.290	2	+.657*	+.454	2	+.749*	+.518
	3	+.420	+.290	3	+.428*	+.296	3	+.625*	+.432	3	+.753*	+.520
	4	+.464*	+.321	4	+.515*	+.356	4	+.663*	+.458	4	+.792*	+.547
	5	+.536*	+.370	5	+.544*	+.376	5	+.685*	+.473	5	+.859*	+.594
				6	+.633*	+.437	6	+.723*	+.500	6	+.894*	+.618
				7	+.730	+.504	7	+.737*	+.509	7	+.865*	+.598
				8	+.762*	+.527	8	+.700*	+.484	8	+.854*	+.590
				9	+.773*	+.534	9	+.630*	+.435	9	+.755*	+.522
				10	+.432*	+.298	10	+.140*	+.097	10	+.187*	+.129

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.835*	-.577	1	-.664	-.459	1	-.929	-.642	1	-.831	-.574	1	-.893	-.617
	2	-.894*	-.618	2	-.666*	-.460	2	-.910	-.629	2	-.833	-.576			
	3	-.902*	-.623	3	-.826	-.571	3	--	--	3	-.779	-.538			
	4	-.934	-.645	4	-.926	-.640	4	-.864	-.597	4	-.827	-.571			
	5	-.953	-.658	5	-.956	-.661	5	-.839	-.580	5	-.826	-.571			
	6	-.941	-.650	6	-.923	-.638	6	-.827	-.571	6	-.822	-.568			
	7	-.944	-.652	7	-.884	-.611	7	-.800	-.553	7	-.820	-.567			
	8	-.921	-.636	8	-.850	-.587	8	-.514	-.355	8	-.811	-.560			
	9	-.907	-.627	9	-.839*	-.580	9	-.780	-.539	9	-.806	-.557			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	-.694	-.480	1	-1.004*	-.694	1	-1.058*	-.731	1	-.979	-.676	1	-.898	-.620
	2	-.722	-.499	2	-.996*	-.688	2	-.907*	-.627	2	-.882	-.609	2	-.815	-.563
	3	--	--	3	-.859	-.594	3	-.929*	-.642	3	-.825	-.570	3	-.832	-.575
	4	-.812	-.561	4	-.750*	-.518	4	-.942*	-.651	4	-.857	-.592	4	-.880	-.608
				5	-.726*	-.502	5	-.953*	-.658	5	-.863	-.596	5	-.857	-.592
				6	-.746	-.515	6	-.948*	-.655	6	-.863	-.596	6	-.863	-.596
				7	-.763*	-.527	7	-.972*	-.672	7	-.919	-.635	7	-.866	-.598
				8	-.763*	-.527	8	-.900	-.622	8	-.885	-.612	8	-.820	-.567
							9	-1.018*	-.703	9	-1.050	-.726			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.608	-.420	1	0*	0	1	-.700	-.484
	2	-.370*	-.256	2	-.372	-.257	2	-.498*	-.344
	3	-.234*	-.162	3	-.317	-.219	3	-.377*	-.260
	4	-.069*	-.048	4	-.210*	-.145	4	-.262*	-.181
	5	-.014*	-.010	5	-.130*	-.090	5	-.246*	-.170
	6	+.024*	+.017	6	-.065*	-.045	6	-.719*	-.497
	7	+.150*	+.104	7	+.007*	+.005	7	-1.209*	-.835
	8	+.192*	+.133	8	-.171*	-.118			
	9	0*	0	9	-.647*	-.447			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p
	1	+.447*	+.309	1	+.521*	+.360	1	+.665*	+.459	1	+.764*	+.528
	2	+.483*	+.334	2	+.539*	+.372	2	+.681*	+.471	2	+.834*	+.576
	3	+.525*	+.363	3	+.568*	+.392	3	+.780*	+.539			
	4	+.534*	+.369	4	+.592*	+.409						
	5	+.500*	+.345									

MISC.

DE	ΔP	C_p
1	+.813*	+.562
2	+.703*	+.486
3	+.631*	+.436
BC 9	-.793	-.548

DATE 4-4-72 WIND DIRECTION: 350° Δh = 1.842 mm Hg P_A = 24.781 in. Hg WIND SPEED: 73.33 fps

TIME 2:00 p.m. Building I T = 60°F ρ_A = 0.00191 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.822*	-.568	1	-.850	-.587	1	-1.047*	-.723	1	-.858	-.593
	2	-.450*	-.311	2	-.466	-.322	2	-.392	-.271	2	-.314	-.217
	3	-.346*	-.239	3	-.390	-.269	3	-.258*	-.178	3	-.082*	-.057
	4	--	--	4	-.296	-.274	4	-.158*	-.109	4	.000*	0
	5	-.286	-.198	5	-.212	-.146	5	-.058*	-.040	5	+.201*	+.139
	6	-.081	-.056	6	-.069	-.048	6	+.112*	+.077	6	+.371*	+.256
	7	-.073	-.050	7	-.150	-.104	7	-.034*	-.024	7	+.036*	+.025
	8	-.063	-.044	8	-.100	-.069	8	+.054*	+.037	8	+.241*	+.167
	9	-.077	-.053	9	-.077*	-.053	9	+.097*	+.067	9	+.300*	+.207
	10	-.006	-.004	10	-.001*	-.001	10	+.277*	+.191	10	+.407*	+.281
	11	+.078*	+.054	11	+.104*	+.072	11	+.292*	+.202	11	+.507*	+.350
	12	+.136	+.094	12	+.210*	+.145	12	+.385*	+.266	12	+.600*	+.415
	13	+.130	+.090	13	+.215*	+.149	13	+.465*	+.321	13	+.715*	+.494
	14	+.135	+.093	14	+.215*	+.149	14	+.502*	+.347	14	+.808*	+.558
	15	--	--	15	--	--	15	--	--	15	+.808*	+.558

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	+.293*	+.202	1	+.500*	+.345	1	+.418*	+.289	1	+.454*	+.314
	2	+.324*	+.224	2	+.402*	+.278	1	+.528*	+.365	2	+.582*	+.402
	3	+.360*	+.249	3	+.428*	+.296	3	+.555*	+.383	3	+.651*	+.388
	4	+.410*	+.283	4	+.458*	+.316	4	+.576*	+.398	4	+.733*	+.506
	5	+.465*	+.321	5	+.503*	+.348	5	+.610*	+.421	5	+.774*	+.535
				6	+.595*	+.411	6	+.636*	+.439	6	+.850*	+.587
				7	+.595	+.411	7	+.674*	+.466	7	+.867*	+.599
				8	+.700*	+.484	8	+.674*	+.466	8	+.867*	+.599
				9	+.714*	+.493	9	+.600*	+.415	9	+.764*	+.528
				10	+.396*	+.274	10	+.120*	+.083	10	+.199*	+.138

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.806*	-.557	1	-.618*	-.427	1	-.944*	-.652	1	-.865	-.598	1	-.828*	-.572
	2	-.857*	-.592	2	-.553*	-.382	2	-.926*	-.640	2	-.876*	-.605			
	3	-.908*	-.627	3	-.780*	-.539	3	--	--	3	-.765*	-.529			
	4	-.945*	-.653	4	-.892*	-.616	4	-.869*	-.600	4	-.854	-.590			
	5	-.951	-.657	5	-.963*	-.665	5	-.858*	-.593	5	-.854	-.590			
	6	-.969	-.670	6	-.963	-.665	6	-.852	-.589	6	-.839	-.580			
	7	-.964*	-.666	7	-.917*	-.634	7	-.839	-.580	7	-.837	-.578			
	8	-.933*	-.645	8	-.864*	-.597	8	-.600	-.415	8	-.826	-.571			
	9	-.923*	-.638	9	-.856*	-.591	9	-.812	-.561	9	-.828	-.572			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	-.700*	-.484	1	-1.000*	-.691	1	-1.079	-.746	1	-.991	-.685	1	-1.063*	-.734
	2	-.700*	-.484	2	-1.007*	-.696	2	-.954	-.659	2	-.889*	-.614	2	-.905*	-.625
	3	--	--	3	-.890*	-.615	3	-.948	-.655	3	-.848	-.586	3	-.838	-.579
	4	-.814*	-.562	4	-.828*	-.572	4	-.952	-.658	4	-.874	-.604	4	-.858	-.593
				5	-.755*	-.522	5	-.959	-.663	5	-.881	-.609	5	-.894	-.618
				6	-.767	-.530	6	-.960	-.663	6	-.882	-.609	6	-.866*	-.598
				7	-.787	-.544	7	-.970	-.670	7	-.940	-.650	7	-.885*	-.612
				8	-.787	-.544	8	-.916	-.633	8	-.913	-.631	8	-.853*	-.589
							9	-1.034	-.714	9	-.744	-.514			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.528*	-.365	1	+.05*	+.035	1	-.644	-.445
	2	-.278*	-.192	2	-.270*	-.187	2	-.428	-.296
	3	-.096	-.066	3	-.211*	-.146	3	-.306	-.211
	4	+.085	+.059	4	-.076*	-.053	4	-.286*	-.198
	5	+.159*	+.110	5	+.011*	+.008	5	-.134*	-.093
	6	+.217*	+.150	6	+.083*	+.057	6	-.124*	-.086
	7	+.362*	+.250	7	+.182*	+.126	7	-.544*	-.376
	8	+.470*	+.325	8	+.300*	+.207			
	9	+.520*	+.360	9	+.226	+.156			

MISC.

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p	DE	ΔP	C_p
	1	+.383*	+.265	1	+.446*	+.308	1	+.562*	+.388	1	+.695*	+.480	1	+.804*	+.556
	2	+.438*	+.303	2	+.445*	+.307	2	+.619*	+.428	2	+.830	+.573	2	+.792*	+.547
	3	+.456*	+.315	3	+.500*	+.345	3	+.700*	+.484				3	+.668*	+.462
	4	+.430*	+.297	4	+.555*	+.383									
	5	+.447*	+.309												

BC 9 -.817* -.565

DATE 4-4-72 WIND DIRECTION: 0° Δh = 1.842 mm Hg P_A = 24.78 in. Hg WIND SPEED: 73.33 fps

TIME 8:30 p.m. Building I T = 60°F ρ_A = .00191 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.764	-.528	1	-.830*	-.573	1	-1.050	-.726	1	-.770*	-.532
	2	-.325	-.225	2	-.368*	-.254	2	-.266*	-.184	2	-.143*	-.099
	3	-.194*	-.134	3	-.270*	-.187	3	-.090*	-.062	3	+.100*	+.069
	4	--	--	4	-.175*	-.121	4	+.012*	+.008	4	+.210*	+.145
	5	-.125*	-.086	5	-.082*	-.057	5	+.150*	+.104	5	+.370*	+.256
	6	+.090*	+.062	6	+.076*	+.053	6	+.324*	+.224	6	+.636*	+.439
	7	+.094*	+.065	7	-.038*	-.026	7	+.139*	+.096	7	+.250*	+.173
	8	+.100*	+.069	8	+.036*	+.025	8	+.246*	+.170	8	+.459*	+.317
	9	+.106*	+.073	9	+.062*	+.043	9	+.300*	+.207	9	+.517*	+.357
	10	+.154*	+.106	10	+.156*	+.108	10	+.460*	+.318	10	+.639*	+.442
	11	+.203*	+.140	11	+.266*	+.184	11	+.502*	+.347	11	+.736*	+.509
	12	+.256*	+.177	12	+.389*	+.269	12	+.658*	+.455	12	+.826*	+.571
	13	+.300*	+.207	13	+.420*	+.290	13	+.694*	+.480	13	+.950*	+.656
	14	+.360*	+.207	14	+.463*	+.320	14	+.714*	+.493	14	+.968*	+.669
	15	--	--	15	--	--	15	--	--	15	+1.062*	+.734

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	+.246*	+.170	1	+.500*	+.345	1	+.164*	+.113	1	+.114*	+.078
	2	+.280*	+.193	2	+.260*	+.180	2	+.190*	+.131	2	+.172*	+.119
	3	+.262*	+.181	3	+.236*	+.163	3	+.268*	+.185	3	+.180*	+.124
	4	+.270*	+.187	4	+.335*	+.231	4	+.260*	+.180	4	+.229*	+.158
	5	+.298*	+.206	5	+.311*	+.215	5	+.261*	+.180	5	+.353*	+.244
				6	+.342*	+.236	6	+.364*	+.252	6	+.574*	+.397
				7	+.403*	+.278	7	+.506*	+.350	7	+.800*	+.553
				8	+.469*	+.324	8	+.537*	+.371	8	+.805*	+.556
				9	+.521*	+.360	9	+.542*	+.375	9	+.751*	+.519
				10	+.321*	+.222	10	+.136*	+.094	10	+.236*	+.163

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.770*	-.532	1	-.970	-.670	1	-.960	-.663	1	-.976	-.674	1	-1.076	-.743
	2	-.826*	-.571	2	-.914	-.632	2	-.971	-.671	2	-.970	-.670			
	3	-.883*	-.610	3	-.924	-.638	3	--	--	3	-.903	-.624			
	4	-.900*	-.622	4	-.920	-.636	4	-.930	-.643	4	-.918	-.634			
	5	-.981	-.678	5	-.949	-.656	5	-.930	-.643	5	-.900	-.622			
	6	-.964	-.666	6	-.946	-.654	6	-.911	-.629	6	-.876	-.605			
	7	-.982	-.679	7	-.942	-.651	7	-.893	-.617	7	-.870	-.601			
	8	-.972	-.672	8	-.930	-.643	8	-.500	-.345	8	-.863	-.596			
	9	-.970	-.670	9	-.933	-.645	9	-.882	-.609	9	-.851	-.588			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	-.785	-.542	1	-.708	-.608	1	-.850	-.587	1	-.950	-.656	1	-1.000	-.691
	2	-.840	-.580	2	-.725	-.501	2	-.800	-.553	2	-.847	-.585	2	-.878	-.607
	3	--	--	3	-.700	-.484	3	-.790	-.546	3	-.789	-.545	3	-.700	-.484
	4	-.880		4	-.700	-.484	4	-.800	-.553	4	-.820	-.567	4	-.832	-.575
				5	-.714	-.493	5	-.841	-.581	5	-.842	-.582	5	-.860	-.594
				6	-.770	-.530	6	-.858	-.593	6	-.865	-.598	6	-.835	-.577
				7	-.850	-.587	7	-.876	-.605	7	-.917	-.634	7	-.855	-.591
				8	-.846	-.585	8	-.834	-.576	8	-.900	-.622	8	-.836	-.578
							9	-1.000	-.691	9	-.720	-.497			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.423*	-.292	1	+.296*	+.205	1	-.572*	-.395
	2	-.174*	-.120	2	-.161*	-.111	2	-.344*	-.238
	3	+.060*	+.041	3	-.070*	-.048	3	-.198*	-.137
	4	+.221*	+.153	4	+.058*	+.040	4	-.082*	-.057
	5	+.323*	+.223	5	+.171*	+.118	5	-.028*	-.019
	6	+.388*	+.268	6	+.247*	+.171	6	+.083*	+.057
	7	+.516*	+.357	7	+.362*	+.250	7	+.071*	+.049
	8	+.593*	+.410	8	+.490*	+.339			
	9	+.628*	+.434	9	+.547*	+.378			

MISC.

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p	DE	ΔP	C_p
	1	+.163*	+.113	1	+.283*	+.196	1	+.374*	+.258	1	+.526*	+.363	1	+.577*	+.399
	2	+.304*	+.210	2	+.300*	+.207	2	+.394*	+.272	2	+.547*	+.378	2	+.829*	+.573
	3	+.329*	+.227	3	+.279*	+.193	3	+.476	+.329				3	+.822*	+.568
	4	+.291*	+.201	4	+.378*	+.261									
	5	+.289*	+.200												
													BC 9	-.981	-.678

DATE 4-5-72 WIND DIRECTION: 10° Δh = 1.840 mm Hg P_A = 24.75 in. Hg WIND SPEED: 73.33 fps

TIME 10:00 a.m. Building I T = 60°F ρ_A = 0.001906 slugs/ft^3

Building Face															
F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p			
	1	-.673*	-.466	1	-.725*	-.501	1	-.958*	-.663	1	-.652	-.451			
	2	-.140*	-.097	2	-.238*	-.165	2	-.104*	-.072	2	+.066*	+.046			
	3	0*	0	3	-.138*	-.095	3	+.076*	+.053	3	+.281*	+.194			
	4	--	--	4	-.030*	-.021	4	+.225*	+.156	4	+.388*	+.268			
	5	+.124*	+.086	5	+.065*	+.045	5	+.327*	+.226	5	+.568*	+.393			
	6	+.302*	+.209	6	+.217*	+.150	6	+.534*	+.369	6	+.794*	+.549			
	7	+.274*	+.190	7	+.085*	+.059	7	+.338*	+.234	7	+.488*	+.338			
	8	+.308*	+.213	8	+.161*	+.111	8	+.462*	+.320	8	+.618*	+.427			
	9	+.306*	+.212	9	+.174*	+.120	9	+.538*	+.372	9	+.756*	+.523			
	10	+.334*	+.231	10	+.258*	+.178	10	+.666*	+.461	10	+.792*	+.548			
	11	+.378*	+.261	11	+.360*	+.249	11	+.671*	+.464	11	+.937*	+.648			
	12	+.370*	+.256	12	+.420*	+.291	12	+.755*	+.522	12	+1.003	+.694			
	13	+.386*	+.267	13	+.459	+.317	13	+.819*	+.567	13	+1.030	+.712			
	14	+.348*	+.241	14	+.465	+.322	14	+.804*	+.556	14	+1.051	+.727			
	15	--	--	15	--	--	15	--	--	15	+1.037	+.717			
D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p			
	1	-.038*	-.026	1	+.368*	+.255	1	+.037	+.026	1	+.016*	+.011			
	2	-.058*	-.040	2	+.005*	+.003	2	+.028	+.019	2	-.008*	-.006			
	3	-.058*	-.040	3	-.031*	-.021	3	+.047	+.033	3	-.092*	-.064			
	4	-.032*	-.022	4	+.016*	+.011	4	+.000	+0	4	-.095*	-.066			
	5	+.096*	+.066	5	+.006*	+.004	5	-.025*	-.017	5	-.095*	-.066			
				6	+.064*	+.044	6	+.005*	+.003	6	+.090	+.062			
				7	+.200	+.138	7	+.112*	+.077	7	+.466*	+.322			
				8	+.185	+.128	8	+.214*	+.148	8	+.463*	+.320			
				9	+.204	+.141	9	+.175	+.121	9	+.588*	+.407			
				10	+.050	+.035	10	-.047*	-.033	10	+.178	+.123			
S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.737	-.510	1	-1.005	-.695	1	-.990	-.685	1	-.986	-.682	1	-1.140*	-.789
	2	-.767	-.531	2	-.874	-.605	2	-.997	-.690	2	-.975	-.674			
	3	-.760	-.526	3	-.992	-.686	3	--	--	3	-.905	-.626			
	4	-.854	-.591	4	-.983	-.680	4	-.966	-.668	4	-.925	-.640			
	5	-.894	-.618	5	-.992	-.686	5	-.928	-.642	5	-.925	-.640			
	6	-1.035	-.716	6	-.570	-.394	6	-.944	-.653	6	-.925	-.640			
	7	-1.054	-.729	7	-.978	-.676	7	-.924	-.639	7	-.898	-.621			
	8	-1.016	-.723	8	-.978	-.676	8	-.866	-.599	8	-.873	-.604			
	9	-1.036	-.717	9	-.978	-.676	9	-.888	-.614	9	-.873	-.604			
B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	-.870*	-.602	1	-.887	-.614	1	-.921	-.637	1	-.963	-.666	1	-.915	-.633
	2	--	--	2	-.572*	-.396	2	-.932	-.645	2	-.866	-.599	2	-.822	-.569
	3	-.884	-.611	3	-.568*	-.393	3	-.914	-.632	3	-.778	-.538	3	-.740	-.512
	4	--	--	4	-.534*	-.369	4	-.844	-.584	4	-.852	-.589	4	-.785	-.543
				5	-.592	-.409	5	-.795	-.550	5	-.852	-.589	5	-.828	-.573
				6	-.776	-.537	6	-.795	-.550	6	-.858	-.593	6	-.782	-.541
				7	-.846	-.585	7	-.826	-.571	7	-.898	-.621	7	-.792	-.548
				8	-.862	-.596	8	-.822	-.569	8	-.870	-.602	8	-.792	-.548
							9	-.984*	-.681	9	-.678*	-.469			
T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p						
	1	-.289	-.200	1	+.561	+.388	1	-.453	-.313						
	2	.000	0	2	-.043*	-.030	2	-.215	-.149						
	3	+.215	+.149	3	+.067*	+.046	3	-.087	-.060						
	4	+.338	+.234	4	+.168*	+.116	4	+.018	+.012						
	5	+.466	+.322	5	+.282*	+.195	5	+.055	+.038						
	6	+.522	+.361	6	+.352*	+.243	6	+.196	+.136						
	7	+.612	+.423	7	+.467*	+.323	7	+.207	+.143						
	8	+.612	+.423	8	+.500*	+.346									
	9	+.557*	+.385	9	+.500	+.346									
													MISC.		
G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p	DE	ΔP	C_p
	1	+.122*	+.084	1	+.098	+.068	1	+.167	+.116	1	+.248	+.171	1	-.082*	-.057
	2	+.142	+.098	2	+.098	+.068	2	+.167*	+.116	2	+.204	+.141	2	+.400*	+.277
	3	+.167	+.116	3	+.184	+.127	3	+.167*	+.116				3	+.622*	+.430
	4	+.247	+.171	4	+.260	+.180									
	5	+.284	+.196												
													BC 9	-.964	-.667

DATE 5-4-72 WIND DIRECTION: 80° Δh = 1.844 mm Hg P_A = 24.818 in. Hg WIND SPEED: 73.33 fps

TIME 9:00 a.m. Building II T = 60°F ρ_A = 0.00196 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.623	-.430	1	-.817	-.564	1	-.976	-.674	1	-.963	-.665
	2	-.671	-.463	2	-.823	-.568	2	-.934	-.645	2	-.919	-.634
	3	-.657	-.453	3	-.847	-.585	3	-.924	-.638	3	-.886	-.612
	4	--	--	4	-.900	-.621	4	-.926	-.639	4	-.870	-.600
	5	-.780	-.538	5	-.963	-.665	5	-.948	-.654	5	-.835	-.576
	6	-.843	-.582	6	-.983	-.678	6	-.953	-.658	6	-.886	-.612
	7	-.918	-.634	7	-.983	-.678	7	-.953	-.658	7	-.876	-.605
	8	-.900	-.621	8	-.972	-.671	8	-.912	-.629	8	-.850	-.587
	9	-.978	-.675	9	-1.048	-.723	9	-.970	-.670	9	-.894	-.617
	10	-1.034	-.714	10	-1.066	-.736	10	-.970	-.670	10	-.887	-.612
	11	-1.046	-.722	11	-1.047	-.723	11	-.955	-.659	11	-.866	-.598
	12	-1.047	-.723	12	-1.044	-.721	12	-.929	-.641	12	-.838	-.578
	13	-.990	-.683	13	-1.043	-.720	13	-.929	-.641	13	-.822	-.567
	14	-1.046	-.722	14	-1.041	-.719	14	-.928	-.641	14	-.816	-.563
	15	--	--	15	-.891	-.615	15	--	--	15	-.796	-.549

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.158	-.109	1	+1.085	+.749	1	+.070	+.048	1	+.340*	+.235
	2	+.092	+.063	2	+.278*	+.192	2	+.634	+.438	2	+.838*	+.578
	3	+.113	+.078	3	+.323	+.223	3	+.665	+.459	3	+.955*	+.659
	4	+.070	+.048	4	+.266	+.184	4	+.682	+.471	4	+.934*	+.645
	5	-.010	-.007	5	-.174	-.120	5	+.130	+.090	5	+.150*	+.104
				6	-.300	-.207	6	-.367	-.253	6	-.715*	-.494
				7	+.900	-.625	7	-.276	-.190	7	-.600*	-.414
				8	-.084	-.058	8	-.077	-.053	8	-.344	-.237
				9	-.077	-.053	9	-.002	-.001	9	-.214	-.148
				10	-.166	-.115	10	-.079*	-.055	10	-.260	-.179

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.706	-.487	1	-.646	-.446	1	-.625	-.431	1	-.637	-.440	1	-1.000	-.690
	2	-.706	-.487	2	-.623	-.430	2	-.628	-.433	2	-.635	-.438			
	3	-.667*	-.460	3	-.639	-.441	3	--	--	3	--	--			
	4	-.665*	-.459	4	-.630	-.435	4	-.634	-.438	4	-.643	-.444			
	5	-.633*	-.437	5	-.665	-.459	5	-.652	-.450	5	-.654	-.451			
	6	-.610*	-.421	6	-.096	-.066	6	-.660	-.456	6	-.666	-.460			
	7	-.612*	-.422	7	-.685	-.473	7	-.681	-.470	7	-.690	-.476			
	8	-.610*	-.421	8	-.700	-.483	8	-.145	-.100	8	-.716	-.494			
	9	-.608*	-.420	9	-.708	-.489	9	-.775	-.535	9	-.765	-.528			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	-.712	-.491	1	-.748	-.516	1	-.746	-.515	1	-.836	-.577	1	-.835	-.576
	2	-.712	-.491	2	-.760	-.525	2	-.672	-.464	2	-.753	-.520	2	-.765	-.528
	3	--	--	3	-.741	-.511	3	-.665	-.459	3	-.698	-.482	3	-.730	-.504
	4	-.728	-.502	4	-.750	-.518	4	-.668	-.461	4	-.730	-.504	4	-.639	-.441
				5	-.722	-.498	5	-.686	-.473	5	-.744	-.514	5	-.557	-.384
				6	-.723	-.499	6	-.722	-.498	6	-.763	-.527	6	-.559	-.386
				7	-.728	-.502	7	-.750	-.518	7	-.785	-.542	7	-.515	-.355
				8	-.714	-.493	8	-.700	-.483	8	-.742	-.512	8	-.431	-.297
							9	-.729	-.503	9	-.524	-.362			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.921	-.636	1	-1.700	-1.173	1	-.902	-.623
	2	-.868	-.599	2	-.868	-.599	2	-.879	-.607
	3	-.862	-.595	3	-.855	-.590	3	-.845	-.584
	4	-.891	-.615	4	-.845	-.583	4	-.844	-.583
	5	-.936	-.646	5	-.905*	-.625	5	-.863	-.596
	6	-.941	-.649	6	-.924*	-.638	6	-.870*	-.600
	7	-.933*	-.644	7	-.972*	-.671	7	-.885*	-.611
	8	-.861	-.594	8	-.991*	-.684			
	9	-.861	-.594	9	-.997*	-.688			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p	MISC. DE	ΔP	C_p
	1	+.073	+.050	1	+.158*	+.109	1	-.019	-.013	1	-.043	-.030	1	-.861	-.594
	2	+.030	+.021	2	-.057	-.039	2	-.079	-.055	2	-.028	-.019	2	-.794	-.548
	3	-.069	-.068	3	-.254	-.176	3	-.004	-.003				3	-.715	-.494
	4	-.333*	-.230	4	-.126	-.087									
	5	-.388*	-.268												
													BC 9	-.687	-.474

DATE 5-4-72 WIND DIRECTION: 90° Δh = 1.836 mm Hg P_A = 24.745 in. Hg WIND SPEED: 73.33 fps

TIME 3:30 p.m. Building II T = 60°F ρ_A = 0.00195 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.648	-.449	1	-.764	-.530	1	-.958	-.664	1	-.964	-.668
	2	-.621	-.430	2	-.789	-.547	2	-.896	-.621	2	-.886	-.614
	3	-.649	-.450	3	-.833	-.577	3	-.879	-.609	3	-.876	-.607
	4	--	--	4	-.898	-.623	4	-.878	-.609	4	-.889	-.616
	5	-.752	-.521	5	-.930	-.645	5	-.895	-.620	5	-.887	-.615
	6	-.764	-.530	6	-.962	-.667	6	-.907	-.629	6	-.943	-.654
	7	-.890	-.617	7	-.953	-.661	7	-.900	-.624	7	-.926	-.642
	8	-.875	-.607	8	-.935	-.648	8	-.870	-.603	8	-.860	-.596
	9	-.949	-.658	9	-1.033	-.716	9	-.928	-.643	9	-.949	-.658
	10	-.981	-.680	10	-1.038	-.720	10	-.927	-.643	10	-.900	-.624
	11	-.992	-.688	11	-1.021	-.708	11	-.900	-.624	11	-.865	-.600
	12	-.985	-.683	12	-1.004	-.696	12	-.900	-.624	12	-.848	-.588
	13	-.960	-.665	13	-.986	-.684	13	-.886	-.614	13	-.831	-.576
	14	-.964	-.668	14	-.986	-.684	14	-.868	-.602	14	-.830	-.575
	15	--	--	15	+.700	+.485	15	--	--	15	-.800	-.555

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.118	-.082	1	+.067*	+.046	1	+1.58*	+1.095	1	+.407	+.282
	2	+.112	+.077	2	+.316	+.219	2	+.590*	+.409	2	+.866	+.600
	3	+.179	+.124	3	+.406	+.281	3	+.731	+.507	3	+.944	+.654
	4	+.130	+.090	4	+.350	+.243	4	+.729	+.505	4	+.945	+.655
	5	+.082*	+.057	5	-.061*	-.042	5	+.273*	+.189	5	+.388	+.269
				6	-.214*	-.148	6	-.214*	-.148	6	-.505	-.350
				7	+.135*	+.094	7	-.138*	-.096	7	-.486	-.337
				8	+.006*	+.004	8	+.046*	+.032	8	-.200*	-.139
				9	+.005*	+.003	9	+.116*	+.080	9	-.074*	-.051
				10	-.078*	-.054	10	-.020*	-.014	10	-.154*	-.107

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.692	-.480	1	-.645	-.447	1	-.628	-.435	1	-.630	-.437	1	-.860	-.596
	2	-.688	-.477	2	-.615	-.426	2	-.630	-.437	2	-.634	-.440			
	3	-.657	-.455	3	-.628	-.435	3	--	--	3	--	--			
	4	-.647	-.449	4	-.631	-.437	4	-.644	-.446	4	-.637	-.442			
	5	-.646	-.448	5	-.686	-.476	5	-.661	-.458	5	-.642	-.445			
	6	-.674	-.467	6	-.354	-.245	6	-.677	-.469	6	-.656	-.455			
	7	-.700	-.485	7	-.715	-.496	7	-.700	-.485	7	-.672	-.466			
	8	-.665	-.461	8	-.728	-.505	8	-.710	-.492	8	-.695	-.482			
	9	-.645	-.447	9	-.729	-.505	9	-.786	-.545	9	-.759	-.526			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	-.710	-.492	1	-.743	-.515	1	-.732	-.507	1	-.826	-.573	1	-.878	-.609
	2	-.704	-.488	2	-.743	-.515	2	-.668	-.463	2	-.740	-.513	2	-.240	-.166
	3	--	--	3	-.736	-.510	3	-.654	-.453	3	-.700	-.485	3	-.718	-.498
	4	-.723	-.501	4	-.738	-.512	4	-.665	-.461	4	-.704	-.488	4	-.642	-.445
				5	-.707	-.490	5	-.685	-.475	5	-.747	-.518	5	-.550	-.381
				6	-.720	-.499	6	-.716	-.496	6	-.752	-.521	6	-.520	-.360
				7	-.718	-.498	7	-.740	-.513	7	-.791	-.548	7	-.520	-.360
				8	-.702	-.487	8	-.684	-.474	8	-.746	-.517	8	-.520	-.360
							9	-.742	-.514	9	-.534	-.370			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.850	-.589	1	-.880	-.610	1	-.851	-.592
	2	-.844	-.585	2	-.770	-.534	2	-.820	-.570
	3	-.861	-.597	3	-.814	-.564	3	-.820	-.570
	4	-.998	-.692	4	-.874	-.606	4	-.843	-.586
	5	-1.039	-.720	5	-.976	-.677	5	-.876	-.609
	6	-1.065	-.738	6	-1.000	-.693	6	-.920	-.640
	7	-1.012	-.702	7	-1.100	-.763	7	-.977	-.679
	8	-.926	-.642	8	-1.062	-.736			
	9	-.872	-.604	9	-1.800	-1.248			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p
	1	+.130*	+.090	1	+.242*	+.168	1	+.090*	+.063	1	+.044*	+.031
	2	+.034*	+.024	2	+.025*	+.017	2	+.020*	+.014	2	+.044*	+.031
	3	-.071*	-.049	3	-.149*	-.104	3	+.044*	+.031			
	4	-.211*	-.147	4	-.006*	-.004						
	5	-.242*	-.168									

MISC.

DE	ΔP	C_p
1	-.842	-.586
2	-.746	-.519
3	-.643	-.447

BC 9 -.684 -.476

DATE 5-8-72 WIND DIRECTION: 100° Δh = 1.844 mm Hg P_A = 24.80 in. Hg WIND SPEED: 73.33 fps

TIME 1:00 p.m. Building II T = 60°F ρ_A = 0.00196 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.636	-.439	1	-.684	-.472	1	-.862	-.595	1	-.919	-.634
	2	-.582	-.402	2	-.724	-.500	2	-.825	-.569	2	-.867	-.598
	3	-.586	-.404	3	-.766	-.529	3	-.800	-.552	3	-.860	-.594
	4	--	--	4	-.808	-.558	4	-.819	-.565	4	-.900	-.621
	5	-.678	-.468	5	-.875	-.604	5	-.858	-.592	5	-.856	-.591
	6	-.686	-.473	6	-.938	-.647	6	-.884	-.610	6	-.992	-.685
	7	-.825	-.569	7	-.916	-.632	7	-.868	-.599	7	-.960	-.663
	8	-.802	-.553	8	-.889	-.614	8	-.820	-.566	8	-.900	-.621
	9	-.880	-.607	9	-1.034	-.713	9	-.836	-.577	9	-1.000	-.690
	10	-.959	-.662	10	-1.064	-.734	10	-.930	-.642	10	-.950	-.656
	11	-1.000	-.690	11	-1.066	-.736	11	-.903	-.623	11	-.905	-.625
	12	-1.007	-.695	12	-1.052	-.726	12	-.900	-.621	12	-.880	-.607
	13	-.990	-.683	13	-1.028	-.710	13	-.875	-.604	13	-.858	-.592
	14	-.980	-.676	14	-1.000	-.690	14	-.852	-.588	14	-.834	-.576
	15	--	--	15	+.280	+.193	15	--	--	15	-.800	-.552

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.096*	-.066	1	-.020*	-.014	1	+.268*	+.185	1	+.505	+.349
	2	+.130*	+.090	2	+.343*	+.237	2	+.666*	+.460	2	+.826	+.570
	3	+.150*	+.104	3	+.394*	+.272	3	+.740*	+.511	3	+.890	+.614
	4	+.138*	+.095	4	+.395*	+.273	4	+.728*	+.502	4	+.926	+.639
	5	+.198*	+.137	5	+.090*	+.062	5	+.415*	+.286	5	+.538	+.371
				6	-.086*	-.059	6	-.016*	-.011	6	-.178*	-.123
				7	+.050*	+.035	7	+.028*	+.019	7	-.200*	-.138
				8	+.148*	+.102	8	+.192*	+.133	8	+.030*	+.021
				9	+.182*	+.126	9	+.238*	+.164	9	+.144*	+.099
				10	+.084*	+.058	10	+.059*	+.041	10	0*	0

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.574	-.396	1	-.600	-.414	1	-.600	-.414	1	-.600	-.414	1	-.642	-.443
	2	-.564	-.389	2	-.587	-.405	2	-.612	-.422	2	-.600	-.414			
	3	-.545	-.376	3	-.578	-.399	3	--	--	3	--	--			
	4	-.585	-.404	4	-.589	-.407	4	-.600	-.414	4	-.587	-.405			
	5	-.650	-.449	5	-.628	-.433	5	-.600	-.414	5	-.582	-.402			
	6	-.700	-.483	6	-.300	-.207	6	-.626	-.432	6	-.592	-.409			
	7	-.670	-.462	7	-.648	-.447	7	-.634	-.438	7	-.600	-.414			
	8	-.634	-.438	8	-.646	-.446	8	-.178*	-.123	8	-.639	-.441			
	9	-.625	-.431	9	-.600	-.414	9	-.702	-.485	9	-.700	-.483			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	-.624	-.431	1	-.700	-.483	1	-.700	-.483	1	-.752	-.519	1	-.790	-.545
	2	-.631	-.436	2	-.700	-.483	2	-.624	-.431	2	-.682	-.471	2	-.700	-.483
	3	--	--	3	-.700	-.483	3	-.615	-.424	3	-.622	-.429	3	-.612	-.422
	4	-.654	-.451	4	-.680	-.469	4	-.624	-.431	4	-.637	-.440	4	-.580	-.400
				5	-.646	-.446	5	-.632	-.436	5	-.663	-.458	5	-.543	-.375
				6	-.647	-.447	6	-.660	-.456	6	-.674	-.465	6	-.488	-.337
				7	-.670	-.462	7	-.676	-.467	7	-.700	-.483	7	-.517	-.357
				8	-.644	-.444	8	-.630	-.435	8	-.680	-.469	8	-.509	-.351
							9	-.700	-.483	9	-.430	-.297			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.810*	-.559	1	-.636	-.439	1	-.745	-.515
	2	-.832*	-.574	2	-.708	-.489	2	-.741	-.511
	3	-.990*	-.583	3	-.849	-.586	3	-.782	-.540
	4	-1.119	-.772	4	-.972	-.671	4	-.868	-.599
	5	-1.172	-.809	5	-1.094	-.755	5	-.994	-.686
	6	-1.148	-.792	6	-1.169	-.807	6	-1.096	-.756
	7	-1.078*	-.744	7	-1.134	-.783	7	-1.174	-.810
	8	-.972	-.671	8	-1.111	-.767			
	9	-.917	-.633	9	-1.080	-.745			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p
	1	+.140*	+.097	1	+.295*	+.204	1	+.198*	+.137	1	+.118*	+.081
	2	-.034*	-.023	2	+.086*	+.059	2	+.100*	+.069	2	+.216*	+.149
	3	-.147*	-.101	3	-.046*	-.032	3	+.055*	+.038			
	4	-.016*	-.011	4	+.066*	+.046						
	5	+.069*	+.048									

MISC.

DE	ΔP	C_p
1	-.684	-.472
2	-.585	-.404
3	-.442	-.305
BC 9	-.676	-.467

DATE 5-9-72 WIND DIRECTION: 110° Δh = 1.844 mm Hg P_A = 24.861 in. Hg WIND SPEED: 73.33 fps

TIME 8:00 a.m. Building II T = 60°F ρ_A = 0.00196 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.522	-.360	1	-.561	-.387	1	-.699	-.482	1	-.742	-.512
	2	-.468	-.323	2	-.571	-.394	2	-.670	-.462	2	-.727	-.502
	3	-.466	-.322	3	-.590	-.407	3	-.670	-.462	3	-.728	-.502
	4	--	--	4	-.649	-.448	4	-.686	-.473	4	-.767	-.529
	5	-.546	-.377	5	-.720	-.697	5	-.740	-.511	5	-.803	-.554
	6	-.558*	-.385	6	-.767	-.529	6	-.772	-.533	6	-.840	-.580
	7	-.656*	-.453	7	-.746	-.515	7	-.763	-.527	7	-.816	-.563
	8	-.643*	-.444	8	-.734	-.507	8	-.723	-.499	8	-.792	-.547
	9	-.762*	-.526	9	-.923	-.637	9	-.859	-.593	9	-.908	-.627
	10	-.878*	-.606	10	-.970	-.670	10	-.879	-.607	10	-.926	-.639
	11	-.983*	-.678	11	-.970	-.670	11	-.876	-.605	11	-.926	-.639
	12	-.978*	-.675	12	-.926	-.639	12	-.846	-.584	12	-.880*	-.607
	13	-.934*	-.645	13	-.922	-.636	13	-.838	-.578	13	-.867*	-.598
	14	--	--	14	-.909	-.627	14	-.817	-.564	14	-.843*	-.582
	15	--	--	15	-.532	-.367	15	--	--	15	-.840*	-.580

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.086*	-.059	1	+.447	+.309	1	+.234*	+.162	1	+.418*	+.289
	2	+.148*	+.102	2	+.327*	+.226	2	+.628*	+.433	2	+.754*	+.520
	3	+.187*	+.129	3	+.433*	+.299	3	+.715*	+.494	3	+.851*	+.587
	4	+.179*	+.124	4	+.453*	+.313	4	+.758*	+.523	4	+.882*	+.609
	5	+.276*	+.190	5	+.149*	+.103	5	+.515*	+.355	5	+.641*	+.442
				6	-.014*	-.010	6	+.115*	+.079	6	+.060*	+.041
				7	+.459	+.317	7	+.127*	+.088	7	+.040*	+.028
				8	+.217*	+.150	8	+.251*	+.173	8	+.179*	+.124
				9	+.277*	+.191	9	+.300	+.207	9	+.282*	+.195
				10	+.171*	+.118	10	+.127*	+.088	10	+.077*	+.053

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.460	-.317	1	-.504	-.348	1	-.511	-.353	1	-.515	-.355	1	-.555	-.383
	2	-.458	-.316	2	-.485	-.335	2	-.504	-.348	2	-.518	-.358			
	3	-.465	-.321	3	-.472	-.326	3	--	--	3	--	--			
	4	-.500	-.345	4	-.489	-.338	4	-.507	-.350	4	-.508	-.351			
	5	-.540	-.373	5	-.500	-.345	5	-.523	-.361	5	-.508	-.351			
	6	-.549	-.379	6	-.256	-.177	6	-.523	-.361	6	-.503	-.347			
	7	-.532	-.367	7	-.516	-.356	7	-.523	-.361	7	-.524	-.362			
	8	-.520	-.359	8	-.513	-.354	8	-1.137	-.785	8	-.545	-.376			
	9	-.512	-.353	9	-.539	-.372	9	-.575	-.397	9	-.583	-.402			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	-.504	-.348	1	-.675*	-.466	1	-.659	-.455	1	-.658	-.454	1	-.575	-.397
	2	-.504	-.348	2	-.686*	-.473	2	-.566	-.391	2	-.582	-.402	2	-.509	-.351
	3	--	--	3	-.662	-.457	3	-.572	-.395	3	-.534	-.369	3	-.509	-.351
	4	-.533	-.368	4	-.600	-.414	4	-.572	-.395	4	-.562	-.388	4	-.517	-.357
				5	-.534	-.369	5	-.576	-.398	5	-.558	-.385	5	-.470	-.324
				6	-.536	-.370	6	-.594	-.410	6	-.573	-.395	6	--	--
				7	-.572	-.395	7	-.610	-.421	7	-.600	-.414	7	-.484	-.334
				8	-.529	-.365	8	-.553	-.382	8	-.575	-.397	8	-.467	-.322
							9	-.620	-.428	9	-.684	-.472			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.690*	-.476	1	-.351	-.242	1	-.630	-.435
	2	-.699*	-.482	2	-.351	-.242	2	-.652	-.450
	3	-.855*	-.590	3	-.777*	-.536	3	-.759	-.524
	4	-.976*	-.474	4	-.924*	-.638	4	-.815	-.563
	5	-1.021	-.705	5	-1.025*	-.707	5	-.931*	-.643
	6	-1.020	-.704	6	-1.042*	-.719	6	-.972*	-.671
	7	-1.009	-.696	7	-1.048*	-.723	7	-1.054	-.727
	8	-.932	-.643	8	-1.048*	-.723			
	9	-.931	-.643	9	-.956	-.660			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p
	1	+.175	+.121	1	+.361	+.249	1	+.278	+.192	1	+.180	+.124
	2	+.040	+.028	2	+.161	+.111	2	+.157	+.108	2	-.338	-.233
	3	-.128	-.088	3	+.024	+.017	3	+.116	+.080			
	4	-.067	-.046	4	+.102	+.070						
	5	+.180	+.124									

MISC.

DE	ΔP	C_p
1	-.362	-.250
2	-.306	-.211
3	-.200	-.138

BC	9	-.537	-.371

DATE 4-25-72 WIND DIRECTION: 120° Δh = 1.82 mm Hg P_A = 24.51 in. Hg WIND SPEED: 73.33 fps

TIME 10:30 a.m. Building II T = 60°F ρ_A = 0.00193 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.376	-.263	1	-.379*	-.265	1	-.412*	-.288	1	-.444*	-.310
	2	-.295	-.206	2	-.376*	-.263	2	-.378*	-.264	2	-.421*	-.294
	3	-.281	-.197	3	-.357*	-.250	3	-.383*	-.268	3	-.424*	-.297
	4	--	--	4	-.355*	-.248	4	-.386*	-.270	4	-.433*	-.303
	5	-.278	-.194	5	-.372*	-.260	5	-.418*	-.292	5	-.334*	-.234
	6	-.253*	-.177	6	-.429*	-.300	6	-.451*	-.315	6	-.436*	-.305
	7	-.294*	-.206	7	-.428*	-.299	7	-.452*	-.316	7	-.499*	-.349
	8	-.309	-.216	8	-.397*	-.278	8	-.449*	-.314	8	-.530*	-.371
	9	-.394*	-.563	9	-.554*	-.387	9	-.555*	-.388	9	-.589*	-.412
	10	-.560*	-.392	10	-.690*	-.483	10	-.692*	-.484	10	-.746*	-.522
	11	-.746	-.521	11	-.770	-.538	11	-.777*	-.543	11	-.878*	-.614
	12	-.758	-.530	12	-.752	-.526	12	-.867*	-.606	12	-1.008*	-.705
	13	-.722*	-.505	13	-.729*	-.510	13	-.898*	-.628	13	-1.026*	-.717
	14	-.707	-.494	14	-.733	-.513	14	-.932*	-.652	14	-1.029*	-.720
	15	--	--	15	-.360*	-.252	15	--	--	15	-1.000*	-.699

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.050*	-.035	1	+1.619	+1.132	1	+.080*	+.055	1	+.241*	+.169
	2	+.125	+.087	2	+.165*	+.115	2	+.388*	+.271	2	+.526*	+.368
	3	+.166	+.116	3	+.238*	+.166	3	+.452*	+.316	3	+.620*	+.434
	4	+.192*	+.134	4	+.310*	+.217	4	+.492*	+.344	4	+.698*	+.488
	5	+.252	+.176	5	+.178*	+.124	5	+.440*	+.308	5	+.638*	+.446
				6	+.086*	+.060	6	+.162*	+.113	6	+.216*	+.151
				7	--	--	7	+.106*	+.074	7	+.061*	+.043
				8	+.235	+.164	8	+.205	+.143	8	+.199*	+.139
				9	+.262	+.183	9	+.228	+.159	9	+.270*	+.189
				10	+.134*	+.094	10	+.074	+.052	10	+.083	+.058

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.340	-.238	1	-.376	-.263	1	-.389	-.272	1	-.388	-.271	1	-.399	-.279
	2	-.344	-.241	2	-.294	-.206	2	-.389	-.272	2	-.384	-.269			
	3	-.356	-.249	3	-.377	-.264	3	--	--	3	--	--			
	4	-.379	-.265	4	-.376	-.263	4	-.384	-.269	4	-.378	-.271			
	5	-.400	-.280	5	-.381	-.266	5	-.384	-.269	5	-.371	-.259			
	6	-.396	-.277	6	+.830	+.580	6	-.384	-.269	6	-.376	-.263			
	7	-.390	-.273	7	-.375	-.262	7	-.387	-.271	7	-.381	-.266			
	8	-.378	-.264	8	-.374	-.262	8	+.100*	+.070	8	-.385	-.269			
	9	-.376	-.263	9	-.367	-.257	9	-.388	-.271	9	-.384	-.269			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	-.362	-.253	1	-.514	-.359	1	-.500	-.350	1	-.511	-.357	1	-.587	-.410
	2	-.369	-.258	2	-.546	-.382	2	-.430	-.300	2	-.446	-.312	2	-.487	-.341
	3	--	--	3	-.506	-.354	3	-.432	-.302	3	-.406	-.284	3	-.406	-.384
	4	-.374	-.262	4	-.449	-.314	4	-.435	-.304	4	-.430	-.301	4	-.416	-.291
				5	-.387	-.271	5	-.442	-.309	5	-.437	-.306	5	-.438	-.306
				6	-.385	-.269	6	-.448	-.313	6	-.449	-.314	6	-.415	-.290
				7	-.390	-.273	7	-.460	-.322	7	-.474	-.331	7	-.416	-.291
				8	-.390	-.273	8	-.415	-.290	8	-.454	-.317	8	-.382	-.267
							9	-.457	-.320	9	-.248	-.173			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.400	-.280	1	-.610	-.427	1	-.436	-.305
	2	-.426	-.298	2	-.376	-.263	2	-.460	-.322
	3	-.508	-.355	3	-.496	-.347	3	-.490	-.343
	4	-.627*	-.438	4	-.566	-.396	4	-.545	-.381
	5	-.704*	-.492	5	-.672	-.470	5	-.649	-.454
	6	-.835*	-.584	6	-.781*	-.546	6	-.766	-.536
	7	-.996*	-.697	7	-.900*	-.629	7	-.844*	-.590
	8	-1.090*	-.762	8	-.987*	-.690			
	9	-1.130*	-.790	9	-.968*	-.677			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p
	1	-.857	-.599	1	+.303	+.212	1	+.261	+.183	1	+.230	+.161
	2	+.150*	+.105	2	+.229	+.160	2	+.203	+.142	2	+.300	+.210
	3	+.076*	+.053	3	+.110	+.077	3	+.200	+.140			
	4	+.118*	+.083	4	+.153	+.107						
	5	+.175	+.122									

MISC.

DE	ΔP	C_p
1	-.126*	-.088
2	-.126*	-.088
3	-.045*	-.031

BC	9	-.385	-.269

DATE 4-27-72 WIND DIRECTION: 130° Δh = 1.83 mm Hg P_A = 24.75 in. Hg WIND SPEED: 73.33 fps

TIME 8:15 a.m. Building II T = 60°F ρ_A = 0.00195 slugs/ft^3

Building Face														
F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p		
	1	-.369	-.257	1	-.409	-.284	1	-.466	-.324	1	-.451	-.314		
	2	-.305	-.212	2	-.348	-.242	2	-.360	-.250	2	-.367	-.255		
	3	-.284	-.198	3	-.339	-.236	3	-.350	-.243	3	-.322	-.224		
	4	--	--	4	-.319	-.222	4	-.340	-.236	4	-.312	-.217		
	5	-.280	-.195	5	-.308	-.214	5	-.337	-.234	5	-.258	-.179		
	6	-.266	-.185	6	-.260	-.181	6	-.275	-.191	6	-.176	-.122		
	7	-.278	-.193	7	-.309	-.215	7	-.328	-.228	7	-.362	-.252		
	8	-.278	-.193	8	-.290	-.202	8	-.300	-.209	8	-.248	-.172		
	9	-.291	-.202	9	-.309	-.215	9	-.310	-.216	9	-.283	-.197		
	10	-.320	-.223	10	-.344	-.239	10	-.303	-.211	10	-.306	-.213		
	11	-.372	-.259	11	-.390	-.271	11	-.425	-.296	11	-.370	-.257		
	12	-.376	-.262	12	-.452	-.314	12	-.569	-.396	12	-.532*	-.370		
	13	-.377	-.262	13	-.526	-.366	13	-.758	-.527	13	-.846*	-.588		
	14	-.377	-.262	14	-.586	-.408	14	-.968*	-.673	14	-1.216*	-.846		
	15	--	--	15	-.128	-.089	15	--	--	15	-1.310*	-.911		
D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p		
	1	-.139	-.097	1	+.134	+.093	1	+.315	+.219	1	+.707*	+.492		
	2	+.054	+.038	2	-.010	-.007	2	+.380	+.264	2	+.707*	+.492		
	3	+.132	+.092	3	+.048	+.033	3	+.388	+.270	3	+.586*	+.408		
	4	+.222	+.154	4	+.171	+.119	4	+.397	+.276	4	+.589*	+.410		
	5	+.314	+.218	5	+.244	+.170	5	+.390	+.271	5	+.541*	+.376		
				6	+.338	+.235	6	+.394	+.274	6	+.526*	+.366		
				7	+.258	+.179	7	+.396	+.275	7	+.465*	+.323		
				8	+.485	+.337	8	+.396	+.275	8	+.453*	+.315		
				9	+.460	+.320	9	+.356	+.248	9	+.406*	+.282		
				10	+.300	+.209	10	+.074	+.051	10	+.100	+.070		
S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.358	-.249	1	-.418	-.291	1	-.400	-.278	1	-.386	-.268	1	-.396	-.275
	2	-.368	-.256	2	-.395	-.275	2	-.405	-.282	2	-.389	-.271			
	3	-.390	-.271	3	-.408	-.284	3	--	--	3	--	--			
	4	-.425	-.296	4	-.410	-.285	4	-.396	-.275	4	-.384	-.267			
	5	-.430	-.299	5	-.412	-.287	5	-.389	-.271	5	-.370	-.257			
	6	-.428	-.298	6	-.330*	-.230	6	-.387	-.269	6	-.366	-.255			
	7	-.444	-.309	7	-.424	-.295	7	-.378	-.263	7	-.365	-.354			
	8	-.439	-.305	8	-.408	-.284	8	-.237	-.165	8	-.363	-.252			
	9	-.441	-.307	9	-.380	-.264	9	-.382	-.266	9	-.358	-.249			
B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	-.371	-.258	1	-.530	-.369	1	-.542	-.377	1	-.554	-.385	1	-.656	-.456
	2	-.380	-.264	2	-.551	-.383	2	-.457	-.318	2	-.473	-.329	2	-.552	-.384
	3	--	--	3	-.525	-.365	3	-.457	-.318	3	-.440	-.306	3	-.476	-.331
	4	-.396	-.275	4	-.474	-.330	4	-.468	-.316	4	-.466	-.324	4	-.501	-.348
				5	-.394	-.274	5	-.469	-.326	5	-.463	-.322	5	-.530	-.369
				6	-.399	-.278	6	-.471	-.328	6	-.470	-.327	6	-.500	-.348
				7	-.399	-.278	7	-.483	-.336	7	-.489	-.340	7	-.506	-.352
				8	-.391	-.272	8	-.438	-.305	8	-.461	-.321	8	-.442	-.307
							9	-.477	-.332	9	-.281	-.195			
T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p						
	1	-.388	-.270	1	-2.403	-1.671	1	-.437	-.304						
	2	-.344	-.239	2	-.302	-.210	2	-.460*	-.320						
	3	-.325	-.226	3	-.364	-.253	3	-.466	-.324						
	4	-.272	-.189	4	-.385	-.268	4	-.539	-.375						
	5	-.323	-.225	5	-.446*	-.310	5	-.682	-.474						
	6	-.362	-.252	6	-.576*	-.401	6	-.835	-.581						
	7	-.454*	-.316	7	-.862	-.600	7	-.874	-.608						
	8	-1.286*	-.894	8	-1.111	-.773									
	9	-1.606*	-1.117	9	-1.100	-.765									
													MISC.		
G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p	DE	ΔP	C_p
	1	+.224	+.156	1	+.254*	+.177	1	+.386*	+.268	1	+.454*	+.316	1	+.321*	+.223
	2	+.303*	+.211	2	+.321*	+.223	2	+.442*	+.307	2	+.571*	+.397	2	+.281*	+.195
	3	+.334*	+.232	3	+.335*	+.233	3	+.407*	+.283				3	+.211*	+.147
	4	+.317*	+.220	4	+.294*	+.204									
	5	+.322*	+.224												
													BC 9	-.439*	-.305

DATE 4-27-72 WIND DIRECTION: 140° Δh = 1.851 mm Hg P_A = 24.915 in. Hg WIND SPEED: 73.33 fps

TIME 3:00 p.m. Building II T = 60°F ρ_A = 0.00196 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.471	-.324	1	-.490	-.337	1	-.589	-.405	1	-.557	-.383
	2	-.347	-.239	2	-.398	-.274	2	-.405	-.278	2	-.383	-.263
	3	-.311	-.214	3	-.374	-.257	3	-.377	-.259	3	-.286	-.197
	4	--	--	4	-.356	-.245	4	-.355	-.244	4	-.262	-.180
	5	-.283	-.195	5	-.337	-.232	5	-.336	-.231	5	-.198	-.136
	6	-.225	-.155	6	-.252	-.173	6	-.266	-.183	6	-.010	-.007
	7	-.251	-.173	7	-.282	-.194	7	-.328	-.226	7	-.348	-.239
	8	-.244	-.168	8	-.263	-.181	8	-.286	-.197	8	-.128	-.088
	9	-.249	-.171	9	-.278	-.191	9	-.281	-.193	9	-.175	-.120
	10	-.249	-.171	10	-.275	-.189	10	-.229	-.157	10	-.149	-.102
	11	-.261	-.179	11	-.275	-.189	11	-.253	-.174	11	-.112	-.077
	12	-.283	-.195	12	-.289	-.199	12	-.270	-.186	12	-.084	-.058
	13	-.260	-.179	13	-.347	-.239	13	-.286	-.197	13	-.131	-.090
	14	-.322	-.221	14	-.418*	-.287	14	-.366*	-.252	14	-.269	-.185
	15	--	--	15	+.066	+.045	15	--	--	15	-.462	-.318

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.201	-.138	1	+.257	+.177	1	+.068*	+.047	1	+.510*	+.351
	2	-.058	-.040	2	-.116	-.080	2	+.116*	+.080	2	+.543	+.373
	3	+.004	+.003	3	-.070	-.048	3	+.129*	+.089	3	+.522	+.359
	4	+.082	+.056	4	+.027	+.019	4	+.155	+.107	4	+.562	+.386
	5	+.164	+.113	5	+.112	+.077	5	+.196	+.135	5	+.587	+.404
				6	+.250	+.172	6	+.260*	+.179	6	+.522	+.359
				7	+.176	+.121	7	+.292*	+.201	7	+.646	+.444
				8	+.460	+.316	8	+.300*	+.206	8	+.637	+.438
				9	+.479	+.329	9	+.264*	+.182	9	+.605	+.416
				10	+.406	+.279	10	+.008	+.006	10	+.112	+.077

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.455	-.313	1	-.521	-.358	1	-.500	-.344	1	-.483	-.332	1	-.482	-.331
	2	-.459	-.316	2	-.447	-.307	2	-.506	-.348	2	-.486	-.334			
	3	-.487	-.335	3	-.500	-.344	3	--	--	3	--	--			
	4	-.498	-.342	4	-.490	-.337	4	-.487	-.335	4	-.475	-.327			
	5	-.498	-.342	5	-.484	-.333	5	-.473	-.325	5	-.465	-.320			
	6	-.498	-.342	6	-.657	-.452	6	-.470	-.323	6	-.467	-.321			
	7	-.492	-.338	7	-.488	-.336	7	-.463	-.318	7	-.452	-.311			
	8	-.492	-.338	8	-.473	-.325	8	-.090	-.062	8	-.454	-.312			
	9	-.479	-.329	9	-.476	-.327	9	-.458	-.315	9	-.451	-.310			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	-.477	-.328	1	-.541	-.372	1	-.606	-.417	1	-.711	-.489	1	-.976	-.671
	2	-.486	-.334	2	-.584	-.402	2	-.540	-.371	2	-.624	-.429	2	-.813	-.559
	3	--	--	3	-.554	-.381	3	-.536	-.369	3	-.572	-.393	3	-.682	-.469
	4	-.506	-.348	4	-.520	-.358	4	-.554	-.381	4	-.600	-.413	4	-.723*	-.497
				5	-.470	-.323	5	-.559	-.384	5	-.606	-.417	5	-.780*	-.536
				6	-.479	-.329	6	-.577	-.397	6	-.612	-.421	6	-.716	-.492
				7	-.500	-.344	7	-.580	-.399	7	-.633	-.435	7	-.689	-.474
				8	-.490	-.337	8	-.536	-.369	8	-.582	-.400	8	-.596	-.410
							9	-.581	-.399	9	-.390	-.268			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.438	-.301	1	-.472	-.325	1	-.494	-.340
	2	-.327	-.225	2	-.323	-.222	2	-.443	-.305
	3	-.274	-.188	3	-.320	-.220	3	-.323	-.222
	4	-.165	-.113	4	-.256	-.176	4	-.322	-.221
	5	-.204	-.140	5	-.226	-.155	5	-.634	-.436
	6	-.200	-.138	6	-.218	-.150	6	-1.058	-.727
	7	-.106	-.073	7	-.252	-.173	7	-1.061	-.730
	8	-.208*	-.143	8	-.914	-.628			
	9	-.750*	-.516	9	-1.098	-.755			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p	MISC. DE	ΔP	C_p
	1	+.150	+.103	1	+.146	+.100	1	+.316*	+.217	1	+.457*	+.314	1	+.760	+.523
	2	+.247	+.170	2	+.218	+.150	2	+.400*	+.275	2	+.576*	+.396	2	+.700	+.481
	3	+.291	+.200	3	+.274	+.188	3	+.396*	+.272				3	+.601	+.413
	4	+.291	+.200	4	+.276	+.190									
	5	+.286	+.197												
													BC 9	-.533	-.366

DATE 4-28-72 WIND DIRECTION: 150° Δh = 1.844 mm Hg P_A = 24.84 in. Hg WIND SPEED: 73.33 fps

TIME 10:00 a.m. Building II T - 60°F ρ_A = 0.00196 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.538	-.371	1	-.589	-.407	1	-.734	-.507	1	-.680	-.469
	2	-.382	-.264	2	-.445	-.307	2	-.452	-.312	2	-.389	-.268
	3	-.336	-.232	3	-.408	-.282	3	-.384	-.265	3	-.276	-.190
	4	--	--	4	-.373	-.257	4	-.355	-.245	4	-.209*	-.144
	5	-.314	-.217	5	-.334	-.231	5	-.317	-.219	5	-.088*	-.061
	6	-.228	-.157	6	-.228	-.157	6	-.224	-.155	6	+.133	+.092
	7	-.245	-.169	7	-.315	-.217	7	-.305	-.211	7	-.289	-.199
	8	-.232	-.160	8	-.278	-.192	8	-.255	-.176	8	-.042*	-.029
	9	-.225	-.155	9	-.275	-.190	9	-.233	-.161	9	-.076*	-.052
	10	-.220	-.152	10	-.274	-.189	10	-.143*	-.099	10	-.019*	-.013
	11	-.252	-.174	11	-.278	-.192	11	-.144*	-.099	11	+.032*	-.022
	12	-.292	-.202	12	-.259*	-.179	12	-.126*	-.087	12	+.105	+.072
	13	-.315*	-.217	13	-.300*	-.207	13	-.090*	-.062	13	+.132	+.091
	14	-.346	-.239	14	-.348*	-.240	14	-.092*	-.063	14	+.100	+.069
	15	--	--	15	-.082*	-.057	15	--	--	15	-.036	-.025

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.258*	-.178	1	+1.451*	+1.000	1	-.061*	-.042	1	+.410*	+.283
	2	-.093*	-.064	2	-.143	-.099	2	+.010*	+.007	2	+.556*	+.384
	3	-.018*	-.012	3	-.111	-.077	3	+.061*	+.042	3	+.545*	+.376
	4	+.061*	+.042	4	+.008	+.006	4	+.108*	+.075	4	+.624*	+.431
	5	+.164*	+.113	5	+.069	+.048	5	+.177*	+.122	5	+.674*	+.465
				6	+.243	+.168	6	+.271*	+.187	6	+.743*	+.513
				7	+1.216	+.839	7	+.321*	+.222	7	+.765*	+.528
				8	+.546*	+.377	8	+.337*	+.233	8	+.751*	+.518
				9	+.581*	+.401	9	+.307*	+.212	9	+.676*	+.467
				10	+.493*	+.340	10	+.007*	+.005	10	+.186*	+.128

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.556	-.384	1	-.621	-.429	1	-.620	-.428	1	-.620	-.428	1	-.628	-.433
	2	-.564	-.389	2	-.592	-.409	2	-.622	-.429	2	-.628	-.433			
	3	-.586	-.404	3	-.600	-.414	3	--	--	3	--	--			
	4	-.595	-.411	4	-.584	-.403	4	-.618*	-.427	4	-.614	-.424			
	5	-.594	-.410	5	-.584	-.403	5	-.605	-.418	5	-.600	-.414			
	6	-.594	-.410	6	+.138	+.095	6	-.600	-.414	6	-.600	-.414			
	7	-.594	-.410	7	-.584	-.403	7	-.592	-.409	7	-.580	-.400			
	8	-.582	-.402	8	-.579	-.400	8	-.297	-.205	8	-.569	-.393			
	9	-.575	-.397	9	-.579	-.400	9	-.576	-.498	9	-.580	-.400			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	-.575	-.397	1	-.600	-.414	1	-.737	-.509	1	-.770	-.531	1	-.974	-.672
	2	-.582	-.402	2	-.669	-.462	2	-.623	-.430	2	-.660	-.456	2	-.779	-.538
	3	--	--	3	-.633	-.440	3	-.619	-.427	3	-.606	-.418	3	-.676	-.467
	4	-.612	-.422	4	-.600	-.414	4	-.640*	-.442	4	-.641	-.442	4	-.688	-.475
				5	-.558	-.385	5	-.644*	-.444	5	-.641	-.442	5	-.756	-.522
				6	-.575	-.397	6	-.658	-.454	6	-.641	-.442	6	-.694	-.479
				7	-.597	-.412	7	-.677	-.467	7	-.686	-.473	7	-.718*	-.496
				8	-.596	-.411	8	-.630	-.435	8	-.652	-.450	8	-.641	-.442
							9	-.715	-.494	9	-.494	-.301			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.483	-.333	1	-.084	-.058	1	-.567	-.391
	2	-.349	-.241	2	-.325	-.224	2	-.500	-.345
	3	-.237	-.164	3	-.308	-.213	3	-.326	-.225
	4	-.083	-.057	4	-.228	-.157	4	-.233	-.161
	5	-.114	-.079	5	-.169	-.117	5	-.345*	-.238
	6	-.081	-.056	6	-.138*	-.095	6	-.911*	-.629
	7	+.040	+.028	7	-.064*	-.044	7	-1.120*	-.773
	8	+.075	+.052	8	-.266*	-.184			
	9	-.161	-.111	9	-.878**	-.606			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p
	1	+.159*	+.110	1	+.150*	+.104	1	+.365	+.252	1	+.551	+.380
	2	+.300*	+.207	2	+.263*	+.182	2	+.437	+.302	2	+.717	+.495
	3	+.340*	+.235	3	+.292*	+.202	3	+.470	+.324			
	4	+.311*	+.215	4	+.286*	+.197						
	5	+.311*	+.215									

MISC.

DE	ΔP	C_p
1	+.851	+.587
2	+.772	+.533
3	+.658	+.454

BC 9 -.658 -.454

DATE 5-1-72 WIND DIRECTION: 160° Δh = 1.844 mm Hg P_A = 24.8 in. Hg WIND SPEED: 73.33 fps

TIME 9:00 a.m. Building II T = 60°F ρ_A = 0.00196 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.607	-.419	1	-.679	-.469	1	-.873	-.603	1	-.725	-.500
	2	-.384	-.265	2	-.470	-.324	2	-.468	-.323	2	-.341	-.235
	3	-.328	-.226	3	-.420	-.290	3	-.380	-.262	3	-.174*	-.120
	4	--	--	4	-.367	-.253	4	-.324	-.224	4	-.108*	-.075
	5	-.271	-.187	5	-.316	-.218	5	-.266	-.184	5	+.010*	+.007
	6	-.158	-.109	6	-.178	-.123	6	-.145	-.100	6	+.310*	+.214
	7	-.162	-.112	7	-.246	-.170	7	-.260	-.178	7	-.168*	-.116
	8	-.161	-.111	8	-.216*	-.149	8	-.185	-.128	8	+.100*	+.069
	9	-.160	-.110	9	-.214*	-.148	9	-.152	-.105	9	+.104*	+.072
	10	-.150*	-.104	10	-.162*	-.112	10	-.020*	-.014	10	+.154*	+.106
	11	-.155*	-.107	11	-.134*	-.092	11	-.010*	-.007	11	+.270*	+.186
	12	-.176*	-.121	12	-.095*	-.066	12	+.016*	+.011	12	+.390*	+.269
	13	-.178*	-.123	13	-.095*	-.066	13	+.068*	+.047	13	+.472*	+.326
	14	-.224*	-.155	14	-.100*	-.069	14	+.062*	+.043	14	+.512*	+.353
	15	--	--	15	-.760	-.525	15	--	--	15	+.536*	+.370

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.384*	-.265	1	+.412	+.284	1	-.225*	-.155	1	-.042	-.029
	2	-.324*	-.224	2	-.301	-.208	2	-.163*	-.113	2	+.263*	+.182
	3	-.253*	-.175	3	-.268	-.185	3	-.109	-.075	3	+.297*	+.205
	4	-.184	-.127	4	-.170	-.117	4	-.052	-.036	4	+.424*	+.293
	5	-.064	-.044	5	-.113	-.078	5	+.019	+.013	5	+.531	+.367
				6	+.053	+.037	6	+.103	+.071	6	+.644	+.444
				7	+.601	+.415	7	+.193	+.133	7	+.693	+.478
				8	+.435*	+.300	8	+.218	+.150	8	+.679	+.469
				9	+.500*	+.345	9	+.189	+.130	9	+.641*	+.442
				10	+.448*	+.309	10	-.072	-.050	10	+.150*	+.104

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.619	-.427	1	-.695	-.480	1	-.725	-.500	1	-.730	-.504	1	-.790	-.545
	2	-.626	-.432	2	-.635	-.438	2	-.718	-.496	2	-.730	-.504			
	3	-.646	-.446	3	-.667	-.460	3	--	--	3	--	--			
	4	-.658	-.454	4	-.645	-.445	4	-.717	-.495	4	-.714	-.493			
	5	-.658	-.454	5	-.668	-.461	5	-.690	-.476	5	-.700	-.483			
	6	-.662	-.457	6	-.244	-.168	6	-.690	-.476	6	-.680	-.470			
	7	-.662	-.457	7	-.668	-.461	7	-.672	-.464	7	-.673	-.465			
	8	-.641	-.442	8	-.667	-.460	8	-.120	-.083	8	-.662	-.457			
	9	-.640	-.442	9	-.653	-.451	9	-.673	-.465	9	-.661	-.456			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	-.672	-.464	1	-.612	-.422	1	-.753	-.520	1	-.796	-.549	1	-.882	-.609
	2	-.693*	-.478	2	-.688	-.475	2	-.674	-.465	2	-.704	-.486	2	-.710	-.490
	3	--	--	3	-.668	-.461	3	-.658	-.454	3	-.637	-.440	3	-.615	-.424
	4	-.694	-.479	4	-.672	-.464	4	-.669	-.462	4	-.662	-.457	4	-.654	-.451
				5	-.650	-.449	5	-.688	-.475	5	-.664	-.458	5	-.692	-.478
				6	-.667	-.460	6	-.700	-.483	6	-.664	-.458	6	-.680	-.469
				7	-.700	-.483	7	-.726	-.501	7	-.700	-.483	7	-.707	-.488
				8	-.700	-.483	8	-.680	-.469	8	-.694	-.479	8	-.654	-.451
							9	-.800	-.552	9	-.615	-.424			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.467	-.322	1	+.500	+.345	1	-.582	-.402
	2	-.284	-.196	2	-.311	-.215	2	-.470	-.324
	3	-.124	-.086	3	-.228	-.157	3	-.288	-.199
	4	+.040	+.028	4	-.127	-.088	4	-.178	-.123
	5	+.057	+.039	5	-.039	-.027	5	-.142	-.098
	6	+.085	+.059	6	+.010	+.007	6	-.146*	-.101
	7	+.236	+.163	7	+.103	+.071	7	-.670*	-.462
	8	+.345	+.238	8	+.242*	+.167			
	9	+.400	+.276	9	+.162*	+.112			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p
	1	-.073*	-.050	1	-.080	-.055	1	+.146	+.101	1	+.437*	+.302
	2	+.070*	+.048	2	.000	0	2	+.246*	+.170	2	+.584*	+.403
	3	+.100*	+.069	3	+.080*	+.055	3	+.300*	+.207			
	4	+.098*	+.068	4	+.131	+.090						
	5	+.116	+.080									

MISC.

DE	ΔP	C_p
1	+.800*	+.552
2	+.800*	+.552
3	+.700*	+.483

BC	9	-.726*	-.501

DATE 5-9-72 WIND DIRECTION: 170° Δh = 1.844 mm Hg P_A = 24.815 in. Hg WIND SPEED: 73.33 fps

TIME 3:00 p.m. Building II T = 60°F ρ_A = 0.00196 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.580	-.400	1	-.661	-.456	1	-.833	-.575	1	-.670	-.462
	2	-.404	-.279	2	-.472	-.326	2	-.464	-.320	2	-.290	-.200
	3	-.350	-.242	3	-.435	-.300	3	-.386	-.266	3	-.136	-.094
	4	--	--	4	-.385	-.266	4	-.339	-.234	4	-.070	-.048
	5	-.318	-.219	5	-.362	-.250	5	-.290	-.200	5	+.004*	+.003
	6	-.240	-.166	6	-.268	-.185	6	-.184	-.127	6	+.377*	+.260
	7	-.250	-.173	7	-.332	-.229	7	-.300	-.207	7	-.095*	-.066
	8	-.240	-.166	8	-.300	-.207	8	-.228	-.157	8	+.078*	+.054
	9	-.265	-.183	9	-.305	-.211	9	-.201	-.139	9	+.107*	+.074
	10	-.265	-.183	10	-.275	-.190	10	-.063	-.043	10	+.194*	+.134
	11	-.279	-.193	11	-.246	-.170	11	-.046	-.032	11	+.318*	+.219
	12	-.310	-.214	12	-.196	-.135	12	+.006	+.004	12	+.454*	+.314
	13	-.296	-.204	13	-.196	-.135	13	+.060	+.041	13	+.590*	+.409
	14	-.337	-.233	14	-.200	-.138	14	+.069	+.048	14	+.670*	+.464
	15	--	--	15	-.145	-.100	15	--	--	15	+.737*	+.511

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.625	-.433	1	+.604	+.419	1	-.341*	-.236	1	-.534*	-.370
	2	-.572	-.397	2	-.376*	-.261	2	-.305*	-.211	2	+.012*	+.008
	3	-.511	-.354	3	-.364*	-.252	3	-.263*	-.182	3	+.118*	+.082
	4	-.377	-.261	4	-.257*	-.178	4	-.211*	-.146	4	+.265*	+.184
	5	-.226*	-.157	5	-.222	-.154	5	-.105*	-.073	5	+.374*	+.259
				6	-.100*	-.069	6	0*	0	6	+.530*	+.367
				7	+.455	+.315	7	+.092*	+.064	7	+.654*	+.453
				8	+.269*	+.186	8	+.158*	+.110	8	+.662*	+.459
				9	+.386*	+.268	9	+.140*	+.097	9	+.595*	+.412
				10	+.384*	+.266	10	-.084*	-.058	10	+.156*	+.108

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.612	-.424	1	-.718	-.498	1	-.726	-.503	1	-.755	-.523	1	-.908	-.629
	2	-.612	-.424	2	-.688	-.477	2	-.731	-.507	2	-.764	-.530			
	3	-.630	-.437	3	-.682	-.473	3	--	--	3	--	--			
	4	-.662	-.459	4	-.653	-.453	4	-.730	-.506	4	-.734	-.509			
	5	-.673	-.467	5	-.678	-.470	5	-.710	-.492	5	-.718	-.498			
	6	-.668	-.463	6	-.326	-.226	6	-.700	-.485	6	-.686	-.476			
	7	-.664	-.460	7	-.672	-.466	7	-.700	-.485	7	-.683	-.473			
	8	-.647	-.449	8	-.677	-.469	8	+.370	+.256	8	-.676	-.469			
	9	-.657	-.455	9	-.666	-.462	9	-.670	-.464	9	-.656	-.455			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	-.738	-.512	1	-.564	-.391	1	-.724	-.502	1	-.750	-.520	1	-.792	-.549
	2	-.742	-.514	2	-.670	-.464	2	-.650	-.451	2	-.672	-.466	2	-.665	-.461
	3	--	--	3	-.685	-.475	3	-.652	-.452	3	-.605	-.419	3	-.582	-.403
	4	-.700	-.485	4	-.670	-.464	4	-.655	-.454	4	-.640	-.444	4	-.602	-.417
				5	-.674	-.467	5	-.660	-.458	5	-.634	-.440	5	-.665	-.461
				6	-.715	-.496	6	-.677	-.469	6	-.635	-.440	6	-.640	-.444
				7	-.729	-.505	7	-.710	-.492	7	-.671	-.465	7	-.670	-.464
				8	-.724	-.502	8	-.672	-.466	8	-.657	-.455	8	-.628	-.435
							9	-.796	-.552	9	-.552	-.383			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.421	-.292	1	+.600	+.416	1	-.535	-.371
	2	-.244	-.169	2	-.242	-.168	2	-.416	-.288
	3	-.052*	-.036	3	-.158	-.110	3	-.231*	-.160
	4	+.104*	+.072	4	-.044*	-.031	4	-.120*	-.083
	5	-.132*	-.092	5	+.044*	+.031	5	-.075*	-.052
	6	+.174*	+.121	6	+.110*	+.076	6	+.030*	+.021
	7	+.200*	+.139	7	+.208*	+.144	7	-.100*	-.069
	8	+.400*	+.277	8	+.358*	+.248			
	9	+.450*	+.312	9	+.374*	+.359			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p
	1	-.300*	-.207	1	-.258*	-.179	1	-.021*	-.015	1	+.258*	+.179
	2	-.159*	-.110	2	-.196*	-.136	2	+.060*	+.042	2	+.438*	+.304
	3	-.105*	-.073	3	-.117*	-.081	3	+.162*	+.112			
	4	-.104*	-.072	4	-.051*	-.035						
	5	-.092*	-.064									

MISC.

DE	ΔP	C_p
1	+.756	+.524
2	+.800	+.554
3	+.700	+.485

BC 9 -.746 -.517

DATE 5-3-72 WIND DIRECTION: 180° Δh = 1.844 mm Hg P_A = 24.82 in. Hg WIND SPEED: 73.33 fps

TIME 11:30 a.m. Building II T = 60°F ρ_A = 0.00196 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-.629	-.436	1	-.722	-.500	1	-.910	-.631	1	-.611	-.424
	2	-.384*	-.266	2	-.470	-.326	2	-.420	-.291	2	-.077*	-.053
	3	-.306	-.212	3	-.415	-.288	3	-.328	-.227	3	+.106*	+.073
	4	--	--	4	-.350*	-.243	4	-.252	-.175	4	+.200	+.139
	5	-.276*	-.191	5	-.287*	-.199	5	-.178	-.123	5	+.323	+.224
	6	-.120*	-.083	6	-.150*	-.104	6	-.060*	-.042	6	+.700	+.485
	7	-.116*	-.080	7	-.197	-.137	7	-.204	-.141	7	+.244	+.169
	8	-.096*	-.067	8	-.179*	-.124	8	-.104	-.072	8	+.360	+.250
	9	-.114*	-.079	9	-.174*	-.121	9	-.061*	-.042	9	+.406	+.281
	10	-.094*	-.065	10	-.114*	-.079	10	+.116	+.080	10	+.520	+.360
	11	-.082*	-.057	11	-.005*	-.003	11	+.220	+.153	11	+.652	+.452
	12	-.084*	-.058	12	+.054*	+.037	12	+.364	+.252	12	+.764	+.530
	13	-.090*	-.062	13	+.070*	+.049	13	+.471	+.327	13	+.824	+.571
	14	-.100*	-.069	14	+.104*	+.072	14	+.541	+.375	14	+.900	+.624
	15	--	--	15	+.143	+.099	15	--	--	15	+.946	+.656

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.101*	-.070	1	+.262*	+.182	1	-.363	-.252	1	-.596	-.413
	2	-.100*	-.069	2	-.230*	-.159	2	-.365	-.253	2	-.408	-.283
	3	+.085*	+.059	3	-.236*	-.164	3	-.384	-.266	3	-.320	-.222
	4	+.100*	+.069	4	-.274*	-.190	4	-.530	-.367	4	-.314	-.218
	5	+.107*	+.074	5	-.312*	-.216	5	-.406	-.281	5	-.063*	-.044
				6	-.134*	-.093	6	+.038*	+.026	6	+.510	+.354
				7	+.080*	+.055	7	+.317*	+.220	7	+.789	+.547
				8	+.365*	+.253	8	+.364*	+.252	8	+.796	+.552
				9	+.468	+.324	9	+.315*	+.218	9	+.724	+.502
				10	+.488	+.338	10	+.013*	+.009	10	+.224	+.155

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.685	-.475	1	-.800	-.555	1	-.830	-.575	1	-.877	-.608	1	-1.110	-.769
	2	-.688	-.477	2	-.747	-.518	2	-.830	-.575	2	-.900	-.624			
	3	-.698	-.484	3	-.762	-.528	3	--	--	3	--	--			
	4	-.721	-.500	4	-.763	-.529	4	-.800	-.555	4	-.858	-.595			
	5	-.740	-.513	5	-.757	-.525	5	-.800	-.555	5	-.800	-.555			
	6	-.730	-.506	6	-.554	-.384	6	-.800	-.555	6	-.800	-.555			
	7	-.730	-.506	7	-.756	-.524	7	-.780	-.541	7	-.777	-.539			
	8	-.728	-.505	8	-.753	-.522	8	-.400	-.277	8	-.770	-.534			
	9	-.716	-.496	9	-.736	-.510	9	-.762	-.528	9	-.754	-.523			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	-.810	-.562	1	-.636	-.441	1	-.830	-.575	1	-.835	-.579	1	-.866	-.600
	2	-.808	-.560	2	-.750	-.520	2	-.734	-.509	2	-.757	-.525	2	-.776	-.538
	3	--	--	3	-.746	-.517	3	-.728	-.505	3	-.707	-.490	3	-.654	-.453
	4	-.788	-.546	4	-.780	-.541	4	-.733	-.508	4	-.721	-.500	4	-.680	-.471
				5	-.774	-.537	5	-.744	-.516	5	-.728	-.505	5	-.754	-.523
				6	-.788	-.546	6	-.780	-.541	6	-.728	-.505	6	-.696	-.482
				7	-.800	-.555	7	-.802	-.556	7	-.756	-.524	7	-.734	-.509
				8	-.796	-.552	8	-.760	-.527	8	-.748	-.519	8	-.692	-.480
							9	-.922	-.639	9	-.636	-.441			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.285*	-.198	1	+.430	+.298	1	-.479	-.332
	2	-.015*	-.010	2	-.115*	-.098	2	-.314	-.218
	3	+.182*	+.126	3	+.017*	+.012	3	-.116*	-.080
	4	+.354*	+.245	4	+.150*	+.104	4	0*	0
	5	+.396*	+.275	5	+.258*	+.179	5	+.074*	+.051
	6	+.435	+.302	6	+.323*	+.224	6	+.215*	+.149
	7	+.550	+.381	7	+.430*	+.298	7	+.262*	+.182
	8	+.610	+.423	8	+.548*	+.380			
	9	+.614	+.426	9	+.578*	+.401			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p	MISC. DE	ΔP	C_p
	1	+.007*	+.005	1	-.067*	-.046	1	-.006*	-.004	1	+.302*	+.209	1	+.426*	+.295
	2	+.036*	+.025	2	-.094*	-.065	2	+.033*	+.023	2	+.486*	+.337	2	+.864	+.599
	3	+.004*	+.003	3	-.130*	-.090	3	+.120*	+.083				3	+.895	+.620
	4	-.141*	-.098	4	-.116*	-.080									
	5	-.160*	-.111												
													BC 9	-.840	-.582

DATE 4-9-72 WIND DIRECTION: 340° Δh = 1.830 mm Hg P_A = 24.62 in. Hg WIND SPEED: 73.33 fps

TIME 1:00 p.m. Building II T = 60° ρ_A = 0.001895 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-1.324*	-.921	1	-1.300	-.904	1	-1.162	-.808	1	-1.040	-.723
	2	-1.336*	-.929	2	-1.296	-.901	2	-1.174	-.817	2	-1.040	-.723
	3	-1.336*	-.929	3	-1.302	-.906	3	-1.180	-.820	3	-1.055	-.734
	4	--	--	4	-1.334	-.928	4	-1.176	-.818	4	-1.088	-.757
	5	-1.310	-.911	5	-1.312	-.912	5	-1.176	-.817	5	-1.056	-.734
	6	-1.084	-.754	6	-1.252	-.871	6	-1.185	-.773	6	-1.043	-.725
	7	-1.074	-.747	7	-1.256	-.874	7	-1.198	-.833	7	-1.100	-.765
	8	-1.056	-.734	8	-1.280	-.890	8	-1.206	-.839	8	-1.136	-.790
	9	-.900	-.626	9	-1.280	-.890	9	-1.208	-.840	9	-1.136	-.790
	10	-.720	-.501	10	-1.146	-.797	10	-1.202	-.836	10	-1.130	-.786
	11	-.620	-.431	11	-1.000	-.695	11	-1.162	-.808	11	-1.086	-.755
	12	-.554	-.385	12	-.850*	-.591	12	-1.118	-.776	12	-1.072	-.746
	13	-.518	-.360	13	-.833*	-.579	13	-1.066	-.741	13	-1.056	-.734
	14	-.534	-.371	14	-.800	-.556	14	-1.050	-.730	14	-1.056	-.734
	15	--	--	15	--	--	15	--	--	15	-1.064	-.740

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.700	-.487	1	-.617	-.429	1	-.858	-.597	1	-.838	-.583
	2	-.658	-.458	2	-.800	-.556	2	-.864	-.601	2	-.858	-.597
	3	-.684	-.476	3	-.790	-.549	3	-.864	-.601	3	-.900	-.626
	4	-.736	-.512	4	-.778	-.541	4	-.921	-.641	4	-.930	-.647
	5	-.766	-.533	5	-.795	-.553	5	-.990	-.689	5	-.948	-.659
				6	-.805	-.560	6	-1.046	-.727	6	-.924	-.643
				7	-.389	-.271	7	-1.102	-.766	7	-.917	-.638
				8	-.830	-.577	8	-1.059	-.737	8	-.900	-.626
				9	-.852	-.593	9	-1.056	-.734	9	-.892	-.620
				10	-1.352	-.940	10	-1.056	-.734	10	-.884	-.615

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	+.200*	+.139	1	+.267*	+.186	1	+.600*	+.417	1	+.850	+.591	1	+.719*	+.500
	2	+.200*	+.139	2	+.294*	+.204	2	+.583*	+.405	2	+.850	+.591			
	3	+.232*	+.161	3	+.314*	+.218	3	--	--	3	+1.579	+1.098			
	4	+.232*	+.161	4	+.274*	+.191	4	+.480*	+.334	4	+.660*	+.459			
	5	+.215*	+.150	5	+.228*	+.159	5	+.396	+.275	5	+.518*	+.360			
	6	+.114*	+.097	6	+.244*	+.170	6	+.246	+.171	6	+.426*	+.296			
	7	-.028*	-.019	7	+.018*	+.013	7	+.146	+1.015	7	+.218*	+.152			
	8	-.271*	-.188	8	-.224*	-.156	8	+.484	+.337	8	-.058*	-.040			
	9	-.538	-.374	9	-.495	-.344	9	-.529	-.368	9	-.502*	-.349			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	+.600*	+.417	1	-.434*	-.302	1	-.514*	-.357	1	-.382*	-.266	1	-.561	-.390
	2	+.576*	+.401	2	+.352*	+.245	2	+.150*	+.104	2	+.258*	+.179	2	-.170*	-.118
	3	--	--	3	+.734*	+.510	3	+.596*	+.415	3	+.700*	+.487	3	+.242*	+.168
	4	+.300*	+.209	4	+.800*	+.556	4	+.746*	+.519	4	+.868*	+.604	4	+.372*	+.259
				5	+.770*	+.536	5	+.786*	+.547	5	+.934*	+.650	5	+.502*	+.349
				6	+.667*	+.464	6	+.773*	+.538	6	+.965*	+.671	6	+.588*	+.409
				7	+.623*	+.433	7	+.800*	+.556	7	+.963*	+.670	7	+.700*	+.487
				8	+.609*	+.424	8	+.807*	+.561	8	+1.036*	+.721	8	+.816*	+.568
							9	+.745*	+.578	9	+1.061*	+.738			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.976	-.679	1	-.800	-.556	1	-1.028	-.715
	2	-.983	-.684	2	-.922	-.641	2	-1.036	-.721
	3	-1.032	-.718	3	-1.016	-.707	3	-1.028	-.715
	4	-1.076	-.748	4	-1.043	-.725	4	-1.010	-.702
	5	-1.090	-.758	5	-1.060	-.737	5	-1.030	-.716
	6	-1.086	-.755	6	-1.069	-.743	6	-1.060	-.737
	7	-1.056	-.734	7	-1.055	-.734	7	-1.092	-.759
	8	-1.075	-.748	8	-1.062	-.739			
	9	-1.100	-.765	9	-1.081	-.752			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p
	1	-0.640*	-.445	1	-.724*	-.504	1	-.770*	-.536	1	-.742	-.516
	2	-.706*	-.491	2	-.738*	-.513	2	-.757*	-.526	2	-.731	-.508
	3	-.750*	-.522	3	-.771*	-.536	3	-.735*	-.511			
	4	-.793*	-.552	4	-.764*	-.531						
	5	-.775*	-.539									

MISC.

DE	ΔP	C_p
1	-.927*	-.645
2	-.902*	-.627
3	-.903*	-.628

BC 9 +.528* +.367

DATE 4-8-72 WIND DIRECTION: 350° Δh = 1.844 mm Hg P_A = 24.800 in. Hg WIND SPEED: 73.33 fps

TIME 12:30 p.m. Building II T = 60°F ρ_A = 0.00191 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-1.386*	-.957	1	-1.340*	-.925	1	-1.200	-.069	1	-1.143	-.789
	2	-1.418*	-.979	2	-1.353	-.934	2	-1.200	-.069	2	-1.150	-.794
	3	-1.426*	-.984	3	-1.353	-.934	3	-1.217	-.840	3	-1.150	-.794
	4	--	--	4	-1.340	-.925	4	-1.229	-.848	4	-1.149	-.793
	5	-1.422*	-.981	5	-1.374*	-.948	5	-1.243	-.858	5	-1.138	-.785
	6	-1.106*	-.763	6	-1.284*	-.886	6	-1.228	-.848	6	-1.106	-.763
	7	-1.150*	-.794	7	-1.306*	-.901	7	-1.255*	-.866	7	-1.106	-.763
	8	-1.156*	-.798	8	-1.306*	-.901	8	-1.258*	-.868	8	-1.168	-.806
	9	-.904*	-.624	9	-1.335*	-.921	9	-1.258*	-.868	9	-1.168	-.806
	10	-.652*	-.450	10	-1.102*	-.761	10	-1.225	-.846	10	-1.168	-.806
	11	-.558*	-.385	11	-.900*	-.621	11	-1.225	-.846	11	-1.161	-.801
	12	-.500	-.345	12	-.800*	-.552	12	-1.160*	-.801	12	-1.165*	-.804
	13	-.448*	-.309	13	-.753*	-.520	13	-1.119*	-.772	13	-1.158*	-.799
	14	-.421*	-.291	14	-.737*	-.509	14	-1.067*	-.736	14	-1.172	-.809
	15	--	--	15	--	--	15	--	--	15	-1.167	-.805

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DE	ΔP	C_p
	1	-.632	-.436	1	-.886	-.612	1	-.924	-.638	1	-.950	-.655
	2	-.658	-.454	2	-.808*	-.558	2	-.924	-.638	2	-.927	-.640
	3	-.667	-.460	3	-.808	-.558	3	-.922	-.636	3	-.940	-.649
	4	-.673	-.465	4	-.766	-.529	4	-.974	-.672	4	-.944	-.652
	5	-.686	-.473	5	-.786	-.543	5	-1.002	-.692	5	-.950	-.656
				6	-.786	-.543	6	-1.083	-.747	6	-.950*	-.656
				7	-.754	-.520	7	-1.120	-.773	7	-.941	-.649
				8	-.795	-.549	8	-1.126	-.777	8	-.933	-.644
				9	-.851	-.587	9	-1.139	-.786	9	-.933	-.644
				10	-1.386	-.957	10	-1.128	-.779	10	-.928	-.641

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	0.00*	0	1	+.002*	+.001	1	+.308	+.213	1	+.505	+.349	1	+.234*	+.162
	2	+.048	+.033	2	+.200*	+.138	2	+.330	+.228	2	+.553	+.382			
	3	+.125	+.086	3	+.208*	+.144	3	--	--	3	--	--			
	4	+.125	+.086	4	+.203*	+.140	4	+.300	+.207	4	+.392	+.271			
	5	+.125	+.086	5	+.112*	+.077	5	+.238*	+.164	5	+.300	+.207			
	6	+.024	+.017	6	+.218	+.150	6	+.130	+.090	6	+.170*	+.117			
	7	-.110	-.076	7	-.100	-.690	7	-.024	-.017	7	0.00*	0			
	8	-.365	-.252	8	-.337	-.233	8	-.200	-.138	8	-.272*	-.188			
	9	-.627	-.433	9	-.620	-.428	9	-.680	-.469	9	-.696*	-.480			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	+.627*	+.433	1	-.500	-.345	1	-.578	-.399	1	+.420*	+.290	1	-.532	-.367
	2	+.502*	+.346	2	+.335	+.231	2	+.100*	+.690	2	+.250*	+.173	2	-.100	-.069
	3	--	--	3	+.656	+.453	3	+.548*	+.378	3	+.719*	+.496	3	+.388*	+.268
	4	+.248*	+.171	4	+.740	+.511	4	+.686*	+.473	4	+.861*	+.594	4	-.508*	-.351
				5	+.664*	+.458	5	+.688*	+.475	5	+.942*	+.651	5	+.626*	+.432
				6	+.632*	+.436	6	+.772*	+.533	6	+.990*	+.683	6	+.796*	+.549
				7	+.602*	+.416	7	+.780*	+.538	7	+1.020*	+.704	7	+.935*	+.645
				8	+.583*	+.402	8	+.780*	+.538	8	+1.048*	+.723	8	+1.055*	+.728
							9	+.768*	+.530	9	+1.114*	+.769			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-1.000*	-.690	1	-.786	-.543	1	-.945	-.652
	2	-1.000*	-.690	2	-.910	-.628	2	-.950	-.656
	3	-1.065*	-.735	3	-1.000	-.690	3	-.978	-.675
	4	-1.092*	-.754	4	-1.011	-.698	4	-.994	-.686
	5	-1.100*	-.759	5	-1.039	-.717	5	-1.042	-.719
	6	-1.129*	-.779	6	-1.042	-.719	6	-1.084	-.748
	7	-1.136*	-.784	7	-1.084	-.748	7	-1.094	-.755
	8	-1.166	-.805	8	-1.098	-.758			
	9	-1.174	-.810	9	-1.131*	-.781			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p
	1	-.579*	-.400	1	-.662*	-.457	1	-.724*	-.500	1	-.730*	-.504
	2	-.676*	-.467	2	-.700*	-.483	2	-.740*	-.511	2	-.726*	-.501
	3	-.697*	-.481	3	-.736*	-.508	3	-.740*	-.511			
	4	-.762*	-.526	4	-.738*	-.509						
	5	-.768*	-.530									

MISC.

DE	ΔP	C_p
1	-.926*	-.639
2	-.926	-.639
3	-.926	-.639

BC 9 +.503 +.347

DATE 4-7-72 WIND DIRECTION: 0° Δh = 1.844 mm Hg P_A = 24.80 in. Hg WIND SPEED: 73.33 fps

TIME 1:30 p.m. Building II T = 60°F ρ_A = 0.00191 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-1.349	-.931	1	-1.274	-.879	1	-1.146	-.791	1	-1.100	-.759
	2	-1.371	-.946	2	-1.300	-.897	2	-1.152	-.795	2	-1.115	-.770
	3	-1.370	-.946	3	-1.300	-.897	3	-1.160	-.801	3	-1.092	-.754
	4	--	--	4	-1.304	-.900	4	-1.180	-.814	4	-1.079	-.744
	5	-1.419	-.979	5	-1.356	-.936	5	-1.184	-.817	5	-1.080	-.745
	6	-1.046	-.722	6	-1.225	-.846	6	-1.180	-.814	6	-1.070	-.739
	7	-1.040	-.718	7	-1.300	-.897	7	-1.220	-.842	7	-1.082	-.747
	8	-1.215	-.839	8	-1.338	-.924	8	-1.210	-.835	8	-1.095	-.756
	9	-.765*	-.528	9	-1.275	-.880	9	-1.244	-.859	9	-1.110	-.766
	10	-.516*	-.356	10	-1.000	-.690	10	-1.170	-.808	10	-1.132	-.781
	11	-.510*	-.352	11	-.726*	-.501	11	-1.134	-.783	11	-1.150	-.794
	12	-.506*	-.349	12	-.622*	-.429	12	-1.010	-.697	12	-1.134	-.7827
	13	-.432*	-.298	13	-.600*	-.414	13	-.965*	-.666	13	-1.102	-.761
	14	-.406*	-.280	14	-.600*	-.414	14	-.940*	-.649	14	-1.128	-.779
	15	--	--	15	--	--	15	--	--	15	-1.090	-.752

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.462	-.319	1	-.567	-.391	1	-.874	-.603	1	-.947	-.654
	2	-.460	-.317	2	-.640	-.442	2	-.848	-.585	2	-.927	-.640
	3	-.490	-.338	3	-.650	-.449	3	-.859	-.593	3	-.915	-.632
	4	-.500	-.345	4	-.650	-.449	4	-.894	-.617	4	-.906	-.625
	5	-.600	-.414	5	-.700	-.483	5	-.979	-.676	5	-.909	-.627
				6	-.683	-.471	6	-1.036	-.715	6	-.903	-.623
				7	-.550	-.380	7	-1.140	-.787	7	-.900	-.621
				8	-.645*	-.445	8	-1.108	-.765	8	-.893	-.616
				9	-.648*	-.447	9	-1.112	-.768	9	-.894	-.617
				10	-1.049	-.724	10	-1.110	-.766	10	-.884	-.610

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.084*	-.058	1	-.020*	-.014	1	+.162*	+.112	1	+.204*	+.141	1	-.298*	-.206
	2	-.023*	-.016	2	+.090*	+.062	2	+.236*	+.163	2	+.300*	+.207			
	3	-.008*	-.006	3	+.072*	+.050	3	--	--	3	--	--			
	4	+.024*	+.017	4	+.038*	+.026	4	+.134*	+.092	4	+.168*	+.116			
	5	0*	0	5	-.010*	-.007	5	+.069*	+.048	5	+.100*	+.069			
	6	-.078*	-.054	6	-.014*	-.010	6	-.059*	-.041	6	-.045*	-.031			
	7	-.198*	-.137	7	-.206*	-.142	7	-.160*	-.110	7	-.190*	-.131			
	8	-.414	-.286	8	-.438	-.302	8	-.407	-.281	8	-.404	-.279			
	9	-.640	-.442	9	-.687	-.474	9	-.762	-.526	9	-.804	-.555			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	+.417*	+.288	1	-.455	-.314	1	-.625*	-.431	1	-.427	-.295	1	-.510*	-.352
	2	+.400*	+.276	2	+.153*	+.106	2	-.006*	-.004	2	+.180*	+.124	2	-.110*	-.076
	3	--	--	3	+.423*	+.292	3	+.364*	+.251	3	+.600*	+.414	3	+.401*	+.277
	4	+.224*	+.155	4	+.476*	+.329	4	+.441*	+.304	4	+.694*	+.479	4	+.600*	+.414
				5	+.450*	+.311	5	+.475*	+.328	5	+.711*	+.491	5	+.830*	+.573
				6	+.412*	+.284	6	+.518*	+.358	6	+.816*	+.563	6	+.959*	+.662
				7	+.378*	+.261	7	+.512	+.353	7	+.857*	+.592	7	+1.105*	+.763
				8	+.400	+.276	8	+.593	+.409	8	+1.004*	+.693	8	+1.214*	+.838
							9	+.649	+.448	9	+1.045*	+.721			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.959*	-.662	1	-.930	-.642	1	-.890	-.614
	2	-.936*	-.646	2	-.835	-.575	2	-.900	-.621
	3	-1.000	-.690	3	-.936	-.646	3	-.957	-.661
	4	-1.029	-.710	4	-.956	-.660	4	-.982	-.678
	5	-1.040	-.718	5	-1.000	-.690	5	-1.000	-.690
	6	-1.076	-.723	6	-1.000	-.690	6	-1.053	-.727
	7	-1.130	-.780	7	-1.028	-.710	7	-1.044	-.721
	8	-1.148	-.792	8	-1.054	-.727			
	9	-1.150	-.794	9	-1.064	-.734			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p	MISC. DE	ΔP	C_p
	1	-.353*	-.244	1	-.508	-.351	1	-.682	-.471	1	-.649	-.448	1	-.880	-.607
	2	-.536*	-.370	2	-.644	-.444	2	-.680	-.469	2	-.613	-.423	2	-.864	-.596
	3	-.570*	-.393	3	-.722	-.498	3	-.660	-.456				3	-.850	-.587
	4	-.700	-.483	4	-.724	-.500									
	5	-.762	-.526												

BC	9	+.389	+.268

DATE 4-7-72 WIND DIRECTION: 10° Δh = 1.844 mm Hg P_A = 24.80 in. Hg WIND SPEED: 73.33 fps

TIME 8:30 a.m. Building II T = 60°F ρ_A = .00191 slugs/ft^3

Building Face

F	FA	ΔP	C_p	FB	ΔP	C_p	FC	ΔP	C_p	FD	ΔP	C_p
	1	-1.29*	-.890	1	-1.155	-.797	1	-1.022	-.705	1	-.910	-.628
	2	-1.342*	-.926	2	-1.184	-.817	2	-1.054	-.727	2	-.941	-.649
	3	-1.41*	-.973	3	-1.228*	-.848	3	-1.058	-.730	3	-.938	-.647
	4	--	--	4	-1.30*	-.897	4	-1.070	-.739	4	-.932	-.643
	5	-1.476*	-1.019	5	-1.408*	-.972	5	-1.120	-.773	5	-.920	-.635
	6	-.528*	-.364	6	-.996*	-.687	6	-1.084	-.748	6	-.922	-.636
	7	-.541*	-.373	7	-1.12*	-.773	7	-1.144	-.790	7	-.913	-.630
	8	-.66*	-.456	8	-1.219*	-.835	8	-1.127	-.778	8	-.964	-.665
	9	-.348*	-.240	9	-.952*	-.657	9	-1.148	-.792	9	-.964	-.665
	10	-.568*	-.392	10	-.726*	-.501	10	-1.074	-.741	10	-1.000	-.690
	11	-.658*	-.454	11	-.642*	-.443	11	-.992	-.685	11	-1.025	-.707
	12	-.658*	-.454	12	-.604*	-.417	12	-.906	-.625	12	-1.028	-.710
	13	-.588*	-.406	13	-.616*	-.425	13	-.848	-.585	13	-1.002	-.692
	14	-.577	-.398	14	-.612	-.422	14	-.826	-.570	14	-1.000	-.690
	15	--	--	15	--	--	15	--	--	15	-.985	-.680

D	DA	ΔP	C_p	DB	ΔP	C_p	DC	ΔP	C_p	DD	ΔP	C_p
	1	-.377*	-.260	1	-.533	-.368	1	-.800	-.552	1	-.930	-.642
	2	-.337*	-.260	2	-.612*	-.422	2	-.787	-.543	2	-.918	-.634
	3	-.36*	-.248	3	-.646*	-.446	3	-.754	-.520	3	- 918	-.634
	4	-.402*	-.277	4	-.676*	-.467	4	-.743	-.513	4	-.912	-.629
	5	-.582*	-.402	5	-.756*	-.522	5	-.778	-.537	5	-.930	-.642
				6	-.702*	-.485	6	-.862	-.595	6	-.936	-.646
				7	-.488	-.337	7	-1.032*	-.712	7	-.940	-.649
				8	-.588	-.406	8	-1.173*	-.810	8	-.936	-.646
				9	-.560	-.387	9	-1.236*	-.853	9	-.922	-.636
				10	-.682	-.471	10	-1.295*	-.894	10	-.922	-.636

S	SA	ΔP	C_p	SB	ΔP	C_p	SC	ΔP	C_p	SD	ΔP	C_p	SE	ΔP	C_p
	1	-.091*	-.063	1	-.064*	-.044	1	-.020*	-.014	1	+.068*	+.047	1	-1.042*	-.719
	2	-.022*	-.015	2	-.018*	-.012	2	0	0	2	+.082*	+.057			
	3	-.070*	-.048	3	-.048*	-.033	3	--	--	3	--	--			
	4	-.051*	-.035	4	-.09*	-.062	4	-.056*	-.039	4	-.052*	-.036			
	5	-.088*	-.061	5	-.12*	-.083	5	-.114*	-.079	5	-.108*	-.075			
	6	-.160*	-.110	6	--	--	6	-.193*	-.133	6	-.205*	-.141			
	7	-.276*	-.190	7	-.318*	-.219	7	-.300*	-.207	7	-.318*	-.219			
	8	-.454*	-.313	8	-.508	-.351	8	-.200*	-.138	8	-.472*	-.326			
	9	-.651*	-.449	9	-.543	-.375	9	-.762	-.526	9	-.762	-.526			

B	BA	ΔP	C_p	BB	ΔP	C_p	BC	ΔP	C_p	BD	ΔP	C_p	BE	ΔP	C_p
	1	+.255*	+.176	1	-.378	-.261	1	-.750	-.518	1	-.534	-.369	1	-.60*	-.414
	2	+.287*	+.198	2	-.065*	-.045	2	-.25*	-.173	2	0	0	2	-.318*	-.219
	3	--	--	3	+.088*	+.061	3	+.030*	+.021	3	+.267*	+.184	3	+.275*	-.190
	4	+.373*	+.257	4	+.109*	+.075	4	+.071*	+.049	4	+.30*	+.207	4	+.616*	+.425
				5	+.092*	+.063	5	+.07*	+.048	5	+.224*	+.155	5	+.970*	+.670
				6	+.092*	+.063	6	+.065*	+.045	6	+.232*	+.160	6	+1.14*	+.787
				7	+.07*	+.048	7	+.038*	+.026	7	+.324*	+.224	7	+1.27*	+.877
				8	+.16*	+.110	8	+.154*	+.106	8	+.587*	+.405	8	+1.345*	+.928
							9	+.216	+.149	9	+.856	+.591			

T	TA	ΔP	C_p	TB	ΔP	C_p	TC	ΔP	C_p
	1	-.86	-.594	1	-.90	-.621	1	-.816	-.563
	2	-.832	-.574	2	-.754	-.520	2	-.826	-.570
	3	-.90	-.621	3	-.845	-.583	3	-.836	-.577
	4	-.915	-.632	4	-.87	-.600	4	-.850	-.587
	5	-.930	-.642	5	-.87	-.600	5	-.881	-.608
	6	-.964	-.665	6	-.885	-.611	6	-.915	-.632
	7	-.986	-.681	7	-.910	-.628	7	-.934	-.645
	8	-1.032	-.712	8	-.936	-.646			
	9	-1.040	-.718	9	-.955	-.659			

G	GA	ΔP	C_p	GB	ΔP	C_p	GC	ΔP	C_p	GD	ΔP	C_p
	1	-.150	-.104	1	-.411	-.284	1	-.734	-.576	1	-.668	-.461
	2	-.341	-.235	2	-.592	-.409	2	-.78	-.538	2	-.656	-.453
	3	-.514	-.355	3	-.842	-.581	3	-.78	-.538			
	4	-.760	-.525	4	-.864	-.596						
	5	-.861	-.594									

MISC.

DE	ΔP	C_p
1	-.838	-.578
2	-.850	-.587
3	-.850	-.587

BC	9	+.180	+.124

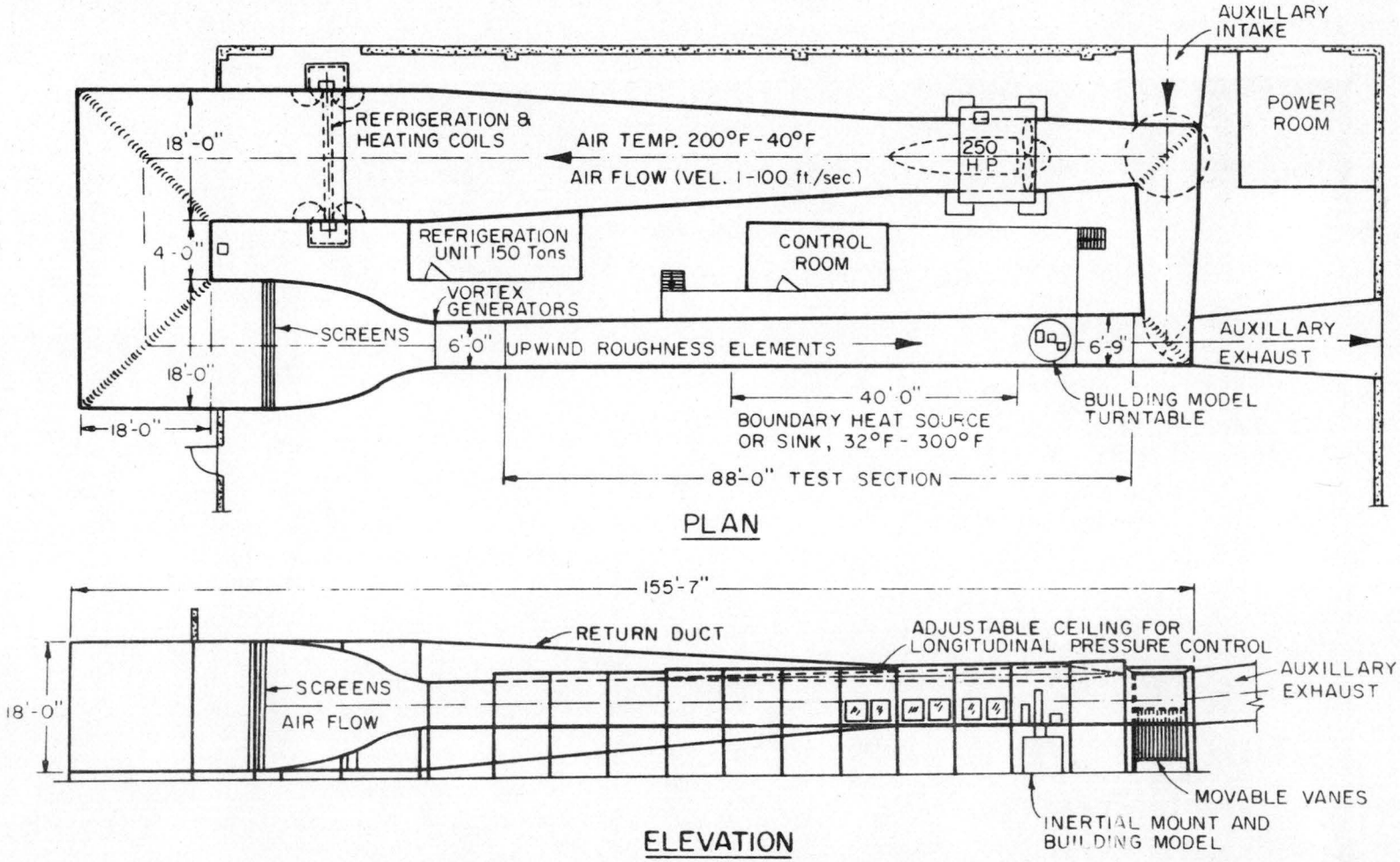

Figure 1. Plan view of meteorological wind tunnel.

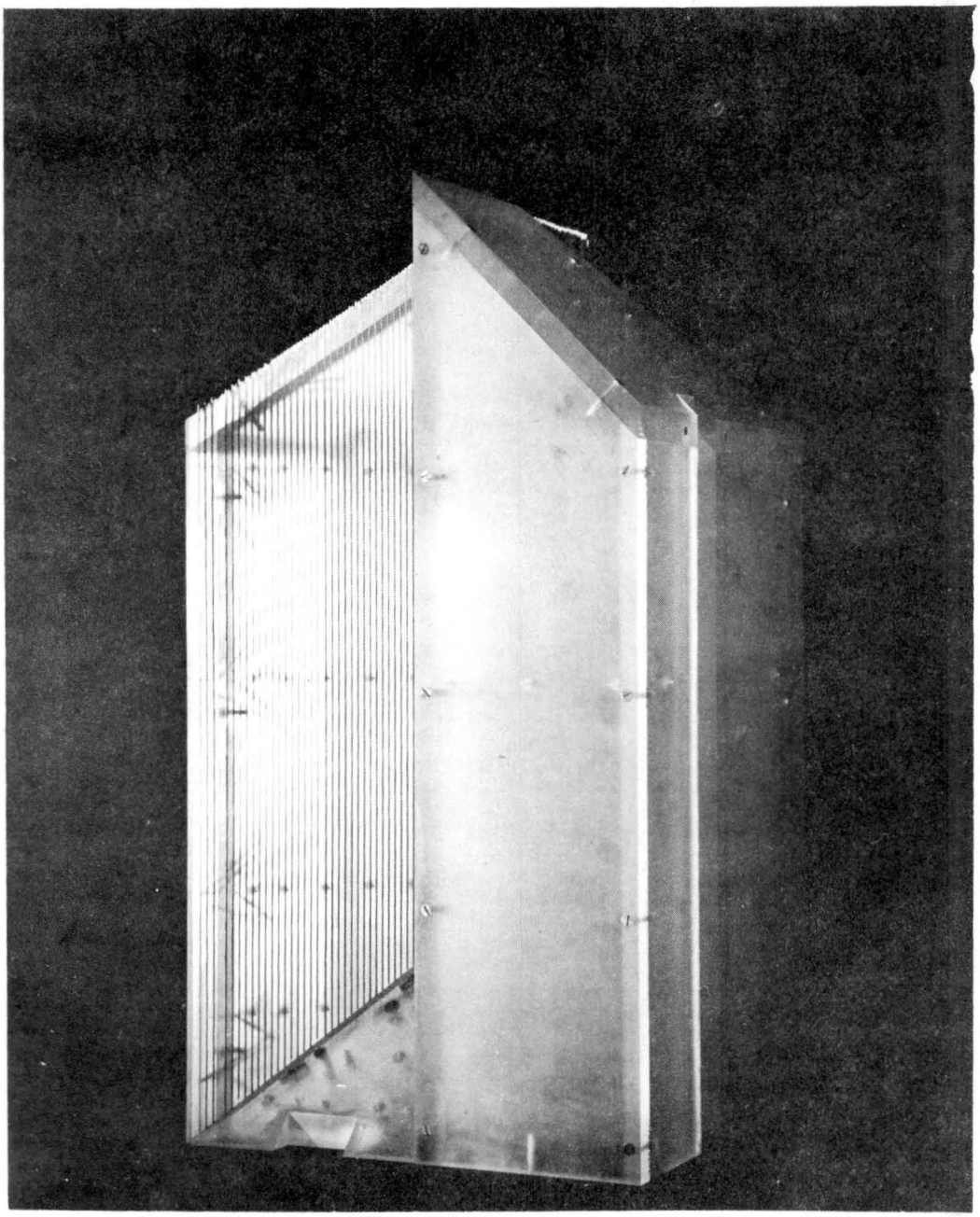

Figure 2. Photograph of the model building.

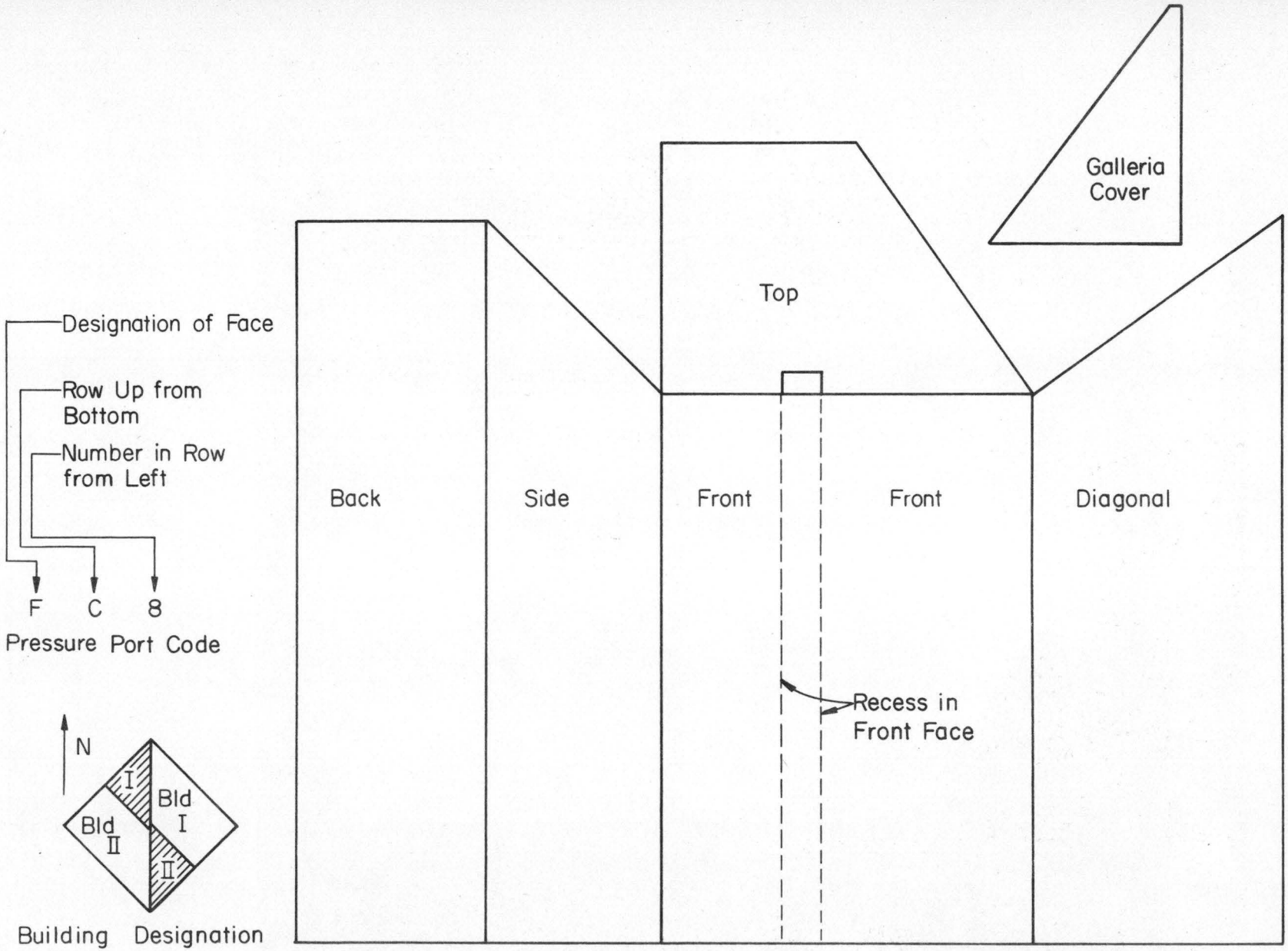

Figure 3. Figure 3a. Pressure tap locations and code.

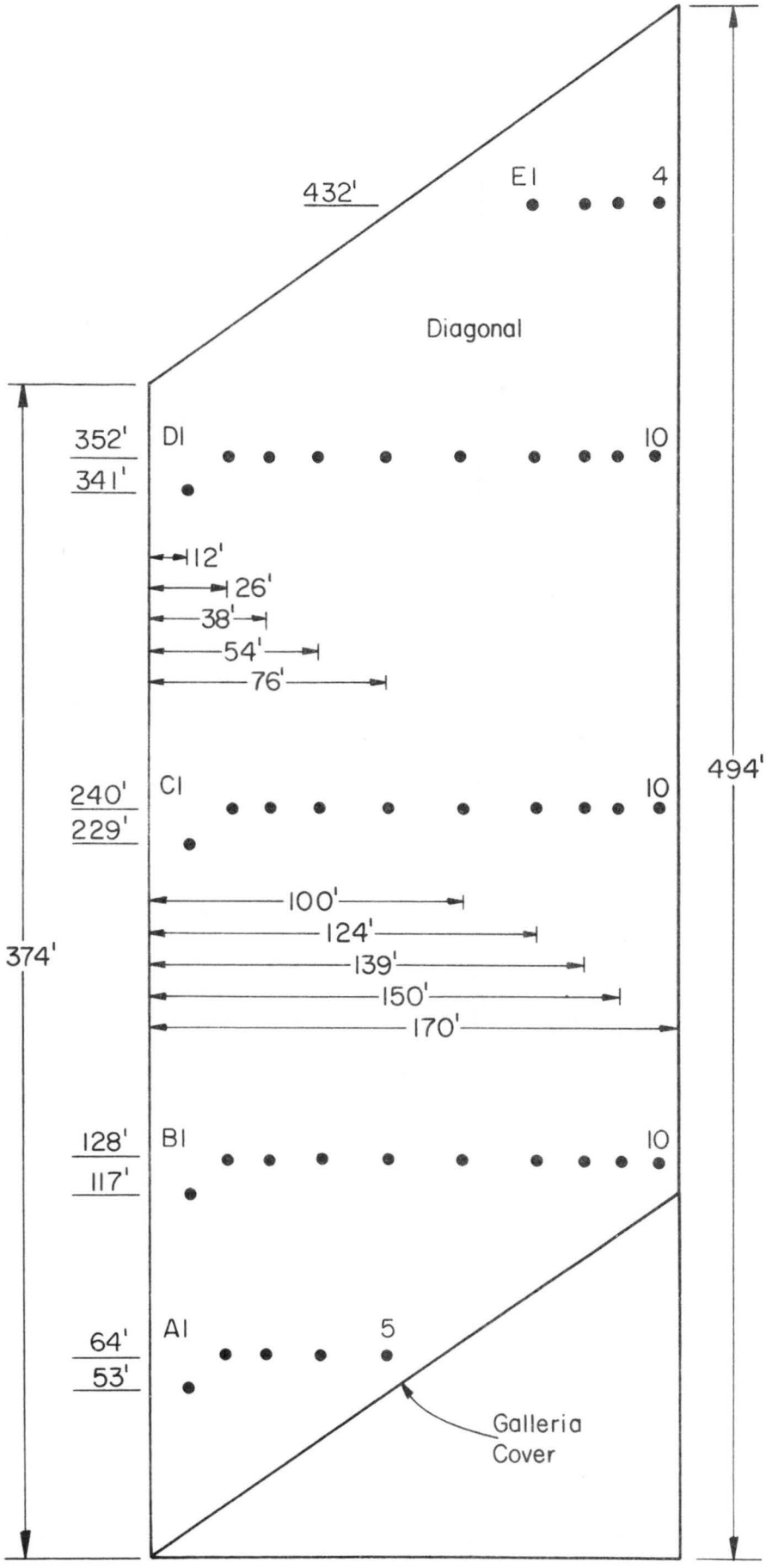

Figure 3b. Pressure tap locations and code.

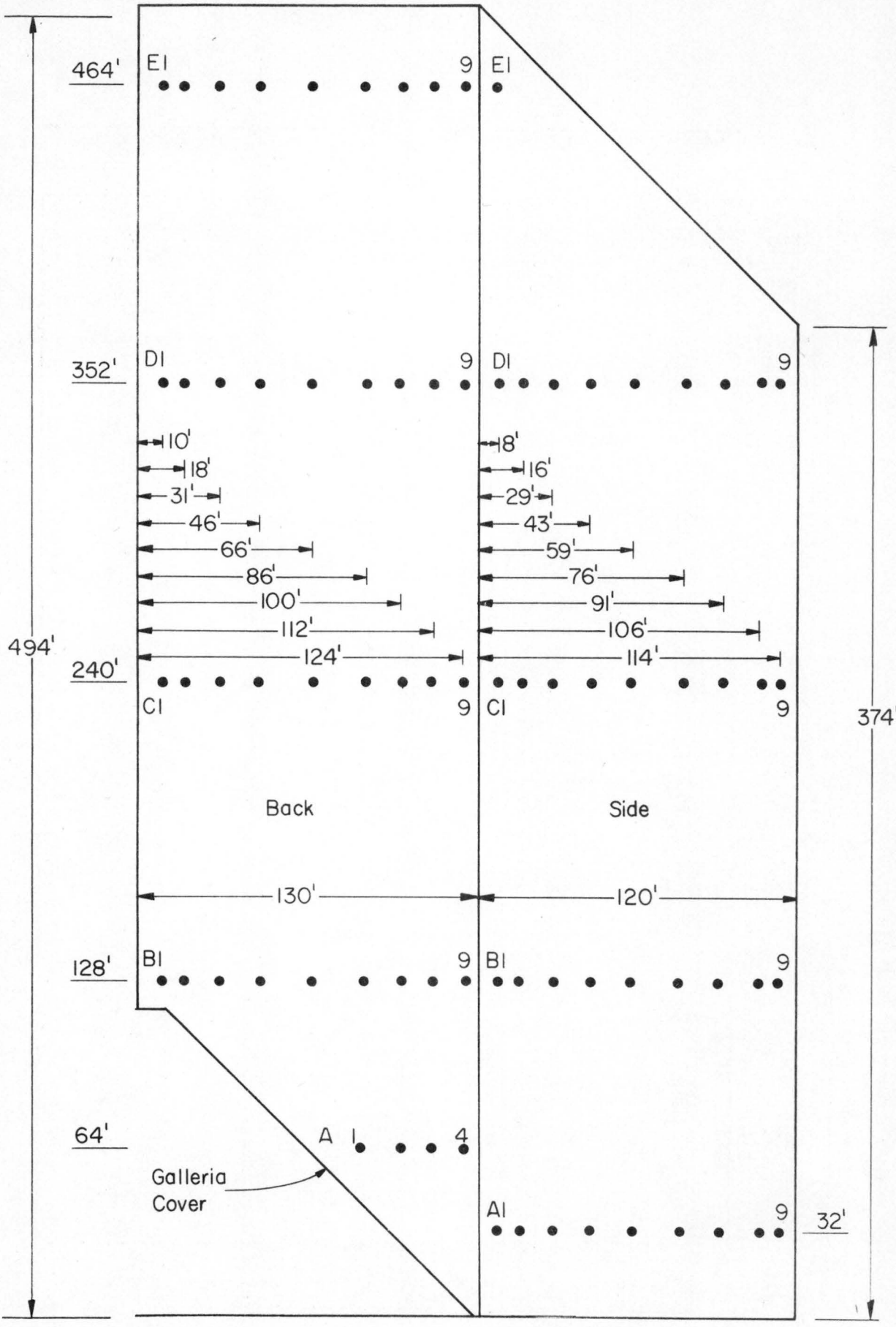

Figure 3c. Pressure tap locations and code.

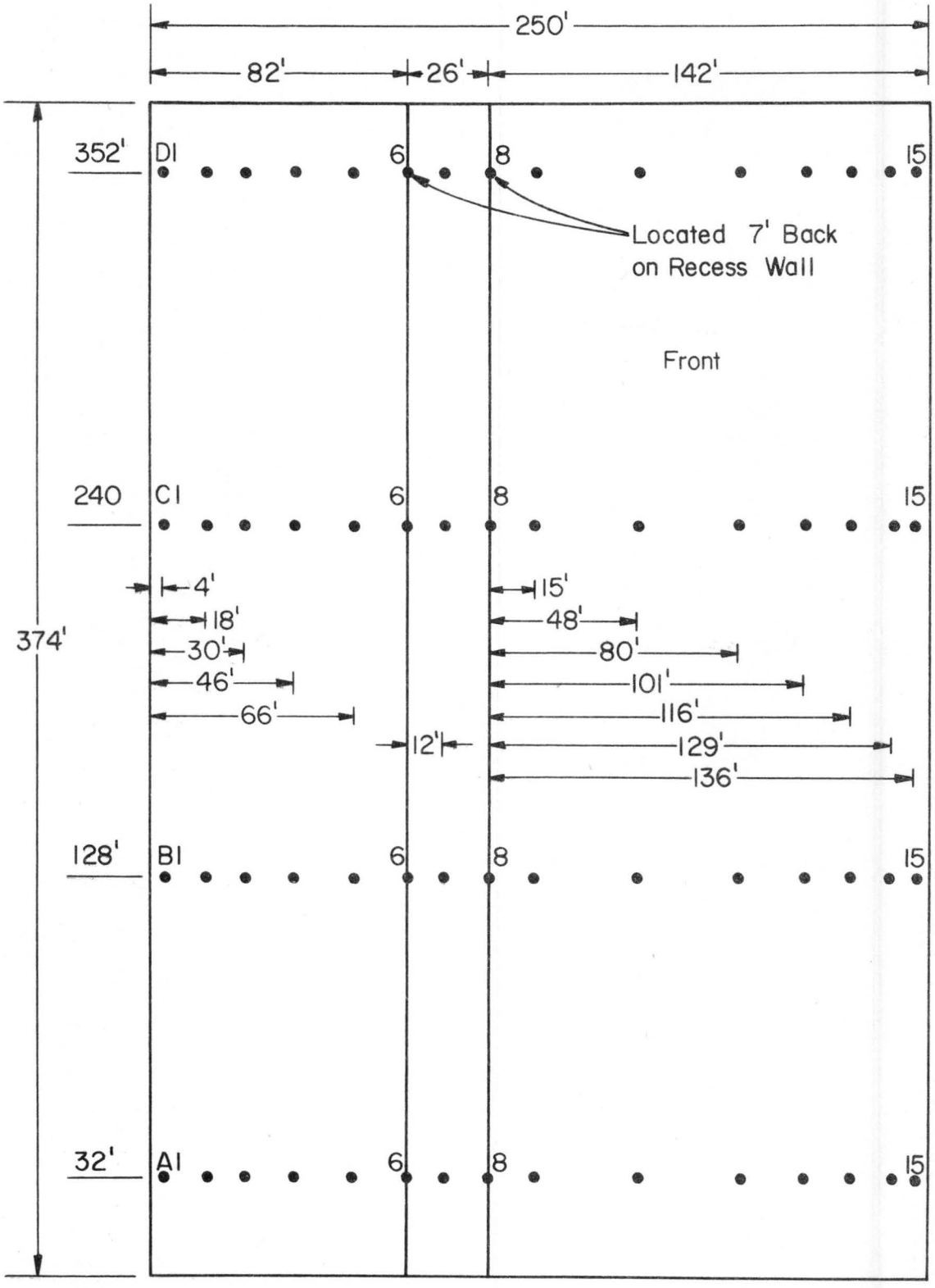

Figure 3d. Pressure tap locations and code.

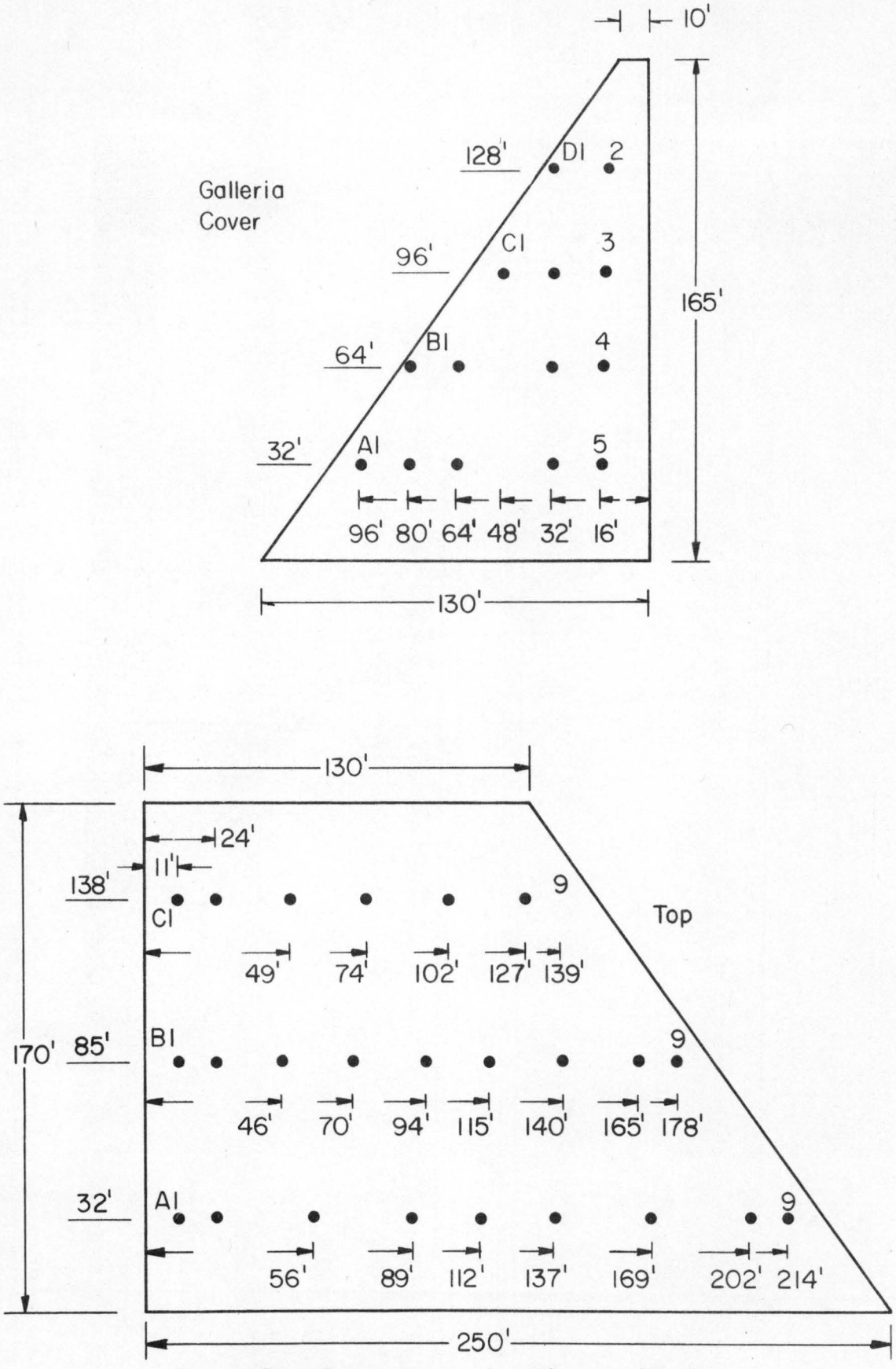

Figure 3e. Pressure tap locations and code.

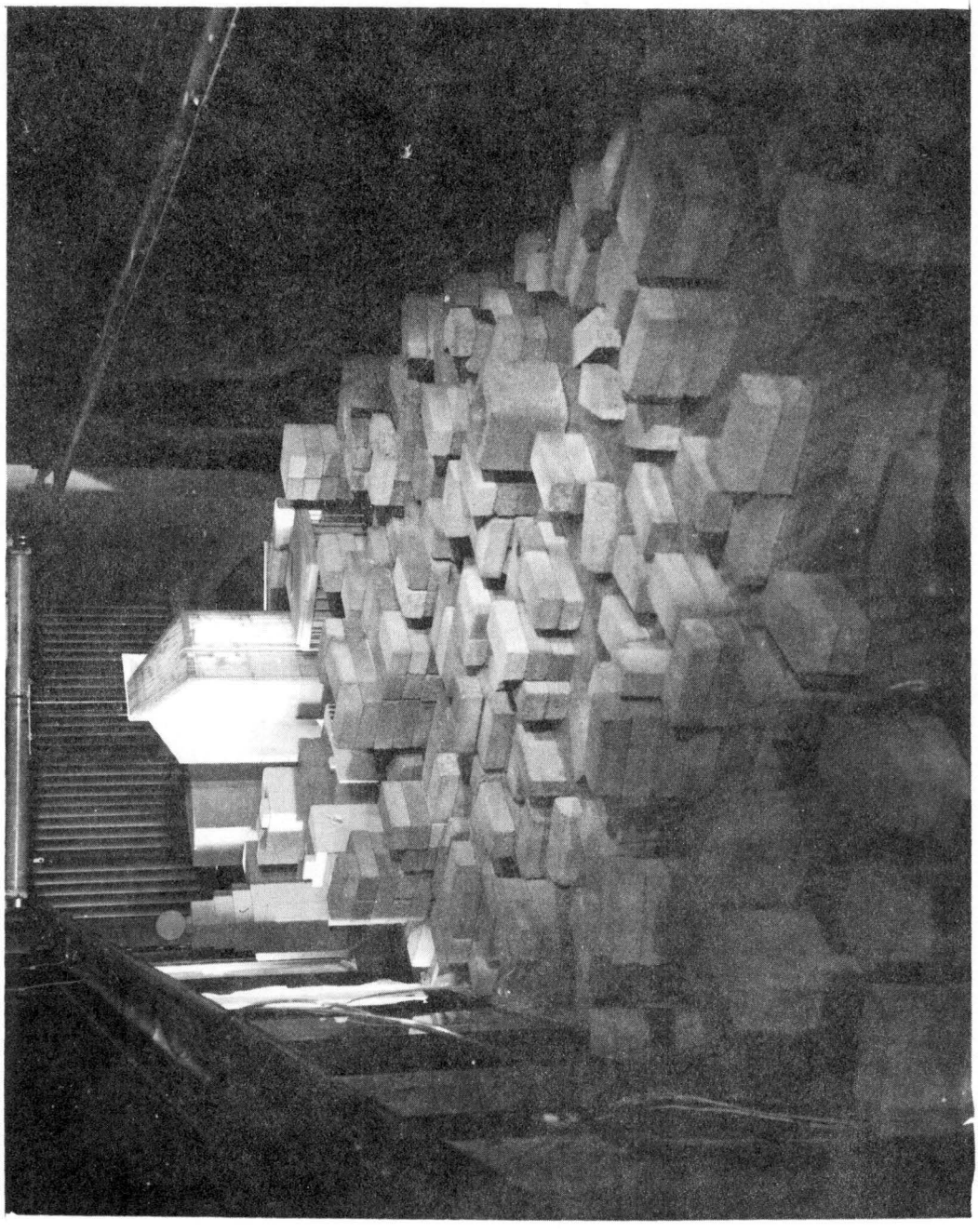

Figure 4. Photograph of city model in the wind tunnel.

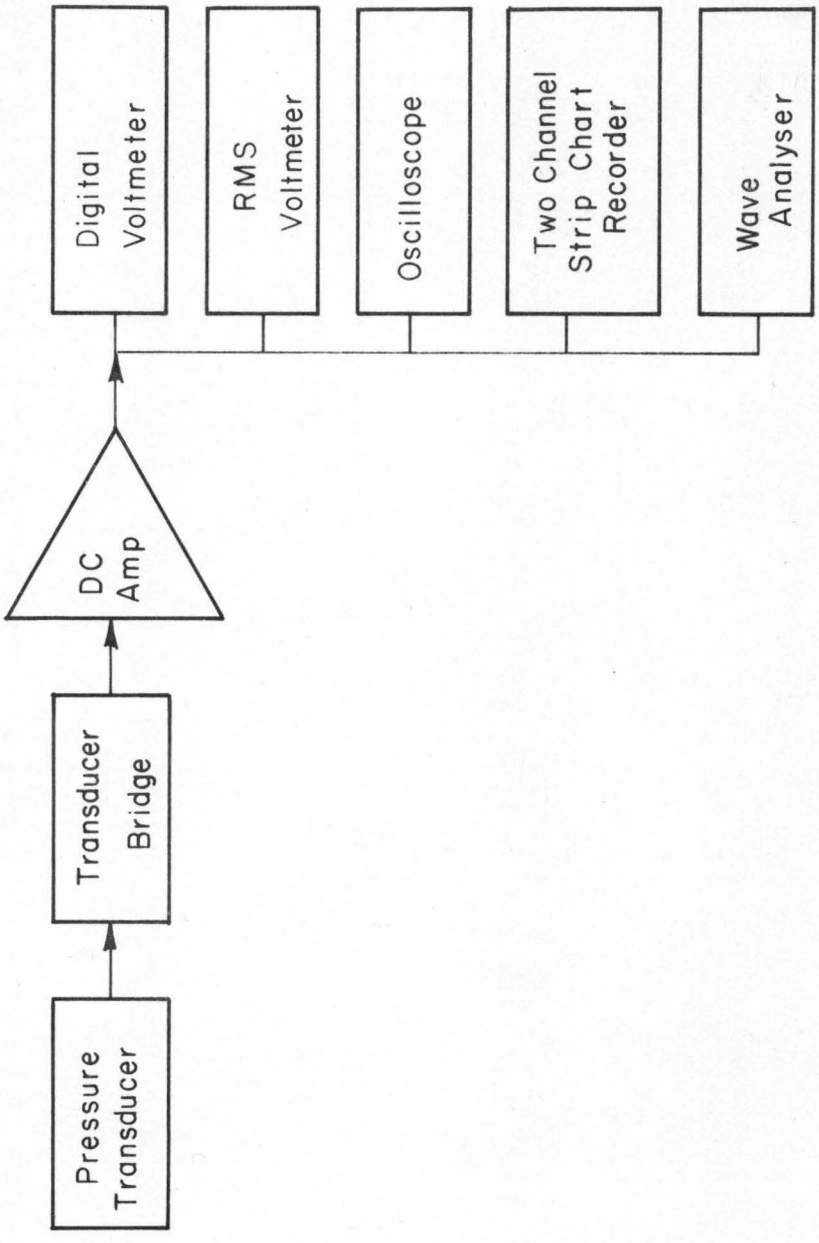

Figure 5. Block diagram of fluctuating pressure instrumentation.

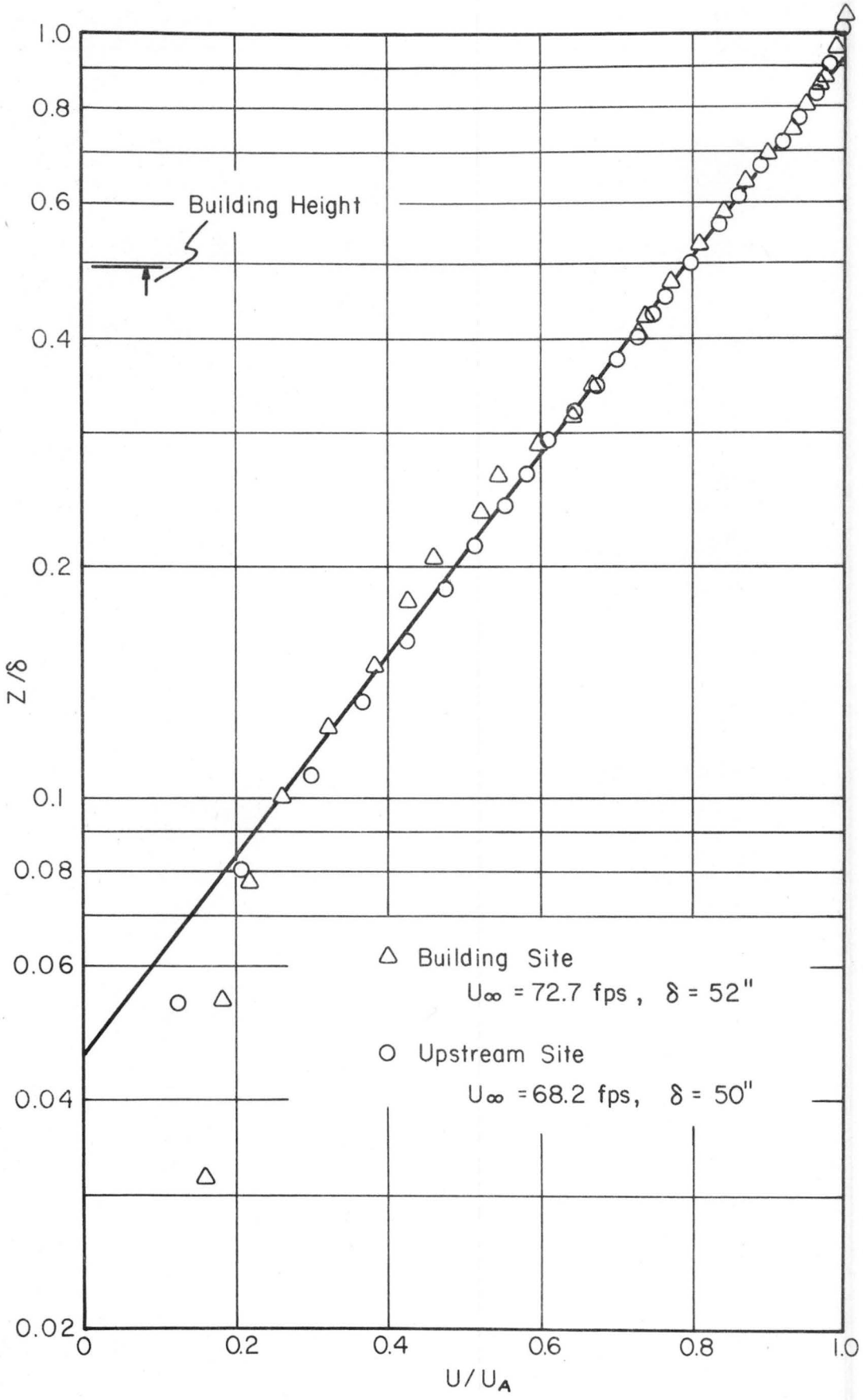

Figure 6. Mean velocity profiles.

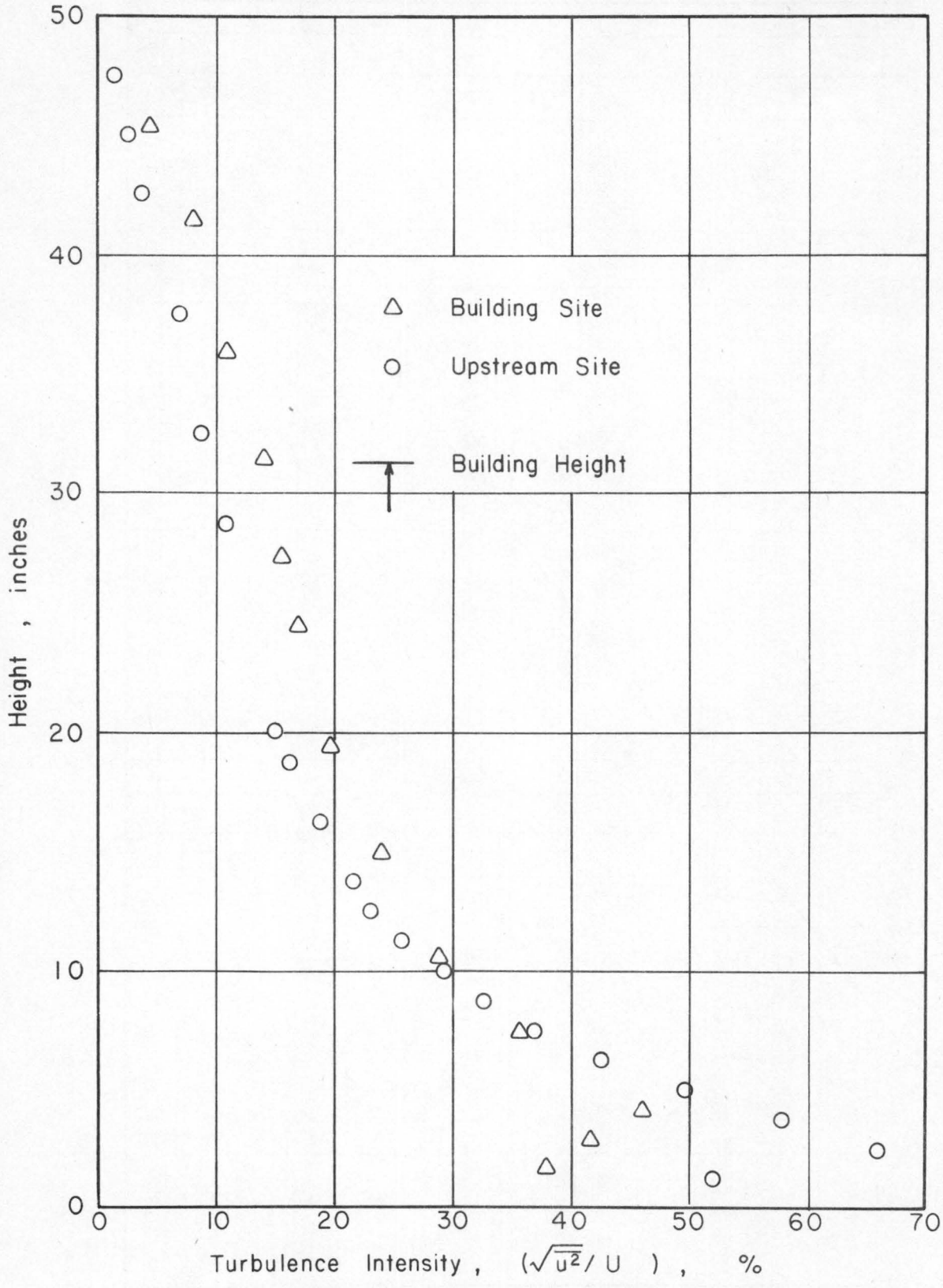

Figure 7. Turbulence intensity profiles.

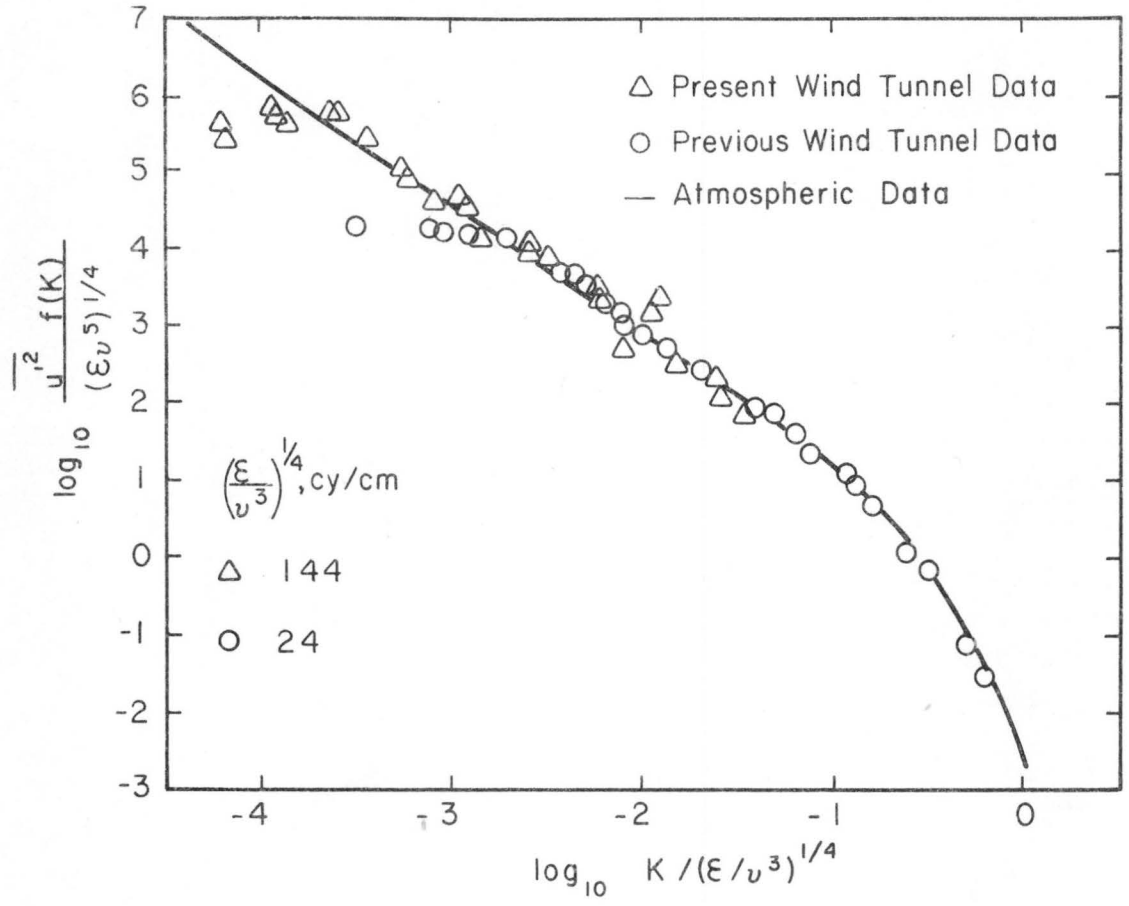

Figure 8. Comparison of velocity power spectra with previous wind-tunnel and field data.

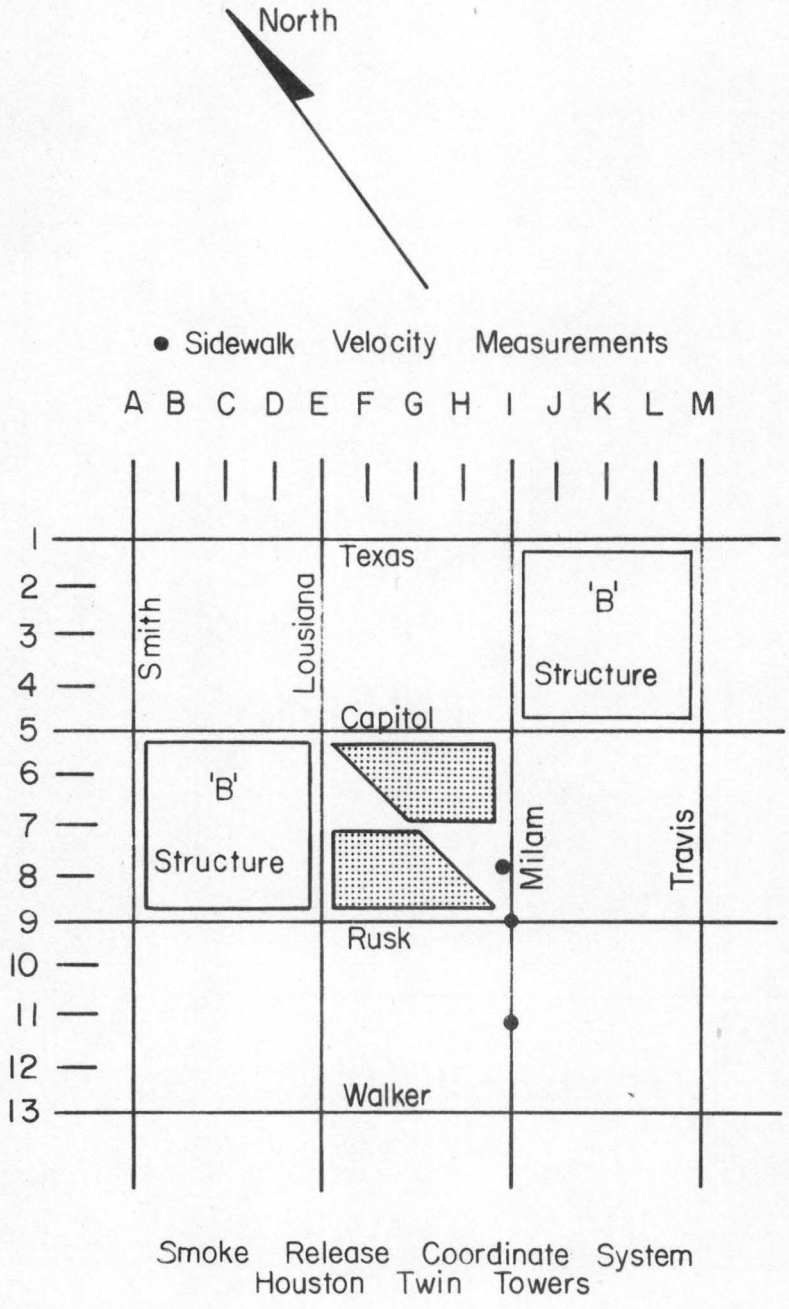

Figure 9. Smoke release coordinate system.

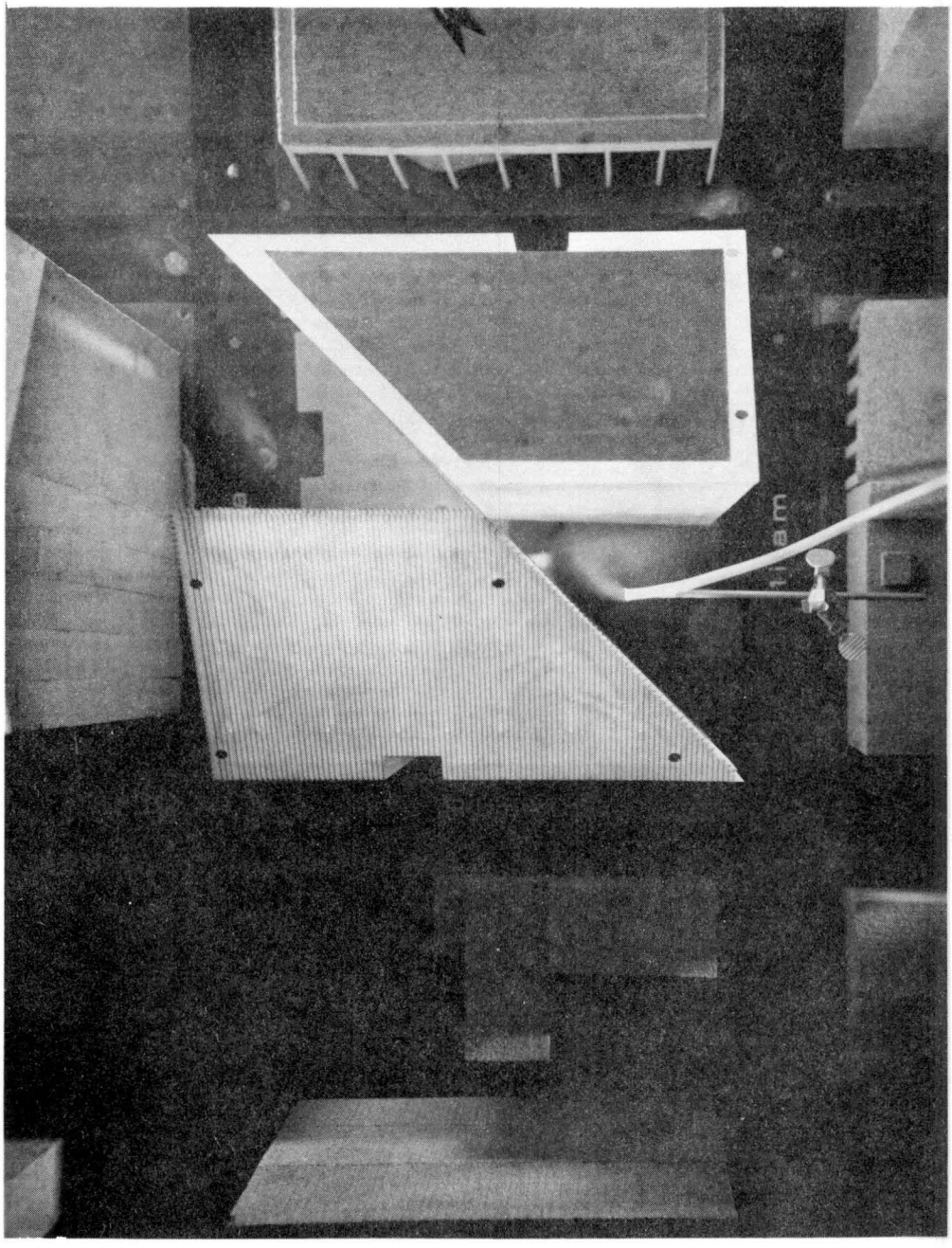

Figure 10. Vortex visualization by smoke flow.

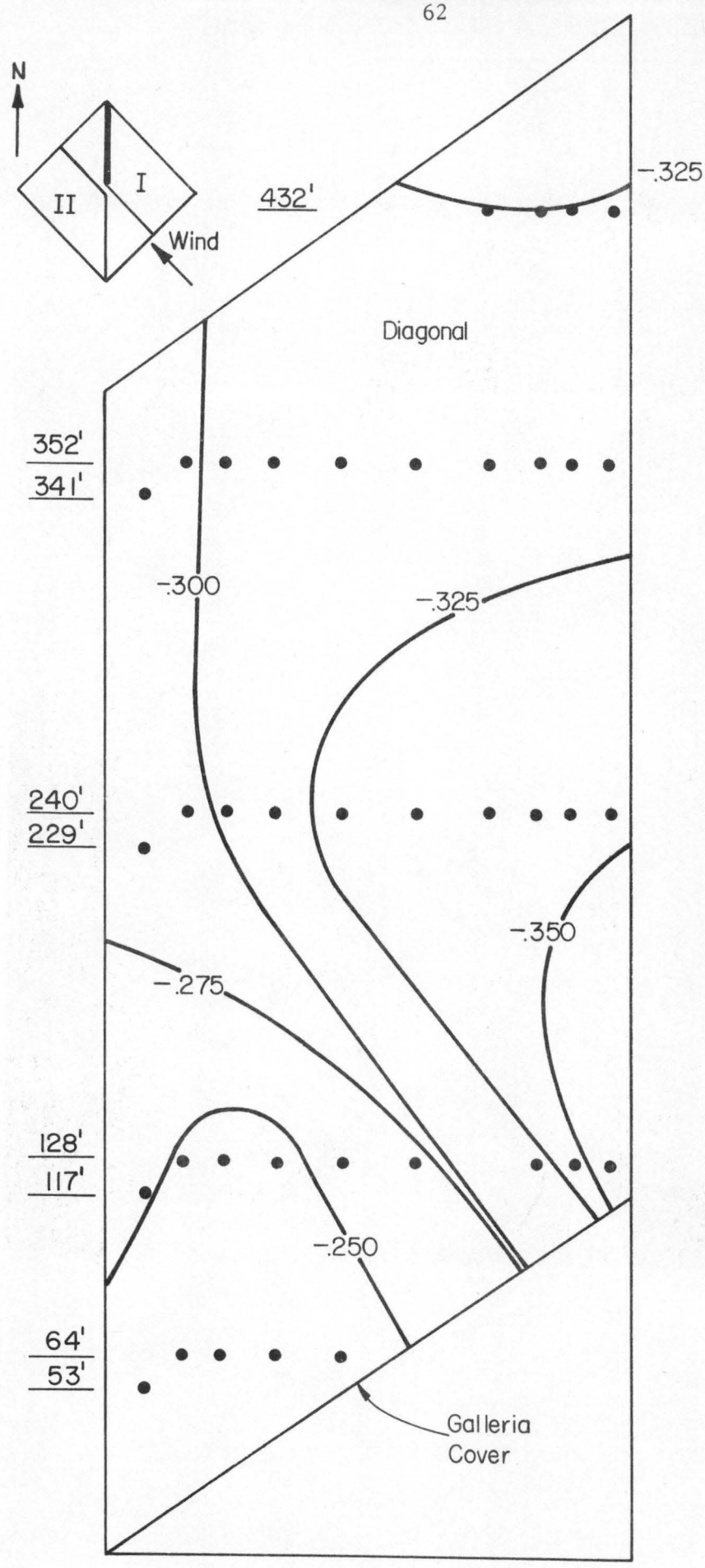

Figure 11a. Pressure contours on Building I for 120° azimuth wind.

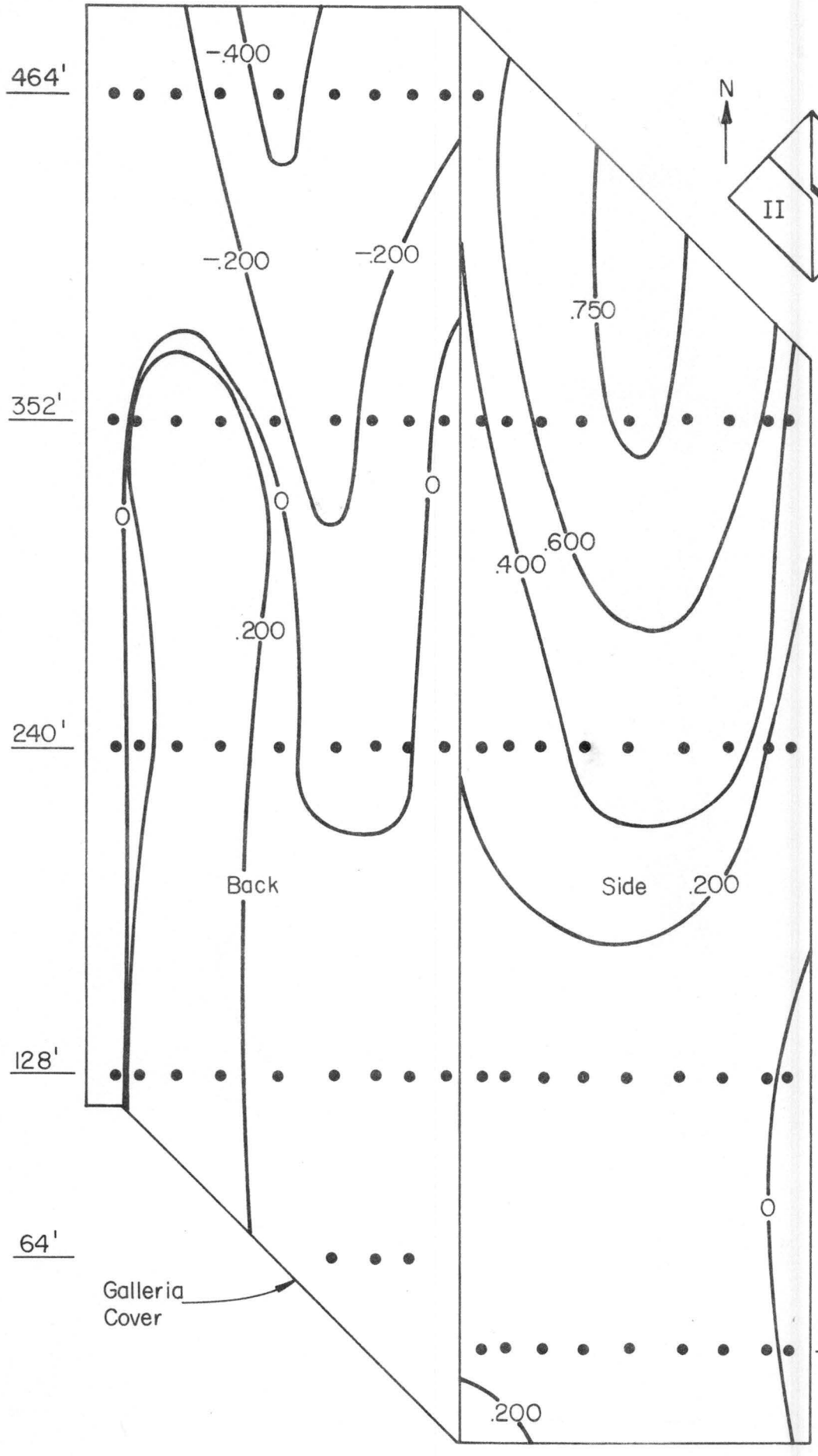

Figure 11b. Pressure contours on Building I for 120° azimuth wind.

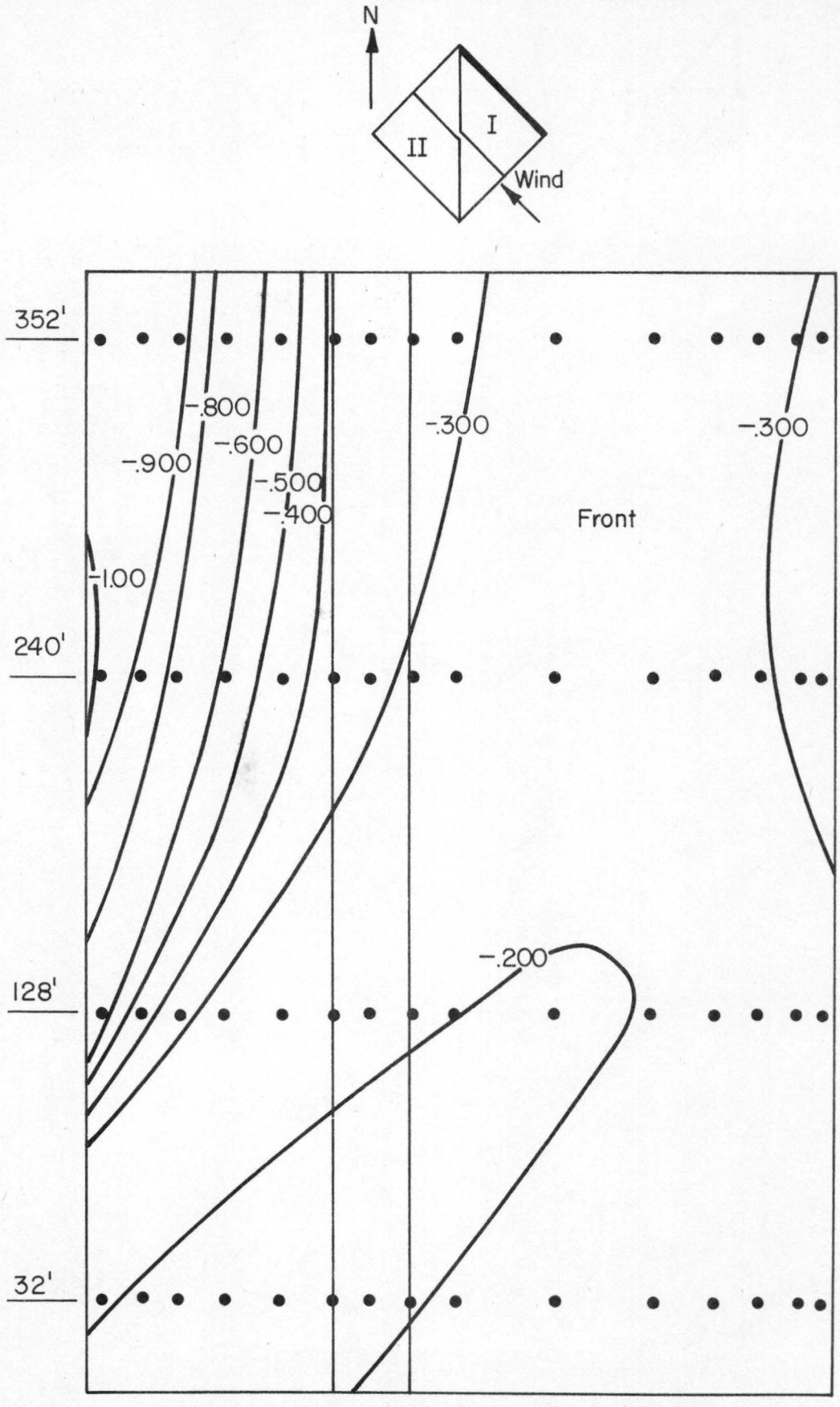

Figure 11c. Pressure contours on Building I for 120° azimuth wind.

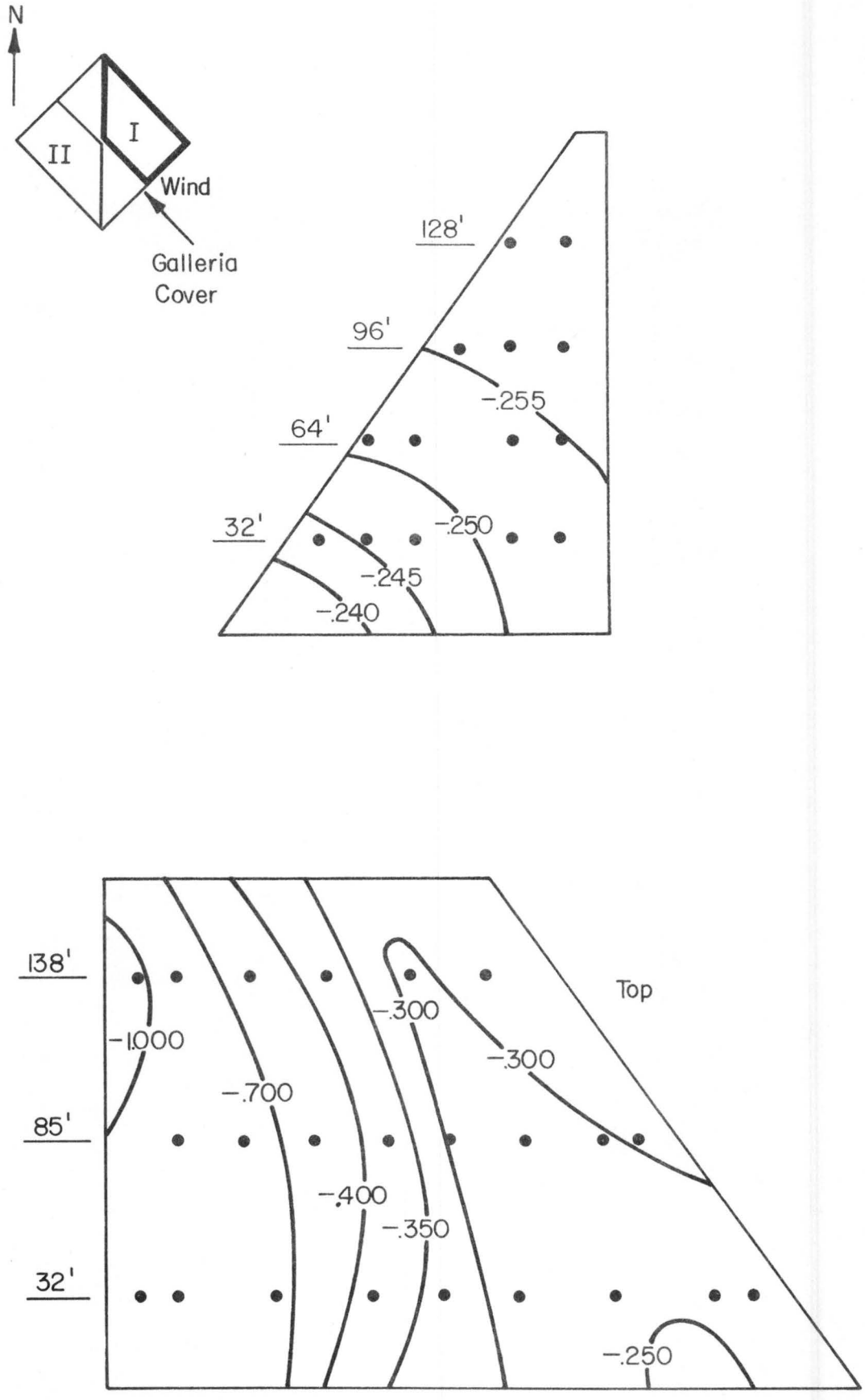

Figure 11d. Pressure contours on Building I for 120° azimuth wind.

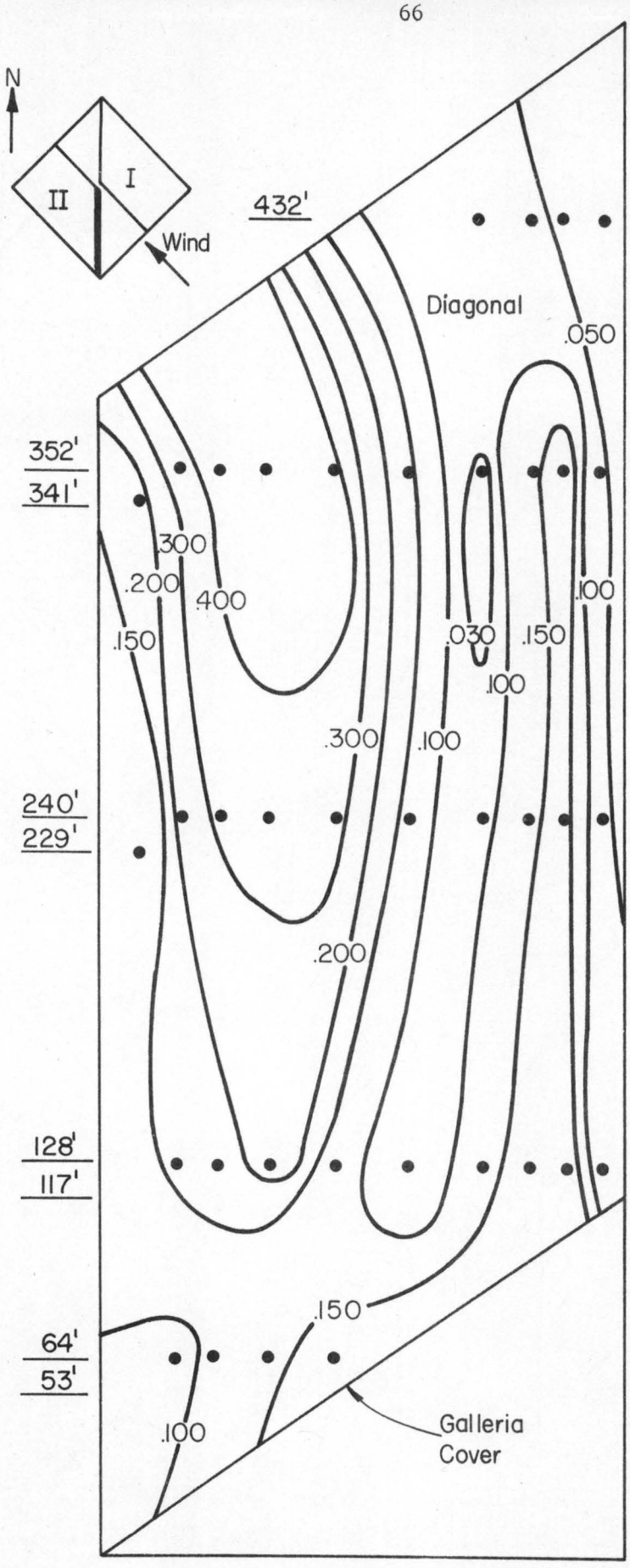

Figure 12a. Pressure contours on Building II for 120° azimuth wind.

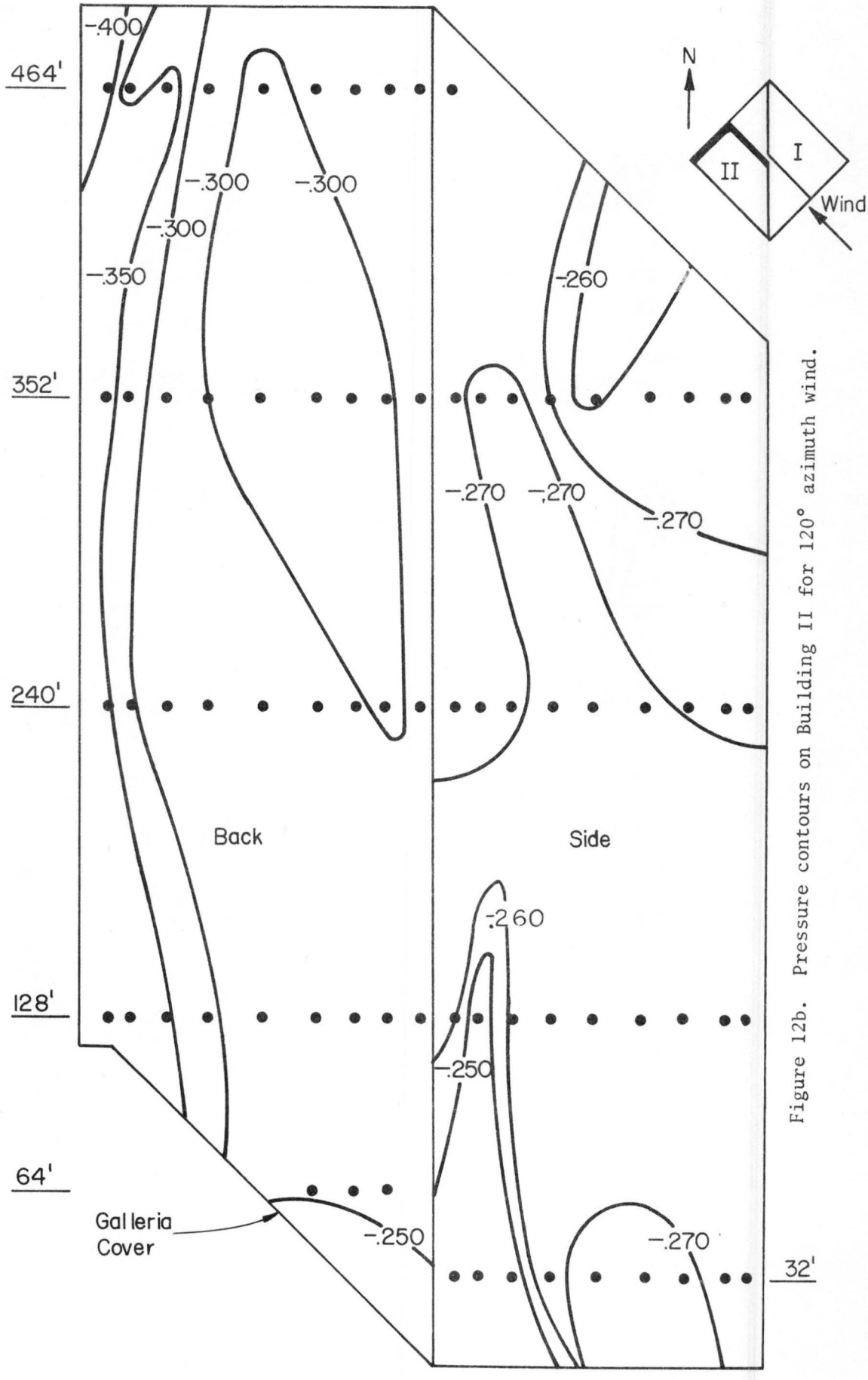

Figure 12b. Pressure contours on Building II for 120° azimuth wind.

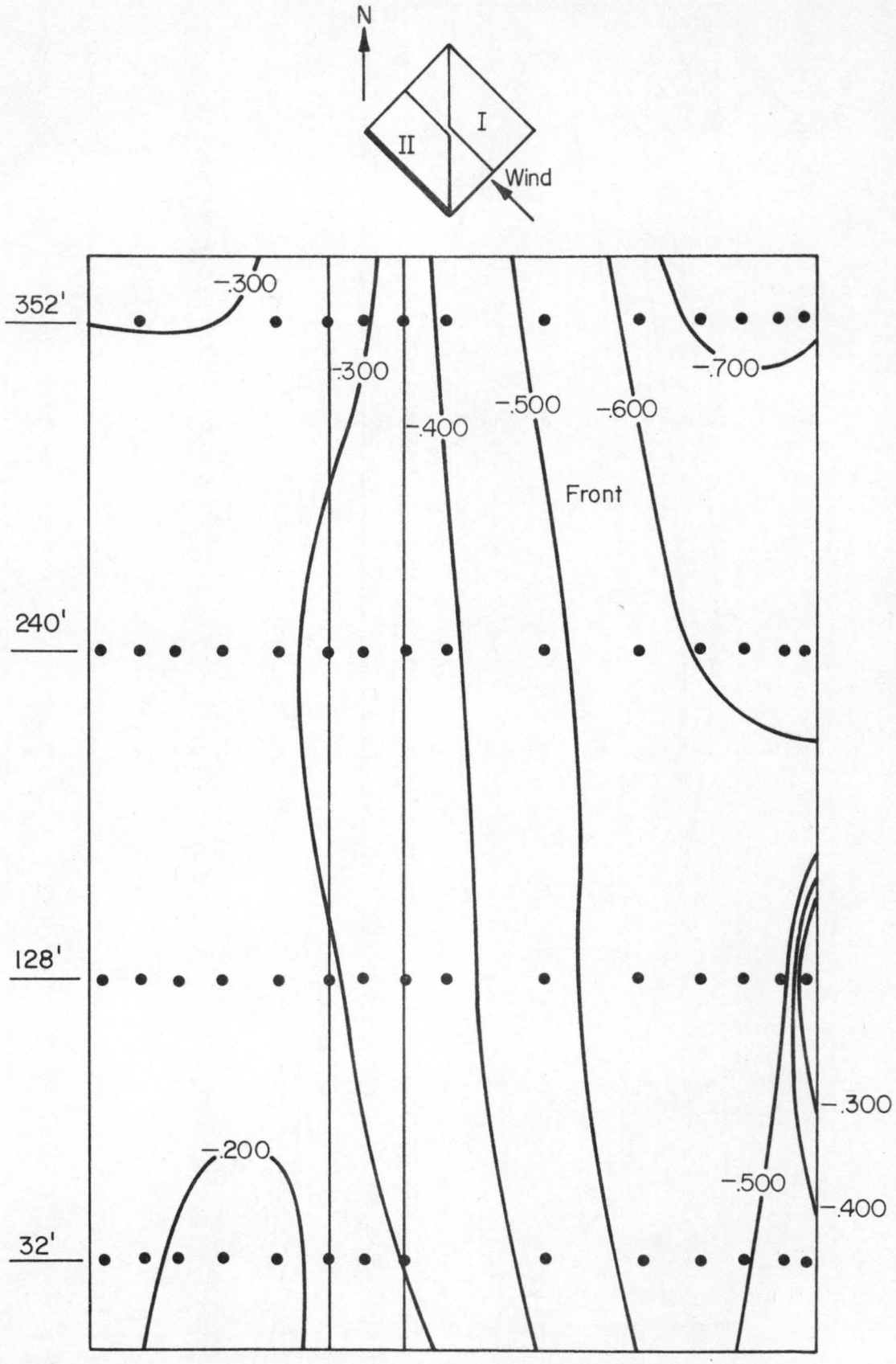

Figure 12c. Pressure contours on Building II for 120° azimuth wind.

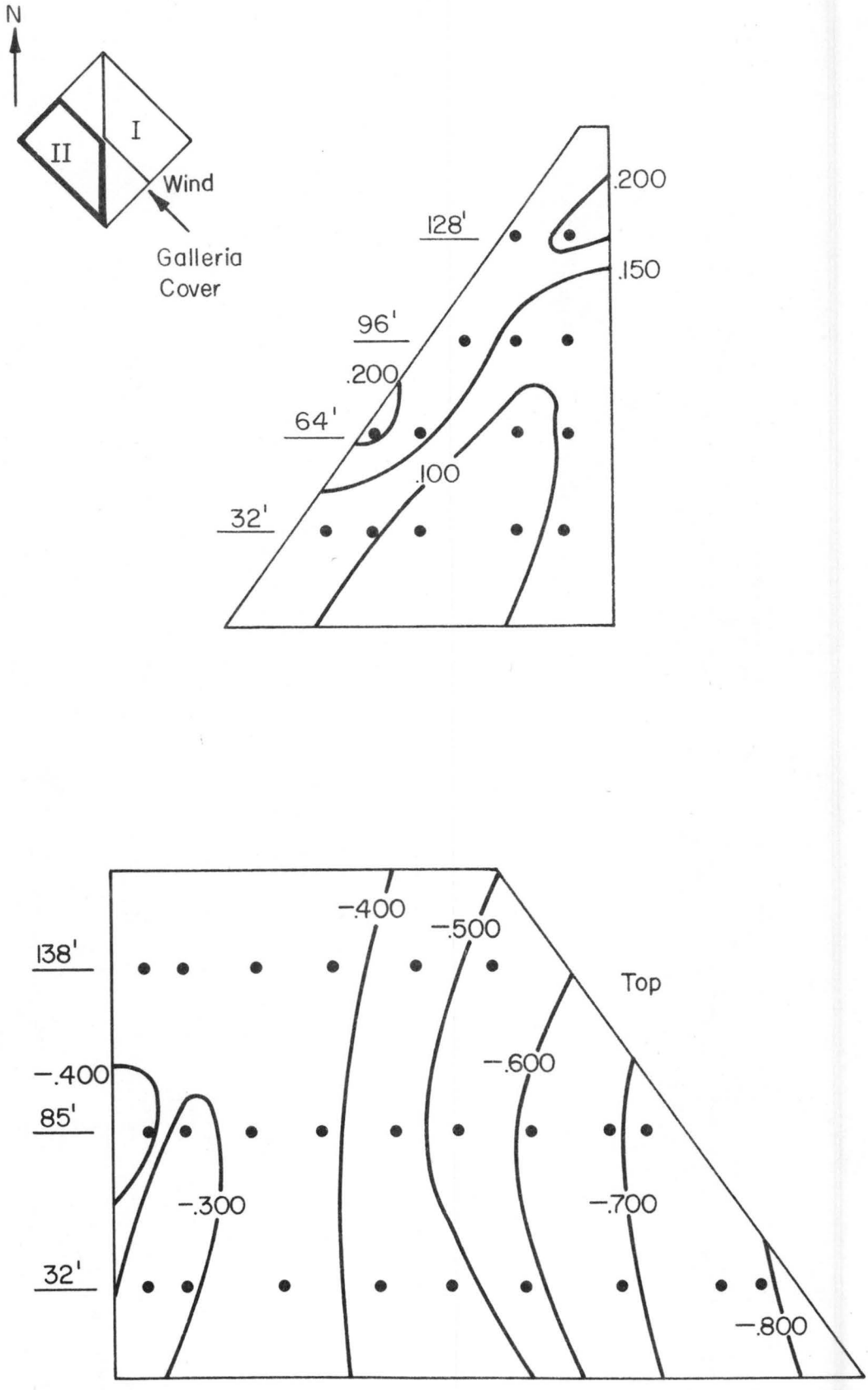

Figure 12d. Pressure contours on Building II for 120° aximuth wind.

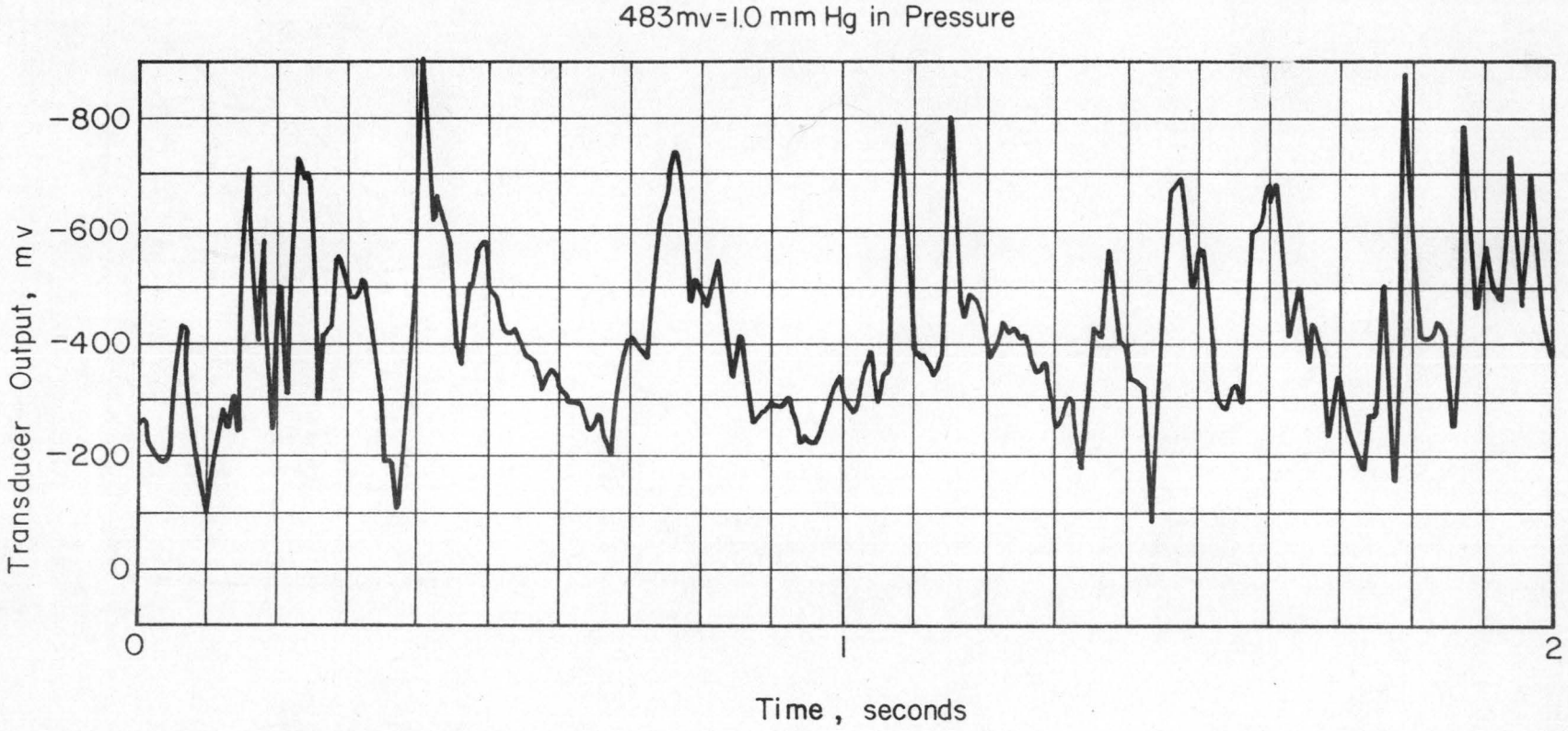

Figure 13. Pressure fluctuations at port FC 13 on Building II for 120° wind azimuth.